





Class TA545

Book D27

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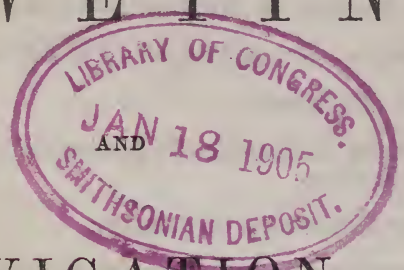
*Julius S. Sully*

ELEMENTS

526.9

OF

SURVEYING,



590  
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NAVIGATION,

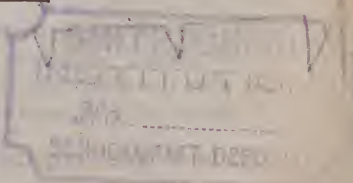
WITH DESCRIPTIONS OF THE INSTRUMENTS AND THE  
NECESSARY TABLES.

BY CHARLES DAVIES, LL. D.,

AUTHOR OF ARITHMETIC, ALGEBRA, PRACTICAL MATHEMATICS FOR PRACTICAL MEN,  
ELEMENTS OF DESCRIPTIVE GEOMETRY, SHADES, SHADOWS, AND PER-  
SPECTIVE, ANALYTICAL GEOMETRY, DIFFERENTIAL AND  
INTEGRAL CALCULUS.

REVISED EDITION.

*Handwritten signature*



NEW YORK:  
PUBLISHED BY A. S. BARNES & CO.,  
No. 51 JOHN-STREET.

CINCINNATI: H. W. DERBY & CO.,  
1853.

DAVIES'  
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TA 545

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## P R E F A C E .

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THE Elements of Surveying, first published in 1830, was designed as a text-book for the pupils of the Military Academy, and in its preparation little regard was had to the supposed wants of other institutions.

The work, however, was received by the public with more favor than was anticipated, and soon became a leading text-book in the Colleges, the Academies, and the higher grade of Schools.

For the purpose of adapting it, more fully, to the supposed wants of these institutions many changes have been made, since its first publication, and the present edition will be found to differ, in many respects, from those which have preceded.

It has been the intention to begin with the very elements of the subject, and to combine those elements in the simplest manner, so as to render the higher branches of plane surveying comparatively easy. All the instruments needed for plotting have been carefully described; and the uses of those required for the measurement of angles are fully explained.

The conventional signs adopted by the Topographical Bureau, which are now used by the United States Engineers in all their Charts and Maps, are given in plates 5 and 6.

Should these signs be generally adopted in the country, it would give entire uniformity to all maps and delineations of the ground, and would establish a kind of language by which all the peculiarities of soil and surface could be accurately represented.

A section has also been added on Geodesy. This branch of Surveying is extensively applied in the Coast Survey, and now forms an important element of a practical or scientific education.

A full account is also given of the manner of surveying the public lands; and, although the method is simple, it has, nevertheless, been productive of great results, by defining, with mathematical precision, the boundaries of lands in the new States, and thus settling their titles on an indisputable basis.

This method was originated by Col. Jared Mansfield, whose great acquirements in science introduced him to the notice of President Jefferson, by whom he was appointed surveyor-general of the North-Western Territory.

May it be permitted to one of his pupils, and a graduate of the Military Academy, further to add, that at the organization of the institution in 1812, he was appointed Professor of Natural and Experimental Philosophy. This situation he filled for sixteen years, when he withdrew from the Academy to spend the evening of his life in retirement and study. His pupils, who had listened to his instructions with delight, who honored his learning and wisdom, and had been brought near to him by his kind and simple manners, have placed his portrait in the public library, that the institution might possess an enduring memorial of one of its brightest ornaments and distinguished benefactors.

At the solicitation of several distinguished teachers, there is added, in the present edition, an article on Plane Sailing, most of which has been taken, by permission of the author, from an excellent work on Trigonometry and its applications, by Professor Charles W. Hackley.

FISHKILL LANDING, }  
 July, 1851. }

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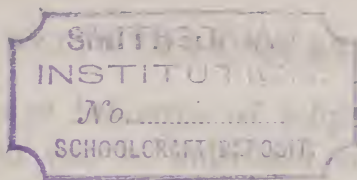
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# ELEMENTS OF SURVEYING.

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## B O O K I.

### SECTION I.

#### OF LOGARITHMS.

1. *The logarithm of a number is the exponent of the power to which it is necessary to raise a fixed number, in order to produce the first number.*

This fixed number is called the *base* of the system, and may be any number except 1: in the common system, 10 is assumed as the base.

2. If we form those powers of 10, which are denoted by entire exponents, we shall have

$$\begin{aligned} 10^0 = 1 & \quad 10^1 = 10, & \quad 10^3 = 1000 \\ & \quad 10^2 = 100, & \quad 10^4 = 10000, \text{ \&c., \&c.,} \end{aligned}$$

From the above table, it is plain, that 0, 1, 2, 3, 4, &c., are respectively the logarithms of 1, 10, 100, 1000, 10000, &c.; we also see, that the logarithm of any number between 1 and 10, is greater than 0 and less than 1: thus,

$$\log 2 = 0.301030.$$

The logarithm of any number greater than 10, and less than 100, is greater than 1 and less than 2: thus,

$$\log 50 = 1.698970.$$

The logarithm of any number greater than 100, and less than 1000, is greater than 2 and less than 3: thus,

$$\log 126 = 2.100371, \text{ \&c.}$$

If the above principles be extended to other numbers, it will appear, that the logarithm of any number, not an exact power of ten, is made up of two parts, *an entire* and a *decimal part*. The *entire part* is called the *characteristic of the logarithm*, and is always *one less* than the number of places of figures in the given number.

3. The principal use of logarithms, is to abridge numerical computations.

Let  $M$  denote any number, and let its logarithm be denoted by  $m$ ; also let  $N$  denote a second number whose logarithm is  $n$ ; then, from the definition, we shall have,

$$10^m = M \quad (1) \qquad 10^n = N \quad (2).$$

Multiplying equations (1) and (2), member by member, we have,

$$10^{m+n} = M \times N \quad \text{or, } m + n = \log(M \times N); \quad \text{hence,}$$

*The sum of the logarithms of any two numbers is equal to the logarithm of their product.*

4. Dividing equation (1) by equation (2), member by member, we have,

$$10^{m-n} = \frac{M}{N} \quad \text{or, } m - n = \log \frac{M}{N}; \quad \text{hence,}$$

*The logarithm of the quotient of two numbers, is equal to the logarithm of the dividend diminished by the logarithm of the divisor.*

5. Since the logarithm of 10 is 1, *the logarithm of the product of any number by 10, will be greater by 1 than the logarithm of that number*; also, *the logarithm of the quotient of any number divided by 10, will be less by 1 than the logarithm of that number.*

Similarly, it may be shown that if any number be multiplied by one hundred, the logarithm of the product will be greater by 2 than the logarithm of that number; and if any number be divided by one hundred, the logarithm of the quotient will be less by 2 than the logarithm of that number, and so on.



## EXAMPLES.

log 327	is	2.514548
log 32.7	“	1.514548
log 3.27	“	0.514548
log .327	“	$\bar{1}.514548$
log .0327	“	$\bar{2}.514548$

From the above examples, we see, that in a number composed of an entire and decimal part, we may change the place of the decimal point without changing the decimal part of the logarithm; but *the characteristic is diminished by 1 for every place that the decimal point is removed to the left.*

In the logarithm of a decimal, the *characteristic* becomes negative, and is numerically 1 greater than the number of ciphers immediately after the decimal point. The negative sign extends only to the characteristic, and is written over it, as in the examples given above.

## TABLE OF LOGARITHMS.

6. A table of logarithms, is a table in which are written the logarithms of all numbers between 1 and some given number. The logarithms of all numbers between 1 and 10,000 are given in the annexed table. Since rules have been given for determining the characteristics of logarithms by simple inspection, it has not been deemed necessary to write them in the table, the decimal part only being given. The characteristic, however, is given for all numbers less than 100.

The left hand column of each page of the table, is the column of numbers, and is designated by the letter N; the logarithms of these numbers are placed opposite them on the same horizontal line. The last column on each page, headed D, shows the difference between the logarithms of two consecutive numbers. This difference is found by subtracting the logarithm under the column headed 4, from the one in the column headed 5 in the same horizontal line, and is nearly a mean of the differences of any two consecutive logarithms on this line.

*To find, from the table, the logarithm of any number.*

7. If the number is less than 100, look on the first page of the table, in the column of numbers under N, until the number is found: the number opposite is the logarithm sought: Thus,

$$\log 9 = 0.954243.$$

*When the number is greater than 100 and less than 10000.*

8. Find in the column of numbers, the first three figures of the given number. Then pass across the page along a horizontal line until you come into the column under the fourth figure of the given number: at this place, there are four figures of the required logarithm, to which two figures taken from the column marked 0, are to be prefixed.

If the four figures already found stand opposite a row of six figures in the column marked 0, the two left hand figures of the six, are the two to be prefixed; but if they stand opposite a row of only four figures, you ascend the column till you find a row of six figures; the two left hand figures of this row are the two to be prefixed. If you prefix to the decimal part thus found, the characteristic, you will have the logarithm sought: Thus,

$$\log 8979 = 3.953228$$

$$\log .08979 = \bar{2}.953228$$

If, however, in passing back from the four figures found, to the 0 column, any dots be met with, the two figures to be prefixed must be taken from the horizontal line directly below: Thus,

$$\log 3098 = 3.491081$$

$$\log 30.98 = 1.491081$$

If the logarithm falls at a place where the dots occur 0 must be written for each dot, and the two figures to be prefixed are, as before, taken from the line below: Thus,

$$\log 2188 = 3.340047$$

$$\log .2188 = \bar{1}.340047$$

*When the number exceeds 10,000.*

9. The characteristic is determined by the rules already given. To find the decimal part of the logarithm: place a decimal point after the fourth figure from the left hand, converting the given number into a whole number and decimal. Find the logarithm of the entire part by the rule just given, then take from the right hand column of the page, under D, the number on the same horizontal line with the logarithm, and multiply it by the decimal part; add the product thus obtained to the logarithm already found, and the sum will be the logarithm sought.

If, in multiplying the number taken from the column D, the decimal part of the product exceeds .5, let 1 be added to the entire part; if it is less than .5, the decimal part of the product is neglected.

#### EXAMPLE.

1. To find the logarithm of the number 672887.

The characteristic is 5.; placing a decimal point after the fourth figure from the left, we have 6728.87. The decimal part of the log 6728 is .827886, and the corresponding number in the column D is 65; then  $65 \times .87 = 56.55$ , and since the decimal part exceeds .5, we have 57 to be added to .827886, which gives .827943.

Hence,  $\log 672887 = 5.827943$

Similarly,  $\log .0672887 = \bar{2}.827943$

The last rule has been deduced under the supposition that the difference of the numbers is proportional to the difference of their logarithms, which is sufficiently exact within the narrow limits considered.

In the above example, 65 is the difference between the logarithm of 672900 and the logarithm of 672800, that is, it is the difference between the logarithms of two numbers which differ by 100.

We have then the proportion

$$100 : 87 :: 65 : 56.55,$$

Hence, 56.55 is the number to be added to the logarithm before found.

To find from the table the number corresponding to a given logarithm.

10. Search in the columns of logarithms for the decimal part of the given logarithm: if it cannot be found in the table, take out the number corresponding to the next less logarithm and set it aside. Subtract this less logarithm from the given logarithm, and annex to the remainder as many zeros as may be necessary, and divide this result by the corresponding number taken from the column marked D, continuing the division as long as desirable: annex the quotient to the number set aside. Point off, from the left hand, as many integer figures as there are units in the characteristic of the given logarithm increased by 1; the result is the required number.

If the characteristic is negative, the number will be entirely decimal, and the number of zeros to be placed at the left of the number found from the table, will be equal to the number of units in the characteristic diminished by 1.

This rule, like its converse, is founded on the supposition that the difference of the logarithms is proportional to the difference of their numbers within narrow limits.

#### EXAMPLE.

1. Find the number corresponding to the logarithm 3.233568.

The decimal part of the given logarithm is .233568  
 The next less logarithm of the table is .233504,  
 and its corresponding number 1712.

Their difference is . . . . . 64

Tabular difference . . . . . 253)6400000(25

Hence, the number sought . . . . . 1712.25.

The number corresponding to the logarithm  $\bar{3}.233568$  is .00171225.

2. What is the number corresponding to the logarithm  $\bar{2}.785407$ ?  
*Ans.* .06101084.

3. What is the number corresponding to the logarithm  $\bar{1}.846741$ ?  
*Ans.* .702653.

## MULTIPLICATION BY LOGARITHMS.

11. When it is required to multiply numbers by means of their logarithms, we first find from the table the logarithms of the numbers to be multiplied; we next add these logarithms together, and their sum is the logarithm of the product of the numbers (Art. 3).

The term *sum* is to be understood in its algebraic sense; therefore, if any of the logarithms have negative characteristics, the difference between their sum and that of the positive characteristics, is to be taken; the sign of the remainder is that of the greater sum.

## EXAMPLES.

1. Multiply 23.14 by 5.062.

$$\log 23.14 = 1.364363$$

$$\log 5.062 = 0.704322$$

$$\text{Product, } 117.1347 \dots \underline{\underline{2.068685}}$$

2. Multiply 3.902, 597.16, and 0.0314728 together.

$$\log 3.902 = 0.591287$$

$$\log 597.16 = 2.776091$$

$$\log 0.0314728 = \bar{2}.497936$$

$$\text{Product, } 73.3354 \dots \underline{\underline{1.865314}}$$

Here, the  $\bar{2}$  cancels the  $+ 2$ , and the 1 carried from the decimal part is set down.

3. Multiply 3.586, 2.1046, 0.8372, and 0.0294 together.

$$\log 3.586 = 0.554610$$

$$\log 2.1046 = 0.323170$$

$$\log 0.8372 = \bar{1}.922829$$

$$\log 0.0294 = \bar{2}.468347$$

$$\text{Product, } 0.1857615 \dots \underline{\underline{1.268956}}$$

In this example the 2, carried from the decimal part, cancels  $\bar{2}$ , and there remains  $\bar{1}$  to be set down.

## DIVISION OF NUMBERS BY LOGARITHMS.

12. When it is required to divide numbers by means of their logarithms, we have only to recollect, that the subtraction of logarithms corresponds to the division of their numbers (Art. 4). Hence, if we find the logarithm of the dividend, and from it subtract the logarithm of the divisor, the remainder will be the logarithm of the quotient.

This additional caution may be added. The difference of the logarithms, as here used, means the *algebraic difference*; so that, if the logarithm of the divisor have a negative characteristic, its sign must be changed to positive, after diminishing it by the unit, if any, carried in the subtraction from the decimal part of the logarithm. Or, if the characteristic of the logarithm of the dividend is negative, it must be treated as a negative number.

## EXAMPLES.

1. To divide 24163 by 4567.

$$\begin{array}{r} \log 24163 = 4.383151 \\ \log 4567 = 3.659631 \\ \hline \text{Quotient, } 5.29078 \quad . \quad . \quad \underline{0.723520} \end{array}$$

2. To divide 0.06314 by .007241.

$$\begin{array}{r} \log 0.06314 = \bar{2}.800305 \\ \log 0.007241 = \bar{3}.859799 \\ \hline \text{Quotient, } 8.7198 \quad . \quad . \quad \underline{0.940506} \end{array}$$

Here, 1 carried from the decimal part to the  $\bar{3}$ , changes it to  $\bar{2}$ , which being taken from  $\bar{2}$ , leaves 0 for the characteristic.

3. To divide 37.149 by 523.76.

$$\begin{array}{r} \log 37.149 = 1.569947 \\ \log 523.76 = 2.719133 \\ \hline \text{Quotient, } 0.0709274 \quad . \quad \underline{\bar{2}.850814} \end{array}$$

4. To divide 0.7438 by 12.9476.

$$\log 0.7438 = \bar{1}.871456$$

$$\log 12.9476 = 1.112189$$

$$\text{Quotient,} \quad 0.057447 \dots \underline{\underline{2.759267}}$$

Here, the 1 taken from  $\bar{1}$ , gives  $\bar{2}$  for a result, as set down.

#### ARITHMETICAL COMPLEMENT.

13. The *Arithmetical complement* of a logarithm is the number which remains after subtracting the logarithm from 10.

Thus,  $10 - 9.274687 = 0.725313.$

Hence, 0.725313 is the arithmetical complement of 9.274687.

14. We will now show that, *the difference between two logarithms is truly found, by adding to the first logarithm the arithmetical complement of the logarithm to be subtracted, and then diminishing the sum by 10.*

Let  $a$  = the first logarithm,  
 $b$  = the logarithm to be subtracted,  
 and  $c = 10 - b$  = the arithmetical complement of  $b$ .

Now the difference between the two logarithms will be expressed by  $a - b$ .

But, from the equation  $c = 10 - b$ , we have

$$c - 10 = -b,$$

hence, if we place for  $-b$  its value, we shall have

$$a - b = a + c - 10,$$

which agrees with the enunciation.

When we wish the arithmetical complement of a logarithm, we may write it directly from the table, *by subtracting the left hand figure from 9, then proceeding to the right, subtract each figure from 9 till we reach the last significant figure, which must be taken from 10: this will be the same as taking the logarithm from 10.*

## EXAMPLES.

1. From 3.274107 take 2.104729.

*By common method.*

3.274107

2.104729Diff. 1.169378

its ar. comp.

*By arith. comp.*

3.274107

7.895271Sum 1.169378 after sub-

tracting 10.

Hence, to perform division by means of the arithmetical complement, we have the following

## RULE.

*To the logarithm of the dividend add the arithmetical complement of the logarithm of the divisor: the sum, after subtracting 10, will be the logarithm of the quotient.*

## EXAMPLES.

1. Divide 327.5 by 22.07.

log 327.5 . . . . . 2.515211

log 22.07 ar. comp. 8.656198Quotient, 14.839 . . . 1.171409

2. Divide 0.7438 by 12.9476.

log 0.7438 . . . . .  $\bar{1}.871456$ log 12.9476 ar. comp. 8.887811Quotient, 0.057447 . . .  $\bar{2}.759267$ 

In this example, the sum of the characteristics is 8, from which, taking 10, the remainder is  $\bar{2}$ .

3. Divide 37.149 by 523.76.

log 37.149 . . . . . 1.569947

log 523.76 ar. comp. 7.280867Quotient, 0.0709273 . .  $\bar{2}.850814$



4. Divide 0.875 by 25. *Ans.* 0.035.  
 5. Divide 3.1416 by .944. *Ans.* 3.3279.  
 6. Divide 2756 by 327. *Ans.* 8.4281.  
 7. Divide 672859 by 0.09657. *Ans.* 6967580.64.

## SECTION II.

### GEOMETRICAL DEFINITIONS AND CONSTRUCTIONS.

1. **EXTENSION** has three dimensions, length, breadth, and thickness.

2. **GEOMETRY** is the science which has for its object:  
 1st. The measurement of extension; and 2dly. To discover, by means of such measurement, the properties and relations of geometrical figures.

3. A **POINT** is that which has place, or position, but not magnitude.

4. A **LINE** is length, without breadth or thickness.

5. A **STRAIGHT LINE** is one which lies in the same direction between any two of its points.



6. A **BROKEN LINE** is one made up of straight lines, not lying in the same direction.



7. A **CURVE LINE** is one which changes its direction at every point.



The word *line* when used alone, will designate a straight line; and the word *curve*, a curve line.

8. A **SURFACE** is that which has length and breadth without thickness.

9. A PLANE is a surface, such, that if any two of its points be joined by a straight line, such line will be wholly in the surface.

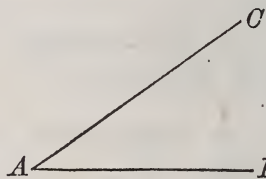
10. Every surface, which is not a plane surface, or composed of plane surfaces, is a *curved surface*.

11. A SOLID, or BODY is that which has length, breadth, and thickness: it therefore combines the three dimensions of extension.

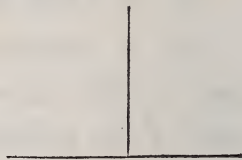
12. An ANGLE is the portion of a plane included between two straight lines which meet at a common point. The two straight lines are called the *sides* of the angle, and the common point of intersection, the *vertex*.

Thus, the part of the plane included between  $AB$  and  $AC$  is called an *angle*:  $AB$  and  $AC$  are its *sides*, and  $A$  its *vertex*.

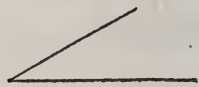
An angle is sometimes designated  $A$  simply by a letter placed at the vertex, as, the angle  $A$ ; but generally, by three letters, as, the angle  $BAC$  or  $CAB$ ,—the letter at the vertex being always placed in the middle.



13. When a straight line meets another straight line, so as to make the adjacent angles equal to each other, each angle is called a *right angle*; and the first line is said to be *perpendicular* to the second.



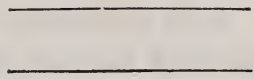
14. An ACUTE ANGLE is an angle less than a right angle.



15. An OBTUSE ANGLE is an angle greater than a right angle.



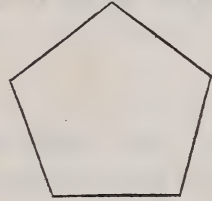
16. Two straight lines are said to be *parallel*, when being situated in the same plane, they cannot meet, how far soever, either way, both of them be produced.



17. A PLANE FIGURE is a portion of a plane terminated on all sides by lines, either straight or curved.

18. A POLYGON, or *rectilineal figure*, is a portion of a plane terminated on all sides by straight lines.

The sum of the bounding lines is called the *perimeter* of the polygon.



19. The polygon of three sides, the simplest of all, is called a *triangle*; that of four sides, a *quadrilateral*; that of five, a *pentagon*; that of six, a *hexagon*; that of seven, a *heptagon*; that of eight, an *octagon*; that of nine, an *nonagon*; that of ten, a *decagon*; and that of twelve, a *dodecagon*.

20. An EQUILATERAL polygon is one which has all its sides equal; an *equiangular* polygon, is one which has all its angles equal.

21. Two polygons are *mutually equilateral*, when they have their sides equal each to each, and placed in the same order: that is to say, when following their bounding lines in the same direction, the first side of the one is equal to the first side of the other, the second to the second, the third to the third, and so on.

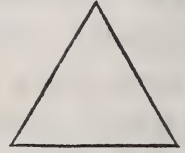
22. Two polygons are mutually *equiangular*, when every angle of the one is equal to a corresponding angle of the other, each to each.

23. Triangles are divided into classes with reference both to their sides and angles.

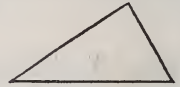
1. An *equilateral triangle* is one which has its three sides equal.



2. An *isosceles triangle* is one which has only two of its sides equal.



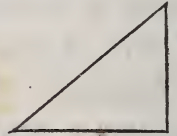
3. A *scalene triangle* is one which has its three sides unequal.



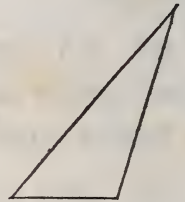
4. An *acute-angled triangle* is one which has its three angles acute.



5. A *right-angled triangle* is one which has a right angle. The side opposite the right angle is called the *hypotenuse*, and the other two sides, the *base* and *perpendicular*.



6. An *obtuse-angled triangle* is one which has an obtuse angle.



24. There are three kinds of QUADRILATERALS:

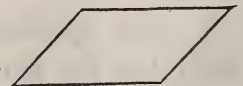
1. The *trapezium*, which has none of its sides parallel.



2. The *trapezoid*, which has only two of its sides parallel.

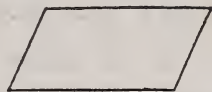


3. The *parallelogram*, which has its opposite sides parallel.



25. There are four kinds of PARALLELOGRAMS:

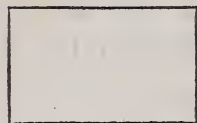
1. The *rhomboid*, which has no right angle.



2. The *rhombus*, or *lozenge*, which is an equilateral rhomboid.



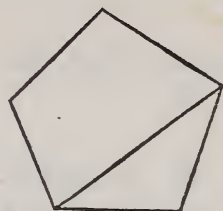
3. The *rectangle*, which is an equiangular parallelogram, but not equilateral.



4. The *square*, which is both equilateral and equiangular.



A **DIAGONAL** of a figure is a line which joins the vertices of two angles not adjacent.



#### EXPLANATION OF SIGNS.

26. The sign  $=$  is the sign of equality; thus, the expression  $A = B$ , signifies that  $A$  is equal to  $B$ .

27. To signify that  $A$  is smaller than  $B$ , the expression  $A < B$  is used.

28. To signify that  $A$  is greater than  $B$ , the expression  $A > B$  is used; the smaller quantity being always at the vertex of the angle.

29. The sign  $+$  is called *plus*; it indicates addition.

30. The sign  $-$  is called *minus*; it indicates subtraction:

Thus,  $A + B$ , represents the sum of the quantities  $A$  and  $B$ ;  $A - B$  represents their difference, or what remains after  $B$  is taken from  $A$ ; and  $A - B + C$ , or  $A + C - B$ , signifies that  $A$  and  $C$  are to be added together, and that  $B$  is to be subtracted from their sum.

31. The sign  $\times$  indicates multiplication: thus  $A \times B$  represents the product of  $A$  and  $B$ .

The expression  $A \times (B + C - D)$  represents the product of  $A$  by the quantity  $B + C - D$ . If  $A + D$  were to be multiplied by  $A - B + C$ , the product would be indicated thus;

$$(A + D) \times (A - B + C),$$

whatever is enclosed within the curved lines, being considered as a single quantity. The same thing may also be indicated by a bar: thus,

$$\overline{A + B + C} \times D,$$

denotes that the sum of  $A$ ,  $B$  and  $C$ , is to be multiplied by  $D$ .

32. A figure placed before a line, or quantity, serves as a multiplier to that line or quantity; thus,  $3AB$  signifies that the line  $AB$  is taken three times;  $\frac{1}{2}A$  signifies the half of the angle  $A$ .

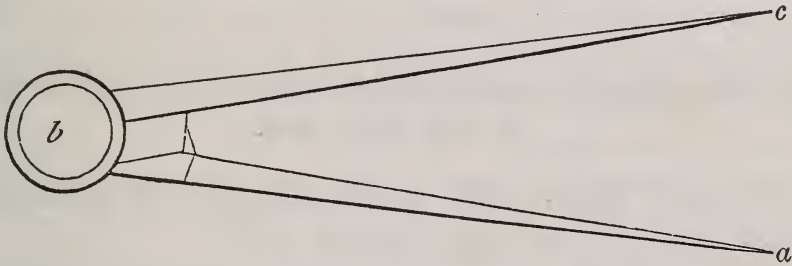
33. The square of the line  $AB$  is designated by  $\overline{AB}^2$ ; its cube by  $\overline{AB}^3$ . What is meant by the square and cube of a line is fully explained in Geometry.

34. The sign  $\sqrt{\quad}$  indicates a root to be extracted; thus,  $\sqrt{2}$  means the square-root of 2;  $\sqrt{A \times B}$  means the square-root of the product of  $A$  and  $B$ .

GEOMETRICAL CONSTRUCTIONS.

35. Before explaining the method of constructing geometrical problems, we shall describe some of the simpler instruments and their uses.

DIVIDERS.



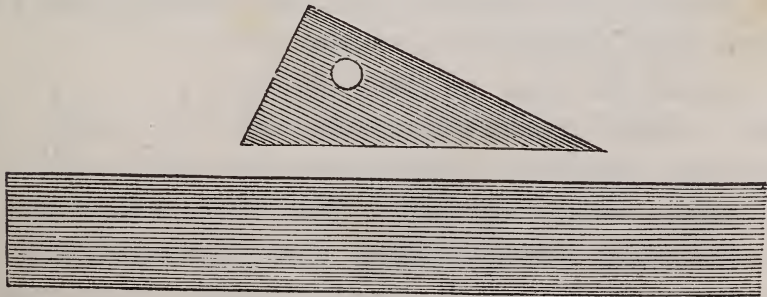
36. The dividers is the most simple and useful of the instruments used for drawing. It consists of two legs  $ba$ ,  $bc$ , which may be easily turned around a joint at  $b$ .

One of the principal uses of this instrument is to lay off on a line, a distance equal to a given line.

For example, to lay off on  $CD$  a distance equal to  $AB$ .

For this purpose, place the forefinger on the joint of the dividers, and  $A$  —————  $B$  set one foot at  $A$ : then extend, with the thumb and other fingers, the  $C$  —————  $\frac{1}{E}$  —————  $D$  other leg of the dividers, until its foot reaches the point  $B$ . Then raise the dividers, place one foot at  $C$ , and mark with the other the distance  $CE$ : this will evidently be equal to  $AB$ .

RULER AND TRIANGLE.



37. A Ruler of convenient size, is about twenty inches in length, two inches wide, and a fifth of an inch in thick-

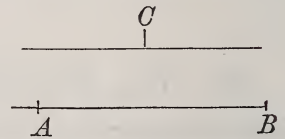
ness. It should be made of a hard material, perfectly straight and smooth.

The hypotenuse of the right-angled triangle, which is used in connection with it, should be about ten inches in length, and it is most convenient to have one of the sides considerably longer than the other. We can solve, with the ruler and triangle, the two following problems.

I. *To draw through a given point a line which shall be parallel to a given line.*

38. Let  $C$  be the given point, and  $AB$  the given line.

Place the hypotenuse of the triangle against the edge of the ruler, and then place the ruler and triangle on the paper, so that one of the sides of the triangle shall coincide exactly with  $AB$ : the triangle being below the line.

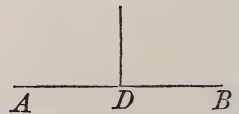


Then placing the thumb and fingers of the left hand firmly on the ruler, slide the triangle with the other hand along the ruler until the side which coincided with  $AB$  reaches the point  $C$ . Leaving the thumb of the left hand on the ruler, extend the fingers upon the triangle and hold it firmly, and with the right hand, mark with a pen or pencil, a line through  $C$ : this line will be parallel to  $AB$ .

II. *To draw through a given point a line which shall be perpendicular to a given line.*

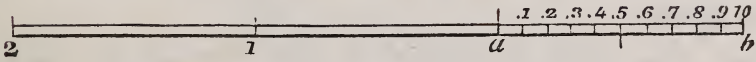
39. Let  $AB$  be the given line, and  $D$  the given point.

Place the hypotenuse of the triangle against the edge of the ruler, as before. Then place the ruler and triangle so that one of the sides of the triangle shall coincide exactly with the line  $AB$ . Then slide the triangle along the ruler until the other side reaches the point  $D$ : draw through  $D$  a right line, and it will be perpendicular to  $AB$ .





SCALE OF EQUAL PARTS.



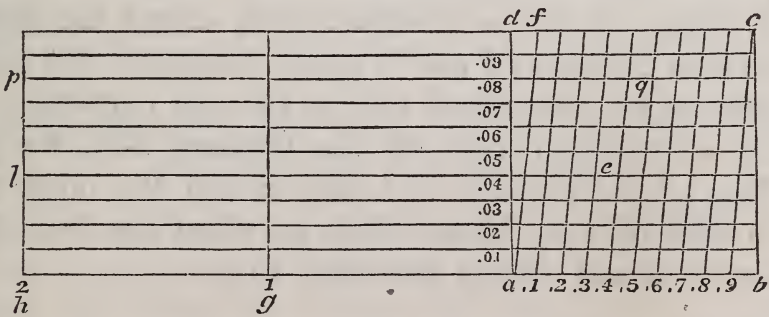
40. A scale of equal parts is formed by dividing a line of a given length into equal portions.

If, for example, the line  $ab$  of a given length, say one inch, be divided into any number of equal parts, as 10, the scale thus formed, is called a scale of ten parts to the inch. The line  $ab$ , which is divided, is called the *unit of the scale*. This unit is laid off several times on the left of the divided line, and the points marked 1, 2, 3, &c.

The unit of scales of equal parts, is, in general, either an inch, or an exact part of an inch. If, for example,  $ab$ , the unit of the scale, were half an inch, the scale would be one of 10 parts to half an inch, or of 20 parts to the inch.

If it were required to take from the scale a line equal to two inches and six-tenths, place one foot of the dividers at 2 on the left, and extend the other to .6, which marks the sixth of the small divisions: the dividers will then embrace the required distance.

DIAGONAL SCALE OF EQUAL PARTS.



41. This scale is thus constructed. Take  $ab$  for the unit of the scale, which may be one inch,  $\frac{1}{2}$ ,  $\frac{1}{4}$  or  $\frac{3}{4}$  of an inch, in length. On  $ab$  describe the square  $abcd$ . Divide the sides  $ab$  and  $dc$  each into ten equal parts. Draw  $af$  and the other nine parallels as in the figure.

Produce  $ba$  to the left, and lay off the unit of the scale any convenient number of times, and mark the points

1, 2, 3, &c. Then, divide the line  $ad$  into ten equal parts, and through the points of division draw parallels to  $ab$ , as in the figure.

Now, the small divisions of the line  $ab$  are each one-tenth (.1) of  $ab$ ; they are therefore .1 of  $ad$ , or .1 of  $ag$  or  $gh$ .

If we consider the triangle  $adf$ , we see that the base  $df$  is one-tenth of  $ad$ , the unit of the scale. Since the distance from  $a$  to the first horizontal line above  $ab$ , is one-tenth of the distance  $ad$ , it follows that the distance measured on that line between  $ad$  and  $af$  is one-tenth of  $df$ : but since one-tenth of a tenth is a hundredth, it follows that this distance is one hundredth (.01) of the unit of the scale. A like distance measured on the second line will be two hundredths (.02) of the unit of the scale; on the third, .03; on the fourth, .04, &c.

If it were required to take, in the dividers, the unit of the scale, and any number of tenths, place one foot of the dividers at 1, and extend the other to that figure between  $a$  and  $b$  which designates the tenths. If two or more units are required, the dividers must be placed on a point of division further to the left.

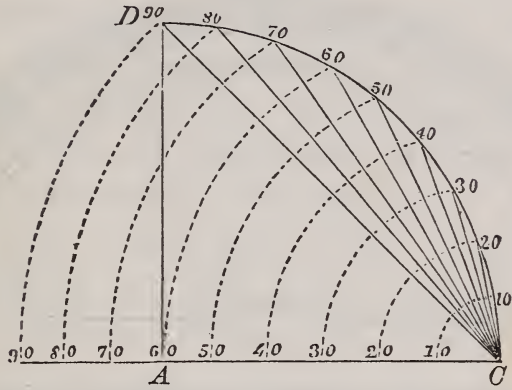
When units, tenths, and hundredths, are required, place one foot of the dividers where the vertical line through the point which designates the units, intersects the line which designates the hundredths: then, extend the dividers to that line between  $ad$  and  $bc$  which designates the tenths: the distance so determined will be the one required.

For example, to take off the distance 2.34, we place one foot of the dividers at  $l$ , and extend the other to  $e$ : and to take off the distance 2.58, we place one foot of the dividers at  $p$  and extend the other to  $q$ .

REMARK I. If a line is so long that the whole of it cannot be taken from the scale, it must be divided, and the parts of it taken from the scale in succession.

REMARK II. If a line be given upon the paper, its length can be found by taking it in the dividers and applying it to the scale.

SCALE OF CHORDS.



42. If, with any radius, as  $AC$ , we describe the quadrant  $CD$ , and then divide it into 90 equal parts, each part is called a degree.

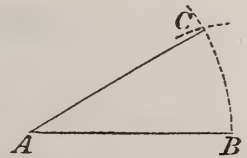
Through  $C$ , and each point of division, let a chord be drawn, and let the lengths of these chords be accurately laid off on a scale: such a scale is called a *scale of chords*. In the figure, the chords are drawn for every ten degrees.

The scale of chords being once constructed, the radius of the circle from which the chords were obtained, is known; for, the chord marked 60 is always equal to the radius of the circle. A scale of chords is generally laid down on the scales which belong to cases of mathematical instruments, and is marked CHO.

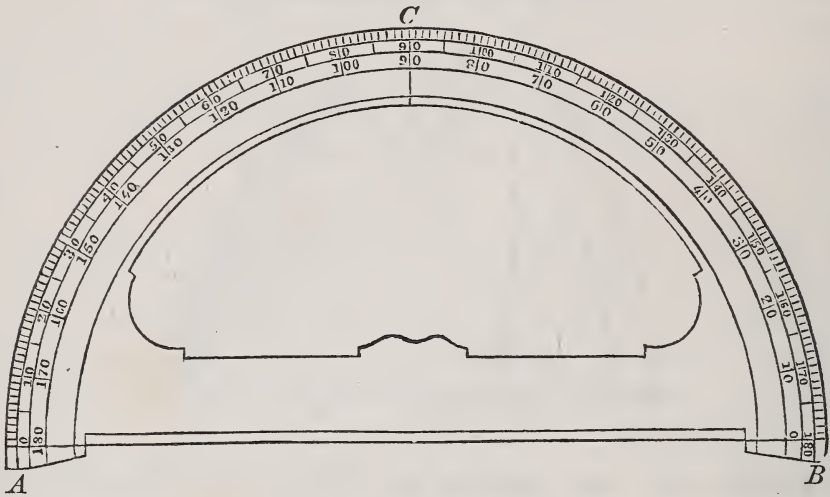
*To lay off, at a given point of a line, with the scale of chords, an angle equal to a given angle.*

43. Let  $AB$  be the line, and  $A$  the given point.

Take from the scale the chord of 60 degrees, and with this radius and the point  $A$  as a centre, describe the arc  $BC$ . Then take from the scale the chord of the given angle, say 30 degrees, and with this line as a radius, and  $B$  as a centre, describe an arc cutting  $BC$  in  $C$ . Through  $A$  and  $C$  draw the line  $AC$ , and  $BAC$  will be the required angle.



## SEMICIRCULAR PROTRACTOR.



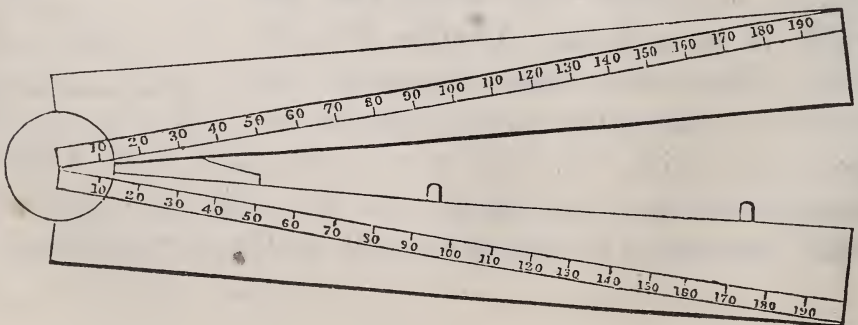
44. This instrument is used to lay down, or protract angles. It may also be used to measure angles included between lines already drawn upon paper.

It consists of a brass semicircle,  $ABC$ , divided to half degrees. The degrees are numbered from 0 to 180, both ways; that is, from  $A$  to  $B$  and from  $B$  to  $A$ . The divisions, in the figure, are made only to degrees. There is a small notch at the middle of the diameter  $AB$ , which indicates the centre of the protractor.

*To lay off an angle with a Protractor.*

45. Place the diameter  $AB$  on the line, so that the centre shall fall on the angular point. Then count the degrees contained in the given angle from  $A$  towards  $B$ , or from  $B$  towards  $A$ , and mark the extremity of the arc with a pin. Remove the protractor, and draw a line through the point so marked and the angular point: this line will make with the given line the required angle.

## SECTORAL SCALE OF EQUAL PARTS.



46. The sector is an instrument generally made of ivory or brass. It consists of two arms, or sides, which open by turning round a joint at their common extremity.

There are several scales laid down on the sector: those, however, which are chiefly used in drawing lines and angles, are, the scale of chords already described, and the scale of equal parts now to be explained.

On each arm of the sector, there is a diagonal line that passes through the point about which the arms turn: these diagonal lines are divided into equal parts.

On the sectors which belong to the cases of English instruments, the diagonal lines are designated by the letter *L*, and numbered from the centre of the sector, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, to the two extremities. On the sectors which belong to cases of French instruments, they are designated, "Les parties egales," and numbered 10, 20, 30, 40, &c., to 200. On the English sectors there are 20 equal divisions between any two of the lines numbered 1, 2, 3, &c., so that there are 200 equal parts on the scale.

The advantage of the sectoral scale of equal parts, is this—

When it is proposed to draw a line upon paper, on such a scale that any number of parts of the line, 40 for example, shall be represented by one inch on the paper, or by any part of an inch, take the inch, or part of the inch, from the scale of inches on the sector: then, placing one foot of the dividers at 40 on one arm of the sector, open the sector until the other foot reaches to the corresponding number on the other arm: then lay the sector on the table without varying the angle.

Now, if we regard the lines on the sector as the sides of a triangle, of which the line 40, measured across, is the base, it is plain, that if any other line be likewise measured across the angle of the sector, the bases of the triangles, so formed, will be proportional to their sides. Therefore, if we extend the dividers from 50 to 50, this distance will represent a line of 50, to the given scale: and similarly for other lines.

Let it now be required to lay down a line of sixty-seven feet, to a scale of twenty feet to the inch.

Take one inch from the scale of inches: then place one foot of the dividers at the twentieth division, and open the sector until the dividers will just reach the twentieth division on the other arm: the sector is then set to the proper angle; after which the required distance to be laid down on the paper is found by extending the dividers from the sixty-seventh division on one arm, to the sixty-seventh division on the other.

#### GUNTER'S SCALE.

47. This is a scale of two feet in length, on the faces of which a variety of scales is marked. The face on which the divisions of inches are made, contains, however, all the scales necessary for laying down lines and angles. These are, the scale of equal parts, the diagonal scale of equal parts, and the scale of chords, all of which have been described.

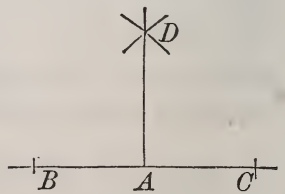
#### SOLUTION OF PROBLEMS REQUIRING THE USE OF THE INSTRUMENTS THAT HAVE BEEN DESCRIBED.

I. *At a given point in a given straight line, to erect a perpendicular to the line.*

48. Let  $A$  be the given point, and  $BC$  the given line.

From  $A$  lay off any two distances,  $AB$  and  $AC$ , equal to each other.

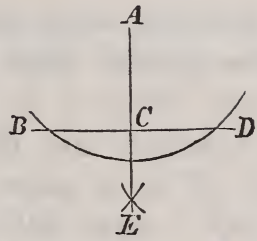
Then, from the points  $B$  and  $C$ , as centres, with a radius greater than  $BA$ , describe two arcs intersecting each other in  $D$ : draw  $AD$ , and it will be the perpendicular required.



II. *From a given point without a straight line, to let fall a perpendicular on the line.*

49. Let  $A$  be the given point, and  $BD$  the given line.

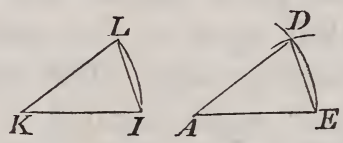
From the point  $A$  as a centre, with a radius sufficiently great, describe an arc cutting the line  $BD$  in the two points  $B$  and  $D$ : then mark a point  $E$ , equally distant from the points  $B$  and  $D$ , and draw  $AE$ :  $AE$  will be the perpendicular required.



III. *At a point, in a given line, to make an angle equal to a given angle.*

50. Let  $A$  be the given point,  $AE$  the given line, and  $IKL$  the given angle.

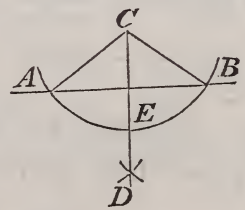
From the vertex  $K$ , as a centre, with any radius, describe the arc  $IL$ , terminating in the two sides of the angle. From the point  $A$  as a centre, with a distance  $AE$  equal to  $KI$ , describe the arc  $ED$ ; then take the chord  $LI$ , with which, from the point  $E$  as a centre, describe an arc cutting the indefinite arc  $DE$ , in  $D$ ; draw  $AD$ , and the angle  $EAD$  will be equal to the given angle  $K$ .



IV. *To divide a given angle, or a given arc, into two equal parts.*

51. Let  $C$  be the given angle, and  $AEB$  the arc which measures it.

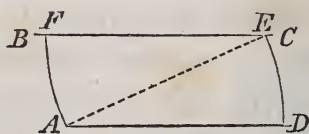
From the points  $A$  and  $B$  as centres, describe with the same radius two arcs cutting each other in  $D$ : through  $D$  and the centre  $C$  draw  $CD$ : the angle  $ACE$  will be equal to the angle  $ECB$ , and the arc  $AE$  to the arc  $EB$ .



V. *Through a given point to draw a parallel to a given line.*

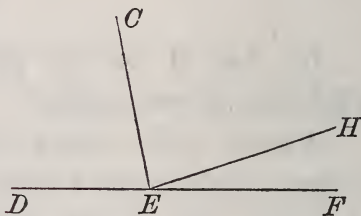
52. Let  $A$  be the given point, and  $BC$  the given line.

From  $A$  as a centre, with a radius greater than the shortest distance from  $A$  to  $BC$ , describe the indefinite arc  $ED$ : from the point  $E$  as a centre, with the same radius, describe the arc  $AF$ ; make  $ED = AF$ , and draw  $AD$ : then will  $AD$  be the parallel required.



VI. *Two angles of a triangle being given, to find the third.*

53. Draw the indefinite line  $DEF$ . At the point  $E$ , make the angle  $DEC$  equal to one of the given angles, and the angle  $CEH$  equal to the other: the remaining angle  $HEF$  will be the third angle required.

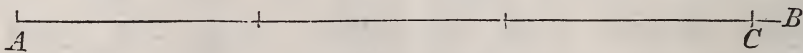


VII. *To represent, on paper, a line of a given length, so that any number of its parts shall correspond to the unit of the scale.*

54. Suppose that the given line were 75 feet in length, and it were required to draw it on paper, on a scale of 25 feet to the inch.

The length of the line 75 feet, being divided by 25, will give 3, the number of inches which will represent the line on paper.

Therefore, draw the indefinite line  $AB$ , on which lay



off a distance  $AC$  equal to 3 inches:  $AC$  will represent the given line of 75 feet, drawn on the required scale.

REMARK I. This problem explains the manner of representing a line upon paper, so that a given number of its parts shall correspond to the unit of the scale, whether that unit be an inch or any part of an inch.

When the length of the line to be laid down is given, and it has been determined how many parts of it are to



be represented on the paper by a distance equal to the unit of the scale, we find the length which is to be taken from the scale by the following

## RULE.

*Divide the length of the line by the number of parts which is to be represented by the unit of the scale: the quotient will show the number of units which is to be taken from the scale.*

## EXAMPLES.

1. If a line of 640 feet is to be laid down on paper, on a scale of 40 feet to the inch; what length must be taken from the scale?

40)640(16 inches.

2. If a line of 357 feet is to be laid down on a scale of 68 feet to the unit of the scale, (which we will suppose half an inch), how many parts are to be taken?

*Ans.*  $\left\{ \begin{array}{l} 5.25 \text{ parts, or} \\ 2.625 \text{ inches.} \end{array} \right.$

3. A line of 384 feet is drawn on paper, on a scale of 45 feet to the inch; what is its length on the paper?

*Ans.* 8.53 inches.

REMARK II. When the length of a line on the paper is given, and it is required to find the true length of the line which it represents, take the line in the dividers and apply it to the scale, and note the number of units, and parts of a unit to which it is equal. Then multiply this number by the number of parts which the unit of the scale represents, and the product will be the length of the line.

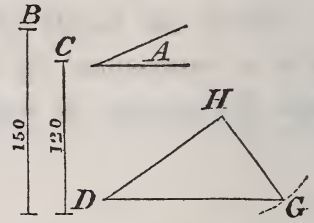
For example, suppose the length of a line drawn on the paper was found to be 3.55 inches, the scale being 40 feet to the inch: then,

$$3.55 \times 40 = 142 \text{ feet, the length of the line.}$$

VIII. *Having given two sides and the included angle of a triangle, to describe the triangle.*

55. Let the line  $B = 150$  feet, and  $C = 120$  feet, be the given sides; and  $A = 30$  degrees, the given angle; to describe the triangle on a scale of 200 feet to the inch.

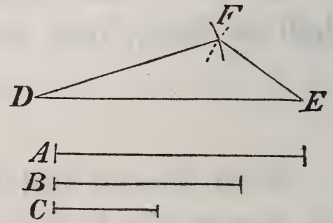
Draw the indefinite line  $DG$ , and at the point  $D$ , make the angle  $GDH$  equal to 30 degrees: then lay off  $DG$  equal to 150, equal to three quarters of an inch, and  $DH$  equal to 120, equal to six tenths of an inch, and draw  $GH$ :  $DHG$  will be the required triangle.



IX. *The three sides of a triangle being given, to describe the triangle.*

56. Let  $A$ ,  $B$  and  $C$ , be the sides.

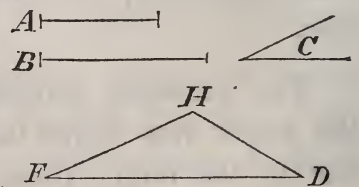
Draw  $DE$  equal to the side  $A$ . From the point  $D$  as a centre, with a radius equal to the second side  $B$ , describe an arc: from  $E$  as a centre, with a radius equal to the third side  $C$ , describe another arc intersecting the former in  $F$ ; draw  $DF$  and  $EF$ , and  $DFE$  will be the triangle required.



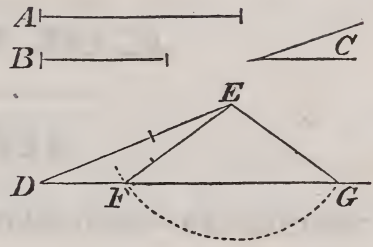
X. *Having given two sides of a triangle and an angle opposite one of them, to describe the triangle.*

57. Let  $A$  and  $B$  be the given sides, and  $C$  the given angle, which we will suppose is opposite the side  $B$ .

Draw the indefinite line  $DF$  and make the angle  $FDH$  equal to the angle  $C$ : take  $DH = A$ , from the point  $H$ , as a centre, with a radius equal to the other given side,  $B$ , describe an arc cutting  $DF$  in  $F$ ; draw  $HF$ : then will  $DHF$  be the required triangle.



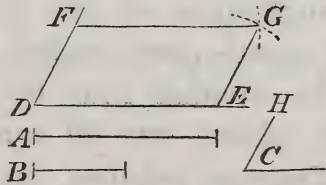
If the angle  $C$  is acute, and the side  $B$  less than  $A$ , then the arc described from the centre  $E$  with the radius  $EF = B$  will cut the side  $DF$  in two points,  $F$  and  $G$ , lying on the same side of  $D$ : hence, there will be two triangles,  $DEF$ , and  $DEG$ , either of which will satisfy all the conditions of the problem.



XI. *The adjacent sides of a parallelogram, with the angle which they contain, being given, to describe the parallelogram.*

58. Let  $A$  and  $B$  be the given sides, and  $C$  the given angle.

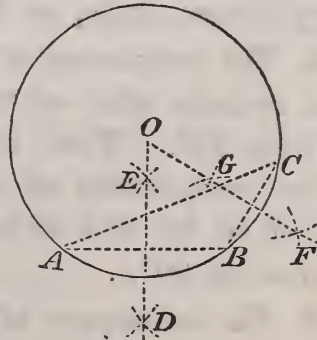
Draw the line  $DH$ , and lay off  $DE$  equal to  $A$ ; at the point  $D$ , make the angle  $EDF = C$ ; take  $DF = B$ : describe two arcs, the one from  $F$ , as a centre, with a radius  $FG = DE$ , the other from  $E$ , as a centre, with a radius  $EG = DF$ ; through the point  $G$ , where these arcs intersect each other, draw  $FG$ ,  $EG$ ;  $DEGF$  will be the parallelogram required.



XII. *To find the centre of a given circle or arc.*

59. Take three points,  $A$ ,  $B$ ,  $C$ , any where in the circumference, or in the arc: draw  $AB$ ,  $BC$ ; bisect these two lines by the perpendiculars,  $DE$ ,  $FG$ : the point  $O$ , where these perpendiculars meet, will be the centre sought.

The same construction serves for making a circumference pass through three given points  $A$ ,  $B$ ,  $C$ , and also for describing a circumference, about a given triangle.



## PLANE TRIGONOMETRY.

## SECTION III.

DEFINITIONS.—APPLICATION TO HEIGHTS AND DISTANCES.

1. In every plane triangle there are six parts: three sides and three angles. These parts are so related to each other, that when one side and any two other parts are given, the remaining ones can be obtained, either by geometrical construction or by trigonometrical computation.

2. *Plane Trigonometry* explains the methods of computing the unknown parts of a plane triangle, when a sufficient number of the six parts is given.

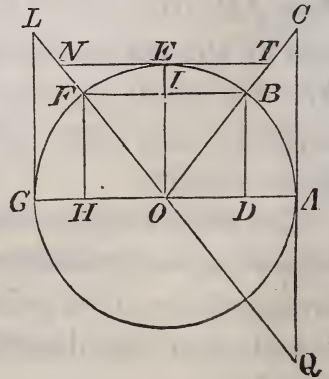
3. For the purpose of trigonometrical calculation, the circumference of the circle is supposed to be divided into 360 equal parts, called degrees; each degree is supposed to be divided into 60 equal parts, called minutes; and each minute into 60 equal parts, called seconds.

Degrees, minutes, and seconds, are designated respectively, by the characters  $^{\circ}$   $'$   $''$ . For example, *ten degrees, eighteen minutes, and fourteen seconds*, would be written  $10^{\circ} 18' 14''$ .

4. If two lines be drawn through the centre of the circle, at right angles to each other, they will divide the circumference into four equal parts, of  $90^{\circ}$  each. Every right angle then, as  $EOA$ , is measured by an arc of  $90^{\circ}$ ; every acute angle, as  $BOA$ , by an arc less than  $90^{\circ}$ ; and every obtuse angle, as  $FOA$ , by an arc greater than  $90^{\circ}$ .

5. The *complement* of an arc is what remains after subtracting the arc from  $90^{\circ}$ . Thus, the arc  $EB$  is the complement of  $AB$ . The sum of an arc and its complement is equal to  $90^{\circ}$ .

6. The *supplement* of an arc is what remains after subtracting the arc from  $180^{\circ}$ . Thus,  $GF$  is the



supplement of the arc  $AEF$ . The sum of an arc and its supplement is equal to  $180^\circ$ .

7. The *sine* of an arc is the perpendicular let fall from one extremity of the arc on the diameter which passes through the other extremity. Thus,  $BD$  is the sine of the arc  $AB$ .

8. The *cosine* of an arc is the part of the diameter intercepted between the foot of the sine and centre. Thus,  $OD$  is the cosine of the arc  $AB$ .

9. The *tangent* of an arc is the line which touches it at one extremity, and is limited by a line drawn through the other extremity and the centre of the circle. Thus,  $AC$  is the tangent of the arc  $AB$ .

10. The *secant* of an arc is the line drawn from the centre of the circle through one extremity of the arc, and limited by the tangent passing through the other extremity. Thus,  $OC$  is the secant of the arc  $AB$ .

11. The four lines,  $BD$ ,  $OD$ ,  $AC$ ,  $OC$ , depend for their values on the arc  $AB$  and the radius  $OA$ ; they are thus designated :

$\sin AB$	for	$BD$
$\cos AB$	for	$OD$
$\tan AB$	for	$AC$
$\sec AB$	for	$OC$

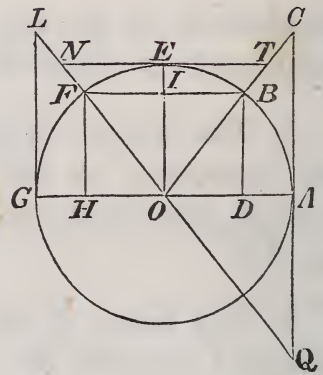
12. If  $ABE$  be equal to a quadrant, or  $90^\circ$ , then  $EB$  will be the complement of  $AB$ . Let the lines  $ET$  and  $IB$  be drawn perpendicular to  $OE$ . Then,

$ET$ , the tangent of  $EB$ , is called the cotangent of  $AB$ ;  
 $IB$ , the sine of  $EB$ , is equal to the cosine of  $AB$ ;  
 $OT$ , the secant of  $EB$ , is called the cosecant of  $AB$ .

In general, if  $A$  is any arc or angle, we have,

$$\begin{aligned}\cos A &= \sin (90^\circ - A) \\ \cot A &= \tan (90^\circ - A) \\ \operatorname{cosec} A &= \sec (90^\circ - A)\end{aligned}$$

13. If we take an arc,  $ABEF$ , greater than  $90^\circ$ , its sine will be  $FH$ ;  $OH$  will be its cosine;  $AQ$  its tangent, and  $OQ$  its secant. But  $FH$  is the sine of the arc  $GF$ , which is the supplement of  $AF$ , and  $OH$  is its cosine; hence, *the sine of an arc is equal to the sine of its supplement; and the cosine of an arc is equal to the cosine of its supplement.\**



Furthermore,  $AQ$  is the tangent of the arc  $AF$ , and  $OQ$  is its secant:  $GL$  is the tangent, and  $OL$  the secant of the supplemental arc  $GF$ . But since  $AQ$  is equal to  $GL$ , and  $OQ$  to  $OL$ , it follows that, *the tangent of an arc is equal to the tangent of its supplement; and the secant of an arc is equal to the secant of its supplement.\**

#### TABLE OF NATURAL SINES.

14. Let us suppose, that in a circle of a given radius, the lengths of the sine, cosine, tangent, and cotangent, have been calculated for every minute or second of the quadrant, and arranged in a table; such a table is called a table of sines and tangents. If the radius of the circle is 1, the table is called a table of natural sines. A table of natural sines, therefore, shows the values of the sines, cosines, tangents, and cotangents of all the arcs of a quadrant, which is divided to minutes or seconds.

If the sines, cosines, tangents, and secants are known for arcs less than  $90^\circ$ , those for arcs which are greater can be found from them. For if an arc is less than  $90^\circ$ , its supplement will be greater than  $90^\circ$ , and the numerical values of these lines are the same for an arc and its supplement. Thus, if we know the sine of  $20^\circ$ , we also know the sine of its supplement  $160^\circ$ ; for the two are equal to each other. The Table of Natural Sines, beginning at page 63, of the tables shows the values of the sines and cosines only.

\* These relations are between the *numerical values* of the trigonometrical lines; the algebraic signs, which they have in the different quadrants, are not considered.

## TABLE OF LOGARITHMIC SINES.

15. In this table are arranged the logarithms of the numerical values of the sines, cosines, tangents, and cotangents of all the arcs of a quadrant, calculated to a radius of 10,000,000,000. The logarithm of this radius is 10. In the first and last horizontal lines of each page, are written the degrees whose sines, cosines, &c., are expressed on the page. The vertical columns on the left and right, are columns of minutes.

## CASE I.

*To find, in the table, the logarithmic sine, cosine, tangent, or cotangent of any given arc or angle.*

16. If the angle is less than  $45^\circ$ , look for the degrees in the first horizontal line of the different pages: when the degrees are found, descend along the column of minutes, on the left of the page, till you reach the number showing the minutes: then pass along a horizontal line till you come into the column designated, sine, cosine, tangent, or cotangent, as the case may be: the number so indicated is the logarithm sought. Thus, on page 37, for  $19^\circ 55'$ , we find,

sine $19^\circ 55'$	. . . . .	9.532312
cos $19^\circ 55'$	. . . . .	9.973215
tan $19^\circ 55'$	. . . . .	9.559097
cot $19^\circ 55'$	. . . . .	10.440903

17. If the angle is greater than  $45^\circ$ , search for the degrees along the bottom line of the different pages: when the number is found, ascend along the column of minutes on the right hand side of the page, till you reach the number expressing the minutes: then pass along a horizontal line into the column designated tang, cot, sine, or cosine, as the case may be: the number so pointed out is the logarithm required.

18. The column designated sine, at the top of the page, is designated by cosine at the bottom; the one designated tang, by cotang, and the one designated cotang, by tang.

The angle found by taking the degrees at the top of the page, and the minutes from the left hand vertical column, is the complement of the angle found by taking the degrees

at the bottom of the page, and the minutes from the right hand column on the same horizontal line with the first. Therefore, sine, at the top of the page, should correspond with cosine, at the bottom; cosine with sine, tang with cotang, and cotang with tang, as in the tables (Art. 12).

If the angle is greater than  $90^\circ$ , we have only to subtract it from  $180^\circ$ , and take the sine, cosine, tangent, or cotangent of the remainder.

The column of the table next to the column of sines, and on the right of it, is designated by the letter *D*. This column is calculated in the following manner.

Opening the table at any page, as 42, the sine of  $24^\circ$  is found to be 9.609313; that of  $24^\circ 01'$ , 9.609597: their difference is 284; this being divided by 60, the number of seconds in a minute, gives 4.73, which is entered in the column *D*.

Now, supposing the increase of the logarithmic sine to be proportional to the increase of the arc, and it is nearly so for  $60''$ , it follows, that 4.73 is the increase of the sine for  $1''$ . Similarly, if the arc were  $24^\circ 20'$ , the increase of the sine for  $1''$ , would be 4.65.

The same remarks are applicable in respect of the column *D*, after the column cosine, and of the column *D*, between the tangents and cotangents. The column *D*, between the columns tangents and cotangents, answers to both of these columns.

Now, if it were required to find the logarithmic sine of an arc expressed in degrees, minutes, and seconds, we have only to find the degrees and minutes as before; then, multiply the corresponding tabular difference by the seconds, and add the product to the number first found, for the sine of the given arc.

Thus, if we wish the sine of  $40^\circ 26' 28''$ .

The sine $40^\circ 26'$	.	.	.	.	9.811952
Tabular difference	2.47	.	.	.	
Number of seconds	28	.	.	.	
Product,	<u>69.16</u>			to be added	69.16
Gives for the sine of $40^\circ 26' 28''$ .					<u>9.812021.</u>



The decimal figures at the right are generally omitted in the last result; but when they exceed five-tenths, the figure on the left of the decimal point is increased by 1; the logarithm obtained is then exact, to within less than one unit of its right hand place.

The tangent of an arc, in which there are seconds, is found in a manner entirely similar. In regard to the cosine and cotangent, it must be remembered, that they increase while the arcs decrease, and decrease as the arcs are increased; consequently, the proportional numbers found for the seconds, must be subtracted, not added.

EXAMPLES.

1. To find the cosine of  $3^{\circ} 40' 40''$ .

The cosine of $3^{\circ} 40'$	. . .	9.999110
Tabular difference .13	. . .	
Number of seconds <u>40</u>	. . .	
Product,	5.20 to be subtracted	<u>5.20</u>
Gives for the cosine of $3^{\circ} 40' 40''$		<u>9.999105.</u>

2. Find the tangent of  $37^{\circ} 28' 31''$ .

*Ans.* 9.884592.

3. Find the cotangent of  $87^{\circ} 57' 59''$ .

*Ans.* 8.550356.

CASE II.

*To find the degrees, minutes, and seconds answering to any given logarithmic sine, cosine, tangent, or cotangent.*

19. Search in the table, in the proper column, and if the number is found, the degrees will be shown either at the top or bottom of the page, and the minutes in the side column either at the left or right.

But, if the number cannot be found in the table, take from the table the degrees and minutes answering to the nearest less logarithm, the logarithm itself, and also the corresponding tabular difference. Subtract the logarithm taken from the table from the given logarithm, annex two

ciphers to the remainder, and then divide the remainder by the tabular difference: the quotient will be seconds, and is to be connected with the degrees and minutes before found: to be added for the sine and tangent, and subtracted for the cosine and cotangent.

## EXAMPLES.

1. Find the arc answering to the sine 9.880054  
 Sine  $49^\circ 20'$ , next less in the table 9.879963  
 Tabular difference, 1.81)91.00(50''.

Hence, the arc  $49^\circ 20' 50''$  corresponds to the given sine 9.880054.

2. Find the arc whose cotangent is 10.008688  
 cot  $44^\circ 26'$ , next less in the table 10.008591  
 Tabular difference, 4.21)97.00(23''.

Hence,  $44^\circ 26' - 23'' = 44^\circ 25' 37''$  is the arc answering to the given cotangent 10.008688.

3. Find the arc answering to tangent 9.979110.  
*Ans.*  $43^\circ 37' 21''.$

4. Find the arc answering to cosine 9.944599.  
*Ans.*  $28^\circ 19' 45''.$

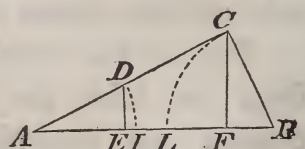
20. We shall now demonstrate the principal theorems of Plane Trigonometry.

## THEOREM I.

*The sides of a plane triangle are proportional to the sines of their opposite angles.*

21. Let  $ABC$  be a triangle; then will  
 $CB : CA :: \sin A : \sin B.$

For, with  $A$  as a centre, and  $AD$  equal to the less side  $BC$ , as a radius, describe the arc  $DI$ : and with  $B$  as a centre and the equal radius  $BC$ , describe the arc  $CL$ , and draw  $DE$  and  $CF$  perpendicular to  $AB$ : now  $DE$  is the sine of the angle  $A$ , and



now  $DE$  is the sine of the angle  $A$ , and

$CF$  is the sine of  $B$ , to the same radius  $AD$  or  $BC$ . But by similar triangles,

$$AD : DE :: AC : CF.$$

But  $AD$  being equal to  $BC$ , we have

$$BC : \sin A :: AC : \sin B, \text{ or}$$

$$BC : AC :: \sin A : \sin B.$$

By comparing the sides  $AB, AC$ , in a similar manner, we should find,

$$AB : AC :: \sin C : \sin B.$$

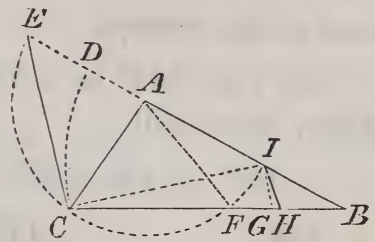
THEOREM II.

*In any triangle, the sum of the two sides containing either angle, is to their difference, as the tangent of half the sum of the two other angles, to the tangent of half their difference.*

22. Let  $ACB$  be a triangle: then will

$$AB + AC : AB - AC :: \tan \frac{1}{2}(C + B) : \tan \frac{1}{2}(C - B).$$

With  $A$  as a centre, and a radius  $AC$ , the less of the two given sides, let the semicircumference  $IFCE$  be described, meeting  $AB$  in  $I$ , and  $BA$  produced; in  $E$ . Then,  $BE$  will be the sum of the sides, and  $BI$  their difference. Draw  $CI$  and  $AF$ .



Since  $CAE$  is an outward angle of the triangle  $ACB$ , it is equal to the sum of the inward angles  $C$  and  $B$  (Bk. I., Prop. XXV., Cor 6). But the angle  $CIE$  being at the circumference, is half the angle  $CAE$  at the centre (Bk. III., Prop. XVIII.); that is, half the sum of the angles  $C$  and  $B$ , or equal to  $\frac{1}{2}(C + B)$ .

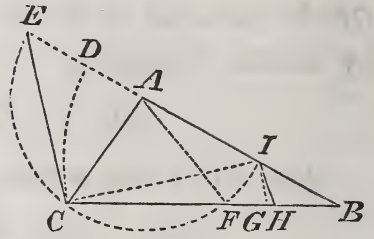
The angle  $AFC = ACB$ , is also equal to  $ABC + BAF$ ; therefore,  $BAF = ACB - ABC$ .

But,  $ICF = \frac{1}{2}(BAF) = \frac{1}{2}(ACB - ABC)$ , or  $\frac{1}{2}(C - B)$ .

With  $I$  and  $C$  as centres, and the common radius  $IC$ , let the arcs  $CD$  and  $IG$  be described, and draw the lines  $CE$  and  $IH$  perpendicular to  $IC$ . The perpendicular  $CE$  will pass through  $E$ , the extremity of the diameter  $IE$ ,

since the right angle  $ICE$  must be inscribed in a semicircle.

But  $CE$  is the tangent of  $CIE = \frac{1}{2}(C+B)$ ; and  $IH$  is the tangent of  $ICB = \frac{1}{2}(C-B)$ , to the common radius  $CI$ .



But since the lines  $CE$  and  $IH$  are parallel, the triangles  $BHI$  and  $BCE$  are similar, and give the proportion,

$$BE : BI :: CE : IH, \text{ or}$$

by placing for  $BE$  and  $BI$ ,  $CE$  and  $IH$ , their values, we have

$$AB + AC : AB - AC :: \tan \frac{1}{2}(C+B) : \tan \frac{1}{2}(C-B).$$

THEOREM III.

*In any plane triangle, if a line is drawn from the vertical angle perpendicular to the base, dividing it into two segments: then, the whole base, or sum of the segments, is to the sum of the two other sides, as the difference of those sides to the difference of the segments.*

23. Let  $BAC$  be a triangle, and  $AD$  perpendicular to the base; then will

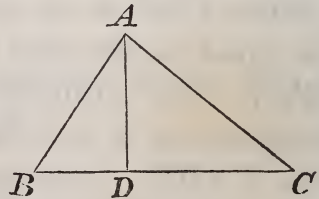
$$BC : CA + AB :: CA - AB : CD - DB.$$

For,  $\overline{AB}^2 = \overline{BD}^2 + \overline{AD}^2$

(Bk. IV., Prop. XI.);

and  $\overline{AC}^2 = \overline{DC}^2 + \overline{AD}^2$

by subtraction,  $\overline{AC}^2 - \overline{AB}^2 = \overline{CD}^2 - \overline{BD}^2.$



But since the difference of the squares of two lines is equivalent to the rectangle contained by their sum and difference (Bk. IV., Prop. X.), we have,

$$\overline{AC}^2 - \overline{AB}^2 = (AC + AB).(AC - AB)$$

and  $\overline{CD}^2 - \overline{DB}^2 = (CD + DB).(CD - DB)$

therefore,  $(CD + DB).(CD - DB) = (AC + AB).(AC - AB)$

hence,  $CD + DB : AC + AB :: AC - AB : CD - DB.$

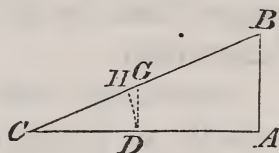
## THEOREM IV.

*In any right-angled plane triangle, radius is to the tangent of either of the acute angles, as the side adjacent to the side opposite.*

24. Let  $CAB$  be the proposed triangle, and denote the radius by  $R$ : then will

$$R : \tan C :: AC : AB.$$

For, with any radius as  $CD$  describe the arc  $DH$ , and draw the tangent  $DG$ .



From the similar triangles  $CDG$  and  $CAB$ , we have,

$$CD : DG :: CA : AB; \text{ hence,}$$

$$R : \tan C :: CA : AB.$$

By describing an arc with  $B$  as a centre, we could show in the same manner that,

$$R : \tan B :: AB : AC.$$

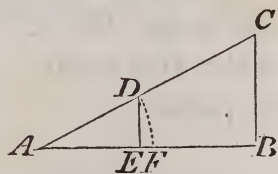
## THEOREM V.

*In every right-angled plane triangle, radius is to the cosine of either of the acute angles, as the hypotenuse to the side adjacent.*

25. Let  $ABC$  be a triangle, right-angled at  $B$ : then will,

$$R : \cos A :: AC : AB.$$

For, from the point  $A$  as a centre, with any radius as  $AD$ , describe the arc  $DF$ , which will measure the angle  $A$ , and draw  $DE$  perpendicular to  $AB$ : then will  $AE$  be the cosine of  $A$ .



The triangles  $ADE$  and  $ACB$ , being similar, we have,

$$AD : AE :: AC : AB; \text{ that is,}$$

$$R : \cos A :: AC : AB.$$

REMARK. The relations between the sides and angles of plane triangles, demonstrated in these five theorems, are

sufficient to solve all the cases of Plane Trigonometry. Of the six parts which make up a plane triangle, three must be given, and at least one of these a side, before the others can be determined.

If the three angles only are given, it is plain, that an indefinite number of similar triangles may be constructed, the angles of which shall be respectively equal to the angles that are given, and therefore, the sides could not be determined.

Assuming, with this restriction, any three parts of a triangle as given, one of the four following cases will always be presented.

- I. When two angles and a side are given.
- II. When two sides and an opposite angle are given.
- III. When two sides and the included angle are given.
- IV. When the three sides are given.

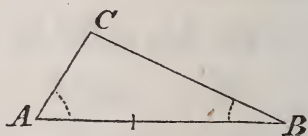
#### CASE I.

*When two angles and a side are given.*

26. Add the given angles together, and subtract their sum from 180 degrees. The remaining parts of the triangle can then be found by Theorem I.

#### EXAMPLES.

1. In a plane triangle,  $ABC$ , there are given the angle  $A = 58^\circ 07'$ , the angle  $B = 22^\circ 37'$ , and the side  $AB = 408$  yards. Required the other parts.



#### GEOMETRICALLY.

27. Draw an indefinite straight line,  $AB$ , and from the scale of equal parts lay off  $AB$  equal to 408. Then, at  $A$ , lay off an angle equal to  $58^\circ 07'$ , and at  $B$  an angle equal to  $22^\circ 37'$ , and draw the lines  $AC$  and  $BC$ : then will  $ABC$  be the triangle required.

The angle  $C$  may be measured either with the protractor or the scale of chords (Sec. II., Arts. 42 and 44), and will be

found equal to  $99^\circ 16'$ . The sides  $AC$  and  $BC$  may be measured by referring them to the scale of equal parts (Sec. II., Art. 40). We shall find  $AC = 158.9$  and  $BC = 351$  yards.

TRIGONOMETRICALLY BY LOGARITHMS.

To the angle . . .  $A = 58^\circ 07'$

Add the angle . . .  $B = 22^\circ 37'$

    Their sum,             $= 80^\circ 44'$

taken from . . .             $180^\circ 00'$

leaves  $C$  . . . . .  $99^\circ 16'$ , of which, as it exceeds  $90^\circ$ , we use the supplement  $80^\circ 44'$ .

*To find the side BC.*

	sin $C$	99° 16'	ar. comp.	0.005705
:	sin $A$	58° 07'		9.928972
::	$AB$	408		2.610660
:	$BC$	351.024	(after rejecting 10)	<u>2.545337</u>

REMARK. The logarithm of the fourth term of a proportion is obtained by adding the logarithm of the second term to that of the third, and subtracting from their sum the logarithm of the first term. But to subtract the first term is the same as to add its arithmetical complement and reject 10 from the sum (Sec. I., Art. 13): hence, the arithmetical complement of the first term added to the logarithms of the second and third terms, minus ten, will give the logarithm of the fourth term.

*To find the side AC.*

	sin $C$	99° 16'	ar. comp.	0.005705
:	sin $B$	22° 37'		9.584968
::	$AB$	408		2.610660
:	$AC$	158.976		<u>2.201333</u>

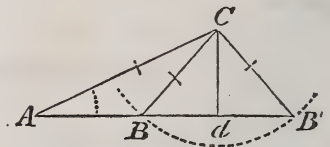
2. In a triangle  $ABC$ , there are given  $A = 38^\circ 25'$ ,  $B = 57^\circ 42'$ , and  $AB = 400$ : required the remaining parts.

*Ans.*  $C = 83^\circ 53'$ ,  $BC = 249.974$ ,  $AC = 340.04$ .

CASE II.

When two sides and an opposite angle are given.

28. In a plane triangle,  $ABC$ , there are given  $AC=216$ ,  $CB=117$ , the angle  $A=22^\circ 37'$ , to find the other parts.



GEOMETRICALLY.

29. Draw an indefinite right line  $ABB'$ : from any point, as  $A$ , draw  $AC$ , making  $BAC=22^\circ 37'$ , and make  $AC=216$ . With  $C$  as a centre, and a radius equal to 117, the other given side, describe the arc  $B'B$ ; draw  $B'C$  and  $BC$ : then will either of the triangles  $ABC$  or  $AB'C$ , answer all the conditions of the question.

TRIGONOMETRICALLY.

To find the angle  $B$ .

	$BC$	117	ar. comp.	7.931814
:	$AC$	216	. . . . .	2.334454
::	$\sin A$	$22^\circ 37'$	. . . . .	9.584968
:	$\sin B'$	$45^\circ 13' 55''$ , or $ABC$	$134^\circ 46' 05''$	9.851236

The ambiguity in this, and similar examples, arises in consequence of the first proportion being true for either of the angles  $ABC$ , or  $AB'C$ , which are supplements of each other, and therefore, have the same sine (Art. 13). As long as the two triangles exist, the ambiguity will continue. But if the side  $CB$ , opposite the given angle, is greater than  $AC$ , the arc  $BB'$  will cut the line  $ABB'$ , on the same side of the point  $A$ , in but one point, and then there will be only one triangle answering the conditions.

If the side  $CB$  is equal to the perpendicular  $Cd$ , the arc  $BB'$  will be tangent to  $ABB'$ , and in this case also there will be but one triangle. When  $CB$  is less than the perpendicular  $Cd$ , the arc  $BB'$  will not intersect the base  $ABB'$ , and in that case, no triangle can be formed, or it will be impossible to fulfil the conditions of the problem.



2. Given two sides of a triangle 50 and 40 respectively, and the angle opposite the latter equal to  $32^\circ$ : required the remaining parts of the triangle.

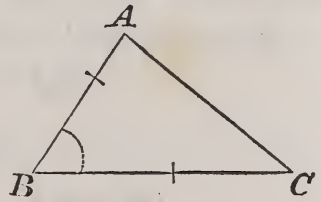
*Ans.* If the angle opposite the side 50 is acute, it is equal to  $41^\circ 28' 59''$ ; the third angle is then equal to  $106^\circ 31' 01''$ , and the third side to 72.368. If the angle opposite the side 50 is obtuse, it is equal to  $138^\circ 31' 01''$ , the third angle to  $9^\circ 28' 59''$ , and the remaining side to 12.436.

## CASE III.

*When the two sides and their included angle are given.*

30. Let  $ABC$  be a triangle;  $AB$ ,  $BC$ , the given sides, and  $B$  the given angle.

Since  $B$  is known, we can find the sum of the two other angles: for



$$A + C = 180^\circ - B, \text{ and,} \\ \frac{1}{2}(A + C) = \frac{1}{2}(180^\circ - B).$$

We next find half the difference of the angles  $A$  and  $C$  by Theorem II., viz.,

$BC + BA : BC - BA :: \tan \frac{1}{2}(A + C) : \tan \frac{1}{2}(A - C)$ ,  
in which we consider  $BC$  greater than  $BA$ , and therefore  $A$  is greater than  $C$ ; since the greater angle must be opposite the greater side.

Having found half the difference of  $A$  and  $C$ , by adding it to the half sum,  $\frac{1}{2}(A + C)$ , we obtain the greater angle, and by subtracting it from half the sum, we obtain the less. That is,

$$\frac{1}{2}(A + C) + \frac{1}{2}(A - C) = A, \text{ and} \\ \frac{1}{2}(A + C) - \frac{1}{2}(A - C) = C.$$

Having found the angles  $A$  and  $C$ , the third side  $AC$  may be found by the proportion,

$$\sin A : \sin B :: BC : AC.$$

EXAMPLES.

1. In the triangle  $ABC$ , let  $BC=540$ ,  $AB=450$ , and the included angle  $B=80^\circ$ : required the remaining parts.

GEOMETRICALLY.

31. Draw an indefinite right line  $BC$ , and from any point, as  $B$ , lay off a distance  $BC=540$ . At  $B$  make the angle  $CBA=80^\circ$ : draw  $BA$ , and make the distance  $BA=450$ ; draw  $AC$ ; then will  $ABC$  be the required triangle.

TRIGONOMETRICALLY.

$BC + BA = 540 + 450 = 990$ ; and  $BC - BA = 540 - 450 = 90$ .

$A + C = 180^\circ - B = 180^\circ - 80^\circ = 100^\circ$ , and therefore,

$$\frac{1}{2}(A + C) = \frac{1}{2}(100^\circ) = 50^\circ.$$

To find  $\frac{1}{2}(A - C)$ .

	$BC + BA$	990	ar. comp.	7.004365
:	$BC - BA$	90	. . . . .	1.954243
::	$\tan \frac{1}{2}(A + C)$	$50^\circ$	. . . . .	10.076187
:	$\tan \frac{1}{2}(A - C)$	$6^\circ 11'$	. . . . .	9.034795.

Hence,  $50^\circ + 6^\circ 11' = 56^\circ 11' = A$ ; and  $50^\circ - 6^\circ 11' = 43^\circ 49' = C$ .

To find the third side  $AC$ .

	$\sin C$	$43^\circ 49'$	ar comp.	0.159672
:	$\sin B$	$80^\circ$	. . . . .	9.993351
::	$AB$	450	. . . . .	2.653213
:	$AC$	640.082	. . . . .	2.806236.

2. Given two sides of a plane triangle, 1686 and 960, and their included angle  $128^\circ 04'$ : required the other parts.

Ans. Angles,  $33^\circ 34' 39''$ ;  $18^\circ 21' 21''$ ; side 2400.

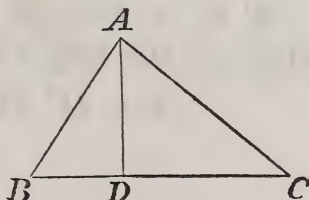
CASE IV.

32. Having given the three sides of a plane triangle, to find the angles.

Let fall a perpendicular from the angle opposite the greater side, dividing the given triangle into two right-angled triangles: then find the difference of the segments of the base by Theorem III. Half this difference being added to half the base, gives the greater segment; and, being subtracted from half the base, gives the less segment. Then, since the greater segment belongs to the right-angled triangle having the greater hypotenuse, we have two sides and the right angle of each of two right-angled triangles, to find the acute angles.

EXAMPLES.

1. The sides of a plane triangle being given; viz.,  $BC = 40$ ,  $AC = 34$ , and  $AB = 25$ : required the angles.



GEOMETRICALLY.

33. With the three given lines as sides construct a triangle as in Prob. IX. Then measure the angles of the triangle either with the protractor or scale of chords.

TRIGONOMETRICALLY.

$$BC : AC + AB :: AC - AB : CD - BD,$$

That is,  $40 : 59 :: 9 : \frac{59 \times 9}{40} = 13.275.$

Then,  $\frac{40 + 13.275}{2} = 26.6375 = CD,$

And,  $\frac{40 - 13.275}{2} = 13.3625 = BD.$

*In the triangle DAC, to find the angle DAC.*

AC	34	ar. comp.	8.468521
:	DC	26.6375 . . . . .	1.425493
::	sin D	90° . . . . .	10.000000
:	sin DAC	51° 34' 40" . . . . .	9.894014.

In the triangle  $BAD$ , to find the angle  $BAD$ .

	$AB$	25	ar. comp.	8.602060
:	$BD$	13.3625	. . . . .	1.125887
::	$\sin D$	$90^\circ$	. . . . .	10.000000
:	$\sin BAD$	$32^\circ 18' 35''$	. . . . .	9.727947.

Hence,  $90^\circ - DAC = 90^\circ - 51^\circ 34' 40'' = 38^\circ 25' 20'' = C$ ,  
 and,  $90^\circ - BAD = 90^\circ - 32^\circ 18' 35'' = 57^\circ 41' 25'' = B$ ,  
 and,  $BAD + DAC = 51^\circ 34' 40'' + 32^\circ 18' 35'' = 83^\circ 53' 15'' = A$ .

2. In a triangle, of which the sides are 4, 5, and 6, what are the angles?

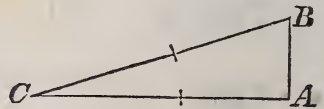
*Ans.*  $41^\circ 24' 35''$ ;  $55^\circ 46' 16''$ ; and  $82^\circ 49' 09''$ .

SOLUTION OF RIGHT-ANGLED TRIANGLES.

34. The unknown parts of a right-angled triangle may be found by either of the four last cases; or, if two of the sides are given, by means of the property that the square of the hypotenuse is equivalent to the sum of the squares of the two other sides. Or the parts may be found by Theorems IV. and V.

EXAMPLES.

1. In a right-angled triangle  $BAC$ , there are given the hypotenuse  $BC = 250$ , and the base  $AC = 240$ : required the other parts.



To find the angle  $B$ .

	$BC$	250	ar. comp.	7.602060
:	$AC$	240	. . . . .	2.380211
::	$\sin A$	$90^\circ$	. . . . .	10.000000
:	$\sin B$	$73^\circ 44' 23''$	. . . . .	9.982271.

But  $C = 90^\circ - B = 90^\circ - 73^\circ 44' 23'' = 16^\circ 15' 37''$ :

Or  $C$  may be found from the proportion.

	$CB$	350	ar. comp.	7.602060
:	$AC$	240	.	2.380211
::	$R$	.	.	10.000000
:	$\cos C$	$16^\circ 15' 37''$	.	9.982271.

To find side  $AB$  by Theorem IV.

	$R$	ar. comp.	0.000000
:	$\tan C$	$16^\circ 15' 37''$	9.464889
::	$AC$	240	2.380211
:	$AB$	70.0003	1.845100.

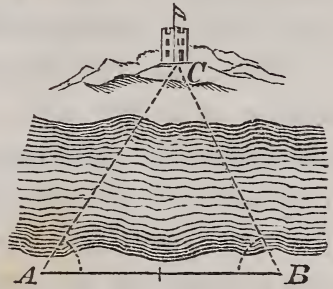
2. In a right-angled triangle  $BAC$ , there are given  $AC=384$ , and  $B=53^\circ 08'$ : required the remaining parts.

*Ans.*  $AB=287.96$ ;  $BC=479.979$ ;  $C=36^\circ 52'$ .

APPLICATION TO HEIGHTS AND DISTANCES.

I. To determine the horizontal distance to a point which is inaccessible by reason of an intervening river.\*

35. Let  $C$  be the point. Measure along the bank of the river a horizontal base line  $AB$ , and select the stations  $A$  and  $B$ , in such a manner that each can be seen from the other, and the point  $C$  from both of them. Then measure the horizontal angles  $CAB$  and  $CBA$ , with an instrument adapted to that purpose.



Let us suppose that we have found  $AB=600$  yards,  $CAB=57^\circ 35'$ , and  $CBA=64^\circ 51'$ .

The angle  $C=180^\circ - (A + B)=57^\circ 34'$ .

To find the distance  $BC$ .

	$\sin C$	57° 34'	ar. comp.	0.073649
:	$\sin A$	57° 35'	.	9.926431
::	$AB$	600	.	2.778151
:	$BC$	600.11 yards	.	2.778231.

\* Read, definitions, from 3 to 14, pages 64 and 65.

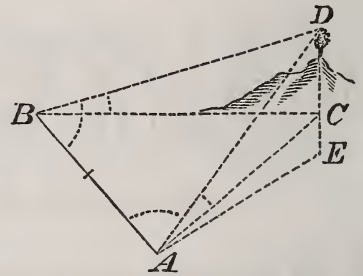
To find the distance  $AC$ .

sin $C$	57° 34'	ar. comp.	0.073649
: sin $B$	64° 51'	. . . . .	9.956744
:: $AB$	600	. . . . .	<u>2.778151</u>
: $AC$	643.94 yards	. . . . .	<u>2.808544.</u>

II. To determine the altitude of an inaccessible object above a given horizontal plane.

FIRST METHOD.

36. Suppose  $D$  to be the inaccessible object, and  $BC$  the horizontal plane from which the altitude is to be estimated: then, if we suppose  $DC$  to be a vertical line, it will represent the required distance.



Measure any horizontal base line, as  $BA$ ; and at the extremities  $B$  and  $A$ , measure the horizontal angles  $CBA$  and  $CAB$ . Measure also the angle of elevation  $DBC$ .

Then in the triangle  $CBA$  there will be known, two angles and the side  $AB$ ; the side  $BC$  can therefore be determined. Having found  $BC$ , we shall have, in the right-angled triangle  $DBC$ , the base  $BC$  and the angle at the base, to find the perpendicular  $DC$ , which measures the altitude of the point  $D$  above the horizontal plane  $BC$ .

Let us suppose that we have found

$BA = 780$  yards, the horizontal angle  $CBA = 41^\circ 24'$ ; the horizontal angle  $CAB = 96^\circ 28'$ , and the angle of elevation  $DBC = 10^\circ 43'$ .

In the triangle  $BCA$ , to find the horizontal distance  $BC$ . The angle  $BCA = 180^\circ - (41^\circ 24' + 96^\circ 28') = 42^\circ 08' = C$ .

sin $C$	42° 08'	ar. comp.	0.173369
: sin $A$	96° 28'	. . . . .	9.997228
:: $AB$	780	. . . . .	<u>2.892095</u>
: $BC$	1155.29	. . . . .	<u>3.062692.</u>

*In the right-angled triangle DBC, to find DC.*

	<i>R</i>	ar. comp.	0.000000
:	tan <i>DBC</i>	10° 43' . . . . .	9.277043
::	<i>BC</i>	1155.29 . . . . .	3.062692
:	<i>DC</i>	218.64 . . . . .	<u>2.339735.</u>

REMARK I. It might, at first, appear, that the solution which we have given, requires that the points *B* and *A* should be in the same horizontal plane; but it is entirely independent of such a supposition.

For, the horizontal distance, which is represented by *BA*, is the same, whether the station *A* is on the same level with *B*, above it, or below it. The horizontal angles *CAB* and *CBA* are also the same, so long as the point *C* is in the vertical line *DC*. Therefore, if the horizontal line through *A* should cut the vertical line *DC*, at any point, as *E*, above or below *C*, *AB* would still be the horizontal distance between *B* and *A*, and *AE*, which is equal to *AC*, would be the horizontal distance between *A* and *C*.

If at *A*, we measure the angle of elevation of the point *D*, we shall know in the right-angled triangle *DAE*, the base *AE*, and the angle at the base; from which the perpendicular *DE* can be determined.

37. Let us suppose that we had measured the angle of elevation *DAE*, and found it equal to 20° 15'.

*First: In the triangle BAC, to find AC or its equal AE.*

	<i>R</i>	ar. comp.	0.173369
:	sin <i>C</i>	42° 08' . . . . .	9.820406
::	<i>AB</i>	780 . . . . .	2.892095
:	<i>AC</i>	768.9 . . . . .	<u>2.885870.</u>

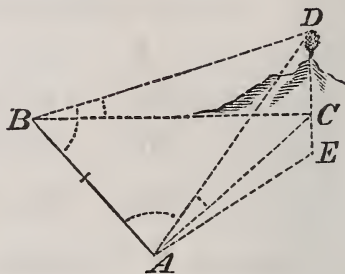
*In the right-angled triangle DAE, to find DE.*

	<i>R</i>	ar. comp.	0.000000
:	tan <i>A</i>	20° 15' . . . . .	9.566932
::	<i>AE</i>	768.9 . . . . .	2.885870
:	<i>DE</i>	283.66 . . . . .	<u>2.452802.</u>

Now, since  $DC$  is less than  $DE$ , it follows that the station  $B$  is above the station  $A$ . That is,

$$DE - DC = 283.66 - 218.64 = 65.02 = EC,$$

which expresses the vertical distance that the station  $B$  is above the station  $A$ .



REMARK II. It should be remembered, that the vertical distance which is obtained by the calculation, is estimated from a horizontal line passing through the eye at the time of observation. Hence, the height of the instrument is to be added, in order to obtain the true result.

#### SECOND METHOD.

38. When the nature of the ground will admit of it, measure a base line  $AB$  in the direction of the object  $D$ . Then measure with the instrument the angles of elevation at  $A$  and  $B$ .

Then, since the outward angle  $DBC$  is equal to the sum of the angles  $A$  and  $ADB$ ,

it follows that the angle  $ADB$  is equal to the difference of the angles of elevation at  $A$  and  $B$ . Hence, we can find all the parts of the triangle  $ADB$ . Having found  $DB$ , and knowing the angle  $DBC$ , we can find the altitude  $DC$ .



This method supposes that the stations  $A$  and  $B$  are on the same horizontal plane; and therefore it can only be used when the line  $AB$  is nearly horizontal.

Let us suppose that we have measured the base line, and the two angles of elevation, and

$$\text{found } \begin{cases} AB = 975 \text{ yards,} \\ A = 15^\circ 36', \\ DBC = 27^\circ 29'; \end{cases}$$

required the altitude  $DC$ .



First:  $ADB = DBC - A = 27^\circ 29' - 15^\circ 36' = 11^\circ 53'$ .

*In the triangle ADB, to find BD.*

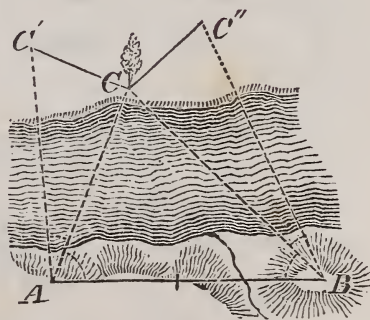
sin D	11° 53'	ar. comp.	0.686302
: sin A	15° 36'	. . . . .	9.429623
:: AB	975	. . . . .	2.989005
: DB	1273.3	. . . . .	<u>3.104930.</u>

*In the triangle DBC, to find DC.*

R		ar. comp.	0.000000
: sin B	27° 29'	. . . . .	9.664163
:: DB	1273.3	. . . . .	3.104930
: DC	587.61	. . . . .	<u>2.769093.</u>

III. To determine the perpendicular distance of an object below a given horizontal plane.

39. Suppose  $C$  to be directly over the given object, and  $A$  the point through which the horizontal plane is supposed to pass.



Measure a horizontal base line  $AB$ , and at the stations  $A$  and  $B$  conceive the two horizontal lines  $AC, BC$ , to be drawn. The

oblique lines from  $A$  and  $B$  to the object are the hypotenuses of two right-angled triangles, of which  $AC, BC$ , are the bases. The perpendiculars of these triangles are the distances from the horizontal lines  $AC, BC$ , to the object. If we turn the triangles about their bases  $AC, BC$ , until they become horizontal, the object, in the first case, will fall at  $C'$ , and in the second at  $C''$ .

Measure the horizontal angles  $CAB, CBA$ , and also the angles of depression  $C'AC, C''BC$ .

Let us suppose that we have

$$\text{found } \begin{cases} AB = 672 \text{ yards} \\ BAC = 72^\circ 29' \\ ABC = 39^\circ 20' \\ C'AC = 27^\circ 49' \\ C''BC = 19^\circ 10'. \end{cases}$$

First: in the triangle  $ABC$ ,  
the horizontal angle  $ACB = 180^\circ - (A + B) = 180^\circ - 111^\circ 49' = 68^\circ 11'$ .

*To find the horizontal distance  $AC$ .*

sin $C$	$68^\circ 11'$	ar. comp.	0.032275
: sin $B$	$39^\circ 20'$	. . . . .	9.801973
:: $AB$	672	. . . . .	<u>2.827369</u>
: $AC$	458.79	. . . . .	<u>2.661617.</u>

*To find the horizontal distance  $BC$ .*

sin $C$	$68^\circ 11'$	ar. comp.	0.032275
: sin $A$	$72^\circ 29'$	. . . . .	9.979380
:: $AB$	672	. . . . .	<u>2.827369</u>
: $BC$	690.28	. . . . .	<u>2.839024.</u>

*In the triangle  $CAC'$ , to find  $CC'$ .*

$R$		ar. comp.	0.000000
: tan $C'AC$	$27^\circ 49'$	. . . . .	9.722315
:: $AC$	458.79	. . . . .	<u>2.661617</u>
: $CC'$	242.06	. . . . .	<u>2.383932.</u>

*In the triangle  $CBC''$ , to find  $CC''$ .*

$R$		ar. comp.	0.000000
: tan $C''BC$	$19^\circ 10'$	. . . . .	9.541061
:: $BC$	690.28	. . . . .	<u>2.839024</u>
: $CC''$	239.93	. . . . .	<u>2.380085.</u>

Hence also,  $CC' - CC'' = 242.06 - 239.93 = 2.13$  yards,  
which is the height of the station  $A$  above station  $B$ .

PROBLEMS.

1. Wanting to know the distance between two inaccessible objects, which lie in a direct level line from the bottom of a tower of 120 feet in height, the angles of depression are measured from the top of the tower, and are found to be, of the nearer  $57^\circ$ , of the more remote  $25^\circ 30'$ : required the distance between the objects.

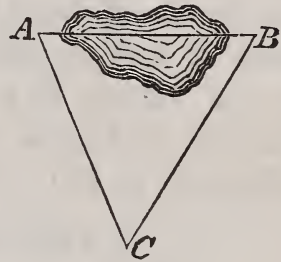
*Ans.* 173.656 feet.

2. In order to find the distance between two trees,  $A$  and  $B$ , which could not be directly measured because of a pool which occupied the intermediate space, the distances of a third point  $C$  from each of them were measured, and also the included angle  $ACB$ : it was found that,

$$\begin{aligned} CB &= 672 \text{ yards,} \\ CA &= 588 \text{ yards,} \\ ACB &= 55^\circ 40'; \end{aligned}$$

required the distance  $AB$ .

*Ans.* 592.967 yards.



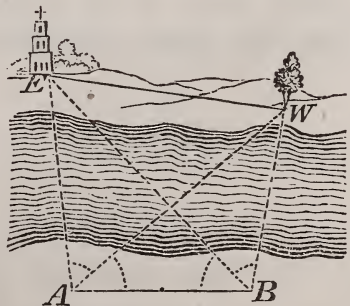
3. Being on a horizontal plane, and wanting to ascertain the height of a tower, standing on the top of an inaccessible hill, there were measured, the angle of elevation of the top of the hill  $40^\circ$ , and of the top of the tower  $51^\circ$ ; then measuring in a direct line 180 feet farther from the hill, the angle of elevation of the top of the tower was  $33^\circ 45'$ ; required the height of the tower.

*Ans.* 83.998.

4. Wanting to know the horizontal distance between two inaccessible objects  $E$  and  $W$ , the following measurements were made.

$$\text{viz. } \begin{cases} AB = 536 \text{ yards} \\ BAW = 40^\circ 16' \\ WAE = 57^\circ 40' \\ ABE = 42^\circ 22' \\ EBW = 71^\circ 07'; \end{cases}$$

required the distance  $EW$ .



*Ans.* 939.527 yards.

5. Wanting to know the horizontal distance between two inaccessible objects  $A$  and  $B$ , and not finding any station from which both of them could be seen, two points  $C$  and  $D$ , were chosen at a distance from each other, equal to 200 yards; from the former of these points  $A$  could be seen, and from the latter  $B$ , and at each of the points  $C$  and  $D$  a staff was set up. From  $C$  a distance  $CF$  was measured, not in the direction  $DC$ , equal to 200 yards, and from  $D$  a distance  $DE$  equal to 200 yards, and the following angles taken,

$$\text{viz. } \begin{cases} AFC = 83^\circ 00', & BDE = 54^\circ 30', \\ ACD = 53^\circ 30', & BDC = 156^\circ 25', \\ ACF = 54^\circ 31', & BED = 88^\circ 30'. \end{cases}$$

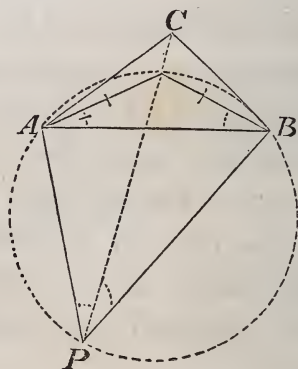
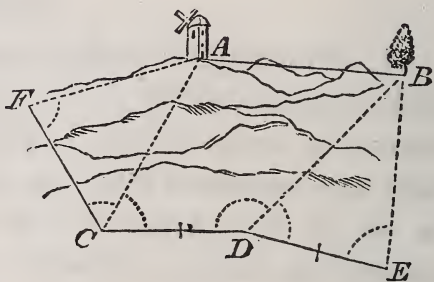
*Ans.*  $AB = 345.467$  yards.

6. From a station  $P$  there can be seen three objects,  $A$ ,  $B$  and  $C$ , whose distances from each other are known: viz.,  $AB = 800$ ,  $AC = 600$ , and  $BC = 400$  yards. Now, there are measured the horizontal angles.

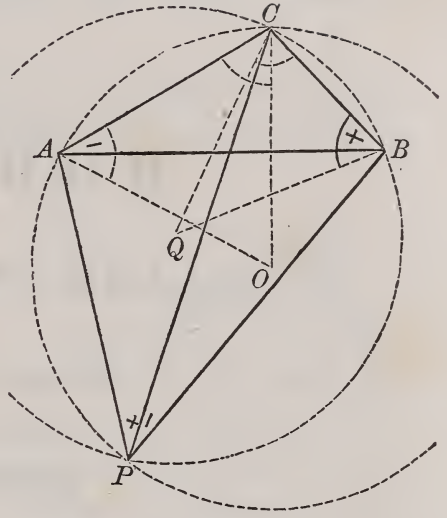
$APC = 33^\circ 45'$  and  $BPC = 22^\circ 30'$ : it is required to find the three distances  $PA$ ,  $PC$ , and  $PB$ .

$$\text{Ans. } \begin{cases} PA = 710.193 \text{ yards.} \\ PC = 1042.522 \\ PB = 934.291. \end{cases}$$

7. This problem is much used in maritime surveying, for the purpose of locating buoys and sounding boats. The trigonometrical solution is somewhat tedious, but it may be solved geometrically by the following easy construction.



Let  $A$ ,  $B$ , and  $C$  be the three fixed points on shore, and  $P$  the position of the boat from which the angles  $APC = 33^\circ 45'$ ,  $CPB = 22^\circ 30'$ , and  $APB = 56^\circ 15'$ , have been measured.



Subtract twice  $APC = 67^\circ 30'$  from  $180^\circ$ , and lay off at  $A$  and  $C$  two angles,  $CAO$ ,  $ACO$ , each equal to half the remainder  $= 56^\circ 15'$ . With the point  $O$ , thus determined, as a centre, and  $OA$  or  $OC$  as a radius, describe the circumference of a circle: then, any angle inscribed in the segment  $APC$ , will be equal to  $33^\circ 45'$ .

Subtract, in like manner, twice  $CPB = 45^\circ$ , from  $180^\circ$ , and lay off half the remainder  $= 67^\circ 30'$ , at  $B$  and  $C$ , determining the centre  $Q$  of a second circle, upon the circumference of which the point  $P$  will be found. The required point  $P$  will be at the intersection of these two circumferences. If the point  $P$  fall on the circumference described through the three points  $A$ ,  $B$ , and  $C$ , the two auxiliary circles will coincide, and the problem will be indeterminate.

# B O O K I I.

## PLANE SURVEYING.

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### SECTION I.

DEFINITIONS.—MEASUREMENT OF ANGLES AND LINES.

1. SURVEYING, in its most extensive signification, comprises all the operations necessary for finding,

1st. The area or contents of any portion of the surface of the earth ;

2d. The lengths and directions of the bounding lines ;  
and,

3d. For making accurate delineations of the surface and bounding lines on paper.

It is divided into two branches, *Plane* and *Geodesic Surveying*.

2. The radius of the earth being very large, the curvature may be neglected, when the survey is limited to small portions of the surface. This branch is called *Plane Surveying*.

When the curvature is taken into account, as it must be in all extensive surveys, the method of measurement and computation is called *Geodesic Surveying*.

3. If at any point of the surface of the earth, regarded as a sphere, a plane be passed perpendicular to the radius, it will be tangent to the surface. Such a plane, and all planes parallel to it, are called *horizontal planes*.

4. A plane perpendicular to a horizontal plane, at a given point, is called a *vertical plane*.

5. All lines of horizontal planes are called *horizontal lines*.

6. Lines which are perpendicular to a horizontal plane, are called *vertical lines*; and all lines which are inclined to it, are called *oblique lines*.

Thus,  $AB$  and  $DC$  are horizontal lines;  $BC$  and  $AD$  are vertical lines; and  $AC$  and  $BD$  are oblique lines.



7. The horizontal distance between two points, is the horizontal line intercepted between the two vertical lines passing through those points. Thus,  $DC$  or  $AB$  is the horizontal distance between the two points  $A$  and  $C$ , or the points  $B$  and  $D$ .

8. A *horizontal angle* is one whose sides are horizontal; its plane is also horizontal.

A horizontal angle may also be defined to be, *the angle included between two vertical planes passing through the angular point, and the two objects which subtend the angle*.

9. A vertical angle is one, the plane of whose sides is vertical.

10. An angle of *elevation*, is a vertical angle having one of its sides horizontal, and the inclined side above the horizontal side.

Thus, in the last figure,  $BAC$  is the angle of elevation from  $A$  to  $C$ .

11. An angle of *depression*, is a vertical angle having one of its sides horizontal, and the inclined side under the horizontal side. Thus,  $DCA$  is the angle of depression from  $C$  to  $A$ .

12. An *oblique angle* is one, the plane of whose sides is oblique to a horizontal plane.

13. All lines, which can be the object of measurement, must belong to one of the classes above named, viz.:

- 1st. Horizontal lines:
- 2d. Vertical lines:
- 3d. Oblique lines.

14. All the angles may also be divided into three classes, viz.:

- 1st. Horizontal angles:
- 2d. Vertical angles; which include angles of elevation and angles of depression: and
- 3d. Oblique angles, or those included by oblique lines.

#### OF THE MEASUREMENT OF LINES AND ANGLES.

15. It has been shown (Bk. I., Sec. III., Art. 1), that at least one side and two of the other parts of a plane triangle must be given or known, before the remaining parts can be found by calculation.

When, therefore, distances are to be found, by trigonometrical calculations, two preliminary steps are necessary:

- 1st. To measure certain lines on the ground:
- 2d. To measure such angles as may be necessary to determine the required parts.

#### MEASURES FOR DISTANCES.

16. Any tape, rod, or chain, divided into equal parts, may be used as a measure; and one of these equal parts is called the *unit* of the measure. The unit of a measure may be a foot, a yard, a rod, or any other ascertained distance.

The measure in general use, is a chain of four rods or sixty-six feet in length; it is called Gunter's chain, from the name of the inventor. This chain is composed of 100 links. Every tenth link from either end, is marked by a small attached brass plate, which is notched, to designate its number from the end. The division of the chain into 100 equal parts, is a very convenient one, since the divisions or links are decimals of the whole chain, and in the calculations may be treated as such.



## TABLE.

1 chain = 4 rods = 66 feet = 792 inches = 100 links.

Hence, 1 link is equal to 7.92 inches.

80 chains = 320 rods = 1 mile.

40 chains =  $\frac{1}{2}$  mile.

20 chains =  $\frac{1}{4}$  mile.

17. Besides the chain, there are needed for measuring, ten marking pins, which should be of iron, each about ten inches in length and an eighth of an inch in thickness. These pins should be strung upon an iron ring, and this ring should be attached to a belt, to be passed over the right shoulder, suspending the pins at the left side. Two staves are also required. Each of these should be about six feet in length, and have a spike in the lower end to aid in holding it firmly, and a horizontal strip of iron to prevent the chain from slipping off; these staves are to be passed through the rings at the ends of the chain.

## TO MEASURE A HORIZONTAL LINE.

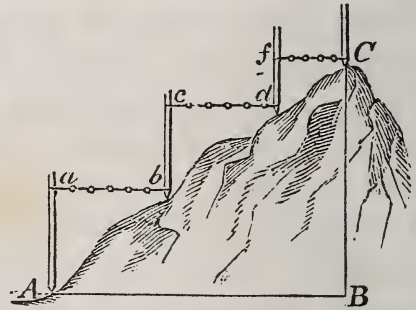
18. At the point where the measurement is to be begun, place, in a vertical position, a signal staff, having a small flag attached to its upper extremity; and place another at the point where the measurement is to be terminated. These two points are generally called *stations*.

Having passed the staves through the rings of the chain, let the ten marking pins and one end of the chain be taken by the person who is to go forward, and who is called the leader, and let him plant the staff as nearly as possible in the direction of the stations. Then, taking the staff in his right hand, let him stand off at arm's length, so that the person at the other end of the chain can align it exactly with the stations: when the alignment is made, let the chain be stretched and a marking pin placed; then measure a second chain in the same manner, and so on, until all the marking pins shall have been placed. When the marking pins are exhausted, a note should be made, that ten chains have been measured; after which, the marking pins are to be returned to the leader, and the

measurement continued as before, until the whole distance is passed over. It will be found desirable to fasten pieces of red cloth to the heads of the marking pins, that they may be more readily found in thick grass, brushwood, &c.

Great care must be taken to keep the chain horizontal, and if the slope of the ground be too great to admit of measuring a whole chain at a time, a part of a chain only should be measured: the sum of all the horizontal lines so measured, is evidently the horizontal distance between the stations.

For example, in measuring the horizontal distance between  $A$  and  $C$ , we first place a staff at  $A$  and another at  $b$ , in the direction towards  $C$ . Then slide up the chain on the staff at  $A$  until it becomes horizontal, and note the distance  $ab$ .



Then remove the staves and place them at  $b$  and  $d$ : make the chain horizontal, and note the distance  $cd$ . Measure in the same manner the line  $fC$ ; the sum of the horizontal lines  $ab$ ,  $cd$ ,  $fC$ , is equal to  $AB$ , the horizontal distance between  $A$  and  $C$ .

19. The length of the chain should be compared, from time to time, with a *standard* kept for the purpose.

To facilitate this comparison, let two stakes be driven in the ground, distant from each other *one chain*, and let nails be driven in the heads of the stakes to mark the exact length of the standard.

Marks made upon the coping of a wall will answer the same purpose. If it is found that any line has been measured with a chain, either too short or too-long, the measured distance may be corrected by the following proportion:

As the length of the chain  
 : the length of the standard  
 :: the measured distance  
 : the true distance.

For the correction of areas we have this proportion,

As the square of the length of the chain  
 : the square of the length of the standard,  
 :: the area found  
 : the area required.

#### MEASUREMENT OF ANGLES.

20. We come now to the measurement of angles, and for this purpose several instruments are used. The one, however, which affords the most accurate results, and which indeed can alone be relied on for nice or extensive operations, is called a Theodolite. This instrument only will be described at present; others will be subsequently explained.

#### OF THE THEODOLITE.

Pl. 1. The theodolite is an instrument used to measure horizontal and vertical angles. It is usually placed on a tripod  $ABC$ , which enters by means of a screw the lower horizontal plate  $DE$ , and becomes firmly attached to the body of the instrument. Through the horizontal plate  $DE$ , four small hollow cylinders are inserted, which receive four screws with milled heads, that work against a second horizontal plate,  $FG$ . The upper side of the plate  $DE$  terminates in a curved surface, which encompasses a ball, that is nearly a semi-sphere, with the plane of its base horizontal. This ball, which is hollow, is firmly connected with the smaller base of a hollow conic frustum, that passes through the curved part of the plate  $DE$ , and screws firmly into the curved part of the second horizontal plate  $FG$ .

A hollow conic spindle passes through the middle of the ball, and the hollow frustum with which it is connected. To this spindle, a third horizontal and circular plate  $HI$ , called *the limb of the instrument*, is permanently attached. Within this spindle, and concentric with it, there is a second spindle, called the *inner, or solid spindle*. To this latter, is united a thin circular plate, called the *vernier plate*,

which rests on the limb of the instrument, and supports the upper frame-work. The two spindles terminate at the base of the spherical ball, where a small screw enters the inner one, and presses a washer against the other, and the base of the ball. On the upper surface of the plate  $FG$ , rests a clamp which goes round the outer spindle, and which, being compressed by the clamp-screw  $K$ , is made fast to it. This clamp is thus connected with the plate  $FG$ . A small cylinder  $a$ , is fastened to the plate  $FG$ : through this cylinder a thumb-screw  $L$  passes, and works into a small cylinder  $b$ , connected with the clamp. The cylinders  $b$  and  $a$ , admit of a motion round their axes, to relieve the screw  $L$  of the pressure which would otherwise be occasioned by working it.

Directly above the clamp, is the lower telescope  $MN$ . This telescope is connected with a hollow cylinder, which is worked freely round the outer spindle, by the thumb-screw  $P$  having a pinion working into a concealed cog-wheel, that is permanently fastened to the limb of the instrument. By means of a clamp-screw  $Q$ , the telescope is made fast to the limb, when it will have a common motion with the limb and outer spindle.

The circular edge of the limb is chamfered, and is generally made of silver, and on this circle the graduation for horizontal angles is made. In the instrument described, the circle is cut into degrees and half degrees; the degrees are numbered from 0 to 360.

On the circular edge of the vernier plate, is a small plate of silver, called a *vernier*; this plate is divided into 30 equal parts, and numbered from the line marked 0 to the left. Two levels, at right angles to each other, are attached to the vernier plate by small adjusting screws; one of the levels is seen in the figure.

The vernier plate turns freely around with the inner spindle. It is made fast to the limb of the instrument by the clamp-screw  $S$ ; after which the smaller motions are made by the tangent-screw  $T$ . There is a compass on the vernier plate, that is concentric with it, the use of which will be explained under the head compass.

The frame-work which supports the horizontal axis of the vertical semicircle  $UV$  and the upper telescope, with its attached level, rests on the vernier plate, to which it is made fast by three adjusting screws, placed at the angular points of an equilateral triangle. The vertical semicircle  $UV$ , is called the *vertical limb*; its motions are governed by the thumb-screw  $Z$ , which has a pinion, that works with the teeth of the vertical limb. On the face of the vertical limb, opposite the thumb-screw  $Z$ , the limb is divided into degrees and half degrees: the degrees are numbered both ways from the line marked 0. There is a small plate resting against the graduated face of the vertical limb, called the vernier; it is divided into 30 equal parts, and the middle line is designated by 0.

On the other face of the vertical limb, are two ranges of divisions, commencing at the 0 point, and extending each way  $45^\circ$ . The one shows the vertical distance of any object to which the upper telescope is directed, above or below the place of the instrument, in 100th parts of the horizontal distance: the other, the difference between the hypotenusal and base lines: the hypotenuse being supposed to be divided into one hundred equal parts: therefore, by mere inspection, we can ascertain the number of links, which must be subtracted from every chain of an oblique line, to reduce it to a true horizontal distance.

The supports of the upper telescope are called the wyes, and designated  $Y$ 's. Two loops, turning on hinges, pass over the telescope, and are made fast by the pins  $c$  and  $d$ ; these loops confine the telescope in the  $Y$ 's. By withdrawing the pins, and turning the loops on their hinges, the telescope may be removed for the purpose of being reversed in position; and in both situations, the telescope can be revolved in the  $Y$ 's about its axis.

In the telescopes attached to the theodolite, are two principal lenses, one at each end. The one at the end where the eye is placed, is called the eye-glass, the other the object-glass.

In order that the axis of the telescope may be directed to an object with precision, two spider's lines, or small

hairs, are fixed at right angles to each other, and placed within the barrel of the telescope, and at the focus of the eye-glass. The vertical hair is moved by two small horizontal screws, one of which,  $f$ , is seen in the figure; and the horizontal hair, by two vertical screws,  $g$  and  $h$ .

Before using the instrument it must be *adjusted*, that is, the parts must be brought to their proper relative positions: there are *four* principal *adjustments*.

FIRST ADJUSTMENT.—*To fix the intersection of the spider's lines in the line of collimation or axis of the telescope.*

Having screwed the tripod to the instrument, extend the legs, and place them firmly. Then loosen the clamp-screw  $S$  of the vernier plate, and direct the telescope to a small, well-defined, and distant object. By means of a small pin  $i$ , on the under side of the telescope, slide the eye-glass till the spider's lines are seen distinctly; then with the thumb-screw  $X$ , which forces out and draws in, the object-glass, adjust this glass to its proper focus, when the object, as well as the spider's lines, will be distinctly seen: after which, by the tangent-screw  $T$  and the thumb-screw  $Z$ , bring the intersection of the spider's lines exactly upon a well-defined point of the object.

Having done this, revolve the telescope in the  $Y$ 's half round, when the attached level  $mn$ , will come to the upper side. See, in this position, if the horizontal hair appears above or below the point, and in either case, loosen one, and tighten the other, of the two screws that work the horizontal hair, till the horizontal hair has been carried over half the space between its last position and the observed point. Carry the telescope back to its place; direct again the intersection of the spider's lines to the point, and repeat the operation till the horizontal hair neither ascends nor descends, while the telescope is revolved. A similar process will arrange the vertical hair, and the line of collimation is then adjusted.

SECOND ADJUSTMENT.—*To make the axis of the attached level of the upper telescope, parallel to the line of collimation.*

Turn the vernier plate, till the telescope comes directly

over two of the levelling screws, between the plates *DE* and *FG*. Turn these screws contrary ways, keeping them firm against the plate *FG*, till the bubble of the level *mn*, stands at the middle of the tube. Then, open the loops, and reverse the telescope. If the bubble still stands in the middle of the tube, the axis of the tube is horizontal; but if not, it is inclined, the bubble being at the elevated end. In that case, by means of the small vertical screws *m* and *n*, at the ends of the level, raise the depressed end, or depress the elevated one, half the inclination; and then, with the levelling screws, bring the level into a horizontal position. Reverse the telescope in the *Y*'s, and make the same correction again; and so on, until the bubble stands in the middle of the tube, in both positions of the telescope: the axis of the level is then horizontal. Let the telescope be now revolved in the *Y*'s. If the bubble continue in the middle of the tube, the axis of the level is not only horizontal, but also parallel to the line of collimation. If, however, the bubble recede from its centre, the axis of the level is inclined to the line of collimation, and must be made parallel to it by means of two small antagonistic screws, (one of which is seen at *p*,) which work horizontally. By loosening one of them, and tightening the other, the level is soon brought parallel to the line of collimation, and then, if the telescope be revolved in the *Y*'s, the bubble will continue in the middle of the tube.

It is difficult to make the first part of this adjustment, while the axis of the level is considerably inclined to the line of collimation; for, if the level were truly horizontal in one position of the telescope, when the telescope is reversed, the bubble would not stand in the middle of the tube, except in one position of the level. This suggests the necessity of making the first part of the adjustment with tolerable accuracy; then, having made the second with care, let the first be examined, and proceed thus till the adjustment is completed.

THIRD ADJUSTMENT.—*To make the axes of the levels on the limb perpendicular to the axis of the instrument.*

This adjustment is effected, partly by the levelling

screws, and partly by the thumb-screw *Z*. Turn the vernier plate, until the upper telescope comes directly over two of the levelling screws, then turn them contrary ways, till the upper telescope is horizontal; after which, turn the vernier plate  $180^\circ$ , and if the bubble of the level remains in the middle of the tube, one line of the limb is horizontal. But if the bubble recede from the centre of the level, raise the lower, or depress the upper end, one-half by the levelling screws, the other by the thumb-screw *Z*, till it is brought into a horizontal position. Turn the vernier plate again  $180^\circ$ , and if the level be not then horizontal, make it so, by dividing the error as before, and repeat the operation until the line of the limb is truly horizontal. Then turn the vernier plate  $90^\circ$ , and level as before. The limb ought now to be truly horizontal; but lest the first horizontal line may have been changed, in obtaining the second, it is well to bring the telescope and level two or three times over the levelling screws, until an entire revolution can be made without displacing the bubble from the middle of the tube. As this can only be the case when the level revolves around a vertical line, it follows that the limb will then be horizontal, and the axis of the instrument vertical. Then, by means of the small screws at the ends of the levels, bring the bubbles to the centres, and the axes of the levels will then be perpendicular to the axis of the instrument.

FOURTH ADJUSTMENT.—*To make the axis of the vertical limb perpendicular to the axis of the instrument.*

Bring the intersection of the spider's lines of the upper telescope upon a plumb line, or any well-defined vertical object, and move the telescope with the thumb-screw *Z*: if the intersection of the spider's lines continue on the vertical line, the axis is horizontal.

Or, the adjustment may be effected thus: Direct the intersection of the spider's lines to a well-defined point that is considerably elevated: then turn the vertical limb, until the axis of the telescope rests on some other well-defined point, upon or near the ground: reverse the telescope, and turn the vernier plate  $180^\circ$ ; now, if in elevating and depressing the telescope, the line of collimation passes



through the two points before noted, the axis is horizontal. If it be found, by either of the above methods, that the axis is not horizontal, it must be made so by the screws which fasten the frame-work to the vernier plate.

There are two important lines of the theodolite, the positions of which are determined with great care by the maker, and fixed permanently. First, the axis of the instrument is placed exactly at right angles with the limb and vernier plate; and unless it have this position, the vernier plate will not revolve at right angles to the axis, as explained in the third adjustment. Secondly, the line of collimation of the upper telescope is fixed at right angles to the horizontal axis of the vertical limb. We can ascertain whether these last lines are truly at right angles, by directing the intersection of the spider's lines to a well-defined point; then removing the caps which confine the horizontal axis in its supports, and reversing the axis: if the intersection of the spider's lines can be made to cover exactly the same point, without moving the vernier plate, the line of collimation is at right angles to the axis.

If the theodolite be so constructed that either of the *Y*'s admits of being moved laterally, so as to vary the angle between the horizontal axis and the line of collimation, these lines may be adjusted at right angles to each other, if they have not been so placed by the maker.

The lower telescope being used merely as a guard, requires no adjustment, although it is better to make the axis, about which its vertical motions are performed, horizontal, or perpendicular to the axis of the instrument; and this is easily effected by means of the two small screws *k* and *l*, which work into the slide *A'*, that is connected with the horizontal axis.

Having explained the methods of properly adjusting the theodolite, we will now explain the particular uses of its several parts, and the manner of measuring angles.

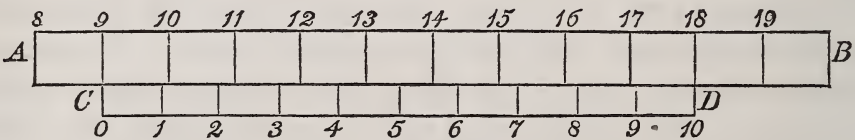
#### VERNIERS.

21. Before explaining the vernier, as applied to the theodolite, we shall discuss the general theory of verniers.

A Vernier is a contrivance for measuring parts of the equal spaces marked off on a given scale or limb.

It is a graduated scale, so arranged, as to cover an exact number of equal spaces on the primary scale or *limb*, to which it is applied. It is divided into a number of equal parts, greater by one than the number of equal spaces which it covers on the limb.

The vernier may be applied to any scale of equal parts. The modes of its application are extremely various; the principle, however, is the same in all, and may be illustrated by a simple diagram.



Let  $AB$  be any *limb* or scale of equal parts, one of which let us suppose equal to  $b$ . Let  $CD$  be a *vernier*, equal in length to nine of these parts, and itself divided into ten equal spaces, each one of which is then equal to nine-tenths of  $b$ . The *difference* between a space on the limb and a space on the vernier, is therefore equal to one-tenth of  $b$  or  $\frac{1}{10}b$ . This is the least space that can be measured by means of the vernier, and is called the *least count*; hence,

*The least count of a vernier is equal to one of the equal divisions of the limb divided by the number of spaces on the vernier.*

22. The true reading of the instrument, for any position of the vernier, expresses the distance from the point where the graduation on the limb begins, marked 0, to the 0 point of the vernier. In the diagram, that distance is expressed by nine units of the scale, or 9.

If, now, the vernier be moved till the division 1 coincides with the division 10 of the limb, the 0 point will have advanced along the limb a distance equal to  $\frac{1}{10}b$ , and the reading will become  $9 + \frac{1}{10}b$ . If we again move the vernier till the division 2 coincides with the division 11 of the scale, the 0 point will have advanced an additional distance, equal to  $\frac{1}{10}b$ , and the reading becomes

$9 + \frac{2}{10}b$ ; when 3 coincides with division 12, the reading will become  $9 + \frac{3}{10}b$ , and so on, till finally, when the point 10 coincides with 19 of the scale, the distance 9 will have been increased by  $\frac{10}{10}b$ , and will become 10, as it should, since, in that case, the 0 point will have been moved a whole space, and will coincide with the division 10 of the limb. Hence, the following rule for reading an instrument which has a vernier.

*Read the limb in the direction of the graduation up to the division line next preceding the 0 point of the vernier; this is called the reading on the limb. Look along the vernier till a dividing line is found to coincide with a line of the limb: multiply the number of this first line by the least count of the vernier: this is the reading on the vernier: the sum of these two readings is the reading of the instrument.*

23. In the theodolite described, the limb is divided into half degrees, and 30 spaces on the vernier cover 29 spaces on the limb. Hence, the least count of this instrument is  $\frac{1}{30}$  of a half degree or 1'. Fig. 2, Plate 1, exhibits the vernier of the horizontal limb, and Fig. 3 the vernier of the vertical limb.

#### TO MEASURE A HORIZONTAL ANGLE WITH THE THEODOLITE.

24. Place the axis of the instrument directly over the point at which the angle is to be measured. This is effected by means of a plumb, suspended from the plate which forms the upper end of the tripod.

Having made the limb truly level, place the 0 of the vernier at 0 or  $360^\circ$  of the limb, and fasten the clamp-screw  $S$  of the vernier plate. Then, facing in the direction between the lines which subtend the angle to be measured, turn the limb with the outer spindle, until the telescope points to the object on the left, very nearly. Clamp the limb with the clamp-screw  $K$ , and by means of the tangent screws  $L$  and  $Z$ , bring the intersection of the spider's lines to coincide exactly with the object.

Having loosened the clamp-screw  $Q$  of the lower telescope  $MN$ , direct it with the thumb-screw  $P$  to the

same object at which the upper telescope is directed; then tighten the clamp-screw  $Q$ . This being done, loosen the clamp-screw  $S$  of the vernier plate, and direct the telescope to the other object: the arc passed over by the 0 point of the vernier, is the measure of the angle sought.

The lower telescope having been made fast to the limb, will indicate any change of the position of the limb, should any have taken place; and, as the accuracy of the measurements depends on the fixedness of the limb, the lower telescope ought to be often examined, and if its position has been altered, the limb must be brought back to its place by the tangent-screw  $L$ .

It is not necessary to place the 0 point of the vernier at the 0 point of the limb, previously to commencing the measurement of the angle, but convenient merely; for, whatever be the position of this point on the limb, it is evident that the arc which it passes over is the true measure of the horizontal angle. If, therefore, its place be carefully noted for the first direction, and also for the second, the difference of these two readings will be the true angle, unless the 0 point of the vernier shall have passed the 0 point of the limb, in which case the greater reading must be subtracted from  $360^\circ$ , and the remainder added to the less.

#### TO MEASURE A VERTICAL ANGLE.

25. We shall first explain the method of determining the *index error*. Having levelled the horizontal limb, direct the telescope to some distinctly marked object as the top of a chimney, and read the instrument. Reverse the telescope in the  $Y$ 's, and turn the vernier plate  $180^\circ$ , and having directed the telescope to the same object, again read the instrument. If the two readings are the same, the limb is adjusted; that is, the 0 of the limb coincides with the 0 of its vernier, when the axis of the telescope is parallel to the horizontal limb.

When the reading found with the eye end of the telescope nearest the vernier, is greater than that obtained in the reversed position, the true elevation of the object

which is equal to a mean of the readings, may be obtained by *subtracting* half their difference from the first reading. If the first reading is less than the second, the half difference must be added to the first. Hence,

*To find the index error, take the reading of the limb when the telescope is directed to a fixed object, first with the eye end of the telescope nearest the vernier, and then with the telescope and vernier plate both reversed. Take half the difference of these readings, and affect it with a minus sign if the first is greater, or a plus sign if the second is the greater; this is equal to the index error.*

Let the operation be repeated several times, using different objects, and a mean of the errors will be more correct than the result of a single observation.

26. Having determined the index error, let the axis of the telescope be directed to any point either above or below the plane of the limb, and read the arc indicated by the 0 of the vernier. To the arc so read apply the proper correction, if any, and the result will be the true angle of elevation or depression.

The angle of elevation may be more correctly found by taking the elevation of the object, and repeating the observation with the telescope and vernier plate reversed, and then taking a mean of the readings for the angle required.

#### MEASUREMENTS WITH THE TAPE OR CHAIN ONLY.

27. It often happens that instruments for the measurement of angles cannot be easily obtained; we must then rely entirely on the tape or chain.

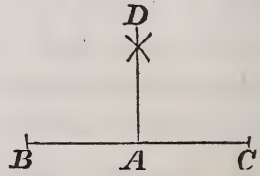
We now propose to explain the best methods of determining distances, without the aid of instruments for the measurement of horizontal or vertical angles.

I. *To trace, on the ground, the direction of a right line, that shall be perpendicular at a given point, to a given right line.*

#### FIRST METHOD.

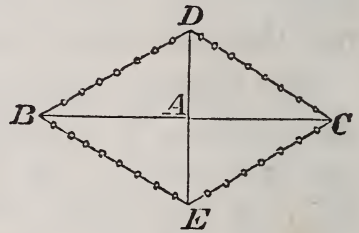
28. Let  $BC$  be the given right line, and  $A$  the given

point. Measure from  $A$ , on the line  $BC$ , two equal distances  $AB$ ,  $AC$ , one on each side of the point  $A$ . Take a portion of the chain or tape, greater than  $AB$ , and place one extremity at  $B$ , and with the other trace the arc of a circle on the ground. Then remove the end which was at  $B$ , to  $C$ , and trace a second arc intersecting the former at  $D$ . The straight line drawn through  $D$  and  $A$  will be perpendicular to  $BC$  at  $A$ .



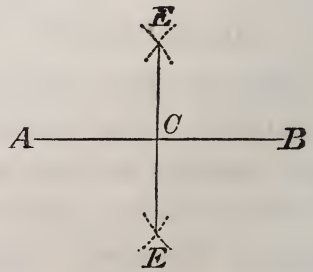
## SECOND METHOD.

29. Having made  $AB = AC$ , take any portion of the tape or chain considerably greater than the distance between  $B$  and  $C$ . Mark the middle point of it, and fasten its two extremities, the one at  $B$  and the other at  $C$ . Then, taking the chain by the middle point, stretch it tightly on either side of  $BC$ , and place a staff at  $D$  or  $E$ :  $DAE$  will be the perpendicular required.



## THIRD METHOD.

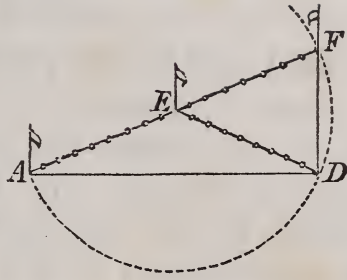
30. Let  $AB$  be the given line, and  $C$  the point at which the perpendicular is to be drawn. From the point  $C$  measure a distance  $CA$  equal to 8. With  $C$  as a centre, and a radius equal to 6, describe an arc on either side of  $AB$ : then, with  $A$  as a centre, and a radius equal to 10, describe a second arc intersecting at  $E$ , the one before described: then draw the line  $EC$ , and it will be perpendicular to  $AB$  at  $C$ .



REMARK. Any three lines, having the ratio of 6, 8, and 10, form a right-angled triangle, of which the side corresponding to 10 is the hypotenuse.

## FOURTH METHOD.

31. Let  $AD$  be the given right line, and  $D$  the point at which the perpendicular is to be drawn. Take any distance on the tape or chain, and place one extremity at  $D$ , and fasten the other at some point, as  $E$ , between



the two lines which are to form the right angle. Place a staff at  $E$ . Then, having stationed a person at  $D$ , remove that extremity of the chain and carry it round until it ranges on the line  $DA$  at  $A$ . Place a staff at  $A$ : then remove the end of the chain at  $A$ , and carry it round until it falls on the line  $AE$  at  $F$ . Then place a staff at  $F$ ;  $ADF$  will be a right angle, being an angle in a semicircle.

32. There is a very simple instrument, used exclusively in laying off right angles on the ground, which is called the

## SURVEYING CROSS.

Pl. 2, Fig. 1. This instrument consists of two bars,  $AB$  and  $CD$ , permanently fixed at right angles to each other, and firmly attached at  $E$  to a pointed staff, which serves as a support. Four sights are screwed firmly to the bars, by means of the screws  $a$ ,  $b$ ,  $c$ , and  $d$ .

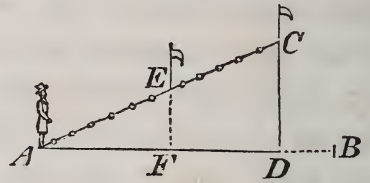
As the only use of this instrument is to lay off right angles, it is of the first importance that the lines of sight be truly at right angles. To ascertain if they are so, let the bar  $AB$  be turned until its sights mark some distinct object; then look through the other sights, and place a staff on the line which they indicate: let the cross be then turned until the sights of the bar  $AB$  come to the same line: if the other sights are directed to the first object, the lines of sight are exactly at right angles.

The sights being at right angles, if one of them be turned in the direction of a given line, the other will mark the direction of a line perpendicular to it, at the point where the instrument is placed.

II. *From a given point without a straight line, to let fall a perpendicular on the line.*

33. Let  $C$  be the given point, and  $AB$  the given line.

From  $C$  measure a line, as  $CA$ , to any point of the line  $AB$ . From  $A$ , measure on  $AB$  any distance as  $AF$ , and at  $F$  erect  $FE$  perpendicular to  $AB$ .



Having stationed a person at  $A$ , measure along the perpendicular  $FE$  until the forward staff is aligned on the line  $AC$ : then measure the distance  $AE$ . Now, by similar triangles, we have,

$$AE : AF :: AC : AD,$$

in which all the terms are known except  $AD$ , which may, therefore, be found. The distance  $AD$  being laid off from  $A$ , the point  $D$ , at which the perpendicular  $CD$  meets  $AB$ , becomes known. If we wish the length of the perpendicular, we use the proportion,

$$AE : EF :: AC : CD,$$

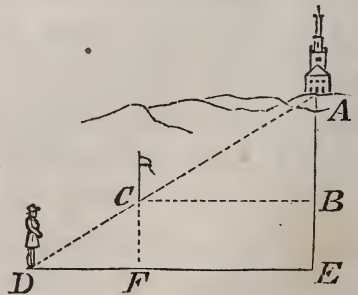
in which all the terms are known, excepting  $CD$ : therefore,  $CD$  may be determined.

III. *To determine the horizontal distance from a given point to an inaccessible object.*

#### FIRST METHOD.

34. Let  $A$  be an inaccessible object, and  $E$  the point from which the distance is to be measured.

At  $E$  lay off the right angle  $AED$ , and measure in the direction  $ED$ , any convenient distance to  $D$ , and place a staff at  $D$ . Then measure from  $E$ , directly towards the object  $A$ , a distance  $EB$  of a convenient length, and at  $B$  lay off a line  $BC$  perpendicular to  $EA$ . Measure along the line  $BC$ ,





until a person at  $D$  shall range the forward staff on the line  $DA$ . Now,  $DF$  is known, being equal to the difference between the two measured lines  $DE$  and  $CB$ . Hence, by similar triangles,

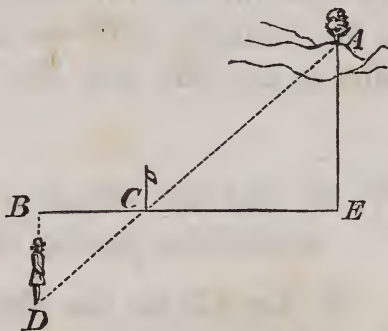
$$DF : FC :: DE : EA,$$

in which proportion all the terms are known, except the fourth, which may, therefore, be found.

#### SECOND METHOD.

35. At the point  $E$  lay off  $EB$  perpendicular to the line  $EA$ , and measure along it any convenient distance, as  $EB$ .

At  $B$  lay off the right angle  $EBD$ , and measure any distance in the direction  $BD$ . Let a person at  $D$  align a staff on  $DA$ , while a second person at  $B$  aligns it on  $BE$ : the staff will thus be fixed at  $C$ . Then measure the distance  $BC$ .



The two triangles  $BCD$  and  $CAE$  being similar, we have,

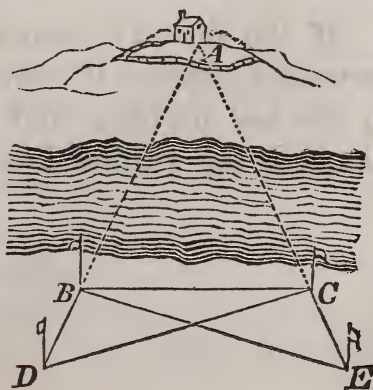
$$BC : BD :: CE : EA,$$

in which all the terms are known, except the fourth, which may, therefore, be found.

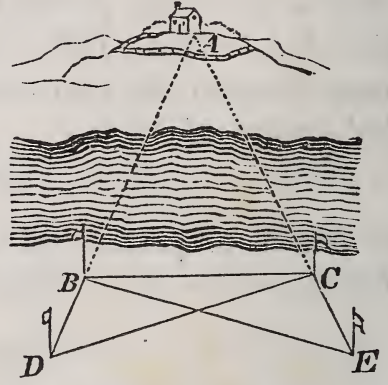
#### THIRD METHOD.

36. Let  $B$  be the given point, and  $A$  the inaccessible object; it is required to find  $BA$ .

Measure any horizontal base line, as  $BC$ . Then, having placed staves at  $B$  and  $C$ , measure any convenient distances  $BD$  and  $CE$ , such that the points  $D$ ,  $B$ , and  $A$ , shall be in the same right line, as also, the points  $E$ ,  $C$ , and  $A$ ; then measure the diagonal lines  $DC$  and  $EB$ .



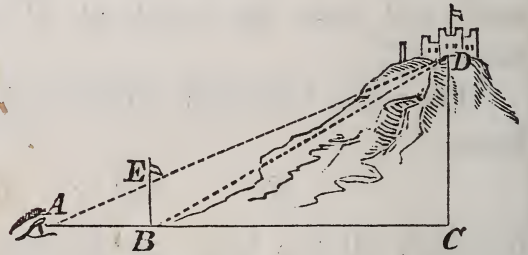
Now, in the triangle  $BEC$ , the three sides are known, therefore, the angle  $ECB$  can be found. In the triangle  $CDB$ , the three sides are also known, therefore the angle  $CBD$  can be determined. These angles being respectively subtracted from  $180^\circ$ , the two angles  $ACB$  and  $ABC$  become known; and hence, in the triangle  $ABC$ , we have two angles and the included side, to find the side  $BA$ .



IV. *To find the altitude of an object, when the distance to the vertical line passing through the top of it is known.*

37. Let  $CD$  be the altitude required, and  $AC$  the known distance.

From  $A$ , measure on the line  $AC$ , any convenient distance  $AB$ , and place a staff vertically at  $B$ . Then placing the eye at  $A$ , sight to the object  $D$ , and let the point, at which the line  $AD$  cuts the staff  $BE$ , be marked. Measure the distance  $BE$  on the staff; then,



$$AB : BE :: AC : CD,$$

whence  $CD$  becomes known.

If the line  $AC$  cannot be measured, on account of intervening objects, it may be determined by calculation, as in the last problem, and then, having found the horizontal distance, the vertical line is readily determined, as before.

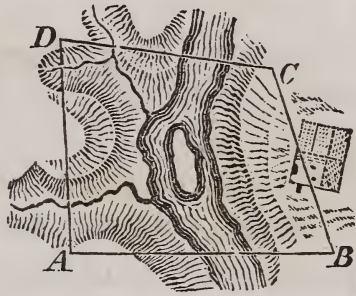
## SECTION II.

## AREA OR CONTENTS OF GROUND.—LAYING OUT LAND.

1. We come next to the determination of the area or superficial contents of ground.

The surface of the ground being, in general, broken and uneven, it is impossible, without great trouble and expense, to ascertain its exact area or contents. To avoid this inconvenience, it has been agreed to refer every surface to a horizontal plane: that is, to regard all its bounding lines as horizontal, and its area as measured by that portion of the horizontal plane which the boundary lines enclose.

For example, if  $ABCD$  were a piece of ground having an uneven surface, we should refer the whole to a horizontal plane, and take for the measure of the area that part of the plane which is included between the bounding horizontal lines  $AB$ ,  $BC$ ,  $CD$ ,  $DA$ .



In estimating land in this manner, the sum of the areas of all the parts into which a tract may be divided, is equal to the area, estimating it as an entire piece: but this would not be the case if the areas of the parts had reference to the actual surface, and the area of the whole were calculated from its bounding lines.

2. The unit of measure of a quantity is a quantity of the same kind regarded as a standard, and with which all quantities of that kind may be compared. For lines, the unit is a right line of a known length, as 1 foot, 1 link, 1 chain, or any other fixed distance.

It has been already observed (Bk. II., Sec. I., Art. 16), that Gunter's chain of four rods or 66 feet in length, and which is divided into 100 links, is the chain in general

use among surveyors. In measuring land, the length of this chain is generally taken for the unit of linear measure.

3. The unit of measure for surfaces is a square described on the unit of linear measure.

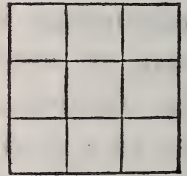
Thus, 1 square foot,

1 foot.



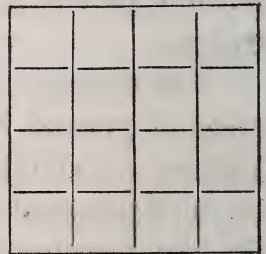
1 square yard or 9 square feet,

1 yard = 3 feet.



1 square chain, or 16 square rods.

1 chain = 4 rods.



When, therefore, the linear measures of ground are feet, yards, rods, or chains, the superficial measures are square feet, square yards, square rods, or square chains; and the numerical expression for the area is the number of times which the unit of superficial measure is contained in the land measured.

4. An *acre* is a surface equivalent in extent to 10 square chains; that is, equivalent to a rectangle of which one side is ten chains, and the other side one chain.

One quarter of an acre is called a *rood*.

Since the chain is 4 rods in length, 1 square chain contains 16 square rods; and therefore, an acre, which is 10 square chains, contains 160 square rods, and a rood contains 40 square rods. The *square rods* are called *perches*.

5. Land is generally computed in acres, roods, and perches, which are respectively designated by the letters *A. R. P.*

$$\begin{array}{r} 356 \\ 356 \\ \hline 40560 \end{array}$$
 87

When the linear dimensions of a survey are chains or links, the area will be expressed in square chains or square links, and it is necessary to form a rule for reducing this area to acres, roods, and perches. For this purpose, let us form the following

TABLE.

Miles.	Acres.	Roods.	Sq. Chains.	Perches.	Sq. Links.
1	640	2560	6400.0	102,400	64,000,000
	1	4	10.0	160	100,000
		1	2.5	40	25,000
			1.0	16	10,000
				1	625

1 square mile = 6400 square chains = 640 acres.

Now, when the linear dimensions are links, the area will be expressed in square links, and may be reduced to acres by dividing by 100000, the number of square links in an acre: that is, by pointing off five decimal places from the right hand.

If the decimal part be then multiplied by 4, and five places of decimals pointed off from the right hand, the figures to the left will express the roods.

If the decimal part of this result be now multiplied by 40, and five places for decimals pointed off, as before, the figures to the left will express the perches.

If one of the dimensions be in links, and the other in chains, the chains may be reduced to links by annexing two ciphers: or, the multiplication may be made without annexing the ciphers, and the product reduced to acres and decimals of an acre, by pointing off three decimal places from the right hand.

When both the dimensions are in chains, the product is reduced to acres by dividing by 10, or pointing off one decimal place.

From which we conclude; that,

1st. *If links be multiplied by links, the product is reduced to acres by pointing off five decimal places from the right hand.*

2d. If chains be multiplied by links, the product is reduced to acres by pointing off three decimal places from the right hand.

3d. If chains be multiplied by chains, the product is reduced to acres by pointing off one decimal place from the right hand.

6. Since there are 16.5 feet in a rod, a square rod is equal to  $16.5 \times 16.5 = 272.25$  square feet.

If the last number be multiplied by 160, we shall have,

$$272.25 \times 160 = 43560 = \text{the square feet in an acre.}$$

Since there are 9 square feet in a square yard, if the last number be divided by 9, we obtain,

$$4840 = \text{the number of square yards in an acre.}$$

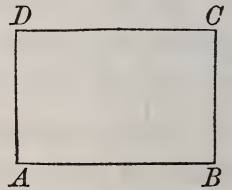
#### PROBLEM I.

7. To find the area of a piece of ground in the form of a square, rectangle, or parallelogram.

*Multiply the base by the altitude, and the product will express the area (Geom., Bk. IV., Prop. IV. and V.)*

1. To find the area of the rectangular field  $ABCD$ .

Measure the two sides  $AB, BC$ : let us suppose that we have found  $AB = 14$  chains 27 links, and  $BC = 9$  chains 75 links. Then,



$$\begin{aligned} AB &= 1427 \text{ links,} \\ BC &= 975 \text{ links,} \\ AB \times BC &= \underline{1391325} \text{ square links,} \\ &= 13.91325 \text{ acres.} \\ &\quad 4 \\ &\underline{\hspace{1.5em}} \\ &3.65300 \text{ roods,} \\ &\quad 40 \\ &\underline{\hspace{1.5em}} \\ &26.12000 \text{ perches.} \end{aligned}$$

*Ans. 13A. 3R. 26P.*

2. What is the area of a square field, of which the sides are each 33 ch. 8 l.?

*Ans. 109A. 1R. 29P.*

3. What are the contents of a rectangular field, of which the longer side is 49 ch. 27 l., and the shorter 38 ch. 7 l.?

*Ans.* 187A. 2R. 11P.

4. What are the contents of a field in the form of a parallelogram, of which the base is 35 ch. 65 l., and altitude 51 ch. 4 l.?

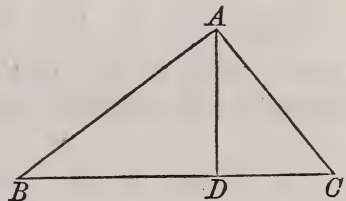
*Ans.* 181A. 3R. 33P.

#### PROBLEM II.

8. To find the contents of a piece of land in the form of a triangle.

#### FIRST METHOD.

*Measure either side of the triangle as BC, and from the opposite angle A let fall a perpendicular AD, and measure this perpendicular; then, multiply the base and perpendicular together, and divide the product by 2, the result will express the area of the triangle. Or, the area is equal to the base multiplied by half the perpendicular, or to the perpendicular multiplied by half the base (Geom., Bk. IV., Prop. VI.).*



1. What are the contents of a triangle whose base is 25 ch. 1 l., and perpendicular 18 ch. 14 l.?

*Ans.* 22A. 2R. 29P.

2. What are the contents of a triangle whose base is 15.48 chains, and altitude 9.67 chains?

*Ans.* 7A. 1R. 38P.

#### SECOND METHOD.

*Measure two sides and their included angle. Then, add together the logarithms of the two sides and the logarithmic sine of their included angle; from this sum subtract the logarithm of the radius, which is 10, and the remainder will be the logarithm of double the area of the triangle. Find, from the table,*

the number answering to this logarithm, and divide it by 2; the quotient will be the required area (Geom. Mens., Art. 6).

1. In a triangle  $ABC$ , suppose that we have found  $AB=57.65$  ch.,  $AC=125.81$  ch., and the included angle  $CAB=57^\circ 25'$ : required the area.

Let the required area be designated by  $Q$ ; then,

$$\log 2Q = \begin{cases} +\log AB \ 57.65 & . . . \ 1.760799 \\ +\log AC \ 125.81 & . . . \ 2.099715 \\ +\log \sin A \ 57^\circ 25' & . \ 9.925626 \\ -\log R & . . . . . \ 10 \end{cases}$$

$$2Q \quad = 6111.4 \quad . . . . \ \underline{3.786140}.$$

And  $Q \quad = 3055.7$  square chains.

*Ans. 305A. 2R. 11P.*

REMARK. In this example, the links are treated as decimal parts of the chain; the result, therefore, is in square chains and decimal parts of a square chain.

2. What is the area of a triangle whose sides are 30 and 40 chains, and their included angle  $28^\circ 57'$ ?

*Ans. 29A. 0R. 7P.*

THIRD METHOD.

*Measure the three sides of the triangle. Then, add them together and take half their sum. From this half sum subtract each side separately. Then, multiply the half sum and the three remainders together, and extract the square root of the product: the result will be the area (Geom. Mens., Art. 7).*

*Or, after having obtained the three remainders, add together the logarithm of the half sum and the logarithms of the respective remainders, and divide their sum by 2: the quotient will be the logarithm of the area.*

1. Find the area of a triangular piece of ground whose sides are 20, 30, and 40 chains.



BY FIRST RULE.

$$\begin{array}{r}
 20 \\
 30 \\
 \hline
 40 \\
 2)90 \\
 \hline
 45 = \text{half sum.}
 \end{array}
 \qquad
 \begin{array}{r}
 45 \\
 -20 \\
 \hline
 25 \text{ 1st rem.}
 \end{array}
 \qquad
 \begin{array}{r}
 45 \\
 -30 \\
 \hline
 15 \text{ 2d rem.}
 \end{array}
 \qquad
 \begin{array}{r}
 45 \\
 -40 \\
 \hline
 5 \text{ 3d rem.}
 \end{array}$$

$45 = \text{half sum.}$  Then,

$45 \times 25 \times 15 \times 5 = 84375$ : and  $\sqrt{84375} = 290.4737 = \text{the area.}$

*Ans. 29A. 0R. 8P.*

2. What is the area of a triangle whose sides are 2569, 4900, and 5035 links?

BY SECOND RULE.

$$\begin{array}{r}
 2569 \\
 4900 \\
 5035 \\
 \hline
 2)12504 \\
 \hline
 6252 = \text{half sum.}
 \end{array}
 \qquad
 \begin{array}{r}
 6252 \\
 -2569 \\
 \hline
 3683 \text{ 1st rem.}
 \end{array}
 \qquad
 \begin{array}{r}
 6252 \\
 -4900 \\
 \hline
 1352 \text{ 2d rem.}
 \end{array}
 \qquad
 \begin{array}{r}
 6252 \\
 -5035 \\
 \hline
 1217 \text{ 3d rem.}
 \end{array}$$

Then,

$$\left\{ \begin{array}{l}
 \log 6252 . . . . . 3.796019 \\
 \log 3683 . . . . . 3.566202 \\
 \log 1352 . . . . . 3.130977 \\
 \log 1217 . . . . . 3.085291
 \end{array} \right.$$

$$2)13.578489$$

Area in square links,  $6155225 . . . . . \underline{6.789244.}$

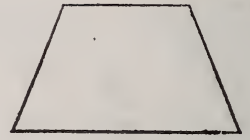
*Ans. 61A. 2R. 8P.*

PROBLEM III.

9. To find the area of a piece of land in the form of a trapezoid.

*Measure the two parallel sides, and also the perpendicular distance between them. Add the two parallel sides together, and take half the sum; then multiply the half sum by the perpendicular, and the product will be the area (Geom., Bk. IV., Prop. VII.)*

1. What is the area of a trapezoid, of which the parallel sides are 30 and 49 chains, and the perpendicular distance between them 16 ch. 60 l., or 16.60 chains?



$$\begin{array}{r}
 30 + 49 = 79; \text{ dividing by } 2, \text{ gives } \dots 39.5 \\
 \text{multiply by } \dots \dots \dots 16.60 \\
 \hline
 \text{area in square chains } \dots \dots \dots 655.700. \\
 \hline
 \end{array}$$

Ans. 65A. 2R. 11P.

2. Required the contents, when the parallel sides are 20 and 32 ch., and the perpendicular distance between them 26 ch.

Ans. 67A. 2R. 16P

PROBLEM IV.

10. To find the area of a piece of land in the form of a quadrilateral.

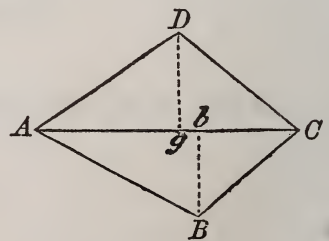
*Measure the four sides of the quadrilateral, and also one of the diagonals: the quadrilateral will thus be divided into two triangles, in both of which all the sides will be known. Then, find the areas of the triangles separately, and their sum will be the area of the quadrilateral.*

1. Suppose that we have measured the sides and diagonal AC, of the quadrilateral ABCD, and found

AB = 40.05 ch. CD = 29.87 ch.,

BC = 26.27 ch. AD = 37.07 ch.,

and AC = 55 ch.:



required the area of the quadrilateral.

Ans. 101A. 1R. 15P.

REMARK. Instead of measuring the four sides of the quadrilateral, we may let fall the perpendiculars Bb, Dg, on the diagonal AC. The area of the triangle may then be determined by measuring these perpendiculars and the diagonal AC. The perpendiculars are Dg = 18.95 ch., and Bb = 17.92 ch.

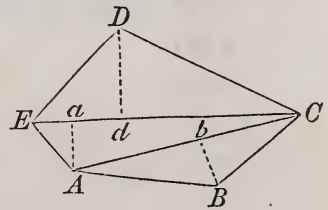
PROBLEM V.

11. To find the contents of a field having any number of sides.

Measure the sides of the field and also the diagonals: the three sides of each of the triangles into which the field will be thus divided will then be known, and the areas of the triangles may then be calculated by the preceding rules. Or, measure the diagonals, and from the angular points of the field draw perpendiculars to the diagonals and measure their lengths: the base and perpendicular of each of the triangles will then be known.

1. Let it be required to determine the contents of the field  $ABCDE$ , having five sides.

Let us suppose that we have measured the diagonals and perpendiculars, and found,



$AC = 36.21$  ch.,  $EC = 39.11$  ch.,  
 $Bb = 4.08$  ch.,  $Dd = 7.26$  ch.,  
 $Aa = 4.19$  ch.; required the area of the field.

Area of triangle $ABC =$	$73.8684$	square chains,
area of " $CDE =$	$141.9693$	" "
area of " $ACE =$	$81.7399$	" "
area of " $ABCDE =$	$297.5776$	" "

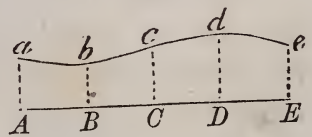
*Ans.* 29A. 3R. 1P.

PROBLEM VI.

12. To find the contents of a long and irregular figure, bounded on one side by a straight line.

Suppose the ground, of which the contents are required, to be of the form  $ABEeda$ , bounded on one side by the right line  $AE$ , and on the other by the curve  $edca$ .

At  $A$  and  $E$ , the extremities of the right line  $AE$ , erect the two perpendiculars  $Aa$ ,  $Ee$ , and on each of them measure the breadth of the land.



Then divide the base into any convenient number of equal parts, and measure the breadth of the land at each point of division.

*Add together the intermediate breadths and half the sum of the two extreme ones: then multiply this sum by one of the equal parts of the base line, and the product will be the required area very nearly (Mens. Art. 11).*

1. The breadths of an irregular figure, at five equidistant places, being 8.20 ch., 7.40 ch., 9.20 ch., 10.20 ch., and 8.60 chains, and the whole length 40 chains, required the area.

$$\begin{array}{r}
 8.20 \\
 8.60 \\
 \hline
 2 \overline{)16.80} \\
 \underline{8.40} \text{ mean of the extremes,} \\
 7.40 \\
 9.20 \\
 10.20 \\
 \hline
 35.20 \text{ sum.}
 \end{array}
 \qquad
 \begin{array}{r}
 4 \overline{)40} \\
 \underline{10} \text{ one of the equal parts.} \\
 \\
 35.20 \text{ sum,} \\
 \underline{10} \\
 \text{area } \underline{352.00} \text{ square ch.}
 \end{array}$$

*Ans. 35A. 32P.*

2. The length of an irregular piece of land being 21 ch., and the breadths, at six equidistant points, being 4.35 ch., 5.15 ch., 3.55 ch., 4.12 ch., 5.02 ch., and 6.10 chains: required the area.

*Ans. 9A. 2R. 30P.*

3. The length of an irregular piece of land is 80 ch., and the breadths at nine equidistant points are 5.75 ch., 6.12 ch., 4.80 ch., 5.09 ch., 3.87 ch., 5.17 ch., 6.00 ch., 3.94 ch., and 5.95 ch.: what is the area?

*Ans. 40A. 3R. 14P.*

4. The length of an irregular field is 39 rods, and its breadths at five equidistant places are 4.8, 5.2, 4.1, 7.3, and 7.2 rods: what is its area?

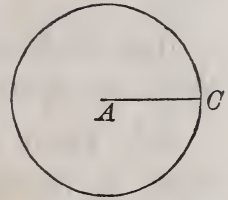
*Ans. 220.35 sq. rods.*

REMARK. If it is not convenient to erect the perpendiculars at equal distances from each other, the areas of the trapezoids, into which the whole figure is divided, must be computed separately: their sum will be the required area.

PROBLEM VII.

13. To find the area of a piece of ground in the form of a circle.

Measure the radius  $AC$ : then multiply the square of the radius by 3.1416 (Mens., Art. 15.).



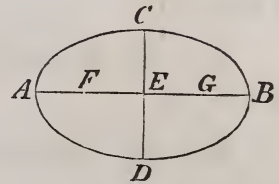
1. To find the area of a circular piece of land, of which the diameter is 25 ch.

*Ans.* 49A. 0R. 14P.

PROBLEM VIII.

14. To find the contents of a piece of ground in the form of an ellipse.

Measure the semi-axes  $AE$ ,  $CE$ . Then multiply them together, and their product by 3.1416.



1. To find the area of an elliptical piece of ground, of which the transverse axis is 16.08 ch., and the conjugate axis 9.72 ch.

*Ans.* 12A. 1R. 4P.

REMARK I. The following is the manner of tracing an ellipse on the ground, when the two axes are known.

From  $C$ , one of the extremities of the conjugate axis as a centre, and  $AE$  half the transverse axis as a radius, describe the arc of a circle cutting  $AE$  in the two points  $F$  and  $G$ : these points are called the *foci* of the ellipse.

Then, take a tape, the length of which is equal to  $AB$ , and fasten the two ends, one at the focus  $F$ , the other at the focus  $G$ . Place a pin against the tape and move it around, keeping the tape tightly stretched: the extremity of the pin will trace the curve of the ellipse.

REMARK II. In determining the contents of ground, in the examples which have been given, the linear dimensions have been taken in chains and decimals of a chain.

If the linear dimensions were taken in terms of any other unit, they may be readily reduced to chains. For, a chain is equal to 4 rods, equal to 22 yards, equal to 66 feet. Hence,

1st. *Rods may be reduced to chains and the decimal of a chain, by dividing by 4.*

2d. *Yards may be reduced to chains and the decimal of a chain, by dividing by 22.*

3d. *Feet may be reduced to chains and the decimal of a chain, by dividing by 66.*

REMARK III. If it is thought best to calculate the area, without reducing the linear dimensions to chains, the result can be reduced to acres :

1st. *By dividing it by 160 when it is in square rods (Art. 5).*

2d. *By dividing it by 4840 when it is in square yards (Art. 6).*

3d. *By dividing it by 43560 when it is in square feet (Art. 6).*

#### OF LAYING OUT LAND.

15. The surveyor is often required to lay off a given quantity of land, in such a way that its bounding lines shall form a particular figure, viz., a square, a rectangle, a triangle, &c. He is also often called upon to divide given pieces of land into parts containing given areas, or bearing certain relations to each other.

The manner of making such divisions must always depend on a judicious application of the principles of geometry to the particular case.

If, for example, it were required to lay out an acre of ground in a square form, it would first be necessary to find, by calculation, the side of such a square, and then to trace, on the ground, a figure bounded by four equal lines at right angles to each other.

## PROBLEM I.

16. To lay out a given quantity of land in a square form.

*Reduce the given area to square chains, or square rods: then extract the square root, and the result will be the side of the required square. This square being described on the ground, will be the figure required.*

1. To trace a square which shall contain 15A. 0R. 12P.

First,  $15A = 60R = 2400P$

Add,  $12P$ ; hence,

$15A\ 0R\ 12P = \overline{2412P}$ ; the square root

of which is 49.11.

Therefore, if a square be traced on the ground, of which the side is 49.11 rods, it will be the required figure.

2. To trace a square which shall contain 176A. 1R. 24P.

First,  $176A = 1760$  square chains,

$1R = 2.5$  " "

hence,  $24P = 1.5$  " "

$176A\ 1R\ 24P = 1764$  square chains: the square root of which is 42. Hence, if a square be traced on the ground, of which the side is 42 ch., it will be the required figure.

## PROBLEM II.

17. To lay out a given quantity of land in a rectangular form, having one of the sides of the rectangle given.

*Divide the given area, reduced to square chains or square rods, by the given side of the required rectangle, and the quotient will be the other side. Then, trace the rectangle on the ground.*

1. To lay off 240 acres in a rectangular form, one of the sides being given, and equal to 80 rods.

First,  $240A = 2400$  square chains = 38400 square rods.

Then,  $80)38400(480$  rods; which is the required side of the rectangle.

18. A great number of similar problems might be proposed. The solution of them does not, however, properly belong to surveying. The laying out of the ground, and

the tracing of lines, after the figure and area have been determined, are the only parts which appertain to a practical treatise. The manner of tracing lines having been already explained, it seems unnecessary to add the numerous examples often given under this head of the subject.

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### SECTION III.

#### SURVEYING WITH THE COMPASS.—DIVIDING LAND.

1. Before considering the principles involved in the method of surveying now to be explained, it will be necessary to describe the instrument principally used in the field, and which is called

#### THE CIRCUMFERENTER, OR SURVEYOR'S COMPASS.

Pl. 2, Fig. 2. This instrument consists of a compass-box  $DCE$ , a magnetic needle, a brass plate  $AB$ , from twelve to fourteen inches long, two plain sights,  $AF$  and  $BG$ , one of which is more fully shown in Fig. 3; and a stand, which is sometimes a tripod, and sometimes a single staff pointed with iron at the lower end, so that it may be placed firmly in the ground.

The open sights,  $AF$  and  $BG$ , are placed at right angles to the plate  $AB$ , and fastened to it firmly by the screws  $a$  and  $b$ . In each sight there is a large and small aperture or slit; the larger aperture being above the smaller in one of the sights, and below it in the other. A hair or thread of silk is drawn vertically through the middle of the large aperture, as shown in Fig. 3.

The compass-box  $DCE$  is circular, and generally about six inches in diameter. At the centre is a small pin, on which the magnetic needle is poised. This needle, if allowed to turn freely around the point of support, will settle to a state of rest: the direction which it then indicates, is that of the *magnetic meridian*.



In the interior of the compass-box, there is a graduated circle divided to degrees, and sometimes to half degrees: the degrees are numbered from the extremities of the diameter  $NS$ , both ways to  $90^\circ$ .

The length of the magnetic needle is a little less than the diameter of the graduated circle, so that the needle can move freely around its centre, within the circle, and its positions be noted on the graduated arc.

The compass-box is turned about its centre, without moving the plate  $AB$ , by means of the milled screw  $L$ : it is fastened to the plate  $AB$ , by the screw  $P$ .

In using the compass, it is important to ascertain the exact angle which may be included between the magnetic meridian and the direction that may be given to the line drawn through the eye and the sights  $AF$  and  $BG$ .

To effect this, a small arc  $HI$  is described on the bar  $AB$ , having its centre at the centre of the compass-box. This arc is divided to degrees, and sometimes to the parts of a degree. A vernier is also used, which is permanently attached to the compass-box.

When the 0 point of this vernier coincides with the 0 point of the graduated arc  $HI$ , the line of the compass-box marked  $NS$ , lies in the plane of the sights.

Now, supposing the 0 of the vernier to coincide with the 0 of the arc  $HI$ , if the end of the needle does not stand at one of the lines of division of the graduated circle, let the whole degrees be read. Then, turn the compass-box by means of the screw  $L$ , until the needle points exactly to the line which marked the whole degrees: the space passed over by the 0 of the vernier, shows the parts of a degree that are to be added to give the true reading.

#### SURVEYING WITH THE COMPASS.

2. The line about which the earth revolves is called its *axis*; and the two points in which the axis meets the surface of the earth, are called the *poles*.

3. A plane passed through the axis is called a *meridian*.

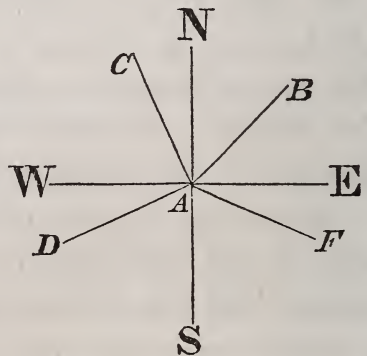
*plane*, and its intersection with the surface is called a *meridian line* or a *meridian*.

4. All the meridians converge towards the poles, but they vary so little from parallelism within the narrow limits of surveys made with the compass, that they may, without error, be regarded as parallel straight lines.

5. If a magnetic needle be suspended freely and allowed to settle to a state of rest, a vertical plane passed through its axis is called the *plane of the magnetic meridian*; and its intersection with the surface of the earth is called the magnetic meridian, or sometimes a North and South line. A line perpendicular to a North and South line is called an East and West line.

6. A line traced or measured on the ground, is called a *course*; and the angle which this line makes with the meridian passing through the point of beginning, is called the *bearing*.

Thus, if we start from the point *A*, and measure in the direction *AB*, the line *AB* is the course, and the angle *NAB* is the bearing.



When the course, like *AB*, falls between the north and east points, the bearing is read, north  $46^\circ$  east, and is written N.  $46^\circ$  E.

When the course, like *AC*, falls between the north and west points, the bearing is read, north  $30^\circ$  west, and is written N.  $30^\circ$  W.

When the course, like *AF*, falls between the south and east points, the bearing is read, south  $70^\circ$  east, and is written S.  $70^\circ$  E.

When the course, like *AD*, falls between the south and west points, the bearing is read, south  $70^\circ$  west, and is written S.  $70^\circ$  W.

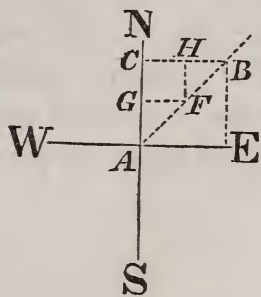
A course which runs due north, or due south, is designated by the letter N or S; and one which runs due east, or due west, by the letter E or W.

7. If, after having passed over a course, the bearing is taken to the back station, this bearing is called the *back sight*, or *reverse bearing*.

8. The perpendicular distance between the east and west lines drawn through the extremities of a course, is called the *northing* or *southing*, according as the course is run towards the north or south. This distance is also called the *difference of latitude*, or simply the latitude, because it shows the distance which one of the points is north or south of the other.

Thus, in running the course from  $A$  to  $B$ ,  $AC$  is the difference of latitude, north.

9. The perpendicular distance between the meridians passing through the extremities of a course, is called the *departure* of that course, and is east or west, according as the course lies on the east or west side of the meridian passing through the point of beginning.



Thus, in running the course  $AB$ ,  $CB$  is the departure, east.

10. It will be found convenient, in explaining the rules for surveying with the compass, to attribute to the latitudes and departures the algebraic signs,  $+$  and  $-$ .

We shall, therefore, consider every northing as affected with the sign  $+$ , and every southing as affected with the sign  $-$ . We shall also consider every easting as affected with the sign  $+$ , and every westing as affected with the sign  $-$ .

11. The *meridian distance* of a point is its perpendicular distance from an assumed meridian. Thus, if the distance be estimated from the meridian  $NS$ ,  $BC$  will be the meridian distance of the point  $B$ .

12. The meridian distance of a line is the meridian distance of its middle point, and is east or west, according as this point lies on the east or west side of the assumed me-

ridian. Thus,  $FG$  drawn through the middle point of  $AB$ , is the meridian distance of the line  $AB$ .

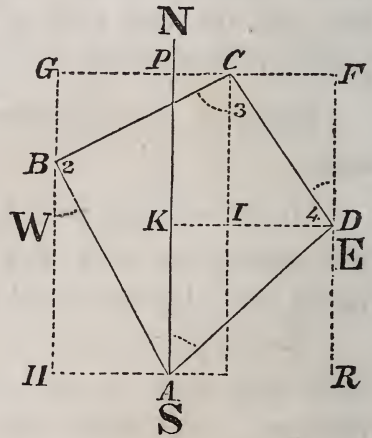
The sign  $+$  will always be given to the meridian distance of a point or line, when it lies on the east of the assumed meridian, and the sign  $-$ , when it lies on the west.

13. When a piece of ground is to be surveyed, we begin at some prominent corner of the field, and go entirely around the land, measuring the lengths of the bounding lines with the chain, and taking their bearings with the compass. It is not material whether the ground be kept on the right hand or on the left, and all the rules deduced for one of the cases, are equally applicable to the other. To preserve uniformity, however, in the language of the rules, we shall suppose the land to be always kept on the right hand of the surveyor.

FIELD OPERATIONS.

14. Let  $ABCD$  be a piece of ground to be surveyed,  $A$  the point where the work is to be begun, and  $NS$  a meridian.

On a sheet of paper, rule three columns, as follows, and head them stations, bearings, distances.



Stations.	Bearings.	Distances.
1	N $31\frac{1}{2}^\circ$ W	10.
2	N $62\frac{3}{4}^\circ$ E	9.25
3	S $36^\circ$ E	7.60
4	S $45\frac{1}{2}^\circ$ W	10.40

Place the compass at  $A$ , and take the bearing to  $B$ , which is  $PAB$ : suppose this angle has been found to be  $31\frac{1}{2}^\circ$ . The bearing from  $A$  to  $B$  is then N.  $31\frac{1}{2}^\circ$  W. En-

ter this bearing in the field notes opposite station 1. Then measure the distance from  $A$  to  $B$ , which we will suppose to be 10 ch., and insert that distance opposite station 1, in the column of distances.

We next take the bearing from  $B$  to  $C$ , N.  $62\frac{3}{4}$  E., and then measure the distance  $BC=9$  ch. 25 l., both of which we insert in the notes opposite station 2.

At station  $C$  we take the bearing to  $D$ , S.  $36^\circ$  E., and then measure the distance  $CD=7$  ch. 60 l., and place them in the notes opposite station 3.

At  $D$  we take the bearing to  $A$ , S.  $45\frac{1}{2}^\circ$  W., and measure the distance  $DA=10$  ch. 40 l. We shall then have made all the measurements on the field which are necessary to determine the contents of the ground.

15. REMARK I. The reverse bearing or back sight, from  $B$  to  $A$ , is the angle  $ABH$ ; and since the meridians  $NS$  and  $HG$  are parallel, this angle is equal to the bearing  $NAB$ . The reverse bearing is, therefore, S.  $31\frac{1}{2}^\circ$  E.

The reverse bearing from  $C$ , is S.  $62\frac{3}{4}^\circ$  W.; that is, it is the angle  $ICB=GBC$ .

And generally, *a reverse bearing, or back sight, is always equal to the forward bearing, and differs from it in both of the letters by which it is designated.*

16. REMARK II. In taking the bearings with the compass, there are two sources of error. 1st. The inaccuracy of the observations: 2d. Local attractions, or the derangement which the needle experiences when brought into the vicinity of iron-ore beds, or any ferruginous substances.

To guard against these sources of error, the reverse bearing should be taken at every station: if this and the forward bearing are of the same value, the work is probably right; but if they differ considerably, they should both be taken again.

17. REMARK III. If the forward and back sights at the end of any course of the survey agree, it may be safely assumed, that no local attraction disturbs the needle at these points; and hence, that the *next foresight* is also free from such disturbing causes. The error, therefore, from

local attraction, when it arises, will first show itself in the difference between a true foresight and an erroneous back sight.

When this difference appears, subtract the back sight from the foresight, and call the difference the *correction* for the next foresight. The correction will be positive when the foresight is the larger, and negative when it is less.

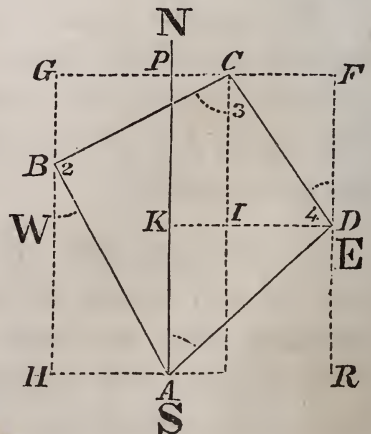
Add this correction, with its proper sign, to the foresight of the next course, when the meridional and longitudinal letters of that course are both the same, or both different from the foresight of the previous course, and subtract it when one of the letters is the same and the other different: the result will be the true bearing. The true bearing of any other course may be found by the same process.

## EXAMPLE.

True Foresights.	Back Sights.	Foresights of next Course.	Foresights Corrected.
1. S 85° 10' W	N 85° 05' E	S 16° 15' W	S 16° 20' W
2. N 16° 20' E	S 18° 20' W	N 15° 25' W	N 17° 25' W
3. N 17° 25' W	S 16° 10' E	N 28° 16' E	N 27° 01' E
4. S. 47° 18' E	N 48° 10' W	S 49° 15' W	N 50° 07' W

NOTE.—If there be no course in the survey in which the forward and back sights agree, take the one in which they agree the nearest, and add half the difference of the bearings to the least, and treat the result as the true bearing.

18. REMARK IV. In passing over the course  $AB$ , the northing is found to be  $HB$ , and the departure, which is west, is represented by  $AH$ . Of the course  $BC$ , the northing is expressed by  $BG$ , and the departure, which is east, by  $GC$ . Of the course  $CD$ , the southing is expressed by  $CI$ , and the departure, which is east, by  $CF$ . Of the course  $DA$ , the south-



ing is expressed by  $KA$ , and the departure, which is west, by  $DK$ . It is seen from the figure, that the sum of the northings is equal to  $HB + BG = HG$ ; and that the sum of the southings is equal to  $CI + KA = PA = HG$ : hence, *the sum of the northings is equal to the sum of the southings.*

If we consider the departures, it is apparent that the sum of the eastings is equal to  $GC + CF = GF$ ; and that the sum of the westings is equal to  $AH + DK = GF$ ; hence also, *the sum of the eastings is equal to the sum of the westings.* We therefore conclude, that when any survey is correctly made, *the sum of the northings will be equal to the sum of the southings, and the sum of the eastings to the sum of the westings.*

It would indeed appear plain, even without a rigorous demonstration, that after having gone entirely round a piece of land, the distance passed over in the direction due north, must be equal to that passed over in the direction due south; and the distance passed over in the direction due east, equal to that passed over in the direction due west.

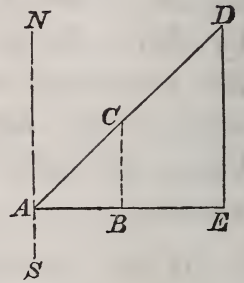
Having now explained the necessary operations on the field, we shall proceed to show the manner of computing the contents of the ground. We shall first explain,

#### THE TRAVERSE TABLE AND ITS USES.

19. This table shows the latitude and departure corresponding to bearings that are expressed in degrees and quarters of a degree from 0 to 90°, and for every course from 1 to 100, computed to two places of decimals.

The following is the method of deducing the formulas for computing a traverse table; by means of these formulas and a table of natural sines, the latitude and departure of a course may be computed to any desirable degree of accuracy.

Let  $AD$  represent any course, and  $NAD = ACB$ , expressed in degrees and minutes, be its bearing. Let  $AC$  be the unit of measure of the course, and also the radius of the table of natural sines (Bk. I., Sec. III., Art. 14). Draw  $DE$  and  $CB$  parallel to  $NS$ , and  $AE$  perpendicular to  $AS$ . Then will  $DE$  be the *latitude*, and  $AE$  the *departure of the course*, and  $CB$  the *co-sine*, and  $AB$  the *sine of the bearing*.



From similar triangles we have these proportions,

$$AC : CB :: AD : DE, \text{ or}$$

$$1 : \cos \text{ of the bearing} :: \text{course} : \text{latitude},$$

$$AC : AB :: AD : AE, \text{ or}$$

$$1 : \sin \text{ of the bearing} :: \text{course} : \text{departure}.$$

Whence,  $\text{lat.} = \text{course} \times \cos \text{ of the bearing},$   
 $\text{dep.} = \text{course} \times \sin \text{ of the bearing}.$

We have then the following practical rule for computing the latitude and departure of any course.

*Look in a table of natural sines for the cosine and sine of the bearing. Multiply each by the length of the course, and the first product will be the latitude, and the second will be the departure of the given course.*

EXAMPLES.

1. The bearing is  $65^\circ 39'$ , the course 69.41 chains: what is the latitude, and what the departure?

Natural cosine of $65^\circ 39'$ . . . . .	.41231
Length of the course . . . . .	69.41
Product, which is the Dif. of Latitude,	<u>28.6184371.</u>

Natural sine of $65^\circ 39'$ . . . . .	.91104
Length of the course . . . . .	69.41
Product, which is the Departure . .	<u>63.2352864.</u>



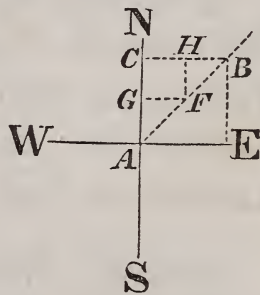
2. The bearing is  $75^\circ 47'$ , the course 89.75 chains: what is the latitude, and what the departure?

Natural cosine of $75^\circ 47'$ . . . . .	.24559
Length of course . . . . .	89.75
Product, which is the Dif. of Latitude,	22.0417025.
Natural sine of $75^\circ 47'$ . . . . .	.96937
Length of course . . . . .	89.75
Product, which is the Departure . . .	87.0009575.

20. In this manner the traverse table given at the end of the book has been computed. When the bearing is given in degrees and quarters of a degree, and the difference of latitude and departure are required to only two places of decimals, they may be taken directly from the traverse table.

If the bearing is less than  $45^\circ$ , the angle will be found at the top of the page; if greater, at the bottom. Then, if the distance is less than 50, it will be found in the column "distance," on the left hand page; if greater than 50, in the corresponding column of the right hand page.

The latitudes or departures of courses of different lengths, but which have the same bearing, are proportional to the lengths of the courses. Thus, in the figure, the latitudes  $AG$ ,  $AC$ , or the departures  $GF$ ,  $CB$ , are to each other as the courses  $AF$ ,  $AB$ .



Therefore, when the distance is greater than 100, it may be divided by any number which will give an exact quotient, less than 100: then the latitude and departure of the quotient being found and multiplied by the divisor, the products will be the latitude and departure of the whole course. It is also plain, that the latitude or departure of two or more courses, having the same bearing, is equal to the sum of the latitudes or departures of the courses taken separately.

Hence, if we have any number greater than 100, as 614, we have only to recollect that,  $610 + 4 = 614$ ; and also, that the latitude and departure of 610, are ten times

as great, respectively, as the latitude and departure of 61: that is, equal to the latitude and departure of 61 multiplied by 10, or with the decimal point removed one place to the right.

## EXAMPLES.

1. To find the latitude and departure for the bearing  $29\frac{1}{2}^\circ$ , and the course 614.

Latitude for 610 . .	530.90	Departure for 610 . .	300.40
Latitude for 4 . .	3.48	Departure for 4 . .	1.97
Latitude for <u>614</u> . .	<u>534.38</u>	Departure for <u>614</u> . .	<u>302.37</u>

In this example, the latitude and departure answering to the bearing  $29\frac{1}{2}^\circ$ , and to the distance 61, are first taken from the table, and the decimal point removed one place to the right: this gives the latitude and departure for the distance 610; the latitude and departure answering to the same bearing and the distance 4, are then taken from the table and added.

2. To find the latitude and departure for the bearing  $62\frac{1}{2}^\circ$ , and the course 7855 chains.

Latitude for 7800 . .	3602.00	Departure for 7800 . .	6919.00
Latitude for 55 . .	25.40	Departure for 55 . .	48.79
Latitude for <u>7855</u> . .	<u>3627.40</u>	Departure for <u>7855</u> . .	<u>6967.79</u>

REMARK. When the distances are expressed in whole numbers and decimals, the manner of finding the latitudes and departures is still the same, except in pointing off the places for decimals: but this is not difficult, when it is remembered that the column of distances in the table, may be regarded as decimals, by removing the decimal point to the left in the other columns.

3. To find the latitude and departure for the bearing  $47\frac{3}{4}^\circ$ , and the course 37.57.

Latitude for 37.00 . .	24.88	Departure for 37.00 . .	27.39
Latitude for .57 . .	.38	Departure for .57 . .	.42
Latitude for <u>37.57</u> . .	<u>25.26</u>	Departure for <u>37.57</u> . .	<u>27.81</u>

## OF BALANCING THE WORK.

21. The use of the traverse table being explained, we can proceed to compute the area of the ground.

The field notes having been completed, rule a new table, as below, with four additional columns, two for latitude, and two for departure.

Then find, from the traverse table, the latitude and departure of each course, and enter them in the proper columns opposite the station.

Then add up the column of northings, and also the column of southings: the two sums should be equal to each other. If they are not, subtract the less from the greater; the remainder is called the *error in latitude*. This error takes the name of that column which is the less. For example, if the sum of the northings is less than the sum of the southings, the error is called, *error in northing*: but if the sum of the southings is less than the sum of the northings, the error is called, *error in southing*. We find the error for each particular course by the following proportion.

As the sum of the courses  
Is to the error of latitude,  
So is each particular course  
To its correction.

The error thus found may be entered in a separate column; after which add it to the latitude of the course when the error and latitude are of the *same name*, but subtract it when they are of *different names*. This will make the sum of the northings equal to the sum of the southings, and is called *balancing* the work. The northings and southings thus corrected are entered in columns on the right, under the head *balanced*.

The eastings and westings are balanced in the same manner; the difference between their sums being called *error in departure*.

For an example, we will resume the one already considered.

Sta.	Bearings.	Distan-ces.	LATITUDE.		DEPARTURE.		Cor. Lat.	Cor. Dep.	BALANCED.				
			N. +	S. -	E. +	W. -			N. +	S. -	E. +	W. -	
1	N 31½° W	10.	8.53			5.22	+0.18	+0.02	8.71				5.24
2	N 62¾° E	9.25	4.23		8.22		+0.17	-0.01	4.40		8.21		
3	S 36° E	7.60		6.15	4.47		-0.14	-0.01		6.01	4.46		
4	S 45½° W	10.40		7.29		7.41	-0.19	+0.02		7.10		7.43	
Sum of courses, 37.25			12.76	13.44 12.76	12.69 12.63	12.63			13.11	13.11	12.67	12.67	

Error in Northing . . . 0.68      0.06 Error in Westing.

As 37.25 : 0.68 :: 10 : 0.18 error in lat. of 1st course  
 As 37.25 : 0.68 :: 9.25 : 0.17 error in lat. of 2d course.  
 As 37.25 : 0.68 :: 7.60 : 0.14\* error in lat. of 3d course.  
 As 37.25 : 0.68 :: 10.40 : 0.19 error in lat. of 4th course.

As 37.25 : 0.06 :: 10 : 0.02\* error in dep. of 1st course.  
 As 37.25 : 0.06 :: 9.25 : 0.01 error in dep. of 2d course.  
 As 37.25 : 0.06 :: 7.60 : 0.01 error in dep. of 3d course.  
 As 37.25 : 0.06 :: 10.40 : 0.02 error in dep. of 4th course.

22. REMARK I. In finding the error in latitude or departure, for a particular course, the last figure is sometimes doubtful: in which case it is best to mark it, as in the third proportion for error in latitude, and the first for error in departure; and then, if the figures taken do not balance the work, let each be increased or diminished by 1.

23. REMARK II. It has already been observed (Art. 18), that if the measurements on the field be correctly made, the sums of the northings and southings will be equal to each other, as also those of the eastings and westings. It is the opinion of some surveyors, that when the error in latitude or departure exceeds one link for every five chains of the courses, the field notes ought not to be relied on. This, perhaps, is a higher degree of accuracy than can be attained. The error, however, should always be made considerably less than one link to a chain.

24. The following is an example in which the latitude and departure of each course have been computed from the table of natural sines.

Sta.	Bearings.	Dist.	Dif. of Latitude.		Departure.		Balanced.			
			N.	S.	E.	W.	N.	S.	E.	W.
1	N 45 55 W	53 ch.	36.87210			38.07149	36.65908			38.07149
2	N 4 50 E	74.40	74.13513		6.26894		73.72813		6.26894	
3	N 89 05 E	125.50	2.00800		125.48368		1.96126		125.49228	
4	S 1 50 W	71.80		71.76338		2.29688		72.17110		2.29688
5	S 7 40 E	31.20		30.92107	4.16239			31.12138	4.16239	
6	N 89 25 W	35.50	0.36139			35.49822	0.36139			35.49822
7	S 84 35 W	40.		3.77600		39.82120		3.80352		39.81260
8	S 74 35 W	21.		5.58264		20.24442		5.61385		20.24442
			113.37662	112.04309	135.91501	135.93221	112.70986	112.70985	135.92361	135.92361
			112.04309			135.91501				
Error in Southing			1.33353			0.01720	Error in Easting.			
Half Error			0.66676			0.00860	Half Error.			

Instead of balancing by the method just explained, we divide each error by two. Now if we subtract half the error in southing from the column of northings, and at the same time add it to the column of southings, these two columns will exactly balance. In like manner, if we subtract half the error in easting from the column of westings, and at the same time add it to the column of eastings, these columns will also balance.

The errors should be distributed in proportion to the lengths of the courses, but this may be done with sufficient accuracy without making the proportions. If any of the courses have been run over rough ground, the probability is that the errors belong to these courses, and they should be distributed among them.

In this example we separate the half error in southing into the three parts .40700, .21302, and .04674, and subtract them respectively from the northings of courses 2, 1, and 3, and then place the northings in the balanced columns. For the southings we separate the half error into the four parts .40772, .20031, .03121, and .02752, and add them respectively to the southings of the courses 4, 5, 8, and 7. We then enter the southings in the balanced columns. As the error in easting is so small, we add half of it to the easting of course 3, and subtract half from the westing of course 7.

## OF THE DOUBLE MERIDIAN DISTANCES OF THE COURSES.

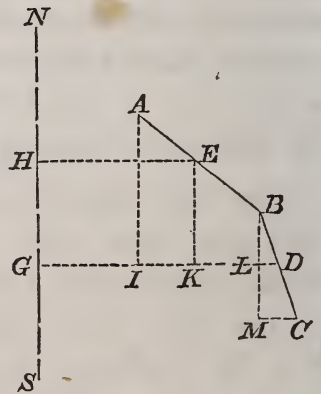
25. After the work has been balanced, the next thing to be done is to calculate the double meridian distance of each course.

For this purpose, a meridian line is assumed, lying either wholly without the land, or passing through any point within it. It is, however, most convenient to take that meridian which passes through the most easterly or westerly station of the survey; and these two stations are readily determined by inspecting the field notes.

Having chosen the meridian, let the station through which it passes, be called the *principal station*, and the course which begins at this point, *the first course*. Care, however, must be taken, not to confound this with the course which begins at station 1, and which is the first course that is entered in the field notes.

It has already been remarked (Art. 10), that all departures in the direction east, are considered as *plus*, and all departures in the direction west as *minus*.

26. To deduce a rule for finding the double meridian distances of the courses. Let  $BC$  represent any course, and  $AB$  the preceding course; also, let  $D$  and  $E$  be their middle points. Draw  $EH$ ,  $CM$ , and  $DG$ , perpendicular to the assumed meridian  $NS$ . Draw also  $AI$ ,  $EK$ , and  $BL$ , parallel to  $NS$ . Then  $2DG$  is the double meridian distance of the course  $BC$ , and  $2EH = 2KG$ , is the double meridian distance of the course  $AB$ .



Now,  $2DG = 2GK + 2KL + 2LD$ ; but  $2KL = IL$  is the departure of the course  $AB$ , and  $2LD = MC$  is the departure of the course  $BC$ ;

consequently,  $2GD = 2GK + IL + MC$ ;

hence, the double meridian distance of a course, is equal to the double meridian distance of the preceding course

plus the departure of that course plus the departure of the course itself; if there is no preceding course, the first two terms become zero. We therefore have the following

RULE.

I. *The double meridian distance of the first course is equal to its departure.*

II. *The double meridian distance of the second course is equal to the double meridian distance of the first course, plus its departure, plus the departure of the second course.*

III. *The double meridian distance of any course is equal to the double meridian distance of the preceding course, plus its departure, plus the departure of the course itself.*

27. REMARK. It should be recollected that *plus* is here used in its algebraic sense, and that when the double meridian distance of a course and the departure which is to be added to it, are of different names, that is, one east and the other west, they will have contrary algebraic signs; hence, their algebraic sum will be expressed by their difference, with the sign of the greater prefixed to it.

If the assumed meridian cuts the enclosure, the double meridian distances, estimated to the left, must be taken with the *minus* sign.

The double meridian distance of the last course should be equal to the departure of that course. A verification of the work is, therefore, obtained by comparing this double meridian distance with the departure of the course.

28. To apply the above rule to the particular example already considered (Art. 21), rule a new table as below, in which are entered the *balanced* northings and southings, and the balanced eastings and westings.

In this table there is but a single column for the differences of latitude, and a single column for the departures. The + sign shows when the difference of latitude is north, and the - sign when it is south. The + sign also shows when the departure is east, and the - sign when it is west.

Sta.	Bearings.	Distances.	Dif. Lat.	Dep.	D. M. D.
1	N 31½° W	10.	+ 8.71	- 5.24	+ 17.91
					- 7.43
					+ 5.24
2*	N 62¾° E	9.25	+ 4.40	+ 8.21	8.21
3	S 36° E	7.60	- 6.01	+ 4.46	+ 8.21
					+ 8.21
					+ 4.46
					+ 20.88
4	S 45½° W	10.40	- 7.10	- 7.43	+ 20.88
					+ 4.46
					- 7.43
					+ 17.91

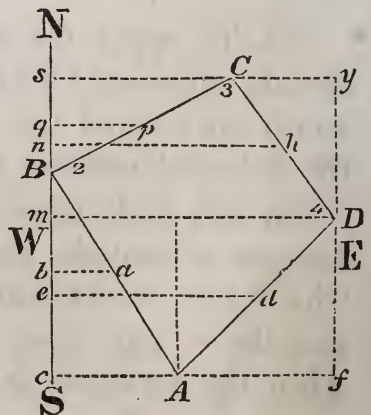
We see, from inspecting the notes, that 2 is the most westerly, and 4 the most easterly station. Either of them may, therefore, be taken for the principal station. Let us assume 2 for the principal station, and distinguish it by a star, thus \*.

Having done so, we enter the departure 8.21 in the column of double meridian distances, which gives the double meridian distance of the first course. The double meridian distances of the other courses are calculated according to the rule; and as the last, opposite to station 1, is equal to the departure of the course, the work is known to be right.

29. Having shown the manner of computing the double meridian distance of each course, we shall now deduce a rule for finding the

AREA.

Let us still consider the same example. We will first write the differences of latitude and the double meridian distances of the courses, in the following table.





Stations.	Dif. of Latitude.	D. M. D.	Area. +	Area. -
1	+ $cB$	+ $2ba$	$2cAB$	
2*	+ $Bs$	+ $2qp$	$2BsC$	
3	- $yD$	+ $2nh$		$2msCD$
4	- $Df$	+ $2ed$		$2cmDA$

It is evident, that  $cB$  multiplied by  $2ba = cA$ , will give double the area of the triangle  $cAB$ . But  $cB$  and  $ba$  are both plus; hence, the product will be plus, and must be put in the column of plus areas. Double the area of the triangle  $BsC$ , is equal to  $Bs$  multiplied by  $2qp$ , which product is also plus.

The area of the trapezoid  $msCD$  is equal to  $yD = ms$  multiplied by  $nh$  (Geom., Bk. IV., Prop. VII., S.); hence, double the area is equal to  $yD$  into  $2nh$ . But since  $yD$  is minus, and  $2nh$  plus, it follows that the product will be negative; hence, it must be placed in the column of negative areas.

Double the area of the trapezoid  $cADm$ , is equal to  $Df = mc$  multiplied by  $2de$ : but, since  $Df$  is negative and  $2de$  positive, the product will be negative.

It is now evident that the difference between the two columns is equal to twice the contents of the figure  $ABCD$ : and since the same may be shown for any other figure, we may write, for finding the areas, the following general

#### RULE.

I. Multiply the double meridian distance of each course by its northing or southing, observing that like signs in the multiplicand and multiplier give plus in the product, and that unlike signs give minus in the product.

II. Place all the products which have a plus sign, in one column, and all the products which have a minus sign, in another.

III. Add up the columns separately and take the difference of their sums: this difference will be double the area of the land.

30. We will now make the calculations in numbers. Having balanced the work, we can place it in the following table.

Sta.	Bearings.	Dist.	Dif. Lat.	Dep.	D. M. D.	Area. +	Area. -
1	N 31½° W	10.	+ 8.71	- 5.24	+ 5.24	45.6404	
2*	N 62¾° E	9.25	+ 4.40	+ 8.21	+ 8.21	36.1240	
3	S 36° E	7.60	- 6.01	+ 4.46	+ 20.88		125.4888
4	S 45½° W	10.40	- 7.10	- 7.43	+ 17.91		127.1610
						81.7644	252.6498
							81.7644
							2)170.8854
							85.4427
							8.54427
							4
							2.17708
							40
							<u>7.08320</u>

Area in square chains . . . . . 85.4427  
 Dividing by 10 . . . . . 8.54427  
 4  
 2.17708  
 40  
*Ans. 8A. 2R. 7P.* . . . . . 7.08320

Observing in the field notes that station 2 is the most westerly point of the land, we assume the meridian which passes through this point, as the one from which the meridian distances are to be calculated. We mark the principal station with a star.

Opposite station 2, we enter, in the column of double meridian distances, headed D. M. D., the departure of the course from 2 to 3, which is the double meridian distance of that course, and plus. To this we add the departure of the course, and also the departure of the next course: their sum is the double meridian distance of the course from 3 to 4.

To the last sum add the departure opposite station 3, and the minus departure opposite station 4: their algebraic sum is the double meridian distance from 4 to 1.

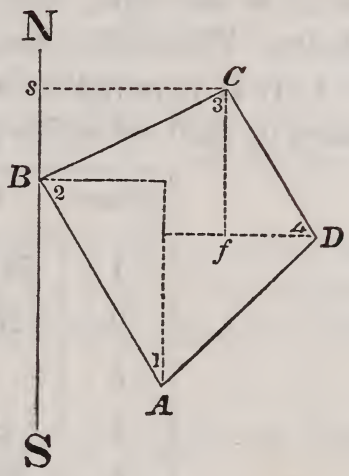
To the last sum add the last departure, which is minus, also the next departure which is likewise minus: this will give the double meridian distance of the course from 1 to 2, which is equal to its departure.

Then forming the products, adding them together, taking their difference, and dividing it by 2, according to the rule, we obtain the contents of the ground.

OF PLOTTING.

31. It only remains to make a plot of the ground.

For this purpose, draw any line, as NS, to represent the meridian passing through the principal station; and on this line take any point, as B, to represent that station.



FIRST METHOD.

Having fixed upon the scale on which the plot is to be made, lay off from B on the meridian, a distance Bs equal to the difference of latitude of the first course, and at s erect a perpendicular to the meridian, and make it equal to the departure of the first course: then draw BC, which will be the first course.

Through C draw a meridian, and make Cf equal to the difference of latitude of the second course, and through f draw a perpendicular fD, and make it equal to the departure of the second course: draw CD, and it will be the second course.

Lay down, in the same manner, the courses DA and AB, and the entire plot will be completed.

SECOND METHOD.

The work may be plotted in another manner, thus. At the principal station B, lay off an angle equal to the bearing from B to C, which will give the direction of BC. Then, from the scale of equal parts, make BC equal to the first course, this will give the station C.

Through C draw a meridian, and lay off an angle equal to the bearing from C to D, and then lay off the course CD. Do the same for the bearing at D and the course DA; also, for the bearing at A and the course AB, and a

complete plot of the ground will thus be obtained. If the work is all right, the last line *AB* will exactly close the figure. This plot is made on a scale of 10 chains to an inch.

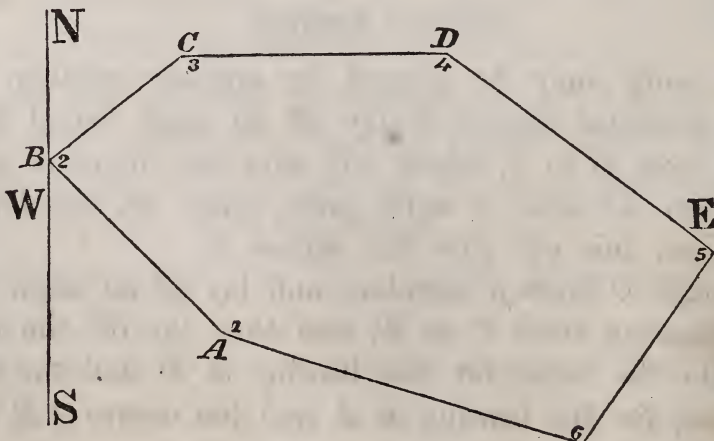
1. It is required to determine the contents and plot of a piece of land, of which the following are the field notes, viz.

Stations.	Bearings.	Distances.
1	N $46\frac{1}{2}^\circ$ W	20 ch.
2*	N $51\frac{3}{4}^\circ$ E	13.80
3	E	21.25
4	S $56^\circ$ E	27.60
5	S $33\frac{1}{4}^\circ$ W	18.80
6	N $74\frac{1}{2}^\circ$ W	30.95

CALCULATION.

Sta- tions.	Bearings.	Dis.	Dif.		Lat.		Dep.		BALANCED.		D.M.D. +	AREA. +	AREA. -
			N +	S -	E +	W -	Lat.	Dep.					
1	N $46\frac{1}{2}^\circ$ W	20 ch	13.77				14.51	+13.88	-14.56	14.56	202.0928		
2*	N $51\frac{3}{4}^\circ$ E	13.80	8.54			10.84		+8.61	+10.81	10.81	93.0741		
3	E	21.25				21.25			+21.20	42.82			
4	S $56^\circ$ E	27.60		15.44	22.88			-15.29	+22.82	86.84		1327.7836	
5	S $33\frac{1}{4}^\circ$ W	18.80		15.72		10.31		-15.63	-10.36	99.30		1552.0590	
6	N $74\frac{1}{2}^\circ$ W	30.95	8.27			29.83		+8.43	-29.91	59.03	497.6229		
Sum of courses 132.40			30.58	31.16	54.97	54.65					792.7898	2879.8426	
				30.58	54.65							792.7898	
Error in northing ..			0.58	0.32	Error in Westing						2)2087.0528		
					Ans. 104A 1R 16P . . . . .						1043.5264		

Plot of the example.



32. REMARK. When a bearing is due east or west, the error in latitude is nothing; the course must then be subtracted from the sum of the courses, and the remainder taken in balancing the columns of latitude. In the last example, the 3d bearing is due east, and the first term of the several proportions for error in latitude, was  $132.40 - 21.25 = 111.15$ .

In like manner, if a bearing is due north or south, the error in departure is nothing; and the sum of the courses must be diminished by this course, before balancing the columns of departure.

2. Required the contents, and plot of a piece of land, of which the following are the field notes.

Stations.	Bearings.	Distances.
1	S $34^\circ$ W	3.95 ch.
2	S	4.60
3	S $36\frac{1}{2}^\circ$ E	8.14
4	N $59\frac{1}{2}^\circ$ E	3.72
5	N $25^\circ$ E	6.24
X 6	N $16^\circ$ W	3.50
7	N $65^\circ$ W	8.20

*Ans.* 10A. 0R. 5P.

3. Required the contents and plot of a piece of land, from the following field notes.

Stations.	Bearings.	Distances.
1	S $40^\circ$ W	70 rods
2	N $45^\circ$ W	89
3	N $36^\circ$ E	125
4	N	54
5	S $81^\circ$ E	186
6	S $8^\circ$ W	137
7	W	130

*Ans.* 207A. 3R. 33P.

4. Required the contents and plot of a piece of land, from the following field notes.

Stations.	Bearings.	Distances.
1	S $40\frac{1}{2}^\circ$ E	31.80 ch.
2	N $54^\circ$ E	2.08
3	N $29\frac{1}{4}^\circ$ E	2.21
4	N $28\frac{3}{4}^\circ$ E	35.35
5	N $57^\circ$ W	21.10
6	S $47^\circ$ W	31.30

*Ans.* 92A. 3R. 32P.

5. Required the area of a survey of which the following are the field notes.

Stations.	Bearings.	Distances.
1	N $42^\circ$ E	5.00 ch.
2	East.	4.00
3	N $9^\circ$ E	4.00
4	S $69^\circ$ E	5.56
5	S $36^\circ$ E	7.00
6	S $42^\circ$ W	4.00
7	S $75^\circ$ W	10.00
8	N $39^\circ$ W	7.50

If, in this example, we assume 1 as the principal station, the double meridian distances will all be plus, and the positive area will exceed the negative.

In balancing we shall find the error in southing to be .28 ch. and in westing .22 ch. The area is 13A. 0R. 11P. It should however be remarked, that in all the examples the answers may be slightly varied by distributing the corrections.

6. What is the area of a survey of which the following are the field notes.

Stations.	Bearings.	Distances.
1	N 75° 00' E	54.8 rods.
2	N 20° 30' E	41.2
3	East.	64.8
4	S 33° 30' W	141.2
5	S 76° 00' W	64.0
6	North.	36.0
7	S 84° 00' W	46.4
8	N 53° 15' W	46.4
9	N 36° 45' E	76.8
10	N 22° 30' E	56.0
11	S 76° 45' E	48.0
12	S 15° 00' W	43.4
13	S 16° 45' W	40.5

In this survey 4 is the most easterly and 9 the most westerly station. The area is equal to 110A. 2R. 23P. It may vary a little, on account of the way in which the balancing is done.

7. What are the contents of a piece of land of which the following are the field notes?

Stations.	Bearings.	Distances.
1	S 75° W	13.70 ch.
2	S 20½° W	10.30
3	West.	16.20
4	N 33½° E	35.30
5	N 76° E	16.00
6	South.	9.00
7	N 84° E	11.60
8	S 53¼° E	11.60
9	S 36¾° W	19.20
10	S 22½° W	14.00
11	N 76¾° W	12.00
12	N 15° E	10.85
13	N 16¾° E	10.12

In this survey 4 is the most westerly station and 9 the most easterly. The area is  $110A. 2R. 23P.$  The result may, however, as in the other examples, be slightly varied by the balancing.

8. What is the area of a survey of which the following are the notes?

Stations.	Bearings.	Distances.
1	S $46\frac{1}{2}^{\circ}$ E	80 rods
2	S $51\frac{3}{4}^{\circ}$ W	55.20
3	West.	85
4	N $56^{\circ}$ W	110.40
5	N $33\frac{1}{4}^{\circ}$ E	75.20
6	S $74\frac{1}{2}^{\circ}$ E	123.80

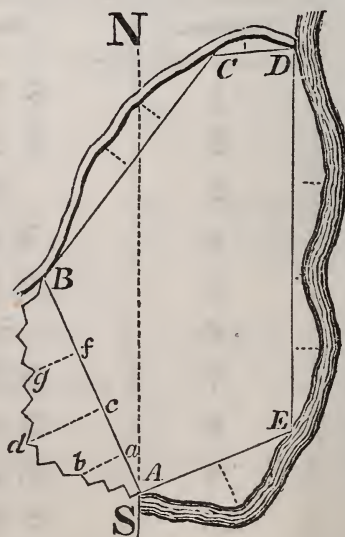
*Ans* 104A. 1R. 16P.

I. To determine the contents and boundary of a piece of land, by means of offsets from the principal lines.

33. An offset is a line measured perpendicular to a course, and may lie either on the right or left of it.

Let  $ABCDE$  be a piece of ground to be surveyed. Let us suppose it to be bounded on the west and north by a fence and road, and on the east and south by a creek or river.

Assume as stations the principal points  $A, B, C, D,$  and  $E.$  Take, with the compass, the bearings from  $A$  to  $B,$  from  $B$  to  $C,$  from  $C$  to  $D,$  from  $D$  to  $E,$  and from  $E$  to  $A;$  and measure the distances  $AB, BC, CD, DE,$  and  $EA.$



At convenient points of the course  $AB,$  as  $a, c,$  and  $f,$  measure the offsets  $ab, cd, fg.$  Then, having measured these lines, as also the distances  $Aa, ac, cf,$  and  $fB,$  enough



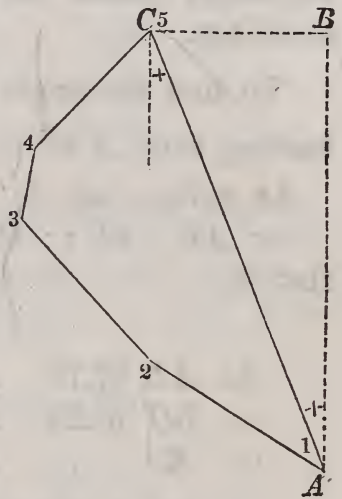
will be known to determine the area which lies without the station line  $AB$ . The points  $b, d$  and  $g$ , of the fence which runs from  $A$  to  $B$ , are also determined.

Erect, in a similar manner, offsets to the other courses, and determine the areas which lie without the station lines. These several areas being added to the area within the station lines, will give the entire area of the ground.

If the offsets fall within the station lines, the corresponding area must be subtracted from the area which is bounded by the station lines.

II. *To determine the bearing and distance from one point to another, when the points are so situated that one cannot be seen from the other.*

34. Let  $A$  and  $C$  be the two points, and  $AB$  a meridian passing through one of them. From either of them, as  $A$ , measure a course  $A2$ , of a convenient length in the direction towards  $C$ , and take the bearing with the compass. At 2, take the bearing of a second course, and measure the distance to 3. At 3, take a third bearing and measure to 4. At 4, take the bearing to  $C$ , and measure the distance from 4 to  $C$ .



Then, the difference between the sum of the northings and the sum of the southings will be represented by  $AB$ , and the difference between the sum of the eastings and the sum of the westings by  $BC$ . The base  $AB$ , and the perpendicular  $BC$  of the right-angled triangle  $ABC$ , are then known. The angle at the base,  $BAC$ , is the bearing from  $A$  to  $C$ ; or the equal alternate angle at  $C$  is the bearing from  $C$  to  $A$ , and the hypotenuse  $AC$  is the distance.

35. Having measured the bearings and courses on the field, form a table, and find the base and perpendicular of the right-angled triangle, in numbers.

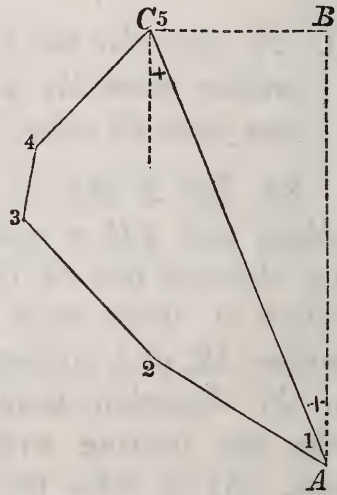
Stations.	Bearings.	Distances.	N.	S.	E.	W.
1	N 61° W	40 ch	19.39			34.98
2	N 42° W	41.	30.47			27.43
3	N 12° E	16.10	15.75		3.35	
4	N 47° E	32.50	22.16		23.77	
$AB = 87.77$					27.12	62.41
						27.12

$CB = 35.29 \text{ ch.}$

REMARK. Had any of the courses run south,  $AB$  would have been equal to the sum of the northings, minus the sum of the southings.

To find the angle  $BAC$ , or the bearing from  $A$  to  $C$ .

As radius :  $\tan A :: AB : BC$ ,  
 or  $AB : BC :: R : \tan A$  :  
 that is,



As	AB 87.77	.	ar. comp.	.	8.056654
:	BC 35.29	.	.	.	1.547652
::	R	.	.	.	10.
:	$\tan A$	21° 54' 12"	.	.	9.604306

To find the distance  $AC$ .

As	sin $A$	21° 54' 12"	ar. comp.	.	0.428242
:	$R$	.	.	.	10.
::	BC	35.29	.	.	1.547652
:	AC	94.6	.	.	1.975894

Hence, the bearing and distance are both found.

OF SUPPLYING OMISSIONS IN THE FIELD NOTES.

36. The last problem affords an easy method of finding the bearing and length of one of the courses of a survey,

when the bearings and lengths of all the others are known. It may be necessary to use this method when there are obstacles which prevent the measuring of a course, or when the bearing cannot be taken. Indeed, *two omissions* may in general be supplied by calculation. It is far better, however, if possible, to take all the notes on the field. For, when any of them are supplied by calculation, there are no tests by which the accuracy of the work can be ascertained, and all the errors of the notes affect also the parts which are supplied.

1. In a survey we have the following notes :

Stations.	Bearings.	Distances.
1	N $31\frac{1}{2}^{\circ}$ W	10 ch.
2	N $62\frac{3}{4}^{\circ}$ E	9.25
3	Lost.	Lost.
4	S $45\frac{1}{2}^{\circ}$ W	10.40

What is the bearing and distance from station 3 to 4 ?

$$Ans. \left\{ \begin{array}{l} \text{Bearing, S } 38^{\circ} 52' \text{ E.} \\ \text{Distance, } 7.03 \text{ ch.} \end{array} \right.$$

2. In a survey we have the following notes :

Stations.	Bearings.	Distances.
1	S $40\frac{1}{2}^{\circ}$ E	31.80 ch.
2	N $54^{\circ}$ E	2.08
3	Lost.	Lost.
4	N $28\frac{3}{4}^{\circ}$ E	35.35
5	N $57^{\circ}$ W	21.10
6	S $47^{\circ}$ W	31.30

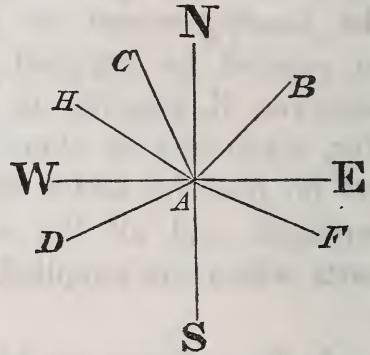
What is the bearing and distance from 3 to 4 ?

$$Ans. \left\{ \begin{array}{l} \text{Bearing, N } 34^{\circ} 47' \text{ E.} \\ \text{Distance, } 2.19 \text{ ch.} \end{array} \right.$$

III. To determine the angle included between any two courses, when their bearings are known.

37. Let NS be a meridian passing through A.

Let AB, AC, AH, AD, and AF, be five courses running from A. We readily deduce the following



PRINCIPLES.

$$\begin{array}{l} AC \text{ is N } 26^\circ \text{ W} \\ AH \text{ is N } 65^\circ \text{ W} \\ \hline CAH = 39^\circ \end{array}$$

When the meridional letters are alike, and those of departure also alike, the difference of the bearings is the angle between the courses.

$$\begin{array}{l} AB \text{ is N } 46^\circ \text{ E} \\ AC \text{ is N } 26^\circ \text{ W} \\ \hline CAB = 72^\circ \end{array}$$

When the meridional letters are alike, and those of departure unlike, the sum of the bearings is the angle between the courses.

$$\begin{array}{l} AC \text{ is N } 26^\circ \text{ W} \\ AD \text{ is S } 66^\circ \text{ W} \\ \hline CAD = 180^\circ - 92^\circ = 88^\circ \end{array}$$

When the meridional letters are unlike, and those of departure alike, the angle between the courses is equal to  $180^\circ$ , minus the sum of the bearings.

$$\begin{array}{l} AC \text{ is N } 26^\circ \text{ W} \\ AF \text{ is S } 66^\circ \text{ E} \\ \hline CAF = 180^\circ - 40^\circ = 140^\circ \end{array}$$

When the meridional letters are unlike, and those of departure also unlike, the angle between the courses is equal to the difference of the bearings taken from  $180^\circ$ .

REMARK. The above principles are determined, under the supposition that the two courses are both run from the angular point. Hence, if it be required to apply them to

two courses run in the ordinary way, as we go around the field, the bearing of one of them must be reversed before the calculation for the angle is made.

1. The bearings of two courses, from the same point, are N  $37^\circ$  E, and S  $85^\circ$  W: what is the angle included between them?

*Ans.*  $132^\circ$ .

2. The bearings of two adjacent courses, in going round a piece of land, are N  $39^\circ$  W, and S  $48^\circ$  W: what is the angle included between them?

*Ans.*  $87^\circ$ .

3. The bearings of two adjacent courses, in going round a piece of land, are S  $85^\circ$  W, and N  $69^\circ$  W: what is the angle included between them?

*Ans.*  $154^\circ$ .

4. The bearings of two adjacent courses, in going round a piece of land, are N  $55^\circ 30'$  E, and S  $69^\circ 20'$  E: what is the angle included between them?

*Ans.*  $124^\circ 50'$ .

#### OF DIVIDING LAND.

38. Fields are so variously shaped that it is difficult to give rules that will apply to all cases. It is by practice alone that facility is obtained in that branch of surveying relating to the division of estates. We shall add only a few examples that may serve as general guides in the application of the principles of Plane Geometry to such cases as may arise.

I. To run a line from the vertex of a triangular field which shall divide it into two parts, having to each other the ratio of  $M$  to  $N$ .

39. Let  $ABC$  be any triangular field.

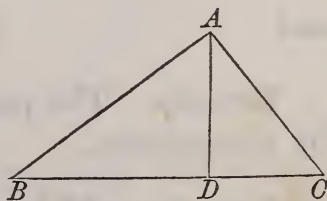
Divide the side  $BC$  into two parts, such that (Geom., Bk. IV., Prob. 1.)

$$BD : DC :: m : n;$$

and draw the line  $AD$ :

then will,

$$ABD : DAC :: m : n.$$



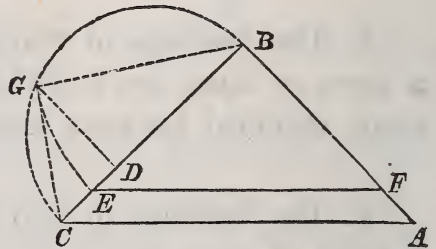
For, the two triangles  $ABD$ ,  $ADC$  having the same altitude are to each other as their bases (Geom., Bk. IV., P. 6, C.): hence, the triangle is divided into parts having the ratio of  $m$  to  $n$ .

II. To run a line parallel to one side of a triangular field, that shall form with the parts of the two other sides a triangle equivalent to the  $\frac{m}{n}$  part of the field.

40. Let  $CBA$  represent a triangular field and  $CA$  the side parallel to which the dividing line is to be drawn.

On the side  $BC$  describe a semicircle: then divide  $BC$  at  $D$ , so that

$$BD : BC :: m : n.$$



At  $D$ , erect the perpendicular  $DG$  to the diameter  $BC$ , and draw  $BG$ . Then, with  $B$  as a centre, and  $BG$  as a radius, describe the arc of a circle cutting  $BC$  at  $E$ . Through  $E$  draw  $EF$  parallel to  $CA$ , and it will divide the triangle in the required ratio.

For, (Geom., Bk. IV., P. 23.)

$$\overline{BG}^2 = \overline{BE}^2 = BC \times BD :$$

or,  $\overline{BE}^2 = \overline{BC}^2 \times \frac{BD}{BC}$ ; whence,

$$\overline{BE}^2 : \overline{BC}^2 :: BD : BC :: m : n.$$

But, since the triangles  $BEF$ ,  $BCA$  are similar,

$$\overline{BE}^2 : \overline{BC}^2 :: BEF : BCA.$$

Wherefore, from equality of ratios,

$$BEF : BCA :: m : n;$$

and

$$BEF = \frac{m}{n} \times BCA.$$

REMARK. The points  $E$  and  $F$  may easily be found by computation.

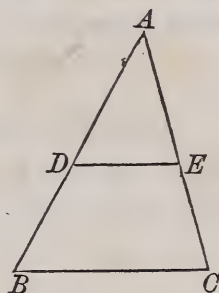
For, since  $\overline{BE}^2 = BC \times BD$ , and  $BD = \frac{m}{n} \times BC$ ,

we have  $\overline{BE}^2 = \overline{BC}^2 \times \frac{m}{n}$ ; or  $BE = BC \sqrt{\frac{m}{n}}$ .

In like manner  $BF = BA \sqrt{\frac{m}{n}}$ .

EXAMPLE.

Let it be required to divide the triangular field  $CAB$ , in which  $AC = 9$  ch.  $AB = 11$  ch. and  $CB = 7$  ch. into two such parts that  $ADE$  shall be one-fourth of the whole field.



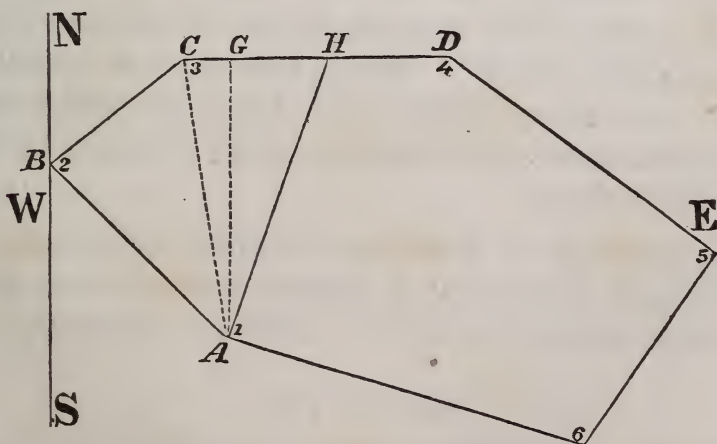
In this case, we have

$$m = 1, n = 4, \text{ and } \sqrt{\frac{m}{n}} = \sqrt{\frac{1}{4}} = \frac{1}{2} :$$

hence,  $AE = 4$  ch. 50 l. and  $AD = 5$  ch. 50 l.

III. To run a line from a given point in the boundary of a piece of land, so as to cut off, on either side of the line, a given portion of the field.

41. Make a complete survey of the field, by the rules already given. Let us take, as an example, the field whose area is computed at page 118. That field contains 104A 1R 16P, and the following is a plot of it.



Let it now be required to run a line from station  $A$ , in such a manner as to cut off on the left any part of the field; say,

$$26A \ 2R \ 31P.$$

It is seen, by examining the field, that the division line will probably terminate on the course  $CD$ . Therefore, draw a line from  $A$  to  $C$ , which we will call the first closing line.

The bearings and lengths of the courses  $AB$ ,  $BC$ , are always known; and in the present example are found in the table on page 118: hence, the bearing and distance from  $C$  to  $A$ , can be calculated by Art. 35: they are in this example,

Bearing S  $9^{\circ} 28'$  E: Course 22.8 ch.

Having calculated the bearing and length of the closing line, find, by the general method, the area which it cuts off: that area, in the present case, is

13A 3R 3P.

It is now evident that the division line must fall on the right of the closing line  $AC$ , and must cut off an area  $ACH$ , equal to the difference between that already cut off, and the given area: that is, an area equal

	26A 2R 31P	given area,
	13A 3R 3P	area already cut off,
	12A 3R 28P.	
to . . .		

Since the bearing of the next course  $CD$ , and the bearing of the closing line  $AC$  are known, the angle  $ACD$  which they form with each other, can be calculated, and is in this example  $80^{\circ} 32'$ . Hence, knowing the hypotenuse  $AC$ , and the angle  $ACG$  at the base, the length  $AG$  of the perpendicular let fall on the course  $CD$ , can be found, and is 22.49 chains.

Since the area of a triangle is equal to its base multiplied by half its altitude, it follows, that the base is equal to the area divided by half the altitude. Therefore, if the area

12A 3R 28P

be reduced to square chains, and divided by  $11.24\frac{1}{2}$  chains, which is half the perpendicular  $AG$ , the quotient, which is 11.58 chains, will be the base  $CH$ . Hence, if we lay off from  $C$ , on  $CD$ , a distance  $CH$ , equal to 11.58 chains, and



then run the line  $AH$ , it will cut off from the land the required area.

REMARK I. If the part cut off by the first closing line, should exceed the given area, the division line will fall on the left of  $AC$ .

REMARK II. If the difference between the given area and the first area cut off, divided by half the perpendicular  $AG$ , gives a quotient larger than the course  $CD$ ; then, draw a line from  $A$  to  $D$ , and consider it as the first closing line, and let fall a perpendicular on  $DE$ .

REMARK III. When the point from which the division line is to be drawn, falls between the extremities of a course, dividing the course into two parts, consider one of the parts as an entire course, and the other as forming a new course, having the same bearing. The manner of making the calculation will then be the same as before.

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## SECTION IV.

### PUBLIC LANDS—VARIATION OF THE NEEDLE.

1. Soon after the organization of the present government, several of the states ceded to the United States large tracts of wild land, and these, together with the lands since acquired by treaty and purchase, constitute what is called the public lands, or public domain. Previous to the year 1802, these lands were parcelled out without reference to any general plan, in consequence of which the titles often conflicted with each other, and in many cases, several grants covered the same premises.

In the year 1802, the following method of surveying the public lands, was adopted by Colonel Jared Mansfield, then surveyor-general of the North-Western Territory.

2. The country to be surveyed is first divided by meridians, six miles distance from each other; and then

again, by a system of east and west lines, also six miles from each other. The country is thus divided into equal squares, which are called *townships*. Hence, each township is a square, six miles on a side, and contains thirty-six square miles.

3. For the purpose of illustration, we have obtained from the general land office the accompanying map, which represents a considerable portion of the State of Arkansas.

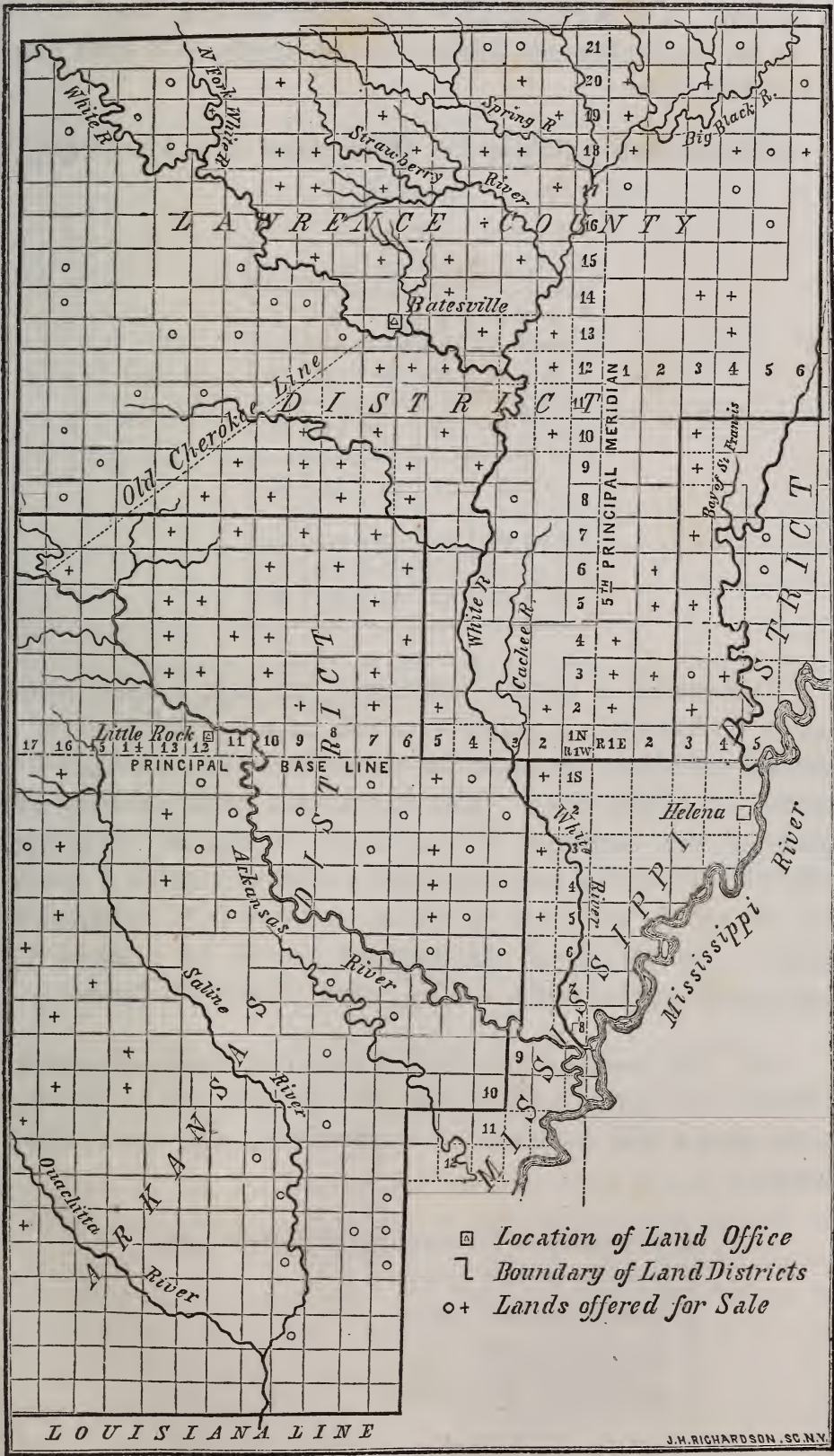
The principal meridian in this Survey is called the 5th meridian, and passes through the point of junction of the White river and the Mississippi. The principal base line, running east and west, intersects this meridian a little to the east of White river; and from the meridian and base line, reckoned from this point of intersection, all the ranges of townships are laid off.

For example, 1 North, will apply to all the townships lying in the first row north of the base line: 1 South, will apply to all the townships in the first row south of the base line. Range 1 East, will apply to all the townships lying in the first row, east of the 5th meridian: and range 1 West, will apply to all lying in the first row to the west of it. The small figures designate the rows of townships, reckoned north and south from the base line, and the ranges reckoned east and west from the 5th meridian. Thus, township 1 North, range 4 West, has its exact place designated, and may be immediately located.

4. The principal meridians, and the principal base lines are established by astronomical observation, and the lines of subdivision run with the compass.

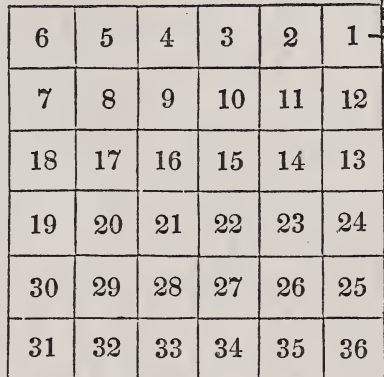
For convenience in making surveys, and for the purpose of designating particular localities, a state or large tract, is often divided into parts called "Districts." There are three such districts in the map before us, the boundaries of which are designated by the full dark lines.

5. Each township is divided into equal squares, by meridians one mile apart, and by east and west lines at the same distance from each other. Hence, each township is divided into 36 square miles, each one of which is called



a *section*. The sections of a township are numbered from 1 to 36, beginning at the north-east angle, and each contains 640 acres.

The diagram exhibits the 36 sections of a township.



6	5	4	3	2	1
7	8	9	10	11	12
18	17	16	15	14	13
19	20	21	22	23	24
30	29	28	27	26	25
31	32	33	34	35	36

To describe a section accurately, we say, section number 5, in township number 4 north, in range 3d west of a known meridian; the one, for example, drawn through the mouth of White river. The description fixes precisely the place of the section. Go to the 3d range of townships, west of the known meridian, find township number 4 north, in this range, and lastly, section number 5 of that township. The corners of the sections should be marked by permanent corner-posts, or by lines blazed on trees.

6. The sections are divided into half sections, quarter sections, and even into eighths of sections. The following table shows the contents of a township, and its subdivisions :

- 1 township = 36 sections = 23040 acres.
- 1 section = 640 acres.
- $\frac{1}{2}$  section = 320 acres.
- $\frac{1}{4}$  section = 160 acres.
- $\frac{1}{8}$  section = 80 acres.

## VARIATION OF THE NEEDLE.

7. The angle which the magnetic meridian makes with the true meridian, at any place on the surface of the earth, is called the *variation of the needle* at that place, and is east or west, according as the north end of the needle lies on the east or west side of the true meridian.

8. The variation is different at different places, and even at the same place it does not remain constant for any length of time. The variation is ascertained by comparing the magnetic, with the true meridian.

9. If we suppose a line to be traced through those points on the surface of the earth, where the needle points directly north, such a line is called the *line of no variation*. At all places lying on the east of this line, the variation of the needle is west; at all places lying on the west of it, the variation is east.

10. The public is much indebted to Professor Loomis, for the valuable results of many observations and much scientific research, on the dip and variation of the needle, contained in the 39th and 42d volumes of Silliman's Journal.

The variation at each place was ascertained for the year 1840; and by a comparison of previous observations and the application of known formulas, the annual motion, or change in variation, at each place, was also ascertained, and both are contained in the tables which follow.

11. If the annual motion was correctly found, and continues uniform, the variation at any subsequent period can be ascertained by simply multiplying the annual motion by the number of years, and adding the product, in the algebraic sense, to the variation in 1840. It will be observed that all variations west are designated by the plus sign; and all variations east, by the minus sign. The annual motions being all west, have all the plus sign.

12. Our first object will be to mark the line, as it was in 1840, of *no variation*. For this purpose we shall make a table of places lying near this line.

## PLACES NEAR THE LINE OF NO VARIATION.

Place.	Latitude.	Longitude.	Variation.	An. Motion.
A Point.	40° 53'	80° 13'	0° 00'	+ 4'.4
Cleveland, O.	41 31	81 45	- 0 19	4.4
Detroit, Mich.	42 24	82 58	- 1 56	4
Mackinaw.	45 51	84 41	- 2 08	3.9
Marietta, O.	39 30	81 28	- 1 24	4.3
Charlottesville, Va.	39 02	78 30	+ 0 19	3.7
Charleston, S. C.	32 42	80 04	- 2 44	1.3

At the point whose latitude is 40° 53', longitude 80° 13', the variation of the needle was nothing in the year 1840, and the direction of the line of no variation, traced north, was N 24° 35' west. The line of no variation, prolonged, passed a little to the east at Cleveland, in Ohio—the variation there being 19 minutes east. Detroit lay still further to the west of this line, the variation there being 1° 56' east; and Mackinaw still further to the west, as the variation at that place was 2° 08' east.

The course of the line of no variation, prolonged south-erly, was S 24° 35' E. Marietta, in Ohio, was west of this line—the variation there being 1° 24' east. Charlottesville, in Virginia, was a little to the east of it—the variation there being 19' west; whilst Charleston, in South Carolina, was on the west,—the variation there being 2° 44' east.

From these results, it will be easy to see about where the line of no variation is traced in our own country.

13. We shall give two additional tables:

PLACES WHERE THE VARIATION WAS WEST.

Places.	Latitude.	Longitude.	Variation.	An. Motion.
Angle of Maine.	48° 00'	67° 37'	+ 19° 30'	+ 8'.8
Waterville, Me.	44 27	69 32	12 36	5.7
Montreal.	45 31	73 35	10 18	5.7
Keesville, N. Y.	44 28	73 32	8 51	5.3
Burlington, Vt.	44 27	73 10	9 27	5.3
Hanover, N. H.	43 42	72 14	9 20	5.2
Cambridge, Mass.	42 22	71 08	9 12	5
Hartford, Ct.	41 46	72 41	6 58	5
Newport, R. I.	41 28	71 21	7 45	5
Geneva, N. Y.	42 52	77 03	4 18	4.1
West Point.	41 25	74 00	6 52	4
New York City.	40 43	71 01	5 34	3.6
Philadelphia.	39 57	75 11	4 08	3.2
Buffalo, N. Y.	42 52	79 06	1 37	4.1

PLACES WHERE THE VARIATION WAS EAST.

Places.	Latitude.	Longitude.	Variation.	An. Motion.
Mouth of Columbia River. }	46° 12'	123° 30'	- 21° 40'	Unknown.
Jacksonville, Ill.	39 43	90 20	8 28	+ 2'.5
St. Louis, Mo.	38 37	90 17	8 37	2.3
Nashville, Tenn.	36 10	86 52	6 42	2
Louisiana, at	29 40	94 00	8 41	1.4
Mobile, Ala.	30 42	88 16	7 05	1.4
Tuscaloosa, Ala.	33 12	87 43	7 26	1.6
Columbus, Geo.	32 28	85 11	5 28	2
Milledgeville, "	33 07	83 24	5 07	2.4
Savannah, "	32 05	81 12	4 13	2.7
Tallahassee, Fl.	30 26	84 27	5 03	1.8
Pensacola, "	30 24	87 23	5 53	1.4
Logansport, Ind.	40 45	86 22	5 24	2.7
Cincinnati, O.	39 06	84 27	4 46	3.1

## METHODS OF ASCERTAINING THE VARIATION.

14. The best practical method of determining the true meridian of a place, is by observing the north star. If this star were precisely at the point in which the axis of the earth, prolonged, pierces the heavens, then, the intersection of the vertical plane passing through it and the place, with the surface of the earth, would be the true meridian. But, the star being at a distance from the pole, equal to  $1^{\circ} 30'$  nearly, it performs a revolution about the pole in a circle, the polar distance of which is  $1^{\circ} 30'$ : the time of revolution is 23 h. and 56 min.

To the eye of an observer, this star is continually in motion, and is due north but twice in 23 h. 56 min.; and is then said to be on the meridian. Now, when it departs from the meridian, it apparently moves east or west, for 5 h. and 59 min., and then returns to the meridian again. When at its greatest distance from the meridian, east or west, it is said to be at its greatest *eastern* or *western* elongation.

The following tables show the times of its greatest eastern and western elongations :

## EASTERN ELONGATIONS.

Days.	April.	May.	June.	July.	August.	Sept.
	H. M.	H. M.	H. M.	H. M.	H. M.	H. M.
1	18 18	16 26	14 24	12 20	10 16	8 20
7	17 56	16 03	14 00	11 55	9 53	7 58
13	17 34	15 40	13 35	11 31	9 30	7 36
19	17 12	15 17	13 10	11 07	9 08	7 15
25	16 49	14 53	12 45	10 43	8 45	6 53

## WESTERN ELONGATIONS.

Days.	Oct.	Nov.	Dec.	Jan.	Feb.	March.
	H. M.	H. M.	H. M.	H. M.	H. M.	H. M.
1	18 18	16 22	14 19	12 02	9 50	8 01
7	17 56	15 59	13 53	11 36	9 26	7 38
13	17 34	15 35	13 27	11 10	9 02	7 16
19	17 12	15 10	13 00	10 44	8 39	6 54
25	16 49	14 45	12 34	10 18	8 16	6 33



The eastern elongations are put down from the first of April to the first of October; and the western, from the first of October to the first of April; the time is computed from 12 at noon. The western elongations in the first case, and the eastern in the second, occurring in the daytime, cannot be used. Some of those put down are also invisible, occurring in the evening, before it is dark, or after daylight in the morning. In such case, if it be necessary to determine the meridian at that particular season of the year, let 5 h. and 59 min. be added to, or subtracted from, the time of greatest eastern or western elongation, and the observation be made at night, when the star is on the meridian.

15. The following table exhibits the angle which the meridian plane makes with the vertical plane passing through the pole-star, when at its greatest eastern or western elongation: such angle is called the *azimuth*. The mean angle only is put down, being calculated for the first of July of each year:

AZIMUTH TABLE.

Year.	Lat. 32° Azimuth.	Lat. 34° Azimuth.	Lat. 36° Azimuth.	Lat. 38° Azimuth.	Lat. 40° Azimuth.	Lat. 42° Azimuth.	Lat. 44° Azimuth.
1851	1° 45½'	1° 48'	1° 50½'	1° 53½'	1° 56¾'	2° 00¼'	2° 04¼'
1852	1° 45'	1° 47½'	1° 50'	1° 53'	1° 56¼'	1° 59¾'	2° 03¾'
1853	1° 44½'	1° 47'	1° 49¾'	1° 52½'	1° 55¾'	1° 59¼'	2° 03¼'
1854	1° 44¼'	1° 46½'	1° 49¼'	1° 52'	1° 55¼'	1° 59'	2° 02¾'
1855	1° 43¾'	1° 46¼'	1° 48¾'	1° 51¾'	1° 54¾'	1° 58½'	2° 02¼'
1856	1° 43¼'	1° 45¾'	1° 48¼'	1° 51¼'	1° 54½'	1° 58'	2° 01¾'
1857	1° 43'	1° 45¼'	1° 48'	1° 50¾'	1° 54'	1° 57½'	2° 01¼'
1858	1° 42½'	1° 44¾'	1° 47½'	1° 50¼'	1° 53½'	1° 57'	2° 00¾'
1859	1° 42'	1° 44½'	1° 47'	1° 49¾'	1° 53'	1° 56½'	2° 00¼'
1860	1° 41¾'	1° 44'	1° 46½'	1° 49½'	1° 52½'	1° 56'	2° 00'
1861	1° 41¼'	1° 43¾'	1° 46¼'	1° 49'	1° 52¼'	1° 55¾'	1° 59½'

The use of the above tables, in finding the true meridian, will soon appear.

TO FIND THE TRUE MERIDIAN WITH THE THEODOLITE.

16. Take a board, of about one foot square, paste white paper upon it, and perforate it through the centre; the diameter of the hole being somewhat larger than the diameter of the telescope of the theodolite. Let this board be so fixed to a vertical staff, as to slide up and down freely: and let a small piece of board, about three inches square, be nailed to the lower edge of it, for the purpose of holding a candle.

About twenty-five minutes before the time of the greatest eastern or western elongation of the pole-star, as shown by the tables of elongations, let the theodolite be placed at a convenient point and levelled. Let the board be placed about one foot in front of the theodolite, a lamp or candle placed on the shelf at its lower edge; and let the board be slipped up or down, until the pole-star can be seen through the hole. The light reflected from the paper will show the cross hairs in the telescope of the theodolite.

Then, let the vertical spider's line be brought exactly upon the pole-star, and, if it is an eastern elongation that is to be observed, and the star has not yet reached the most easterly point, it will move from the line towards the east, and the reverse when the elongation is west.

At the time the star attains its greatest elongation, it will appear to coincide with the vertical spider's line for some time, and then leave it, in the direction contrary to its former motion.

As the star moves towards the point of greatest elongation, the telescope must be continually directed to it, by means of the tangent-screw of the vernier plate; and when the star has attained its greatest elongation, great care should be taken that the instrument be not afterwards moved.

Now, if it be not convenient to leave the instrument in its place until daylight, let a staff, with a candle or small

lamp upon its upper extremity, be arranged at thirty or forty yards from the theodolite, and in the same vertical plane with the axis of the telescope. This is easily effected, by revolving the vertical limb about its horizontal axis without moving the vernier plate, and aligning the staff to coincide with the vertical hair. Then mark the point directly under the theodolite; the line passing through this point and the staff, makes an angle with the true meridian equal to the azimuth of the pole-star.

From the table of azimuths, take the azimuth corresponding to the year and nearest latitude. If the observed elongation was east, the true meridian lies on the west of the line which has been found, and makes with it an angle equal to the azimuth. If the elongation was west, the true meridian lies on the east of the line: and, in either case, laying off the azimuth angle with the theodolite, gives the true meridian.

#### TO FIND THE TRUE MERIDIAN WITH THE COMPASS.

17. 1. Drive two posts firmly into the ground, in a line nearly east and west; the uppermost ends, after the posts are driven, being about three feet above the surface, and the posts about four feet apart: then lay a plank, or piece of timber three or four inches in width, and smooth on the upper side, upon the posts, and let it be pinned or nailed, to hold it firmly.

2. Prepare a piece of board four or five inches square, and smooth on the under side. Let one of the compass-sights be placed at right angles to the upper surface of the board, and let a nail be driven through the board, so that it can be tacked to the timber resting on the posts.

3. At about twelve feet from the stakes, and in the direction of the pole-star, let a plumb be suspended from the top of an inclined stake or pole. The top of the pole should be of such a height that the pole-star will appear about six inches below it; and the plumb should be swung in a vessel of water to prevent it from vibrating.

This being done, about twenty minutes before the time of elongation, place the board, to which the compass-sight is fastened, on the horizontal plank, and slide it east or west, until the aperture of the compass-sight, the plumb-line, and the star, are brought into the same range. Then if the star depart from the plumb-line, move the compass-sight, east or west, along the timber, as the case may be, until the star shall attain its greatest elongation, when it will continue behind the plumb-line for several minutes; and will then recede from it in the direction contrary to its motion before it became stationary. Let the compass-sight be now fastened to the horizontal plank. During this observation it will be necessary to have the plumb-line lighted: this may be done by an assistant holding a candle near it.

Let now a staff, with a candle or lamp upon it, be placed at a distance of thirty or forty yards from the plumb-line, and in the same direction with it and the compass-sight. The line so determined, makes, with the true meridian, an angle equal to the azimuth of the pole-star; and, from this line, the variation of the needle is readily determined, even without tracing the true meridian on the ground.

Place the compass upon this line, turn the sights in the direction of it, and note the angle shown by the needle. Now, if the elongation, at the time of observation, was west, and the north end of the needle is on the west side of the line, the azimuth, plus the angle shown by the needle, is the true variation. But should the north end of the needle be found on the east side of the line, the elongation being west, the difference between the azimuth and the angle would show the variation: and the reverse when the elongation is east.

1. Elongation west, azimuth . . .  $2^{\circ} 04'$   
 North end of the needle on the west, angle  $4^{\circ} 06'$

Variation  $6^{\circ} 10'$  west.

2. Elongation west, azimuth . . .  $1^{\circ} 59'$   
 North end of the needle on the east, angle  $4^{\circ} 50'$   
 Variation  $2^{\circ} 51'$  east.

3. Elongation east, azimuth . . .  $2^{\circ} 05'$   
 North end of the needle on the west, angle  $8^{\circ} 30'$   
 Variation  $6^{\circ} 25'$  west.

4. Elongation east, azimuth . . .  $1^{\circ} 57'$   
 North end of the needle on the east, angle  $8^{\circ} 40'$   
 Variation  $10^{\circ} 37'$  east.

REMARK I. The variation at West Point, in September, 1835, was  $6^{\circ} 32'$  west.

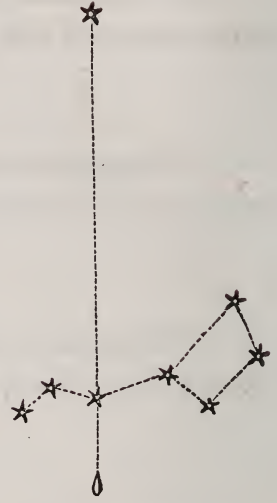
REMARK II. The variation of the needle should always be noted on every survey made with the compass, and then if the land be surveyed at a future time, the old lines can always be re-run.

18. It has been found by observation, that heat and cold sensibly affect the magnetic needle, and that the same needle will, at the same place, indicate different lines at different hours of the day.

If the magnetic meridian be observed early in the morning, and again at different hours of the day, it will be found that the needle will continue to recede from the meridian as the day advances, until about the time of the highest temperature, when it will begin to return, and at evening will make the same line as in the morning. This change is called the *diurnal variation*, and varies, during the summer season, from one-fourth to one-fifth of a degree.

19. A very near approximation to a true meridian, and consequently to the variation, may be had, by remembering that the pole-star very nearly reaches the true meridian, when it is in the same vertical plane with the star Alioth in the tail of the Great Bear, which lies nearest the four stars forming the quadrilateral.

The vertical position can be ascertained by means of a plumb-line. To see the spider's lines in the field of the telescope at the same time with the star, a faint light should be placed near the object-glass. When the plumb-line, the star Alioth, and the north star, fall on the vertical spider's line, the horizontal limb is firmly clamped, and the telescope brought down to the horizon; a light, seen through a small aperture in a board, and held at some distance by an assistant, is then moved according to signals, until it is covered by the intersection of the spider's lines. A picket driven into the ground, under the light, serves to mark the meridian line for reference by day, when the angle formed by it and the magnetic meridian may be measured.



# B O O K I I I .

## LEVELLING AND TOPOGRAPHICAL SURVEYING.

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### SECTION I.

#### OF LEVELLING.

1. LEVELLING is the art of determining the relative distances of points from the centre of the earth.

2. A line whose points are all equally distant from the centre of the earth, is called a line of *true level*, and a surface, all whose points are equally distant from the centre of the earth, as the surface of still water, is called a *level surface*.

3. One point is said to be above another, when it is farther from the centre of the earth; and this difference of distance from the centre, is called the *difference of level* between the two points.

4. A straight line drawn tangent to a line of true level at any point, is a horizontal line, and is called a line of *apparent level*. Thus (Pl. 4, Fig. 1), if  $C$  is the centre of the earth and  $AEF$  a line of true level,  $ABD$  is a line of apparent level. This is the line of level determined by an instrument. The difference between the *apparent* and *true* level at any distant station  $B$ , as determined from  $A$ , is  $BE$ , or the *excess* of the secant of the arc  $AE$  over the radius.

5. To find a general formula for computing this excess, we have (Geom. B. IV., Prop. XXX.)

$$\overline{AB}^2 = BE (BE + 2EC);$$

but since the arc  $AE$  is very small in comparison with the

radius of the earth, the arc  $AE$  will not differ sensibly from the tangent  $AB$ ; the diameter  $2EC$  may, for the same reason, be taken for the secant  $(BE + 2EC)$ : hence,

$$\overline{AE}^2 = BE \times 2EC, \text{ or dividing by } 2EC,$$

$$BE = \frac{\overline{AE}^2}{2EC} \quad (1).$$

If we take the mean diameter of the earth to be 7919 miles, formula (1) gives  $BE = \frac{\overline{AE}^2}{7919}$  (2): hence,

*The departure of the apparent from the true level, starting from a given point, is equal to the square of the distance to the second point, divided by the diameter of the earth.*

If in formula (2) you give to  $AE$ , in succession, every value from 1 chain to any given number of chains, (say 100), and reduce at the same time both terms of the fraction to inches, a table may be computed as below.

*Table showing the differences in inches between the true and apparent level, for distances between 1 and 100 chains.*

Chains.	Inches.	Chains.	Inches.	Chains.	Inches.	Chains.	Inches.
1	.001	26	.845	51	3.255	76	7.221
2	.005	27	.911	52	3.380	77	7.412
3	.011	28	.981	53	3.511	78	7.605
4	.020	29	1.051	54	3.645	79	7.802
5	.031	30	1.125	55	3.781	80	8.001
6	.045	31	1.201	56	3.925	81	8.202
7	.061	32	1.280	57	4.061	82	8.406
8	.080	33	1.360	58	4.205	83	8.612
9	.101	34	1.446	59	4.351	84	8.832
10	.125	35	1.531	60	4.500	85	9.042
11	.151	36	1.620	61	4.654	86	9.246
12	.180	37	1.711	62	4.805	87	9.462
13	.211	38	1.805	63	4.968	88	9.681
14	.245	39	1.901	64	5.120	89	9.902
15	.281	40	2.003	65	5.281	90	10.126
16	.320	41	2.101	66	5.443	91	10.351
17	.361	42	2.208	67	5.612	92	10.587
18	.405	43	2.311	68	5.787	93	10.812
19	.451	44	2.420	69	5.955	94	11.046
20	.500	45	2.531	70	6.125	95	11.233
21	.552	46	2.646	71	6.302	96	11.521
22	.605	47	2.761	72	6.480	97	11.763
23	.661	48	2.880	73	6.662	98	12.017
24	.720	49	3.004	74	6.846	99	12.246
25	.781	50	3.125	75	7.032	100	12.502



Observing that for  $AE = 80$  chains = 1 mile,  $BE$  is equal to 8.001 inches, or about two-thirds of a foot, and since the differences of level vary as the squares of the distances, we have the following easy rule for finding the correction in feet.

*The correction for curvature, in feet, is equal to two-third of the square of the distance in miles.*

#### INSTRUMENTS.

6. Before proceeding further in the discussion of the principles of levelling, we will describe some of the instruments used, and first,

#### THE Y LEVEL.

7. A level is an instrument used to determine horizontal lines, and the difference of level of any two points on the surface of the earth.

The part of the instrument shown in Pl. 4, Fig. 2, rests on a tripod, to which it is permanently attached at  $Z$ .  $HH$  is a horizontal brass plate, through which four levelling screws with milled heads are passed, and worked against a second horizontal plate  $GG$ . Two of these screws,  $K$  and  $I$ , are seen in the figure.  $S$  is a clamp-screw, which, being loosened, allows the upper part of the instrument to turn freely around its axis.  $Q$  is a tangent-screw, by means of which the upper part of the instrument is moved gently, after the clamp-screw  $S$  has been made fast.  $EE$  is a horizontal bar, perpendicular to which are the wyes, designated  $Y$ 's, that support the telescope  $LB$ . This telescope is confined in the  $Y$ 's by the loops  $r, r$ , which are fastened by the pins  $p$  and  $p$ . The object-glass  $B$ , is adjusted to its focus by the screw  $X$ ; the eye-glass  $L$  slides out and in freely. The screws  $f, f$ , work the slide which carries the horizontal hair; and two horizontal screws, only one of which,  $a$ , is seen, work the slide that carries the vertical hair.  $CD$  is an attached spirit-level. The screw  $N$  elevates and depresses the  $Y$ , nearest the eye-glass. In some instruments this  $Y$  is elevated and depressed, by means of two screws at  $M$  and  $R$ .

Before using this level, it must be adjusted. The adjustment consists in bringing the different parts to their proper places.

The line of *collimation* is the axis of the telescope. With this axis, the line drawn through the centre of the eye-glass and the intersection of the spider's lines, within the barrel of the telescope, ought to coincide.

FIRST ADJUSTMENT.\* *To fix the intersection of the spider's lines in the axis of the telescope.*

Having screwed the tripod to the instrument, extend the legs, and place them firmly. Then loosen the clamp-screw *S*, and direct the telescope to a small, well-defined, and distant object. Then slide the eye-glass till the spider's lines are seen distinctly; after which, with the screw *X*, adjust the object-glass to its proper focus, when the object and the spider's lines will be distinctly seen. Note now the precise point covered by the intersection of the spider's lines.

Having done this, revolve the telescope in the *Y*'s, half round, when the attached level *CD* will come to the upper side. See if, in this position, the horizontal hair appears above or below the point, and in either case, loosen the one, and tighten the other, of the two screws which work the horizontal hair, until it has been carried over half the space between its last position and the observed point. Carry the telescope back to its place; direct again, by the screws at *M* and *R*, the intersection of the spider's lines to the point, and repeat the operation, till the horizontal hair neither ascends nor descends while the telescope is revolved. A similar process will arrange the vertical hair, and the line of collimation is then adjusted.

SECOND ADJUSTMENT. *To make the axis of the attached level *CD* parallel to the line of collimation.*

Turn the levelling screws *M* and *R*, until the bubble

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\* This, and some of the following adjustments, are so similar to those of the theolite, that they would not be here repeated, but that some may use the level without wishing to study a more complicated instrument.

of the level  $DC$  stands at the middle of the tube. Then open the loops, and reverse the telescope. If the bubble still stands at the middle of the tube, the axis of the level is horizontal; but if not, it is inclined, the bubble being at the elevated end. In such case, raise the depressed, or depress the elevated end, by means of the small screw  $h$ , half the inclination; and then with the screws, at  $M$  and  $R$ , bring the level to a horizontal position. Reverse the telescope in the  $Y$ 's, and make similar corrections again; and proceed thus, until the bubble stands in the middle of the tube, in both positions of the telescope; the axis of the level is then horizontal.

Let the telescope be now revolved in the  $Y$ 's. If the bubble continues in the middle of the tube, the axis of the level is not only horizontal, but also parallel to the line of collimation. If, however, the bubble recedes from the centre, the axis of the level is inclined to the line of collimation, and must be made parallel to it, by means of two small screws, which work horizontally; one of these screws is seen at  $q$ . By loosening one of them, and tightening the other, the level is soon brought parallel to the line of collimation; and then, if the telescope be revolved in the  $Y$ 's, the bubble will continue at the middle of the point of the tube. It is, however, difficult to make the first part of this adjustment, while the axis of the level is considerably inclined to the line of collimation: for, allowing the level to be truly horizontal in one position of the telescope, after it is reversed, there will be but one corresponding position in which the bubble will stand at the middle of the tube. This suggests the necessity of making the first part of the adjustment with tolerable accuracy; then, having made the second with care, re-examine the first, and proceed thus till the adjustment is completed.

**THIRD ADJUSTMENT.** *To make the level  $CD$  and the line of collimation perpendicular to the axis of the instrument, or parallel to the horizontal bar  $EE$ .*

Loosen the clamp-screw  $S$ , and turn the bar  $EE$ , until the level  $DC$  comes directly over two of the levelling

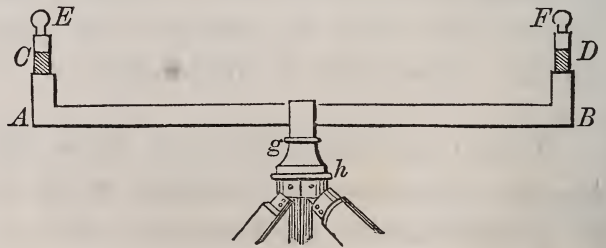
screws. By means of these screws, make the level  $CD$  truly horizontal. Then, turn the level quite round; if, during the revolution, it continue horizontal, it must be at right angles to the axis of the instrument about which it has been revolved. But if, after the revolution, the level  $CD$  be not horizontal, rectify half the error with the screws at  $M$  and  $R$ , and half with the levelling screws. Then place the bar  $EE$  over the other two levelling screws, and make the same examinations and corrections as before; and proceed thus, until the level can be turned entirely around without displacing the bubble at the centre. When this can be done, it is obvious that the level  $DC$  and the line of collimation, are at right angles to the axis of the instrument about which they revolve; and since the axis is carefully adjusted by the maker, at right angles to the bar  $EE$ , it follows, that the line of collimation, the level  $DC$ , and the bar  $EE$ , are parallel to each other.

The level is now adjusted. When used, however, it is best to re-examine it every day or two, as the work will be erroneous unless the instrument is accurately adjusted.

#### THE WATER LEVEL.

8. The Water Level is an instrument that possesses the advantage of *never requiring adjustment*, and also of being very cheap; in fact, any ordinary workman may construct one. Having no telescope, it is impossible to take long sights, but for such work as is required to be done by the ordinary surveyor, it gives very good results.

Two brass cups,  $C$  and  $D$ , about one inch in diameter, and from four to five inches in height, are permanently attached to a hollow brass tube of three feet long and half an inch in diameter. The cups are for the purpose of receiving the ends  $E$  and  $F$  of two bottles, the bottoms of which have been cut off. The bottoms may be cut off by means of a hot iron, or file. The ends are fixed in their places with putty.



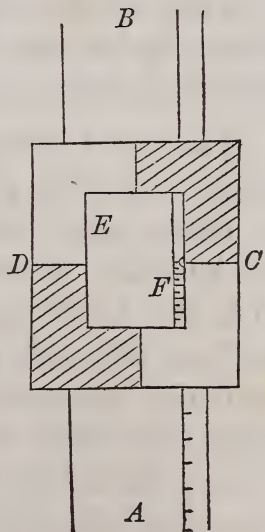
The projecting axis  $g$  works in a hollow cylinder  $h$ , which forms the top of a stand. The tube, when the level is required for use, is filled with water (colored with lake or indigo), till it nearly reaches the necks of the bottles. After placing the stand tolerably level by the eye, withdraw both corks, and the surface of the water in the bottles will indicate a horizontal line in whatever direction the tube is turned. This level is well adapted to tracing contour lines as described in the next section.

#### LEVELLING STAVES.

9. The levelling staves are used to determine the points at which a given horizontal line intersects lines that are perpendicular to the surface of the earth, and to show the distances of such points of intersection from the ground.

The levelling staff is a necessary accompaniment to either of the levels described. Several kinds are used.

One of the best, consists of a staff 12 or 15 feet long, and graduated to feet, tenths, and hundredths. A sliding vane is made to move up or down by a cord and pulleys, and on the vane is a vernier, by means of which the reading of the staff may be effected to thousandths of a foot.  $AB$  represents a portion of the staff,  $DC$  the moveable vane, with an opening  $EF$ , through which the graduation on the staff is seen.  $F$  is the vernier of the vane, the 0 being determined by the transverse line  $DC$ . To render this line more distinct, the vane is divided into four quarters, and the alternate ones are painted black, which, by their contrast with the white quarters, show the line  $DC$  distinctly.



10. Another variety of levelling staff is shown in Pl. 4, Fig. 3. It is formed of two pieces, each about six feet long, one of which slides in a groove of the other, and bears a vane similar to that already described. It is graduated to feet, inches, and eighths of an inch. The line of

sight of the telescope is always directed to the centre of the vane. When the line of sight is less than six feet from the ground, the staff is reversed,—the vane run up the staff, and the readings made by means of the reversed figures at the right, where they are cut by the lower line of the vane. When the line of sight is more than six feet from the ground, the staff stands as in the figure, the reading is then made at the line *bc*, and the figures indicating the height, are found on the sliding part which carries the vane. The reading of the staff, as it now stands, is seven feet.

11. Another rod is sometimes used on which the figures are marked so plainly, that they may be read by the observer himself, without the aid of a vane; thus avoiding errors through ignorance or negligence of the rodman.

If the telescope used, inverts the object, the figures should be made inverted on the staff, so as to appear erect. Each of the rods described, has its advantages, and either one may be used according to the circumstances of the survey.

12. There is a method of testing the adjustments of the Y level, which ought not to be neglected, since all the results depend on the accuracy of the instrument. The method is this:

The level being adjusted, place it at any convenient point, as *G* (Fig. 4). At equal distances of about 100 yards, on either side, and in the same line with the level, place the levelling staves, *CE*, *BF*. Make the level horizontal with the levelling screws. Then, turn it towards either staff, as *BF*, and run the vane up or down, as required, until the intersection of the hairs strikes the centre: then make the slide fast, and note carefully the height of the vane. Turn the level half round, and do the same in respect of the staff *CE*.

Let the telescope be now reversed in the Y's. Sight again to the staff *BF*, and note the exact height of the vane. Let the telescope be now turned half round, and the same be done for the staff *CE*. If the two heights last observed, are equal to those first noted, each to each, the line of collimation is perpendicular to the axis of the

instrument, and if the bubble has, at the same time, preserved its place at the middle point of the tube, the instrument is truly adjusted.

For, had the line of collimation been inclined to the axis of the level, it would, in the first instance, have taken the direction  $AF$  or  $Ad$ ; and when turned half round, it would have taken the direction  $AE$  or  $Ab$ . The telescope being reversed in the  $Y$ 's, and again directed to the staff  $BF$ , the line of collimation would take the direction  $Ad$  or  $AF$ , and when turned to the staff  $CE$ , it would take the direction  $Ab$  or  $AE$ : and the two distances  $BF$ ,  $Bd$ , or  $Cb$ ,  $CE$ , can only be equal to each other when the line of collimation falls on the horizontal line  $gf$ .

#### LEVELLING IN THE FIELD.

13. The operation of levelling may be undertaken:

1st. For the purpose of determining the difference of level between two given points.

2d. For the purpose of obtaining a section or profile along a given line, as in the reconnoissance for a line of railroad.

3d. For the purpose of determining the contour lines in a topographical survey, as described in the next section.

#### DIFFERENCE OF LEVEL BETWEEN TWO POINTS.

14. When it is proposed to find the difference of level of any two objects, or stations, all levels made in the direction of the station at which the work is begun, are called, for the sake of distinction merely, *back-sights*; and levels taken in the direction of the other station, *fore-sights*.

Before going on the field with the level, rule three columns, as below, and head them, stations, back-sights, fore-sights.

## FIELD NOTES.

Stations.	+ Back-Sights.	— Fore-Sights.
1	10	3
2	11-6	0
3	6-8	4-9
4	3-9	8-3
Sums . . . . .	31-11 16-00	16-0
Dif. of level. . . . .	<hr/> 15-11	

## EXAMPLE.

*Find the difference of level between any two points, as A and G (Pl. 4, Fig. 5.)*

The level being adjusted, place it at any point, as *B*, as nearly in the line joining *A* and *G* as may be convenient. Place a levelling staff at *A*, and another at *N*, a point lying as near as may be in the direction of *G*. Make the level horizontal, by means of the levelling screws; turn the telescope to the staff at *A*, and direct the person at the staff to slide up the vane until the horizontal line *ab* pierces its centre; then note the distance *Ab* (equal to 10 feet in the present example), and enter it in the column of back-sights, opposite station 1. Sight also to the staff at *N*, and enter the distance *Na*, equal to 3 feet, in the column of fore-sights, opposite station 1.

Take up the level, and place it at some other convenient station, as *C*, and remove the staff at *A*, to *M*. Having levelled the instrument, sight to the staff at *N*, and enter the distance *Nd*, 11 feet 6 inches, in the column of back-sights, opposite station 2: sight also to the staff at *M*, and enter the distance *Mf*, equal 0, in the column of fore-sights, opposite station 2.



Let the level be now removed to any other station, as  $D$ , and the staff at  $N$ , to some other point, as  $P$ . Let the distance  $Mg$ , equal to 6 feet 8 inches, be entered in the column of back-sights, opposite station 3, and the distance  $Ph$ , equal to 4 feet 9 inches, in the column of fore-sights. Let the instrument be now placed at  $E$ , and the distance  $Pm$ , equal to 3 feet 9 inches, and  $Gn$ , equal to 8 feet 3 inches, be entered opposite station 4, in their proper columns.

It is evident from the figure, that the difference of level  $NF$ , between  $A$  and  $N$ , is equal to the back-sight  $bA$ , diminished by the fore-sight  $aN$ ; also that the difference of level between  $N$  and  $M$  is equal to the back-sight  $dN$ , diminished by the foresight  $0$ , and since each set of observations is entirely independent of every other set, we may infer that *the difference of level between two points as determined by one position of the level, is equal to the back-sight, diminished by the fore-sight.* If the fore-sight be greater than the back-sight, the difference will be affected with a *minus* sign, a result which shows that the second point is lower than the first. Generally, *the difference of level between any two points, determined as above, is equal to the sum of the back-sights diminished by the sum of the fore-sights.* If the result is plus, the second point is higher than the first; if negative, it is lower.

In the example given, the difference of level between  $A$  and  $G$ , is 15 feet 11 inches.

15. In the previous example, we did not regard the difference between the true and apparent level. If it be necessary to ascertain the result with extreme accuracy, this difference must be considered: and then, the horizontal distances between the level, at each of its positions, and the staves, must be measured, and the apparent levels diminished by the differences of level; which differences can be found from the table.

THE FOLLOWING IS SUCH AN EXAMPLE.

Stat.	Back-sts.	Distances.	Fore-st.	Distances.	Cor. back-sights	Cor. fore-sts.
1	9-8	20 ch.	1-6	32 ch.	9-7.500	1-4.720
2	8-7	25 ch.	2-4	28 ch.	8-6.219	2-3.019
3	5-2	18 ch.	3-1	16 ch.	5-1.595	3-0.680
4	10-3	29 ch.	1-9	87 ch.	10-1.949	0-11.538
5	11-0	45 ch.	2-5	72 ch.	10-9.469	1-10.520
					44-2.732	9-6.477

In this example, the first column shows the stations; the second, the back-sights; the third, the distances from the level in each of its positions to the back staff; the fourth, the fore-sights; the fifth, the distances from the level to the forward staff; the sixth and seventh, are the columns of back and fore-sights, corrected by the difference of level. The corrections are thus made:—The difference of level in the table corresponding to 20 chains, is 5 tenths of an inch, which being subtracted from 9 feet 8 inches, leaves 9 feet 7.5 inches for the corrected back-sights; this is entered opposite station 1 in the sixth column. The difference of level corresponding to 32 chains, is 1.280 inches, which being subtracted from the apparent level, 1 foot 6 inches, leaves 1 foot 4.720 inches for the true fore-sight from station 1. The other corrections are made in the same manner.

The sum of the back-sights being 44 feet 2.732 inches, and the sum of the fore-sights 9 feet 6.477 inches, it follows, that the difference, 34 feet 8.255 inches, is the true difference of level.

16. In finding the true from the apparent level, we have not regarded the effect caused by refraction on the apparent elevation of objects, as well because the refraction is different in different states of the atmosphere, as because the corrections are inconsiderable in themselves.

17. The small errors that would arise from regarding the apparent as the true level, may be avoided by placing

*the levelling staves at equal distances from the level.* In such case, it is plain, 1st, that equal corrections must be made in the fore and back-sights; and, 2dly, that when the fore and back-sights are diminished equally, the result, which is always the difference of their sums, will not be affected.

This method should always be followed, if practicable, as it avoids the trouble of making corrections for the difference of true and apparent level.

The differences between the true and apparent level, being very inconsiderable for short distances, if only ordinary accuracy be required, it will be unnecessary to make measurements at all. Care, however, ought to be taken, in placing the levelling staves, to have them at as nearly equal distances from the level as can be determined by the eye; and if the distances are unequal, let the next distances also be made unequal; that is, if the back-sight is the longer in the first case, let it be made proportionably shorter in the second, and the reverse.

#### LEVELLING FOR SECTION.

18. Having decided upon the line along which a section is to be taken, let a permanent mark be made at the beginning of the line: this is called a *bench-mark*. A bench-mark is made by drilling a hole in a rock, or by painting upon a rock or fence, or sometimes by driving a stake in the ground, with its upper end marked by a nail-head. Bench-marks should be made from time to time along the line, to serve as checks, in case a re-survey should become necessary.

The operations in the field are similar to those in the last example, and the field notes are kept in the same manner, except that a new column is added for bearings, when it is necessary to make a plot of the line of survey. The total distance of each point above or below the starting point may be computed, and written in a separate column, paying particular attention to the signs. We annex an example, in which the heights are estimated in feet, and decimals of a foot.

Sta- tion.	Distances in feet.	B. Sight.	F. Sight.	Dif. between B. S. and F. S.	Total Dif. of Level.	REMARKS.
1	650	2.35	14.55	- 12.20	- 12.20	Commenced at bench-mark <i>A</i> .
2	700	3.56	9.58	- 6.02	- 18.22	
3	750	10.34	6.21	+ 4.13	- 14.09	
4	650	14.55	0.25	+ 14.30	+ 0.21	
5	600	9.98	1.67	+ 8.31	+ 8.52	
6	650	3.62	14.54	- 10.92	- 2.40	
	B.M	1.23	13.45	- 12.22	- 14.62	Bench-mark on rock.
7	500	2.23	12.05	- 9.82	- 24.44	Terminating at <i>BM</i> on oak tree.
8	750	6.20	19.55	- 13.35	- 37.79	

The fifth column shows the difference of level between any two consecutive positions of the levelling staff, and is found by subtracting the fore-sight from the corresponding back-sight, and giving to the remainder the proper sign. The sixth column shows the distance of each point above or below the bench-mark *A*, and is obtained by continual additions of the numbers in column 5. Thus,  $(-12.20) + (-6.02) = -18.22$ ;  $(-18.22) + 4.13 = -14.09$ ; and so on.

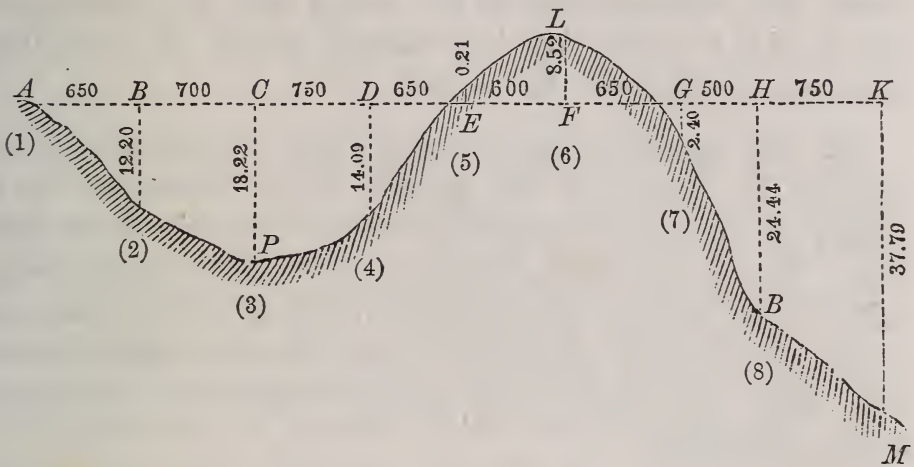
It will be seen that the point of termination is 37.79 feet below the starting point.

#### PLOTTING THE SECTION OR PROFILE.

19. The vertical distances being generally very small as compared with the horizontal distances, two different scales become necessary in plotting a profile. In order that the vertical distances may be fully exhibited in the plan, the scale used for them is much larger than is used for lines measured in a horizontal direction. This becomes absolutely necessary where long lines of profile, with a gentle slope, are to be plotted, as is always the case in the trial section of a railroad survey. We shall illustrate the manner of plotting, by drawing the section determined by the field-notes just given.

20. Draw a horizontal line *AK*, called a *datum* line, and

assume some point as *A*, to represent the point of beginning: lay off on the datum line, distances equal to the



measured distances 650, 700, 750, &c., feet to *K*, using in this case a scale of 1500 feet to 1 inch. At the points *B*, *C*, *D*, *E*, &c., thus determined, erect perpendiculars, making them equal, on a scale of 25 feet to the inch, to the corresponding differences of level taken from the field-book; through the points thus found, draw the irregular line *APLM*, and it will represent the surface of the ground along the line of level.

The bench-mark, between stations 7 and 8, is not plotted, as it is supposed to be out of the line of the section, and no distances are measured to it.

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## SECTION II.

### TOPOGRAPHICAL SURVEYING.

21. Besides the surveys that are made to determine the area of land and the relative positions of objects, it is frequently necessary to make minute and careful examinations for the purpose of ascertaining the form and accidents of the ground, and to make such a plan as will distinguish the swelling hill from the sunken valley, and the course of the rivulet from the unbroken plain.

22. This branch of surveying is called Topography. In surveys made with a view to the location of extensive works, the determination of the slopes and irregularities of the ground is of the first importance: indeed, the examinations would otherwise be useless.

23. The manner of ascertaining these irregularities is, to suppose the surface of the ground to be intersected by a system of horizontal planes at equal distances from each other; the curves determined by these secant planes, being lines of the surface, will indicate its form at the places of section, and, as the planes are nearer or more distant from each other, the form of the surface is more or less accurately ascertained.

If such a system of curves be determined, and then projected or let fall on a horizontal plane, it is obvious that the curves on such plane will be nearer together or farther apart, as the ascent of the hill is steep or gentle.

If, therefore, such intersections be made, and the curves so determined be accurately delineated on paper, the map will give such a representation of the ground as will show its form, its inequalities, and its striking characteristics.

24. The subject divides itself, naturally, into two parts.

1st. To make the necessary examinations and measurements on the field; and,

2d. To make the delineations on paper:

For the former of these objects, the theodolite is the best instrument; the common level, however, will answer all the purposes, though it is less convenient.

Before going on the field, it is necessary to provide a number of wooden stakes, about two feet in length, with heads. These stakes are used to designate particular points, and are to be driven to the surface of the ground. A nail should then be driven into the head of each of them, to mark its centre.

25. We shall, perhaps, be best understood, by giving an example or two, and then adding such general remarks as

will extend the particular cases to all others that can occur.

Let  $A$  (Pl. 4, Fig. 6), be the summit of a hill, the contour of which it is required to represent. At  $A$ , let a stake be driven, and let the axis of the theodolite, or level, be placed directly over the nail which marks its centre. From  $A$ , measure any line down the hill, as  $AB$ , using the telescope of the theodolite or level to arrange all its points in the same vertical plane. Great care must be taken to keep the measuring chain horizontal, for it is the *horizontal distances* that are required. At different points of this line, as  $a, b, c, d$ , &c., let stakes be driven, and let the horizontal distances  $Aa, ab, bc$ , and  $cd$ , be carefully measured. In placing the stakes, reference must be had to the abruptness of the declivity, and the accuracy with which the surface is to be delineated: their differences of level ought not to exceed once and a half, or twice, the distance between the horizontal planes of section.

Having placed stakes, and measured all the distances along the line  $AB$ , run another line down the hill, as  $AC$ , placing stakes at the points  $e, f, g$ , and  $h$ , and measuring the horizontal distances  $Ae, ef, fg$ , and  $gh$ . Run also the line  $AD$ , placing stakes at  $i, l, m$ , and  $n$ , and measuring the horizontal distances  $Ai, il, lm$ , and  $mn$ .

Each line,  $AB, AC, AD$ , running down the hill from  $A$ , may be regarded as the intersection of the hill by a vertical plane; and these secant planes are to be continued over all the ground which is to be surveyed. If the work is done with a theodolite, or with a level having a compass, the angles  $DAB$  and  $BAC$ , contained by the vertical secant planes, can be measured; if it is done with a level, having no needle, let any of the distances  $ae, bf, ai, bl$ , &c., be measured with the chain, and there will then be known the three sides of the triangles  $Aae, Abf, Aai, Abl$ , &c.

Let now, the difference of level of the several points marked in each of the lines  $AB, AD, AC$ , be determined.

In the present example the results of the measurements and levelling, are—

Line  $AB$ .

Distances.	Difference of Level.
$Aa = 40$ feet	$A$ above $a$ 12 feet
$ab = 50$ "	$a$ above $b$ 8 "
$bc = 30$ "	$b$ above $c$ 9 "
$cd = 46$ "	$c$ above $d$ 11 "

Line  $AC$ .

Distances.	Difference of Level.
$Ae = 28$ feet	$A$ above $e$ 11 feet
$ef = 45$ "	$e$ above $f$ 9 "
$fg = 55$ "	$f$ above $g$ 12 "
$gh = 49$ "	$g$ above $h$ 14 "

Line  $AD$ .

Distances.	Difference of Level.
$Ai = 25$ feet	$A$ above $i$ 9 feet
$il = 55$ "	$i$ above $l$ 13 "
$lm = 38$ "	$l$ above $m$ 7 "
$mn = 48$ "	$m$ above $n$ 14 "

Angle  $CAB = 25^\circ$ , Angle  $DAB = 30^\circ$ .

These data are sufficient, not only to find the intersections of horizontal planes with the surface of the hill, but also for delineating such curves of section on paper.

Having drawn on the paper the line  $AB$ , lay off the angle  $BAC = 25^\circ$ , and the angle  $BAD = 30^\circ$ . Then, from a convenient scale of equal parts, lay off the distances  $Aa$ ,  $ab$ ,  $bc$ ,  $cd$ ,  $Ae$ ,  $ef$ ,  $fg$ ,  $gh$ ,  $Ai$ ,  $il$ ,  $lm$ , and  $mn$ .

Let it be required that the horizontal planes be at a distance of eight feet from each other. Since  $A$  is the highest point of the hill, and the difference of level of the points  $A$  and  $a$ , is 12 feet, the first plane, reckoning downwards, will intersect the line traced on the ground from  $A$  to  $B$ , between  $A$  and  $a$ . Regarding the descent as uniform, which we may do for small distances without sensible error, we have this proportion; as the difference of level of the points  $A$  and  $a$ , is to the horizontal distance  $Aa$ , so is 8 feet, to the horizontal distance from  $A$  to where the first



horizontal plane will cut the line from  $A$  to  $B$ . This distance being thus found, and laid off from  $A$  to  $a$ , gives  $a$ , a point of the curve in which the first plane intersects the ground. The points at which it cuts the line from  $A$  to  $C$ , and the line from  $A$  to  $D$ , are determined similarly, and three points in the first curve are thus found.

The graphic operations are greatly facilitated by the aid of the sector. Let it be borne in mind, that the descent from  $A$  to  $a$ , is 12 feet, and that it is required, upon the supposition of the descent being uniform, to find that part of the distance corresponding to a descent of 8 feet. Take the distance from  $A$  to  $a$ , in the dividers, and open the arms of the sector until the dividers will reach from 12 on the line of equal parts, on one side, to 12 on the line of equal parts, on the other. Then, without changing the angle, extend the dividers from 8 on one side, to 8 on the other; this will give the proportional distance to be laid off from  $A$  to  $a$ . Or, if the dividers be extended from 4 to 4, the proportional distance may be laid off from  $a$  to  $a$ .

If the distances to be taken from the sector fall too near the joint, let multiples of them be used; as for instance, on the French sectors, let the arms be extended until the dividers reach from 120 on the one, to 120 on the other, then 80 or 40 will be the proportional numbers. Other multiples may be used, though it is generally more convenient to multiply by 10.

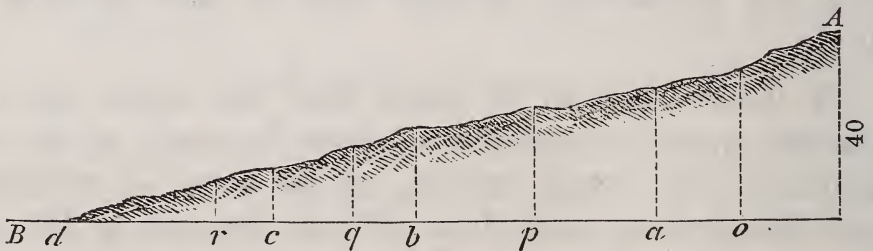
26. The second plane is to pass 8 feet below the first, that is, 16 feet below  $A$ , or 4 feet below  $a$ ,  $a$  being 12 feet below  $A$ . Take the distance  $ab$  in the dividers, and extend the sector, so that the dividers will reach from 8 to (the descent from  $a$  to  $b$  being 8 feet) 8, or from 80 to 80; then, the distance from 4 to 4, or from 40 to 40, being laid off from  $a$  to  $p$ , gives  $p$ , a point of the second curve.

The difference of level between  $a$  and  $b$  being 8 feet, and the difference of level between  $a$  and  $p$  being 4 feet, the difference of level between  $p$  and  $b$  must also be 4 feet; hence, the third plane will pass 4 feet below  $b$ , and

$q$ , determined as above, is a point of the third curve, and so on. After having determined the points in which each contour line cuts the lines diverging from  $A$ , let the contour lines be drawn through them, so as to indicate the surface of the hill. The numbers (8), (16), &c., show the vertical distances of the respective planes below the point  $A$ .

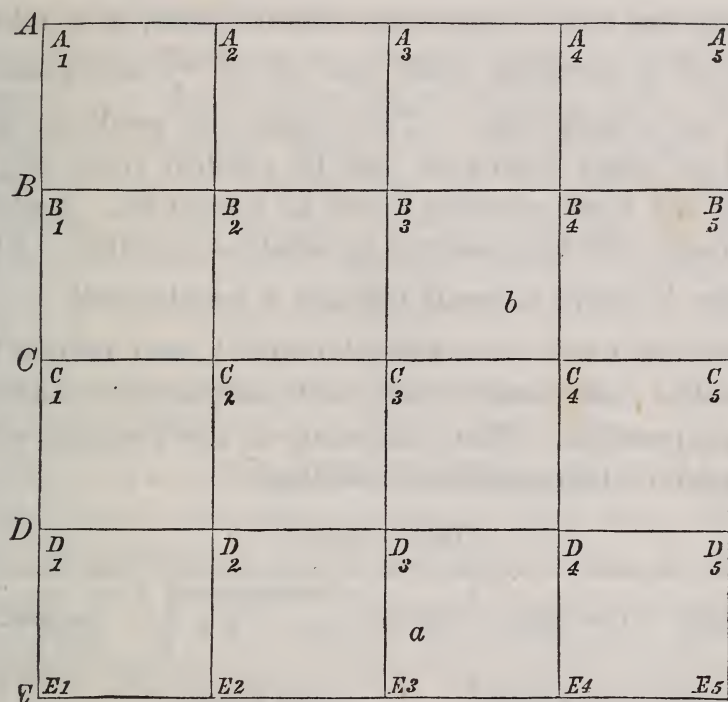
27. Having drawn the horizontal curves, the next thing to be done is so to shade the drawing that it may represent accurately the surface of the ground. This is done by drawing a system of small broken lines, as in the figure, perpendicular in direction to the horizontal curves already described. In all topographical representations of undulating ground, the lines of shading are drawn perpendicular to the horizontal curves.

A profile along either of the diverging lines may be plotted by the rules already given (Art. 20.) The diagram shows the profile along the line  $AB$ .



28. The following example will illustrate the methods employed in making a topographical survey, where great accuracy is required.

By means of a theodolite or level, range a line of stakes  $A, B, C, D, E$ , &c., along one side, or through the middle of the ground to be surveyed, at equal and convenient distances from each other, say 50 feet apart. Mark, with a piece of red chalk, on each stake in this row, one of the letters of the alphabet,  $A, B, C, D, E$ , &c., in their order. At  $A$ , range a line of stakes, perpendicular to  $AE$ , planting the stakes at intervals of 50 feet; and mark them with the letters  $A_1, A_2, A_3$ , &c., which are read  $A$  first,  $A$  second,  $A$  third, &c.



At *B*, range a line of stakes also perpendicular to *AE*, and at distances of 50 feet from each other, and designate them  $\frac{1}{1}$ ,  $\frac{1}{2}$ ,  $\frac{1}{3}$ , &c. Do the same at *C*, *D*, *E*, &c., until all the stakes are placed, dividing the area to be surveyed into squares of 50 feet on a side. The letters and figures should be plainly marked on a smooth face of each stake, for facility of reference. If this system of notation be followed, the stakes may be recorded without danger of confusion.

The next operation is to determine the difference of level between each stake, and some fixed horizontal plane, which is called a *plane of reference*. If the sea is near, the plane of mean low water, may be taken as the plane of reference. If not, assume the horizontal plane, passing through the lowest point of the ground to be surveyed, and make a permanent bench-mark at the point of beginning. If the lowest point cannot be easily determined, assume such a plane of reference as shall pass quite below the lowest point of the ground.

In the example, which we have taken for illustration, the stake  $\frac{1}{3}$  is at the lowest point, and let us assume the plane of reference to pass through that point.



If we subtract the first fore-sight (D3), from the back-sight (E3), the difference, entered in the column headed *difference*, is evidently the height of (D3), above the plane of reference through (E3); and we accordingly enter it under the column headed *total diff. of level*, as well as in the column of differences. If we subtract the fore-sight (C4) from the fore-sight (D3), the difference, entered in the column of difference, is evidently the height of (C4) above (D3); if we now add this difference to the previous total, we shall find the height of (C4) above (E3). Subtracting the fore-sight (E2) from the back-sight (C4), we get the difference of level between (E2) and (C4) which, added to the previous total, gives the height of (E2), above the stake (E3). In subtracting the fore-sight (E4) from the fore-sight (E2), we find a negative result which shows that (E4) is below (E2). We enter, then, this difference with its negative sign, and to get the total, we subtract this difference from the previous total, and so on.

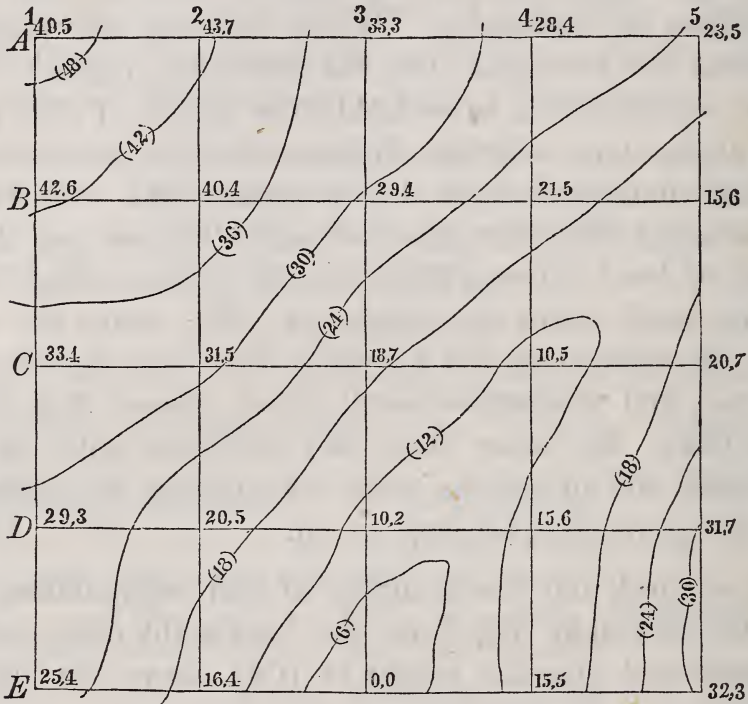
As a check on the accuracy of our computation, subtract the fore-sight (C4) from the back-sight (E3), and the difference will give the height of (C4), above the plane of reference.

Again, subtract the fore-sight (B4) from the back-sight (C4), and add the remainder to the height of (C4), and we shall find the height of (B4), which should agree with the height found under the heading, *total diff. of level*; and so on for each time the level is moved.

#### PLOTTING THE WORK.

29. Draw, on a piece of paper, a straight line  $AE$ . From a scale of equal parts, set off distances  $AB$ ,  $BC$ , &c., each to represent 50 feet. Erect perpendiculars at each of the points  $A$ ,  $B$ ,  $C$ , &c., and then set off the distances from  $A$  to 2, from 2 to 3, &c., each to represent 50 feet; and through the points 2, 3, 4 and 5, draw parallels to  $AE$ . These, by their intersections with the lines drawn through  $A$ ,  $B$ ,  $C$ , &c., will determine the position of the stakes,  $A_1$ ,  $A_2$ , &c.; and write in red ink on the plot, the

height above the plane of reference of each stake, taken from the column of total differences in the field-book. Let us suppose that the horizontal planes are to be taken at distances of 6 feet. We may find the points in which the contour



lines intersect the lines at right angles, by the previous method, or perhaps still better, let the Surveyor take the plot thus commenced into the field, and by the eye trace the contour lines on the map. If we note where the lines at right angles cut fences, roads, streams, &c., we can, by joining the points, obtain a plot of the ground.

30. The contour lines may be found as follows: Set up the level at *a*, and observe that the back-sight, to the stake, placed at (*E3*), gave a reading of 11.432. Depress the vane equal to the distance between the horizontal secant planes, that is, 6 feet, which is done by placing it at the reading 5.432. Then direct the rodman, by signals up or down the hill, till the horizontal hair of the telescope coincides with the horizontal line of the vane. The foot of the staff is then 6 feet above the first point. Let a stake, marked 6, be driven here, and direct the rodman around the hill, until a second position shall be found, when the

horizontal hair of the telescope will cut the vane, and drive there another stake, marked 6; and so on, until a sufficient number of stakes have been driven to determine the curve (6). Then, let the line of stakes, marked 6, be surveyed with the compass and chain, and plotted. Other contour lines may be found in a similar manner.

31. We will add another example for determining the contour of an undulating piece of ground (Pl. 4, Fig. 7,) by means of horizontal sections. Let rows of stakes *DA, HE, IF, &c.*, be driven at intervals, depending upon the required accuracy of the survey, and let *f, g, h, &c.*, be stakes driven along the lines, at such points as will best show the accidents of ground. Determine as before the difference of level between each stake, and some fixed point, and then determine where the contour lines cut the lines *AD, EH, &c.*, by the rules already laid down.

After the stakes are all placed, and the distances measured, let the differences of level of all the points so designated be found. In the present example, the results of the measurements are,

	Ft.	Ft.	Ft.	Ft.	Ft.
<i>Aa</i> = 80	<i>AE</i> = 100	<i>EF</i> = 100	<i>FG</i> = 100	<i>GB</i> = 100	
<i>ab</i> = 60	<i>Ef</i> = 105	<i>Fi</i> = 74	<i>Gm</i> = 96	<i>Bq</i> = 76	
<i>bc</i> = 90	<i>fg</i> = 85	<i>ik</i> = 115	<i>mn</i> = 76	<i>qs</i> = 85	
<i>cd</i> = 55	<i>gh</i> = 71	<i>kl</i> = 60	<i>np</i> = 76	<i>st</i> = 127	
<i>dD</i> = 50	<i>hH</i> = 74	<i>lI</i> = 86	<i>pL</i> = 87	<i>tC</i> = 47	

Of the Levelling.

Line <i>AD.</i>	Line <i>EH.</i>	Line <i>FI.</i>	Line <i>GL.</i>	Line <i>BC.</i>
Ft.	Ft.	Ft.	Ft.	Ft.
<i>A</i> above <i>a</i> 5	<i>E</i> below <i>A</i> 3	<i>F</i> below <i>E</i> 2	<i>G</i> below <i>F</i> 1	<i>B</i> below <i>G</i> 2
<i>a</i> " <i>b</i> 6	<i>E</i> above <i>f</i> 9	<i>F</i> above <i>i</i> 3	<i>G</i> above <i>m</i> 2	<i>B</i> above <i>q</i> 3
<i>b</i> " <i>c</i> 7	<i>f</i> " <i>g</i> 3	<i>i</i> " <i>k</i> 5	<i>m</i> " <i>n</i> 1	<i>q</i> " <i>s</i> 2
<i>c</i> below <i>d</i> 2	<i>g</i> " <i>h</i> 1	<i>k</i> " <i>l</i> 2	<i>n</i> " <i>p</i> 2	<i>s</i> " <i>t</i> 3
<i>d</i> above <i>D</i> 4	<i>h</i> below <i>H</i> 3	<i>l</i> below <i>I</i> 3	<i>p</i> below <i>L</i> 4	<i>t</i> below <i>C</i> 5

The heights of the points are here compared with each other, two and two. Before, however, we can conceive

clearly their relative heights, we must assume some one point, and compare all the others with it. Let the point *A* be taken. The height of

	Ft.		Ft.		Ft.		Ft.
<i>A</i> above <i>a</i>	5	<i>A</i> above <i>f</i>	12	<i>A</i> above <i>k</i>	13	<i>A</i> above <i>p</i>	11
<i>A</i> " <i>b</i>	11	<i>A</i> " <i>g</i>	15	<i>A</i> " <i>l</i>	15	<i>A</i> " <i>L</i>	7
<i>A</i> " <i>c</i>	18	<i>A</i> " <i>h</i>	16	<i>A</i> " <i>I</i>	12	<i>A</i> " <i>B</i>	8
<i>A</i> " <i>d</i>	16	<i>A</i> " <i>H</i>	13	<i>A</i> " <i>G</i>	6	<i>A</i> " <i>q</i>	11
<i>A</i> " <i>D</i>	20	<i>A</i> " <i>F</i>	5	<i>A</i> " <i>m</i>	8	<i>A</i> " <i>s</i>	13
<i>A</i> " <i>E</i>	3	<i>A</i> " <i>i</i>	8	<i>A</i> " <i>n</i>	9	<i>A</i> " <i>t</i>	16

And of *A* above *C*, 11 feet.

This being done, a mere inspection shows us the highest and lowest points, as also the relative heights of the others, reckoning upwards or downwards. Let them be now written in the order of their heights above the lowest point, which is *D*. The difference of level between *A* and *D* being 20 feet, if the difference of level of each of the points below *A*, be taken from 20 feet, the remainder will be the height above *D*. Arranging them in their order, we have

	Ft.		Ft.		Ft.		Ft.
<i>c</i> above <i>D</i>	2	<i>H</i> above <i>D</i>	7	<i>p</i> above <i>D</i>	9	<i>B</i> above <i>D</i>	12
<i>d</i> " <i>D</i>	4	<i>k</i> " <i>D</i>	7	<i>q</i> " <i>D</i>	9	<i>L</i> " <i>D</i>	13
<i>h</i> " <i>D</i>	4	<i>s</i> " <i>D</i>	7	<i>C</i> " <i>D</i>	9	<i>G</i> " <i>D</i>	14
<i>t</i> " <i>D</i>	4	<i>f</i> " <i>D</i>	8	<i>n</i> " <i>D</i>	11	<i>a</i> " <i>D</i>	15
<i>g</i> " <i>D</i>	5	<i>I</i> " <i>D</i>	8	<i>i</i> " <i>D</i>	12	<i>F</i> " <i>D</i>	15
<i>l</i> " <i>D</i>	5	<i>b</i> " <i>D</i>	9	<i>m</i> " <i>D</i>	12	<i>E</i> " <i>D</i>	17

*A* above *D*, 20 feet.

In this example, the plane of reference is assumed through *D*, the lowest point of the ground; and the secant planes are taken 3 feet apart.

32. The manner of shading the map, so as to indicate the hills and slopes, consists in drawing the lines of shading perpendicular to the horizontal curves, as already explained. These shading lines are drawn close together, when the slope is abrupt, and further apart, as it grows more gentle. Fig. 7 indicates the method of shading.



33. When the plane of reference is so chosen that the points of the work fall on different sides of it, all the references on one side are called positive, and those on the other, negative. The curves having a negative reference are distinguished by placing the minus sign before the number; thus — ( ).

34. In topographical surveys, great care should be taken to leave some *permanent marks*, with their levels written on them in a durable manner. For example, if there are any rocks, let one or more of them be smoothed, and the vertical distance from the plane of reference marked thereon: or let the vertical distance of a point on some prominent building, be ascertained and marked permanently on the building. Such points should also be noted on the map, so that a person, although unacquainted with the ground, could by means of the map, go upon it, and trace out all the points, together with their differences of level.

35. Besides representing the contour of the ground, it is often necessary to make a map which shall indicate the cultivated field, the woodland, the marsh, and the winding river. For this, certain characters, or conventional signs, have been agreed upon, as the representatives of things, and when these are once fixed in the mind, they readily suggest the objects for which they stand. Those which are given in Plates 5 and 6, have been adopted by the Engineer Department, and are used in all plans and maps made by the United States Engineers.

It is very desirable that a uniform method of delineation should be adopted, and none would seem to be of higher authority than that established by the Topographical Bureau. It is, therefore, recommended, that the conventional signs given in Plates 5 and 6, be carefully studied and uniformly followed.

# B O O K I V .

## GEODESIC, TRIGONOMETRIC AND MARITIME SURVEYING.

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### SECTION I.

#### GEODESIC AND TRIGONOMETRIC SURVEYING.

1. WHEN a large extent of territory, or a long line of sea-coast is to be surveyed, it becomes necessary to consider the curvature of the earth's surface; this branch of surveying is called *Geodesic* surveying.

2. Extensive geodesic operations prove that the earth is an oblate spheroid, the shortest diameter of which coincides with the terrestrial axis, and all of whose meridians, are equal ellipses. The meridian lines, however, differ so little from the circumferences of circles, that they may be taken for them, except when great accuracy is required. The earth, will, therefore, in the following pages, be regarded as a perfect sphere.

3. The operations necessary to the successful execution of a Geodesic Survey, require the minutest attention, and when performed, numerous corrections are to be applied to the measured lines and angles, on account of the various causes of error incident to such operations.

To investigate those causes of error, and to deduce rules for correcting the errors, in all cases, would far exceed the limits of an elementary treatise. We shall, therefore, attempt nothing more than a brief outline of the operations

of a trigonometric survey, with the application of some of the more important corrections.

4. It may be observed that most of the operations described in this section, are equally applicable, whether we regard the area surveyed as plane or spherical: in either case, the basis of an accurate survey, is an extensive system of triangulation.

5. After having made a preliminary examination or *reconnaissance* of the territory to be surveyed, suitable stations are selected at the most prominent points, and these points are marked by *staves* or *signals*.

A *base line* is then measured. The length of the base will, in general, depend upon the magnitude of the survey, and each extremity is marked by a signal.

The next step is the *triangulation*. At each extremity of the base, the angles between the base, and the lines drawn to each of the visible signals, are carefully measured by means of a theodolite. The sides of the triangles thus obtained, serve as new bases upon which other triangles may be formed, and so on, until the entire area is covered by a net-work of triangles.

6. This system of triangles is called the *primary* system, and the operation of forming them is called the *primary triangulation*. Within the primary triangles, and depending upon them, a system of smaller triangles is formed in the same manner, called the *secondary system*; and if the extent or importance of the work should demand it, the secondary may be sub-divided into *tertiary triangles*.

Having completed the triangulation, the characteristics of the surface, such as roads, streams, villages, boundaries, &c., are filled in by means of the compass, plain table, or some of the methods already explained.

After the field work is completed, the triangles, when regarded as spherical, are reduced by applying the formula for *spherical excess*, hereafter explained, and other necessary corrections, and thus the whole work is plotted upon paper.

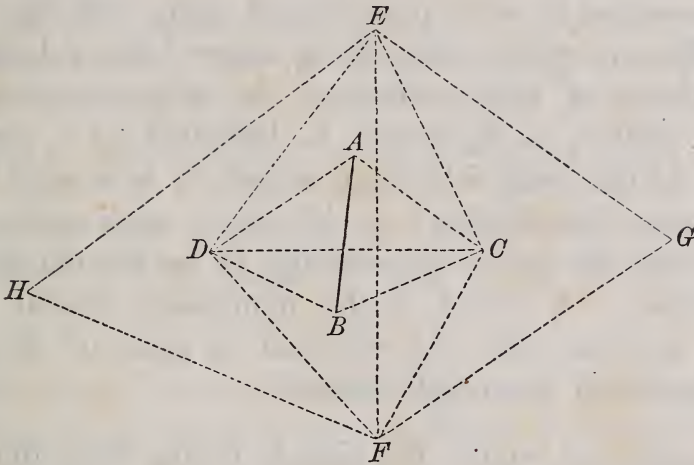
## PRELIMINARY RECONNOISSANCE AND ESTABLISHMENT OF SIGNALS.

7. Before commencing a trigonometrical survey, an examination of the entire territory should be made for the purpose of selecting a location for the base line, and proper points for stations; this examination should be more or less elaborate, according to the nature and extent of the survey.

The proper distribution and combination of the triangles, so as to adapt them to the survey in hand, require great judgment and care, and but few rules can be given for the selection of trigonometrical points. Those points should, in general, be chosen in such a manner, that they may be distinctly visible from each other, and so that the triangles formed, by uniting them, may be as nearly as possible equilateral.

It is easily seen, that a triangle which has an obtuse or a very acute angle, will experience a greater change of form for a given error, than one which is nearly equilateral; and since the accuracy of each triangle depends upon the preceding ones, it is further evident, that the introduction of a single ill-conditioned triangle, might vitiate the whole survey. Except in extreme cases, no angle, less than  $30^\circ$ , should be used, and even angles of  $30^\circ$  should not be admitted when the locality can be so chosen as to prevent it. The base is usually much shorter than the sides of the primary triangles; these sides, however, should be increased as rapidly as is consistent with the above remarks.

8. The accompanying diagram will illustrate the manner of increasing the sides without introducing ill-conditioned triangles. Having measured the base  $AB$ , and the requisite angles, the triangles  $ABC$  and  $ABD$ , may be determined, and the line  $DC$  computed; with  $DC$  as a base, the triangles  $DCE$  and  $DCF$  are formed, and thence  $EHF$ , and  $EGF$ , in which the sides are much greater than the base  $AB$ .

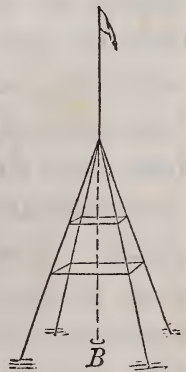


In this manner the sides may be increased to any desirable extent. An ordinary map of the country, or a sketch made with the pocket compass, will be of material assistance in making a proper distribution of the *stations*.

9. The stations are marked by signals, which may be constructed in a great variety of ways, depending upon the locality of the stations, and the lengths of the sides of the triangles.

Sometimes a signal has to be raised above the level of the adjacent country, in which case it is constructed of timbers, and upon the apex, is placed a vertical staff, bearing a flag. The exact trigonometrical point is determined by a plumb-line, suspended from the apex of the signal.

A temporary signal may be constructed with three or four pieces of scantling framed and traced, as shown in the annexed figure, with a short pole projecting from the apex. The plumb determines the point *B*, which is the exact trigonometrical point over which the theodolite is to be placed. Where the sides of the triangles are not very great, a pole, planted vertically, and surmounted by a flag, will answer as a signal.



In order to distinguish the different signals, the flags which they bear, should be different from each other. They may be formed by arranging stripes of white and

red, according to some pre-arranged plan, and the flags of the different stations should be entered in a book. For the purpose of future reference, the trigonometrical point, at each station, as *B*, should be indicated by a permanent mark. If the point falls upon a rock, a hole may be drilled to show the locality; or if not, a mark-stone may be sunk under the point, deep enough to be beyond the reach of accident. A record of the monument should be preserved, together with its reference to some of the permanent objects in the neighborhood.

In order to render the signals visible from the distant stations, polished tin plates are sometimes attached to the signal-post, so as to reflect the sun towards the stations at certain hours of the day. The Drummond-light has also been used to show very distant stations. A light may also be produced that can be seen at a distance of 60 or 70 miles, by placing a ball of lime about a quarter of an inch in diameter, in the focus of a parabolic reflector, and heating it intensely by a stream of oxygen gas, directed by a blow-pipe, through a flame of alcohol. If obstacles, as trees, and under-brush intervene, vistas have to be opened along the lines, from station to station.

#### MEASUREMENT OF A BASE LINE.

10. The measurement of a base line on which the accuracy of the entire survey depends, is one of the most difficult operations of geodesic surveying, and one, for the successful accomplishment of which, art and science have been strongly taxed. The selection of a proper site for a base line, forms one of the first objects of the preliminary reconnaissance. It should, if possible, be fixed on an open plain. It must be so chosen, that the surrounding signals may be distinctly seen from its extreme points; and hence, those signals which mark points of the adjacent triangulation, should be selected with reference to the base. The length of the *base*, should, in a measure, depend upon the magnitude of the survey, though circumstances seldom admit its being taken more than 6 or 8 miles in length.

11. Different instruments have been used for measuring base lines, such as steel chains, glass, platinum and deal rods; and more recently, a combination of rods, of different metals, so adjusted, that the apparatus maintains an invariable length at all temperatures. This last mentioned apparatus, has been much improved, and most successfully used by Prof. Bache, in the Survey of the United States Coast.

12. In minor surveys, where the base line does not much exceed 1000 or 2000 feet, sufficient accuracy may be attained by the use of wooden rods. To render the rods less susceptible of change, from moisture, they should be saturated with boiling oil, and covered with a thick coating of varnish.

The ends of the rods should be protected by metallic caps, which prevent their wearing, and insure a more perfect contact.

When the rods are prepared for use, they should be carefully compared with some standard measure, and from time to time this comparison should be repeated, in order to detect any minute change of length, should such change take place.

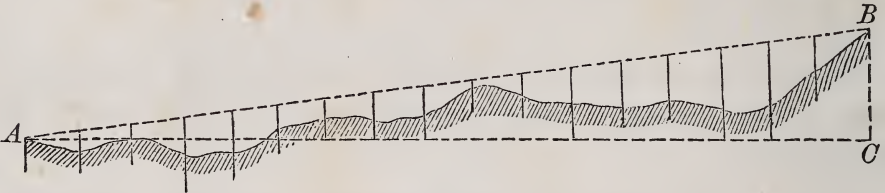
13. The following method of measuring a *base* line of 1000 or 2000 feet, may be rendered very accurate.

Having decided upon the direction of the base, and measured it carefully, two or three times with a chain, let a theodolite be planted at one end of the line, and directed upon a flag, planted at the other. Then, by means of the vertical limb, let a row of pickets be driven along the base, taking care to plant them at a distance from each other, equal to the length of one of the deal rods. Then, plant in the place of each picket, a vertical post, 6 or 8 inches in diameter, and projecting a sufficient distance above the surface of the ground. If necessary, let the posts be steadied by heaping about them, earth or stones. Next, with the assistance of a spirit-level, let each post be sawed off, so as to bring their tops to the same horizontal

plane, and by means of the theodolite, let a line be marked on the top of each post, in the direction of the base. This line will determine the direction in which the rods are to be placed, and the contact of the ends must all be on this line.

The contact of the rods should be made with great care, so as to avoid moving the rod already established; and this will be more readily done, when three rods are used. The measurement should be repeated two or three times to guard against error.

14. If the nature of the ground does not admit of the posts being brought to a level, let them, by means of the theodolite, be brought into an oblique plane  $AB$ , and after



having measured, as before, the line  $AB$ , determine accurately the difference of level between the points  $A$  and  $B$ , equal to  $BC$ : then, from the right-angled triangle  $ABC$ , we should find the horizontal distance  $AC = \sqrt{AB^2 - BC^2}$ .

15. In very extensive surveys, the base should be several miles in length, and the apparatus for measurement, as well as the operations on the field, become more complicated. For a full description of a very perfect *base* apparatus, and the method of using it, the reader is referred to Prof. Bache's pamphlet, on the subject—the details of the description would exceed our limits.

#### TRIANGULATION.

16. The theodolite is generally used for measuring the angles of a trigonometric survey. The extent of the survey, and the standard of accuracy to which the results are required to conform, must determine the size and perfection of the instrument to be employed. The angles of the primary triangles of the United States Coast Survey, are measured with theodolites, whose horizontal circles are 24 or 30



inches in diameter; and to eliminate as much as possible, every source of error, great numbers of operations are made on each station, the readings being made on different points of the arc. Usually from 40 to 60 observations are made for each angle—one measurement, with the telescope direct, and one with it reverted, constituting a complete observation. With these precautions, it has been found that the error in a primary triangle (where the sum of its three angles has been compared with  $180^\circ$ ), has fallen much within 3 seconds. The error of 3 seconds has been adopted as the highest admissible limit of error.

17. Observations are also made at the principal stations upon the pole-star, and other stars near the pole, for the purpose of determining the angle, made by the sides of the triangle with the meridian. In minor surveys, and in a secondary triangulation, the operations are much less elaborate; still, every precaution is to be taken to insure the greatest attainable accuracy. As a general rule, all the angles of every triangle, should be measured, if possible.

18. To illustrate the manner of carrying on a minor triangulation, let us refer to the plan of the harbor [plate 6], in which  $AB$  is the measured base,  $C, D, E,$  &c., triangulation points, at which signals have been erected. Commence the triangulation at  $A$ , the west end of the base; and for convenience in plotting, it would be well to make the line, passing through the 0 point, and  $180^\circ$  parallel, in each position of the instrument, to the base  $AB$ . Having brought the 0 of the vernier to the 0 of the limb, clamp the vernier plate, and direct the upper telescope to the signal at  $B$ , and clamp the limb. Enter the observation as in the following table:

OBSERVATION AT STATION  $A$ .

Name of Station.	Vernier I.	Vernier II.	Mean.
Station B	$00^\circ 00' 00''$	$00' 00''$	$00^\circ 00' 00''$
Station E	$72^\circ 24' 55''$	$25' 5''$	$72^\circ 25' 00'$
Station G	$138^\circ 34' 56''$	$35' 4''$	$138^\circ 35' 00''$
&c.	&c.	&c.	&c.

Having recorded the reading of the first vernier, and the minutes and seconds of the second vernier, unclamp the vernier plate, and direct the telescope to the station at  $E$ , and record both verniers, as before. Again unclamp the vernier plate, and direct the telescope on the signal at  $G$ ; and then read and record, as before.

Having determined the angles subtended by all the signals visible from  $A$ , let the theodolite be removed to  $B$ . Bring the 0 of the vernier I to  $180^\circ$  on the limb, and direct the telescope on the signal at  $A$ —the line ( $0^\circ$ ,  $180^\circ$ ) will then be parallel to its first position, and the limb may be clamped. Read now the angles to the signals at  $A$ ,  $E$ ,  $C$ , &c., and record as before.

If the theodolite is now removed to the station  $E$ , the line ( $0^\circ$ ,  $180^\circ$ ), may be made parallel to its first position, by adding  $180^\circ$  to the reading of the first vernier, from  $A$  to  $E$ , and then directing the telescope on the signal at  $A$ . The line ( $0^\circ$ ,  $180^\circ$ ), will thus be made parallel to  $AB$ , and the reading may be made and recorded as before; and so on until all the stations have been visited, and the angles measured. From the field records, the angles  $BAE$ ,  $EAG$ ,  $ABE$ ,  $EBG$ , &c., may be easily deduced, the whole may be plotted on paper, or the several sides may be computed trigonometrically. It may be observed that the line ( $0^\circ$ ,  $180^\circ$ ), has been made parallel to the *base line* at each station; where great accuracy is required, this cannot be done, since a single reading is insufficient to give the angle. The angle is then determined, as directed in the previous article, or by means of the principle of repetition.

19. To illustrate this principle of repetition, suppose the 0 of the vernier to coincide with the 0 of the limb, and the telescope to be directed, from the station  $A$ , upon one of the objects, as the signal at  $B$ . Clamp the limb, and unclamping the vernier plate, direct the telescope on the second object, as the signal at  $E$ . If we now clamp the vernier plate, and unclamping the limb, direct the telescope on the signal at  $B$ , the line ( $0^\circ$ ,  $180^\circ$ ), of the limb, will make with  $AB$ , an angle equal to  $BAE$ . Again clamp the limb,

and unclamping the vernier plate, direct the telescope on the signal at *E*. The reading will evidently be equal to twice the angle *BAE*, and if we repeat the operation, the reading will be three times the angle, and so on. After ten repetitions, if we add  $360^\circ$  each time the 0 of the vernier passes the 0 of the limb, the final reading will be ten times the angle *BAE*, affected with the joint errors of the ten observations, and one-tenth of this will be the reading required, to a greater degree of accuracy than could probably be attained by a single observation.

20. The method of reading angles, by this mode, is as follows:

Angles at station *A*, between signals *B* (left), and *E* (right.)

*June 8th, 1851.*

No. of Repetitions.	Vernier I.	Vernier II.	Mean of Verniers.	
1	72° 24' 55"	25' 5"	72° 25' 00"	
2	144° 49' 55"	50' 0"	144° 49' 58"	
3	217° 14' 50"	15' 10"	217° 15' 00"	
4	289° 39' 50"	40' 00"	289° 39' 55"	
				4)289° 39' 55"
			Mean reading	72° 24' 59"

#### FILLING UP THE SURVEY.

21. After the triangulation is completed, the interior may be filled up by the aid of the Compass, or the plane-table.

#### USE OF THE COMPASS.

22. When the *secondary* and *tertiary* triangles have been considerably multiplied, the compass is taken in hand. The field-notes may be kept in the following manner. Divide a page of the note-book into two equal parts, by two parallel lines near to each other, and consider each part as a separate leaf or page. Each leaf is divided into three

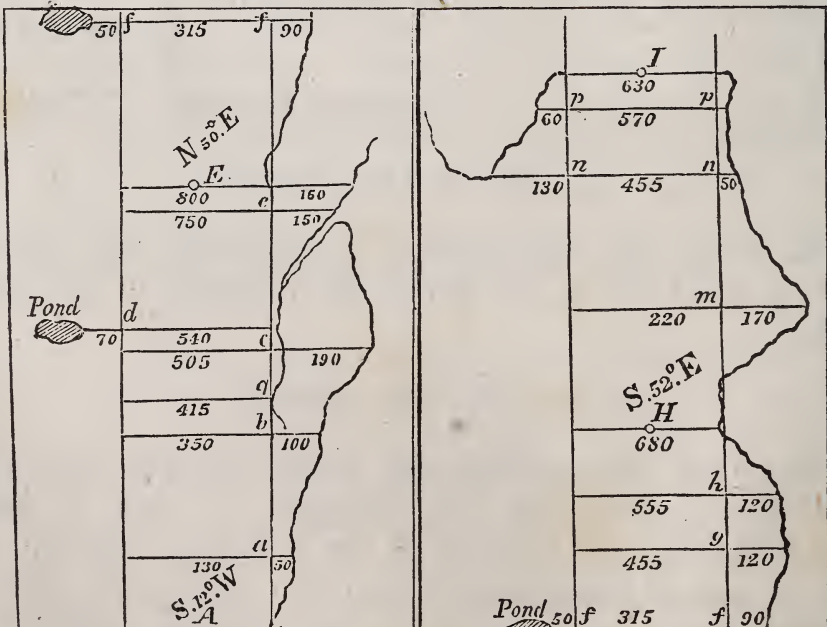
spaces, and the middle space is generally smaller than either of the others, which are equal.

The notes begin at the bottom of the first page, and run up the page to the top. They then commence again at the bottom of the next page, and run up to the top; thence to the bottom of the third page, and thus, for as many pages as the work may require.

When the compass is used in the way we are about to explain, the distances to objects which lie on the right or left of the courses, are determined by means of offsets.

The beginning of every course is designated in the middle column by 0, and the bearing is entered directly above. The other figures of the middle column, express the distances from the beginning of each course to the offsets, and those in the side columns indicate the lengths of the offsets, or the distances to objects on the right or left of the compass lines.

To explain more definitely the manner of using the compass on the field, let us suppose that we have determined the prominent points and longer lines with the theodolite. Place the compass at *A* (Plate 6), and take the bearing of the line *AE*, which is  $S\ 12^\circ\ W$ .



Enter this bearing at *A*. Then measure along the line

$AE$  any distance, as  $Aa$  equal to 130 yards, and make an offset to the lake, which we measure and find to be 50 yards. Enter the 130 in the middle column, and as the lake lies on the right (in going from  $A$  to  $E$ ), we insert the 50 in the right hand column.

We then measure along the line  $AE$  to  $b$ , 350 yards from  $A$ . Here we make a second offset to the lake, and find it to be equal to 100 yards. Having entered the distances in the notes, we measure to  $q$ , the point where the line  $AE$  crosses the creek, and we enter the distance from  $A$ , 415 yards.

At  $d$ , we lay off an offset on the left, to the pond, 70 yards: at  $e$ , an offset to the mouth of the creek, 150 yards: and at  $E$ , where the course terminates, an offset to the lake, of 160 yards. The entire distance from  $A$  to  $E$  is 800 yards.

At  $E$ , we take the bearing to  $H$ , which is  $N\ 50^\circ\ E$ . Having measured along this line to  $f$ , 315 yards, we make an offset to the pond, on the left, of 50 yards, and to the shore, on the right, of 90 yards. Having entered these distances, we recommence the notes at 315 below, which we suppose to be at the bottom of the second page. Having reached  $H$ , the extremity of the course, we enter the entire distance from  $E$ , 680 yards. We next take the bearing to  $I$ ,  $S\ 52^\circ\ E$ . We then measure the distances to  $m$ ,  $n$ ,  $p$ , and  $I$ , and enter them, together with the offsets, as in the notes.

23. It is also well to make, in the columns on the right and left, such sketches of the ground, fields, houses, creeks and rivers, as will afford the means of making an accurate delineation on paper.

#### THE PLANE-TABLE—ITS USES.

24. Pl. 3, Fig. 1. The plane-table consists of two parts; a rectangular board  $CDBA$ , and a tripod  $EHG$ , to which it is firmly secured.

Directly under the rectangular board are four milled screws which pass through sockets inserted in a horizontal

brass plate: these screws are worked against a second horizontal plate, for the purpose of levelling the table; the table having a ball and socket motion, similar to the limb of the theodolite.

For the purpose of levelling the table, a small detached spirit-level is used. This level being placed over the centre, and also over two of the levelling screws, the screws are turned contrary ways until the level is horizontal; after which, it is placed over the other two screws, and made horizontal in the same manner.

Between the upper horizontal plate and the table, there is a clamp-screw, similar to the clamp-screw of the theodolite, which being loosened, the table can be turned freely about its axis. There is, also, a small tangent-screw, by which the smaller motions of the table are regulated, after the clamp-screw is made fast. Neither of these screws can be seen in the figure.

The upper side of the table is bordered by four brass plates, about one inch in width, and the centre of the table is marked by a small pin, *F*. About this centre, and tangent to the sides of the table, conceive a circle to be described. Suppose the circumference of the circle to be divided into degrees and parts of a degree, and radii to be drawn through the centre and the points of division. The points in which these radii intersect the outer edge of the brass border, are marked by lines on the brass plates, and the degrees are numbered in the direction from left to right, from the point *L* to the point *I*,  $180^\circ$ , and from the point *I* to the point *L*,  $180^\circ$ . In some plane-tables, however, they are numbered from 0 to  $360^\circ$ .

There are, generally, diagonal scales of equal parts cut on the plates *DLC* and *AIB*, the use of which will be explained hereafter.

Near the two other edges of the table, two small grooves are made, into which the plates of brass *DB* and *CA* are fitted, and these plates are drawn to their places by means of milled screws, which pass through the table from the under side, and screw firmly into the plates. The heads

of two of the screws,  $Q$  and  $S$ , are seen in the figure, as also one of the plates and its two screws in Fig. 3. The object of these plates is to confine a sheet of paper on the table. By loosening the screws, and pressing them upwards, the plates are raised above the surface of the table; the edges of the paper can then be placed under them: then, by turning the screws back again, the plates are drawn down and the paper held tightly. Fig. 1 represents the table with the paper partly put upon it: one edge of the paper has been placed under the plate  $DB$ , and the screws  $S$  and  $Q$ , tightened. The paper, before being put on, should be moistened, in order to expand it; and then, after it has been dried, it will fit closely to the table.

A ruler,  $AB$  (Fig. 2), with open vertical sights, is used with the plane-table. This ruler has a fiducial edge, which is in the same vertical plane with the hairs of the sights. A ruler with a telescope, and a vertical limb, similar to the vertical limb of the theodolite, is sometimes used with the plane-table. A compass, also, is often attached to the table, to show the bearings of the lines.

The plane-table is used for two distinct objects.

1st. For the measurement of horizontal angles.

2dly. For the determination of the shorter lines of a survey, both in extent and position.

#### TO MEASURE A HORIZONTAL ANGLE.

25. Place, by means of a plumb, the centre of the table directly over the angular point: then level the table; after which, place the fiducial edge of the ruler against the small pin at the centre: direct the sights to one of the objects, and note the degrees on the brass plate; then turn the ruler and sights to the other object, and note the degrees as before. If the ruler has not passed over the 0 point, the difference of the readings is the angle sought; but, if it has, the larger taken from  $180^\circ$ , and the remainder added to the smaller, gives the required angle.

#### TO DETERMINE LINES IN EXTENT AND POSITION.

26. Having placed a paper on the table, examine the

objects and lines which are to be determined, and select for a base a convenient portion of such a line of those already formed in the triangulation, that most of the objects can be seen from its extremities. Then place the plane-table with its centre, nearly, though not accurately, over one extremity of the base; make it truly horizontal, and turn it until the larger part of the paper lies on the same side of the base with the objects.

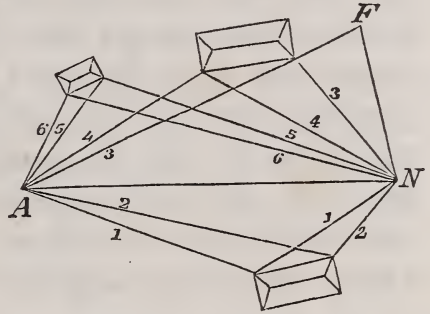
Then, tighten the clamp-screw, and mark with a pin the point of the paper directly over the station, which point is determined most accurately by suspending a plumb from the lower side of the table. Press the pin firmly on this point, bring the fiducial edge of the ruler against it, and sight to the other extremity of the base line, and mark with the pin or pencil, the direction of the line on the paper. Sight in like manner to every other object, and draw on the paper the corresponding lines, numbering them from the base line, 1, 2, 3, 4, &c.

Then, with a pair of dividers, take from the scale a certain number of equal parts to represent the base, and lay off the distance on the base line from the place of the pin. Take up the table, carry it to the other extremity of the base, and place the point of the paper corresponding to that extremity, directly over it. Place the fiducial edge of the ruler on the base line, and turn the table, by means of the tangent-screw, until the sights are directed to the first station. If, however, in bringing the table to this position, the corresponding point of the paper has been moved from over the extremity of the base line, move the legs of the tripod until it is brought back to its place. Let the table be then levelled, after which, place the ruler again on the base line, and bring the table to its proper position by the tangent-screw, and continue the adjustment until the extremity of the base line on the paper is directly over the station, and in the same vertical plane with the base line on the ground. Then direct the sights to all the objects sighted to from the other station, and mark the lines 1, 2, 3, 4, &c., from the base line, as before. The intersections of the corresponding lines 1,1, 2,2, 3,3, 4,4,



&c., determine, on the paper, the positions of the several objects; and a reference of these lines to the scale of equal parts, determines the true distances.

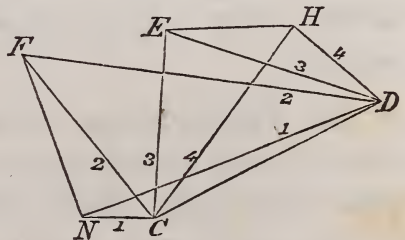
27. Let it be required, for example, to determine, by means of the plane-table, the relative positions of several houses.



From station  $A$ , and on one of the lines of the triangulation, as  $AB$ , measure the base line  $AN$ , which we will suppose equal to 300 yards. Place the plain-table at  $A$ , and sight to the corners of the houses, and mark the lines 1, 2, 3, 4, &c. Then remove the table to  $N$ , and sight to the same corners as before, and draw the lines as in the figure. The points at which they intersect the corresponding lines before drawn, determine the corners of the houses. The front lines of the houses may then be drawn on the paper. Draw lines at right angles to the front lines, and on them lay off the depths of the houses, with the same scale as that used for the base line.

To find the length of any line drawn on the paper, as the line 1, drawn through  $A$ , for example, place the dividers at  $A$  and extend them to the other extremity of the line, and then apply the line to the scale. The length of the line 1 is equal to 198 yards.

28. In this example, we determine from the base line  $CD$ , the positions of the points  $F$ ,  $E$ , and  $H$ .



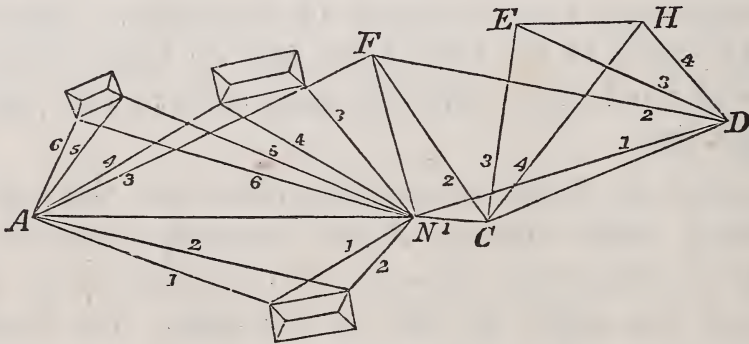
OF CHANGING THE PAPER.

29. When one paper is filled, and there is yet more work to be done, let the paper be removed, and a second paper put on the table; after which, the table may be used as before.

Now, in order that the two papers may be put together and form one entire plan, it is necessary that two points determined on the first paper, be also determined on the second; and then, by placing the lines joining these points, one on the other, all the lines on the two papers will have the same relative position as the corresponding lines on the ground; and the same for as many papers as it may be necessary to use. If different scales are used, the corresponding points will not join, and then the work must be reduced to the same scale, before the papers can be put together.

In the first example, the position of the point  $F$  was determined, in order to unite the first paper with the second.

In the second example, we sighted from  $C$  and  $D$ , the extremities of the base line, to the points  $N$  and  $F$ ; we thus determined the line  $NF$  on the second paper. Placing the line  $NF$  of the one paper on  $NF$  of the other, we have the following plan.



In this plan, all the points and lines are accurately laid down. Any number of papers may be joined in the same manner.

30. The principal use of the plane-table is for the interior filling up of trigonometrical surveys; it is also used with advantage, when only a plot of a field is wanted.

It ought not be used for the determination of long lines, nor can it be relied on for determining extended areas.

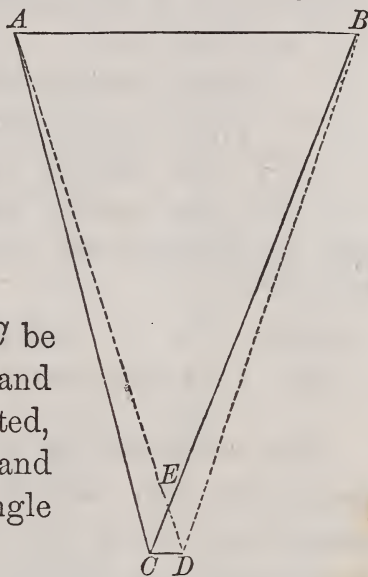
Having finished the field-work, some corrections are necessary, before plotting the survey. The principal corrections are, the reduction to the centre of the station, and the correction for spherical excess.

## REDUCTION TO THE CENTRE.

31. It sometimes happens that fixed objects, as steeples, towers, and the like, are used instead of signals, in a survey. The theodolite cannot be placed over the centre of such stations. In all such cases, the instrument must be planted as near as possible to the station; then the angles, subtended by the various objects being measured, the true angle subtended at the centre of the station, is computed by the following formula.

Suppose  $A$ ,  $B$  and  $C$ , to be the three stations. Let us suppose that the theodolite cannot be placed over  $C$ , but that it can be placed at  $D$ , a point near  $C$ .

Let the angles  $ADB$  and  $ADC$  be measured; also the distance  $CD$ , and the distances  $AC$  and  $BC$  computed, approximately, from the side  $AB$  and the angles  $A$  and  $B$ . The true angle  $ACB$  may then be found.



For,  $AEB = ACB + CAD$  (Geom., Bk. I., Prop. 25, C. 6);  
and  $AEB = ADB + DBC$ ;

hence, by equating the equal values,

$$ACB + CAD = ADB + DBC,$$

or,  $ACB = ADB + DBC - CAD.$

But,  $BC : CD :: \sin BDC : \sin DBC$ ;

or,  $\sin DBC = \frac{CD}{BC} \sin BDC$ ;

and  $AC : CD :: \sin ADC : \sin CAD$ ;

or,  $\sin CAD = \frac{CD}{AC} \sin ADC.$

Hence, by substitution, we have

$$ACB = ADB + \left( \frac{CD}{BC} \sin BDC - \frac{CD}{AC} \sin ADC \right);$$

for, since the distance  $DC$  is very small in comparison with  $BC$  and  $AC$ , the angles  $DBC$  and  $CAD$  are very small; and hence, their sines may be substituted for the angles themselves

It is to be observed, that when the radius is unity, in the above formula, the natural sines of the angles are used, and that the correction within the parenthesis, is expressed in linear units, and will be positive or negative, according as the second term is less or greater than the first.

To convert the linear correction into seconds of an arc, whose radius is unity, let the deduced correction, within the parenthesis, be denoted by  $c$ . Then, since the radius is 1, we shall have

length of semi-circumference  
 : the linear correction  
 :: the number of seconds in  $180^\circ$   
 : the number of seconds in the correction:

that is, denoting the number of seconds in the correction by  $n$ ,

$3.1416 : c :: 648000'' : n$ ; or  $n = c \times 206264.3''$ :  
 $c$  will, in all cases, be a very small fraction.

This correction is not often necessary, for in extensive operations, such stations are chosen as will allow of the measurement of all the angles, and in secondary triangles, it is admissible to measure only two of the angles.

#### SPHERICAL EXCESS.

32. It has already been noticed, that the triangles measured, are on the surface of a sphere, and consequently, the angles taken between any three points, by a theodolite, are, strictly speaking, the angles of a spherical triangle; hence, the sum must exceed  $180^\circ$ , (Geom., Bk. IX., P. 14). This excess is called the *spherical excess*. In the processes of triangulation, we reduce all triangles to rectilinear triangles; and hence, the sides of the triangle, which we seek, are chords of the sphere, and not arcs measured on the surface.

33. In small triangles, where the sides do not exceed 6 or 8 miles, the spherical excess may be altogether neglected; but in large triangles, it must be taken into account. Of all the methods, yet known, of correcting for the spherical excess, Legendre's is considered the best.

This method is based upon the proposition that, *the area of a spherical triangle, which is very small when compared with the entire surface of the sphere, is nearly identical with a rectilinear triangle, whose sides are of the same length as those of the spherical triangle, and whose angles are each diminished by one-third of the spherical excess.*

34. The first thing, then, is to find the spherical excess, and for this, we must know the area of the triangle. The rules for determining the area of the rectilinear triangles, will afford results sufficiently near, and the first approximate area may be computed in square feet, as though the triangle were rectilinear. Having found this area, the formula of Legendre, gives the logarithm of the spherical excess, estimated in seconds, equal to the logarithm of the area of the triangle computed in square feet, minus the constant logarithm 9.326770. That is, if we put

$E$  = the spherical excess, in seconds.

$A$  = area of the triangle, in square feet.

Constant log. = 9.326770;

we shall have,

$$\text{Log } E = \text{log } A - 9.326770.$$

Having found the spherical excess, we divide it by 3, and then diminish each angle of the triangle by the quotient; the sum of the three angles should then be equal to  $180^\circ$ . With these new angles, we compute all the parts of the triangle.

35. The spherical excess between latitude  $25^\circ$  and  $45^\circ$ , is about  $1''$  for an area of 75.5 miles; hence, to obtain a close approximation to the spherical excess, *divide the number of square miles in the area of the triangle by 75.5, the quotient will be the number of seconds required.*

36. To find the spherical excess, knowing the two sides  $a$  and  $b$ , and the included angle  $C$ .

$$\text{area} = \frac{a b \sin C}{2 R}.$$

Suppose  $a = 248230$  feet,  $b = 212628$  feet, and  $C = 103^\circ 19' 10''$ .

$a$ . . . . .	248230 . . . . .	log . . . . .	5.394854
$b$ . . . . .	212628 . . . . .	log . . . . .	5.327620
$C$ . . . . .	$103^\circ 19' 10''$ . . . . .	log sine . . . . .	9.988158
ar. comp. of 2, diminished by 10 . . . . .			<u>1.698970</u>
			20.409602
Log of R . . . . .			<u>10.</u>
Log A . . . . .			10.409602
Constant logarithm . . . . .			<u>9.326770</u>

Hence,  $E = 12.1''$  . . . . . 1.082832. The sum of the three measured angles ought therefore to exceed  $180^\circ$ , by this amount. The angles being corrected, by subtracting  $4.\frac{1}{3}''$  from each, the parts of the triangle may be computed, by regarding the sides as rectilinear.

#### PLOTTING THE TRIANGULATION.

37. The sides of the triangles being computed, after having made the necessary corrections, the work may then be plotted, as already explained, either by means of the circular protractor, or by the method of chords.

#### THE CIRCULAR PROTRACTOR.

38. This instrument consists of a brass circular limb (Pl. 2, Fig. 4), of about six inches in diameter, with a movable index  $AB$ , having a vernier at one extremity  $A$ , and a milled screw at the other extremity  $B$ , with a concealed cog-wheel that works with the cogs of the limb, and thus moves the index  $AB$  about the centre of the protractor. At the centre of the protractor is a small circular glass plate, on which two lines are cut; the point of their intersection, is the exact centre of the instrument. The limb is generally divided to half degrees; the degrees are numbered from 0 to 360.

At the 0 point, and at the opposite extremities of the diameter passing through that point, are small lines on the inner edge of the limb; the two extremities of the diam-

eter, perpendicular to this latter, are designated in the same way.

Two angular pieces of brass, each having a small and sharp steel pin at its extremity, are fastened to the index, and revolve freely around the lines  $ab$  and  $cd$ . The small screws,  $a$ ,  $b$ ,  $c$ , and  $d$ , move them in the directions of the lines  $ab$ ,  $cd$ , for the purpose of bringing the steel pins exactly into the line which passes through the 0 of the index and the centre of the protractor.

To adjust them to their places, place the centre of the protractor over a marked point, and the 0 of the index to the 0 of the limb. Then mark the place of the index by the pins: after which, turn the index  $180^\circ$ , and see if the pins will mark the same points as before. If they do, the index is adjusted; if they do not, correct the error with the screws  $a$ ,  $b$ ,  $c$ , and  $d$ .

#### TO LAY OFF AN ANGLE WITH THE PROTRACTOR.

39. Let its centre be placed over the angular point, and the diameter passing through 0 and  $180^\circ$ , on the given line. Turn the screw that works the index, until the 0 of the vernier coincides with the division corresponding to the given angle; then let the angular brass pieces be turned down; the points dotted by the steel pins will show the direction of the required line.

If this line does not pass through the angular point, the pins are out of place, and must be adjusted.

#### FIRST METHOD OF PLOTTING.

40. Suppose it were required to make the plan of the harbor on a scale of 450 yards to an inch.

Divide the length of the base line  $AB$ , which we will suppose equal to 1140 yards, by 450, and the quotient 2.53 will express the length which is to represent the base line on the paper (Bk. I., Art. 54.)

Draw an indefinite line  $AB$ , to represent the base, and having chosen any point, as  $A$ , for the first station, lay off 2.53 inches to  $B$ . The other extremity of the base line will thus be determined.

Then, place the circular protractor at  $A$ , and lay off the angle  $BAE$ , and then the angle  $EAG$ . Next, place the protractor at  $B$ , and lay off the angles  $ABE$  and  $EBC$ . The intersection of the lines  $AE$  and  $BE$  will determine the station  $E$ . Let the protractor be then placed at this point, and all the angles of station  $E$ , laid down.

The point  $G$ , where  $EG$  intersects  $AG$ , and the point  $C$ , where  $EC$  intersects  $BC$ , will then be found.

By placing the protractor at  $C$  and  $G$ , we can determine the points  $D$  and  $F$ , when the place, on the paper, of all the stations will be known.

To unite the work done with the compass, spread the compass-notes before you, and draw through  $A$  a line to represent the meridian. This line makes an angle of  $12^\circ$  with the course  $AE$ .

Then, lay off from the scale the distances  $Aa$ ,  $Ab$ ,  $Aq$ ,  $Ac$ ,  $Ad$ ,  $Ae$ , and at the several points erect perpendiculars to  $AE$ . Lay off on these perpendiculars the lengths of the offsets, and the curve traced through the points so determined, will be the margin of the lake.

At  $E$ , draw a parallel to the meridian through  $A$ , and lay down the course  $EH$ , which makes an angle of  $50^\circ$  with the meridian. Then, lay down the several distances to the offsets, and draw the offsets and lay off their lengths. Do the same for the course  $HI$ , and all the compass-work will be plotted.

The work done with the plane-table (Art. 28), is united to the work done with the theodolite, by simply placing the line  $AN$  on the paper of the plain-table, upon the line  $AN$ , drawn on the plot of the triangulation.

#### SECOND METHOD OF PLOTTING.

41. Place the centre of the protractor near the centre of the paper, and draw a line through the points  $0$  and  $180^\circ$ . This line will have the same position with the circular protractor that the base line  $AB$  had with the limb of the theodolite.



Lay off then from the 0 point an arc equal to the direction from  $A$  to  $E$ , also an arc equal to the direction  $AG$ , and through the centre point, and the points so determined, draw lines. Lay off in succession, in a similar manner, the directions taken at all the stations; and through the centre point, and the points so determined, draw lines, and designate each by the letters of the direction to which it corresponds.

Now, since all the lines drawn on the paper have the same position with the circular protractor, as the corresponding lines on the ground have with the limb of the theodolite, it follows that each direction will be parallel to its corresponding line upon the ground.

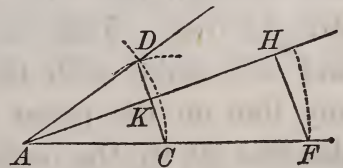
Hence, any line may be drawn parallel to that passing through 0 and  $180^\circ$ , to represent the base line  $AB$ . Having drawn such a line, and marked a point for the station  $A$ , lay off the length of the base, and the extremity will be the station  $B$ .

Through  $A$  and  $B$ , so determined, draw parallels respectively to the lines corresponding to the directions  $AE$  and  $BE$ , and the point of intersection will determine station  $E$ . Through  $B$  and  $E$  draw parallels to the lines which correspond to the directions  $BC$ ,  $CE$ , and their point of intersection will determine station  $C$ . Through  $C$  and  $E$  draw lines parallel to the lines corresponding to the directions  $CE$  and  $ED$ , and the point of intersection will determine  $D$ . In a similar manner we may determine the stations  $F$  and  $G$ .

METHOD OF CHORDS.

42. Let us first prove that *the chord of a given arc is equal to the sine of half the arc with double the radius.*

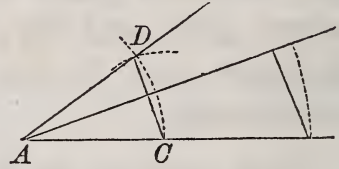
Let  $DAF$  be any given angle, and  $AH$  a line bisecting it. Let  $DC$  be the chord of the arc  $CD$ , described with a given radius, and  $HF$  parallel to  $CD$ , the sine of half the given angle, to a radius  $AF = 2AC$ .



Since  $AF=2AC$  we have, from similar triangles,  $HF=2KC$ , but  $DC=2KC$ , hence  $HF=CD$ .

TO LAY OFF AN ANGLE.

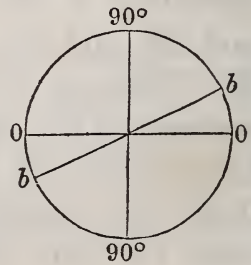
43. To avoid, as far as possible, the use of fractions, let us suppose the radius of the table of natural sines to be 1 *ten*, or 10 inches.



Take from a scale 5 equal parts, with which as a radius, from the centre  $A$ , describe an arc  $CD$ . Take from the table the natural sine of half the arc, and remove the decimal point one place to the right; the result will express the sine of half the arc to the radius 10, or the chord of the arc to the radius 5. From the same scale, take this sine in the dividers, and from  $C$ , as a centre, describe an arc cutting  $CD$  in  $D$ ; draw  $AD$ , and  $CAD$  will be the angle required.

This is the most accurate of all the methods of laying off an angle, and it may also be applied advantageously to the second method of plotting, thus:

Draw a fine straight line, generally in the direction of the meridian or of the base line of the survey; and also a line exactly perpendicular to it. From the point of intersection, as a centre, with a radius of 5 equal parts of the scale, describe the circumference of a circle cutting the straight lines in the points marked 0 and  $90^\circ$ .



To lay off an angle, as for instance, the angle  $14^\circ 29'$ . The half of it is  $7^\circ 14' 30''$ , the natural sine of which is 0.126005, or 1.26 to the radius of 10 inches. Set off from 0 to  $b$ , as in the figure, this distance taken from the scale, and through the two points  $b, b$ , thus determined, draw a straight line. This line should pass through the centre, and will make with the line (0, 0) the angle  $14^\circ 29'$ ; and any line on the paper drawn parallel to it, will make with the line (0, 0) the same angle. The further application is obvious.

## SECTION II.

## MARITIME SURVEYING.

44. When, in connection with a trigonometrical survey on shore, a harbor is to be surveyed for the purpose of ascertaining the channels, their depth and width, the positions of shoals, and the depth of water thereon, other means must be used, and other examinations made in addition to those already referred to.

Let buoys be anchored on the principal shoals and along the edges of the channel, and using any one of the lines already determined as a base, let the angles subtended by lines drawn from its extremities, to the buoys respectively, be measured with the theodolite. Then, there will be known in each triangle the base and angles at the base, from which the distances to the buoys are easily found; and hence, their positions become known.

Having made the soundings, and ascertained the exact depth of the water at each of the buoys, several points of the harbor are established, at which the precise depth of the water is known; and by increasing the number of the buoys, the depth of the water can be found at as many points as may be deemed necessary.

45. If a person with a theodolite, or with any other instrument adapted to the measurement of horizontal angles, be stationed at each extremity of the base line, it will not be necessary to establish buoys. A boat, provided with an anchor, a sounding line, and a signal flag, has only to throw its anchor, hoist its signal flag, and make the sounding, while the persons at the extremities of the base line measure the angles;—from these data, the precise place of the boat can be determined.

46. There is another method of determining the places at which the soundings are made, that admits of great

despatch, and which, if the observations are made with care, affords results sufficiently accurate.

Having established, trigonometrically, three points which can be seen from all parts of the harbor, and having provided a sextant, let the sounding be made at any place in the harbor, and at the same time the three angles subtended by lines drawn to the three fixed points, measured with the sextant.

The problem, to find, from these data, the place of the boat at the time of the sounding, is the same as example 6, page 62.

It is only necessary to measure two of the angles, but it is safest to measure the third also, as it affords a verification of the work.

The great rapidity with which angles can be measured with the sextant, by one skilled in its use, renders this a most expeditious method of sounding and surveying a harbor.

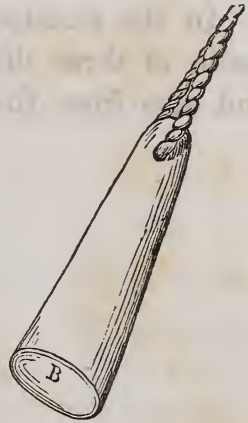
The sextant is not described, nor are its uses explained in these Elements, because its construction combines many philosophical principles, with which the Surveyor cannot be supposed conversant.

47. There is yet another method of finding the soundings, which, although not as accurate as those already explained, will, nevertheless, afford results approximating nearly to the truth. It is this:—Let a boat be rowed uniformly across the harbor, from one extremity to the other of any of the lines determined trigonometrically. Let soundings be made continually, and let the precise time of making each be carefully noted. Then, knowing the length of the entire line, the time spent in passing over it, as also the time of making each of the soundings, we can easily find the points of the line at which the several soundings were made; and hence, the depth of water at those points becomes known.

48. If a person stationed on shore with a theodolite, takes the bearing of the boat, at every second or third sounding, determined by hoisting a flag, it will fix the positions of the

soundings with great accuracy. Soundings may thus be made along any number of known lines, and a comparison of the depths found on different lines, at or near their points of intersection, will show with what degree of accuracy the work has been done.

— Sounding-lines should be made of strong cord, and divided into feet or fathoms, by different colored rags or other marks. The lead is shaped like the frustum of a cone, with the base *B*, hollowed out, to hold some grease. The sand or mud of the bottom adheres to the grease, and thus shows the nature of the bottom, which should be entered in the field-book, and laid down upon the map. As the cord is liable to change its length, it should be compared from time to time with some standard. In tide-waters, the exact time of each sounding is to be noticed, and an assistant should note the height of the tide at regular intervals, upon a tide-gauge. The tide-gauge is permanently placed at some convenient point of the harbor, and its 0 point is referred by means of a spirit-level, to some fixed bench-mark, on a level with mean low-water mark, to which all the soundings must be reduced.



49. Having plotted the work done with the theodolite, as also the outline of the harbor traced with the compass, it remains to delineate the bottom of the harbor; and this is done by means of horizontal curves, which have already been used to represent broken or undulating ground.

Let the plane of reference be taken through low-water mark, or to coincide with the surface of the water at low tide. The accuracy with which the bottom of the harbor is to be delineated, will guide us in fixing the distance between the horizontal planes of section.

The first horizontal plane should be passed at a distance below the shallowest point that has been sounded, equal to the number of feet fixed upon for the distance between the planes of section; and the curve, in which it

intersects the bottom of the harbor determined as in Book III. Sec. II. And similarly, for the other horizontal planes of section.

Having thus delineated the bottom of the harbor, and noted on the map the distance of each intersecting plane below the plane of reference, let such lines be drawn as will indicate the channels, shoals, sunken rocks, and direction of the current.

In the example given in plate 6, soundings have been made in three directions from the sand-bar in the harbor, and also from the rocky shore across to the light-house.

# B O O K V.

## O F N A V I G A T I O N .

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### SECTION I.

#### DEFINITIONS.

1. WE have given, in the preceding parts of this work, various applications of Plane Trigonometry. We propose, in this Book to explain the best methods of determining the place of a ship at sea. This application of Trigonometry constitutes the science and art of *Navigation*.

2. There are two methods of determining the place of a ship at sea.

1st. When a ship departs on her voyage, if we note her courses and the distance sailed, we may, at any time, by means of Plane Trigonometry, determine her place, very nearly.

2d. By means of observations on the heavenly bodies, and the aid of Spherical Trigonometry, we may determine with great accuracy, the place of the ship. This method is called *Nautical Astronomy*.

The first part of Navigation, viz., the cases which can be solved without the aid of observations on the heavenly bodies, will be alone treated of.

3. The earth is nearly spherical. For the purposes of Navigation it may be considered as perfectly so. It revolves round one of its diameters, called the *axis*, in about twenty-four hours.

4. The great circle, whose poles are the extremities of the axis, is called the *equator*. The poles of the equator

are called the poles of the earth—one is called the north pole, and the other the south pole.

5. The circumference of every great circle which passes through the poles, cuts the equator at right angles, and is a *meridian circle*. Every place on the surface of the earth has its own meridian; but for the purposes of Geography and Navigation, all the meridians are reckoned from a particular meridian, which is called the *first meridian*. The English have fixed on the meridian of the Greenwich Observatory, for the first meridian.

6. The *longitude* of any place is the arc of the equator, intercepted between the meridian of that place and the first meridian, and is east or west, according as the place lies east or west of the first meridian.

7. The *difference of longitude* of two places is the arc of the equator included between their meridians; this arc is equal to the difference of longitudes when they are of the same name, and to the sum of the longitudes, when they are of different names.

8. The *latitude* of a place is its distance from the equator, measured on the meridian of the place, and is north or south according as the place lies north or south of the equator.

9. The small circles drawn parallel to the equator, are called *parallels* of latitude. The arc of any meridian intercepted between the parallels passing through any two places, measures the difference of latitude of those places; this difference is found by subtracting the less latitude from the greater, when the latitudes are of the same name, and by adding them when they are of different names.

10. The *sensible horizon* of any place is an imaginary plane, supposed to touch the earth at that place, and to be extended indefinitely.

A plane passing through the centre of the earth, and parallel to the sensible horizon, is called the *rational horizon*.

The north and south line, is the intersection of the plane of the meridian circle with the sensible horizon, and the line which is drawn perpendicular to this, is called the east and west line.



11. The *course* of a ship, at any point, is the angle which her track or keel makes with the meridian. So long as the course is unchanged, the ship would sail in a straight line, if the meridians were truly parallel; but as the meridians bend constantly toward the pole, the direction of her path is continually changing, and she moves in a curve called the *rhumbl line*. The course of a ship is indicated by the mariner's compass.

12. The *mariner's compass* consists of a circular card, whose circumference is divided into thirty-two equal parts called *points*; each point being subdivided into four parts, called *quarter points*.

To the under side of this card a slender bar of magnetized steel, called a *needle*, is permanently attached. The direction of the needle corresponds to the diameter NS. The diameter EW, at right angles to NS, is intended to indicate the east and west points. The points of the compass are thus read: beginning at the north point, and going east, we say, *north and by east*, north north east, north east and by north, north east; and so on, round the compass, as indicated by the letters.

The card being permitted to turn freely on the pin, on which it is poised, as a centre, the line NS will always indicate the true magnetic meridian, but this, as we have seen in (Bk. II., Sec. 7-14), is not the *true* meridian, and hence, the variation must always be allowed for.

On the interior of the compass box, in which the card swings, are two marks *a* and *b*, which lie in a line passing through the centre of the card, and the compass box is so



placed that this line shall be parallel to the keel of the ship. Consequently, if  $b$  be placed towards the bow of the vessel, the point which it marks on the card will show the compass course, for the line NS is always on the magnetic meridian, and EW is east and west. The course is generally read to quarter points, and as a quadrant contains eight points, each point is equal to  $90^\circ \div 8 = 11^\circ 15'$ ; and a quarter point  $= 11^\circ 15' \div 4 = 2^\circ 48' 45''$ . The table of Rhumbs, after the Traverse Table, shows the degrees in each course, to quarter points.

13. A ship's *rate* of sailing is determined by means of an instrument, called the *log*, and an attached line called the log line. The log is a piece of wood in the form of a sector of a circle, the rim of which is loaded with lead, so that when it is heaved into the sea it assumes a vertical position. The log line is so attached as to hold the log square against the water, that it may not be drawn along after the ship as the line unwinds from the reel, by the ship's forward motion.

The time in which the log line unwinds from the reel, is noted by a sand-glass, through which the sand passes in *half* a minute; that is, in the *one hundred and twentieth part of an hour*.

For convenience, the log line is divided into equal parts, marked by *knots*, and each part is equal to the one hundred and twentieth part of a nautical or geographical mile\*.

Now, since half a minute is the one hundred and twentieth part of an hour, and each knot indicates the one hundred and twentieth part of a mile, it follows that the *number* of knots reeled off while the half minute glass runs out, will indicate the rate of the ship's sailing per hour.

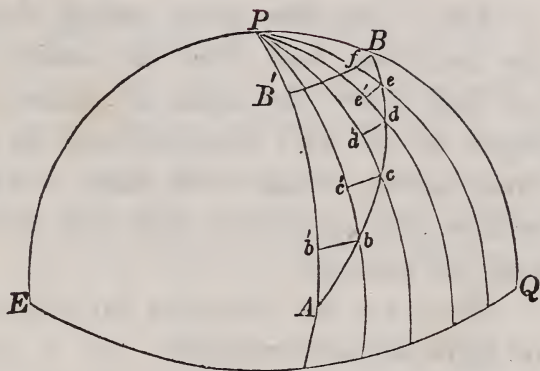
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\* A geographical mile is one minute, or one-sixtieth of a degree, measured on the equator. Taking the diameter at 7916 English miles, the geographical mile will be about 6079 feet; that is, one-sixth greater than the English mile, which is 5280 feet.

SECTION II.

OF PLANE SAILING.

14. Let the diagram  $EPQ$  represent a portion of the earth's surface,  $P$  the pole, and  $EQ$  the equator. Let  $AB$  be any rhumb line, or track described by a ship in sailing from  $A$  to  $B$ .



Conceive the path of the ship to be divided into very small parts, and through the points of division draw meridians, and also the parallels of latitude  $b'b$ ,  $c'c$ ,  $d'd$ ,  $e'e$ , and  $B'B$ : a series of triangles will thus be formed, but so small that each may be considered as a plane triangle.

In these triangles, the sum of the bases

$$Ab' + bc' + cd' + de' + ef = AB',$$

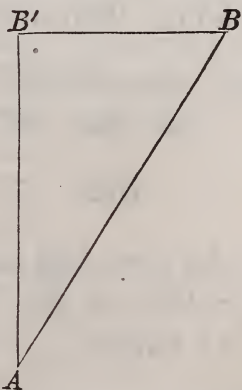
which is equal to the difference of latitude between the points  $A$  and  $B$ . Also,

$$b'b + c'c + d'd + e'e + fB = BB',$$

which is equal to the distance that the ship has departed from the meridian  $AB'P$ , and is called the departure in sailing from  $A$  to  $B$ .

Therefore, the *distance* sailed, the *difference of latitude* made, and the *departure*, may be represented by the hypotenuse, the base and perpendicular of a right-angled triangle, of which the angle opposite the departure is the course.

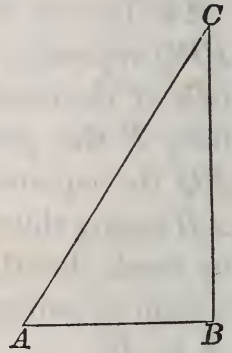
When any of the four parts above-named are given, the other two can be determined. This method of determining the place of a ship reduces all the elements to the parts of a plane triangle, and hence is called *plane sailing*.



EXAMPLES.

1. A ship from latitude  $47^\circ 30'$  N. has sailed S. W. by S. 98 miles. What latitude is she in, and what departure has she made?

Let  $C$  be the place sailed from,  $CB$  the meridian, and  $BCA$  the course, which we find from the table of rhumbs to be equal to  $33^\circ 45'$ ; then  $AC$  will be the distance sailed, equal to 98 miles. Also,  $AB$  will be the departure, and  $CB$  the difference of latitude.



Then by the formulas for the solution of right angled triangles,

As radius	ar. c.	0.000000		As radius	ar. c.	0.000000
: cos	$C\ 33^\circ 45'$	9.919846		: sin	$C\ 33^\circ 45'$	9.744739
::	$AC\ 98$	1.991226		::	$CA\ 98$	1.991226
·	$CB\ 81.48$	1.911072		:	$AB\ 54.45$	1.735965

Latitude left  $47^\circ 30'$  N.

Dif. lat. = 81.48 miles = 81.48 minutes =  $1^\circ 22'$  S.

In latitude  $46^\circ 08'$

Departure, 54.45 miles.

2. A ship sails 24 hours on a direct course, from latitude  $38^\circ 32'$  N. till she arrives at latitude  $36^\circ 56'$  N. The course is between S. and E. and the rate  $5\frac{1}{2}$  miles an hour. Required the course, distance, and departure.

Lat. left  $38^\circ 32'$  N.       $24 \times 5\frac{1}{2} = 132$  miles = distance.

In lat.  $36^\circ 56'$

Diff.  $1^\circ 36' = 96$  miles.

As dist. 132	ar. c.	7.879426		As radius	ar. c.	0.000000
: diff. lat. 96		1.982271		: dist. 132		2.120574
::	radius	10.000000		::	sin course $43^\circ 20'$	9.836477
: cos course $43^\circ 20'$		9.861697		: dep.	90.58	1.957051

Hence, the course is S.  $43^{\circ} 20'$  E., and the departure 90.58 miles east.

3. A ship sails from latitude  $3^{\circ} 52'$  S. to latitude  $4^{\circ} 30'$  N., the course being N. W. by W.  $\frac{1}{2}$  W.: required the distance and departure.

*Ans.* Dist. 1065 miles; dep. 939.2 miles W.

4. Two points are under the same meridian, one in latitude  $52^{\circ} 30'$  N., the other in latitude  $47^{\circ} 10'$  N. A ship from the southern place sails due east, at the rate of 9 miles an hour, and two days after meets a sloop that had sailed from the other: required the sloop's direct course, and distance run.

*Ans.* Course S.  $53^{\circ} 28'$  E.; dist. 537.6 miles.

5. If a ship from latitude  $48^{\circ} 27'$  S., sail S. W. by W. 7 miles an hour, in what time will she reach the parallel of  $50^{\circ}$  south? *Ans.* 23.914 hours.

### SECTION III.

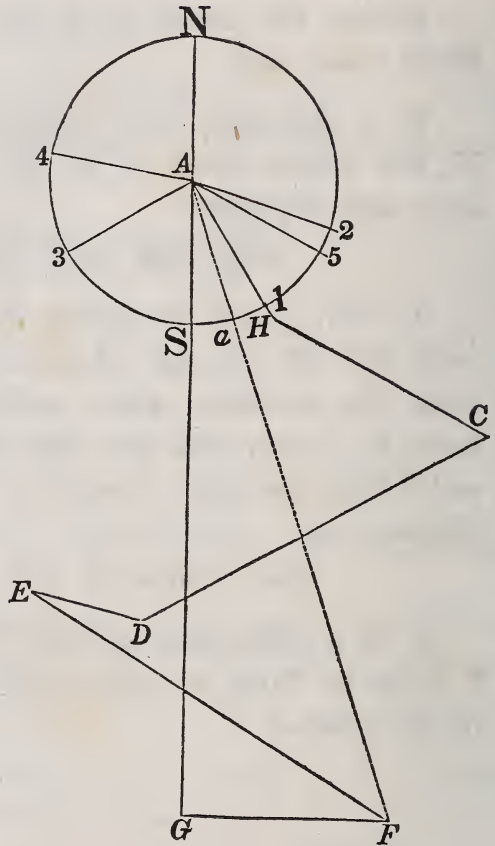
#### OF TRAVERSE SAILING.

15. When a ship, in going from one place to another, sails on different courses, it is called *Traverse Sailing*. The determination of the distance and course, from the place of departure to the place of termination, is called *compounding* or *working* the traverse. This is done by the aid of the "Traverse Table," which has already been explained, and the method of working the traverse, is in all respects similar to that adopted in the Prob. of Art. 34, page 123.

#### EXAMPLES.

1. A ship from Cape Clear, in lat.  $51^{\circ} 25'$  N., sails, 1st, S. S. E.  $\frac{1}{4}$  E. 16 miles; 2d, E. S. E. 23 miles; 3d, S. W. by W.  $\frac{1}{2}$  W. 36 miles; 4th, W.  $\frac{3}{4}$  N. 12 miles; 5th, S. E. by E.  $\frac{1}{4}$  E. 41 miles: required the distance run, the direct course, and the latitude.

We first form the table below, in which we enter the courses, from the table of rhumbs, omitting the seconds, and then enter the latitudes and departures, taken from the traverse table, to the nearest quarter degree. Thus, in taking the latitude and departure for  $25^\circ 18'$  we take for  $25\frac{1}{4}^\circ$ . The difference of latitudes gives the line  $AG$ , and the difference of departures the line  $GF$ .



TRAVERSE TABLE.

Courses.		Dist's.	Diff. of Latitude.		Departure.	
No	Angle.		N.	S.	E.	W.
1	S. S. E. $\frac{1}{4}$ E. . . . .	$25^\circ 18'$	16	14.47	6.83	
2	E. S. E. . . . .	$67^\circ 30'$	23	8.80	21.25	
3	S. W. by W. $\frac{1}{2}$ W. . . . .	$61^\circ 52'$	36	17.04		31.71
4	W. $\frac{3}{4}$ N. . . . .	$81^\circ 33'$	12	1.77		11.87
5	S. E. by E. $\frac{1}{4}$ E. . . . .	$59^\circ 03'$	41	21.12	35.14	
			1.77	61.43	63.22	43.58
				1.77	43.58	
			Diff.	59.66	19.64	

Latitude left  $51^\circ 25' N.$   
 Difference of latitude 59.66 miles =  $1^\circ 00' S.$   


---

 In latitude  $50^\circ 25' N.$

Then, by formulas for the solution of right-angled triangles, we have,

As $AG$ , diff. lat. ar. c. 8.224317 : departure 19.64 1.293141 :: radius, 10.000000 <hr style="width: 50%; margin-left: 0;"/> : tang course $18^\circ 13'$ 9.517458		As sin course ar. c. .504995 : radius 10.000000 :: departure 19.64 1.293141 <hr style="width: 50%; margin-left: 0;"/> : distance 62.83 1.798136
---	--	--

Therefore the direct course is S.  $18^\circ 13'$  E., and the distance 62.83 miles.

#### OF PLOTTING.

16. There is yet another method of finding the direct course and distance, much practiced by seamen, although it does not afford a high degree of accuracy. It is a method by plotting, which requires the use of a mariner's scale and a pair of dividers.

One of the scales marked on the mariner's scale, is a scale of chords, commonly called a scale of rhumbs, being divided to every quarter point of the compass; and there is also a second scale of chords divided to degrees. Both of these scales are constructed in reference to the same common radius, so that the chords on the scale of rhumbs correspond to those on the scale of marked chords. The manner of using the scales will appear in plotting the last example.

To construct this traverse, describe a circle with a radius equal to the chord of  $60^\circ$  and draw the meridian  $NS$ . Then take from the line of rhumbs the chord of the first course  $2\frac{1}{4}$  points, and apply it from  $S$  to 1, to the right of  $NS$ , since the course is southeasterly, and draw  $A1$ ; take, in like manner, the chord of the second course, 6 points, from  $S$  to 2, and lay it off also to the right of the meridian line. Apply the chord of the third course,  $5\frac{1}{2}$  points, from  $S$  to 3, to the left of the meridian; the fourth course,  $7\frac{1}{4}$  points from  $N$  to 4, to the left of  $NS$ , this course being northwesterly; and, lastly, apply the chord of the fifth course,  $5\frac{1}{4}$  points, from  $S$  to 5, to the right of  $NS$ , and join all the lines as in the figure.

In the direction  $A1$ , lay off the distance  $AH = 16$  miles from a scale of equal parts, and through the extremity  $H$ , draw  $HC$  parallel to  $A2$ , and lay off  $HC = 23$  miles. Draw  $CD$  parallel to  $A3$ , and lay off  $CD = 36$  miles; then draw  $DE$  parallel to  $A4$ , and lay off 12 miles; and lastly, draw  $EF$  parallel to  $A5$ , and lay off 41 miles, and  $F$  will be the place of the ship. Hence, we conclude that  $AF$  is the distance made good, and  $GAF$  is the course.

Applying, then, the distance  $AF$  to the scale of equal parts, we find it equal to  $62\frac{3}{4}$  miles; and applying the chord  $Sa$  to the scale of chords, we find the course  $GAF = 18\frac{1}{4}^\circ$ .

2. A ship sails from a place in latitude  $24^\circ 32' N.$ , and runs the following courses and distances, viz., 1st, S. W. by W. dist. 45 miles; 2d, E. S. E. dist. 50 miles; 3d, S. W. dist. 30 miles; 4th, S. E. by E. dist. 60 miles; 5th, S. W. by S.  $\frac{1}{4}$  W. dist. 63 miles: required her latitude, and the direct course and distance from the place left to the place arrived at, and the construction of the traverse.

$$Ans. \begin{cases} \text{Lat. } 22^\circ 3' N., \text{ course S.} \\ \text{Dist. } 149.2 \text{ miles.} \end{cases}$$

3. A ship from lat.  $28^\circ 32' N.$  has run the following courses, viz., 1st, N. W. by N. 20 miles; 2d, S. W. 40 miles; 3d, N. E. by E. 60 miles; 4th, S. E. 55 miles; 5th, W. by S. 41 miles; 6th, E. N. E. 66 miles: required her latitude, the distance made good, and the direct course, also the construction of the traverse.

$$Ans. \text{ Dist. } 70.2 \text{ miles, course E.}$$

4. A ship from lat.  $41^\circ 12' N.$  sails S. W. by W. 21 miles; S. W.  $\frac{1}{2}$  S. 31 miles; W. S. W.  $\frac{1}{2}$  S. 16 miles; S.  $\frac{3}{4}$  E. 18 miles; S. W.  $\frac{1}{4}$  W. 14 miles; then W.  $\frac{1}{2}$  N. 30 miles: required the latitude, the direct course, and the distance.

$$Ans. \begin{cases} \text{Lat. } 40^\circ 05', \text{ course S. } 52^\circ 49' \text{ W.} \\ \text{Dist. } 111.7 \text{ miles.} \end{cases}$$

5. A ship runs the following courses, viz.:

1st, S. E. 40 miles; 2d, N. E. 28 miles; 3d, S. W. by W. 52 miles; 4th, N. W. by W. 30 miles; 5th, S. S. E.



36 miles; 6th, S. E. by E. 58 miles: required the direct course, and distance made good.

*Ans.* { Direct course S.  $25^{\circ} 59'$  E., or S. S. E.  $\frac{1}{4}$  E., nearly.  
 { Distance 95.87 miles.

6. A ship sails, 1st, N. W. by W.  $\frac{1}{2}$  W. 40 miles; 2d N. W. by  $\frac{1}{4}$  N., 41 miles; 3d, N. by E. 16.1 miles; and 4th, N. E.  $\frac{1}{4}$  E. 32.5 miles: required the distance made, and the direct course.

*Ans.* Course,  $21^{\circ} 54'$  West of North. Dist. 94.6 miles.

These examples will, perhaps, suffice to illustrate the principles of plane sailing.

The longitude, made on any course, cannot be determined by these methods, for this being the arc of the equator intercepted between two meridians, cannot be found under the supposition that the meridians are parallel.

The most simple case of finding the difference of longitude is when the ship sails due east or due west: this is called *Parallel Sailing*.

## SECTION IV.

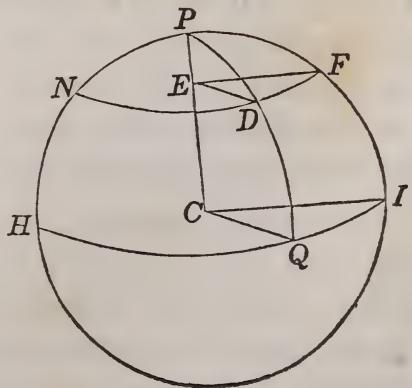
### PARALLEL SAILING.

17. The entire theory of parallel sailing is comprehended in the following proposition, viz.:

*The cosine of the latitude of the parallel, is to radius, as the distance run to the difference of longitude.*

Let  $IQH$  represent the equator, and  $FDN$  any parallel of latitude: then,  $CI$  will be the radius of the equator, and  $EF$  the radius of the parallel.

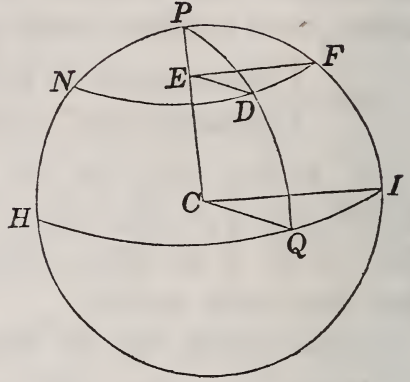
Suppose  $FD$  to be the distance sailed, then the difference of longitude will be measured by  $IQ$ , the arc intercepted on the equator. Then,



since similar arcs are to each other as their radii (Geom., Bk. V., Prop. 14), we have,  
 $EF : CI :: \text{dist. } FD : \text{diff. long. } IQ.$

But  $EF$  is the sine of  $PF$ , or cosine of  $FI$ , the latitude: and  $CI$  is the radius of the sphere: hence,

$$\cos \text{ lat.} : R :: \text{distance} : \text{diff. longitude.}$$



18. If we denote by  $D$  the distance between any two meridians, measured on the parallel whose latitude is  $L$ ; and by  $D'$  the distance between the same meridians measured on the parallel whose latitude is  $L'$ , the arcs are similar, and we shall have (Geom., Bk. V., Prop. 14),

$$\cos L : D :: \cos L' : D',$$

that is,  $\cos L : \cos L' :: D : D'.$

Hence, *when the longitude made on different parallels is the same, the distances sailed are proportional to the cosines of the parallels of latitude.*

19. By referring to Th. V., Bk. I., we see that in any right-angled triangle

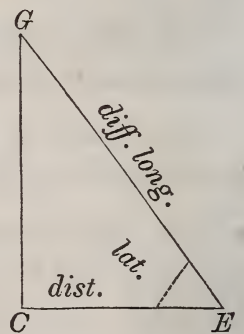
$$R : \cos \text{ angle at base} :: \text{hyp.} : \text{base,}$$

$$\text{or } \cos E : R :: EC : EG;$$

and by comparing this with the proportion,

$$\cos \text{ lat.} : R :: \text{dist.} : \text{diff. long.};$$

we see, that if in a right-angled triangle the angle at the base be made equal to the latitude of the parallel, and the base to the distance run; then, the hypotenuse will represent the difference of longitude.



It follows therefore, that any problem in parallel sailing, may be solved as a simple case of plane sailing. For, if we regard the latitude as the course, the distance run as the base, the difference of longitude will be the hypotenuse of the corresponding right-angled triangle.

## EXAMPLES.

1. A ship from latitude  $53^{\circ} 56'$  N., longitude  $10^{\circ} 18'$  E., has sailed due west, 236 miles: required her present longitude.

By the rule

As cos lat.	$53^{\circ} 56'$	.	ar. c.	.	.230087
: radius	.	.	.	.	10.000000
:: distance	236	.	.	.	<u>2.372912</u>
: diff. long.	400.8	.	.	.	<u>2.602999</u>

Long. left . . .  $10^{\circ} 18'$  E.

Diff. long. =  $\frac{400}{60}$  degrees =  $6^{\circ} 40'$  W.

Long. . . .  $3^{\circ} 38'$  E.

2. If a ship sails E. 126 miles from the North Cape, in lat.  $71^{\circ} 10'$  N., and then due N., till she reaches lat.  $73^{\circ} 26'$  N.; how far must she sail W. to reach the meridian of the North Cape?

Here the ship sails on two parallels of latitude, first on the parallel of  $71^{\circ} 10'$ , and then on the parallel of  $73^{\circ} 26'$ , and makes the same difference of longitude on each parallel.

Hence, by Art. 18,

As cos lat.	$71^{\circ} 10'$	arith. comp.	0.491044
: distance	126	.	2.100371
:: cos lat.	$73^{\circ} 26'$	.	<u>9.455044</u>
: distance	111.3	.	<u>2.046459</u>

3. A ship in latitude  $32^{\circ}$  N. sails due E. till her difference of longitude is 384 miles: required the distance run.  
*Ans.* 325.6 miles.

4. If two ships in latitude  $44^{\circ} 30'$  N., distant from each other 216 miles, should both sail directly S. till their distance is 256 miles, what latitude would they arrive at?  
*Ans.*  $32^{\circ} 17'$  N.

5. Two ships in the parallel of  $47^{\circ} 54'$  N., have  $9^{\circ} 35'$  difference of longitude, and they both sail directly S., a distance of 836 miles: required their distance from each other at the parallel left, and at that reached.

*Ans.* 385.5 miles, and 479.9 miles.

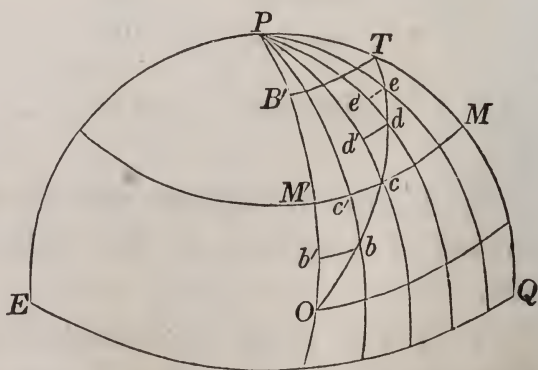
## SECTION V.

### MIDDLE LATITUDE SAILING.

20. Having seen how the longitude which a ship makes when sailing on a parallel of latitude may be determined, we come now to examine the more general problem, viz., to find the longitude which a ship makes when sailing upon any oblique rhumb.

There are two methods of solving this problem, the one by what is called *middle latitude sailing*, and the other by *Mercator's sailing*. The first of these methods is confined in its application, and is moreover somewhat inaccurate even where applicable; the second is perfectly general, and rigorously true; but still there are cases in which it is advisable to employ the method of middle latitude sailing, in preference to that of Mercator's sailing. It is, therefore, proper that middle latitude sailing should be explained, especially since, by means of a correction to be hereafter noticed, the usual inaccuracy of this method may be rectified.

Middle latitude sailing proceeds on the supposition that the departure or sum of all the meridional distances,  $b'b$ ,  $c'c$ ,  $d'd$ , &c., from  $O$  to  $T$ , is equal to the distance  $M'M$  between the meridians



passing through  $O$  and  $T$ , measured on the parallel of latitude equally distant from  $O$  and  $T$ .

The middle latitude is *half the sum* of the two extreme latitudes, if they are both of the same name, and *half their difference*, if they are of contrary names.

The supposition above becomes very inaccurate when the course is small, and the distance run great; for it is plain that the middle latitude distance will receive a much greater accession than the departure, if the track  $OT$  cuts the successive meridians at a very small angle.

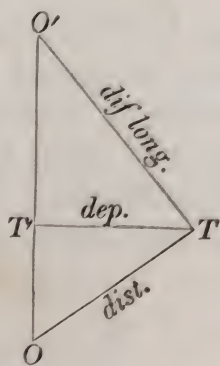
The principal approaches nearer to accuracy as the angle  $O$  of the course increases, because then as but little advance is made in latitude, the several component departures lie more in the immediate vicinity of the parallel  $M'M$ . But still, in very high latitudes, a small advance in latitude makes a considerable difference in meridional distance; hence, this principle is not to be used in such latitudes, if much accuracy is required.

By means, however, of a small table of corrections, constructed by *Mr. Workman*, the imperfections of the middle latitude method may be removed, and the results of it rendered in all cases accurate. This table we have given at the end of this work.

21. The rules for middle latitude sailing may be thus deduced.

We have seen, in the first case of plane sailing, that if a ship sails on an oblique rhumb from  $O$  to  $T$ , that the hypotenuse  $OT$  will represent the distance;  $OT'$  the difference of latitude, and  $T'T$ , the departure. Now, by the present hypothesis, the departure  $T'T$  is equal to the middle parallel of latitude between the meridians of the places sailed from and arrived at:

so that the difference of longitude of these two places is the same as if the ship had sailed the distance  $T'T$  on the middle parallel of latitude. The determination of the difference of longitude is, therefore, reduced to the case of parallel sailing: for,  $T'T$  now representing the distance on the parallel, if the angle  $T'TO'$  be made equal to the latitude of



that parallel, we shall have, by the last case, the difference of longitude represented by the hypotenuse  $O'T$ . We therefore have the following theorems:

I. In the triangle  $O'TT'$ ,

$$\cos O'TT' : TT' :: R : TO';$$

that is,

$$\cos \text{mid. lat.} : \text{departure} :: R : \text{diff. longitude.}$$

II. In the triangle  $O'TO$

$$\sin O' : OT :: \sin O : O'T;$$

that is, since  $\sin O' = \cos O'TT'$

$$\cos \text{mid. lat.} : \text{distance} :: \sin \text{course} : \text{diff. longitude.}$$

III. In the triangle  $OTT'$ , we have

$$R : \text{tangent } O :: OT' : TT';$$

comparing this with the first proportion, and observing that the extremes of this are the means of that, we have

$$OT' : O'T :: \cos O'TT' : \text{tang } O;$$

that is,

$$\text{diff. lat.} : \text{diff. long.} :: \cos \text{mid. lat.} : \text{tang course.}$$

These three propositions comprise the theory of middle latitude sailing; and when to the middle latitude sailing, the proper correction, taken from Mr. Workman's table, is applied, these theorems will be rendered accurate.

In the table of pages 93 and 94, the middle latitude is to be found in the first column to the left. Then, along the horizontal line, and under the given difference of latitude, is inserted the proper correction to be *added* to the middle latitude to obtain the latitude in which the meridian distance is accurately equal to the departure. Thus, if the middle latitude be  $37^\circ$ , and the difference of latitude  $18^\circ$ , the correction will be found on page 94, and is equal to  $0^\circ 40'$ .

#### EXAMPLES.

1. A ship, in latitude  $51^\circ 18' N.$ , longitude  $22^\circ 6' W.$ , is bound to a place in the S. E. quarter, 1024 miles distant, and in lat.  $37^\circ N.$ : what is her direct course and dis-

tance, as also the difference of longitude between the two places?

Lat. from	51° 18' N.	}	Sum of latitudes	. . 88° 18'
Lat. to	37° 0' N.			
	—————		Mid. lat.	. . . 44° 9'
Diff. lat.	14° 18' = 858 miles.			
As distance	1024	6.989700	Cos mid lat 44° 9' ar c	0.144167
: radius		10.000000	: tang course 33° 5'	9.813899
:: diff. lat.	858	2.933487	:: diff. lat.	858 2.933487
		—————		
: cos course 33° 5'		9.923187	: diff. long.	779 2.891553
		—————		—————

In this operation the middle latitude has not been corrected, so that the difference of longitude here determined is not without error. To find the proper correction, look for the given middle latitude, viz., 44° 9', in the table of corrections, the nearest to which we find to be 45°; against this and under 14° diff. of lat. we find 27'; and also, under 15° we find 31', the difference between the two being 4'; hence, corresponding to 14° 18' the correction will be about 28'. Hence, the corrected middle latitude is 44° 37', therefore,

Cos corrected mid. lat.	44° 37' ar. comp.	0.147629		
: tang. course	33° 5'	. . . 9.813899		
:: diff. lat.	858 . . .	2.933487		
		—————		
: diff. long	785.3 . . .	2.895015		—————

therefore, the error in the former result is about 6½ miles.

2. A ship sails in the N. W. quarter, 248 miles, till her departure is 135 miles, and her difference of longitude 310 miles: required her course, the latitude left, and the latitude come to.

*Ans.* } Course N. 32° 59' W.;  
 } Lat. left 62° 27' N.; lat. in 65° 55' N.

3. A ship, from latitude 37° N., longitude 9° 2' W., having sailed between the N. and W., 1027 miles, reckons that she has made 564 miles of departure: what was her direct course, and the latitude and longitude reached?

*Ans.* } Course N. 33° 19' W., or N. W. nearly;  
 } Lat. 51° 18' N.; long. 22° 8' W.

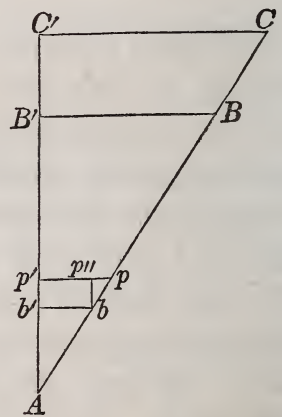
4. Required the course and distance from the east point of St. Michael's, lat.  $37^{\circ} 48'$  N., long.  $25^{\circ} 13'$  W., to the Start Point, lat.  $50^{\circ} 13'$  N., long.  $3^{\circ} 38'$  W.; the middle latitude being corrected by Workman's table.

*Ans.* Course N.  $51^{\circ} 11'$  E.; dist. 1189 miles.

#### MERCATOR'S SAILING.

22. It has already been observed, that when a ship sails on an oblique rhumb, the departure, the difference of latitude, and the distance run, are truly represented by the sides of a right-angled triangle.

Thus, if a ship sails from  $A$  to  $B$ , the departure  $B'B$  will represent the sum of all the very small meridian distances, or elementary departures,  $b'b$ ,  $p''p$ , &c.; the difference of latitude  $AB'$  will represent, in like manner, the small differences of latitude  $Ab'$ ,  $b'p'$ , &c.; and the hypotenuse  $AB$ , will express the sum of the distances corresponding to these several differences of latitude and departure.



Each of these elements is supposed to be taken so small, as to form on the surface of the sphere a series of triangles, differing insensibly from plane triangles.

Let  $ABB'$  be a triangle, in which the angle  $A$  represents the course,  $AB'$  the difference of latitude,  $B'B$  the departure, and  $AB$  the distance run. Produce the side  $AB'$  to  $C'$ , until  $CC'$  shall be equal to the difference of longitude of the two extremities of the course: then, for the sake of distinction, we call

$AB' =$  the *proper* difference of latitude,

$AC' =$  the *meridional difference* of latitude,

and we are now to explain the manner of constructing a table, called a table of meridional parts, which will furnish the *meridional differences* of latitude when the *proper* differences are known.

Let  $Ab'b$  represent one of the elementary triangles;  $b'b$  will then be one of the elements of departure; and  $Ab'$  the corresponding difference of latitude. Now, as  $b'b$  is a small arc of a parallel of latitude, it is to a portion of the



equator containing an equal number of degrees, as the cosine of its latitude is to radius (Art. 17). This similar portion of the equator, is the difference of longitude between  $b'$  and  $b$ .

Suppose, now, that  $Ab'$  is prolonged to  $p'$ , making  $p'p$  equal to the difference of longitude between  $b$  and  $b'$ : then

$$bb' : pp' :: \cos \text{ lat. } b'b : R \text{ (Art. 17.)}$$

But, by similar triangles, we have

$$bb' : pp' :: Ab' : Ap',$$

and consequently,

$$\text{proper lat. } Ab' : \text{mer. diff. of lat. } Ap' :: \cos \text{ lat. } bb' : 1.$$

Denoting the proper difference of latitude by  $d$ , the meridional difference of latitude by  $D$ , the latitude of  $b'b$  by  $l$ , and the radius by 1, which is, indeed, the radius of the table of natural sines, we shall have

$$d : D :: \cos l : 1,$$

which gives

$$D = d \secant l, \quad \text{since} \quad \frac{1}{\cos l} = \sec. l.$$

If then, we know the latitude  $l$  of the beginning of a course, and the proper difference of latitude  $d$  of the extremity of the course, we can easily find the meridional latitude  $D$  corresponding to that course.

The determination of  $AC'$  which represents the meridional difference of latitude, involves the determination of all the elementary parts, on which it depends. If  $d$  be taken equal to 1', we shall have from the equation above

$$D = 1' \sec. l, \quad \text{or} \quad D = \sec. l,$$

it being understood that  $l$  expresses minutes or geographical miles.

From this equation, the value of  $D$ , corresponding to every minute of  $l$ , from the equator to the pole, may be calculated; and from the continued addition of these, there may be obtained, in succession, the meridional parts corresponding to 1', 2', 3', 4', &c., of proper latitude, and when registered in a table, they form a table of meridional parts, given in all books on Navigation.

The following may serve as a specimen of the manner in which such a table may be constructed, and, indeed, of the manner in which the first table of meridional parts was

actually formed by Mr. Wright, the proposer of this valuable method.

Mer. pts. of  $1'$  = nat. sec.  $1'$ .

Mer. pts. of  $2'$  = nat. sec.  $1'$  + nat. sec.  $2'$ .

Mer. pts. of  $3'$  = nat. sec.  $1'$  + nat. sec.  $2'$  + nat. sec.  $3'$ .

Mer. pts. of  $4'$  = nat. sec.  $1'$  + nat. sec.  $2'$  + nat. sec.  $3'$  + &c.

Hence, by means of a table of natural secants we have

	Nat. Secs.	Mer. Pts.
Mer. pts. of $1'$ =	1.000000	= 1.0000000
Mer. pts. of $2'$ =	1.0000000 + 1.0000000	= 2.0000002
Mer. pts. of $3'$ =	2.0000002 + 1.0000004	= 3.0000006
Mer. pts. of $4'$ =	3.0000006 + 1.0000007	= 4.0000013, &c.

There are other methods of construction, but this is the most simple and obvious. The meridional parts thus determined, are all expressed in geographical miles, because in the general expression

$$D = 1' \text{ sec. } l,$$

$1'$  is a geographical mile.

23. Having thus formed the table of meridional parts, if we find from it, the meridional parts corresponding to the latitudes of the place left and the place arrived at, their difference will be the meridional difference of latitude, or the line  $AC'$  in the diagram. The difference of longitude denoted by  $C'C$  may then be found by the following proportion.

1. *As radius is to the tangent of the course, so is the meridional difference of latitude to the difference of longitude.*

But if the departure be given instead of the course, then,

II. *As the proper difference of latitude is to the departure, so is the meridional difference of latitude to the longitude.*

Other proportions may also be deduced from the diagram.

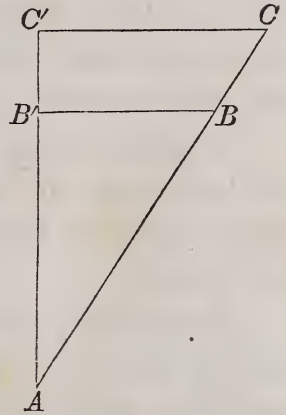
#### EXAMPLES.

As an example of Mercator's or rather Wright's, sailing, let us take the following:

1. Required the course and distance from the east point of St. Michael's to the Start point: the latitudes being  $37^{\circ} 48' N.$ , and  $50^{\circ} 13' N.$ , and the longitudes  $25^{\circ} 13' W.$ , and  $3^{\circ} 38' W.$

Start Point, lat. 50° 13' N.	Mer. pts. 3495
St. Michael's, lat. 37° 48' N.	Mer. pts. 2453
Proper difference of lat. <u>12° 25'</u>	Mer. diff. <u>1042</u>
60	Diff. of long. 21° 35'
Diff. in miles <u>745</u>	60
	Diff. in miles <u>1295</u>

Now, let us suppose that we have sailed from *A* to *B*: we shall then know *AB'* equal proper diff. lat. = 745 miles; *AC'* = meridional diff. of lat. = 1042; and *C'C* = the difference of longitude equal to 1295 miles. It is required to find the course *B'AB*, and the distance *AB*.



For the Course.		For the Distance.	
As <i>AC'</i>	1042	As cos <i>A</i>	51° 11'
: radius	10.000000	: <i>AB'</i>	745
:: <i>C'C</i>	1295	: : radius	10.000000
: tang. <i>A</i>	51° 11' E.	: <i>AB</i>	1189
	10.094402		3.075006

2. A ship sails from latitude 37° N. longitude 22° 56' W., on the course N. 33° 19' E.: till she arrives at 51° 18' N.: required the distance sailed, and the longitude arrived at. *Ans.* Dis. 1027 miles; long. 9° 45' W.

MERCATOR'S CHART.

24. MERCATOR'S CHART is a Map constructed for the use of Navigators. In this chart all the meridians are represented by straight lines drawn parallel to each other, and the parallels of latitude are also represented by parallel straight lines drawn at right-angles to the meridians.

The chart may be thus constructed. Draw on the lower part of the paper a horizontal line to represent the parallel of latitude which is to bound the southern portion of the chart. From a scale of equal parts, corresponding in size

to the extent of the map to be made, lay off, on this line, any number of equal distances, and through the points draw a series of parallels to represent the meridians.

Then draw a line on the side of the map, and for the second parallel of latitude, find from the table of meridional parts the meridional difference of latitude corresponding to the degrees between the first and second parallel, and lay off this distance for the interval between the two parallels. Then find the meridional difference between the second and third, and lay it off in the same way for the third parallel, and so on, for the fourth, fifth, &c.

A place whose latitude and longitude are known, may be laid down in the same manner; for it will always be determined by the intersection of the meridian and parallel of latitude.

If the chart is constructed on a small scale, the divisions on the graduated lines, may be *degrees* instead of minutes; and the meridians and parallels may be drawn only for every fifth or tenth degree.

We have already seen (Art. 23), that the meridional difference of latitude bears a constant ratio to the difference of longitude, so long as the course remains unchanged: and hence we see that on Mercator's chart, every rhumb will be represented by a straight line.

#### LINE OF MERIDIONAL PARTS ON GUNTER'S SCALE.

25. This scale corresponds exactly with the table of meridional parts, excepting, that in the table, the circle is divided to minutes, while the scale is divided only to degrees. A scale of equal parts is placed directly beneath the scale of meridional parts; if the former corresponds to divisions of longitude, the latter will represent those of latitude. Hence, a chart may be constructed from those scales, by using the scale of equal parts for the lines of longitude, and the scale of meridional parts for those of latitude.

# A TABLE

## OF

### LOGARITHMS OF NUMBERS

FROM 1 TO 10,000.

N.	Log.	N.	Log.	N.	Log.	N.	Log.
1	0.000000	26	1.414973	51	1.707570	76	1.880814
2	0.301030	27	1.431364	52	1.716003	77	1.886491
3	0.477121	28	1.447158	53	1.724276	78	1.892095
4	0.602060	29	1.462398	54	1.732394	79	1.897627
5	0.698970	30	1.477121	55	1.740363	80	1.903090
6	0.778151	31	1.491362	56	1.748188	81	1.908485
7	0.845098	32	1.505150	57	1.755875	82	1.913814
8	0.903090	33	1.518514	58	1.763428	83	1.919078
9	0.954243	34	1.531479	59	1.770852	84	1.924279
10	1.000000	35	1.544068	60	1.778151	85	1.929419
11	1.041393	36	1.556303	61	1.785330	86	1.934498
12	1.079181	37	1.568202	62	1.792392	87	1.939519
13	1.113943	38	1.579784	63	1.799341	88	1.944483
14	1.146128	39	1.591065	64	1.806181	89	1.949390
15	1.176091	40	1.602060	65	1.812913	90	1.954243
16	1.204120	41	1.612784	66	1.819544	91	1.959041
17	1.230449	42	1.623249	67	1.826075	92	1.963788
18	1.255273	43	1.633468	68	1.832509	93	1.968483
19	1.278754	44	1.643453	69	1.838849	94	1.973128
20	1.301030	45	1.653213	70	1.845098	95	1.977724
21	1.322219	46	1.662758	71	1.851258	96	1.982271
22	1.342423	47	1.672098	72	1.857333	97	1.986772
23	1.361728	48	1.681241	73	1.863323	98	1.991226
24	1.380211	49	1.690196	74	1.869232	99	1.995635
25	1.397940	50	1.698970	75	1.875061	100	2.000000

REMARK. In the following table, in the nine right hand columns of each page, where the first or leading figures change from 9's to 0's, points or dots are introduced in stead of the 0's, to catch the eye, and to indicate that from thence the two figures of the Logarithm to be taken from the second column, stand in the next line below.

N.	0	1	2	3	4	5	6	7	8	9	D.
100	000000	0434	0868	1301	1734	2166	2598	3029	3461	3891	432
101	4321	4751	5181	5609	6038	6466	6894	7321	7748	8174	428
102	8600	9026	9451	9876	•300	•724	1147	1570	1993	2415	424
103	012837	3259	3680	4100	4521	4940	5360	5779	6197	6616	419
104	7033	7451	7868	8284	8700	9116	9532	9947	•361	•775	416
105	021189	1603	2016	2428	2841	3252	3664	4075	4486	4896	412
106	5306	5715	6125	6533	6942	7350	7757	8164	8571	8978	408
107	9384	9789	•195	•600	1004	1408	1812	2216	2619	3021	404
108	033424	3826	4227	4628	5029	5430	5830	6230	6629	7028	400
109	7426	7825	8223	8620	9017	9414	9811	•207	•602	•998	396
110	041393	1787	2182	2576	2969	3362	3755	4148	4540	4932	393
111	5323	5714	6105	6495	6885	7275	7664	8053	8442	8830	389
112	9218	9606	9993	•380	•766	1153	1538	1924	2309	2694	386
113	053078	3463	3846	4230	4613	4996	5378	5760	6142	6524	382
114	6905	7286	7666	8046	8426	8805	9185	9563	9942	•320	379
115	060698	1075	1452	1829	2206	2582	2958	3333	3709	4083	376
116	4458	4832	5206	5580	5953	6326	6699	7071	7443	7815	372
117	8186	8557	8928	9298	9668	••38	•407	•776	1145	1514	369
118	071882	2250	2617	2985	3352	3718	4085	4451	4816	5182	366
119	5547	5912	6276	6640	7004	7368	7731	8094	8457	8819	363
120	079181	9543	9904	•266	•626	•987	1347	1707	2067	2426	360
121	082785	3144	3503	3861	4219	4576	4934	5291	5647	6004	357
122	6360	6716	7071	7426	7781	8136	8490	8845	9198	9552	355
123	9905	•258	•611	•963	1315	1667	2018	2370	2721	3071	351
124	093422	3772	4122	4471	4820	5169	5518	5866	6215	6562	349
125	6910	7257	7604	7951	8298	8644	8990	9335	9681	••26	346
126	100371	0715	1059	1403	1747	2091	2434	2777	3119	3462	343
127	3804	4146	4487	4828	5169	5510	5851	6191	6531	6871	340
128	7210	7549	7888	8227	8565	8903	9241	9579	9916	•253	338
129	110590	0926	1263	1599	1934	2270	2605	2940	3275	3609	335
130	113943	4277	4611	4944	5278	5611	5943	6276	6608	6940	333
131	7271	7603	7934	8265	8595	8926	9256	9586	9915	•245	330
132	120574	0903	1231	1560	1888	2216	2544	2871	3198	3525	328
133	3852	4178	4504	4830	5156	5481	5806	6131	6456	6781	325
134	7105	7429	7753	8076	8399	8722	9045	9368	9690	••12	323
135	130334	0655	0977	1298	1619	1939	2260	2580	2900	3219	321
136	3539	3858	4177	4496	4814	5133	5451	5769	6086	6403	318
137	6721	7037	7354	7671	7987	8303	8618	8934	9249	9564	315
138	9879	•194	•508	•822	1136	1450	1763	2076	2389	2702	314
139	143015	3327	3639	3951	4263	4574	4885	5196	5507	5818	311
140	146128	6438	6748	7058	7367	7676	7985	8294	8603	8911	309
141	9219	9527	9835	•142	•449	•756	1063	1370	1676	1982	307
142	152288	2594	2900	3205	3510	3815	4120	4424	4728	5032	305
143	5336	5640	5943	6246	6549	6852	7154	7457	7759	8061	303
144	8362	8664	8965	9266	9567	9868	•168	•469	•769	1068	301
145	161368	1667	1967	2266	2564	2863	3161	3460	3758	4055	299
146	4353	4650	4947	5244	5541	5838	6134	6430	6726	7022	297
147	7317	7613	7908	8203	8497	8792	9086	9380	9674	9968	295
148	170262	0555	0848	1141	1434	1726	2019	2311	2603	2895	293
149	3186	3478	3769	4060	4351	4641	4932	5222	5512	5802	291
150	176091	6381	6670	6959	7248	7536	7825	8113	8401	8689	289
151	8977	9264	9552	9839	•126	•413	•699	•985	1272	1558	287
152	181844	2129	2415	2700	2985	3270	3555	3839	4123	4407	285
153	4691	4975	5259	5542	5825	6108	6391	6674	6956	7239	283
154	7521	7803	8084	8366	8647	8928	9209	9490	9771	••51	281
155	190332	0612	0892	1171	1451	1730	2010	2289	2567	2846	279
156	3125	3403	3681	3959	4237	4514	4792	5069	5346	5623	278
157	5899	6176	6453	6729	7005	7281	7556	7832	8107	8382	276
158	8657	8932	9206	9481	9755	••29	•303	•577	•850	1124	274
159	201397	1670	1943	2216	2488	2761	3033	3305	3577	3848	272
N.	0	1	2	3	4	5	6	7	8	9	D.

N.	0	1	2	3	4	5	6	7	8	9	D.
160	204120	4391	4663	4934	5204	5475	5746	6016	6286	6556	271
161	6826	7096	7365	7634	7904	8173	8441	8710	8979	9247	269
162	9515	9783	••51	•319	•586	•853	1121	1388	1654	1921	267
163	212188	2454	2720	2986	3252	3518	3783	4049	4314	4579	266
164	4844	5109	5373	5638	5902	6166	6430	6694	6957	7221	264
165	7484	7747	8010	8273	8536	8798	9060	9323	9585	9846	262
166	220108	0370	0631	0892	1153	1414	1675	1936	2196	2456	261
167	2716	2976	3236	3496	3755	4015	4274	4533	4792	5051	259
168	5309	5568	5826	6084	6342	6600	6858	7115	7372	7630	258
169	7887	8144	8400	8657	8913	9170	9426	9682	9938	•193	256
170	230449	0704	0960	1215	1470	1724	1979	2234	2488	2742	254
171	2996	3250	3504	3757	4011	4264	4517	4770	5023	5276	253
172	5528	5781	6033	6285	6537	6789	7041	7292	7544	7795	252
173	8046	8297	8548	8799	9049	9299	9550	9800	••50	•300	250
174	240549	0799	1048	1297	1546	1795	2044	2293	2541	2790	249
175	3038	3286	3534	3782	4030	4277	4525	4772	5019	5266	248
176	5513	5759	6006	6252	6499	6745	6991	7237	7482	7728	246
177	7973	8219	8464	8709	8954	9198	9443	9687	9932	•176	245
178	250420	0664	0908	1151	1395	1638	1881	2125	2368	2610	243
179	2853	3096	3338	3580	3822	4064	4306	4548	4790	5031	242
180	255273	5514	5755	5996	6237	6477	6718	6958	7198	7439	241
181	7679	7918	8158	8398	8637	8877	9116	9355	9594	9833	239
182	260071	0310	0548	0787	1025	1263	1501	1739	1976	2214	238
183	2451	2688	2925	3162	3399	3636	3873	4109	4346	4582	237
184	4818	5054	5290	5525	5761	5996	6232	6467	6702	6937	235
185	7172	7406	7641	7875	8110	8344	8578	8812	9046	9279	234
186	9513	9746	9980	•213	•446	•679	•912	1144	1377	1609	233
187	271842	2074	2306	2538	2770	3001	3233	3464	3696	3927	232
188	4158	4389	4620	4850	5081	5311	5542	5772	6002	6232	230
189	6462	6692	6921	7151	7380	7609	7838	8067	8296	8525	229
190	278754	8982	9211	9439	9667	9895	•123	•351	•578	•806	228
191	281033	1261	1488	1715	1942	2169	2396	2622	2849	3075	227
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454	7056	7152	7247	7343	7438	7534	7629	7725	7820	7916	96
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798	2003	2057	2112	2166	2221	2275	2329	2384	2438	2492	54
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854	1458	1509	1560	1610	1661	1712	1763	1814	1865	1915	51
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856	2474	2524	2575	2626	2677	2727	2778	2829	2879	2930	51
857	2981	3031	3082	3133	3183	3234	3285	3335	3386	3437	51
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859	3993	4044	4094	4145	4195	4246	4296	4347	4397	4448	51
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865	7016	7066	7117	7167	7217	7267	7317	7367	7418	7468	50
866	7518	7568	7618	7668	7718	7769	7819	7869	7919	7969	50
867	8019	8069	8119	8169	8219	8269	8320	8370	8420	8470	50
868	8520	8570	8620	8670	8720	8770	8820	8870	8920	8970	50
869	9020	9070	9120	9170	9220	9270	9320	9369	9419	9469	50
870	939519	9569	9619	9669	9719	9769	9819	9869	9918	9968	50
871	940018	0068	0118	0168	0218	0267	0317	0367	0417	0467	50
872	0516	0566	0616	0666	0716	0765	0815	0865	0915	0964	50
873	1014	1064	1114	1163	1213	1263	1313	1362	1412	1462	50
874	1511	1561	1611	1660	1710	1760	1809	1859	1909	1958	50
875	2008	2058	2107	2157	2207	2256	2306	2355	2405	2455	50
876	2504	2554	2603	2653	2702	2752	2801	2851	2901	2950	50
877	3000	3049	3099	3148	3198	3247	3297	3346	3396	3445	50
878	3495	3544	3593	3643	3692	3742	3791	3841	3890	3939	50
879	3989	4038	4088	4137	4186	4236	4285	4335	4384	4433	50
N.	0	1	2	3	4	5	6	7	8	9	D.

N.	0	1	2	3	4	5	6	7	8	9	D.
880	944483	4532	4581	4631	4680	4729	4779	4828	4877	4927	49
881	4976	5025	5074	5124	5173	5222	5272	5321	5370	5419	49
882	5469	5518	5567	5616	5665	5715	5764	5813	5862	5912	49
883	5961	6010	6059	6108	6157	6207	6256	6305	6354	6403	49
884	6452	6501	6551	6600	6649	6698	6747	6796	6845	6894	49
885	6943	6992	7041	7090	7140	7189	7238	7287	7336	7385	49
886	7434	7483	7532	7581	7630	7679	7728	7777	7826	7875	49
887	7924	7973	8022	8071	8120	8169	8217	8266	8315	8364	49
888	8413	8462	8511	8560	8609	8657	8706	8755	8804	8853	49
889	8902	8951	8999	9048	9097	9146	9195	9244	9292	9341	49
890	949390	9439	9488	9536	9585	9634	9683	9731	9780	9829	49
891	9878	9926	9975	••24	••73	•121	•170	•219	•267	•316	49
892	950365	0414	0462	0511	0560	0608	0657	0706	0754	0803	49
893	0851	0900	0949	0997	1046	1095	1143	1192	1240	1289	49
894	1338	1386	1435	1483	1532	1580	1629	1677	1726	1775	49
895	1823	1872	1920	1969	2017	2066	2114	2163	2211	2260	48
896	2308	2356	2405	2453	2502	2550	2599	2647	2696	2744	48
897	2792	2841	2889	2938	2986	3034	3083	3131	3180	3228	48
898	3276	3325	3373	3421	3470	3518	3566	3615	3663	3711	48
899	3700	3808	3856	3905	3953	4001	4049	4098	4146	4194	48
900	954243	4291	4339	4387	4435	4484	4532	4580	4628	4677	48
901	4725	4773	4821	4869	4918	4966	5014	5062	5110	5158	48
902	5207	5255	5303	5351	5399	5447	5495	5543	5592	5640	48
903	5688	5736	5784	5832	5880	5928	5976	6024	6072	6120	48
904	6168	6216	6265	6313	6361	6409	6457	6505	6553	6601	48
905	6649	6697	6745	6793	6840	6888	6936	6984	7032	7080	48
906	7128	7176	7224	7272	7320	7368	7416	7464	7512	7559	48
907	7607	7655	7703	7751	7799	7847	7894	7942	7990	8038	48
908	8086	8134	8181	8229	8277	8325	8373	8421	8468	8516	48
909	8564	8612	8659	8707	8755	8803	8850	8898	8946	8994	48
910	959041	9089	9137	9185	9232	9280	9328	9375	9423	9471	48
911	9518	9566	9614	9661	9709	9757	9804	9852	9900	9947	48
912	9995	••42	••90	•138	•185	•233	•280	•328	•376	•423	48
913	960471	0518	0566	0613	0661	0709	0756	0804	0851	0899	48
914	0946	0994	1041	1089	1136	1184	1231	1279	1326	1374	47
915	1421	1469	1516	1563	1611	1658	1706	1753	1801	1848	47
916	1895	1943	1990	2038	2085	2132	2180	2227	2275	2322	47
917	2369	2417	2464	2511	2559	2606	2653	2701	2748	2795	47
918	2843	2890	2937	2985	3032	3079	3126	3174	3221	3268	47
919	3316	3363	3410	3457	3504	3552	3599	3646	3693	3741	47
920	963788	3835	3882	3929	3977	4024	4071	4118	4165	4212	47
921	4260	4307	4354	4401	4448	4495	4542	4590	4637	4684	47
922	4731	4778	4825	4872	4919	4966	5013	5061	5108	5155	47
923	5202	5249	5296	5343	5390	5437	5484	5531	5578	5625	47
924	5672	5719	5766	5813	5860	5907	5954	6001	6048	6095	47
925	6142	6189	6236	6283	6329	6376	6423	6470	6517	6564	47
926	6611	6658	6705	6752	6799	6845	6892	6939	6986	7033	47
927	7080	7127	7173	7220	7267	7314	7361	7408	7454	7501	47
928	7548	7595	7642	7688	7735	7782	7829	7875	7922	7969	47
929	8016	8062	8109	8156	8203	8249	8296	8343	8390	8436	47
930	968483	8530	8576	8623	8670	8716	8763	8810	8856	8903	47
931	8950	8996	9043	9090	9136	9183	9229	9276	9323	9369	47
932	9416	9463	9509	9556	9602	9649	9695	9742	9789	9835	47
933	9882	9928	9975	••21	••68	•114	•161	•207	•254	•300	47
934	970347	0393	0440	0486	0533	0579	0626	0672	0719	0765	46
935	0812	0858	0904	0951	0997	1044	1090	1137	1183	1229	46
936	1276	1322	1369	1415	1461	1508	1554	1601	1647	1693	46
937	1740	1786	1832	1879	1925	1971	2018	2064	2110	2157	46
938	2203	2249	2295	2342	2388	2434	2481	2527	2573	2619	46
939	2666	2712	2758	2804	2851	2897	2943	2989	3035	3082	46
N.	0	1	2	3	4	5	6	7	8	9	D.

N.	0	1	2	3	4	5	6	7	8	9	D.
940	973128	5174	3220	3266	3313	3359	3405	3451	3497	3543	46
941	3590	3636	3682	3728	3774	3820	3866	3913	3959	4005	46
942	4051	4097	4143	4189	4235	4281	4327	4374	4420	4466	46
943	4512	4558	4604	4650	4696	4742	4788	4834	4880	4926	46
944	4972	5018	5064	5110	5156	5202	5248	5294	5340	5386	46
945	5432	5478	5524	5570	5616	5662	5707	5753	5799	5845	46
946	5891	5937	5983	6029	6075	6121	6167	6212	6258	6304	46
947	6350	6396	6442	6488	6533	6579	6625	6671	6717	6763	46
948	6808	6854	6900	6946	6992	7037	7083	7129	7175	7220	46
949	7266	7312	7358	7403	7449	7495	7541	7586	7632	7678	46
950	977724	7769	7815	7861	7906	7952	7998	8043	8089	8135	46
951	8181	8226	8272	8317	8363	8409	8454	8500	8546	8591	46
952	8637	8683	8728	8774	8819	8865	8911	8956	9002	9047	46
953	9093	9138	9184	9230	9275	9321	9366	9412	9457	9503	46
954	9548	9594	9639	9685	9730	9776	9821	9867	9912	9958	46
955	980003	0049	0094	0140	0185	0231	0276	0322	0367	0412	45
956	0458	0503	0549	0594	0640	0685	0730	0776	0821	0867	45
957	0912	0957	1003	1048	1093	1139	1184	1229	1275	1320	45
958	1366	1411	1456	1501	1547	1592	1637	1683	1728	1773	45
959	1819	1864	1909	1954	2000	2045	2090	2135	2181	2226	45
960	982271	2316	2362	2407	2452	2497	2543	2588	2633	2678	45
961	2723	2769	2814	2859	2904	2949	2994	3040	3085	3130	45
962	3175	3220	3265	3310	3356	3401	3446	3491	3536	3581	45
963	3626	3671	3716	3762	3807	3852	3897	3942	3987	4032	45
964	4077	4122	4167	4212	4257	4302	4347	4392	4437	4482	45
965	4527	4572	4617	4662	4707	4752	4797	4842	4887	4932	45
966	4977	5022	5067	5112	5157	5202	5247	5292	5337	5382	45
967	5426	5471	5516	5561	5606	5651	5696	5741	5786	5830	45
968	5875	5920	5965	6010	6055	6100	6144	6189	6234	6279	45
969	6324	6369	6413	6458	6503	6548	6593	6637	6682	6727	45
970	986772	6817	6861	6906	6951	6996	7040	7085	7130	7175	45
971	7219	7264	7309	7353	7398	7443	7488	7532	7577	7622	45
972	7666	7711	7756	7800	7845	7890	7934	7979	8024	8068	45
973	8113	8157	8202	8247	8291	8336	8381	8425	8470	8514	45
974	8559	8604	8648	8693	8737	8782	8826	8871	8916	8960	45
975	9005	9049	9094	9138	9183	9227	9272	9316	9361	9405	45
976	9450	9494	9539	9583	9628	9672	9717	9761	9806	9850	44
977	9895	9939	9983	••28	••72	•117	•161	•206	•250	•294	44
978	990339	0383	0428	0472	0516	0561	0605	0650	0694	0738	44
979	0783	0827	0871	0916	0960	1004	1049	1093	1137	1182	44
980	991226	1270	1315	1359	1403	1448	1492	1536	1580	1625	44
981	1669	1713	1758	1802	1846	1890	1935	1979	2023	2067	44
982	2111	2156	2200	2244	2288	2333	2377	2421	2465	2509	44
983	2554	2598	2642	2686	2730	2774	2819	2863	2907	2951	44
984	2995	3039	3083	3127	3172	3216	3260	3304	3348	3392	44
985	3436	3480	3524	3568	3613	3657	3701	3745	3789	3833	44
986	3877	3921	3965	4009	4053	4097	4141	4185	4229	4273	44
987	4317	4361	4405	4449	4493	4537	4581	4625	4669	4713	44
988	4757	4801	4845	4889	4933	4977	5021	5065	5108	5152	44
989	5196	5240	5284	5328	5372	5416	5460	5504	5547	5591	44
990	995635	5679	5723	5767	5811	5854	5898	5942	5986	6030	44
991	6074	6117	6161	6205	6249	6293	6337	6380	6424	6468	44
992	6512	6555	6599	6643	6687	6731	6774	6818	6862	6906	44
993	6949	6993	7037	7080	7124	7168	7212	7255	7299	7343	44
994	7386	7430	7474	7517	7561	7605	7648	7692	7736	7779	44
995	7823	7867	7910	7954	7998	8041	8085	8129	8172	8216	44
996	8259	8303	8347	8390	8434	8477	8521	8564	8608	8652	44
997	8695	8739	8782	8826	8869	8913	8956	9000	9043	9087	44
998	9131	9174	9218	9261	9305	9348	9392	9435	9479	9522	44
999	9565	9609	9652	9696	9739	9783	9826	9870	9913	9957	43
N.	0	1	2	3	4	5	6	7	8	9	D.

A TABLE  
OF  
LOGARITHMIC  
SINES AND TANGENTS  
FOR EVERY  
DEGREE AND MINUTE  
OF THE QUADRANT.

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REMARK. The minutes in the left-hand column of each page, increasing downwards, belong to the degrees at the top; and those increasing upwards, in the right-hand column, belong to the degrees below.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0			10.000000		0.000000		Infinite.	60
1	6.463726	5017.17	000000	.00	6.463726	5017.17	13.536274	59
2	764756	2934.85	000000	.00	764756	2934.83	235244	58
3	940847	2082.31	000000	.00	940847	2082.31	059153	57
4	7.065786	1615.17	000000	.00	7.065786	1615.17	12.934214	56
5	162696	1319.68	000000	.00	162696	1319.69	837304	55
6	241877	1115.75	9.999999	.01	241878	1115.78	758122	54
7	308824	966.53	999999	.01	308825	996.53	691175	53
8	366816	852.54	999999	.01	366817	852.54	633183	52
9	417968	762.63	999999	.01	417970	762.63	582030	51
10	463725	689.88	999998	.01	463727	689.88	536273	50
11	7.505118	629.81	9.999998	.01	7.505120	629.81	12.494880	49
12	542906	579.36	999997	.01	542909	579.33	457091	48
13	577668	536.41	999997	.01	577672	536.42	422328	47
14	609853	499.38	999996	.01	609857	499.39	390143	46
15	639816	467.14	999996	.01	639820	467.15	360180	45
16	667845	438.81	999995	.01	667849	438.82	332151	44
17	694173	413.72	999995	.01	694179	413.73	305821	43
18	718997	391.35	999994	.01	719004	391.36	280997	42
19	742477	371.27	999993	.01	742484	371.28	257516	41
20	764754	353.15	999993	.01	764761	351.36	235239	40
21	7.785943	336.72	9.999992	.01	7.785951	336.73	12.214049	39
22	806146	321.75	999991	.01	806155	321.76	193845	38
23	825451	308.05	999990	.01	825460	308.06	174540	37
24	843934	295.47	999989	.02	843944	295.49	156056	36
25	861662	283.88	999988	.02	861674	283.90	138326	35
26	878695	273.17	999988	.02	878708	273.18	121292	34
27	895085	263.23	999987	.02	895099	263.25	104901	33
28	910879	253.99	999986	.02	910894	254.01	089106	32
29	926119	245.38	999985	.02	926134	245.40	073866	31
30	940842	237.33	999983	.02	940858	237.35	059142	30
31	7.955082	229.80	9.999982	.02	7.955100	229.81	12.044900	29
32	968870	222.73	999981	.02	968889	222.75	031111	28
33	982233	216.08	999980	.02	982253	216.10	017747	27
34	995198	209.81	999979	.02	995219	209.83	004781	26
35	8.007787	203.90	999977	.02	8.007809	203.92	11.992191	25
36	020021	198.31	999976	.02	020045	198.33	979955	24
37	031919	193.02	999975	.02	031945	193.05	968055	23
38	043501	188.01	999973	.02	043527	188.03	956473	22
39	054781	183.25	999972	.02	054809	183.27	945191	21
40	065776	178.72	999971	.02	065806	178.74	934194	20
41	8.076500	174.41	9.999969	.02	8.076531	174.44	11.923469	19
42	086965	170.31	999968	.02	086997	170.34	913003	18
43	097183	166.39	999966	.02	097217	166.42	902783	17
44	107167	162.65	999964	.03	107202	162.68	892797	16
45	116926	159.08	999963	.03	116963	159.10	883037	15
46	126471	155.66	999961	.03	126510	155.68	873490	14
47	135810	152.38	999959	.03	135851	152.41	864149	13
48	144953	149.24	999958	.03	144996	149.27	855004	12
49	153907	146.22	999955	.03	153952	146.27	846048	11
50	162681	143.33	999954	.03	162727	143.36	837273	10
51	8.171280	140.54	9.999952	.03	8.171328	140.57	11.828672	9
52	179713	137.86	999950	.03	179763	137.90	820237	8
53	187985	135.29	999948	.03	188036	135.32	811964	7
54	196102	132.80	999946	.03	196156	132.84	803844	6
55	204070	130.41	999944	.03	204126	130.44	795874	5
56	211895	128.10	999942	.04	211953	128.14	788047	4
57	219581	125.87	999940	.04	219641	125.90	780359	3
58	227134	123.72	999938	.04	227195	123.76	772805	2
59	234557	121.64	999936	.04	234621	121.68	765379	1
60	241855	119.63	999934	.04	241921	119.67	758079	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	8.241855	119.63	9.999934	.04	8.241921	119.67	11.758079	60
1	249033	117.68	999932	.04	249102	117.72	750898	59
2	256094	115.80	999929	.04	256165	115.84	743835	58
3	263042	113.98	999927	.04	263115	114.02	736885	57
4	269881	112.21	999925	.04	269956	112.25	730044	56
5	276614	110.50	999922	.04	276691	110.54	723309	55
6	283243	108.83	999920	.04	283323	108.87	716677	54
7	289773	107.21	999918	.04	289856	107.26	710144	53
8	296207	105.65	999915	.04	296292	105.70	703708	52
9	302546	104.13	999913	.04	302634	104.18	697366	51
10	308794	102.66	999910	.04	308884	102.70	691116	50
11	8.314904	101.22	9.999907	.04	8.315046	101.26	11.684954	49
12	321027	99.82	999905	.04	321122	99.87	678878	48
13	327016	98.47	999902	.04	327114	98.51	672886	47
14	332924	97.14	999899	.05	333025	97.19	666975	46
15	338753	95.86	999897	.05	338856	95.90	661144	45
16	344504	94.60	999894	.05	344610	94.65	655390	44
17	350181	93.38	999891	.05	350289	93.43	649711	43
18	355783	92.19	999888	.05	355895	92.24	644105	42
19	361315	91.03	999885	.05	361430	91.08	638570	41
20	366777	89.90	999882	.05	366892	89.95	633105	40
21	8.372171	88.80	9.999879	.05	8.372292	88.85	11.627708	39
22	377499	87.72	999876	.05	377622	87.77	622378	38
23	382762	86.67	999873	.05	382889	86.72	617111	37
24	387962	85.64	999870	.05	388092	85.70	611908	36
25	393101	84.64	999867	.05	393234	84.70	606766	35
26	398179	83.66	999864	.05	398315	83.71	601685	34
27	403199	82.71	999861	.05	403338	82.76	596662	33
28	408161	81.77	999858	.05	408304	81.82	591696	32
29	413068	80.86	999854	.05	413213	80.91	586787	31
30	417919	79.96	999851	.06	418068	80.02	581932	30
31	8.422717	79.09	9.999848	.06	8.422869	79.14	11.577131	29
32	427462	78.23	999844	.06	427618	78.30	572382	28
33	432156	77.40	999841	.06	432315	77.45	567685	27
34	436800	76.57	999838	.06	436962	76.63	563038	26
35	441394	75.77	999834	.06	441560	75.83	558440	25
36	445941	74.99	999831	.06	446110	75.05	553890	24
37	450440	74.22	999827	.06	450613	74.28	549387	23
38	454893	73.46	999823	.06	455070	73.52	544930	22
39	459301	72.73	999820	.06	459481	72.79	540519	21
40	463665	72.00	999816	.06	463849	72.06	536151	20
41	8.467985	71.29	9.999812	.06	8.468172	71.35	11.531828	19
42	472263	70.60	999809	.06	472454	70.66	527546	18
43	476498	69.91	999805	.06	476693	69.98	523307	17
44	480693	69.24	999801	.06	480892	69.31	519108	16
45	484848	68.59	999797	.07	485050	68.65	514950	15
46	488963	67.94	999793	.07	489170	68.01	510830	14
47	493040	67.31	999790	.07	493250	67.38	506750	13
48	497078	66.69	999786	.07	497293	66.76	502707	12
49	501080	66.08	999782	.07	501298	66.15	498702	11
50	505045	65.48	999778	.07	505267	65.55	494733	10
51	8.508974	64.89	9.999774	.07	8.509200	64.96	11.490800	9
52	512867	64.31	999769	.07	513098	64.39	486902	8
53	516726	63.75	999765	.07	516961	63.82	483039	7
54	520551	63.19	999761	.07	520790	63.26	479210	6
55	524343	62.64	999757	.07	524586	62.72	475414	5
56	528102	62.11	999753	.07	528349	62.18	471651	4
57	531828	61.58	999748	.07	532080	61.65	467920	3
58	535523	61.06	999744	.07	535779	61.13	464221	2
59	539186	60.55	999740	.07	539447	60.62	460553	1
60	542819	60.04	999735	.07	543084	60.12	456916	0
	Cosine	D.	Sine		Cotang.	D.	Tang	

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	8.542819	60.04	9.999735	.07	8.543084	60.12	11.456916	60
1	546422	59.55	999731	.07	546691	59.62	453309	59
2	549995	59.06	999726	.07	550268	59.14	449732	58
3	553539	58.58	999722	.08	553817	58.66	446183	57
4	557054	58.11	999717	.08	557336	58.19	442664	56
5	560540	57.65	999713	.08	560828	57.73	439172	55
6	563999	57.19	999708	.08	564291	57.27	435709	54
7	567431	56.74	999704	.08	567727	56.82	432273	53
8	570836	56.30	999699	.08	571137	56.38	428863	52
9	574214	55.87	999694	.08	574520	55.95	425480	51
10	577566	55.44	999689	.08	577877	55.52	422123	50
11	8.580892	55.02	9.999685	.08	8.581208	55.10	11.418792	49
12	584193	54.60	999680	.08	584514	54.68	415486	48
13	587469	54.19	999675	.08	587795	54.27	412205	47
14	590721	53.79	999670	.08	591051	53.87	408949	46
15	593948	53.39	999665	.08	594283	53.47	405717	45
16	597152	53.00	999660	.08	597492	53.08	402508	44
17	600332	52.61	999655	.08	600677	52.70	399323	43
18	603489	52.23	999650	.08	603839	52.32	396161	42
19	606623	51.86	999645	.09	606978	51.94	393022	41
20	609734	51.49	999640	.09	610094	51.58	389906	40
21	8.612823	51.12	9.999635	.09	8.613189	51.21	11.386811	39
22	615891	50.76	999629	.09	616262	50.85	383738	38
23	618937	50.41	999624	.09	619313	50.50	380687	37
24	621962	50.06	999619	.09	622343	50.15	377657	36
25	624965	49.72	999614	.09	625352	49.81	374648	35
26	627948	49.38	999608	.09	628340	49.47	371660	34
27	630911	49.04	999603	.09	631308	49.13	368692	33
28	633854	48.71	999597	.09	634256	48.80	365744	32
29	636776	48.39	999592	.09	637184	48.48	362816	31
30	639680	48.06	999586	.09	640093	48.16	359907	30
31	8.642563	47.75	9.999581	.09	8.642982	47.84	11.357018	29
32	645428	47.43	999575	.09	645853	47.53	354147	28
33	648274	47.12	999570	.09	648704	47.22	351296	27
34	651102	46.82	999564	.09	651537	46.91	348463	26
35	653911	46.52	999558	.10	654352	46.61	345648	25
36	656702	46.22	999553	.10	657149	46.31	342851	24
37	659475	45.92	999547	.10	659928	46.02	340072	23
38	662230	45.63	999541	.10	662689	45.73	337311	22
39	664968	45.35	999535	.10	665433	45.44	334567	21
40	667689	45.06	999529	.10	668160	45.26	331840	20
41	8.670393	44.79	9.999524	.10	8.670870	44.88	11.329130	19
42	673080	44.51	999518	.10	673563	44.61	326437	18
43	675751	44.24	999512	.10	676239	44.34	323761	17
44	678405	43.97	999506	.10	678900	44.17	321100	16
45	681043	43.70	999500	.10	681544	43.80	318456	15
46	683665	43.44	999493	.10	684172	43.54	315828	14
47	686272	43.18	999487	.10	686784	43.28	313216	13
48	688863	42.92	999481	.10	689381	43.03	310619	12
49	691438	42.67	999475	.10	691963	42.77	308037	11
50	693998	42.42	999469	.10	694529	42.52	305471	10
51	8.696543	42.17	9.999463	.11	8.697081	42.28	11.302919	9
52	699073	41.92	999456	.11	699617	42.03	300383	8
53	701589	41.68	999450	.11	702139	41.79	297861	7
54	704090	41.44	999443	.11	704646	41.55	295354	6
55	706577	41.21	999437	.11	707140	41.32	292860	5
56	709049	40.97	999431	.11	709618	41.08	290382	4
57	711507	40.74	999424	.11	712083	40.85	287917	3
58	713952	40.51	999418	.11	714534	40.62	285465	2
59	716383	40.29	999411	.11	716972	40.40	283028	1
60	718800	40.06	999404	.11	719396	40.17	280604	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.



M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	8.718800	40.06	9.999404	.11	8.719396	40.17	11.280604	60
1	721204	39.84	999398	.11	721806	39.95	278194	59
2	723595	39.62	999391	.11	724204	39.74	275796	58
3	725972	39.41	999384	.11	726588	39.52	273412	57
4	728337	39.19	999378	.11	728959	39.30	271041	56
5	730688	38.98	999371	.11	731317	39.09	268683	55
6	733027	38.77	999364	.12	733663	38.89	266337	54
7	735354	38.57	999357	.12	735996	38.68	264004	53
8	737667	38.36	999350	.12	738317	38.48	261683	52
9	739969	38.16	999343	.12	740626	38.27	259374	51
10	742259	37.96	999336	.12	742922	38.07	257078	50
11	8.744536	37.76	9.999329	.12	8.745207	37.87	11.254793	49
12	746802	37.56	999322	.12	747479	37.68	252521	48
13	749055	37.37	999315	.12	749740	37.49	250260	47
14	751297	37.17	999308	.12	751989	37.29	248011	46
15	753528	36.98	999301	.12	754227	37.10	245773	45
16	755747	36.79	999294	.12	756453	36.92	243547	44
17	757955	36.61	999286	.12	758668	36.73	241332	43
18	760151	36.42	999279	.12	760872	36.55	239128	42
19	762337	36.24	999272	.12	763065	36.36	236935	41
20	764511	36.06	999265	.12	765246	36.18	234754	40
21	8.766675	35.88	9.999257	.12	8.767417	36.00	11.232583	39
22	768828	35.70	999250	.13	769578	35.83	230422	38
23	770970	35.53	999242	.13	771727	35.65	228273	37
24	773101	35.35	999235	.13	773866	35.48	226134	36
25	775223	35.18	999227	.13	775995	35.31	224005	35
26	777333	35.01	999220	.13	778114	35.14	221886	34
27	779434	34.84	999212	.13	780222	34.97	219778	33
28	781524	34.67	999205	.13	782320	34.80	217680	32
29	783605	34.51	999197	.13	784408	34.64	215592	31
30	785675	34.31	999189	.13	786486	34.47	213514	30
31	8.787736	34.18	9.999181	.13	8.788554	34.31	11.211446	29
32	789787	34.02	999174	.13	790613	34.15	209387	28
33	791828	33.86	999166	.13	792662	33.99	207338	27
34	793859	33.70	999158	.13	794701	33.83	205299	26
35	795881	33.54	999150	.13	796731	33.68	203269	25
36	797894	33.39	999142	.13	798752	33.52	201248	24
37	799897	33.23	999134	.13	800763	33.37	199237	23
38	801892	33.08	999126	.13	802765	33.22	197235	22
39	803876	32.93	999118	.13	804758	33.07	195242	21
40	805852	32.78	999110	.13	806742	32.92	193258	20
41	8.807819	32.63	9.999102	.13	8.808717	32.78	11.191283	19
42	809777	32.49	999094	.14	810683	32.62	189317	18
43	811726	32.34	999086	.14	812641	32.48	187359	17
44	813667	32.19	999077	.14	814589	32.33	185411	16
45	815599	32.05	999069	.14	816529	32.19	183471	15
46	817522	31.91	999061	.14	818461	32.05	181539	14
47	819436	31.77	999053	.14	820384	31.91	179616	13
48	821343	31.63	999044	.14	822298	31.77	177702	12
49	823240	31.49	999036	.14	824205	31.63	175795	11
50	825130	31.35	999027	.14	826103	31.50	173897	10
51	8.827011	31.22	9.999019	.14	8.827992	31.36	11.172008	9
52	828884	31.08	999010	.14	829874	31.23	170126	8
53	830749	30.95	999002	.14	831748	31.10	168252	7
54	832607	30.82	998993	.14	833613	30.96	166387	6
55	834456	30.69	998984	.14	835471	30.83	164529	5
56	836297	30.56	998976	.14	837321	30.70	162679	4
57	838130	30.43	998967	.15	839163	30.57	160837	3
58	839956	30.30	998958	.15	840998	30.45	159002	2
59	841774	30.17	998950	.15	842825	30.32	157175	1
60	843585	30.00	998941	.15	844644	30.19	155356	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	8.843585	30.05	9.998941	.15	8.844644	30.19	11.155356	60
1	845387	29.02	998932	.15	846455	30.07	153545	59
2	847183	29.80	998923	.15	848260	29.95	151740	58
3	848971	29.67	998914	.15	850057	29.82	149943	57
4	850751	29.55	998905	.15	851846	29.70	148154	56
5	852525	29.43	998896	.15	853628	29.58	146372	55
6	854291	29.31	998887	.15	855403	29.46	144597	54
7	856049	29.19	998878	.15	857171	29.35	142829	53
8	857801	29.07	998869	.15	858932	29.23	141068	52
9	859546	28.96	998860	.15	860686	29.11	139314	51
10	861283	28.84	998851	.15	862433	29.00	137567	50
11	8.863014	28.73	9.998841	.15	8.864173	28.88	11.135827	49
12	864738	28.61	998832	.15	865906	28.77	134094	48
13	866455	28.50	998823	.16	867632	28.66	132368	47
14	868165	28.39	998813	.16	869351	28.54	130649	46
15	869868	28.28	998804	.16	871064	28.43	128936	45
16	871565	28.17	998795	.16	872770	28.32	127230	44
17	873255	28.06	998785	.16	874469	28.21	125531	43
18	874938	27.95	998776	.16	876162	28.11	123838	42
19	876615	27.86	998766	.16	877849	28.00	122151	41
20	878285	27.73	998757	.16	879529	27.89	120471	40
21	8.879949	27.63	9.998747	.16	8.881202	27.79	11.118798	39
22	881607	27.52	998738	.16	882869	27.68	117131	38
23	883258	27.42	998728	.16	884530	27.58	115470	37
24	884903	27.31	998718	.16	886185	27.47	113815	36
25	886542	27.21	998708	.16	887833	27.37	112167	35
26	888174	27.11	998699	.16	889476	27.27	110524	34
27	889801	27.00	998689	.16	891112	27.17	108888	33
28	891421	26.90	998679	.16	892742	27.07	107258	32
29	893035	26.80	998669	.17	894366	26.97	105634	31
30	894643	26.70	998659	.17	895984	26.87	104016	30
31	8.896246	26.60	9.998649	.17	8.897596	26.77	11.102404	29
32	897842	26.51	998639	.17	899203	26.67	100797	28
33	899432	26.41	998629	.17	900803	26.58	999197	27
34	901017	26.31	998619	.17	902398	26.48	997602	26
35	902596	26.22	998609	.17	903987	26.38	996013	25
36	904169	26.12	998599	.17	905570	26.29	994430	24
37	905736	26.03	998589	.17	907147	26.20	992853	23
38	907297	25.93	998578	.17	908719	26.10	991281	22
39	908853	25.84	998568	.17	910285	26.01	989715	21
40	910404	25.75	998558	.17	911846	25.92	988154	20
41	8.911949	25.66	9.998548	.17	8.913401	25.83	11.086599	19
42	913488	25.56	998537	.17	914951	25.74	986549	18
43	915022	25.47	998527	.17	916495	25.65	985005	17
44	916550	25.38	998516	.18	918034	25.56	983466	16
45	918073	25.29	998506	.18	919568	25.47	981932	15
46	919591	25.20	998495	.18	921096	25.38	979904	14
47	921103	25.12	998485	.18	922619	25.30	977381	13
48	922610	25.03	998474	.18	924136	25.21	975864	12
49	924112	24.94	998464	.18	925649	25.12	974351	11
50	925609	24.86	998453	.18	927156	25.03	972844	10
51	8.927100	24.77	9.998442	.18	8.928658	24.95	11.071342	9
52	928587	24.69	998431	.18	930155	24.86	969845	8
53	930068	24.60	998421	.18	931647	24.78	968353	7
54	931544	24.52	998410	.18	933134	24.70	966866	6
55	933015	24.43	998399	.18	934616	24.61	965384	5
56	934481	24.35	998388	.18	936093	24.53	963907	4
57	935942	24.27	998377	.18	937565	24.45	962435	3
58	937398	24.19	998366	.18	939032	24.37	960968	2
59	938850	24.11	998355	.18	940494	24.30	959506	1
60	940296	24.03	998344	.18	941952	24.21	958048	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	8.940296	24.03	9.998344	.19	8.941952	24.21	11.058048	60
1	941738	23.94	998333	.19	943404	24.13	056596	59
2	943174	23.87	998322	.19	944852	24.05	055148	58
3	944606	23.79	998311	.19	946295	23.97	053705	57
4	946034	23.71	998300	.19	947734	23.90	052266	56
5	947456	23.63	998289	.19	949168	23.82	050832	55
6	948874	23.55	998277	.19	950597	23.74	049403	54
7	950287	23.48	998266	.19	952021	23.66	047979	53
8	951696	23.40	998255	.19	953441	23.60	046559	52
9	953100	23.32	998243	.19	954856	23.51	045144	51
10	954499	23.25	998232	.19	956267	23.44	043733	50
11	8.955894	23.17	9.998220	.19	8.957674	23.37	11.042326	49
12	957284	23.10	998209	.19	959075	23.29	040925	48
13	958670	23.02	998197	.19	960473	23.23	039527	47
14	960052	22.95	998186	.19	961866	23.14	038134	46
15	961429	22.88	998174	.19	963255	23.07	036745	45
16	962801	22.80	998163	.19	964639	23.00	035361	44
17	964170	22.73	998151	.19	966019	22.93	033981	43
18	965534	22.66	998139	.20	967394	22.86	032606	42
19	966893	22.59	998128	.20	968766	22.79	031234	41
20	968249	22.52	998116	.20	970133	22.71	029867	40
21	8.969600	22.44	9.998104	.20	8.971496	22.65	11.028504	39
22	970947	22.38	998092	.20	972855	22.57	027145	38
23	972289	22.31	998080	.20	974209	22.51	025791	37
24	973628	22.24	998068	.20	975560	22.44	024440	36
25	974962	22.17	998056	.20	976906	22.37	023094	35
26	976293	22.10	998044	.20	978248	22.30	021752	34
27	977619	22.03	998032	.20	979586	22.23	020414	33
28	978941	21.97	998020	.20	980921	22.17	019079	32
29	980259	21.90	998008	.20	982251	22.10	017749	31
30	981573	21.83	997996	.20	983577	22.04	016423	30
31	8.982883	21.77	9.997985	.20	8.984899	21.97	11.015101	29
32	984189	21.70	997972	.20	986217	21.91	013783	28
33	985491	21.63	997959	.20	987532	21.84	012468	27
34	986789	21.57	997947	.20	988842	21.78	011158	26
35	988083	21.50	997935	.21	990149	21.71	009851	25
36	989374	21.44	997922	.21	991451	21.65	008549	24
37	990660	21.38	997910	.21	992750	21.58	007250	23
38	991943	21.31	997897	.21	994045	21.52	005955	22
39	993222	21.25	997885	.21	995337	21.46	004663	21
40	994497	21.19	997872	.21	996624	21.40	003376	20
41	8.995768	21.12	9.997860	.21	8.997908	21.34	11.002092	19
42	997036	21.06	997847	.21	999188	21.27	000812	18
43	998299	21.00	997835	.21	9.000465	21.21	10.999535	17
44	999560	20.94	997822	.21	001738	21.15	998262	16
45	9.000816	20.87	997809	.21	003007	21.09	996993	15
46	002069	20.82	997797	.21	004272	21.03	995728	14
47	003318	20.76	997784	.21	005534	20.97	994466	13
48	004563	20.70	997771	.21	006792	20.91	993208	12
49	005805	20.64	997758	.21	008047	20.85	991953	11
50	007044	20.58	997745	.21	009298	20.80	990702	10
51	9.008278	20.52	9.997732	.21	9.010546	20.74	10.989454	9
52	009510	20.46	997719	.21	011790	20.68	988210	8
53	010737	20.40	997706	.21	013031	20.62	986969	7
54	011962	20.34	997693	.22	014268	20.56	985732	6
55	013182	20.29	997680	.22	015502	20.51	984498	5
56	014400	20.23	997667	.22	016732	20.45	983268	4
57	015613	20.17	997654	.22	017959	20.40	982041	3
58	016824	20.12	997641	.22	019183	20.33	980817	2
59	018031	20.06	997628	.22	020403	20.28	979597	1
60	019235	20.00	997614	.22	021620	20.23	978380	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.019235	20.00	9.997614	.22	9.021620	20.23	10.978380	60
1	020435	19.05	997601	.22	022834	20.17	977166	59
2	021632	19.09	997588	.22	024044	20.11	975956	58
3	022825	19.84	997574	.22	025251	20.06	974749	57
4	024016	19.78	997561	.22	026455	20.00	973545	56
5	025203	19.73	997547	.22	027655	19.95	972345	55
6	026386	19.67	997534	.23	028852	19.90	971148	54
7	027567	19.62	997520	.23	030046	19.85	969954	53
8	028744	19.57	997507	.23	031237	19.79	968763	52
9	029918	19.51	997493	.23	032425	19.74	967575	51
10	031089	19.47	997480	.23	033609	19.69	966391	50
11	9.032257	19.41	9.997466	.23	9.034791	19.64	10.965209	49
12	033421	19.36	997452	.23	035969	19.58	964031	48
13	034582	19.30	997439	.23	037144	19.53	962856	47
14	035741	19.25	997425	.23	038316	19.48	961684	46
15	036896	19.20	997411	.23	039485	19.43	960515	45
16	038048	19.15	997397	.23	040651	19.38	959349	44
17	039197	19.10	997383	.23	041813	19.33	958187	43
18	040342	19.05	997369	.23	042973	19.28	957027	42
19	041485	18.99	997355	.23	044130	19.23	955870	41
20	042625	18.94	997341	.23	045284	19.18	954716	40
21	9.043762	18.89	9.997327	.24	9.046434	19.13	10.953566	39
22	044895	18.84	997313	.24	047582	19.08	952418	38
23	046026	18.79	997299	.24	048727	19.03	951273	37
24	047154	18.75	997285	.24	049869	18.98	950131	36
25	048279	18.70	997271	.24	051008	18.93	948992	35
26	049400	18.65	997257	.24	052144	18.89	947856	34
27	050519	18.60	997242	.24	053277	18.84	946723	33
28	051635	18.55	997228	.24	054407	18.79	945593	32
29	052749	18.50	997214	.24	055535	18.74	944465	31
30	053859	18.45	997199	.24	056659	18.70	943341	30
31	9.054966	18.41	9.997185	.24	9.057781	18.65	10.942219	29
32	056071	18.36	997170	.24	058900	18.69	941100	28
33	057172	18.31	997156	.24	060016	18.55	939984	27
34	058271	18.27	997141	.24	061130	18.51	938870	26
35	059367	18.22	997127	.24	062240	18.46	937760	25
36	060460	18.17	997112	.24	063348	18.42	936652	24
37	061551	18.13	997098	.24	064453	18.37	935547	23
38	062639	18.08	997083	.25	065556	18.33	934444	22
39	063724	18.04	997068	.25	066655	18.28	933345	21
40	064806	17.99	997053	.25	067752	18.24	932248	20
41	9.065885	17.94	9.997039	.25	9.068846	18.19	10.931154	19
42	066962	17.90	997024	.25	069938	18.15	930062	18
43	068036	17.86	997009	.25	071027	18.10	928973	17
44	069107	17.81	996994	.25	072113	18.06	927887	16
45	070176	17.77	996979	.25	073197	18.02	926803	15
46	071242	17.72	996964	.25	074278	17.97	925722	14
47	072306	17.68	996949	.25	075356	17.93	924644	13
48	073366	17.63	996934	.25	076432	17.89	923568	12
49	074424	17.59	996919	.25	077505	17.84	922495	11
50	075480	17.55	996904	.25	078576	17.80	921424	10
51	9.076533	17.50	9.996889	.25	9.079644	17.76	10.920356	9
52	077583	17.46	996874	.25	080710	17.72	919290	8
53	078631	17.42	996858	.25	081773	17.67	918227	7
54	079676	17.38	996843	.25	082833	17.63	917167	6
55	080719	17.33	996828	.25	083891	17.59	916109	5
56	081759	17.29	996812	.26	084947	17.55	915053	4
57	082797	17.25	996797	.26	086000	17.51	914000	3
58	083832	17.21	996782	.26	087050	17.47	912950	2
59	084864	17.17	996766	.26	088098	17.43	911902	1
60	085894	17.13	996751	.26	089144	17.38	910856	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.085894	17.13	9.996751	.26	9.089144	17.38	10.910856	60
1	086922	17.09	996735	.26	090187	17.34	909813	59
2	087947	17.04	996720	.26	091228	17.30	908772	58
3	088970	17.00	996704	.26	092266	17.27	907734	57
4	089990	16.96	996688	.26	093302	17.22	906698	56
5	091008	16.92	996673	.26	094336	17.19	905664	55
6	092024	16.88	996657	.26	095367	17.15	904633	54
7	093037	16.84	996641	.26	096395	17.11	903605	53
8	094047	16.80	996625	.26	097422	17.07	902578	52
9	095056	16.76	996610	.26	098446	17.03	901554	51
10	096062	16.73	996594	.26	099468	16.99	900532	50
11	9.097065	16.68	9.996578	.27	9.100487	16.95	10.899513	49
12	098066	16.65	996562	.27	101504	16.91	898496	48
13	099065	16.61	996546	.27	102519	16.87	897481	47
14	100062	16.57	996530	.27	103532	16.84	896468	46
15	101056	16.53	996514	.27	104542	16.80	895458	45
16	102048	16.49	996498	.27	105550	16.76	894450	44
17	103037	16.45	996482	.27	106556	16.72	893444	43
18	104025	16.41	996465	.27	107559	16.69	892441	42
19	105010	16.38	996449	.27	108560	16.65	891440	41
20	105992	16.34	996433	.27	109559	16.61	890441	40
21	9.106973	16.30	9.996417	.27	9.110556	16.58	10.889444	39
22	107951	16.27	996400	.27	111551	16.54	888449	38
23	108927	16.23	996384	.27	112543	16.50	887457	37
24	109901	16.19	996368	.27	113533	16.46	886467	36
25	110873	16.16	996351	.27	114521	16.43	885479	35
26	111842	16.12	996335	.27	115507	16.39	884493	34
27	112809	16.08	996318	.27	116491	16.36	883509	33
28	113774	16.05	996302	.28	117472	16.32	882528	32
29	114737	16.01	996285	.28	118452	16.29	881548	31
30	115698	15.97	996269	.28	119429	16.25	880571	30
31	9.116656	15.94	9.996252	.28	9.120404	16.22	10.879596	29
32	117613	15.90	996235	.28	121377	16.18	878623	28
33	118567	15.87	996219	.28	122348	16.15	877652	27
34	119519	15.83	996202	.28	123317	16.11	876683	26
35	120469	15.80	996185	.28	124284	16.07	875716	25
36	121417	15.76	996168	.28	125249	16.04	874751	24
37	122362	15.73	996151	.28	126211	16.01	873789	23
38	123306	15.69	996134	.28	127172	15.97	872828	22
39	124248	15.66	996117	.28	128130	15.94	871870	21
40	125187	15.62	996100	.28	129087	15.91	870913	20
41	9.126125	15.59	9.996083	.29	9.130041	15.87	10.869959	19
42	127060	15.56	996066	.29	130994	15.84	869006	18
43	127993	15.52	996049	.29	131944	15.81	868056	17
44	128925	15.49	996032	.29	132893	15.77	867107	16
45	129854	15.45	996015	.29	133839	15.74	866161	15
46	130781	15.42	995998	.29	134784	15.71	865216	14
47	131706	15.39	995980	.29	135726	15.67	864274	13
48	132630	15.35	995963	.29	136667	15.64	863333	12
49	133551	15.32	995946	.29	137605	15.61	862395	11
50	134470	15.29	995928	.29	138542	15.58	861458	10
51	9.135387	15.25	9.995911	.29	9.139476	15.55	10.860524	9
52	136303	15.22	995894	.29	140409	15.51	859591	8
53	137216	15.19	995876	.29	141340	15.48	858660	7
54	138128	15.16	995859	.29	142269	15.45	857731	6
55	139037	15.12	995841	.29	143196	15.42	856804	5
56	139944	15.09	995823	.29	144121	15.39	855879	4
57	140850	15.06	995806	.29	145044	15.35	854956	3
58	141754	15.03	995788	.29	145966	15.32	854034	2
59	142655	15.00	995771	.29	146885	15.29	853115	1
60	143555	14.96	995753	.29	147803	15.26	852197	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.143555	14.96	9.995753	.30	9.147803	15.26	10.852197	60
1	144453	14.93	995735	.30	148718	15.23	851282	59
2	145349	14.90	995717	.30	149632	15.20	850368	58
3	146243	14.87	995699	.30	150544	15.17	849456	57
4	147136	14.84	995681	.30	151454	15.14	848546	56
5	148026	14.81	995664	.30	152363	15.11	847637	55
6	148915	14.78	995646	.30	153269	15.08	846731	54
7	149802	14.75	995628	.30	154174	15.05	845826	53
8	150686	14.72	995610	.30	155077	15.02	844923	52
9	151569	14.69	995591	.30	155978	14.99	844022	51
10	152451	14.66	995573	.30	156877	14.96	843123	50
11	9.153330	14.63	9.995555	.30	9.157775	14.93	10.842225	49
12	154208	14.60	995537	.30	158671	14.90	841326	48
13	155083	14.57	995519	.30	159565	14.87	840435	47
14	155957	14.54	995501	.31	160457	14.84	839543	46
15	156830	14.51	995482	.31	161347	14.81	838653	45
16	157700	14.48	995464	.31	162236	14.79	837764	44
17	158569	14.45	995446	.31	163123	14.76	836877	43
18	159435	14.42	995427	.31	164008	14.73	835992	42
19	160301	14.39	995409	.31	164892	14.70	835108	41
20	161164	14.36	995390	.31	165774	14.67	834226	40
21	9.162025	14.33	9.995372	.31	9.166654	14.64	10.833346	39
22	162885	14.30	995353	.31	167532	14.61	832468	38
23	163743	14.27	995334	.31	168409	14.58	831591	37
24	164600	14.24	995316	.31	169284	14.55	830716	36
25	165454	14.22	995297	.31	170157	14.53	829843	35
26	166307	14.19	995278	.31	171029	14.50	828971	34
27	167159	14.16	995260	.31	171899	14.47	828101	33
28	168008	14.13	995241	.32	172767	14.44	827233	32
29	168856	14.10	995222	.32	173634	14.42	826366	31
30	169702	14.07	995203	.32	174499	14.39	825501	30
31	9.170547	14.05	9.995184	.32	9.175362	14.36	10.824638	29
32	171389	14.02	995165	.32	176224	14.33	823776	28
33	172230	13.99	995146	.32	177084	14.31	822916	27
34	173070	13.96	995127	.32	177942	14.28	822058	26
35	173908	13.94	995108	.32	178799	14.25	821201	25
36	174744	13.91	995089	.32	179655	14.23	820345	24
37	175578	13.88	995070	.32	180508	14.20	819492	23
38	176411	13.86	995051	.32	181360	14.17	818640	22
39	177242	13.83	995032	.32	182211	14.15	817789	21
40	178072	13.80	995013	.32	183059	14.12	816941	20
41	9.178900	13.77	9.994993	.32	9.183907	14.09	10.816093	19
42	179726	13.74	994974	.32	184752	14.07	815248	18
43	180551	13.72	994955	.32	185597	14.04	814403	17
44	181374	13.69	994935	.32	186439	14.02	813561	16
45	182196	13.66	994916	.33	187280	13.99	812720	15
46	183016	13.64	994896	.33	188120	13.96	811880	14
47	183834	13.61	994877	.33	188958	13.93	811042	13
48	184651	13.59	994857	.33	189794	13.91	810206	12
49	185466	13.56	994838	.33	190629	13.89	809371	11
50	186280	13.53	994818	.33	191462	13.86	808538	10
51	9.187092	13.51	9.994798	.33	9.192294	13.84	10.807706	9
52	187903	13.48	994779	.33	193124	13.81	806876	8
53	188712	13.46	994759	.33	193953	13.79	806047	7
54	189519	13.43	994739	.33	194780	13.76	805220	6
55	190325	13.41	994719	.33	195606	13.74	804394	5
56	191130	13.38	994700	.33	196430	13.71	803570	4
57	191933	13.36	994680	.33	197253	13.69	802747	3
58	192734	13.33	994660	.33	198074	13.66	801926	2
59	193534	13.30	994640	.33	198894	13.64	801106	1
60	194332	13.28	994620	.33	199713	13.61	800287	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.194332	13.28	9.994620	.33	9.199713	13.61	10.800287	60
1	195129	13.26	994600	.33	200529	13.59	799471	59
2	195925	13.23	994580	.33	201345	13.56	798655	58
3	196719	13.21	994560	.34	202159	13.54	797841	57
4	197511	13.18	994540	.34	202971	13.52	797029	56
5	198302	13.16	994519	.34	203782	13.49	796218	55
6	199091	13.13	994499	.34	204592	13.47	795408	54
7	199879	13.11	994479	.34	205400	13.45	794600	53
8	200666	13.08	994459	.34	206207	13.42	793793	52
9	201451	13.06	994438	.34	207013	13.40	792987	51
10	202234	13.04	994418	.34	207817	13.38	792183	50
11	9.203017	13.01	9.994397	.34	9.208619	13.35	10.791381	49
12	203797	12.99	994377	.34	209420	13.33	790580	48
13	204577	12.96	994357	.34	210220	13.31	789780	47
14	205354	12.94	994336	.34	211018	13.28	788982	46
15	206131	12.92	994316	.34	211815	13.26	788185	45
16	206906	12.89	994295	.34	212611	13.24	787389	44
17	207679	12.87	994274	.35	213405	13.21	786595	43
18	208452	12.85	994254	.35	214198	13.19	785802	42
19	209222	12.82	994233	.35	214989	13.17	785011	41
20	209992	12.80	994212	.35	215780	13.15	784220	40
21	9.210760	12.78	9.994191	.35	9.216568	13.12	10.783432	39
22	211526	12.75	994171	.35	217356	13.10	782644	38
23	212291	12.73	994150	.35	218142	13.08	781858	37
24	213055	12.71	994129	.35	218926	13.05	781074	36
25	213818	12.68	994108	.35	219710	13.03	780290	35
26	214579	12.66	994087	.35	220492	13.01	779508	34
27	215338	12.64	994066	.35	221272	12.99	778728	33
28	216097	12.61	994045	.35	222052	12.97	777948	32
29	216854	12.59	994024	.35	222830	12.94	777170	31
30	217609	12.57	994003	.35	223606	12.92	776394	30
31	9.218363	12.55	9.993981	.35	9.224382	12.90	10.775618	29
32	219116	12.53	993960	.35	225156	12.88	774844	28
33	219868	12.50	993939	.35	225929	12.86	774071	27
34	220618	12.48	993918	.35	226700	12.84	773300	26
35	221367	12.46	993896	.36	227471	12.81	772529	25
36	222115	12.44	993875	.36	228239	12.79	771761	24
37	222861	12.42	993854	.36	229007	12.77	770993	23
38	223606	12.39	993832	.36	229773	12.75	770227	22
39	224349	12.37	993811	.36	230539	12.73	769461	21
40	225092	12.35	993789	.36	231302	12.71	768698	20
41	9.225833	12.33	9.993768	.36	9.232065	12.69	10.767935	19
42	226573	12.31	993746	.36	232826	12.67	767174	18
43	227311	12.28	993725	.36	233586	12.65	766414	17
44	228048	12.26	993703	.36	234345	12.62	765655	16
45	228784	12.24	993681	.36	235103	12.60	764897	15
46	229518	12.22	993660	.36	235859	12.58	764141	14
47	230252	12.20	993638	.36	236614	12.56	763386	13
48	230984	12.18	993616	.36	237368	12.54	762632	12
49	231714	12.16	993594	.37	238120	12.52	761880	11
50	232444	12.14	993572	.37	238872	12.50	761128	10
51	9.233172	12.12	9.993550	.37	9.239622	12.48	10.760378	9
52	233899	12.09	993528	.37	240371	12.46	759629	8
53	234625	12.07	993506	.37	241118	12.44	758882	7
54	235349	12.05	993484	.37	241865	12.42	758135	6
55	236073	12.03	993462	.37	242610	12.40	757390	5
56	236795	12.01	993440	.37	243354	12.38	756646	4
57	237515	11.99	993418	.37	244097	12.36	755903	3
58	238235	11.97	993396	.37	244839	12.34	755161	2
59	238953	11.95	993374	.37	245579	12.32	754421	1
60	239670	11.93	993351	.37	246319	12.30	753681	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.239670	11.93	9.993351	.37	9.246319	12.30	10.753681	60
1	240386	11.91	993329	.37	247057	12.28	752943	59
2	241101	11.89	993307	.37	247794	12.26	752206	58
3	241814	11.87	993285	.37	248530	12.24	751470	57
4	242526	11.85	993262	.37	249264	12.22	750736	56
5	243237	11.83	993240	.37	249998	12.20	750002	55
6	243947	11.81	993217	.38	250730	12.18	749270	54
7	244656	11.79	993195	.38	251461	12.17	748539	53
8	245363	11.77	993172	.38	252191	12.15	747809	52
9	246069	11.75	993149	.38	252920	12.13	747080	51
10	246775	11.73	993127	.38	253648	12.11	746352	50
11	9.247478	11.71	9.993104	.38	9.254374	12.09	10.745626	49
12	248181	11.69	993081	.38	255100	12.07	744900	48
13	248883	11.67	993059	.38	255824	12.05	744176	47
14	249583	11.65	993036	.38	256547	12.03	743453	46
15	250282	11.63	993013	.38	257269	12.01	742731	45
16	250980	11.61	992990	.38	257990	12.00	742010	44
17	251677	11.59	992967	.38	258710	11.98	741290	43
18	252373	11.58	992944	.38	259429	11.96	740571	42
19	253067	11.56	992921	.38	260146	11.94	739854	41
20	253761	11.54	992898	.38	260863	11.92	739137	40
21	9.254453	11.52	9.992875	.38	9.261578	11.90	10.738422	39
22	255144	11.50	992852	.38	262292	11.89	737708	38
23	255834	11.48	992829	.39	263005	11.87	736995	37
24	256523	11.46	992806	.39	263717	11.85	736283	36
25	257211	11.44	992783	.39	264428	11.83	735572	35
26	257898	11.42	992759	.39	265138	11.81	734862	34
27	258583	11.41	992736	.39	265847	11.79	734153	33
28	259268	11.39	992713	.39	266555	11.78	733445	32
29	259951	11.37	992690	.39	267261	11.76	732739	31
30	260633	11.35	992666	.39	267967	11.74	732033	30
31	9.261314	11.33	9.992643	.39	9.268671	11.72	10.731329	29
32	261994	11.31	992619	.39	269375	11.70	730625	28
33	262673	11.30	992596	.39	270077	11.69	729923	27
34	263351	11.28	992572	.39	270779	11.67	729221	26
35	264027	11.26	992549	.39	271479	11.65	728521	25
36	264703	11.24	992525	.39	272178	11.64	727822	24
37	265377	11.22	992501	.39	272876	11.62	727124	23
38	266051	11.20	992478	.40	273573	11.60	726427	22
39	266723	11.19	992454	.40	274269	11.58	725731	21
40	267395	11.17	992430	.40	274964	11.57	725036	20
41	9.268065	11.15	9.992406	.40	9.275658	11.55	10.724342	19
42	268734	11.13	992382	.40	276351	11.53	723649	18
43	269402	11.11	992359	.40	277043	11.51	722957	17
44	270069	11.10	992335	.40	277734	11.50	722266	16
45	270735	11.08	992311	.40	278424	11.48	721576	15
46	271400	11.06	992287	.40	279113	11.47	720887	14
47	272064	11.05	992263	.40	279801	11.45	720199	13
48	272726	11.03	992239	.40	280488	11.43	719512	12
49	273388	11.01	992214	.40	281174	11.41	718826	11
50	274049	10.99	992190	.40	281858	11.40	718142	10
51	9.274708	10.98	9.992166	.40	9.282542	11.38	10.717458	9
52	275367	10.96	992142	.40	283225	11.36	716775	8
53	276024	10.94	992117	.41	283907	11.35	716093	7
54	276681	10.92	992093	.41	284588	11.33	715412	6
55	277337	10.91	992069	.41	285268	11.31	714732	5
56	277991	10.89	992044	.41	285947	11.30	714053	4
57	278644	10.87	992020	.41	286624	11.28	713376	3
58	279297	10.86	991996	.41	287301	11.26	712699	2
59	279948	10.84	991971	.41	287977	11.25	712023	1
60	280599	10.82	991947	.41	288652	11.23	711348	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.



M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.280599	10.82	9.991947	.41	9.288652	11.23	10.711348	60
1	281248	10.81	991922	.41	289326	11.22	710674	59
2	281897	10.79	991897	.41	289999	11.20	710001	58
3	282544	10.77	991873	.41	290671	11.18	709329	57
4	283190	10.76	991848	.41	291342	11.17	708658	56
5	283836	10.74	991823	.41	292013	11.15	707987	55
6	284480	10.72	991799	.41	292682	11.14	707318	54
7	285124	10.71	991774	.42	293350	11.12	706650	53
8	285766	10.69	991749	.42	294017	11.11	705983	52
9	286408	10.67	991724	.42	294684	11.09	705316	51
10	287048	10.66	991699	.42	295349	11.07	704651	50
11	9.287687	10.64	9.991674	.42	9.296013	11.06	10.703987	49
12	288326	10.63	991649	.42	296677	11.04	703323	48
13	288964	10.61	991624	.42	297339	11.03	702661	47
14	289600	10.59	991599	.42	298001	11.01	701999	46
15	290236	10.58	991574	.42	298662	11.00	701338	45
16	290870	10.56	991549	.42	299322	10.98	700678	44
17	291504	10.54	991524	.42	299980	10.96	700020	43
18	292137	10.53	991498	.42	300638	10.95	699362	42
19	292768	10.51	991473	.42	301295	10.93	698705	41
20	293399	10.50	991448	.42	301951	10.92	698049	40
21	9.294029	10.48	9.991422	.42	9.302607	10.90	10.697393	39
22	294658	10.46	991397	.42	303261	10.89	696739	38
23	295286	10.45	991372	.43	303914	10.87	696086	37
24	295913	10.43	991346	.43	304567	10.86	695433	36
25	296539	10.42	991321	.43	305218	10.84	694782	35
26	297164	10.40	991295	.43	305869	10.83	694131	34
27	297788	10.39	991270	.43	306519	10.81	693481	33
28	298412	10.37	991244	.43	307168	10.80	692832	32
29	299034	10.36	991218	.43	307815	10.78	692185	31
30	299655	10.34	991193	.43	308463	10.77	691537	30
31	9.300276	10.32	9.991167	.43	9.309109	10.75	10.690891	29
32	300895	10.31	991141	.43	309754	10.74	690246	28
33	301514	10.29	991115	.43	310398	10.73	689602	27
34	302132	10.28	991090	.43	311042	10.71	688958	26
35	302748	10.26	991064	.43	311685	10.70	688315	25
36	303364	10.25	991038	.43	312327	10.68	687673	24
37	303979	10.23	991012	.43	312967	10.67	687033	23
38	304593	10.22	990986	.43	313608	10.65	686392	22
39	305207	10.20	990960	.43	314247	10.64	685753	21
40	305819	10.19	990934	.44	314885	10.62	685115	20
41	9.306430	10.17	9.990908	.44	9.315523	10.61	10.684477	19
42	307041	10.16	990882	.44	316159	10.60	683841	18
43	307650	10.14	990855	.44	316795	10.58	683205	17
44	308259	10.13	990829	.44	317430	10.57	682570	16
45	308867	10.11	990803	.44	318064	10.55	681936	15
46	309474	10.10	990777	.44	318697	10.54	681303	14
47	310080	10.08	990750	.44	319329	10.53	680671	13
48	310685	10.07	990724	.44	319961	10.51	680039	12
49	311289	10.05	990697	.44	320592	10.50	679408	11
50	311893	10.04	990671	.44	321222	10.48	678778	10
51	9.312495	10.03	9.990644	.44	9.321851	10.47	10.678149	9
52	313097	10.01	990618	.44	322479	10.45	677521	8
53	313698	10.00	990591	.44	323106	10.44	676894	7
54	314297	9.98	990565	.44	323733	10.43	676267	6
55	314897	9.97	990538	.44	324358	10.41	675642	5
56	315495	9.96	990511	.45	324983	10.40	675017	4
57	316092	9.94	990485	.45	325607	10.39	674393	3
58	316689	9.93	990458	.45	326231	10.37	673769	2
59	317284	9.91	990431	.45	326853	10.36	673147	1
60	317879	9.90	990404	.45	327475	10.35	672525	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.317879	9.00	9.990404	.45	9.327474	10.35	10.672526	60
1	318473	9.88	990378	.45	328095	10.33	671905	59
2	319066	9.87	990351	.45	328715	10.32	671285	58
3	319658	9.86	990324	.45	329334	10.30	670666	57
4	320249	9.84	990297	.45	329953	10.29	670047	56
5	320840	9.83	990270	.45	330570	10.28	669430	55
6	321430	9.82	990243	.45	331187	10.26	668813	54
7	322019	9.80	990215	.45	331803	10.25	668197	53
8	322607	9.79	990188	.45	332418	10.24	667582	52
9	323194	9.77	990161	.45	333033	10.23	666967	51
10	323780	9.76	990134	.45	333646	10.21	666354	50
11	9.324366	9.75	9.990107	.46	9.334259	10.20	10.665741	49
12	324950	9.73	990079	.46	334871	10.19	665129	48
13	325534	9.72	990052	.46	335482	10.17	664518	47
14	326117	9.70	990025	.46	336093	10.16	663907	46
15	326700	9.69	989997	.46	336702	10.15	663298	45
16	327281	9.68	989970	.46	337311	10.13	662689	44
17	327862	9.66	989942	.46	337919	10.12	662081	43
18	328442	9.65	989915	.46	338527	10.11	661473	42
19	329021	9.64	989887	.46	339133	10.10	660867	41
20	329599	9.62	989860	.46	339739	10.08	660261	40
21	9.330176	9.61	9.989832	.46	9.340344	10.07	10.659656	39
22	330753	9.60	989804	.46	340948	10.06	659052	38
23	331329	9.58	989777	.46	341552	10.04	658448	37
24	331903	9.57	989749	.47	342155	10.03	657845	36
25	332478	9.56	989721	.47	342757	10.02	657243	35
26	333051	9.54	989693	.47	343358	10.00	656642	34
27	333624	9.53	989665	.47	343958	9.99	656042	33
28	334195	9.52	989637	.47	344558	9.98	655442	32
29	334766	9.50	989609	.47	345157	9.97	654843	31
30	335337	9.49	989582	.47	345755	9.96	654245	30
31	9.335906	9.48	9.989553	.47	9.346353	9.94	10.653647	29
32	336475	9.46	989525	.47	346949	9.93	653051	28
33	337043	9.45	989497	.47	347545	9.92	652455	27
34	337610	9.44	989469	.47	348141	9.91	651859	26
35	338176	9.43	989441	.47	348735	9.90	651265	25
36	338742	9.41	989413	.47	349329	9.88	650671	24
37	339306	9.40	989384	.47	349922	9.87	650078	23
38	339871	9.39	989356	.47	350514	9.86	649486	22
39	340434	9.37	989328	.47	351107	9.85	648894	21
40	340996	9.36	989300	.47	351697	9.83	648303	20
41	9.341558	9.35	9.989271	.47	9.352287	9.82	10.647713	19
42	342119	9.34	989243	.47	352876	9.81	647124	18
43	342679	9.32	989214	.47	353465	9.80	646535	17
44	343239	9.31	989186	.47	354053	9.79	645947	16
45	343797	9.30	989157	.47	354640	9.77	645360	15
46	344355	9.29	989128	.48	355227	9.76	644773	14
47	344912	9.27	989100	.48	355813	9.75	644187	13
48	345469	9.26	989071	.48	356398	9.74	643602	12
49	346024	9.25	989042	.48	356982	9.73	643018	11
50	346579	9.24	989014	.48	357566	9.71	642434	10
51	9.347134	9.22	9.988985	.48	9.358149	9.70	10.641851	9
52	347687	9.21	988956	.48	358731	9.69	641269	8
53	348240	9.20	988927	.48	359313	9.68	640687	7
54	348792	9.19	988898	.48	359893	9.67	640107	6
55	349343	9.17	988869	.48	360474	9.66	639526	5
56	349893	9.16	988840	.48	361053	9.65	638947	4
57	350443	9.15	988811	.49	361632	9.63	638368	3
58	350992	9.14	988782	.49	362210	9.62	637790	2
59	351540	9.13	988753	.49	362787	9.61	637213	1
60	352088	9.11	988724	.49	363364	9.60	636636	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.352088	9.11	9.987724	.49	9.363364	9.60	10.636636	60
1	352635	9.10	988695	.49	363940	9.59	636060	59
2	353181	9.09	988666	.49	364515	9.58	635485	58
3	353726	9.08	988636	.49	365090	9.57	634910	57
4	354271	9.07	988607	.49	365664	9.55	634336	56
5	354815	9.05	988578	.49	366237	9.54	633763	55
6	355358	9.04	988548	.49	366810	9.53	633190	54
7	355901	9.03	988519	.49	367382	9.52	632618	53
8	356443	9.02	988489	.49	367953	9.51	632047	52
9	356984	9.01	988460	.49	368524	9.50	631476	51
10	357524	8.99	988430	.49	369094	9.49	630906	50
11	9.358064	8.98	9.988401	.49	9.369663	9.48	10.630337	49
12	358603	8.97	988371	.49	370232	9.46	629768	48
13	359141	8.96	988342	.49	370799	9.45	629201	47
14	359678	8.95	988312	.50	371367	9.44	628633	46
15	360215	8.93	988282	.50	371933	9.43	628067	45
16	360752	8.92	988252	.50	372499	9.42	627501	44
17	361287	8.91	988223	.50	373064	9.41	626936	43
18	361822	8.90	988193	.50	373629	9.40	626371	42
19	362356	8.89	988163	.50	374193	9.39	625807	41
20	362889	8.88	988133	.50	374756	9.38	625244	40
21	9.363422	8.87	9.988103	.50	9.375319	9.37	10.624681	39
22	363954	8.85	988073	.50	375881	9.35	624119	38
23	364485	8.84	988043	.50	376442	9.34	623558	37
24	365016	8.83	988013	.50	377003	9.33	622997	36
25	365546	8.82	987983	.50	377563	9.32	622437	35
26	366075	8.81	987953	.50	378122	9.31	621878	34
27	366604	8.80	987922	.50	378681	9.30	621319	33
28	367131	8.79	987892	.50	379239	9.29	620761	32
29	367659	8.77	987862	.50	379797	9.28	620203	31
30	368185	8.76	987832	.51	380354	9.27	619646	30
31	9.368711	8.75	9.987801	.51	9.380910	9.26	10.619090	29
32	369236	8.74	987771	.51	381466	9.25	618534	28
33	369761	8.73	987740	.51	382020	9.24	617980	27
34	370285	8.72	987710	.51	382575	9.23	617425	26
35	370808	8.71	987679	.51	383129	9.22	616871	25
36	371330	8.70	987649	.51	383682	9.21	616318	24
37	371852	8.69	987618	.51	384234	9.20	615766	23
38	372373	8.67	987588	.51	384786	9.19	615214	22
39	372894	8.66	987557	.51	385337	9.18	614663	21
40	373414	8.65	987526	.51	385888	9.17	614112	20
41	9.373933	8.64	9.987496	.51	9.386438	9.15	10.613562	19
42	374452	8.63	987465	.51	386987	9.14	613013	18
43	374970	8.62	987434	.51	387536	9.13	612464	17
44	375487	8.61	987403	.52	388084	9.12	611916	16
45	376003	8.60	687372	.52	388631	9.11	611369	15
46	376519	8.59	987341	.52	389178	9.10	610822	14
47	377035	8.58	987310	.52	389724	9.09	610276	13
48	377549	8.57	987279	.52	390270	9.08	609730	12
49	378063	8.56	987248	.52	390815	9.07	609185	11
50	378577	8.54	987217	.52	391360	9.06	608640	10
51	9.379089	8.53	9.987186	.52	9.391903	9.05	10.608097	9
52	379601	8.52	987155	.52	392447	9.04	607553	8
53	380113	8.51	987124	.52	392989	9.03	607011	7
54	380624	8.50	987092	.52	393531	9.02	606469	6
55	381134	8.49	987061	.52	394073	9.01	605927	5
56	381643	8.48	987030	.52	394614	9.00	605386	4
57	382152	8.47	986998	.52	395154	8.99	604846	3
58	382661	8.46	986967	.52	395694	8.98	604306	2
59	383168	8.45	986936	.52	396233	8.97	603767	1
60	383675	8.44	986904	.52	396771	8.96	603229	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.383675	8.44	9.986904	.52	9.396771	8.96	10.603229	60
1	384182	8.43	986873	.53	397309	8.96	602691	59
2	384687	8.42	986841	.53	397846	8.95	602154	58
3	385192	8.41	986809	.53	398383	8.94	601617	57
4	385697	8.40	986778	.53	398919	8.93	601081	56
5	386201	8.39	986746	.53	399455	8.92	600545	55
6	386704	8.38	986714	.53	399990	8.91	600010	54
7	387207	8.37	986683	.53	400524	8.90	599476	53
8	387709	8.36	986651	.53	401058	8.89	598942	52
9	388210	8.35	986619	.53	401591	8.88	598409	51
10	388711	8.34	986587	.53	402124	8.87	597876	50
11	9.389211	8.33	9.986555	.53	9.402656	8.86	10.597344	49
12	389711	8.32	986523	.53	403187	8.85	596813	48
13	390210	8.31	986491	.53	403718	8.84	596282	47
14	390708	8.30	986459	.53	404249	8.83	595751	46
15	391206	8.28	986427	.53	404778	8.82	595222	45
16	391703	8.27	986395	.53	405308	8.81	594692	44
17	392199	8.26	986363	.54	405836	8.80	594164	43
18	392695	8.25	986331	.54	406364	8.79	593636	42
19	393191	8.24	986299	.54	406892	8.78	593108	41
20	393685	8.23	986266	.54	407419	8.77	592581	40
21	9.394179	8.22	9.986234	.54	9.407945	8.76	10.592055	39
22	394673	8.21	986202	.54	408471	8.75	591529	38
23	395166	8.20	986169	.54	408997	8.74	591003	37
24	395658	8.19	986137	.54	409521	8.74	590479	36
25	396150	8.18	986104	.54	410045	8.73	589955	35
26	396641	8.17	986072	.54	410569	8.72	589431	34
27	397132	8.17	986039	.54	411092	8.71	588908	33
28	397621	8.16	986007	.54	411615	8.70	588385	32
29	398111	8.15	985974	.54	412137	8.69	587863	31
30	398600	8.14	985942	.54	412658	8.68	587342	30
31	9.399088	8.13	9.985909	.55	9.413179	8.67	10.586821	29
32	399575	8.12	985876	.55	413699	8.66	586301	28
33	400062	8.11	985843	.55	414219	8.65	585781	27
34	400549	8.10	985811	.55	414738	8.64	585262	26
35	401035	8.09	985778	.55	415257	8.64	584743	25
36	401520	8.08	985745	.55	415775	8.63	584225	24
37	402005	8.07	985712	.55	416293	8.62	583707	23
38	402489	8.06	985679	.55	416810	8.61	583190	22
39	402972	8.05	985646	.55	417326	8.60	582674	21
40	403455	8.04	985613	.55	417842	8.59	582158	20
41	9.403938	8.03	9.985580	.55	9.418358	8.58	10.581642	19
42	404420	8.02	985547	.55	418873	8.57	581127	18
43	404901	8.01	985514	.55	419387	8.56	580613	17
44	405382	8.00	985480	.55	419901	8.55	580099	16
45	405862	7.99	985447	.55	420415	8.55	579585	15
46	406341	7.98	985414	.56	420927	8.54	579073	14
47	406820	7.97	985380	.56	421440	8.53	578560	13
48	407299	7.96	985347	.56	421952	8.52	578048	12
49	407777	7.95	985314	.56	422463	8.51	577537	11
50	408254	7.94	985280	.56	422974	8.50	577026	10
51	9.408731	7.94	9.985247	.56	9.423484	8.49	10.576516	9
52	409207	7.93	985213	.56	423993	8.48	576007	8
53	409682	7.92	985180	.56	424503	8.48	575497	7
54	410157	7.91	985146	.56	425011	8.47	574989	6
55	410632	7.90	985113	.56	425519	8.46	574481	5
56	411106	7.89	985079	.56	426027	8.45	573973	4
57	411579	7.88	985045	.56	426534	8.44	573466	3
58	412052	7.87	985011	.56	427041	8.43	572959	2
59	412524	7.86	984978	.56	427547	8.43	572453	1
60	412996	7.85	984944	.56	428052	8.42	571948	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.412996	7.85	9.984944	.57	9.428052	8.42	10.571948	60
1	413467	7.84	984910	.57	428557	8.41	571443	59
2	413938	7.83	984876	.57	429062	8.40	570938	58
3	414408	7.83	984842	.57	429566	8.39	570434	57
4	414878	7.82	984808	.57	430070	8.38	569930	56
5	415347	7.81	984774	.57	430573	8.38	569427	55
6	415815	7.80	984740	.57	431075	8.37	568925	54
7	416283	7.79	984706	.57	431577	8.36	568423	53
8	416751	7.78	984672	.57	432079	8.35	567921	52
9	417217	7.77	984637	.57	432580	8.34	567420	51
10	417684	7.76	984603	.57	433080	8.33	566920	50
11	9.418150	7.75	9.984569	.57	9.433580	8.32	10.566420	49
12	418615	7.74	984535	.57	434080	8.32	565920	48
13	419079	7.73	984500	.57	434579	8.31	565421	47
14	419544	7.73	984466	.57	435078	8.30	564922	46
15	420007	7.72	984432	.58	435576	8.29	564424	45
16	420470	7.71	984397	.58	436073	8.28	563927	44
17	420933	7.70	984363	.58	436570	8.28	563430	43
18	421395	7.69	984328	.58	437067	8.27	562933	42
19	421857	7.68	984294	.58	437563	8.26	562437	41
20	422318	7.67	984259	.58	438059	8.25	561941	40
21	9.422778	7.67	9.984224	.58	9.438554	8.24	10.561446	39
22	423238	7.66	984190	.58	439048	8.23	560952	38
23	423697	7.65	984155	.58	439543	8.23	560457	37
24	424156	7.64	984120	.58	440036	8.22	559964	36
25	424615	7.63	984085	.58	440529	8.21	559471	35
26	425073	7.62	984050	.58	441022	8.20	558978	34
27	425530	7.61	984015	.58	441514	8.19	558486	33
28	425987	7.60	983981	.58	442006	8.19	557994	32
29	426443	7.60	983946	.58	442497	8.18	557503	31
30	426899	7.59	983911	.58	442988	8.17	557012	30
31	9.427354	7.58	9.983875	.58	9.443479	8.16	10.556521	29
32	427809	7.57	983840	.59	443968	8.16	556032	28
33	428263	7.56	983805	.59	444458	8.15	555542	27
34	428717	7.55	983770	.59	444947	8.14	555053	26
35	429170	7.54	983735	.59	445435	8.13	554565	25
36	429623	7.53	983700	.59	445923	8.12	554077	24
37	430075	7.52	983664	.59	446411	8.12	553589	23
38	430527	7.52	983629	.59	446898	8.11	553102	22
39	430978	7.51	983594	.59	447384	8.10	552616	21
40	431429	7.50	983558	.59	447870	8.09	552130	20
41	9.431879	7.49	9.983523	.59	9.448356	8.09	10.551644	19
42	432329	7.49	983487	.59	448841	8.08	551159	18
43	432778	7.48	983452	.59	449326	8.07	550674	17
44	433226	7.47	983416	.59	449810	8.06	550190	16
45	433675	7.46	983381	.59	450294	8.06	549706	15
46	434122	7.45	983345	.59	450777	8.05	549223	14
47	434569	7.44	983309	.59	451260	8.04	548740	13
48	435016	7.44	983273	.60	451743	8.03	548257	12
49	435462	7.43	983238	.60	452225	8.02	547775	11
50	435908	7.42	983202	.60	452706	8.02	547294	10
51	9.436353	7.41	9.983166	.60	9.453187	8.01	10.546813	9
52	436798	7.40	983130	.60	453668	8.00	546332	8
53	437242	7.40	983094	.60	454148	7.99	545852	7
54	437686	7.39	983058	.60	454628	7.99	545372	6
55	438129	7.38	983022	.60	455107	7.98	544893	5
56	438572	7.37	982986	.60	455586	7.97	544414	4
57	439014	7.36	982950	.60	456064	7.96	543936	3
58	439456	7.36	982914	.60	456542	7.96	543458	2
59	439897	7.35	982878	.60	457019	7.95	542981	1
60	440338	7.34	982842	.60	457496	7.94	542504	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.440338	7.34	9.982842	.60	9.457496	7.94	10.542504	60
1	440778	7.33	982805	.60	457973	7.93	542027	59
2	441218	7.32	982769	.61	458449	7.93	541551	58
3	441658	7.31	982733	.61	458925	7.92	541075	57
4	442096	7.31	982696	.61	459400	7.91	540600	56
5	442535	7.30	982660	.61	459875	7.90	540125	55
6	442973	7.29	982624	.61	460349	7.90	539651	54
7	443410	7.28	982587	.61	460823	7.89	539177	53
8	443847	7.27	982551	.61	461297	7.88	538703	52
9	444284	7.27	982514	.61	461770	7.88	538230	51
10	444720	7.26	982477	.61	462242	7.87	537758	50
11	9.445155	7.25	9.982441	.61	9.462714	7.86	10.537286	49
12	445590	7.24	982404	.61	463186	7.85	536814	48
13	446025	7.23	982367	.61	463658	7.85	536342	47
14	446459	7.23	982331	.61	464129	7.84	535871	46
15	446893	7.22	982294	.61	464599	7.83	535401	45
16	447326	7.21	982257	.61	465069	7.83	534931	44
17	447759	7.20	982220	.62	465539	7.82	534461	43
18	448191	7.20	982183	.62	466008	7.81	533992	42
19	448623	7.19	982146	.62	466476	7.80	533524	41
20	449054	7.18	982109	.62	466945	7.80	533055	40
21	9.449485	7.17	9.982072	.62	9.467413	7.79	10.532587	39
22	449915	7.16	982035	.62	467880	7.78	532120	38
23	450345	7.16	981998	.62	468347	7.78	531653	37
24	450775	7.15	981961	.62	468814	7.77	531186	36
25	451204	7.14	981924	.62	469280	7.76	530720	35
26	451632	7.13	981886	.62	469746	7.75	530254	34
27	452060	7.13	981849	.62	470211	7.75	529789	33
28	452488	7.12	981812	.62	470676	7.74	529324	32
29	452915	7.11	981774	.62	471141	7.73	528859	31
30	453342	7.10	981737	.62	471605	7.73	528395	30
31	9.453768	7.10	9.981699	.63	9.472068	7.72	10.527932	29
32	454194	7.09	981662	.63	472532	7.71	527468	28
33	454619	7.08	981625	.63	472995	7.71	527005	27
34	455044	7.07	981587	.63	473457	7.70	526543	26
35	455469	7.07	981549	.63	473919	7.69	526081	25
36	455893	7.06	981512	.63	474381	7.69	525619	24
37	456316	7.05	981474	.63	474842	7.68	525158	23
38	456739	7.04	981436	.63	475303	7.67	524697	22
39	457162	7.04	981399	.63	475763	7.67	524237	21
40	457584	7.03	981361	.63	476223	7.66	523777	20
41	9.458006	7.02	9.981323	.63	9.476683	7.65	10.523317	19
42	458427	7.01	981285	.63	477142	7.65	522858	18
43	458848	7.01	981247	.63	477601	7.64	522399	17
44	459268	7.00	981209	.63	478059	7.63	521941	16
45	459688	6.99	981171	.63	478517	7.63	521483	15
46	460108	6.98	981133	.64	478975	7.62	521025	14
47	460527	6.98	981095	.64	479432	7.61	520568	13
48	460946	6.97	981057	.64	479889	7.61	520111	12
49	461364	6.96	981019	.64	480345	7.60	519655	11
50	461782	6.95	980981	.64	480801	7.59	519199	10
51	9.462199	6.95	9.980942	.64	9.481257	7.59	10.518743	9
52	462616	6.94	980904	.64	481712	7.58	518288	8
53	463032	6.93	980866	.64	482167	7.57	517833	7
54	463448	6.93	980827	.64	482621	7.57	517379	6
55	463864	6.92	980789	.64	483075	7.56	516925	5
56	464279	6.91	980750	.64	483529	7.55	516471	4
57	464694	6.90	980712	.64	483982	7.55	516018	3
58	465108	6.90	980673	.64	484435	7.54	515565	2
59	465522	6.89	980635	.64	484887	7.53	515113	1
60	465935	6.88	980596	.64	485339	7.53	514661	0
	Cosine	D.	Sine		Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.465935	6.88	9.980596	.64	9.485339	7.55	10.514661	60
1	466348	6.88	980558	.64	485791	7.52	514209	59
2	466761	6.87	980519	.65	486242	7.51	513758	58
3	467173	6.86	980480	.65	486693	7.51	513307	57
4	467585	6.85	980442	.65	487143	7.50	512857	56
5	467996	6.85	980403	.65	487593	7.49	512407	55
6	468407	6.84	980364	.65	488043	7.49	511957	54
7	468817	6.83	980325	.65	488492	7.48	511508	53
8	469227	6.83	980286	.65	488941	7.47	511059	52
9	469637	6.82	980247	.65	489390	7.47	510610	51
10	470046	6.81	980208	.65	489838	7.46	510162	50
11	9.470455	6.80	9.980169	.65	9.490286	7.46	10.509714	49
12	470863	6.80	980130	.65	490733	7.45	509267	48
13	471271	6.79	980091	.65	491180	7.44	508820	47
14	471679	6.78	980052	.65	491627	7.44	508373	46
15	472086	6.78	980012	.65	492073	7.43	507927	45
16	472492	6.77	979973	.65	492519	7.43	507481	44
17	472898	6.76	979934	.66	492965	7.42	507035	43
18	473304	6.76	979895	.66	493410	7.41	506590	42
19	473710	6.75	979855	.66	493854	7.40	506146	41
20	474115	6.74	979816	.66	494299	7.40	505701	40
21	9.474519	6.74	9.979776	.66	9.494743	7.40	10.505257	39
22	474923	6.73	979737	.66	495186	7.39	504814	38
23	475327	6.72	979697	.66	495630	7.38	504370	37
24	475730	6.72	979658	.66	496073	7.37	503927	36
25	476133	6.71	979618	.66	496515	7.37	503485	35
26	476536	6.70	979579	.66	496957	7.36	503043	34
27	476938	6.69	979539	.66	497399	7.36	502601	33
28	477340	6.69	979499	.66	497841	7.35	502159	32
29	477741	6.68	979459	.66	498282	7.34	501718	31
30	478142	6.67	979420	.66	498722	7.34	501278	30
31	9.478542	6.67	9.979380	.66	9.499163	7.33	10.500837	29
32	478942	6.66	979340	.66	499603	7.33	500397	28
33	479342	6.65	979300	.67	500042	7.32	499958	27
34	479741	6.65	979260	.67	500481	7.31	499519	26
35	480140	6.64	979220	.67	500920	7.31	499080	25
36	480539	6.63	979180	.67	501359	7.30	498641	24
37	480937	6.63	979140	.67	501797	7.30	498203	23
38	481334	6.62	979100	.67	502235	7.29	497765	22
39	481731	6.61	979059	.67	502672	7.28	497328	21
40	482128	6.61	979019	.67	503109	7.28	496891	20
41	9.482525	6.60	9.978979	.67	9.503546	7.27	10.496454	19
42	482921	6.59	978939	.67	503982	7.27	496018	18
43	483316	6.59	978898	.67	504418	7.26	495582	17
44	483712	6.58	978858	.67	504854	7.25	495146	16
45	484107	6.57	978817	.67	505289	7.25	494711	15
46	484501	6.57	978777	.67	505724	7.24	494276	14
47	484895	6.56	978736	.67	506159	7.24	493841	13
48	485289	6.55	978696	.68	506593	7.23	493407	12
49	485682	6.55	978655	.68	507027	7.22	492973	11
50	486075	6.54	978615	.68	507460	7.22	492540	10
51	9.486467	6.53	9.978574	.68	9.507893	7.21	10.492107	9
52	486860	6.53	978533	.68	508326	7.21	491674	8
53	487251	6.52	978493	.68	508759	7.20	491241	7
54	487643	6.51	978452	.68	509191	7.19	490809	6
55	488034	6.51	978411	.68	509622	7.19	490378	5
56	488424	6.50	978370	.68	510054	7.18	489946	4
57	488814	6.50	978329	.68	510485	7.18	489515	3
58	489204	6.49	978288	.68	510916	7.17	489084	2
59	489593	6.48	978247	.68	511346	7.16	488654	1
60	489982	6.48	978206	.68	511776	7.16	488224	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.489982	6.48	9.978206	.68	9.511776	7.16	10.488224	60
1	490371	6.48	978165	.68	512206	7.16	487794	59
2	490759	6.47	978124	.68	512635	7.15	487365	58
3	491147	6.46	978083	.69	513064	7.14	486936	57
4	491535	6.46	978042	.69	513493	7.14	486507	56
5	491922	6.45	978001	.69	513921	7.13	486079	55
6	492308	6.44	977959	.69	514349	7.13	485651	54
7	492695	6.44	977918	.69	514777	7.12	485223	53
8	493081	6.43	977877	.69	515204	7.12	484796	52
9	493466	6.42	977835	.69	515631	7.11	484369	51
10	493851	6.42	977794	.69	516057	7.10	483943	50
11	9.494236	6.41	9.977752	.69	9.516484	7.10	10.483516	49
12	494621	6.41	977711	.69	516910	7.09	483090	48
13	495005	6.40	977669	.69	517335	7.09	482665	47
14	495388	6.39	977628	.69	517761	7.08	482239	46
15	495772	6.39	977586	.69	518185	7.08	481815	45
16	496154	6.38	977544	.70	518610	7.07	481390	44
17	496537	6.37	977503	.70	519034	7.06	480966	43
18	496919	6.37	977461	.70	519458	7.06	480542	42
19	497301	6.36	977419	.70	519882	7.05	480118	41
20	497682	6.36	977377	.70	520305	7.05	479695	40
21	9.498064	6.35	9.977335	.70	9.520728	7.04	10.479272	39
22	498444	6.34	977293	.70	521151	7.03	478849	38
23	498825	6.34	977251	.70	521573	7.03	478427	37
24	499204	6.33	977209	.70	521995	7.03	478005	36
25	499584	6.32	977167	.70	522417	7.02	477583	35
26	499963	6.32	977125	.70	522838	7.02	477162	34
27	500342	6.31	977083	.70	523259	7.01	476741	33
28	500721	6.31	977041	.70	523680	7.01	476320	32
29	501099	6.30	976999	.70	524100	7.00	475900	31
30	501476	6.29	976957	.70	524520	6.99	475480	30
31	9.501854	6.29	9.976914	.70	9.524939	6.99	10.475061	29
32	502231	6.28	976872	.71	525359	6.98	474641	28
33	502607	6.28	976830	.71	525778	6.98	474222	27
34	502984	6.27	976787	.71	526197	6.97	473803	26
35	503360	6.26	976745	.71	526615	6.97	473385	25
36	503735	6.26	976702	.71	527033	6.96	472967	24
37	504110	6.25	976660	.71	527451	6.96	472549	23
38	504485	6.25	976617	.71	527868	6.95	472132	22
39	504860	6.24	976574	.71	528285	6.95	471715	21
40	505234	6.23	976532	.71	528702	6.94	471298	20
41	9.505608	6.23	9.976489	.71	9.529119	6.93	10.470881	19
42	505981	6.22	976446	.71	529535	6.93	470465	18
43	506354	6.22	976404	.71	529950	6.93	470050	17
44	506727	6.21	976361	.71	530366	6.92	469634	16
45	507099	6.20	976318	.71	530781	6.91	469219	15
46	507471	6.20	976275	.71	531196	6.91	468804	14
47	507843	6.19	976232	.72	531611	6.90	468389	13
48	508214	6.19	976189	.72	532025	6.90	467975	12
49	508585	6.18	976146	.72	532439	6.89	467561	11
50	508956	6.18	976103	.72	532853	6.89	467147	10
51	9.509326	6.17	9.976060	.72	9.533266	6.88	10.466734	9
52	509696	6.16	976017	.72	533679	6.88	466321	8
53	510065	6.16	975974	.72	534092	6.87	465908	7
54	510434	6.15	975930	.72	534504	6.87	465496	6
55	510803	6.15	975887	.72	534916	6.86	465084	5
56	511172	6.14	975844	.72	535328	6.86	464672	4
57	511540	6.13	975800	.72	535739	6.85	464261	3
58	511907	6.13	975757	.72	536150	6.85	463850	2
59	512275	6.12	975714	.72	536561	6.84	463439	1
60	512642	6.12	975670	.72	536972	6.84	463028	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.



M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.512642	6.12	9.975670	.73	9.536972	6.84	10.463028	60
1	513009	6.11	975627	.73	537382	6.83	462618	59
2	513375	6.11	975583	.73	537792	6.83	462208	58
3	513741	6.10	975539	.73	538202	6.82	461798	57
4	514107	6.09	975496	.73	538611	6.82	461389	56
5	514472	6.09	975452	.73	539020	6.81	460980	55
6	514837	6.08	975408	.73	539429	6.81	460571	54
7	515202	6.08	975365	.73	539837	6.80	460163	53
8	515566	6.07	975321	.73	540245	6.80	459755	52
9	515930	6.07	975277	.73	540653	6.79	459347	51
10	516294	6.06	975233	.73	541061	6.79	458939	50
11	9.516657	6.05	9.975189	.73	9.541468	6.78	10.458532	49
12	517020	6.05	975145	.73	541875	6.78	458125	48
13	517382	6.04	975101	.73	542281	6.77	457719	47
14	517745	6.04	975057	.73	542688	6.77	457312	46
15	518107	6.03	975013	.73	543094	6.76	456906	45
16	518468	6.03	974969	.74	543499	6.76	456501	44
17	518829	6.02	974925	.74	543905	6.75	456095	43
18	519190	6.01	974880	.74	544310	6.75	455690	42
19	519551	6.01	974836	.74	544715	6.74	455285	41
20	519911	6.00	974792	.74	545119	6.74	454881	40
21	9.520271	6.00	9.974748	.74	9.545524	6.73	10.454476	39
22	520631	5.99	974703	.74	545928	6.73	454072	38
23	520990	5.99	974659	.74	546331	6.72	453669	37
24	521349	5.98	974614	.74	546735	6.72	453265	36
25	521707	5.98	974570	.74	547138	6.71	452862	35
26	522066	5.97	974525	.74	547540	6.71	452460	34
27	522424	5.96	974481	.74	547943	6.70	452057	33
28	522781	5.96	974436	.74	548345	6.70	451655	32
29	523138	5.95	974391	.74	548747	6.69	451253	31
30	523495	5.95	974347	.75	549149	6.69	450851	30
31	9.523852	5.94	9.974302	.75	9.549550	6.68	10.450450	29
32	524208	5.94	974257	.75	549951	6.68	450049	28
33	524564	5.93	974212	.75	550352	6.67	449648	27
34	524920	5.93	974167	.75	550752	6.67	449248	26
35	525275	5.92	974122	.75	551152	6.66	448848	25
36	525630	5.91	974077	.75	551552	6.66	448448	24
37	525984	5.91	974032	.75	551952	6.65	448048	23
38	526339	5.90	973987	.75	552351	6.65	447649	22
39	526693	5.90	973942	.75	552750	6.65	447250	21
40	527046	5.89	973897	.75	553149	6.64	446851	20
41	9.527400	5.89	9.973852	.75	9.553548	6.64	10.446452	19
42	527753	5.88	973807	.75	553946	6.63	446054	18
43	528105	5.88	973761	.75	554344	6.63	445656	17
44	528458	5.87	973716	.76	554741	6.62	445259	16
45	528810	5.87	973671	.76	555139	6.62	444861	15
46	529161	5.86	973625	.76	555536	6.61	444464	14
47	529513	5.86	973580	.76	555933	6.61	444067	13
48	529864	5.85	973535	.76	556329	6.60	443671	12
49	530215	5.85	973489	.76	556725	6.60	443275	11
50	530565	5.84	973444	.76	557121	6.59	442879	10
51	9.530915	5.84	9.973398	.76	9.557517	6.59	10.442483	9
52	531265	5.83	973352	.76	557913	6.59	442087	8
53	531614	5.82	973307	.76	558308	6.58	441692	7
54	531963	5.82	973261	.76	558702	6.58	441298	6
55	532312	5.81	973215	.76	559097	6.57	440903	5
56	532661	5.81	973169	.76	559491	6.57	440509	4
57	533009	5.80	973124	.76	559885	6.56	440115	3
58	533357	5.80	973078	.76	560279	6.56	439721	2
59	533704	5.79	973032	.77	560673	6.55	439327	1
60	534052	5.78	972986	.77	561066	6.55	438934	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.534052	5.78	9.972986	.77	9.561066	6.55	10.438934	60
1	534399	5.77	972940	.77	561459	6.54	438541	59
2	534749	5.77	972894	.77	561851	6.54	438149	58
3	535092	5.77	972848	.77	562244	6.53	437756	57
4	535438	5.76	972802	.77	562636	6.53	437364	56
5	535783	5.76	972755	.77	563028	6.53	436972	55
6	536129	5.75	972709	.77	563419	6.52	436581	54
7	536474	5.74	972663	.77	563811	6.52	436189	53
8	536818	5.74	972617	.77	564202	6.51	435798	52
9	537163	5.73	972570	.77	564592	6.51	435408	51
10	537507	5.73	972524	.77	564983	6.50	435017	50
11	9.537851	5.72	9.972478	.77	9.565373	6.50	10.434627	49
12	538194	5.72	972431	.78	565763	6.49	434237	48
13	538538	5.71	972385	.78	566153	6.49	433847	47
14	538880	5.71	972338	.78	566542	6.49	433458	46
15	539223	5.70	972291	.78	566932	6.48	433068	45
16	539565	5.70	972245	.78	567320	6.48	432680	44
17	539907	5.69	972198	.78	567709	6.47	432291	43
18	540249	5.69	972151	.78	568098	6.47	431902	42
19	540590	5.68	972105	.78	568486	6.46	431514	41
20	540931	5.68	972058	.78	568873	6.46	431127	40
21	9.541272	5.67	9.972011	.78	9.569261	6.45	10.430739	39
22	541613	5.67	971964	.78	569648	6.45	430352	38
23	541953	5.66	971917	.78	570035	6.45	429965	37
24	542293	5.66	971870	.78	570422	6.44	429578	36
25	542632	5.65	971823	.78	570809	6.44	429191	35
26	542971	5.65	971776	.78	571195	6.43	428805	34
27	543310	5.64	971729	.79	571581	6.43	428419	33
28	543649	5.64	971682	.79	571967	6.42	428033	32
29	543987	5.63	971635	.79	572352	6.42	427648	31
30	544325	5.63	971588	.79	572738	6.42	427262	30
31	9.544663	5.62	9.971540	.79	9.573123	6.41	10.426877	29
32	545000	5.62	971493	.79	573507	6.41	426493	28
33	545338	5.61	971446	.79	573892	6.40	426108	27
34	545674	5.61	971398	.79	574276	6.40	425724	26
35	546011	5.60	971351	.79	574660	6.39	425340	25
36	546347	5.60	971303	.79	575044	6.39	424956	24
37	546683	5.59	971256	.79	575427	6.39	424573	23
38	547019	5.59	971208	.79	575810	6.38	424190	22
39	547354	5.58	971161	.79	576193	6.38	423807	21
40	547689	5.58	971113	.79	576576	6.37	423424	20
41	9.548024	5.57	9.971066	.80	9.576958	6.37	10.423041	19
42	548359	5.57	971018	.80	577341	6.36	422659	18
43	548693	5.56	970970	.80	577723	6.36	422277	17
44	549027	5.56	970922	.80	578104	6.36	421896	16
45	549360	5.55	970874	.80	578486	6.35	421514	15
46	549693	5.55	970827	.80	578867	6.35	421133	14
47	550026	5.54	970779	.80	579248	6.34	420752	13
48	550359	5.54	970731	.80	579629	6.34	420371	12
49	550692	5.53	970683	.80	580009	6.34	419991	11
50	551024	5.53	970635	.80	580389	6.33	419611	10
51	9.551356	5.52	9.970586	.80	9.580769	6.33	10.419231	9
52	551687	5.52	970538	.80	581149	6.32	418851	8
53	552018	5.52	970490	.80	581528	6.32	418472	7
54	552349	5.51	970442	.80	581907	6.32	418093	6
55	552680	5.51	970394	.80	582286	6.31	417714	5
56	553010	5.50	970345	.81	582665	6.31	417335	4
57	553341	5.50	970297	.81	583043	6.30	416957	3
58	553670	5.49	970249	.81	583422	6.30	416578	2
59	554000	5.49	970200	.81	583800	6.29	416200	1
60	554329	5.48	970152	.81	584177	6.29	415823	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.554329	5.48	9.970152	.81	9.584177	6.29	10.415823	60
1	554658	5.48	970103	.81	584555	6.29	415445	59
2	554987	5.47	970055	.81	584932	6.28	415068	58
3	555315	5.47	970006	.81	585309	6.28	414691	57
4	555643	5.46	969957	.81	585686	6.27	414314	56
5	555971	5.46	969909	.81	586062	6.27	413938	55
6	556299	5.45	969860	.81	586439	6.27	413561	54
7	556626	5.45	969811	.81	586815	6.26	413185	53
8	556953	5.44	969762	.81	587190	6.26	412810	52
9	557280	5.44	969714	.81	587566	6.25	412434	51
10	557606	5.43	969665	.81	587941	6.25	412059	50
11	9.557932	5.43	9.969616	.82	9.588316	6.25	10.411684	49
12	558258	5.43	969567	.82	588691	6.24	411309	48
13	558583	5.42	969518	.82	589066	6.24	410934	47
14	558909	5.42	969469	.82	589440	6.23	410560	46
15	559234	5.41	969420	.82	589814	6.23	410186	45
16	559558	5.41	969370	.82	590188	6.23	409812	44
17	559883	5.40	969321	.82	590562	6.22	409438	43
18	560207	5.40	969272	.82	590935	6.22	409065	42
19	560531	5.39	969223	.82	591308	6.22	408692	41
20	560855	5.39	969173	.82	591681	6.21	408319	40
21	9.561178	5.38	9.969124	.82	9.592054	6.21	10.407946	39
22	561501	5.38	969075	.82	592426	6.20	407574	38
23	561824	5.37	969025	.82	592798	6.20	407202	37
24	562146	5.37	968976	.82	593170	6.19	406829	36
25	562468	5.36	968926	.83	593542	6.19	406458	35
26	562790	5.36	968877	.83	593914	6.18	406086	34
27	563112	5.36	968827	.83	594285	6.18	405715	33
28	563433	5.35	968777	.83	594656	6.18	405344	32
29	563755	5.35	968728	.83	595027	6.17	404973	31
30	564075	5.34	968678	.83	595398	6.17	404602	30
31	9.564396	5.34	9.968628	.83	9.595768	6.17	10.404232	29
32	564716	5.33	968578	.83	596138	6.16	403862	28
33	565036	5.33	968528	.83	596508	6.16	403492	27
34	565356	5.32	968479	.83	596878	6.16	403122	26
35	565676	5.32	968429	.83	597247	6.15	402753	25
36	565995	5.31	968379	.83	597616	6.15	402384	24
37	566314	5.31	968329	.83	597985	6.15	402015	23
38	566632	5.31	968278	.83	598354	6.14	401646	22
39	566951	5.30	968228	.84	598722	6.14	401278	21
40	567269	5.30	968178	.84	599091	6.13	400909	20
41	9.567587	5.29	9.968128	.84	9.599459	6.13	10.400541	19
42	567904	5.29	968078	.84	599827	6.13	400173	18
43	568222	5.28	968027	.84	600194	6.12	399806	17
44	568539	5.28	967977	.84	600562	6.12	399438	16
45	568856	5.28	967927	.84	600929	6.11	399071	15
46	569172	5.27	967876	.84	601296	6.11	398704	14
47	569488	5.27	967826	.84	601662	6.11	398338	13
48	569804	5.26	967775	.84	602029	6.10	397971	12
49	570120	5.26	967725	.84	602395	6.10	397605	11
50	570435	5.25	967674	.84	602761	6.10	397239	10
51	9.570751	5.25	9.967624	.84	9.603127	6.09	10.396873	9
52	571066	5.24	967573	.84	603493	6.09	396507	8
53	571380	5.24	967522	.85	603858	6.09	396142	7
54	571695	5.23	967471	.85	604223	6.08	395777	6
55	572009	5.23	967421	.85	604588	6.08	395412	5
56	572323	5.23	967370	.85	604953	6.07	395047	4
57	572636	5.22	967319	.85	605317	6.07	394683	3
58	572950	5.22	967268	.85	605682	6.07	394318	2
59	573263	5.21	967217	.85	606046	6.06	393954	1
60	573575	5.21	967166	.85	606410	6.06	393590	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.573575	5.21	9.967166	.85	9.606410	6.06	10.393590	60
1	573888	5.20	967115	.85	606773	6.06	393227	59
2	574200	5.20	967064	.85	607137	6.05	392863	58
3	574512	5.19	967013	.85	607500	6.05	392500	57
4	574824	5.19	966961	.85	607863	6.04	392137	56
5	575136	5.19	966910	.85	608225	6.04	391775	55
6	575447	5.18	966859	.85	608588	6.04	391412	54
7	575758	5.18	966808	.85	608950	6.03	391050	53
8	576069	5.17	966756	.86	609312	6.03	390688	52
9	576379	5.17	966705	.86	609674	6.03	390326	51
10	576689	5.16	966653	.86	610036	6.02	389964	50
11	9.576999	5.16	9.966602	.86	9.610397	6.02	10.389603	49
12	577309	5.16	966550	.86	610759	6.02	389241	48
13	577618	5.15	966499	.86	611120	6.01	388880	47
14	577927	5.15	966447	.86	611480	6.01	388520	46
15	578236	5.14	966395	.86	611841	6.01	388159	45
16	578545	5.14	966344	.86	612201	6.00	387799	44
17	578853	5.13	966292	.86	612561	6.00	387439	43
18	579162	5.13	966240	.86	612921	6.00	387079	42
19	579470	5.13	966188	.86	613281	5.99	386719	41
20	579777	5.12	966136	.86	613641	5.99	386359	40
21	9.580085	5.12	9.966085	.87	9.614000	5.98	10.386000	39
22	580392	5.11	966033	.87	614359	5.98	385641	38
23	580699	5.11	965981	.87	614718	5.98	385282	37
24	581005	5.11	965928	.87	615077	5.97	384923	36
25	581312	5.10	965876	.87	615435	5.97	384565	35
26	581618	5.10	965824	.87	615793	5.97	384207	34
27	581924	5.09	965772	.87	616151	5.96	383849	33
28	582229	5.09	965720	.87	616509	5.96	383491	32
29	582535	5.09	965668	.87	616867	5.96	383133	31
30	582840	5.08	965615	.87	617224	5.95	382776	30
31	9.583145	5.08	9.965563	.87	9.617582	5.95	10.382418	29
32	583449	5.07	965511	.87	617939	5.95	382061	28
33	583754	5.07	965458	.87	618295	5.94	381705	27
34	584058	5.06	965406	.87	618652	5.94	381348	26
35	584361	5.06	965353	.88	619008	5.94	380992	25
36	584665	5.06	965301	.88	619364	5.93	380636	24
37	584968	5.05	965248	.88	619721	5.93	380279	23
38	585272	5.05	965195	.88	620076	5.93	379924	22
39	585574	5.04	965143	.88	620432	5.92	379568	21
40	585877	5.04	965090	.88	620787	5.92	379213	20
41	9.586179	5.03	9.965037	.88	9.621142	5.92	10.378858	19
42	586482	5.03	964984	.88	621497	5.91	378503	18
43	586783	5.03	964931	.88	621852	5.91	378148	17
44	587085	5.02	964879	.88	622207	5.90	377793	16
45	587386	5.02	964826	.88	622561	5.90	377439	15
46	587688	5.01	964773	.88	622915	5.90	377085	14
47	587989	5.01	964719	.88	623269	5.89	376731	13
48	588289	5.01	964666	.89	623623	5.89	376377	12
49	588590	5.00	964613	.89	623976	5.89	376024	11
50	588890	5.00	964560	.89	624330	5.88	375670	10
51	9.589190	4.99	9.964507	.89	9.624683	5.88	10.375317	9
52	589489	4.99	964454	.89	625036	5.88	374964	8
53	589789	4.99	964400	.89	625388	5.87	374612	7
54	590088	4.98	964347	.89	625741	5.87	374259	6
55	590387	4.98	964294	.89	626093	5.87	373907	5
56	590686	4.97	964240	.89	626445	5.86	373555	4
57	590984	4.97	964187	.89	626797	5.86	373203	3
58	591282	4.97	964133	.89	627149	5.86	372851	2
59	591580	4.96	964080	.89	627501	5.85	372499	1
60	591878	4.96	964026	.89	627852	5.85	372148	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.591878	4.96	9.964026	.89	9.627852	5.85	10.372148	60
1	592176	4.95	963972	.89	628203	5.85	371797	59
2	592473	4.95	963919	.89	628554	5.85	371446	58
3	592770	4.95	963865	.90	628905	5.84	371095	57
4	593067	4.94	963811	.90	629255	5.84	370745	56
5	593363	4.94	963757	.90	629606	5.83	370394	55
6	593659	4.93	963704	.90	629956	5.83	370044	54
7	593955	4.93	963650	.90	630306	5.83	369694	53
8	594251	4.93	963596	.90	630656	5.83	369344	52
9	594547	4.92	963542	.90	631005	5.82	368995	51
10	594842	4.92	963488	.90	631355	5.82	368645	50
11	9.595137	4.91	9.963434	.90	9.631704	5.82	10.368296	49
12	595432	4.91	963379	.90	632053	5.81	367947	48
13	595727	4.91	963325	.90	632401	5.81	367599	47
14	596021	4.90	963271	.90	632750	5.81	367250	46
15	596315	4.90	963217	.90	633098	5.80	366902	45
16	596609	4.89	963163	.90	633447	5.80	366553	44
17	596903	4.89	963108	.91	633795	5.80	366205	43
18	597196	4.89	963054	.91	634143	5.79	365857	42
19	597490	4.88	962999	.91	634490	5.79	365510	41
20	597783	4.88	962945	.91	634838	5.79	365162	40
21	9.598075	4.87	9.962890	.91	9.635185	5.78	10.364815	39
22	598368	4.87	962836	.91	635532	5.78	364468	38
23	598660	4.87	962781	.91	635879	5.78	364121	37
24	598952	4.86	962727	.91	636226	5.77	363774	36
25	599244	4.86	962672	.91	636572	5.77	363428	35
26	599536	4.85	962617	.91	636919	5.77	363081	34
27	599827	4.85	962562	.91	637265	5.77	362735	33
28	600118	4.85	962508	.91	637611	5.76	362389	32
29	600409	4.84	962453	.91	637956	5.76	362044	31
30	600700	4.84	962398	.92	638302	5.76	361698	30
31	9.600990	4.84	9.962343	.92	9.638647	5.75	10.361353	29
32	601280	4.83	962288	.92	638992	5.75	361008	28
33	601570	4.83	962233	.92	639337	5.75	360663	27
34	601860	4.82	962178	.92	639682	5.74	360318	26
35	602150	4.82	962123	.92	640027	5.74	359973	25
36	602439	4.82	962067	.92	640371	5.74	359629	24
37	602728	4.81	962012	.92	640716	5.73	359284	23
38	603017	4.81	961957	.92	641060	5.73	358940	22
39	603305	4.81	961902	.92	641404	5.73	358596	21
40	603594	4.80	961846	.92	641747	5.72	358253	20
41	9.603882	4.80	9.961791	.92	9.642091	5.72	10.357909	19
42	604170	4.79	961735	.92	642434	5.72	357566	18
43	604457	4.79	961680	.92	642777	5.72	357223	17
44	604745	4.79	961624	.93	643120	5.71	356880	16
45	605032	4.78	961569	.93	643463	5.71	356537	15
46	605319	4.78	961513	.93	643806	5.71	356194	14
47	605606	4.78	961458	.93	644148	5.70	355852	13
48	605892	4.77	961402	.93	644490	5.70	355510	12
49	606179	4.77	961346	.93	644832	5.70	355168	11
50	606465	4.76	961290	.93	645174	5.69	354826	10
51	9.606751	4.76	9.961235	.93	9.645516	5.69	10.354484	9
52	607036	4.76	961179	.93	645857	5.69	354143	8
53	607322	4.75	961123	.93	646199	5.69	353801	7
54	607607	4.75	961067	.93	646540	5.68	353460	6
55	607892	4.74	961011	.93	646881	5.68	353119	5
56	608177	4.74	960955	.93	647222	5.68	352778	4
57	608461	4.74	960899	.93	647562	5.67	352438	3
58	608745	4.73	960843	.94	647903	5.67	352097	2
59	609029	4.73	960786	.94	648243	5.67	351757	1
60	609313	4.73	960730	.94	648583	5.66	351417	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.609313	4.73	9.960730	.94	9.648583	5.66	10.351417	60
1	609597	4.72	960674	.94	648923	5.66	351077	59
2	609880	4.72	960618	.94	649263	5.66	350737	58
3	610164	4.72	960561	.94	649602	5.66	350398	57
4	610447	4.71	960505	.94	649942	5.65	350058	56
5	610729	4.71	960448	.94	650281	5.65	349719	55
6	611012	4.70	960392	.94	650620	5.65	349380	54
7	611294	4.70	960335	.94	650959	5.64	349041	53
8	611576	4.70	960279	.94	651297	5.64	348703	52
9	611858	4.69	960222	.94	651636	5.64	348364	51
10	612140	4.69	960165	.94	651974	5.63	348026	50
11	9.612421	4.69	9.960109	.95	9.652312	5.63	10.347688	49
12	612702	4.68	960052	.95	652650	5.63	347350	48
13	612983	4.68	959995	.95	652988	5.63	347012	47
14	613264	4.67	959938	.95	653326	5.62	346674	46
15	613545	4.67	959882	.95	653663	5.62	346337	45
16	613825	4.67	959825	.95	654000	5.62	346000	44
17	614105	4.66	959768	.95	654337	5.61	345663	43
18	614385	4.66	959711	.95	654674	5.61	345326	42
19	614665	4.66	959654	.95	655011	5.61	344989	41
20	614944	4.65	959596	.95	655348	5.61	344652	40
21	9.615223	4.65	9.959539	.95	9.655684	5.60	10.344316	39
22	615502	4.65	959482	.95	656020	5.60	343980	38
23	615781	4.64	959425	.95	656356	5.60	343644	37
24	616060	4.64	959368	.95	656692	5.59	343308	36
25	616338	4.64	959310	.96	657028	5.59	342972	35
26	616616	4.63	959253	.96	657364	5.59	342636	34
27	616894	4.63	959195	.96	657699	5.59	342301	33
28	617172	4.62	959138	.96	658034	5.58	341966	32
29	617450	4.62	959081	.96	658369	5.58	341631	31
30	617727	4.62	959023	.96	658704	5.58	341296	30
31	9.618004	4.61	9.958965	.96	9.659039	5.58	10.340961	29
32	618281	4.61	958908	.96	659373	5.57	340627	28
33	618558	4.61	958850	.96	659708	5.57	340292	27
34	618834	4.60	958792	.96	660042	5.57	339958	26
35	619110	4.60	958734	.96	660376	5.57	339624	25
36	619386	4.60	958677	.96	660710	5.56	339290	24
37	619662	4.59	958619	.96	661043	5.56	338957	23
38	619938	4.59	958561	.96	661377	5.56	338623	22
39	620213	4.59	958503	.97	661710	5.55	338290	21
40	620488	4.58	958445	.97	662043	5.55	337957	20
41	9.620763	4.58	9.958387	.97	9.662376	5.55	10.337624	19
42	621038	4.57	958329	.97	662709	5.54	337291	18
43	621313	4.57	958271	.97	663042	5.54	336958	17
44	621587	4.57	958213	.97	663375	5.54	336625	16
45	621861	4.56	958154	.97	663707	5.54	336293	15
46	622135	4.56	958096	.97	664039	5.53	335961	14
47	622409	4.56	958038	.97	664371	5.53	335629	13
48	622682	4.55	957979	.97	664703	5.53	335297	12
49	622956	4.55	957921	.97	665035	5.53	334965	11
50	623229	4.55	957863	.97	665366	5.52	334634	10
51	9.623502	4.54	9.957804	.97	9.665697	5.52	10.334303	9
52	623774	4.54	957746	.98	666029	5.52	333971	8
53	624047	4.54	957687	.98	666360	5.51	333640	7
54	624319	4.53	957628	.98	666691	5.51	333309	6
55	624591	4.53	957570	.98	667021	5.51	332979	5
56	624863	4.53	957511	.98	667352	5.51	332648	4
57	625135	4.52	957452	.98	667682	5.50	332318	3
58	625406	4.52	957393	.98	668013	5.50	331987	2
59	625677	4.52	957335	.98	668343	5.50	331657	1
60	625948	4.51	957276	.98	668672	5.50	331328	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.625948	4.51	9.957276	.98	9.668673	5.50	10.331327	60
1	626219	4.51	957217	.98	669002	5.49	330998	59
2	626490	4.51	957158	.98	669332	5.49	330668	58
3	626760	4.50	957099	.98	669661	5.49	330339	57
4	627030	4.50	957040	.98	669991	5.48	330009	56
5	627300	4.50	956981	.98	670320	5.48	329680	55
6	627570	4.49	956921	.99	670649	5.48	329351	54
7	627840	4.49	956862	.99	670977	5.48	329023	53
8	628109	4.49	956803	.99	671306	5.47	328694	52
9	628378	4.48	956744	.99	671634	5.47	328366	51
10	628647	4.48	956684	.99	671963	5.47	328037	50
11	9.628916	4.47	9.956625	.99	9.672291	5.47	10.327709	49
12	629185	4.47	956566	.99	672619	5.46	327381	48
13	629453	4.47	956506	.99	672947	5.46	327053	47
14	629721	4.46	956447	.99	673274	5.46	326726	46
15	629989	4.46	956387	.99	673602	5.46	326398	45
16	630257	4.46	956327	.99	673929	5.45	326071	44
17	630524	4.46	956268	.99	674257	5.45	325743	43
18	630792	4.45	956208	1.00	674584	5.45	325416	42
19	631059	4.45	956148	1.00	674910	5.44	325090	41
20	631326	4.45	956089	1.00	675237	5.44	324763	40
21	9.631593	4.44	9.956029	1.00	9.675564	5.44	10.324436	39
22	631859	4.44	955969	1.00	675890	5.44	324410	38
23	632125	4.44	955909	1.00	676216	5.43	323784	37
24	632392	4.43	955849	1.00	676543	5.43	323457	36
25	632658	4.43	955789	1.00	676869	5.43	323131	35
26	632923	4.43	955729	1.00	677194	5.43	322806	34
27	633189	4.42	955669	1.00	677520	5.42	322480	33
28	633454	4.42	955609	1.00	677846	5.42	322154	32
29	633719	4.42	955548	1.00	678171	5.42	321829	31
30	633984	4.41	955488	1.00	678496	5.42	321504	30
31	9.634249	4.41	9.955428	1.01	9.678821	5.41	10.321179	29
32	634514	4.40	955368	1.01	679146	5.41	320854	28
33	634778	4.40	955307	1.01	679471	5.41	320529	27
34	635042	4.40	955247	1.01	679795	5.41	320205	26
35	635306	4.39	955186	1.01	680120	5.40	319880	25
36	635570	4.39	955126	1.01	680444	5.40	319556	24
37	635834	4.39	955065	1.01	680768	5.40	319232	23
38	636097	4.38	955005	1.01	681092	5.40	318908	22
39	636360	4.38	954944	1.01	681416	5.39	318584	21
40	636623	4.38	954883	1.01	681740	5.39	318260	20
41	9.636886	4.37	9.954823	1.01	9.682063	5.39	10.317937	19
42	637148	4.37	954762	1.01	682387	5.39	317613	18
43	637411	4.37	954701	1.01	682710	5.38	317290	17
44	637673	4.37	954640	1.01	683033	5.38	316967	16
45	637935	4.36	954579	1.01	683356	5.38	316644	15
46	638197	4.36	954518	1.02	683679	5.38	316321	14
47	638458	4.36	954457	1.02	684001	5.37	315999	13
48	638720	4.35	954396	1.02	684324	5.37	315676	12
49	638981	4.35	954335	1.02	684646	5.37	315354	11
50	639242	4.35	954274	1.02	684968	5.37	315032	10
51	9.639503	4.34	9.954213	1.02	9.685290	5.36	10.314710	9
52	639764	4.34	954152	1.02	685612	5.36	314388	8
53	640024	4.34	954090	1.02	685934	5.36	314066	7
54	640284	4.33	954029	1.02	686255	5.36	313745	6
55	640544	4.33	953968	1.02	686577	5.35	313423	5
56	640804	4.33	953906	1.02	686898	5.35	313102	4
57	641064	4.32	953845	1.02	687219	5.35	312781	3
58	641324	4.32	953783	1.02	687540	5.35	312460	2
59	641584	4.32	953722	1.03	687861	5.34	312139	1
60	641842	4.31	953660	1.03	688182	5.34	311818	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.641842	4.31	9.953660	1.03	9.688182	5.34	10.311818	60
1	642101	4.31	953599	1.03	688502	5.34	311498	59
2	642360	4.31	953537	1.03	688823	5.34	311177	58
3	642618	4.30	953475	1.03	689143	5.33	310857	57
4	642877	4.30	953413	1.03	689463	5.33	310537	56
5	643135	4.30	953352	1.03	689783	5.33	310217	55
6	643393	4.30	953290	1.03	690103	5.33	309897	54
7	643650	4.29	953228	1.03	690423	5.33	309577	53
8	643908	4.29	953166	1.03	690742	5.32	309258	52
9	644165	4.29	953104	1.03	691062	5.32	308938	51
10	644423	4.28	953042	1.03	691381	5.32	308619	50
11	9.644680	4.28	9.952980	1.04	9.691700	5.31	10.308300	49
12	644936	4.28	952918	1.04	692019	5.31	307981	48
13	645193	4.27	952855	1.04	692338	5.31	307662	47
14	645450	4.27	952793	1.04	692656	5.31	307344	46
15	645706	4.27	952731	1.04	692975	5.31	307025	45
16	645962	4.26	952669	1.04	693293	5.30	306707	44
17	646218	4.26	952606	1.04	693612	5.30	306388	43
18	646474	4.26	952544	1.04	693930	5.30	306070	42
19	646729	4.25	952481	1.04	694248	5.30	305752	41
20	646984	4.25	952419	1.04	694566	5.29	305434	40
21	9.647240	4.25	9.952356	1.04	9.694883	5.29	10.305117	39
22	647494	4.24	952294	1.04	695201	5.29	304799	38
23	647749	4.24	952231	1.04	695518	5.29	304482	37
24	648004	4.24	952168	1.05	695836	5.29	304164	36
25	648258	4.24	952106	1.05	696153	5.28	303847	35
26	648512	4.23	952043	1.05	696470	5.28	303530	34
27	648766	4.23	951980	1.05	696787	5.28	303213	33
28	649020	4.23	951917	1.05	697103	5.28	302897	32
29	649274	4.22	951854	1.05	697420	5.27	302580	31
30	649527	4.22	951791	1.05	697736	5.27	302264	30
31	9.649781	4.22	9.951728	1.05	9.698053	5.27	10.301947	29
32	650034	4.22	951665	1.05	698369	5.27	301631	28
33	650287	4.21	951602	1.05	698685	5.26	301315	27
34	650539	4.21	951539	1.05	699001	5.26	300999	26
35	650792	4.21	951476	1.05	699316	5.26	300684	25
36	651044	4.20	951412	1.05	699632	5.26	300368	24
37	651297	4.20	951349	1.06	699947	5.26	300053	23
38	651549	4.20	951286	1.06	700263	5.25	299737	22
39	651800	4.19	951222	1.06	700578	5.25	299422	21
40	652052	4.19	951159	1.06	700893	5.25	299107	20
41	9.652304	4.19	9.951096	1.06	9.701208	5.24	10.298792	19
42	652555	4.18	951032	1.06	701523	5.24	298477	18
43	652806	4.18	950968	1.06	701837	5.24	298163	17
44	653057	4.18	950905	1.06	702152	5.24	297848	16
45	653308	4.18	950841	1.06	702466	5.24	297534	15
46	653558	4.17	950778	1.06	702780	5.23	297220	14
47	653808	4.17	950714	1.06	703095	5.23	296905	13
48	654059	4.17	950650	1.06	703409	5.23	296591	12
49	654309	4.16	950586	1.06	703723	5.23	296277	11
50	654558	4.16	950522	1.07	704036	5.22	295964	10
51	9.654808	4.16	9.950458	1.07	9.704350	5.22	10.295650	9
52	655058	4.16	950394	1.07	704663	5.22	295337	8
53	655307	4.15	950330	1.07	704977	5.22	295023	7
54	655556	4.15	950266	1.07	705290	5.22	294710	6
55	655805	4.15	950202	1.07	705603	5.21	294397	5
56	656054	4.14	950138	1.07	705916	5.21	294084	4
57	656302	4.14	950074	1.07	706228	5.21	293772	3
58	656551	4.14	950010	1.07	706541	5.21	293459	2
59	656799	4.13	949945	1.07	706854	5.21	293146	1
60	657047	4.13	949881	1.07	707166	5.20	292834	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.



M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.657047	4.13	9.949881	1.07	9.707166	5.20	10.292834	60
1	657295	4.13	949816	1.07	707478	5.20	292522	59
2	657542	4.12	949752	1.07	707790	5.20	292210	58
3	657790	4.12	949688	1.08	708102	5.20	291898	57
4	658037	4.12	949623	1.08	708414	5.19	291586	56
5	658284	4.12	949558	1.08	708726	5.19	291274	55
6	658531	4.11	949494	1.08	709037	5.19	290963	54
7	658778	4.11	949429	1.08	709349	5.19	290651	53
8	659025	4.11	949364	1.08	709660	5.19	290340	52
9	659271	4.10	949300	1.08	709971	5.18	290029	51
10	659517	4.10	949235	1.08	710282	5.18	289718	50
11	9.659763	4.10	9.949170	1.08	9.710593	5.18	10.289407	49
12	660009	4.09	949105	1.08	710904	5.18	289096	48
13	660255	4.09	949040	1.08	711215	5.18	288785	47
14	660501	4.09	948975	1.08	711525	5.17	288475	46
15	660746	4.09	948910	1.08	711836	5.17	288164	45
16	660991	4.08	948845	1.08	712146	5.17	287854	44
17	661236	4.08	948780	1.09	712456	5.17	287544	43
18	661481	4.08	948715	1.09	712766	5.16	287234	42
19	661726	4.07	948650	1.09	713076	5.16	286924	41
20	661970	4.07	948584	1.09	713386	5.16	286614	40
21	9.662214	4.07	9.948519	1.09	9.713696	5.16	10.286304	39
22	662459	4.07	948454	1.09	714005	5.16	285995	38
23	662703	4.06	948388	1.09	714314	5.15	285686	37
24	662946	4.06	948323	1.09	714624	5.15	285376	36
25	663190	4.06	948257	1.09	714933	5.15	285067	35
26	663433	4.05	948192	1.09	715242	5.15	284758	34
27	663677	4.05	948126	1.09	715551	5.14	284449	33
28	663920	4.05	948060	1.09	715860	5.14	284140	32
29	664163	4.05	947995	1.10	716168	5.14	283832	31
30	664406	4.04	947929	1.10	716477	5.14	283523	30
31	9.664648	4.04	9.947863	1.10	9.716785	5.14	10.283215	29
32	664891	4.04	947797	1.10	717093	5.13	282907	28
33	665133	4.03	947731	1.10	717401	5.13	282599	27
34	665375	4.03	947665	1.10	717709	5.13	282291	26
35	665617	4.03	947600	1.10	718017	5.13	281983	25
36	665859	4.02	947533	1.10	718325	5.13	281670	24
37	666100	4.02	947467	1.10	718633	5.12	281367	23
38	666342	4.02	947401	1.10	718940	5.12	281060	22
39	666583	4.02	947335	1.10	719248	5.12	280752	21
40	666824	4.01	947269	1.10	719555	5.12	280445	20
41	9.667065	4.01	9.947203	1.10	9.719862	5.12	10.280138	19
42	667305	4.01	947136	1.11	720169	5.11	279831	18
43	667546	4.01	947070	1.11	720476	5.11	279524	17
44	667786	4.00	947004	1.11	720783	5.11	279217	16
45	668027	4.00	946937	1.11	721089	5.11	278911	15
46	668267	4.00	946871	1.11	721396	5.11	278604	14
47	668506	3.99	946804	1.11	721702	5.10	278298	13
48	668746	3.99	946738	1.11	722009	5.10	277991	12
49	668986	3.99	946671	1.11	722315	5.10	277685	11
50	669225	3.99	946604	1.11	722621	5.10	277379	10
51	9.669464	3.98	9.946538	1.11	9.722927	5.10	10.277073	9
52	669703	3.98	946471	1.11	723232	5.09	276768	8
53	669942	3.98	946404	1.11	723538	5.09	276462	7
54	670181	3.97	946337	1.11	723844	5.09	276156	6
55	670419	3.97	946270	1.12	724149	5.09	275851	5
56	670658	3.97	946203	1.12	724454	5.09	275546	4
57	670896	3.97	946136	1.12	724759	5.08	275241	3
58	671134	3.96	946069	1.12	725065	5.08	274935	2
59	671372	3.96	946002	1.12	725369	5.08	274631	1
60	671609	3.96	945935	1.12	725674	5.08	274326	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.671609	3.96	9.945935	1.12	9.725674	5.08	10.274326	60
1	671847	3.95	945868	1.12	725979	5.08	274021	59
2	672084	3.95	945800	1.12	726284	5.07	273716	58
3	672321	3.95	945733	1.12	726588	5.07	273412	57
4	672558	3.95	945666	1.12	726892	5.07	273108	56
5	672795	3.94	945598	1.12	727197	5.07	272803	55
6	673032	3.94	945531	1.12	727501	5.07	272499	54
7	673268	3.94	945464	1.13	727805	5.06	272195	53
8	673505	3.94	945396	1.13	728109	5.06	271891	52
9	673741	3.93	945328	1.13	728412	5.06	271588	51
10	673977	3.93	945261	1.13	728716	5.06	271284	50
11	9.674213	3.93	9.945193	1.13	9.729020	5.06	10.270980	49
12	674448	3.92	945125	1.13	729323	5.05	270677	48
13	674684	3.92	945058	1.13	729626	5.05	270374	47
14	674919	3.92	944990	1.13	729929	5.05	270071	46
15	675155	3.92	944922	1.13	730233	5.05	269767	45
16	675390	3.91	944854	1.13	730535	5.05	269465	44
17	675624	3.91	944786	1.13	730838	5.04	269162	43
18	675859	3.91	944718	1.13	731141	5.04	268859	42
19	676094	3.91	944650	1.13	731444	5.04	268556	41
20	676328	3.90	944582	1.14	731746	5.04	268254	40
21	9.676562	3.90	9.944514	1.14	9.732048	5.04	10.267952	39
22	676796	3.90	944446	1.14	732351	5.03	267649	38
23	677030	3.90	944377	1.14	732653	5.03	267347	37
24	677264	3.89	944309	1.14	732955	5.03	267045	36
25	677498	3.89	944241	1.14	733257	5.03	266743	35
26	677731	3.89	944172	1.14	733558	5.03	266442	34
27	677964	3.88	944104	1.14	733860	5.02	266140	33
28	678197	3.88	944036	1.14	734162	5.02	265838	32
29	678430	3.88	943967	1.14	734463	5.02	265537	31
30	678663	3.88	943899	1.14	734764	5.02	265236	30
31	9.678895	3.87	9.943830	1.14	9.735066	5.02	10.264934	29
32	679128	3.87	943761	1.14	735367	5.02	264633	28
33	679360	3.87	943693	1.15	735668	5.01	264332	27
34	679592	3.87	943624	1.15	735969	5.01	264031	26
35	679824	3.86	943555	1.15	736269	5.01	263731	25
36	680056	3.86	943486	1.15	736570	5.01	263430	24
37	680288	3.86	943417	1.15	736871	5.01	263129	23
38	680519	3.85	943348	1.15	737171	5.00	262829	22
39	680750	3.85	943279	1.15	737471	5.00	262529	21
40	680982	3.85	943210	1.15	737771	5.00	262229	20
41	9.681213	3.85	9.943141	1.15	9.738071	5.00	10.261929	19
42	681443	3.84	943072	1.15	738371	5.00	261629	18
43	681674	3.84	943003	1.15	738671	4.99	261329	17
44	681905	3.84	942934	1.15	738971	4.99	261029	16
45	682135	3.84	942864	1.15	739271	4.99	260729	15
46	682365	3.83	942795	1.16	739570	4.99	260430	14
47	682595	3.83	942726	1.16	739870	4.99	260130	13
48	682825	3.83	942656	1.16	740169	4.99	259831	12
49	683055	3.83	942587	1.16	740468	4.98	259532	11
50	683284	3.82	942517	1.16	740767	4.98	259233	10
51	9.683514	3.82	9.942448	1.16	9.741066	4.98	10.258934	9
52	683743	3.82	942378	1.16	741365	4.98	258635	8
53	683972	3.82	942308	1.16	741664	4.98	258336	7
54	684201	3.81	942239	1.16	741962	4.97	258038	6
55	684430	3.81	942169	1.16	742261	4.97	257739	5
56	684658	3.81	942099	1.16	742559	4.97	257441	4
57	684887	3.80	942029	1.16	742858	4.97	257142	3
58	685115	3.80	941959	1.16	743156	4.97	256844	2
59	685343	3.80	941889	1.17	743454	4.97	256546	1
60	685571	3.80	941819	1.17	743752	4.96	256248	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.685571	3.80	9.941819	1.17	9.743752	4.96	10.256248	60
1	685799	3.79	941749	1.17	744050	4.96	255950	59
2	686027	3.79	941679	1.17	744348	4.96	255652	58
3	686254	3.79	941609	1.17	744645	4.96	255355	57
4	686482	3.79	941539	1.17	744943	4.96	255057	56
5	686709	3.78	941469	1.17	745240	4.96	254760	55
6	686936	3.78	941398	1.17	745538	4.95	254462	54
7	687163	3.78	941328	1.17	745835	4.95	254165	53
8	687389	3.78	941258	1.17	746132	4.95	253868	52
9	687616	3.77	941187	1.17	746429	4.95	253571	51
10	687843	3.77	941117	1.17	746726	4.95	253274	50
11	9.688069	3.77	9.941046	1.18	9.747023	4.94	10.252977	49
12	688295	3.77	940975	1.18	747319	4.94	252681	48
13	688521	3.76	940905	1.18	747616	4.94	252384	47
14	688747	3.76	940834	1.18	747913	4.94	252087	46
15	688972	3.76	940763	1.18	748209	4.94	251791	45
16	689198	3.76	940693	1.18	748505	4.93	251495	44
17	689423	3.75	940622	1.18	748801	4.93	251199	43
18	689648	3.75	940551	1.18	749097	4.93	250903	42
19	689873	3.75	940480	1.18	749393	4.93	250607	41
20	690098	3.75	940409	1.18	749689	4.93	250311	40
21	9.690323	3.74	9.940338	1.18	9.749985	4.93	10.250015	39
22	690548	3.74	940267	1.18	750281	4.92	249719	38
23	690772	3.74	940196	1.18	750576	4.92	249424	37
24	690996	3.74	940125	1.19	750872	4.92	249128	36
25	691220	3.73	940054	1.19	751167	4.92	248833	35
26	691444	3.73	939982	1.19	751462	4.92	248538	34
27	691668	3.73	939911	1.19	751757	4.92	248243	33
28	691892	3.73	939840	1.19	752052	4.91	247948	32
29	692115	3.72	939768	1.19	752347	4.91	247653	31
30	692339	3.72	939697	1.19	752642	4.91	247358	30
31	9.692562	3.72	9.939625	1.19	9.752937	4.91	10.247063	29
32	692785	3.71	939554	1.19	753231	4.91	246769	28
33	693008	3.71	939482	1.19	753526	4.91	246474	27
34	693231	3.71	939410	1.19	753820	4.90	246180	26
35	693453	3.71	939339	1.19	754115	4.90	245885	25
36	693676	3.70	939267	1.20	754409	4.90	245591	24
37	693898	3.70	939195	1.20	754703	4.90	245297	23
38	694120	3.70	939123	1.20	754997	4.90	245003	22
39	694342	3.70	939052	1.20	755291	4.90	244709	21
40	694564	3.69	938980	1.20	755585	4.89	244415	20
41	9.694786	3.69	9.938908	1.20	9.755878	4.89	10.244122	19
42	695007	3.69	938836	1.20	756172	4.89	243828	18
43	695229	3.69	938763	1.20	756465	4.89	243535	17
44	695450	3.68	938691	1.20	756759	4.89	243241	16
45	695671	3.68	938619	1.20	757052	4.89	242948	15
46	695892	3.68	938547	1.20	757345	4.88	242655	14
47	696113	3.68	938475	1.20	757638	4.88	242362	13
48	696334	3.67	938402	1.21	757931	4.88	242069	12
49	696554	3.67	938330	1.21	758224	4.88	241776	11
50	696775	3.67	938258	1.21	758517	4.88	241483	10
51	9.696995	3.67	9.938185	1.21	9.758810	4.88	10.241190	9
52	697215	3.66	938113	1.21	759102	4.87	240898	8
53	697435	3.66	938040	1.21	759395	4.87	240605	7
54	697654	3.66	937967	1.21	759687	4.87	240313	6
55	697874	3.66	937895	1.21	759979	4.87	240021	5
56	698094	3.65	937822	1.21	760272	4.87	239728	4
57	698313	3.65	937749	1.21	760564	4.87	239436	3
58	698532	3.65	937676	1.21	760856	4.86	239144	2
59	698751	3.65	937604	1.21	761148	4.86	238852	1
60	698970	3.64	937531	1.21	761439	4.86	238561	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.698970	3.64	9.937531	1.21	9.761439	4.86	10.238561	60
1	699189	3.64	937458	1.22	761731	4.86	238269	59
2	699407	3.64	937385	1.22	762023	4.86	237977	58
3	699626	3.64	937312	1.22	762314	4.86	237686	57
4	699844	3.63	937238	1.22	762606	4.85	237394	56
5	700062	3.63	937165	1.22	762897	4.85	237103	55
6	700280	3.63	937092	1.22	763188	4.85	236812	54
7	700498	3.63	937019	1.22	763479	4.85	236521	53
8	700716	3.63	936946	1.22	763770	4.85	236230	52
9	700933	3.62	936872	1.22	764061	4.85	235939	51
10	701151	3.62	936799	1.22	764352	4.84	235648	50
11	9.701368	3.62	9.936725	1.22	9.764643	4.84	10.235357	49
12	701585	3.62	936652	1.23	764933	4.84	235067	48
13	701802	3.61	936578	1.23	765224	4.84	234776	47
14	702019	3.61	936505	1.23	765514	4.84	234486	46
15	702236	3.61	936431	1.23	765805	4.84	234195	45
16	702452	3.61	936357	1.23	766095	4.84	233905	44
17	702669	3.60	936284	1.23	766385	4.83	233615	43
18	702885	3.60	936210	1.23	766675	4.83	233325	42
19	703101	3.60	936136	1.23	766965	4.83	233035	41
20	703317	3.60	936062	1.23	767255	4.83	232745	40
21	9.703533	3.59	9.935988	1.23	9.767545	4.83	10.232455	39
22	703749	3.59	935914	1.23	767834	4.83	232166	38
23	703964	3.59	935840	1.23	768124	4.82	231876	37
24	704179	3.59	935766	1.24	768413	4.82	231587	36
25	704395	3.59	935692	1.24	768703	4.82	231297	35
26	704610	3.58	935618	1.24	768992	4.82	231008	34
27	704825	3.58	935543	1.24	769281	4.82	230719	33
28	705040	3.58	935469	1.24	769570	4.82	230430	32
29	705254	3.58	935395	1.24	769860	4.81	230140	31
30	705469	3.57	935320	1.24	770148	4.81	229852	30
31	9.705683	3.57	9.935246	1.24	9.770437	4.81	10.229563	29
32	705898	3.57	935171	1.24	770726	4.81	229274	28
33	706112	3.57	935097	1.24	771015	4.81	228985	27
34	706326	3.56	935022	1.24	771303	4.81	228697	26
35	706539	3.56	934948	1.24	771592	4.81	228408	25
36	706753	3.56	934873	1.24	771880	4.80	228120	24
37	706967	3.56	934798	1.25	772168	4.80	227832	23
38	707180	3.55	934723	1.25	772457	4.80	227543	22
39	707393	3.55	934649	1.25	772745	4.80	227255	21
40	707606	3.55	934574	1.25	773033	4.80	226967	20
41	9.707819	3.55	9.934499	1.25	9.773321	4.80	10.226679	19
42	708032	3.54	934424	1.25	773608	4.79	226392	18
43	708245	3.54	934349	1.25	773896	4.79	226104	17
44	708458	3.54	934274	1.25	774184	4.79	225816	16
45	708670	3.54	934199	1.25	774471	4.79	225529	15
46	708882	3.53	934123	1.25	774759	4.79	225241	14
47	709094	3.53	934048	1.25	775046	4.79	224954	13
48	709306	3.53	933973	1.25	775333	4.79	224667	12
49	709518	3.53	933898	1.26	775621	4.78	224379	11
50	709730	3.53	933822	1.26	775908	4.78	224092	10
51	9.709941	3.52	9.933747	1.26	9.776195	4.78	10.223805	9
52	710153	3.52	933671	1.26	776482	4.78	223518	8
53	710364	3.52	933596	1.26	776769	4.78	223231	7
54	710575	3.52	933520	1.26	777055	4.78	222945	6
55	710786	3.51	933445	1.26	777342	4.78	222658	5
56	710997	3.51	933369	1.26	777628	4.77	222372	4
57	711208	3.51	933293	1.26	777915	4.77	222085	3
58	711419	3.51	933217	1.26	778201	4.77	221799	2
59	711629	3.50	933141	1.26	778487	4.77	221512	1
60	711839	3.50	933066	1.26	778774	4.77	221226	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.711839	3.50	9.933066	1.26	9.778774	4.77	10.221226	60
1	712050	3.50	932990	1.27	779060	4.77	220940	59
2	712260	3.50	932914	1.27	779346	4.76	220654	58
3	712469	3.49	932838	1.27	779632	4.76	220368	57
4	712679	3.49	932762	1.27	779918	4.76	220082	56
5	712889	3.49	932685	1.27	780203	4.76	219797	55
6	713098	3.49	932609	1.27	780489	4.76	219511	54
7	713308	3.49	932533	1.27	780775	4.76	219225	53
8	713517	3.48	932457	1.27	781060	4.76	218940	52
9	713726	3.48	932380	1.27	781346	4.75	218654	51
10	713935	3.48	932304	1.27	781631	4.75	218369	50
11	9.714144	3.48	9.932228	1.27	9.781916	4.75	10.218084	49
12	714352	3.47	932151	1.27	782201	4.75	217799	48
13	714561	3.47	932075	1.28	782486	4.75	217514	47
14	714769	3.47	931998	1.28	782771	4.75	217229	46
15	714978	3.47	931921	1.28	783056	4.75	216944	45
16	715186	3.47	931845	1.28	783341	4.75	216659	44
17	715394	3.46	931768	1.28	783626	4.74	216374	43
18	715602	3.46	931691	1.28	783910	4.74	216090	42
19	715809	3.46	931614	1.28	784195	4.74	215805	41
20	716017	3.46	931537	1.28	784479	4.74	215521	40
21	9.716224	3.45	9.931460	1.28	9.784764	4.74	10.215236	39
22	716432	3.45	931383	1.28	785048	4.74	214952	38
23	716639	3.45	931306	1.28	785332	4.73	214668	37
24	716846	3.45	931229	1.29	785616	4.73	214384	36
25	717053	3.45	931152	1.29	785900	4.73	214100	35
26	717259	3.44	931075	1.29	786184	4.73	213816	34
27	717466	3.44	930998	1.29	786468	4.73	213532	33
28	717673	3.44	930921	1.29	786752	4.73	213248	32
29	717879	3.44	930843	1.29	787036	4.73	212964	31
30	718085	3.43	930766	1.29	787319	4.72	212681	30
31	9.718291	3.43	9.930688	1.29	9.787603	4.72	10.212397	29
32	718497	3.43	930611	1.29	787886	4.72	212114	28
33	718703	3.43	930533	1.29	788170	4.72	211830	27
34	718909	3.43	930456	1.29	788453	4.72	211547	26
35	719114	3.42	930378	1.29	788736	4.72	211264	25
36	719320	3.42	930300	1.30	789019	4.72	210981	24
37	719525	3.42	930223	1.30	789302	4.71	210698	23
38	719730	3.42	930145	1.30	789585	4.71	210415	22
39	719935	3.41	930067	1.30	789868	4.71	210132	21
40	720140	3.41	929989	1.30	790151	4.71	209849	20
41	9.720345	3.41	9.929911	1.30	9.790433	4.71	10.209567	19
42	720549	3.41	929833	1.30	790716	4.71	209284	18
43	720754	3.40	929755	1.30	790999	4.71	209001	17
44	720958	3.40	929677	1.30	791281	4.71	208719	16
45	721162	3.40	929599	1.30	791563	4.70	208437	15
46	721366	3.40	929521	1.30	791846	4.70	208154	14
47	721570	3.40	929442	1.30	792128	4.70	207872	13
48	721774	3.39	929364	1.31	792410	4.70	207590	12
49	721978	3.39	929286	1.31	792692	4.70	207308	11
50	722181	3.39	929207	1.31	792974	4.70	207026	10
51	9.722385	3.39	9.929129	1.31	9.793256	4.70	10.206744	9
52	722588	3.39	929050	1.31	793538	4.69	206462	8
53	722791	3.38	928972	1.31	793819	4.69	206181	7
54	722994	3.38	928893	1.31	794101	4.69	205899	6
55	723197	3.38	928815	1.31	794383	4.69	205617	5
56	723400	3.38	928736	1.31	794664	4.69	205336	4
57	723603	3.37	928657	1.31	794945	4.69	205055	3
58	723805	3.37	928578	1.31	795227	4.69	204773	2
59	724007	3.37	928499	1.31	795508	4.68	204492	1
60	724210	3.37	928420	1.31	795789	4.68	204211	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.724210	3.37	9.928420	1.32	9.795789	4.68	10.204211	60
1	724412	3.37	928342	1.32	796070	4.68	203930	59
2	724614	3.36	928263	1.32	796351	4.68	203649	58
3	724816	3.36	928183	1.32	796632	4.68	203368	57
4	725017	3.36	928104	1.32	796913	4.68	203087	56
5	725219	3.36	928025	1.32	797194	4.68	202806	55
6	725420	3.35	927946	1.32	797475	4.68	202525	54
7	725622	3.35	927867	1.32	797755	4.68	202245	53
8	725823	3.35	927787	1.32	798036	4.67	201964	52
9	726024	3.35	927708	1.32	798316	4.67	201684	51
10	726225	3.35	927629	1.32	798596	4.67	201404	50
11	9.726426	3.34	9.927549	1.32	9.798877	4.67	10.201123	49
12	726626	3.34	927470	1.33	799157	4.67	200843	48
13	726827	3.34	927390	1.33	799437	4.67	200563	47
14	727027	3.34	927310	1.33	799717	4.67	200283	46
15	727228	3.34	927231	1.33	799997	4.66	200003	45
16	727428	3.33	927151	1.33	800277	4.66	199723	44
17	727628	3.33	927071	1.33	800557	4.66	199443	43
18	727828	3.33	926991	1.33	800836	4.66	199164	42
19	728027	3.33	926911	1.33	801116	4.66	198884	41
20	728227	3.33	926831	1.33	801396	4.66	198604	40
21	9.728427	3.32	9.926751	1.33	9.801675	4.66	10.198325	39
22	728626	3.32	926671	1.33	801955	4.66	198045	38
23	728825	3.32	926591	1.33	802234	4.65	197766	37
24	729024	3.32	926511	1.34	802513	4.65	197487	36
25	729223	3.31	926431	1.34	802792	4.65	197208	35
26	729422	3.31	926351	1.34	803072	4.65	196928	34
27	729621	3.31	926270	1.34	803351	4.65	196649	33
28	729820	3.31	926190	1.34	803630	4.65	196370	32
29	730018	3.30	926110	1.34	803908	4.65	196092	31
30	730216	3.30	926029	1.34	804187	4.65	195813	30
31	9.730415	3.30	9.925949	1.34	9.804466	4.64	10.195534	29
32	730613	3.30	925868	1.34	804745	4.64	195255	28
33	730811	3.30	925788	1.34	805023	4.64	194977	27
34	731009	3.29	925707	1.34	805302	4.64	194698	26
35	731206	3.29	925626	1.34	805580	4.64	194420	25
36	731404	3.29	925545	1.35	805859	4.64	194141	24
37	731602	3.29	925465	1.35	806137	4.64	193863	23
38	731799	3.29	925384	1.35	806415	4.63	193585	22
39	731996	3.28	925303	1.35	806693	4.63	193307	21
40	732193	3.28	925222	1.35	806971	4.63	193029	20
41	9.732390	3.28	9.925141	1.35	9.807249	4.63	10.192751	19
42	732587	3.28	925060	1.35	807527	4.63	192473	18
43	732784	3.28	924979	1.35	807805	4.63	192195	17
44	732980	3.27	924897	1.35	808083	4.63	191917	16
45	733177	3.27	924816	1.35	808361	4.63	191639	15
46	733373	3.27	924735	1.36	808638	4.62	191362	14
47	733569	3.27	924654	1.36	808916	4.62	191084	13
48	733765	3.27	924572	1.36	809193	4.62	190807	12
49	733961	3.26	924491	1.36	809471	4.62	190529	11
50	734157	3.26	924409	1.36	809748	4.62	190252	10
51	9.734353	3.26	9.924328	1.36	9.810025	4.62	10.189975	9
52	734549	3.26	924246	1.36	810302	4.62	189698	8
53	734744	3.25	924164	1.36	810580	4.62	189420	7
54	734939	3.25	924083	1.36	810857	4.62	189143	6
55	735135	3.25	924001	1.36	811134	4.61	188866	5
56	735330	3.25	923919	1.36	811410	4.61	188590	4
57	735525	3.25	923837	1.36	811687	4.61	188313	3
58	735719	3.24	923755	1.37	811964	4.61	188036	2
59	735914	3.24	923673	1.37	812241	4.61	187759	1
60	736109	3.24	923591	1.37	812517	4.61	187483	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.736109	3.24	9.923591	1.37	9.812517	4.61	10.187482	60
1	736303	3.24	923509	1.37	812794	4.61	187206	59
2	736498	3.24	923427	1.37	813070	4.61	186930	58
3	736692	3.23	923345	1.37	813347	4.60	186653	57
4	736886	3.23	923263	1.37	813623	4.60	186377	56
5	737080	3.23	923181	1.37	813899	4.60	186101	55
6	737274	3.23	923098	1.37	814175	4.60	185825	54
7	737467	3.23	923016	1.37	814452	4.60	185548	53
8	737661	3.22	922933	1.37	814728	4.60	185272	52
9	737855	3.22	922851	1.37	815004	4.60	184996	51
10	738048	3.22	922768	1.38	815279	4.60	184721	50
11	9.738241	3.22	9.922686	1.38	9.815555	4.59	10.184445	49
12	738434	3.22	922603	1.38	815831	4.59	184169	48
13	738627	8.21	922520	1.38	816107	4.59	183893	47
14	738820	3.21	922438	1.38	816382	4.59	183618	46
15	739013	3.21	922355	1.38	816658	4.59	183342	45
16	739206	3.21	922272	1.38	816933	4.59	183067	44
17	739398	3.21	922189	1.38	817209	4.59	182791	43
18	739590	3.20	922106	1.38	817484	4.59	182516	42
19	739783	3.20	922023	1.38	817759	4.59	182241	41
20	739975	3.20	921940	1.38	818035	4.58	181965	40
21	9.740167	3.20	9.921857	1.39	9.818310	4.58	10.181690	39
22	740359	3.20	921774	1.39	818585	4.58	181415	38
23	740550	3.19	921691	1.39	818860	4.58	181140	37
24	740742	3.19	921607	1.39	819135	4.58	180865	36
25	740934	3.19	921524	1.39	819410	4.58	180590	35
26	741125	3.19	921441	1.39	819684	4.58	180316	34
27	741316	3.19	921357	1.39	819959	4.58	180041	33
28	741508	3.18	921274	1.39	820234	4.58	179766	32
29	741699	3.18	921190	1.39	820508	4.57	179492	31
30	741889	3.18	921107	1.39	820783	4.57	179217	30
31	9.742086	3.18	9.921023	1.39	9.821057	4.57	10.178943	29
32	742271	3.18	920939	1.40	821322	4.57	178668	28
33	742462	3.17	920856	1.40	821606	4.57	178394	27
34	742652	3.17	920772	1.40	821880	4.57	178120	26
35	742842	3.17	920688	1.40	822154	4.57	177846	25
36	743033	3.17	920604	1.40	822429	4.57	177571	24
37	743223	3.17	920520	1.40	822703	4.57	177297	23
38	743413	3.16	920436	1.40	822977	4.56	177023	22
39	743602	3.16	920352	1.40	823250	4.56	176750	21
40	743792	3.16	920268	1.40	823524	4.56	176476	20
41	9.743982	3.16	9.920184	1.40	9.823798	4.56	10.176202	19
42	744171	3.16	920099	1.40	824072	4.56	175928	18
43	744361	3.15	920015	1.40	824345	4.56	175655	17
44	744550	3.15	919931	1.41	824619	4.56	175381	16
45	744739	3.15	919846	1.41	824893	4.56	175107	15
46	744928	3.15	919762	1.41	825166	4.56	174834	14
47	745117	3.15	919677	1.41	825439	4.55	174561	13
48	745306	3.14	919593	1.41	825713	4.55	174287	12
49	745494	3.14	919508	1.41	825986	4.55	174014	11
50	745683	3.14	919424	1.41	826259	4.55	173741	10
51	9.745871	3.14	9.919339	1.41	9.826532	4.55	10.173468	9
52	746059	3.14	919254	1.41	826805	4.55	173195	8
53	746248	3.13	919169	1.41	827078	4.55	172922	7
54	746436	4.13	919085	1.41	827351	4.55	172649	6
55	746624	3.13	919000	1.41	827624	4.55	172376	5
56	746812	3.13	918915	1.42	827897	4.54	172103	4
57	746999	3.13	918830	1.42	828170	4.54	171830	3
58	747187	3.12	918745	1.42	828442	4.54	171558	2
59	747374	3.12	918659	1.42	828715	4.54	171285	1
60	747562	3.12	918574	1.42	828987	4.54	171013	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.747562	3.12	9.918574	1.42	9.828987	4.54	10.171013	60
1	747749	3.12	918489	1.42	829260	4.54	170740	59
2	747936	3.12	918404	1.42	829532	4.54	170468	58
3	748123	3.11	918318	1.42	829805	4.54	170195	57
4	748310	3.11	918233	1.42	830077	4.54	169923	56
5	748497	3.11	918147	1.42	830349	4.53	169651	55
6	748683	3.11	918062	1.42	830621	4.53	169379	54
7	748870	3.11	917976	1.43	830893	4.53	169107	53
8	749056	3.10	917891	1.43	831165	4.53	168835	52
9	749243	3.10	917805	1.43	831437	4.53	168563	51
10	749429	3.10	917719	1.43	831709	4.53	168291	50
11	9.749615	3.10	9.917634	1.43	9.831981	4.53	10.168019	49
12	749801	3.10	917548	1.43	832253	4.53	167747	48
13	749987	3.09	917462	1.43	832525	4.53	167475	47
14	750172	3.09	917376	1.43	832796	4.53	167204	46
15	750358	3.09	917290	1.43	833068	4.52	166932	45
16	750543	3.09	917204	1.43	833339	4.52	166661	44
17	750729	3.09	917118	1.44	833611	4.52	166389	43
18	750914	3.08	917032	1.44	833882	4.52	166118	42
19	751099	3.08	916946	1.44	834154	4.52	165846	41
20	751284	3.08	916859	1.44	834425	4.52	165575	40
21	9.751469	3.08	9.916773	1.44	9.834696	4.52	10.165304	39
22	751654	3.08	916687	1.44	834967	4.52	165033	38
23	751839	3.08	916600	1.44	835238	4.52	164762	37
24	752023	3.07	916514	1.44	835509	4.52	164491	36
25	752208	3.07	916427	1.44	835780	4.51	164220	35
26	752392	3.07	916341	1.44	836051	4.51	163949	34
27	752576	3.07	916254	1.44	836322	4.51	163678	33
28	752760	3.07	916167	1.45	836593	4.51	163407	32
29	752944	3.06	916081	1.45	836864	4.51	163136	31
30	753128	3.06	915994	1.45	837134	4.51	162866	30
31	9.753312	3.06	9.915907	1.45	9.837405	4.51	10.162595	29
32	753495	3.06	915820	1.45	837675	4.51	162325	28
33	753679	3.06	915733	1.45	837946	4.51	162054	27
34	753862	3.05	915646	1.45	838216	4.51	161784	26
35	754046	3.05	915559	1.45	838487	4.50	161513	25
36	754229	3.05	915472	1.45	838757	4.50	161243	24
37	754412	3.05	915385	1.45	839027	4.50	160973	23
38	754595	3.05	915297	1.45	839297	4.50	160703	22
39	754778	3.04	915210	1.45	839568	4.50	160432	21
40	754960	3.04	915123	1.46	839838	4.50	160162	20
41	9.755143	3.04	9.915035	1.46	9.840108	4.50	10.159892	19
42	755326	3.04	914948	1.46	840378	4.50	159622	18
43	755508	3.04	914860	1.46	840647	4.50	159353	17
44	755690	3.04	914773	1.46	840917	4.49	159083	16
45	755872	3.03	914685	1.46	841187	4.49	158813	15
46	756054	3.03	914598	1.46	841457	4.49	158543	14
47	756236	3.03	914510	1.46	841726	4.49	158274	13
48	756418	3.03	914422	1.46	841996	4.49	158004	12
49	756600	3.03	914334	1.46	842266	4.49	157734	11
50	756782	3.02	914246	1.47	842535	4.49	157465	10
51	9.756963	3.02	9.914158	1.47	9.842805	4.49	10.157195	9
52	757144	3.02	914070	1.47	843074	4.49	156926	8
53	757326	3.02	913982	1.47	843343	4.49	156657	7
54	757507	3.02	913894	1.47	843612	4.49	156388	6
55	757688	3.01	913806	1.47	843882	4.48	156118	5
56	757869	3.01	913718	1.47	844151	4.48	155849	4
57	758050	3.01	913630	1.47	844420	4.48	155580	3
58	758230	3.01	913541	1.47	844689	4.48	155311	2
59	758411	3.01	913453	1.47	844958	4.48	155042	1
60	758591	3.01	913365	1.47	845227	4.48	154773	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.



M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.758591	3.01	9.913365	1.47	9.845227	4.48	10.154773	60
1	758772	3.00	913276	1.47	845496	4.48	154504	59
2	758952	3.00	913187	1.48	845764	4.48	154236	58
3	759132	3.00	913099	1.48	846033	4.48	153967	57
4	759312	3.00	913010	1.48	846302	4.48	153698	56
5	759492	3.00	912922	1.48	846570	4.47	153430	55
6	759672	2.99	912833	1.48	846839	4.47	153161	54
7	759852	2.99	912744	1.48	847107	4.47	152893	53
8	760031	2.99	912655	1.48	847376	4.47	152624	52
9	760211	2.99	912566	1.48	847644	4.47	152356	51
10	760390	2.99	912477	1.48	847913	4.47	152087	50
11	9.760569	2.98	9.912388	1.48	9.848181	4.47	10.151819	49
12	760748	2.98	912299	1.49	848449	4.47	151551	48
13	760927	2.98	912210	1.49	848717	4.47	151283	47
14	761106	2.98	912121	1.49	848986	4.47	151014	46
15	761285	2.98	912031	1.49	849254	4.47	150746	45
16	761464	2.98	911942	1.49	849522	4.47	150478	44
17	761642	2.97	911853	1.49	849790	4.46	150210	43
18	761821	2.97	911763	1.49	850058	4.46	149942	42
19	761999	2.97	911674	1.49	850325	4.46	149675	41
20	762177	2.97	911584	1.49	850593	4.46	149407	40
21	9.762356	2.97	9.911495	1.49	9.850861	4.46	10.149139	39
22	762534	2.96	911405	1.49	851129	4.46	148871	38
23	762712	2.96	911315	1.50	851396	4.46	148604	37
24	762889	2.96	911226	1.50	851664	4.46	148336	36
25	763067	2.96	911136	1.50	851931	4.46	148069	35
26	763245	2.96	911046	1.50	852199	4.46	147801	34
27	763422	2.96	910956	1.50	852466	4.46	147534	33
28	763600	2.95	910866	1.50	852733	4.45	147267	32
29	763777	2.95	910776	1.50	853001	4.45	146999	31
30	763954	2.95	910686	1.50	853268	4.45	146732	30
31	9.764131	2.95	9.910596	1.50	9.853535	4.45	10.146465	29
32	764308	2.95	910506	1.50	853802	4.45	146198	28
33	764485	2.94	910415	1.50	854069	4.45	145931	27
34	764662	2.94	910325	1.51	854336	4.45	145664	26
35	764838	2.94	910235	1.51	854603	4.45	145397	25
36	765015	2.94	910144	1.51	854870	4.45	145130	24
37	765191	2.94	910054	1.51	855137	4.45	144863	23
38	765367	2.94	909963	1.51	855404	4.45	144596	22
39	765544	2.93	909873	1.51	855671	4.44	144329	21
40	765720	2.93	909782	1.51	855938	4.44	144062	20
41	9.765896	2.93	9.909691	1.51	9.856204	4.44	10.143796	19
42	766072	2.93	909601	1.51	856471	4.44	143529	18
43	766247	2.93	909510	1.51	856737	4.44	143263	17
44	766423	2.93	909419	1.51	857004	4.44	142996	16
45	766598	2.92	909328	1.52	857270	4.44	142730	15
46	766774	2.92	909237	1.52	857537	4.44	142463	14
47	766949	2.92	909146	1.52	857803	4.44	142197	13
48	767124	2.92	909055	1.52	858069	4.44	141931	12
49	767300	2.92	908964	1.52	858336	4.44	141664	11
50	767475	2.91	908873	1.52	858602	4.43	141398	10
51	9.767649	2.91	9.908781	1.52	9.858868	4.43	10.141132	9
52	767824	2.91	908690	1.52	859134	4.43	140866	8
53	767999	2.91	908609	1.52	859400	4.43	140600	7
54	768173	2.91	908507	1.52	859666	4.43	140334	6
55	768348	2.90	908416	1.53	859932	4.43	140068	5
56	768522	2.90	908324	1.53	860198	4.43	139802	4
57	768697	2.90	908233	1.53	860464	4.43	139536	3
58	768871	2.90	908141	1.53	860730	4.43	139270	2
59	769045	2.90	908049	1.53	860995	4.43	139005	1
60	769219	2.90	907958	1.53	861261	4.43	138739	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.769219	2.90	9.907958	1.53	9.861261	4.43	10.138739	60
1	769393	2.89	907866	1.53	861527	4.43	138473	59
2	769366	2.89	907774	1.53	861792	4.42	138208	58
3	769740	2.89	907682	1.53	862058	4.42	137942	57
4	769913	2.89	907590	1.53	862323	4.42	137677	56
5	770087	2.89	907498	1.53	862589	4.42	137411	55
6	770260	2.88	907406	1.53	862854	4.42	137146	54
7	770433	2.88	907314	1.54	863119	4.42	136881	53
8	770606	2.88	907222	1.54	863385	4.42	136615	52
9	770779	2.88	907129	1.54	863650	4.42	136350	51
10	770952	2.88	907037	1.54	863915	4.42	136085	50
11	9.771125	2.88	9.906945	1.54	9.864180	4.42	10.135820	49
12	771298	2.87	906852	1.54	864445	4.42	135555	48
13	771470	2.87	906760	1.54	864710	4.42	135290	47
14	771643	2.87	906667	1.54	864975	4.41	135025	46
15	771815	2.87	906575	1.54	865240	4.41	134760	45
16	771987	2.87	906482	1.54	865505	4.41	134495	44
17	772159	2.87	906389	1.55	865770	4.41	134230	43
18	772331	2.86	906296	1.55	866035	4.41	133965	42
19	772503	2.86	906204	1.55	866300	4.41	133700	41
20	772675	2.86	906111	1.55	866564	4.41	133436	40
21	9.772847	2.86	9.906018	1.55	9.866829	4.41	10.133171	39
22	773018	2.86	905925	1.55	867094	4.41	132906	38
23	773190	2.86	905832	1.55	867358	4.41	132642	37
24	773361	2.85	905739	1.55	867623	4.41	132377	36
25	773533	2.85	905645	1.55	867887	4.41	132113	35
26	773704	2.85	905552	1.55	868152	4.40	131848	34
27	773875	2.85	905459	1.55	868416	4.40	131584	33
28	774046	2.85	905366	1.56	868680	4.40	131320	32
29	774217	2.85	905272	1.56	868945	4.40	131055	31
30	774388	2.84	905179	1.56	869209	4.40	130794	30
31	9.774558	2.84	9.905085	1.56	9.869473	4.40	10.130527	29
32	774729	2.84	904992	1.56	869737	4.40	130263	28
33	774899	2.84	904898	1.56	870001	4.40	129999	27
34	775070	2.84	904804	1.56	870265	4.40	129735	26
35	775240	2.84	904711	1.56	870529	4.40	129471	25
36	775410	2.83	904617	1.56	870793	4.40	129207	24
37	775580	2.83	904523	1.56	871057	4.40	128943	23
38	775750	2.83	904429	1.57	871321	4.40	128679	22
39	775920	2.83	904335	1.57	871585	4.40	128415	21
40	776090	2.83	904241	1.57	871849	4.39	128151	20
41	9.776259	2.83	9.904147	1.57	9.872112	4.39	10.127888	19
42	776429	2.82	904053	1.57	872376	4.39	127624	18
43	776598	2.82	903959	1.57	872640	4.39	127360	17
44	776768	2.82	903864	1.57	872903	4.39	127097	16
45	776937	2.82	903770	1.57	873167	4.39	126833	15
46	777106	2.82	903676	1.57	873430	4.39	126570	14
47	777275	2.81	903581	1.57	873694	4.39	126306	13
48	777444	2.81	903487	1.57	873957	4.39	126043	12
49	777613	2.81	903392	1.58	874220	4.39	125780	11
50	777781	2.81	903298	1.58	874484	4.39	125516	10
51	9.777950	2.81	9.903203	1.58	9.874747	4.39	10.125253	9
52	778119	2.81	903108	1.58	875010	4.39	124990	8
53	778287	2.80	903014	1.58	875273	4.38	124727	7
54	778455	2.80	902919	1.58	875536	4.38	124464	6
55	778624	2.80	902824	1.58	875800	4.38	124200	5
56	778792	2.80	902729	1.58	876063	4.38	123937	4
57	778960	2.80	902634	1.58	876326	4.38	123674	3
58	779128	2.80	902539	1.59	876589	4.38	123411	2
59	779295	2.79	902444	1.59	876851	4.38	123149	1
60	779463	2.79	902349	1.59	877114	4.38	122886	0
	Cosine	D.	Sine	D.	Tang.	D.	Cotang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.779463	2.79	9.902349	1.59	9.877114	4.38	10.122886	60
1	779631	2.79	902253	1.59	877377	4.38	122623	59
2	779798	2.79	902158	1.59	877640	4.38	122360	58
3	779966	2.79	902063	1.59	877903	4.38	122097	57
4	780133	2.79	901967	1.59	878165	4.38	121835	56
5	780300	2.78	901872	1.59	878428	4.38	121572	55
6	780467	2.78	901776	1.59	878691	4.38	121309	54
7	780634	2.78	901681	1.59	878953	4.37	121047	53
8	780801	2.78	901585	1.59	879216	4.37	120784	52
9	780968	2.78	901490	1.59	879478	4.37	120522	51
10	781134	2.78	901394	1.60	879741	4.37	120259	50
11	9.781301	2.77	9.901298	1.60	9.880003	4.37	10.119997	49
12	781468	2.77	901202	1.60	880265	4.37	119735	48
13	781634	2.77	901106	1.60	880528	4.37	119472	47
14	781800	2.77	901010	1.60	880790	4.37	119210	46
15	781966	2.77	900914	1.60	881052	4.37	118948	45
16	782132	2.77	900818	1.60	881314	4.37	118686	44
17	782298	2.76	900722	1.60	881576	4.37	118424	43
18	782464	2.76	900626	1.60	881839	4.37	118161	42
19	782630	2.76	900529	1.60	882101	4.37	117899	41
20	782796	2.76	900433	1.61	882363	4.36	117637	40
21	9.782961	2.76	9.900337	1.61	9.882625	4.36	10.117375	39
22	783127	2.76	900240	1.61	882887	4.36	117113	38
23	783292	2.75	900144	1.61	883148	4.36	116852	37
24	783458	2.75	900047	1.61	883410	4.36	116590	36
25	783623	2.75	899951	1.61	883672	4.36	116328	35
26	783788	2.75	899854	1.61	883934	4.36	116066	34
27	783953	2.75	899757	1.61	884196	4.36	115804	33
28	784118	2.75	899660	1.61	884457	4.36	115543	32
29	784282	2.74	899564	1.61	884719	4.36	115281	31
30	784447	2.74	899467	1.62	884980	4.36	115020	30
31	9.784612	2.74	9.899370	1.62	9.885242	4.36	10.114758	29
32	784776	2.74	899273	1.62	885503	4.36	114497	28
33	784941	2.74	899176	1.62	885765	4.36	114235	27
34	785105	2.74	899078	1.62	886026	4.36	113974	26
35	785269	2.73	898981	1.62	886288	4.36	113712	25
36	785433	2.73	898884	1.62	886549	4.35	113451	24
37	785597	2.73	898787	1.62	886810	4.35	113190	23
38	785761	2.73	898689	1.62	887072	4.35	112928	22
39	785925	2.73	898592	1.62	887333	4.35	112667	21
40	786089	2.73	898494	1.63	887594	4.35	112406	20
41	9.786252	2.72	9.898397	1.63	9.887855	4.35	10.112145	19
42	786416	2.72	898299	1.63	888116	4.35	111884	18
43	786579	2.72	898202	1.63	888377	4.35	111623	17
44	786742	2.72	898104	1.63	888639	4.35	111361	16
45	786906	2.72	898006	1.63	888900	4.35	111100	15
46	787069	2.72	897908	1.63	889160	4.35	110840	14
47	787232	2.71	897810	1.63	889421	4.35	110579	13
48	787395	2.71	897712	1.63	889682	4.35	110318	12
49	787557	2.71	897614	1.63	889943	4.35	110057	11
50	787720	2.71	897516	1.63	890204	4.34	109796	10
51	9.787883	2.71	9.897418	1.64	9.890465	4.34	10.109535	9
52	788045	2.71	897320	1.64	890725	4.34	109275	8
53	788208	2.71	897222	1.64	890986	4.34	109014	7
54	788370	2.70	897123	1.64	891247	4.34	108753	6
55	788532	2.70	897025	1.64	891507	4.34	108493	5
56	788694	2.70	896926	1.64	891768	4.34	108232	4
57	788856	2.70	896828	1.64	892028	4.34	107972	3
58	789018	2.70	896729	1.64	892289	4.34	107711	2
59	789180	2.70	896631	1.64	892549	4.34	107451	1
60	789342	2.69	896532	1.64	892810	4.34	107190	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.789342	2.69	9.896532	1.64	9.892810	4.34	10.107190	60
1	789504	2.69	896433	1.65	893070	4.34	106930	59
2	789665	2.69	896335	1.65	893331	4.34	106669	58
3	789827	2.69	896236	1.65	893591	4.34	106409	57
4	789988	2.69	896137	1.65	893851	4.34	106149	56
5	790149	2.69	896038	1.65	894111	4.34	105889	55
6	790310	2.68	895939	1.65	894371	4.34	105629	54
7	790471	2.68	895840	1.65	894632	4.33	105368	53
8	790632	2.68	895741	1.65	894892	4.33	105108	52
9	790793	2.68	895641	1.65	895152	4.33	104848	51
10	790954	2.68	895542	1.65	895412	4.33	104588	50
11	9.791115	2.68	9.895443	1.66	9.895672	4.33	10.104328	49
12	791275	2.67	895343	1.66	895932	4.33	104068	48
13	791436	2.67	895244	1.66	896192	4.33	103808	47
14	791596	2.67	895145	1.66	896452	4.33	103548	46
15	791757	2.67	895045	1.66	896712	4.33	103288	45
16	791917	2.67	894945	1.66	896971	4.33	103029	44
17	792077	2.67	894846	1.66	897231	4.33	102769	43
18	792237	2.66	894746	1.66	897491	4.33	102509	42
19	792397	2.66	894646	1.66	897751	4.33	102249	41
20	792557	2.66	894546	1.66	898010	4.33	101990	40
21	9.792716	2.66	9.894446	1.67	9.898270	4.33	10.101730	39
22	792876	2.66	894346	1.67	898530	4.33	101470	38
23	793035	2.66	894246	1.67	898789	4.33	101211	37
24	793195	2.65	894146	1.67	899049	4.32	100951	36
25	793354	2.65	894046	1.67	899308	4.32	100692	35
26	793514	2.65	893946	1.67	899568	4.32	100432	34
27	793673	2.65	893846	1.67	899827	4.32	100173	33
28	793832	2.65	893745	1.67	900086	4.32	999914	32
29	793991	2.65	893645	1.67	900346	4.32	999654	31
30	794150	2.64	893544	1.67	900605	4.32	999395	30
31	9.794308	2.64	9.893444	1.68	9.900864	4.32	10.099136	29
32	794467	2.64	893343	1.68	901124	4.32	998876	28
33	794626	2.64	893243	1.68	901383	4.32	998617	27
34	794784	2.64	893142	1.68	901642	4.32	998358	26
35	794942	2.64	893041	1.68	901901	4.32	998099	25
36	795101	2.64	892940	1.68	902160	4.32	997840	24
37	795259	2.63	892839	1.68	902419	4.32	997581	23
38	795417	2.63	892739	1.68	902679	4.32	997321	22
39	795575	2.63	892638	1.68	902938	4.32	997062	21
40	795733	2.63	892536	1.68	903197	4.31	996803	20
41	9.795891	2.63	9.892435	1.69	9.903455	4.31	10.096545	19
42	796049	2.63	892334	1.69	903714	4.31	996286	18
43	796206	2.63	892233	1.69	903973	4.31	996027	17
44	796364	2.62	892132	1.69	904232	4.31	995768	16
45	796521	2.62	892030	1.69	904491	4.31	995509	15
46	796679	2.62	891929	1.69	904750	4.31	995250	14
47	796836	2.62	891827	1.69	905008	4.31	994992	13
48	796993	2.62	891726	1.69	905267	4.31	994733	12
49	797150	2.61	891624	1.69	905526	4.31	994474	11
50	797307	2.61	891523	1.70	905784	4.31	994216	10
51	9.797464	2.61	9.891421	1.70	9.906043	4.31	10.093957	9
52	797621	2.61	891319	1.70	906302	4.31	993698	8
53	797777	2.61	891217	1.70	906560	4.31	993440	7
54	797934	2.61	891115	1.70	906819	4.31	993181	6
55	798091	2.61	891013	1.70	907077	4.31	992923	5
56	798247	2.61	890911	1.70	907336	4.31	992664	4
57	798403	2.60	890809	1.70	907594	4.31	992406	3
58	798560	2.60	890707	1.70	907852	4.31	992148	2
59	798716	2.60	890605	1.70	908111	4.30	991889	1
60	798872	2.60	890503	1.70	908369	4.30	991631	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.798872	2.60	9.890503	1.70	9.908369	4.30	10.091631	60
1	799028	2.60	890400	1.71	908628	4.30	091372	59
2	799184	2.60	890298	1.71	908886	4.30	091114	58
3	799339	2.59	890195	1.71	909144	4.30	090856	57
4	799495	2.59	890093	1.71	909402	4.30	090598	56
5	799651	2.59	889990	1.71	909660	4.30	090340	55
6	799806	2.59	889888	1.71	909918	4.30	090082	54
7	799962	2.59	889785	1.71	910177	4.30	089823	53
8	800117	2.59	889682	1.71	910435	4.30	089565	52
9	800272	2.58	889579	1.71	910693	4.30	089307	51
10	800427	2.58	889477	1.71	910951	4.30	089049	50
11	9.800582	2.58	9.889374	1.72	9.911209	4.30	10.088791	49
12	800737	2.58	889271	1.72	911467	4.30	088533	48
13	800892	2.58	889168	1.72	911724	4.30	088276	47
14	801047	2.58	889064	1.72	911982	4.30	088018	46
15	801201	2.58	888961	1.72	912240	4.30	087760	45
16	801356	2.57	888858	1.72	912498	4.30	087502	44
17	801511	2.57	888755	1.72	912756	4.30	087244	43
18	801665	2.57	888651	1.72	913014	4.29	086986	42
19	801819	2.57	888548	1.72	913271	4.29	086729	41
20	801973	2.57	888444	1.73	913529	4.29	086471	40
21	9.802128	2.57	9.888341	1.73	9.913787	4.29	10.086213	39
22	802282	2.56	888237	1.73	914044	4.29	085956	38
23	802436	2.56	888134	1.73	914302	4.29	085698	37
24	802589	2.56	888030	1.73	914560	4.29	085440	36
25	802743	2.56	887926	1.73	914817	4.29	085183	35
26	802897	2.56	887822	1.73	915075	4.29	084925	34
27	803050	2.56	887718	1.73	915332	4.29	084668	33
28	803204	2.56	887614	1.73	915590	4.29	084410	32
29	803357	2.55	887510	1.73	915847	4.29	084153	31
30	803511	2.55	887406	1.74	916104	4.29	083896	30
31	9.803664	2.55	9.887302	1.74	9.916362	4.29	10.083638	29
32	803817	2.55	887198	1.74	916619	4.29	083381	28
33	803970	2.55	887093	1.74	916877	4.29	083123	27
34	804123	2.55	886989	1.74	917134	4.29	082866	26
35	804276	2.54	886885	1.74	917391	4.29	082609	25
36	804428	2.54	886780	1.74	917648	4.29	082352	24
37	804581	2.54	886676	1.74	917905	4.29	082095	23
38	804734	2.54	886571	1.74	918163	4.28	081837	22
39	804886	2.54	886466	1.74	918420	4.28	081580	21
40	805039	2.54	886362	1.75	918677	4.28	081323	20
41	9.805191	2.54	9.886257	1.75	9.918934	4.28	10.081066	19
42	805343	2.53	886152	1.75	919191	4.28	080809	18
43	805495	2.53	886047	1.75	919448	4.28	080552	17
44	805647	2.53	885942	1.75	919705	4.28	080295	16
45	805799	2.53	885837	1.75	919962	4.28	080038	15
46	805951	2.53	885732	1.75	920219	4.28	079781	14
47	806103	2.53	885627	1.75	920476	4.28	079524	13
48	806254	2.53	885522	1.75	920733	4.28	079267	12
49	806406	2.52	885416	1.75	920990	4.28	079010	11
50	806557	2.52	885311	1.76	921247	4.28	078753	10
51	9.806709	2.52	9.885205	1.76	9.921503	4.28	10.078497	9
52	806860	2.52	885100	1.76	921760	4.28	078240	8
53	807011	2.52	884994	1.76	922017	4.28	077983	7
54	807163	2.52	884889	1.76	922274	4.28	077726	6
55	807314	2.52	884783	1.76	922530	4.28	077470	5
56	807465	2.51	884677	1.76	922787	4.28	077213	4
57	807615	2.51	884572	1.76	923044	4.28	076956	3
58	807766	2.51	884466	1.76	923300	4.28	076700	2
59	807917	2.51	884360	1.76	923557	4.27	076443	1
60	808067	2.51	884254	1.77	923813	4.27	076187	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.808067	2.51	9.884254	1.77	9.923813	4.27	10.076187	60
1	808218	2.51	884148	1.77	924070	4.27	075930	59
2	808368	2.51	884042	1.77	924327	4.27	075673	58
3	808519	2.50	883936	1.77	924583	4.27	075417	57
4	808669	2.50	883829	1.77	924840	4.27	075160	56
5	808819	2.50	883723	1.77	925096	4.27	074904	55
6	808969	2.50	883617	1.77	925352	4.27	074648	54
7	809119	2.50	883510	1.77	925609	4.27	074391	53
8	809269	2.50	883404	1.77	925865	4.27	074135	52
9	809419	2.49	883297	1.78	926122	4.27	073878	51
10	809569	2.49	883191	1.78	926378	4.27	073622	50
11	9.809718	2.49	9.883084	1.78	9.926634	4.27	10.073366	49
12	809868	2.49	882977	1.78	926890	4.27	073110	48
13	810017	2.49	882871	1.78	927147	4.27	072853	47
14	810167	2.49	882764	1.78	927403	4.27	072597	46
15	810316	2.48	882657	1.78	927659	4.27	072341	45
16	810465	2.48	882550	1.78	927915	4.27	072085	44
17	810614	2.48	882443	1.78	928171	4.27	071829	43
18	810763	2.48	882336	1.79	928427	4.27	071573	42
19	810912	2.48	882229	1.79	928683	4.27	071317	41
20	811061	2.48	882121	1.79	928940	4.27	071060	40
21	9.811210	2.48	9.882014	1.79	9.929196	4.27	10.070804	39
22	811358	2.47	881907	1.79	929452	4.27	070548	38
23	811507	2.47	881799	1.79	929708	4.27	070292	37
24	811655	2.47	881692	1.79	929964	4.26	070036	36
25	811804	2.47	881584	1.79	930220	4.26	069780	35
26	811952	2.47	881477	1.79	930475	4.26	069525	34
27	812100	2.47	881369	1.79	930731	4.26	069269	33
28	812248	2.47	881261	1.80	930987	4.26	069013	32
29	812396	2.46	881153	1.80	931243	4.26	068757	31
30	812544	2.46	881046	1.80	931499	4.26	068501	30
31	9.812692	2.46	9.880938	1.80	9.931755	4.26	10.068245	29
32	812840	2.46	880830	1.80	932010	4.26	067990	28
33	812988	2.46	880722	1.80	932266	4.26	067734	27
34	813135	2.46	880613	1.80	932522	4.26	067478	26
35	813283	2.46	880505	1.80	932778	4.26	067222	25
36	813430	2.45	880397	1.80	933033	4.26	066967	24
37	813578	2.45	880289	1.81	933289	4.26	066711	23
38	813725	2.45	880180	1.81	933545	4.26	066455	22
39	813872	2.45	880072	1.81	933800	4.26	066200	21
40	814019	2.45	879963	1.81	934056	4.26	065944	20
41	9.814166	2.45	9.879855	1.81	9.934311	4.26	10.065689	19
42	814313	2.45	879746	1.81	934567	4.26	065433	18
43	814460	2.44	879637	1.81	934823	4.26	065177	17
44	814607	2.44	879529	1.81	935078	4.26	064922	16
45	814753	2.44	879420	1.81	935333	4.26	064667	15
46	814900	2.44	879311	1.81	935589	4.26	064411	14
47	815046	2.44	879202	1.82	935844	4.26	064156	13
48	815193	2.44	879093	1.82	936100	4.26	063900	12
49	815339	2.44	878984	1.82	936355	4.26	063645	11
50	815485	2.43	878875	1.82	936610	4.26	063390	10
51	9.815631	2.43	9.878766	1.82	9.936866	4.25	10.063134	9
52	815778	2.43	878656	1.82	937121	4.25	062879	8
53	815924	2.43	878547	1.82	937376	4.25	062624	7
54	816069	2.43	878438	1.82	937632	4.25	062368	6
55	816215	2.43	878328	1.82	937887	4.25	062113	5
56	816361	2.43	878219	1.83	938142	4.25	061858	4
57	816507	2.42	878109	1.83	938398	4.25	061602	3
58	816652	2.42	877999	1.83	938653	4.25	061347	2
59	816798	2.42	877890	1.83	938908	4.25	061092	1
60	816943	2.42	877780	1.83	939163	4.25	060837	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.816943	2.42	9.877780	1.83	9.939163	4.25	10.060837	60
1	817088	2.42	877670	1.83	939418	4.25	060582	59
2	817233	2.42	877560	1.83	939673	4.25	060327	58
3	817379	2.42	877450	1.83	939928	4.25	060072	57
4	817524	2.41	877340	1.83	940183	4.25	059817	56
5	817668	2.41	877230	1.84	940438	4.25	059562	55
6	817813	2.41	877120	1.84	940694	4.25	059306	54
7	817958	2.41	877010	1.84	940949	4.25	059051	53
8	818103	2.41	876899	1.84	941204	4.25	058796	52
9	818247	2.41	876789	1.84	941458	4.25	058542	51
10	818392	2.41	876678	1.84	941714	4.25	058286	50
11	9.818536	2.40	9.876568	1.84	9.941968	4.25	10.058032	49
12	818681	2.40	876457	1.84	942223	4.25	057777	48
13	818825	2.40	876347	1.84	942478	4.25	057522	47
14	818969	2.40	876236	1.85	942733	4.25	057267	46
15	819113	2.40	876125	1.85	942988	4.25	057012	45
16	819257	2.40	876014	1.85	943243	4.25	056757	44
17	819401	2.40	875904	1.85	943498	4.25	056502	43
18	819545	2.39	875793	1.85	943753	4.25	056248	42
19	819689	2.39	875682	1.85	944007	4.25	055993	41
20	819832	2.39	875571	1.85	944262	4.25	055738	40
21	9.819976	2.39	9.875459	1.85	9.944517	4.25	10.055483	39
22	820120	2.39	875348	1.85	944771	4.24	055229	38
23	820263	2.39	875237	1.85	945026	4.24	054974	37
24	820406	2.39	875126	1.86	945281	4.24	054719	36
25	820550	2.38	875014	1.86	945535	4.24	054465	35
26	820693	2.38	874903	1.86	945790	4.24	054210	34
27	820836	2.38	874791	1.86	946045	4.24	053955	33
28	820979	2.38	874680	1.86	946299	4.24	053701	32
29	821122	2.38	874568	1.86	946554	4.24	053446	31
30	821265	2.38	874456	1.86	946808	4.24	053192	30
31	9.821407	2.38	9.874344	1.86	9.947063	4.24	10.052937	29
32	821550	2.38	874232	1.87	947318	4.24	052682	28
33	821693	2.38	874121	1.87	947572	4.24	052428	27
34	821835	2.37	874009	1.87	947826	4.24	052174	26
35	821977	2.37	873896	1.87	948081	4.24	051919	25
36	822120	2.37	873784	1.87	948336	4.24	051664	24
37	822262	2.37	873672	1.87	948590	4.24	051410	23
38	822404	2.37	873560	1.87	948844	4.24	051156	22
39	822546	2.37	873448	1.87	949099	4.24	050901	21
40	822688	2.36	873335	1.87	949353	4.24	050647	20
41	9.822830	2.36	9.873223	1.87	9.949607	4.24	10.050393	19
42	822972	2.36	873110	1.88	949862	4.24	050138	18
43	823114	2.36	872998	1.88	950116	4.24	049884	17
44	823255	2.36	872885	1.88	950370	4.24	049630	16
45	823397	2.36	872772	1.88	950625	4.24	049375	15
46	823539	2.36	872659	1.88	950879	4.24	049121	14
47	823680	2.35	872547	1.88	951133	4.24	048867	13
48	823821	2.35	872434	1.88	951388	4.24	048612	12
49	823963	2.35	872321	1.88	951642	4.24	048358	11
50	824104	2.35	872208	1.88	951896	4.24	048104	10
51	9.824245	2.35	9.872095	1.89	9.952150	4.24	10.047850	9
52	824386	2.35	871981	1.89	952405	4.24	047595	8
53	824527	2.35	871868	1.89	952659	4.24	047341	7
54	824668	2.34	871755	1.89	952913	4.24	047087	6
55	824808	2.34	871641	1.89	953167	4.23	046833	5
56	824949	2.34	871528	1.89	953421	4.23	046579	4
57	825090	2.34	871414	1.89	953675	4.23	046325	3
58	825230	2.34	871301	1.89	953929	4.23	046071	2
59	825371	2.34	871187	1.89	954183	4.23	045817	1
60	825511	2.34	871073	1.90	954437	4.23	045563	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.825511	2.34	9.871073	1.90	9.954437	4.23	10.045563	60
1	825651	2.33	870960	1.90	954691	4.23	045309	59
2	825791	2.33	870846	1.90	954945	4.23	045055	58
3	825931	2.33	870732	1.90	955200	4.23	044800	57
4	826071	2.33	870618	1.90	955454	4.23	044546	56
5	826211	2.33	870504	1.90	955707	4.23	044293	55
6	826351	2.33	870390	1.90	955961	4.23	044039	54
7	826491	2.33	870276	1.90	956215	4.23	043785	53
8	826631	2.33	870161	1.90	956469	4.23	043531	52
9	826770	2.32	870047	1.91	956723	4.23	043277	51
10	826910	2.32	869933	1.91	956977	4.23	043023	50
11	9.827049	2.32	9.869818	1.91	9.957231	4.23	10.042769	49
12	827189	2.32	869704	1.91	957485	4.23	042515	48
13	827328	2.32	869589	1.91	957739	4.23	042261	47
14	827467	2.32	869474	1.91	957993	4.23	042007	46
15	827606	2.32	869360	1.91	958246	4.23	041754	45
16	827745	2.32	869245	1.91	958500	4.23	041500	44
17	827884	2.31	869130	1.91	958754	4.23	041246	43
18	828023	2.31	869015	1.92	959008	4.23	040992	42
19	828162	2.31	868900	1.92	959262	4.23	040738	41
20	828301	2.31	868785	1.92	959516	4.23	040484	40
21	9.828439	2.31	9.868670	1.92	9.959769	4.23	10.040231	39
22	828578	2.31	868555	1.92	960023	4.23	039977	38
23	828716	2.31	868440	1.92	960277	4.23	039723	37
24	828855	2.30	868324	1.92	960531	4.23	039469	36
25	828993	2.30	868209	1.92	960784	4.23	039216	35
26	829131	2.30	868093	1.92	961038	4.23	038962	34
27	829269	2.30	867978	1.93	961291	4.23	038709	33
28	829407	2.30	867862	1.93	961545	4.23	038455	32
29	829545	2.30	867747	1.93	961799	4.23	038201	31
30	829683	2.30	867631	1.93	962052	4.23	037948	30
31	9.829821	2.29	9.867515	1.93	9.962306	4.23	10.037694	29
32	829959	2.29	867399	1.93	962560	4.23	037440	28
33	830097	2.29	867283	1.93	962813	4.23	037187	27
34	830234	2.29	867167	1.93	963067	4.23	036933	26
35	830372	2.29	867051	1.93	963320	4.23	036680	25
36	830509	2.29	866935	1.94	963574	4.23	036426	24
37	830646	2.29	866819	1.94	963827	4.23	036173	23
38	830784	2.29	866703	1.94	964081	4.23	035919	22
39	830921	2.28	866586	1.94	964335	4.23	035665	21
40	831058	2.28	866470	1.94	964588	4.22	035412	20
41	9.831195	2.28	9.866353	1.94	9.964842	4.22	10.035158	19
42	831332	2.28	866237	1.94	965095	4.22	034905	18
43	831469	2.28	866120	1.94	965349	4.22	034651	17
44	831606	2.28	866004	1.95	965602	4.22	034398	16
45	831742	2.28	865887	1.95	965855	4.22	034145	15
46	831879	2.28	865770	1.95	966105	4.22	033891	14
47	832015	2.27	865653	1.95	966362	4.22	033638	13
48	832152	2.27	865536	1.95	966616	4.22	033384	12
49	832288	2.27	865419	1.95	966869	4.22	033131	11
50	832425	2.27	865302	1.95	967123	4.22	032877	10
51	9.832561	2.27	9.865185	1.95	9.967376	4.22	10.032624	9
52	832697	2.27	865068	1.95	967629	4.22	032371	8
53	832833	2.27	864950	1.95	967883	4.22	032117	7
54	832969	2.26	864833	1.96	968136	4.22	031864	6
55	833105	2.26	864716	1.96	968389	4.22	031611	5
56	833241	2.26	864598	1.96	968643	4.22	031357	4
57	833377	2.26	864481	1.96	968896	4.22	031104	3
58	833512	2.26	864363	1.96	969149	4.22	030851	2
59	833648	2.26	864245	1.96	969403	4.22	030597	1
60	833783	2.26	864127	1.96	969656	4.22	030344	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.



M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.833783	2.26	9.864127	1.96	9.966656	4.22	10.030344	50
1	833919	2.25	864010	1.96	969909	4.22	030091	59
2	834054	2.25	863892	1.97	970162	4.22	029838	58
3	834189	2.25	863774	1.97	970416	4.22	029584	57
4	834325	2.25	863656	1.97	970669	4.22	029331	56
5	834460	2.25	863538	1.97	970922	4.22	029078	55
6	834595	2.25	863419	1.97	971175	4.22	028825	54
7	834730	2.25	863301	1.97	971429	4.22	028571	53
8	834865	2.25	863183	1.97	971682	4.22	028318	52
9	834999	2.24	863064	1.97	971935	4.22	028065	51
10	835134	2.24	862946	1.98	972188	4.22	027812	50
11	9.835269	2.24	9.862827	1.98	9.972441	4.22	10.027559	49
12	835403	2.24	862709	1.98	972694	4.22	027306	48
13	835538	2.24	862590	1.98	972948	4.22	027052	47
14	835672	2.24	862471	1.98	973201	4.22	026799	46
15	835807	2.24	862353	1.98	973454	4.22	026546	45
16	835941	2.24	862234	1.98	973707	4.22	026293	44
17	836075	2.23	862115	1.98	973960	4.22	026040	43
18	836209	2.23	861996	1.98	974213	4.22	025787	42
19	836343	2.23	861877	1.98	974466	4.22	025534	41
20	836477	2.23	861758	1.99	974719	4.22	025281	40
21	9.836611	2.23	9.861638	1.99	9.974973	4.22	10.025027	39
22	836745	2.23	861519	1.99	975226	4.22	024774	38
23	836878	2.23	861400	1.99	975479	4.22	024521	37
24	837012	2.22	861280	1.99	975732	4.22	024268	36
25	837146	2.22	861161	1.99	975985	4.22	024015	35
26	837279	2.22	861041	1.99	976238	4.22	023762	34
27	837412	2.22	860922	1.99	976491	4.22	023509	33
28	837546	2.22	860802	1.99	976744	4.22	023256	32
29	837679	2.22	860682	2.00	976997	4.22	023003	31
30	837812	2.22	860562	2.00	977250	4.22	022750	30
31	9.837945	2.22	9.860442	2.00	9.977503	4.22	10.022497	29
32	838078	2.21	860322	2.00	977756	4.22	022244	28
33	838211	2.21	860202	2.00	978009	4.22	021991	27
34	838344	2.21	860082	2.00	978262	4.22	021738	26
35	838477	2.21	859962	2.00	978515	4.22	021485	25
36	838610	2.21	859842	2.00	978768	4.22	021232	24
37	838742	2.21	859721	2.01	979021	4.22	020979	23
38	838875	2.21	859601	2.01	979274	4.22	020726	22
39	839007	2.21	859480	2.01	979527	4.22	020473	21
40	839140	2.20	859360	2.01	979780	4.22	020220	20
41	9.839272	2.20	9.859239	2.01	9.980033	4.22	10.019967	19
42	839404	2.20	859119	2.01	980286	4.22	019714	18
43	839536	2.20	858998	2.01	980538	4.22	019462	17
44	839668	2.20	858877	2.01	980791	4.21	019209	16
45	839800	2.20	858756	2.02	981044	4.21	018956	15
46	839932	2.20	858635	2.02	981297	4.21	018703	14
47	840064	2.19	858514	2.02	981550	4.21	018450	13
48	840196	2.19	858393	2.02	981803	4.21	018197	12
49	840328	2.19	858272	2.02	982056	4.21	017944	11
50	840459	2.19	858151	2.02	982309	4.21	017691	10
51	9.840591	2.19	9.858029	2.02	9.982562	4.21	10.017438	9
52	840722	2.19	857908	2.02	982814	4.21	017186	8
53	840854	2.19	857786	2.02	983067	4.21	016933	7
54	840985	2.19	857665	2.03	983320	4.21	016680	6
55	841116	2.18	857543	2.03	983573	4.21	016427	5
56	841247	2.18	857422	2.03	983826	4.21	016174	4
57	841378	2.18	857300	2.03	984079	4.21	015921	3
58	841509	2.18	857178	2.03	984331	4.21	015669	2
59	841640	2.18	857056	2.03	984584	4.21	015416	1
60	841771	2.18	856934	2.03	984837	4.21	015163	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.841771	2.18	9.856934	2.03	9.984837	4.21	10.015163	60
1	841902	2.18	856812	2.03	985090	4.21	014910	59
2	842033	2.18	856690	2.04	985343	4.21	014657	58
3	842163	2.17	856568	2.04	985596	4.21	014404	57
4	842294	2.17	856446	2.04	985848	4.21	014152	56
5	842424	2.17	856323	2.04	986101	4.21	013899	55
6	842555	2.17	856201	2.04	986354	4.21	013646	54
7	842685	2.17	856078	2.04	986607	4.21	013393	53
8	842815	2.17	855956	2.04	986860	4.21	013140	52
9	842946	2.17	855833	2.04	987112	4.21	012888	51
10	843076	2.17	855711	2.05	987365	4.21	012635	50
11	9.843206	2.16	9.855588	2.05	9.987618	4.21	10.012382	49
12	843336	2.16	855465	2.05	987871	4.21	012129	48
13	843466	2.16	855342	2.05	988123	4.21	011877	47
14	843595	2.16	855219	2.05	988376	4.21	011624	46
15	843725	2.16	855096	2.05	988629	4.21	011371	45
16	843855	2.16	854973	2.05	988882	4.21	011118	44
17	843984	2.16	854850	2.05	989134	4.21	010866	43
18	844114	2.15	854727	2.06	989387	4.21	010613	42
19	844243	2.15	854603	2.06	989640	4.21	010360	41
20	844372	2.15	854480	2.06	989893	4.21	010107	40
21	9.844502	2.15	9.854356	2.06	9.990145	4.21	10.009855	39
22	844631	2.15	854233	2.06	990398	4.21	009602	38
23	844760	2.15	854109	2.06	990651	4.21	009349	37
24	844889	2.15	853986	2.06	990903	4.21	009097	36
25	845018	2.15	853862	2.06	991156	4.21	008844	35
26	845147	2.15	853738	2.06	991409	4.21	008591	34
27	845276	2.14	853614	2.07	991662	4.21	008338	33
28	845405	2.14	853490	2.07	991914	4.21	008086	32
29	845533	2.14	853366	2.07	992167	4.21	007833	31
30	845662	2.14	853242	2.07	992420	4.21	007580	30
31	9.845790	2.14	9.853118	2.07	9.992672	4.21	10.007328	29
32	845919	2.14	852994	2.07	992925	4.21	007075	28
33	846047	2.14	852869	2.07	993178	4.21	006822	27
34	846175	2.14	852745	2.07	993430	4.21	006570	26
35	846304	2.14	852620	2.07	993683	4.21	006317	25
36	846432	2.13	852496	2.08	993936	4.21	006064	24
37	846560	2.13	852371	2.08	994189	4.21	005811	23
38	846688	2.13	852247	2.08	994441	4.21	005559	22
39	846816	2.13	852122	2.08	994694	4.21	005306	21
40	846944	2.13	851997	2.08	994947	4.21	005053	20
41	9.847071	2.13	9.851872	2.08	9.995199	4.21	10.004801	19
42	847199	2.13	851747	2.08	995452	4.21	004548	18
43	847327	2.13	851622	2.08	995705	4.21	004295	17
44	847454	2.12	851497	2.09	995957	4.21	004043	16
45	847582	2.12	851372	2.09	996210	4.21	003790	15
46	847709	2.12	851246	2.09	996463	4.21	003537	14
47	847836	2.12	851121	2.09	996715	4.21	003285	13
48	847964	2.12	850996	2.09	996968	4.21	003032	12
49	848091	2.12	850870	2.09	997221	4.21	002779	11
50	848218	2.12	850745	2.09	997473	4.21	002527	10
51	9.848345	2.12	9.850619	2.09	9.997726	4.21	10.002274	9
52	848472	2.11	850493	2.10	997979	4.21	002021	8
53	848599	2.11	850368	2.10	998231	4.21	001769	7
54	848726	2.11	850242	2.10	998484	4.21	001516	6
55	848852	2.11	850116	2.10	998737	4.21	001263	5
56	848979	2.11	849990	2.10	998989	4.21	001011	4
57	849106	2.11	849864	2.10	999242	4.21	000758	3
58	849232	2.11	849738	2.10	999495	4.21	000505	2
59	849359	2.11	849611	2.10	999748	4.21	000253	1
60	849485	2.11	849485	2.10	10.000000	4.21	10.000000	0
	Cosine	D.	Sine	D.	Cotang.	D.	Tang.	M.

M	0 Deg.		1 Deg.		2 Deg.		3 Deg.		4 Deg.		M
	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	
0	00000	Unit.	01745	99985	03490	99930	05234	99863	06976	99756	60
1	00029	I.0000	01774	99984	03519	99938	05263	99861	07005	99754	59
2	00058	I.0000	01803	99984	03548	99937	05292	99860	07034	99752	58
3	00087	I.0000	01832	99983	03577	99936	05321	99858	07063	99750	57
4	00116	I.0000	01862	99983	03606	99935	05350	99857	07092	99748	56
5	00145	I.0000	01891	99982	03635	99934	05379	99855	07121	99746	55
6	00175	I.0000	01920	99982	03664	99933	05408	99854	07150	99744	54
7	00204	I.0000	01949	99981	03693	99932	05437	99852	07179	99742	53
8	00233	I.0000	01978	99980	03723	99931	05466	99851	07208	99740	52
9	00262	I.0000	02007	99980	03752	99930	05495	99849	07237	99738	51
10	00291	I.0000	02036	99979	03781	99929	05524	99847	07266	99736	50
11	00320	99999	02065	99979	03810	99927	05553	99846	07295	99734	49
12	00349	99999	02094	99978	03839	99926	05582	99844	07324	99731	48
13	00378	99999	02123	99977	03868	99925	05611	99842	07353	99729	47
14	00407	99999	02152	99977	03897	99924	05640	99841	07382	99727	46
15	00436	99999	02181	99976	03926	99923	05669	99839	07411	99725	45
16	00465	99999	02211	99976	03955	99922	05698	99838	07440	99723	44
17	00495	99999	02240	99975	03984	99921	05727	99836	07469	99721	43
18	00524	99999	02269	99974	04013	99919	05756	99834	07498	99719	42
19	00553	99998	02298	99974	04042	99918	05785	99833	07527	99716	41
20	00582	99998	02327	99973	04071	99917	05814	99831	07556	99714	40
21	00611	99998	02356	99972	04100	99916	05844	99829	07585	99712	39
22	00640	99998	02385	99972	04129	99915	05873	99827	07614	99710	38
23	00669	99998	02414	99971	04159	99913	05902	99826	07643	99708	37
24	00698	99998	02443	99970	04188	99912	05931	99824	07672	99705	36
25	00727	99997	02472	99969	04217	99911	05960	99822	07701	99703	35
26	00756	99997	02501	99969	04246	99910	05989	99821	07730	99701	34
27	00785	99997	02530	99968	04275	99909	06018	99819	07759	99699	33
28	00814	99997	02560	99967	04304	99907	06047	99817	07788	99696	32
29	00844	99996	02589	99966	04333	99906	06076	99815	07817	99694	31
30	00873	99996	02618	99966	04362	99905	06105	99813	07846	99692	30
31	00902	99996	02647	99965	04391	99904	06134	99812	07875	99689	29
32	00931	99996	02676	99964	04420	99902	06163	99810	07904	99687	28
33	00960	99995	02705	99963	04449	99901	06192	99808	07933	99685	27
34	00989	99995	02734	99963	04478	99900	06221	99806	07962	99683	26
35	01018	99995	02763	99962	04507	99898	06250	99804	07991	99680	25
36	01047	99995	02792	99961	04536	99897	06279	99803	08020	99678	24
37	01076	99994	02821	99960	04565	99896	06308	99801	08049	99676	23
38	01105	99994	02850	99959	04594	99894	06337	99799	08078	99673	22
39	01134	99994	02879	99959	04623	99893	06366	99797	08107	99671	21
40	01164	99993	02908	99958	04653	99892	06395	99795	08136	99668	20
41	01193	99993	02938	99957	04682	99890	06424	99793	08165	99666	19
42	01222	99993	02967	99956	04711	99889	06453	99792	08194	99664	18
43	01251	99992	02996	99955	04740	99888	06482	99790	08223	99661	17
44	01280	99992	03025	99954	04769	99886	06511	99788	08252	99659	16
45	01309	99991	03054	99953	04798	99885	06540	99786	08281	99657	15
46	01338	99991	03083	99952	04827	99883	06569	99784	08310	99654	14
47	01367	99991	03112	99952	04856	99882	06598	99782	08339	99652	13
48	01396	99990	03141	99951	04885	99881	06627	99780	08368	99649	12
49	01425	99990	03170	99950	04914	99879	06656	99778	08397	99647	11
50	01454	99989	03199	99949	04943	99878	06685	99776	08426	99644	10
51	01483	99989	03228	99948	04972	99876	06714	99774	08455	99642	9
52	01513	99989	03257	99947	05001	99875	06743	99772	08484	99639	8
53	01542	99988	03286	99946	05030	99873	06773	99770	08513	99637	7
54	01571	99988	03316	99945	05059	99872	06802	99768	08542	99635	6
55	01600	99987	03345	99944	05088	99870	06831	99766	08571	99632	5
56	01629	99987	03374	99943	05117	99869	06860	99764	08600	99630	4
57	01658	99986	03403	99942	05146	99867	06889	99762	08629	99627	3
58	01687	99986	03432	99941	05175	99866	06918	99760	08658	99625	2
59	01716	99985	03461	99940	05205	99864	06947	99758	08687	99622	1
M	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	M
	89 Deg.		88 Deg.		87 Deg.		86 Deg.		85 Deg.		

M	5 Deg.		6 Deg.		7 Deg.		8 Deg.		9 Deg.		M
	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	
0	08716	99619	10453	99452	12187	99255	13917	99027	15643	98769	60
1	08745	99617	10482	99449	12216	99251	13946	99023	15672	98764	59
2	08774	99614	10511	99446	12245	99248	13975	99019	15701	98760	58
3	08803	99612	10540	99443	12274	99244	14004	99015	15730	98755	57
4	08831	99609	10569	99440	12302	99240	14033	99011	15758	98751	56
5	08860	99607	10597	99437	12331	99237	14061	99006	15787	98746	55
6	08889	99604	10626	99434	12360	99233	14090	99002	15816	98741	54
7	08918	99602	10655	99431	12389	99230	14119	98998	15845	98737	53
8	08947	99599	10684	99428	12418	99226	14148	98994	15873	98732	52
9	08976	99596	10713	99424	12447	99222	14177	98990	15902	98728	51
10	09005	99594	10742	99421	12476	99219	14205	98986	15931	98723	50
11	09034	99591	10771	99418	12504	99215	14234	98982	15959	98718	49
12	09063	99588	10800	99415	12533	99211	14263	98978	15988	98714	48
13	09092	99586	10829	99412	12562	99208	14292	98973	16017	98709	47
14	09121	99583	10858	99409	12591	99204	14320	98969	16046	98704	46
15	09150	99580	10887	99406	12620	99200	14349	98965	16074	98700	45
16	09179	99578	10916	99402	12649	99197	14378	98961	16103	98695	44
17	09208	99575	10945	99399	12678	99193	14407	98957	16132	98690	43
18	09237	99572	10973	99396	12706	99189	14436	98953	16160	98686	42
19	09266	99570	11002	99393	12735	99186	14464	98948	16189	98681	41
20	09295	99567	11031	99390	12764	99182	14493	98944	16218	98676	40
21	09324	99564	11060	99386	12793	99178	14522	98940	16246	98671	39
22	09353	99562	11089	99383	12822	99175	14551	98936	16275	98667	38
23	09382	99559	11118	99380	12851	99171	14580	98931	16304	98662	37
24	09411	99556	11147	99377	12880	99167	14608	98927	16333	98657	36
25	09440	99553	11176	99374	12908	99163	14637	98923	16361	98652	35
26	09469	99551	11205	99370	12937	99160	14666	98919	16390	98648	34
27	09498	99548	11234	99367	12966	99156	14695	98914	16419	98643	33
28	09527	99545	11263	99364	12995	99152	14723	98910	16447	98638	32
29	09556	99542	11291	99360	13024	99148	14752	98906	16476	98633	31
30	09585	99540	11320	99357	13053	99144	14781	98902	16505	98629	30
31	09614	99537	11349	99354	13081	99141	14810	98897	16533	98624	29
32	09642	99534	11378	99351	13110	99137	14838	98893	16562	98619	28
33	09671	99531	11407	99347	13139	99133	14867	98889	16591	98614	27
34	09700	99528	11436	99344	13168	99129	14896	98884	16620	98609	26
35	09729	99526	11465	99341	13197	99125	14925	98880	16648	98604	25
36	09758	99523	11494	99337	13226	99122	14954	98876	16677	98600	24
37	09787	99520	11523	99334	13254	99118	14982	98871	16706	98595	23
38	09816	99517	11552	99331	13283	99114	15011	98867	16734	98590	22
39	09845	99514	11580	99327	13312	99110	15040	98863	16763	98585	21
40	09874	99511	11609	99324	13341	99106	15069	98858	16792	98580	20
41	09903	99508	11638	99320	13370	99102	15097	98854	16820	98575	19
42	09932	99506	11667	99317	13399	99098	15126	98849	16849	98570	18
43	09961	99503	11696	99314	13427	99094	15155	98845	16878	98565	17
44	09990	99500	11725	99310	13456	99091	15184	98841	16906	98561	16
45	10019	99497	11754	99307	13484	99087	15212	98836	16935	98556	15
46	10048	99494	11783	99303	13514	99083	15241	98832	16964	98551	14
47	10077	99491	11812	99300	13543	99079	15270	98827	16992	98546	13
48	10106	99488	11840	99297	13572	99075	15299	98823	17021	98541	12
49	10135	99485	11869	99293	13600	99071	15327	98818	17050	98536	11
50	10164	99482	11898	99290	13629	99067	15356	98814	17078	98531	10
51	10192	99479	11927	99286	13658	99063	15385	98809	17107	98526	9
52	10221	99476	11956	99283	13687	99059	15414	98805	17136	98521	8
53	10250	99473	11985	99279	13716	99055	15442	98800	17164	98516	7
54	10279	99470	12014	99276	13744	99051	15471	98796	17193	98511	6
55	10308	99467	12043	99272	13773	99047	15500	98791	17222	98506	5
56	10337	99464	12071	99269	13802	99043	15529	98787	17250	98501	4
57	10366	99461	12100	99265	13831	99039	15557	98782	17279	98496	3
58	10395	99458	12129	99262	13860	99035	15586	98778	17308	98491	2
59	10424	99455	12158	99258	13889	99031	15615	98773	17336	98486	1
M	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	M
	84 Deg.		83 Deg.		82 Deg.		81 Deg.		80 Deg.		

M	10 Deg.		11 Deg.		12 Deg.		13 Deg.		14 Deg.		M
	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	
0	17365	98481	19081	98163	20791	97815	22495	97437	24192	97030	60
1	17393	98476	19109	98157	20820	97809	22523	97430	24220	97023	59
2	17422	98471	19138	98152	20848	97803	22552	97424	24249	97015	58
3	17451	98466	19167	98146	20877	97797	22580	97417	24277	97008	57
4	17479	98461	19195	98140	20905	97791	22608	97411	24305	97001	56
5	17508	98455	19224	98135	20933	97784	22637	97404	24333	96994	55
6	17537	98450	19252	98129	20962	97778	22665	97398	24362	96987	54
7	17565	98445	19281	98124	20990	97772	22693	97391	24390	96980	53
8	17594	98440	19309	98118	21019	97766	22722	97384	24418	96973	52
9	17623	98435	19338	98112	21047	97760	22750	97378	24446	96966	51
10	17651	98430	19366	98107	21076	97754	22778	97371	24474	96959	50
11	17680	98425	19395	98101	21104	97748	22807	97365	24503	96952	49
12	17708	98420	19423	98096	21132	97742	22835	97358	24531	96945	48
13	17737	98414	19452	98090	21161	97735	22863	97351	24559	96937	47
14	17766	98409	19481	98084	21189	97729	22892	97345	24587	96930	46
15	17794	98404	19509	98079	21218	97723	22920	97338	24615	96923	45
16	17823	98399	19538	98073	21246	97717	22948	97331	24644	96916	44
17	17852	98394	19566	98067	21275	97711	22977	97325	24672	96909	43
18	17880	98389	19595	98061	21303	97705	23005	97318	24700	96902	42
19	17909	98383	19623	98056	21331	97699	23033	97311	24728	96894	41
20	17937	98378	19652	98050	21360	97692	23062	97304	24756	96887	40
21	17966	98373	19680	98044	21388	97686	23090	97298	24784	96880	39
22	17995	98368	19709	98039	21417	97680	23118	97291	24813	96873	38
23	18023	98362	19737	98033	21445	97673	23146	97284	24841	96866	37
24	18052	98357	19766	98027	21474	97667	23175	97278	24869	96858	36
25	18081	98352	19794	98021	21502	97661	23203	97271	24897	96851	35
26	18109	98347	19823	98016	21530	97655	23231	97264	24925	96844	34
27	18138	98341	19851	98010	21559	97648	23260	97257	24953	96837	33
28	18166	98336	19880	98004	21587	97642	23288	97251	24982	96829	32
29	18195	98331	19908	97998	21616	97636	23316	97244	25010	96822	31
30	18224	98325	19937	97992	21644	97630	23345	97237	25038	96815	30
31	18252	98320	19965	97987	21672	97623	23373	97230	25066	96807	29
32	18281	98315	19994	97981	21701	97617	23401	97223	25094	96800	28
33	18309	98310	20022	97975	21729	97611	23429	97217	25122	96793	27
34	18338	98304	20051	97969	21758	97604	23458	97210	25151	96786	26
35	18367	98299	20079	97963	21786	97598	23486	97203	25179	96778	25
36	18395	98294	20108	97958	21814	97592	23514	97196	25207	96771	24
37	18424	98288	20136	97952	21843	97585	23542	97189	25235	96764	23
38	18452	98283	20165	97946	21871	97579	23571	97182	25263	96756	22
39	18481	98277	20193	97940	21899	97573	23599	97176	25291	96749	21
30	18509	98272	20222	97934	21928	97566	23627	97169	25320	96742	20
41	18538	98267	20250	97928	21956	97560	23656	97162	25348	96734	19
42	18567	98261	20279	97922	21985	97553	23684	97155	25376	96727	18
43	18595	98256	20307	97916	22013	97547	23712	97148	25404	96719	17
44	18624	98250	20336	97910	22041	97541	23740	97141	25432	96712	16
45	18652	98245	20364	97905	22070	97534	23769	97134	25460	96705	15
46	18681	98240	20393	97899	22098	97528	23797	97127	25488	96697	14
47	18710	98234	20421	97893	22126	97521	23825	97120	25516	96690	13
48	18738	98229	20450	97887	22155	97515	23853	97113	25545	96682	12
49	18767	98223	20478	97881	22183	97508	23882	97106	25573	96675	11
50	18795	98218	20507	97875	22212	97502	23910	97100	25601	96667	10
51	18824	98212	20535	97869	22240	97496	23938	97093	25629	96660	9
52	18852	98207	20563	97863	22268	97489	23966	97086	25657	96653	8
53	18881	98201	20592	97857	22297	97483	23995	97079	25685	96645	7
54	18910	98196	20620	97851	22325	97476	24023	97072	25713	96638	6
55	18938	98190	20649	97845	22353	97470	24051	97065	25741	96630	5
56	18967	98185	20677	97839	22382	97463	24079	97058	25769	96623	4
57	18995	98179	20706	97833	22410	97457	24108	97051	25798	96615	3
58	19024	98174	20734	97827	22438	97450	24136	97044	25826	96608	2
59	19052	98168	20763	97821	22467	97444	24164	97037	25854	96600	1
M	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	M
	79 Deg.		78 Deg.		77 Deg.		76 Deg.		75 Deg.		

M	15 Deg.		16 Deg.		17 Deg.		18 Deg.		19 Deg.		M
	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	S. C.	
0	25882	96593	27564	96126	29237	95630	30902	95106	32557	94552	60
1	25910	96585	27592	96118	29265	95622	30929	95097	32584	94542	59
2	25938	96578	27620	96110	29293	95613	30957	95088	32612	94533	58
3	25966	96570	27648	96102	29321	95605	30985	95079	32639	94523	57
4	25994	96562	27676	96094	29348	95596	31012	95070	32667	94514	56
5	26022	96555	27704	96086	29376	95588	31040	95061	32694	94504	55
6	26050	96547	27731	96078	29404	95579	31068	95052	32722	94495	54
7	26079	96540	27759	96070	29432	95571	31095	95043	32749	94485	53
8	26107	96532	27787	96062	29460	95562	31123	95033	32777	94476	52
9	26135	96524	27815	96054	29487	95554	31151	95024	32804	94466	51
10	26163	96517	27843	96046	29515	95545	31178	95015	32832	94457	50
11	26191	96509	27871	96037	29543	95536	31206	95006	32859	94447	49
12	26219	96502	27899	96029	29571	95528	31233	94997	32887	94438	48
13	26247	96494	27927	96021	29599	95519	31261	94988	32914	94428	47
14	26275	96486	27955	96013	29626	95511	31289	94979	32942	94418	46
15	26303	96479	27983	96005	29654	95502	31316	94970	32969	94409	45
16	26331	96471	28011	95997	29682	95493	31344	94961	32997	94399	44
17	26359	96463	28039	95989	29710	95485	31372	94952	33024	94390	43
18	26387	96456	28067	95981	29737	95476	31399	94943	33051	94380	42
19	26415	96448	28095	95972	29765	95467	31427	94933	33079	94370	41
20	26443	96440	28123	95964	29793	95459	31454	94924	33106	94361	40
21	26471	96433	28150	95956	29821	95450	31482	94915	33134	94351	39
22	26500	96425	28178	95948	29849	95441	31510	94906	33161	94342	38
23	26528	96417	28206	95940	29876	95433	31537	94897	33189	94332	37
24	26556	96410	28234	95931	29904	95424	31565	94888	33216	94322	36
25	26584	96402	28262	95923	29932	95415	31593	94878	33244	94313	35
26	26612	96394	28290	95915	29960	95407	31620	94869	33271	94303	34
27	26640	96386	28318	95907	29987	95398	31648	94860	33298	94293	33
28	26668	96379	28346	95898	30015	95389	31675	94851	33326	94284	32
29	26696	96371	28374	95890	30043	95380	31703	94842	33353	94274	31
30	26724	96363	28402	95882	30071	95372	31730	94832	33381	94264	30
31	26752	96355	28429	95874	30098	95363	31758	94823	33408	94254	29
32	26780	96347	28457	95865	30126	95354	31786	94814	33436	94245	28
33	26808	96340	28485	95857	30154	95345	31813	94805	33463	94235	27
34	26836	96332	28513	95849	30182	95337	31841	94795	33490	94225	26
35	26864	96324	28541	95841	30209	95328	31868	94786	33518	94215	25
36	26892	96316	28569	95832	30237	95319	31896	94777	33545	94206	24
37	26920	96308	28597	95824	30265	95310	31923	94768	33573	94196	23
38	26948	96301	28625	95816	30292	95301	31951	94758	33600	94186	22
39	26976	96293	28652	95807	30320	95293	31979	94749	33627	94176	21
40	27004	96285	28680	95799	30348	95284	32006	94740	33655	94167	20
41	27032	96277	28708	95791	30376	95275	32034	94730	33682	94157	19
42	27060	96269	28736	95782	30403	95266	32061	94721	33710	94147	18
43	27088	96261	28764	95774	30431	95257	32089	94712	33737	94137	17
44	27116	96253	28792	95766	30459	95248	32116	94702	33764	94127	16
45	27144	96246	28820	95757	30486	95240	32144	94693	33792	94118	15
46	27172	96238	28847	95749	30514	95231	32171	94684	33819	94108	14
47	27200	96230	28875	95740	30542	95222	32199	94674	33846	94098	13
48	27228	96222	28903	95732	30570	95213	32227	94665	33874	94088	12
49	27256	96214	28931	95724	30597	95204	32254	94656	33901	94078	11
50	27284	96206	28959	95715	30625	95195	32282	94646	33929	94068	10
51	27312	96198	28987	95707	30653	95186	32309	94637	33956	94058	9
52	27340	96190	29015	95698	30680	95177	32337	94627	33983	94049	8
53	27368	96182	29042	95690	30708	95168	32364	94618	34011	94039	7
54	27396	96174	29070	95681	30736	95159	32392	94609	34038	94029	6
55	27424	96166	29098	95673	30763	95150	32419	94599	34065	94019	5
56	27452	96158	29126	95664	30791	95142	32447	94590	34093	94009	4
57	27480	96150	29154	95656	30819	95133	32474	94580	34120	93999	3
58	27508	96142	29182	95647	30846	95124	32502	94571	34147	93989	2
59	27536	96134	29209	95639	30874	95115	32529	94561	34175	93979	1
M	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	M
	74 Deg.		73 Deg.		72 Deg.		71 Deg.		70 Deg.		

M	20 Deg.		21 Deg.		22 Deg.		23 Deg.		24 Deg.		M
	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	
0	34202	93969	35837	93358	37461	92718	39073	92050	40674	91355	60
1	34229	93959	35864	93348	37488	92707	39100	92039	40700	91343	59
2	34257	93949	35891	93337	37515	92697	39127	92028	40727	91331	58
3	34284	93939	35918	93327	37542	92686	39153	92016	40753	91319	57
4	34311	93929	35945	93316	37569	92675	39180	92005	40780	91307	56
5	34339	93919	35973	93306	37595	92664	39207	91994	40806	91295	55
6	34366	93909	36000	93295	37622	92653	39234	91982	40833	91283	54
7	34393	93899	36027	93285	37649	92642	39260	91971	40860	91272	53
8	34421	93889	36054	93274	37676	92631	39287	91959	40886	91260	52
9	34448	93879	36081	93264	37703	92620	39314	91948	40913	91248	51
10	34475	93869	36108	93253	37730	92609	39341	91936	40939	91236	50
11	34503	93859	36135	93243	37757	92598	39367	91925	40966	91224	49
12	34530	93849	36162	93232	37784	92587	39394	91914	40992	91212	48
13	34557	93839	36190	93222	37811	92576	39421	91902	41019	91200	47
14	34584	93829	36217	93211	37838	92565	39448	91891	41045	91188	46
15	34612	93819	36244	93201	37865	92554	39474	91879	41072	91176	45
16	34639	93809	36271	93190	37892	92543	39501	91868	41098	91164	44
17	34666	93799	36298	93180	37919	92532	39528	91856	41125	91152	43
18	34694	93789	36325	93169	37946	92521	39555	91845	41151	91140	42
19	34721	93779	36352	93159	37973	92510	39581	91833	41178	91128	41
20	34748	93769	36379	93148	37999	92499	39608	91822	41204	91116	40
21	34775	93759	36406	93137	38026	92488	39635	91810	41231	91104	39
22	34803	93748	36434	93127	38053	92477	39661	91799	41257	91092	38
23	34830	93738	36461	93116	38080	92466	39688	91787	41284	91080	37
24	34857	93728	36488	93106	38107	92455	39715	91775	41310	91068	36
25	34884	93718	36515	93095	38134	92444	39741	91764	41337	91056	35
26	34912	93708	36542	93084	38161	92432	39768	91752	41363	91044	34
27	34939	93698	36569	93074	38188	92421	39795	91741	41390	91032	33
28	34966	93688	36596	93063	38215	92410	39822	91729	41416	91020	32
29	34993	93677	36623	93052	38241	92399	39848	91718	41443	91008	31
30	35021	93667	36650	93042	38268	92388	39875	91706	41469	90996	30
31	35048	93657	36677	93031	38295	92377	39902	91694	41496	90984	29
32	35075	93647	36704	93020	38322	92366	39928	91683	41522	90972	28
33	35102	93637	36731	93010	38349	92355	39955	91671	41549	90960	27
34	35130	93626	36758	92999	38376	92343	39982	91660	41575	90948	26
35	35157	93616	36785	92988	38403	92332	40008	91648	41602	90936	25
36	35183	93606	36812	92978	38430	92321	40035	91636	41628	90924	24
37	35211	93596	36839	92967	38456	92310	40062	91625	41655	90911	23
38	35239	93585	36867	92956	38483	92299	40088	91613	41681	90899	22
39	35266	93575	36894	92945	38510	92287	40115	91601	41707	90887	21
40	35293	93565	36921	92935	38537	92276	40141	91590	41734	90875	20
41	35320	93555	36948	92924	38564	92265	40168	91578	41760	90863	19
42	35347	93544	36975	92913	38591	92254	40195	91566	41787	90851	18
43	35375	93534	37002	92902	38617	92243	40221	91555	41813	90839	17
44	35402	93524	37029	92892	38644	92231	40248	91543	41840	90826	16
45	35429	93514	37056	92881	38671	92220	40275	91531	41866	90814	15
46	35456	93503	37083	92870	38698	92209	40301	91519	41892	90802	14
47	35484	93493	37110	92859	38725	92198	40328	91508	41919	90790	13
48	35511	93483	37137	92849	38752	92186	40355	91496	41945	90778	12
49	35538	93472	37164	92838	38778	92175	40381	91484	41972	90766	11
50	35565	93462	37191	92827	38805	92164	40408	91472	41998	90753	10
51	35592	93452	37218	92816	38832	92152	40434	91461	42024	90741	9
52	35619	93441	37245	92805	38859	92141	40461	91449	42051	90729	8
53	35647	93431	37272	92794	38886	92130	40488	91437	42077	90717	7
54	35674	93420	37299	92784	38912	92119	40514	91425	42104	90704	6
55	35701	93410	37326	92773	38939	92107	40541	91414	42130	90692	5
56	35728	93400	37353	92762	38966	92096	40567	91402	42156	90680	4
57	35755	93389	37380	92751	38993	92085	40594	91390	42183	90668	3
58	35782	93379	37407	92740	39020	92073	40621	91378	42209	90655	2
59	35810	93368	37434	92729	39046	92062	40647	91366	42235	90643	1
M	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	M
	69 Deg.		68 Deg.		67 Deg.		66 Deg.		65 Deg.		

M	25 Deg.		26 Deg.		27 Deg.		28 Deg.		29 Deg.		M
	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	
0	42262	90631	43837	89879	45399	89101	46947	88295	48481	87462	60
1	42288	90618	43863	89867	45425	89087	46973	88281	48506	87448	59
2	42315	90606	43889	89854	45451	89074	46999	88267	48532	87434	58
3	42341	90594	43916	89841	45477	89061	47024	88254	48557	87420	57
4	42367	90582	43942	89828	45503	89048	47050	88240	48583	87406	56
5	42394	90569	43968	89816	45529	89035	47076	88226	48608	87391	55
6	42420	90557	43994	89803	45554	89021	47101	88213	48634	87377	54
7	42446	90545	44020	89790	45580	89008	47127	88199	48659	87363	53
8	42473	90532	44046	89777	45606	88995	47153	88185	48684	87349	52
9	42499	90520	44072	89764	45632	88981	47178	88172	48710	87335	51
10	42525	90507	44098	89752	45658	88968	47204	88158	48735	87321	50
11	42552	90495	44124	89739	45684	88955	47229	88144	48761	87306	49
12	42578	90483	44151	89726	45710	88942	47255	88130	48786	87292	48
13	42604	90470	44177	89713	45736	88928	47281	88117	48811	87278	47
14	42631	90458	44203	89700	45762	88915	47306	88103	48837	87264	46
15	42657	90446	44229	89687	45787	88902	47332	88089	48862	87250	45
16	42683	90433	44255	89674	45813	88888	47358	88075	48888	87235	44
17	42709	90421	44281	89662	45839	88875	47383	88062	48913	87221	43
18	42736	90408	44307	89649	45865	88862	47409	88048	48938	87207	42
19	42762	90396	44333	89636	45891	88848	47434	88034	48964	87193	41
20	42788	90383	44359	89623	45917	88835	47460	88020	48989	87178	40
21	42815	90371	44385	89610	45942	88822	47486	88006	49014	87164	39
22	42841	90358	44411	89597	45968	88808	47511	87993	49040	87150	38
23	42867	90346	44437	89584	45994	88795	47537	87979	49065	87136	37
24	42894	90334	44464	89571	46020	88782	47562	87965	49090	87121	36
25	42920	90321	44490	89558	46046	88768	47588	87951	49116	87107	35
26	42946	90309	44516	89545	46072	88755	47614	87937	49141	87093	34
27	42972	90296	44542	89532	46097	88741	47639	87923	49166	87079	33
28	42999	90284	44568	89519	46123	88728	47665	87909	49192	87064	32
29	43025	90271	44594	89506	46149	88715	47690	87896	49217	87050	31
30	43051	90259	44620	89493	46175	88701	47716	87882	49242	87036	30
31	43077	90246	44646	89480	46201	88688	47741	87868	49268	87021	29
32	43104	90233	44672	89467	46226	88674	47767	87854	49293	87007	28
33	43130	90221	44698	89454	46252	88661	47793	87840	49318	86993	27
34	43156	90208	44724	89441	46278	88647	47818	87826	49344	86978	26
35	43182	90196	44750	89428	46304	88634	47844	87812	49369	86964	25
36	43209	90183	44776	89415	46330	88620	47869	87798	49394	86949	24
37	43235	90171	44802	89402	46355	88607	47895	87784	49419	86935	23
38	43261	90158	44828	89389	46381	88593	47920	87770	49445	86921	22
39	43287	90146	44854	89376	46407	88580	47946	87756	49470	86906	21
40	43313	90133	44880	89363	46433	88566	47971	87743	49495	86892	20
41	43340	90120	44906	89350	46458	88553	47997	87729	49521	86878	19
42	43366	90108	44932	89337	46484	88539	48022	87715	49546	86863	18
43	43392	90095	44958	89324	46510	88526	48048	87701	49571	86849	17
44	43418	90082	44984	89311	46536	88512	48073	87687	49596	86834	16
45	43445	90070	45010	89298	46561	88499	48099	87673	49622	86820	15
46	43471	90057	45036	89285	46587	88485	48124	87659	49647	86805	14
47	43497	90045	45062	89272	46613	88472	48150	87645	49672	86791	13
48	43523	90032	45088	89259	46639	88458	48175	87631	49697	86777	12
49	43549	90019	45114	89245	46664	88445	48201	87617	49723	86762	11
50	43575	90007	45140	89232	46690	88431	48226	87603	49748	86748	10
51	43602	89994	45166	89219	46716	88417	48252	87589	49773	86733	9
52	43628	89981	45192	89206	46742	88404	48277	87575	49798	86719	8
53	43654	89968	45218	89193	46767	88390	48303	87561	49824	86704	7
54	43680	89956	45243	89180	46793	88377	48328	87546	49849	86690	6
55	43706	89943	45269	89167	46819	88363	48354	87532	49874	86675	5
56	43733	89930	45295	89153	46844	88349	48379	87518	49899	86661	4
57	43759	89918	45321	89140	46870	88336	48405	87504	49924	86646	3
58	43785	89905	45347	89127	46896	88322	48430	87490	49950	86632	2
59	43811	89892	45373	89114	46921	88308	48456	87476	49975	86617	1
M	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	M
	64 Deg.		63 Deg.		62 Deg.		61 Deg.		60 Deg.		



M	30 Deg.		31 Deg.		32 Deg.		33 Deg.		34 Deg.		M
	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	
0	50000	86603	51504	85717	52992	84805	54464	83867	55919	82904	60
1	50025	86588	51529	85702	53017	84789	54488	83851	55943	82887	59
2	50050	86573	51554	85687	53041	84774	54513	83835	55968	82871	58
3	50076	86559	51579	85672	53066	84759	54537	83819	55992	82855	57
4	50101	86544	51604	85657	53091	84743	54561	83804	56016	82839	56
5	50126	86530	51628	85642	53115	84728	54586	83788	56040	82822	55
6	50151	86515	51653	85627	53140	84712	54610	83772	56064	82806	54
7	50176	86501	51678	85612	53164	84697	54635	83756	56088	82790	53
8	50201	86486	51703	85597	53189	84681	54659	83740	56112	82773	52
9	50227	86471	51728	85582	53214	84666	54683	83724	56136	82757	51
10	50252	86457	51753	85567	53238	84650	54708	83708	56160	82741	50
11	50277	86442	51778	85551	53263	84635	54732	83692	56184	82724	49
12	50302	86427	51803	85536	53288	84619	54756	83676	56208	82708	48
13	50327	86413	51828	85521	53312	84604	54781	83660	56232	82692	47
14	50352	86398	51852	85506	53337	84588	54805	83645	56256	82675	46
15	50377	86384	51877	85491	53361	84573	54829	83629	56280	82659	45
16	50403	86369	51902	85476	53386	84557	54854	83613	56305	82643	44
17	50428	86354	51927	85461	53411	84542	54878	83597	56329	82626	43
18	50453	86340	51952	85446	53435	84526	54902	83581	56353	82610	42
19	50478	86325	51977	85431	53460	84511	54927	83565	56377	82593	41
20	50503	86310	52002	85416	53484	84495	54951	83549	56401	82577	40
21	50528	86295	52026	85401	53509	84480	54975	83533	56425	82561	39
22	50553	86281	52051	85385	53534	84464	54999	83517	56449	82544	38
23	50578	86266	52076	85370	53558	84448	55024	83501	56473	82528	37
24	50603	86251	52101	85355	53583	84433	55048	83485	56497	82511	36
25	50628	86237	52126	85340	53607	84417	55072	83469	56521	82495	35
26	50654	86222	52151	85325	53632	84402	55097	83453	56545	82478	34
27	50679	86207	52175	85310	53656	84386	55121	83437	56569	82462	33
28	50704	86192	52200	85294	53681	84370	55145	83421	56593	82446	32
29	50729	86178	52225	85279	53705	84355	55169	83405	56617	82429	31
30	50754	86163	52250	85264	53730	84339	55194	83389	56641	82413	30
31	50779	86148	52275	85249	53754	84324	55218	83373	56665	82396	29
32	50804	86133	52299	85234	53779	84308	55242	83356	56689	82380	28
33	50829	86119	52324	85218	53804	84292	55266	83340	56713	82363	27
34	50854	86104	52349	85203	53828	84277	55291	83324	56736	82347	26
35	50879	86089	52374	85188	53853	84261	55315	83308	56760	82330	25
36	50904	86074	52399	85173	53877	84245	55339	83292	56784	82314	24
37	50929	86059	52423	85157	53902	84230	55363	83276	56808	82297	23
38	50954	86045	52448	85142	53926	84214	55388	83260	56832	82281	22
39	50979	86030	52473	85127	53951	84198	55412	83244	56856	82264	21
40	51004	86015	52498	85112	53975	84182	55436	83228	56880	82248	20
41	51029	86000	52522	85096	54000	84167	55460	83212	56904	82231	19
42	51054	85985	52547	85081	54024	84151	55484	83195	56928	82214	18
43	51079	85970	52572	85066	54049	84135	55509	83179	56952	82198	17
44	51104	85956	52597	85051	54073	84120	55533	83163	56976	82181	16
45	51129	85941	52621	85035	54097	84104	55557	83147	57000	82165	15
46	51154	85926	52646	85020	54122	84088	55581	83131	57024	82148	14
47	51179	85911	52671	85005	54146	84072	55605	83115	57047	82132	13
48	51204	85896	52696	84989	54171	84057	55630	83098	57071	82115	12
49	51229	85881	52720	84974	54195	84041	55654	83082	57095	82098	11
50	51254	85866	52745	84959	54220	84025	55678	83066	57119	82082	10
51	51279	85851	52770	84943	54244	84009	55702	83050	57143	82065	9
52	51304	85836	52794	84928	54269	83994	55726	83034	57167	82048	8
53	51329	85821	52819	84913	54293	83978	55750	83017	57191	82032	7
54	51354	85806	52844	84897	54317	83962	55775	83001	57215	82015	6
55	51379	85792	52869	84882	54342	83946	55799	82985	57238	81999	5
56	51404	85777	52893	84866	54366	83930	55823	82969	57262	81982	4
57	51429	85762	52918	84851	54391	83915	55847	82953	57286	81965	3
58	51454	85747	52943	84836	54415	83899	55871	82936	57310	81949	2
59	51479	85732	52967	84820	54440	83883	55895	82920	57334	81932	1
M	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	M
	59 Deg.		58 Deg.		57 Deg.		56 Deg.		55 Deg.		

M	35 Deg.		36 Deg.		37 Deg.		38 Deg.		39 Deg.		M
	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	
0	57358	81915	58779	80902	60182	79864	61566	78801	62932	77715	60
1	57381	81899	58802	80885	60205	79846	61589	78783	62955	77696	59
2	57405	81882	58826	80867	60228	79829	61612	78765	62977	77678	58
3	57429	81865	58849	80850	60251	79811	61635	78747	63000	77660	57
4	57453	81848	58873	80833	60274	79793	61658	78729	63022	77641	56
5	57477	81832	58896	80816	60298	79776	61681	78711	63045	77623	55
6	57501	81815	58920	80799	60321	79758	61704	78694	63068	77605	54
7	57524	81798	58943	80782	60344	79741	61726	78676	63090	77586	53
8	57548	81782	58967	80765	60367	79723	61749	78658	63113	77568	52
9	57572	81765	58990	80748	60390	79706	61772	78640	63135	77550	51
10	57596	81748	59014	80730	60414	79688	61795	78622	63158	77531	50
11	57619	81731	59037	80713	60437	79671	61818	78604	63180	77513	49
12	57643	81714	59061	80696	60460	79653	61841	78586	63203	77494	48
13	57667	81698	59084	80679	60483	79635	61864	78568	63225	77476	47
14	57691	81681	59108	80662	60506	79618	61887	78550	63248	77458	46
15	57715	81664	59131	80644	60529	79600	61909	78532	63271	77439	45
16	57738	81647	59154	80627	60553	79583	61932	78514	63293	77421	44
17	57762	81631	59178	80610	60576	79565	61955	78496	63316	77402	43
18	57786	81614	59201	80593	60599	79547	61978	78478	63338	77384	42
19	57810	81597	59225	80576	60622	79530	62001	78460	63361	77366	41
20	57833	81580	59248	80558	60645	79512	62024	78442	63383	77347	40
21	57857	81563	59272	80541	60668	79494	62046	78424	63406	77329	39
22	57881	81546	59295	80524	60691	79477	62069	78405	63428	77310	38
23	57904	81530	59318	80507	60714	79459	62092	78387	63451	77292	37
24	57928	81513	59342	80489	60738	79441	62115	78369	63473	77273	36
25	57952	81496	59365	80472	60761	79424	62138	78351	63496	77255	35
26	57976	81479	59389	80455	60784	79406	62160	78333	63518	77236	34
27	57999	81462	59412	80438	60807	79388	62183	78315	63540	77218	33
28	58023	81445	59436	80420	60830	79371	62206	78297	63563	77199	32
29	58047	81428	59459	80403	60853	79353	62229	78279	63585	77181	31
30	58070	81412	59482	80386	60876	79335	62251	78261	63608	77162	30
31	58094	81395	59506	80368	60899	79318	62274	78243	63630	77144	29
32	58118	81378	59529	80351	60922	79300	62297	78225	63653	77125	28
33	58141	81361	59552	80334	60945	79282	62320	78206	63675	77107	27
34	58165	81344	59576	80316	60968	79264	62342	78188	63698	77088	26
35	58189	81327	59599	80299	60991	79247	62365	78170	63720	77070	25
36	58212	81310	59622	80282	61015	79229	62388	78152	63742	77051	24
37	58236	81293	59646	80264	61038	79211	62411	78134	63765	77033	23
38	58260	81276	59669	80247	61061	79193	62433	78116	63787	77014	22
39	58283	81259	59693	80230	61084	79176	62456	78098	63810	76996	21
40	58307	81242	59716	80212	61107	79158	62479	78079	63832	76977	20
41	58330	81225	59739	80195	61130	79140	62502	78061	63854	76959	19
42	58354	81208	59763	80178	61153	79122	62524	78043	63877	76940	18
43	58378	81191	59786	80160	61176	79105	62547	78025	63899	76921	17
44	58401	81174	59809	80143	61199	79087	62570	78007	63922	76903	16
45	58425	81157	59832	80125	61222	79069	62592	77988	63944	76884	15
46	58449	81140	59856	80108	61245	79051	62615	77970	63966	76866	14
47	58472	81123	59879	80091	61268	79033	62638	77952	63989	76847	13
48	58496	81106	59902	80073	61291	79015	62660	77934	64011	76828	12
49	58519	81089	59926	80056	61314	78998	62683	77916	64033	76810	11
50	58543	81072	59949	80038	61337	78980	62706	77897	64056	76791	10
51	58567	81055	59972	80021	61360	78962	62728	77879	64078	76772	9
52	58590	81038	59995	80003	61383	78944	62751	77861	64100	76754	8
53	58614	81021	60019	79986	61406	78926	62774	77843	64123	76735	7
54	58637	81004	60042	79968	61429	78908	62796	77824	64145	76717	6
55	58661	80987	60065	79951	61451	78891	62819	77806	64167	76698	5
56	58684	80970	60089	79934	61474	78873	62842	77788	64190	76679	4
57	58708	80953	60112	79916	61497	78855	62864	77769	64212	76661	3
58	58731	80936	60135	79899	61520	78837	62887	77751	64234	76642	2
59	58755	80919	60158	79881	61543	78819	62909	77733	64256	76623	1
M	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	M
	54 Deg.		53 Deg.		52 Deg.		51 Deg.		50 Deg.		

M	40 Deg.		41 Deg.		42 Deg.		43 Deg.		44 Deg.		M
	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	
0	64279	76604	65606	75471	66913	74314	68200	73135	69466	71934	60
1	64301	76586	65628	75452	66935	74295	68221	73116	69487	71914	59
2	64323	76567	65650	75433	66956	74276	68242	73096	69508	71894	58
3	64346	76548	65672	75414	66978	74257	68264	73076	69529	71873	57
4	64368	76530	65694	75395	66999	74237	68285	73056	69549	71853	56
5	64390	76511	65716	75375	67021	74217	68306	73036	69570	71833	55
6	64412	76492	65738	75356	67043	74198	68327	73016	69591	71813	54
7	64435	76473	65759	75337	67064	74178	68349	72996	69612	71792	53
8	64457	76455	65781	75318	67086	74159	68370	72976	69633	71772	52
9	64479	76436	65803	75299	67107	74139	68391	72957	69654	71752	51
10	64501	76417	65825	75280	67129	74120	68412	72937	69675	71732	50
11	64524	76398	65847	75261	67151	74100	68433	72917	69696	71711	49
12	64546	76380	65869	75241	67172	74080	68455	72897	69717	71691	48
13	64568	76361	65891	75222	67194	74061	68476	72877	69737	71671	47
14	64590	76342	65913	75203	67215	74041	68497	72857	69758	71650	46
15	64612	76323	65935	75184	67237	74022	68518	72837	69779	71630	45
16	64635	76304	65956	75165	67258	74002	68539	72817	69800	71610	44
17	64657	76286	65978	75146	67280	73983	68561	72797	69821	71590	43
18	64679	76267	66000	75126	67301	73963	68582	72777	69842	71569	42
19	64701	76248	66022	75107	67323	73944	68603	72757	69862	71549	41
20	64723	76229	66044	75088	67344	73924	68624	72737	69883	71529	40
21	64746	76210	66066	75069	67366	73904	68645	72717	69904	71508	39
22	64768	76192	66088	75050	67387	73885	68666	72697	69925	71488	38
23	64790	76173	66109	75030	67409	73865	68688	72677	69946	71468	37
24	64812	76154	66131	75011	67430	73846	68709	72657	69966	71447	36
25	64834	76135	66153	74992	67452	73826	68730	72637	69987	71427	35
26	64856	76116	66175	74973	67473	73806	68751	72617	70008	71407	34
27	64878	76097	66197	74953	67495	73787	68772	72597	70029	71386	33
28	64901	76078	66218	74934	67516	73767	68793	72577	70049	71366	32
29	64923	76059	66240	74915	67538	73747	68814	72557	70070	71345	31
30	64945	76041	66262	74896	67559	73728	68835	72537	70091	71325	30
31	64967	76022	66284	74876	67580	73708	68857	72517	70112	71305	29
32	64989	76003	66306	74857	67602	73688	68878	72497	70132	71284	28
33	65011	75984	66327	74838	67623	73669	68899	72477	70153	71264	27
34	65033	75965	66349	74818	67645	73649	68920	72457	70174	71243	26
35	65055	75946	66371	74799	67666	73629	68941	72437	70195	71223	25
36	65077	75927	66393	74780	67688	73610	68962	72417	70215	71203	24
37	65099	75908	66414	74760	67709	73590	68983	72397	70236	71182	23
38	65122	75889	66436	74741	67730	73570	69004	72377	70257	71162	22
39	65144	75870	66458	74722	67752	73551	69025	72357	70277	71141	21
40	65166	75851	66480	74703	67773	73531	69046	72337	70298	71121	20
41	65188	75832	66501	74683	67795	73511	69067	72317	70319	71100	19
42	65210	75813	66523	74664	67816	73491	69088	72297	70339	71080	18
43	65232	75794	66545	74644	67837	73472	69109	72277	70360	71059	17
44	65254	75775	66566	74625	67859	73452	69130	72257	70381	71039	16
45	65276	75756	66588	74606	67880	73432	69151	72236	70401	71019	15
46	65298	75738	66610	74586	67901	73412	69172	72216	70422	70998	14
47	65320	75719	66632	74567	67923	73393	69193	72196	70443	70978	13
48	65342	75699	66653	74548	67944	73373	69214	72176	70463	70957	12
49	65364	75680	66675	74528	67965	73353	69235	72156	70484	70937	11
50	65386	75661	66697	74509	67987	73333	69256	72136	70505	70916	10
51	65408	75642	66718	74489	68008	73314	69277	72116	70525	70896	9
52	65430	75623	66740	74470	68029	73294	69298	72095	70546	70875	8
53	65452	75604	66762	74451	68051	73274	69319	72075	70567	70855	7
54	65474	75585	66783	74431	68072	73254	69340	72055	70587	70834	6
55	65496	75566	66805	74412	68093	73234	69361	72035	70608	70813	5
56	65518	75547	66827	74392	68115	73215	69382	72015	70628	70793	4
57	65540	75528	66848	74373	68136	73195	69403	71995	70649	70772	3
58	65562	75509	66870	74353	68157	73175	69424	71974	70670	70752	2
59	65584	75490	66891	74334	68179	73155	69445	71954	70690	70731	1
60	65606	75471	66913	74314	68200	73135	69466	71934	70711	70711	0
M	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	C. S.	S.	M
	49 Deg.		48 Deg.		47 Deg.		46 Deg.		45 Deg.		

## TRAVERSE TABLE.

Distance.	$\frac{1}{4}$ Deg.		$\frac{1}{2}$ Deg.		$\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.00	1.00	0.01	1.00	0.01	1
2	2.00	0.01	2.00	0.02	2.00	0.03	2
3	3.00	0.01	3.00	0.03	3.00	0.04	3
4	4.00	0.02	4.00	0.03	4.00	0.05	4
5	5.00	0.02	5.00	0.04	5.00	0.07	5
6	6.00	0.03	6.00	0.05	6.00	0.08	6
7	7.00	0.03	7.00	0.06	7.00	0.09	7
8	8.00	0.03	8.00	0.07	8.00	0.10	8
9	9.00	0.04	9.00	0.08	9.00	0.12	9
10	10.00	0.04	10.00	0.09	10.00	0.13	10
11	11.00	0.05	11.00	0.10	11.00	0.14	11
12	12.00	0.05	12.00	0.10	12.00	0.16	12
13	13.00	0.06	13.00	0.11	13.00	0.17	13
14	14.00	0.06	14.00	0.12	14.00	0.18	14
15	15.00	0.07	15.00	0.13	15.00	0.20	15
16	16.00	0.07	16.00	0.14	16.00	0.21	16
17	17.00	0.07	17.00	0.15	17.00	0.22	17
18	18.00	0.08	18.00	0.16	18.00	0.24	18
19	19.00	0.08	19.00	0.17	19.00	0.25	19
20	20.00	0.09	20.00	0.17	20.00	0.26	20
21	21.00	0.09	21.00	0.18	21.00	0.27	21
22	22.00	0.10	22.00	0.19	22.00	0.29	22
23	23.00	0.10	23.00	0.20	23.00	0.30	23
24	24.00	0.10	24.00	0.21	24.00	0.31	24
25	25.00	0.11	25.00	0.22	25.00	0.33	25
26	26.00	0.11	26.00	0.23	26.00	0.34	26
27	27.00	0.12	27.00	0.24	27.00	0.35	27
28	28.00	0.12	28.00	0.24	28.00	0.37	28
29	29.00	0.13	29.00	0.25	29.00	0.38	29
30	30.00	0.13	30.00	0.26	30.00	0.39	30
31	31.00	0.14	31.00	0.27	31.00	0.41	31
32	32.00	0.14	32.00	0.28	32.00	0.42	32
33	33.00	0.14	33.00	0.29	33.00	0.43	33
34	34.00	0.15	34.00	0.30	34.00	0.45	34
35	35.00	0.15	35.00	0.31	35.00	0.46	35
36	36.00	0.16	36.00	0.31	36.00	0.47	36
37	37.00	0.16	37.00	0.32	37.00	0.48	37
38	38.00	0.17	38.00	0.33	38.00	0.50	38
39	39.00	0.17	39.00	0.34	39.00	0.51	39
40	40.00	0.17	40.00	0.35	40.00	0.52	40
41	41.00	0.18	41.00	0.36	41.00	0.54	41
42	42.00	0.18	42.00	0.37	42.00	0.55	42
43	43.00	0.19	43.00	0.38	43.00	0.56	43
44	44.00	0.19	44.00	0.38	44.00	0.58	44
45	45.00	0.20	45.00	0.39	45.00	0.59	45
46	46.00	0.20	46.00	0.40	46.00	0.60	46
47	47.00	0.21	47.00	0.41	47.00	0.62	47
48	48.00	0.21	48.00	0.42	48.00	0.63	48
49	49.00	0.21	49.00	0.43	49.00	0.64	49
50	50.00	0.22	50.00	0.44	50.00	0.65	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	$89\frac{3}{4}$ Deg.		$89\frac{1}{2}$ Deg.		$89\frac{1}{4}$ Deg.		

Distance.	$\frac{1}{4}$ Deg.		$\frac{1}{2}$ Deg.		$\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	51.00	0.22	51.00	0.45	51.00	0.67	51
52	52.00	0.23	52.00	0.45	52.00	0.68	52
53	53.00	0.23	53.00	0.46	53.00	0.69	53
54	54.00	0.24	54.00	0.47	54.00	0.71	54
55	55.00	0.24	55.00	0.48	55.00	0.72	55
56	56.00	0.24	56.00	0.49	56.00	0.73	56
57	57.00	0.25	57.00	0.50	57.00	0.75	57
58	58.00	0.25	58.00	0.51	57.99	0.76	58
59	59.00	0.26	59.00	0.51	58.99	0.77	59
60	60.00	0.26	60.00	0.52	59.99	0.79	60
61	61.00	0.27	61.00	0.53	60.99	0.80	61
62	62.00	0.27	62.00	0.54	61.99	0.81	62
63	63.00	0.27	63.00	0.55	62.99	0.82	63
64	64.00	0.28	64.00	0.56	63.99	0.84	64
65	65.00	0.28	65.00	0.57	64.99	0.85	65
66	66.00	0.29	66.00	0.58	65.99	0.86	66
67	67.00	0.29	67.00	0.58	66.99	0.88	67
68	68.00	0.30	68.00	0.59	67.99	0.89	68
69	69.00	0.30	69.00	0.60	68.99	0.90	69
70	70.00	0.31	70.00	0.61	69.99	0.92	70
71	71.00	0.31	71.00	0.62	70.99	0.93	71
72	72.00	0.31	72.00	0.63	71.99	0.94	72
73	73.00	0.32	73.00	0.64	72.99	0.96	73
74	74.00	0.32	74.00	0.65	73.99	0.97	74
75	75.00	0.33	75.00	0.65	74.99	0.98	75
76	76.00	0.33	76.00	0.66	75.99	0.99	76
77	77.00	0.34	77.00	0.67	76.99	1.01	77
78	78.00	0.34	78.00	0.68	77.99	1.02	78
79	79.00	0.34	79.00	0.69	78.99	1.03	79
80	80.00	0.35	80.00	0.70	79.99	1.05	80
81	81.00	0.35	81.00	0.71	80.99	1.06	81
82	82.00	0.36	82.00	0.72	81.99	1.07	82
83	83.00	0.36	83.00	0.72	82.99	1.09	83
84	84.00	0.37	84.00	0.73	83.99	1.10	84
85	85.00	0.37	85.00	0.74	84.99	1.11	85
86	86.00	0.38	86.00	0.75	85.99	1.13	86
87	87.00	0.38	87.00	0.76	86.99	1.14	87
88	88.00	0.38	88.00	0.77	87.99	1.15	88
89	89.00	0.39	89.00	0.78	88.99	1.16	89
90	90.00	0.39	90.00	0.79	89.99	1.18	90
91	91.00	0.40	91.00	0.79	90.99	1.19	91
92	92.00	0.40	92.00	0.80	91.99	1.20	92
93	93.00	0.41	93.00	0.81	92.99	1.22	93
94	94.00	0.41	94.00	0.82	93.99	1.23	94
95	95.00	0.41	95.00	0.83	94.99	1.24	95
96	96.00	0.42	96.00	0.84	95.99	1.26	96
97	97.00	0.42	97.00	0.85	96.99	1.27	97
98	98.00	0.43	98.00	0.86	97.99	1.28	98
99	99.00	0.43	99.00	0.86	98.99	1.30	99
100	100.00	0.44	100.00	0.87	99.99	1.31	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	$89\frac{3}{4}$ Deg.		$89\frac{1}{2}$ Deg.		$89\frac{1}{4}$ Deg.		

Distance.	1 Deg.		1 $\frac{1}{4}$ Deg.		1 $\frac{1}{2}$ Deg.		1 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.02	1.00	0.02	1.00	0.03	1.00	0.03	1
2	2.00	0.03	2.00	0.04	2.00	0.05	2.00	0.06	2
3	3.00	0.05	3.00	0.07	3.00	0.08	3.00	0.09	3
4	4.00	0.07	4.00	0.09	4.00	0.10	4.00	0.12	4
5	5.00	0.09	5.00	0.11	5.00	0.13	5.00	0.15	5
6	6.00	0.10	6.00	0.13	6.00	0.16	6.00	0.18	6
7	7.00	0.12	7.00	0.15	7.00	0.18	7.00	0.21	7
8	8.00	0.14	8.00	0.17	8.00	0.21	8.00	0.25	8
9	9.00	0.16	9.00	0.20	9.00	0.24	9.00	0.28	9
10	10.00	0.17	10.00	0.22	10.00	0.26	10.00	0.31	10
11	11.00	0.19	11.00	0.24	11.00	0.28	10.99	0.34	11
12	12.00	0.21	12.00	0.26	12.00	0.31	11.99	0.37	12
13	13.00	0.23	13.00	0.28	13.00	0.34	12.99	0.40	13
14	14.00	0.24	14.00	0.31	14.00	0.37	13.99	0.43	14
15	15.00	0.26	15.00	0.33	14.99	0.39	14.99	0.46	15
16	16.00	0.28	16.00	0.35	15.99	0.42	15.99	0.49	16
17	17.00	0.30	17.00	0.37	16.99	0.45	16.99	0.52	17
18	18.00	0.31	18.00	0.39	17.99	0.47	17.99	0.55	18
19	19.00	0.33	19.00	0.41	18.99	0.50	18.99	0.58	19
20	20.00	0.35	20.00	0.44	19.99	0.52	19.99	0.61	20
21	21.00	0.37	21.00	0.46	20.99	0.55	20.99	0.64	21
22	22.00	0.38	21.99	0.48	21.99	0.58	21.99	0.67	22
23	23.00	0.40	22.99	0.50	22.99	0.60	22.99	0.70	23
24	24.00	0.42	23.99	0.52	23.99	0.63	23.99	0.73	24
25	25.00	0.44	24.99	0.55	24.99	0.65	24.99	0.76	25
26	26.00	0.45	25.99	0.57	25.99	0.68	25.99	0.79	26
27	27.00	0.47	26.99	0.59	26.99	0.71	26.99	0.83	27
28	28.00	0.49	27.99	0.61	27.99	0.73	27.99	0.86	28
29	29.00	0.51	28.99	0.63	28.99	0.76	28.99	0.89	29
30	30.00	0.52	29.99	0.65	29.99	0.79	29.99	0.92	30
31	31.00	0.54	30.99	0.68	30.99	0.81	30.99	0.95	31
32	32.00	0.56	31.99	0.70	31.99	0.84	31.99	0.98	32
33	32.99	0.58	32.99	0.72	32.99	0.86	32.98	1.01	33
34	33.99	0.59	33.99	0.74	33.99	0.89	33.98	1.04	34
35	34.99	0.61	34.99	0.76	34.99	0.92	34.98	1.07	35
36	35.99	0.63	35.99	0.79	35.99	0.94	35.98	1.10	36
37	36.99	0.65	36.99	0.81	36.99	0.97	36.98	1.13	37
38	37.99	0.66	37.99	0.83	37.99	0.99	37.98	1.16	38
39	38.99	0.68	38.99	0.85	38.99	1.02	38.98	1.19	39
40	39.99	0.70	39.99	0.87	39.99	1.05	39.98	1.22	40
41	40.99	0.72	40.99	0.89	40.99	1.07	40.98	1.25	41
42	41.99	0.73	41.99	0.92	41.99	1.10	41.98	1.28	42
43	42.99	0.75	42.99	0.94	42.99	1.13	42.98	1.31	43
44	43.99	0.77	43.99	0.96	43.99	1.15	43.98	1.34	44
45	44.99	0.79	44.99	0.98	44.99	1.18	44.98	1.37	45
46	45.99	0.80	45.99	1.00	45.99	1.20	45.98	1.40	46
47	46.99	0.82	46.99	1.03	46.99	1.23	46.98	1.44	47
48	47.99	0.84	47.99	1.05	47.98	1.26	47.98	1.47	48
49	48.99	0.86	48.99	1.07	48.98	1.28	48.98	1.50	49
50	49.99	0.87	49.99	1.09	49.98	1.31	49.98	1.53	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	89 Deg.		88 $\frac{3}{4}$ Deg.		88 $\frac{1}{2}$ Deg.		88 $\frac{1}{4}$ Deg.		

Distance.	1 Deg.		1¼ Deg.		1½ Deg.		1¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.99	0.89	50.99	1.11	50.98	1.34	50.98	1.56	51
52	51.99	0.91	51.99	1.13	51.98	1.36	51.98	1.59	52
53	52.99	0.92	52.99	1.16	52.98	1.39	52.98	1.62	53
54	53.99	0.94	53.99	1.18	53.98	1.41	53.97	1.65	54
55	54.99	0.96	54.99	1.20	54.98	1.44	54.97	1.68	55
56	55.99	0.98	55.99	1.22	55.98	1.47	55.97	1.71	56
57	56.99	0.99	56.99	1.24	56.98	1.49	56.97	1.74	57
58	57.99	1.01	57.99	1.27	57.98	1.52	57.97	1.77	58
59	58.99	1.03	58.99	1.29	58.98	1.54	58.97	1.80	59
60	59.99	1.05	59.99	1.31	59.98	1.57	59.97	1.83	60
61	60.99	1.06	60.99	1.33	60.98	1.60	60.97	1.86	61
62	61.99	1.08	61.99	1.35	61.98	1.62	61.97	1.89	62
63	62.99	1.10	62.99	1.37	62.98	1.65	62.97	1.92	63
64	63.99	1.12	63.98	1.40	63.98	1.68	63.97	1.95	64
65	64.99	1.13	64.98	1.42	64.98	1.70	64.97	1.99	65
66	65.99	1.15	65.98	1.44	65.98	1.73	65.97	2.02	66
67	66.99	1.17	66.98	1.46	66.98	1.75	66.97	2.05	67
68	67.99	1.19	67.98	1.48	67.98	1.78	67.97	2.08	68
69	68.99	1.20	68.98	1.51	68.98	1.81	68.97	2.11	69
70	69.99	1.22	69.98	1.53	69.98	1.83	69.97	2.14	70
71	70.99	1.24	70.98	1.55	70.98	1.86	70.97	2.17	71
72	71.99	1.26	71.98	1.57	71.98	1.88	71.97	2.20	72
73	72.99	1.27	72.98	1.59	72.97	1.91	72.97	2.23	73
74	73.99	1.29	73.98	1.61	73.97	1.94	73.97	2.26	74
75	74.99	1.31	74.98	1.64	74.97	1.96	74.97	2.29	75
76	75.99	1.33	75.98	1.66	75.97	1.99	75.96	2.32	76
77	76.99	1.34	76.98	1.68	76.97	2.02	76.96	2.35	77
78	77.99	1.36	77.98	1.70	77.97	2.04	77.96	2.38	78
79	78.99	1.38	78.98	1.72	78.97	2.07	78.96	2.41	79
80	79.99	1.40	79.98	1.75	79.97	2.09	79.96	2.44	80
81	80.99	1.41	80.98	1.77	80.97	2.12	80.96	2.47	81
82	81.99	1.43	81.98	1.79	81.97	2.15	81.96	2.50	82
83	82.99	1.45	82.98	1.81	82.97	2.17	82.96	2.53	83
84	83.99	1.47	83.98	1.83	83.97	2.20	83.96	2.57	84
85	84.99	1.48	84.98	1.85	84.97	2.23	84.96	2.60	85
86	85.99	1.50	85.98	1.88	85.97	2.25	85.96	2.63	86
87	86.99	1.52	86.98	1.90	86.97	2.28	86.96	2.66	87
88	87.99	1.54	87.98	1.92	87.97	2.30	87.96	2.69	88
89	88.99	1.55	88.98	1.94	88.97	2.33	88.96	2.72	89
90	89.99	1.57	89.98	1.96	89.97	2.36	89.96	2.75	90
91	90.99	1.59	90.98	1.99	90.97	2.38	90.96	2.78	91
92	91.99	1.61	91.98	2.01	91.97	2.41	91.96	2.81	92
93	92.99	1.62	92.98	2.03	92.97	2.43	92.96	2.84	93
94	93.99	1.64	93.98	2.05	93.97	2.46	93.96	2.87	94
95	94.99	1.66	94.98	2.07	94.97	2.49	94.96	2.90	95
96	95.99	1.68	95.98	2.09	95.97	2.51	95.96	2.94	96
97	96.99	1.69	96.98	2.12	96.97	2.54	96.95	2.96	97
98	97.99	1.71	97.98	2.14	97.97	2.57	97.95	2.99	98
99	98.98	1.73	98.98	2.16	98.97	2.59	98.95	3.02	99
100	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	89 Deg.		88¾ Deg.		88½ Deg.		88¼ Deg.		

## TRAVERSE TABLE.

Distance.	2 Deg.		2 $\frac{1}{4}$ Deg.		2 $\frac{1}{2}$ Deg.		2 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.03	1.00	0.04	1.00	0.04	1.00	0.05	1
2	2.00	0.07	2.00	0.08	2.00	0.09	2.00	0.10	2
3	3.00	0.10	3.00	0.12	3.00	0.13	3.00	0.14	3
4	4.00	0.14	4.00	0.16	4.00	0.17	4.00	0.19	4
5	5.00	0.17	5.00	0.20	5.00	0.22	4.99	0.24	5
6	6.00	0.21	6.00	0.24	5.99	0.26	5.99	0.29	6
7	7.00	0.24	6.99	0.27	6.99	0.31	6.99	0.34	7
8	7.99	0.28	7.99	0.31	7.99	0.35	7.99	0.38	8
9	8.99	0.31	8.99	0.35	8.99	0.39	8.99	0.43	9
10	9.99	0.35	9.99	0.39	9.99	0.44	9.99	0.48	10
11	10.99	0.38	10.99	0.43	10.99	0.48	10.99	0.53	11
12	11.99	0.42	11.99	0.47	11.99	0.52	11.99	0.58	12
13	12.99	0.45	12.99	0.51	12.99	0.57	12.99	0.62	13
14	13.99	0.49	13.99	0.55	13.99	0.61	13.98	0.67	14
15	14.99	0.52	14.99	0.59	14.99	0.65	14.98	0.72	15
16	15.99	0.56	15.99	0.63	15.99	0.70	15.98	0.77	16
17	16.99	0.59	16.99	0.67	16.98	0.74	16.98	0.82	17
18	17.99	0.63	17.99	0.71	17.98	0.79	17.98	0.86	18
19	18.99	0.66	18.99	0.75	18.98	0.83	18.98	0.91	19
20	19.99	0.70	19.98	0.79	19.98	0.87	19.98	0.96	20
21	20.99	0.73	20.98	0.82	20.98	0.92	20.98	1.01	21
22	21.99	0.77	21.98	0.86	21.98	0.96	21.97	1.06	22
23	22.99	0.80	22.98	0.90	22.98	1.00	22.97	1.10	23
24	23.99	0.84	23.98	0.94	23.98	1.05	23.97	1.15	24
25	24.98	0.87	24.98	0.98	24.98	1.09	24.97	1.20	25
26	25.98	0.91	25.98	1.02	25.98	1.13	25.97	1.25	26
27	26.98	0.94	26.98	1.06	26.97	1.18	26.97	1.30	27
28	27.98	0.98	27.98	1.10	27.97	1.22	27.97	1.34	28
29	28.98	1.01	28.98	1.14	28.97	1.26	28.97	1.39	29
30	29.98	1.05	29.98	1.18	29.97	1.31	29.97	1.44	30
31	30.98	1.08	30.98	1.22	30.97	1.35	30.96	1.49	31
32	31.98	1.12	31.98	1.26	31.97	1.40	31.96	1.54	32
33	32.98	1.15	32.97	1.30	32.97	1.44	32.96	1.58	33
34	33.98	1.19	33.97	1.33	33.97	1.48	33.96	1.63	34
35	34.98	1.22	34.97	1.37	34.97	1.53	34.96	1.68	35
36	35.98	1.26	35.97	1.41	35.97	1.57	35.96	1.73	36
37	36.98	1.29	36.97	1.45	36.96	1.61	36.96	1.78	37
38	37.98	1.33	37.97	1.49	37.96	1.66	37.96	1.82	38
39	38.98	1.36	38.97	1.53	38.96	1.70	38.96	1.87	39
40	39.98	1.40	39.97	1.57	39.96	1.75	39.95	1.92	40
41	40.98	1.43	40.97	1.61	40.96	1.77	40.95	1.97	41
42	41.97	1.47	41.97	1.65	41.96	1.83	41.95	2.02	42
43	42.97	1.50	42.97	1.69	42.96	1.88	42.95	2.06	43
44	43.97	1.54	43.97	1.73	43.96	1.92	43.95	2.11	44
45	44.97	1.57	44.97	1.77	44.96	1.96	44.95	2.16	45
46	45.97	1.61	45.96	1.81	45.96	2.01	45.95	2.21	46
47	46.97	1.64	46.96	1.85	46.96	2.05	46.95	2.25	47
48	47.97	1.68	47.96	1.88	47.95	2.09	47.95	2.30	48
49	48.97	1.71	48.96	1.92	48.95	2.14	48.94	2.35	49
50	49.97	1.74	49.96	1.96	49.95	2.18	49.94	2.40	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	88 Deg.		87 $\frac{3}{4}$ Deg.		87 $\frac{1}{2}$ Deg.		87 $\frac{1}{4}$ Deg.		



Distance.	2 Deg.		2¼ Deg.		2½ Deg.		2¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.97	1.78	50.96	2.00	50.95	2.22	50.94	2.45	51
52	51.97	1.81	51.96	2.04	51.95	2.27	51.94	2.50	52
53	52.97	1.85	52.96	2.08	52.95	2.31	52.94	2.54	53
54	53.97	1.88	53.96	2.12	53.95	2.36	53.94	2.59	54
55	54.97	1.92	54.96	2.16	54.95	2.40	54.94	2.64	55
56	55.97	1.95	55.96	2.20	55.95	2.44	55.94	2.69	56
57	56.97	1.99	56.96	2.24	56.95	2.49	56.93	2.73	57
58	57.96	2.02	57.96	2.28	57.94	2.53	57.93	2.78	58
59	58.96	2.06	58.95	2.32	58.94	2.57	58.93	2.83	59
60	59.96	2.09	59.95	2.36	59.94	2.62	59.93	2.88	60
61	60.96	2.13	60.95	2.39	60.94	2.66	60.93	2.93	61
62	61.96	2.16	61.95	2.43	61.94	2.70	61.93	2.97	62
63	62.96	2.20	62.95	2.47	62.94	2.75	62.93	3.02	63
64	63.96	2.23	63.95	2.51	63.94	2.79	63.93	3.07	64
65	64.96	2.27	64.95	2.55	64.94	2.84	64.93	3.12	65
66	65.96	2.30	65.95	2.59	65.94	2.88	65.92	3.17	66
67	66.96	2.34	66.95	2.63	66.94	2.92	66.92	3.21	67
68	67.96	2.37	67.95	2.67	67.94	2.97	67.92	3.26	68
69	68.96	2.41	68.95	2.71	68.93	3.01	68.92	3.31	69
70	69.96	2.44	69.95	2.75	69.93	3.05	69.92	3.36	70
71	70.96	2.48	70.95	2.79	70.93	3.10	70.92	3.41	71
72	71.96	2.51	71.94	2.83	71.93	3.14	71.92	3.45	72
73	72.96	2.55	72.94	2.87	72.93	3.18	72.92	3.50	73
74	73.95	2.58	73.94	2.91	73.93	3.23	73.91	3.55	74
75	74.95	2.62	74.94	2.94	74.93	3.27	74.91	3.60	75
76	75.95	2.65	75.94	2.98	75.93	3.31	75.91	3.65	76
77	76.95	2.69	76.94	3.02	76.93	3.36	76.91	3.70	77
78	77.95	2.72	77.94	3.06	77.93	3.40	77.91	3.74	78
79	78.95	2.76	78.94	3.10	78.92	3.45	78.91	3.79	79
80	79.95	2.79	79.94	3.14	79.92	3.49	79.91	3.84	80
81	80.95	2.83	80.94	3.18	80.92	3.53	80.91	3.89	81
82	81.95	2.86	81.94	3.22	81.92	3.58	81.91	3.93	82
83	82.95	2.90	82.94	3.26	82.92	3.62	82.90	3.98	83
84	83.95	2.93	83.94	3.30	83.92	3.66	83.90	4.03	84
85	84.95	2.97	84.93	3.34	84.92	3.71	84.90	4.08	85
86	85.95	3.00	85.93	3.38	85.92	3.75	85.90	4.13	86
87	86.95	3.04	86.93	3.42	86.92	3.79	86.90	4.17	87
88	87.95	3.07	87.93	3.45	87.92	3.84	87.90	4.22	88
89	88.95	3.11	88.93	3.49	88.92	3.88	88.90	4.27	89
90	89.95	3.14	89.93	3.53	89.91	3.93	89.90	4.32	90
91	90.95	3.18	90.93	3.57	90.91	3.97	90.90	4.37	91
92	91.94	3.21	91.93	3.61	91.91	4.01	91.89	4.41	92
93	92.94	3.25	92.93	3.65	92.91	4.06	92.89	4.46	93
94	93.94	3.28	93.93	3.69	93.91	4.10	93.89	4.51	94
95	94.94	3.32	94.93	3.73	94.91	4.14	94.89	4.56	95
96	95.94	3.35	95.93	3.77	95.91	4.19	95.89	4.61	96
97	96.94	3.39	96.93	3.81	96.91	4.23	96.89	4.65	97
98	97.94	3.42	97.92	3.85	97.91	4.27	97.89	4.70	98
99	98.94	3.46	98.92	3.89	98.91	4.32	98.89	4.75	99
100	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	88 Deg.		87¼ Deg.		87½ Deg.		87¾ Deg.		

Distance.	3 Deg.		3 $\frac{1}{4}$ Deg.		3 $\frac{1}{2}$ Deg.		3 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.05	1.00	0.06	1.00	0.06	1.00	0.06	1
2	2.00	0.10	2.00	0.11	2.00	0.12	2.00	0.13	2
3	3.00	0.16	3.00	0.17	2.99	0.18	2.99	0.20	3
4	3.99	0.21	3.99	0.23	3.99	0.24	3.99	0.26	4
5	4.99	0.26	4.99	0.28	4.99	0.31	4.99	0.33	5
6	5.99	0.31	5.99	0.34	5.99	0.37	5.99	0.39	6
7	6.99	0.37	6.99	0.40	6.99	0.43	6.99	0.46	7
8	7.99	0.42	7.99	0.45	7.99	0.49	7.98	0.52	8
9	8.99	0.47	8.99	0.51	8.98	0.55	8.98	0.59	9
10	9.99	0.52	9.98	0.57	9.98	0.61	9.98	0.65	10
11	10.98	0.58	10.98	0.62	10.98	0.67	10.98	0.72	11
12	11.98	0.63	11.98	0.68	11.98	0.73	11.97	0.78	12
13	12.98	0.68	12.98	0.73	12.98	0.79	12.97	0.85	13
14	13.98	0.73	13.98	0.79	13.97	0.85	13.97	0.92	14
15	14.98	0.79	14.98	0.85	14.97	0.92	14.97	0.98	15
16	15.98	0.84	15.97	0.91	15.97	0.98	15.97	1.05	16
17	16.98	0.89	16.97	0.96	16.97	1.04	16.96	1.11	17
18	17.98	0.94	17.97	1.02	17.97	1.10	17.96	1.18	18
19	18.98	0.99	18.97	1.08	18.96	1.16	18.96	1.24	19
20	19.97	1.05	19.97	1.13	19.96	1.22	19.96	1.31	20
21	20.97	1.10	20.97	1.19	20.96	1.28	20.96	1.37	21
22	21.97	1.15	21.96	1.25	21.96	1.34	21.95	1.44	22
23	22.97	1.20	22.96	1.30	22.96	1.40	22.95	1.50	23
24	23.97	1.26	23.96	1.36	23.96	1.47	23.95	1.57	24
25	24.97	1.31	24.96	1.42	24.95	1.53	24.95	1.64	25
26	25.96	1.36	25.96	1.47	25.95	1.59	25.94	1.70	26
27	26.96	1.41	26.96	1.53	26.95	1.65	26.94	1.77	27
28	27.96	1.47	27.95	1.59	27.95	1.71	27.94	1.83	28
29	28.96	1.52	28.95	1.64	28.95	1.77	28.94	1.90	29
30	29.96	1.57	29.95	1.70	29.94	1.83	29.94	1.96	30
31	30.96	1.62	30.95	1.76	30.94	1.89	30.93	2.03	31
32	31.96	1.67	31.95	1.81	31.94	1.95	31.93	2.09	32
33	32.95	1.73	32.95	1.87	32.94	2.01	32.93	2.16	33
34	33.95	1.78	33.95	1.93	33.94	2.08	33.93	2.22	34
35	34.95	1.83	34.94	1.98	34.93	2.14	34.92	2.29	35
36	35.95	1.88	35.94	2.04	35.93	2.20	35.92	2.35	36
37	36.95	1.94	36.94	2.10	36.93	2.26	36.92	2.42	37
38	37.95	1.99	37.94	2.15	37.93	2.32	37.92	2.49	38
39	38.95	2.04	38.94	2.21	38.93	2.38	38.92	2.55	39
40	39.95	2.09	39.94	2.27	39.93	2.44	39.91	2.62	40
41	40.94	2.15	40.93	2.32	40.92	2.50	40.91	2.68	41
42	41.94	2.20	41.93	2.38	41.92	2.56	41.91	2.75	42
43	42.94	2.25	42.93	2.44	42.92	2.63	42.91	2.81	43
44	43.94	2.30	43.93	2.49	43.92	2.69	43.91	2.88	44
45	44.94	2.36	44.93	2.55	44.92	2.75	44.90	2.94	45
46	45.94	2.41	45.93	2.61	45.91	2.81	45.90	3.01	46
47	46.94	2.46	46.92	2.66	46.91	2.87	46.90	3.07	47
48	47.93	2.51	47.92	2.72	47.91	2.93	47.90	3.14	48
49	48.93	2.56	48.92	2.78	48.91	2.99	48.90	3.20	49
50	49.93	2.62	49.92	2.83	49.91	3.05	49.89	3.27	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	87 Deg.		86 $\frac{3}{4}$ Deg.		86 $\frac{1}{2}$ Deg.		86 $\frac{1}{4}$ Deg.		

Distance.	3 Deg.		3¼ Deg.		3½ Deg.		3¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.93	2.67	50.92	2.89	50.90	3.11	50.89	3.34	51
52	51.93	2.72	51.92	2.95	51.90	3.17	51.89	3.40	52
53	52.93	2.77	52.91	3.00	52.90	3.24	52.89	3.47	53
54	53.93	2.83	53.91	3.06	53.90	3.30	53.88	3.53	54
55	54.92	2.88	54.91	3.12	54.90	3.36	54.88	3.60	55
56	55.92	2.93	55.91	3.17	55.90	3.42	55.88	3.66	56
57	56.92	2.98	56.91	3.23	56.89	3.48	56.88	3.73	57
58	57.92	3.04	57.91	3.29	57.89	3.54	57.88	3.79	58
59	58.92	3.09	58.91	3.34	58.89	3.60	58.87	3.86	59
60	59.92	3.14	59.90	3.40	59.89	3.66	59.87	3.92	60
61	60.92	3.19	60.90	3.46	60.89	3.72	60.87	3.99	61
62	61.92	3.24	61.90	3.51	61.88	3.79	61.87	4.05	62
63	62.91	3.30	62.90	3.57	62.88	3.85	62.87	4.12	63
64	63.91	3.35	63.90	3.63	63.88	3.91	63.86	4.19	64
65	64.91	3.40	64.90	3.69	64.88	3.97	64.86	4.25	65
66	65.91	3.45	65.89	3.74	65.88	4.03	65.86	4.32	66
67	66.91	3.51	66.89	3.80	66.88	4.09	66.86	4.38	67
68	67.91	3.56	67.89	3.86	67.87	4.15	67.85	4.45	68
69	68.91	3.61	68.89	3.91	68.87	4.21	68.85	4.51	69
70	69.90	3.66	69.89	3.97	69.87	4.27	69.85	4.58	70
71	70.90	3.72	70.89	4.03	70.87	4.33	70.85	4.64	71
72	71.90	3.77	71.88	4.08	71.87	4.40	71.85	4.71	72
73	72.90	3.82	72.88	4.14	72.86	4.46	72.84	4.77	73
74	73.90	3.87	73.88	4.20	73.86	4.52	73.84	4.84	74
75	74.90	3.93	74.88	4.25	74.86	4.58	74.84	4.91	75
76	75.90	3.98	75.88	4.31	75.86	4.64	75.84	4.97	76
77	76.89	4.03	76.88	4.37	76.86	4.70	76.84	5.04	77
78	77.89	4.08	77.87	4.42	77.85	4.76	77.83	5.10	78
79	78.89	4.13	78.87	4.48	78.85	4.82	78.83	5.17	79
80	79.89	4.19	79.87	4.54	79.85	4.88	79.83	5.23	80
81	80.89	4.24	80.87	4.59	80.85	4.94	80.83	5.30	81
82	81.89	4.29	81.87	4.65	81.85	5.01	81.82	5.36	82
83	82.89	4.34	82.87	4.71	82.85	5.07	82.82	5.43	83
84	83.88	4.40	83.86	4.76	83.84	5.13	83.82	5.49	84
85	84.88	4.45	84.86	4.82	84.84	5.19	84.82	5.56	85
86	85.88	4.50	85.86	4.88	85.84	5.25	85.82	5.62	86
87	86.88	4.55	86.86	4.93	86.84	5.31	86.81	5.69	87
88	87.88	4.61	87.86	4.99	87.84	5.37	87.81	5.76	88
89	88.88	4.66	88.86	5.05	88.83	5.43	88.81	5.82	89
90	89.88	4.71	89.86	5.10	89.83	5.49	89.81	5.89	90
91	90.88	4.76	90.85	5.16	90.83	5.56	90.81	5.95	91
92	91.87	4.81	91.85	5.22	91.83	5.62	91.80	6.02	92
93	92.87	4.87	92.85	5.27	92.83	5.68	92.80	6.08	93
94	93.87	4.92	93.85	5.33	93.82	5.74	93.80	6.15	94
95	94.87	4.97	94.85	5.39	94.82	5.80	94.80	6.21	95
96	95.87	5.02	95.85	5.44	95.82	5.86	95.79	6.28	96
97	96.87	5.08	96.84	5.50	96.82	5.92	96.79	6.34	97
98	97.87	5.13	97.84	5.56	97.82	5.98	97.79	6.41	98
99	98.86	5.18	98.84	5.61	98.82	6.04	98.79	6.47	99
100	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	87 Deg.		86¼ Deg.		86½ Deg.		86¼ Deg.		

Distance.	4 Deg.		4 $\frac{1}{4}$ Deg.		4 $\frac{1}{2}$ Deg.		4 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.07	1.00	0.07	1.00	0.08	1.00	0.08	1
2	2.00	0.14	1.99	0.15	1.99	0.16	1.99	0.17	2
3	2.99	0.21	2.99	0.22	2.99	0.24	2.99	0.25	3
4	3.99	0.28	3.99	0.30	3.99	0.31	3.98	0.33	4
5	4.99	0.35	4.99	0.37	4.98	0.39	4.98	0.41	5
6	5.99	0.42	5.98	0.44	5.98	0.47	5.98	0.50	6
7	6.98	0.49	6.98	0.52	6.98	0.55	6.97	0.58	7
8	7.98	0.56	7.98	0.59	7.98	0.63	7.97	0.66	8
9	8.98	0.63	8.98	0.67	8.97	0.71	8.97	0.75	9
10	9.98	0.70	9.97	0.74	9.97	0.78	9.97	0.83	10
11	10.97	0.77	10.97	0.82	10.97	0.86	10.96	0.91	11
12	11.97	0.84	11.97	0.89	11.96	0.94	11.96	0.99	12
13	12.97	0.91	12.96	0.96	12.96	1.02	12.96	1.08	13
14	13.97	0.98	13.96	1.04	13.96	1.10	13.95	1.16	14
15	14.96	1.05	14.96	1.11	14.95	1.18	14.95	1.24	15
16	15.96	1.12	15.96	1.19	15.95	1.26	15.95	1.32	16
17	16.96	1.19	16.95	1.26	16.95	1.33	16.94	1.41	17
18	17.96	1.26	17.95	1.33	17.94	1.41	17.94	1.49	18
19	18.95	1.33	18.95	1.40	18.94	1.49	18.93	1.57	19
20	19.95	1.40	19.95	1.48	19.94	1.57	19.93	1.66	20
21	20.95	1.46	20.94	1.56	20.94	1.65	20.93	1.74	21
22	21.95	1.53	21.94	1.63	21.93	1.73	21.92	1.82	22
23	22.94	1.60	22.94	1.70	22.93	1.80	22.92	1.90	23
24	23.94	1.67	23.93	1.78	23.93	1.88	23.92	1.99	24
25	24.94	1.74	24.93	1.85	24.92	1.96	24.91	2.07	25
26	25.94	1.81	25.93	1.93	25.92	2.04	25.91	2.15	26
27	26.93	1.88	26.93	2.00	26.92	2.12	26.91	2.24	27
28	27.93	1.95	27.92	2.08	27.91	2.20	27.90	2.32	28
29	28.93	2.02	28.92	2.15	28.91	2.28	28.90	2.40	29
30	29.93	2.09	29.92	2.22	29.91	2.35	29.90	2.48	30
31	30.92	2.16	30.91	2.30	30.90	2.43	30.89	2.57	31
32	31.92	2.23	31.91	2.37	31.90	2.51	31.89	2.65	32
33	32.92	2.30	32.91	2.45	32.90	2.59	32.89	2.73	33
34	33.92	2.37	33.91	2.52	33.90	2.67	33.88	2.82	34
35	34.91	2.44	34.90	2.59	34.89	2.75	34.88	2.90	35
36	35.91	2.51	35.90	2.67	35.89	2.82	35.88	2.98	36
37	36.91	2.58	36.90	2.74	36.89	2.90	36.87	3.06	37
38	37.91	2.65	37.90	2.82	37.88	2.98	37.87	3.15	38
39	38.90	2.72	38.89	2.89	38.88	3.06	38.87	3.23	39
40	39.90	2.79	39.89	2.96	39.88	3.14	39.86	3.31	40
41	40.90	2.86	40.89	3.04	40.87	3.22	40.86	3.40	41
42	41.90	2.93	41.88	3.11	41.87	3.30	41.86	3.48	42
43	42.90	3.00	42.88	3.19	42.87	3.37	42.85	3.56	43
44	43.89	3.07	43.88	3.26	43.86	3.45	43.85	3.64	44
45	44.89	3.14	44.88	3.33	44.86	3.53	44.85	3.73	45
46	45.89	3.21	45.87	3.41	45.86	3.61	45.84	3.81	46
47	46.89	3.28	46.87	3.48	46.86	3.69	46.84	3.89	47
48	47.88	3.35	47.87	3.56	47.85	3.77	47.84	3.97	48
49	48.88	3.42	48.87	3.63	48.85	3.84	48.83	4.06	49
50	49.88	3.49	49.86	3.71	49.85	3.92	49.83	4.14	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	86 Deg.		85 $\frac{3}{4}$ Deg.		85 $\frac{1}{2}$ Deg.		85 $\frac{1}{4}$ Deg.		

Distance.	4 Deg.		4 $\frac{1}{4}$ Deg.		4 $\frac{1}{2}$ Deg.		4 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.88	3.56	50.86	3.78	50.84	4.00	50.82	4.22	51
52	51.87	3.63	51.86	3.85	51.84	4.08	51.82	4.31	52
53	52.87	3.70	52.85	3.93	52.84	4.16	52.82	4.39	53
54	53.87	3.77	53.85	4.00	53.83	4.24	53.81	4.47	54
55	54.87	3.84	54.85	4.08	54.83	4.32	54.81	4.55	55
56	55.86	3.91	55.85	4.15	55.83	4.39	55.81	4.64	56
57	56.86	3.98	56.84	4.22	56.82	4.47	56.80	4.72	57
58	57.86	4.05	57.84	4.30	57.82	4.55	57.80	4.80	58
59	58.86	4.12	58.84	4.37	58.82	4.63	58.80	4.89	59
60	59.85	4.19	59.84	4.45	59.82	4.71	59.79	4.97	60
61	60.85	4.26	60.83	4.52	60.81	4.79	60.79	5.05	61
62	61.85	4.32	61.83	4.59	61.81	4.86	61.79	5.13	62
63	62.85	4.39	62.83	4.67	62.81	4.94	62.78	5.22	63
64	63.84	4.46	63.82	4.74	63.80	5.02	63.78	5.30	64
65	64.84	4.53	64.82	4.82	64.80	5.10	64.78	5.38	65
66	65.84	4.60	65.82	4.89	65.80	5.18	65.77	5.47	66
67	66.84	4.67	66.82	4.97	66.79	5.26	66.77	5.55	67
68	67.83	4.74	67.81	5.04	67.79	5.34	67.77	5.63	68
69	68.83	4.81	68.81	5.11	68.79	5.41	68.76	5.71	69
70	69.83	4.88	69.81	5.19	69.78	5.49	69.76	5.80	70
71	70.83	4.95	70.80	5.26	70.78	5.57	70.76	5.88	71
72	71.82	5.02	71.80	5.34	71.78	5.65	71.75	5.96	72
73	72.82	5.09	72.80	5.41	72.77	5.73	72.75	6.04	73
74	73.82	5.16	73.80	5.48	73.77	5.81	73.75	6.13	74
75	74.82	5.23	74.79	5.56	74.77	5.88	74.74	6.21	75
76	75.81	5.30	75.79	5.63	75.77	5.96	75.74	6.29	76
77	76.81	5.37	76.79	5.71	76.76	6.04	76.74	6.38	77
78	77.81	5.44	77.79	5.78	77.76	6.12	77.73	6.46	78
79	78.81	5.51	78.78	5.85	78.76	6.20	78.73	6.54	79
80	79.81	5.58	79.78	5.93	79.75	6.28	79.73	6.62	80
81	80.80	5.65	80.78	6.00	80.75	6.36	80.72	6.71	81
82	81.80	5.72	81.78	6.08	81.75	6.43	81.72	6.79	82
83	82.80	5.79	82.77	6.15	82.74	6.51	82.71	6.87	83
84	83.80	5.86	83.77	6.23	83.74	6.59	83.71	6.96	84
85	84.79	5.93	84.77	6.30	84.74	6.67	84.71	7.04	85
86	85.79	6.00	85.76	6.37	85.73	6.75	85.70	7.12	86
87	86.79	6.07	86.76	6.45	86.73	6.83	86.70	7.20	87
88	87.79	6.14	87.76	6.52	87.73	6.90	87.70	7.29	88
89	88.78	6.21	88.76	6.60	88.73	6.98	88.70	7.37	89
90	89.78	6.28	89.75	6.67	89.72	7.06	89.69	7.45	90
91	90.78	6.35	90.75	6.74	90.72	7.14	90.69	7.54	91
92	91.78	6.42	91.75	6.82	91.72	7.22	91.68	7.62	92
93	92.77	6.49	92.74	6.89	92.71	7.30	92.68	7.70	93
94	93.77	6.56	93.74	6.97	93.71	7.38	93.68	7.78	94
95	94.77	6.63	94.74	7.04	94.71	7.45	94.67	7.87	95
96	95.77	6.70	95.74	7.11	95.70	7.53	95.67	7.95	96
97	96.76	6.77	96.73	7.19	96.70	7.61	96.67	8.03	97
98	97.76	6.84	97.73	7.26	97.70	7.69	97.66	8.12	98
99	98.76	6.91	98.73	7.34	98.69	7.77	98.66	8.20	99
100	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	86 Deg.		85 $\frac{1}{4}$ Deg.		85 $\frac{1}{2}$ Deg.		85 $\frac{3}{4}$ Deg.		

TRAVERSE TABLE.

Distance.	5 Deg.		5¼ Deg.		5½ Deg.		5¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.09	1.00	0.09	1.00	0.10	0.99	0.10	1
2	1.99	0.17	1.99	0.18	1.99	0.19	1.99	0.20	2
3	2.99	0.26	2.99	0.27	2.99	0.29	2.98	0.30	3
4	3.98	0.35	3.98	0.37	3.98	0.38	3.98	0.40	4
5	4.98	0.44	4.98	0.46	4.98	0.48	4.97	0.50	5
6	5.98	0.52	5.97	0.55	5.97	0.58	5.97	0.60	6
7	6.97	0.61	6.97	0.64	6.97	0.67	6.96	0.70	7
8	7.97	0.70	7.97	0.73	7.96	0.76	7.96	0.80	8
9	8.97	0.78	8.96	0.82	8.96	0.86	8.95	0.90	9
10	9.96	0.87	9.96	0.92	9.95	0.96	9.95	1.00	10
11	10.96	0.96	10.95	1.01	10.95	1.05	10.94	1.10	11
12	11.95	1.05	11.95	1.10	11.94	1.15	11.94	1.20	12
13	12.95	1.13	12.95	1.19	12.94	1.25	12.93	1.30	13
14	13.95	1.22	13.94	1.28	13.94	1.34	13.93	1.40	14
15	14.94	1.31	14.94	1.37	14.93	1.44	14.92	1.50	15
16	15.94	1.39	15.93	1.46	15.93	1.53	15.92	1.60	16
17	16.94	1.48	16.93	1.56	16.92	1.63	16.91	1.70	17
18	17.93	1.57	17.92	1.65	17.92	1.73	17.91	1.80	18
19	18.93	1.66	18.92	1.74	18.91	1.82	18.90	1.90	19
20	19.92	1.74	19.92	1.83	19.91	1.92	19.90	2.00	20
21	20.92	1.83	20.91	1.92	20.90	2.01	20.89	2.10	21
22	21.92	1.92	21.91	2.01	21.90	2.11	21.89	2.20	22
23	22.91	2.00	22.90	2.10	22.89	2.20	22.88	2.30	23
24	23.91	2.09	23.90	2.20	23.89	2.30	23.88	2.40	24
25	24.90	2.18	24.90	2.29	24.88	2.40	24.87	2.50	25
26	25.90	2.27	25.89	2.38	25.88	2.49	25.87	2.60	26
27	26.90	2.35	26.89	2.47	26.88	2.59	26.86	2.71	27
28	27.89	2.44	27.88	2.56	27.87	2.68	27.86	2.81	28
29	28.89	2.53	28.88	2.65	28.87	2.78	28.85	2.91	29
30	29.89	2.61	29.87	2.75	29.86	2.88	29.85	3.01	30
31	30.88	2.70	30.87	2.84	30.86	2.97	30.84	3.11	31
32	31.88	2.79	31.87	2.93	31.85	3.07	31.84	3.21	32
33	32.87	2.88	32.86	3.02	32.85	3.16	32.83	3.31	33
34	33.87	2.96	33.86	3.11	33.84	3.26	33.83	3.41	34
35	34.87	3.05	34.85	3.20	34.84	3.35	34.82	3.51	35
36	35.86	3.14	35.85	3.29	35.83	3.45	35.82	3.61	36
37	36.86	3.22	36.84	3.39	36.83	3.55	36.81	3.71	37
38	37.86	3.31	37.84	3.48	37.83	3.64	37.81	3.81	38
39	38.85	3.40	38.84	3.57	38.82	3.74	38.80	3.91	39
40	39.85	3.49	39.83	3.66	39.82	3.83	39.80	4.01	40
41	40.84	3.57	40.83	3.75	40.81	3.93	40.79	4.11	41
42	41.84	3.66	41.82	3.84	41.81	4.03	41.79	4.21	42
43	42.84	3.75	42.82	3.93	42.80	4.12	42.78	4.31	43
44	43.83	3.83	43.82	4.03	43.80	4.22	43.78	4.41	44
45	44.83	3.92	44.81	4.12	44.79	4.31	44.77	4.51	45
46	45.82	4.01	45.81	4.21	45.79	4.41	45.77	4.61	46
47	46.82	4.10	46.80	4.30	46.78	4.50	46.76	4.71	47
48	47.82	4.18	47.80	4.39	47.78	4.60	47.76	4.81	48
49	48.81	4.27	48.79	4.48	48.77	4.70	48.75	4.91	49
50	49.81	4.36	49.79	4.58	49.77	4.79	49.75	5.01	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	85 Deg.		84¾ Deg.		84½ Deg.		84¼ Deg.		

Distance.	5 Deg.		5½ Deg.		5½ Deg.		5¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.81	4.44	50.79	4.67	50.77	4.89	50.74	5.11	51
52	51.80	4.53	51.78	4.76	51.76	4.98	51.74	5.21	52
53	52.80	4.62	52.78	4.85	52.76	5.08	52.73	5.31	53
54	53.79	4.71	53.77	4.94	53.75	5.18	53.73	5.41	54
55	54.79	4.79	54.77	5.03	54.75	5.27	54.72	5.51	55
56	55.79	4.88	55.77	5.12	55.74	5.37	55.72	5.61	56
57	56.78	4.97	56.76	5.22	56.74	5.46	56.71	5.71	57
58	57.78	5.06	57.76	5.31	57.73	5.56	57.71	5.81	58
59	58.78	5.14	58.75	5.40	58.73	5.65	58.70	5.91	59
60	59.77	5.23	59.75	5.49	59.72	5.75	59.70	6.01	60
61	60.77	5.32	60.74	5.58	60.72	5.85	60.69	6.11	61
62	61.76	5.40	61.74	5.67	61.71	5.94	61.69	6.21	62
63	62.76	5.49	62.74	5.76	62.71	6.04	62.68	6.31	63
64	63.76	5.58	63.73	5.86	63.71	6.13	63.68	6.41	64
65	64.75	5.67	64.73	5.95	64.70	6.23	64.67	6.51	65
66	65.75	5.75	65.72	6.04	65.70	6.33	65.67	6.61	66
67	66.75	5.84	66.72	6.13	66.69	6.42	66.66	6.71	67
68	67.74	5.93	67.71	6.22	67.69	6.52	67.66	6.81	68
69	68.74	6.01	68.71	6.31	68.68	6.61	68.65	6.91	69
70	69.73	6.10	69.71	6.41	69.68	6.71	69.65	7.01	70
71	70.73	6.19	70.70	6.50	70.67	6.81	70.64	7.11	71
72	71.73	6.28	71.70	6.59	71.67	6.90	71.64	7.21	72
73	72.72	6.36	72.69	6.68	72.66	7.00	72.63	7.31	73
74	73.72	6.45	73.69	6.77	73.66	7.09	73.63	7.41	74
75	74.71	6.54	74.69	6.86	74.65	7.19	74.62	7.51	75
76	75.71	6.62	75.68	6.95	75.65	7.28	75.62	7.61	76
77	76.71	6.71	76.68	7.05	76.65	7.38	76.61	7.71	77
78	77.70	6.80	77.67	7.14	77.64	7.48	77.61	7.81	78
79	78.70	6.89	78.67	7.23	78.64	7.57	78.60	7.91	79
80	79.70	6.97	79.66	7.32	79.63	7.67	79.60	8.02	80
81	80.69	7.06	80.66	7.41	80.63	7.76	80.59	8.12	81
82	81.69	7.15	81.66	7.50	81.62	7.86	81.59	8.22	82
83	82.68	7.23	82.65	7.59	82.62	7.96	82.58	8.32	83
84	83.68	7.32	83.65	7.69	83.61	8.05	83.58	8.42	84
85	84.68	7.41	84.64	7.78	84.61	8.15	84.57	8.52	85
86	85.67	7.50	85.64	7.87	85.60	8.24	85.57	8.62	86
87	86.67	7.58	86.64	7.96	86.60	8.34	86.56	8.72	87
88	87.67	7.67	87.63	8.05	87.59	8.43	87.56	8.82	88
89	88.66	7.76	88.63	8.14	88.59	8.53	88.55	8.92	89
90	89.66	7.84	89.62	8.24	89.59	8.63	89.55	9.02	90
91	90.65	7.93	90.62	8.33	90.58	8.72	90.54	9.12	91
92	91.65	8.02	91.61	8.42	91.58	8.82	91.54	9.22	92
93	92.65	8.11	92.61	8.51	92.57	8.91	92.53	9.32	93
94	93.64	8.19	93.61	8.60	93.57	9.01	93.53	9.42	94
95	94.64	8.28	94.60	8.69	94.56	9.11	94.52	9.52	95
96	95.63	8.37	95.60	8.78	95.56	9.20	95.52	9.62	96
97	96.63	8.45	96.59	8.88	96.55	9.30	96.51	9.72	97
98	97.63	8.54	97.59	8.97	97.55	9.39	97.51	9.82	98
99	98.62	8.63	98.59	9.06	98.54	9.49	98.50	9.92	99
100	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	85 Deg.		84½ Deg.		84½ Deg.		84¼ Deg.		

Distance.	6 Deg.		6½ Deg.		6½ Deg.		6¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.99	0.10	0.99	0.11	0.99	0.11	0.99	0.12	1
2	1.99	0.21	1.99	0.22	1.99	0.23	1.99	0.24	2
3	2.98	0.31	2.98	0.33	2.98	0.34	2.98	0.35	3
4	3.98	0.41	3.98	0.44	3.97	0.45	3.97	0.47	4
5	4.97	0.52	4.97	0.54	4.97	0.57	4.97	0.59	5
6	5.97	0.63	5.96	0.65	5.96	0.68	5.96	0.71	6
7	6.96	0.73	6.96	0.76	6.96	0.79	6.95	0.82	7
8	7.96	0.84	7.95	0.87	7.95	0.91	7.94	0.94	8
9	8.95	0.94	8.95	0.98	8.94	1.02	8.94	1.06	9
10	9.95	1.05	9.94	1.09	9.94	1.13	9.93	1.18	10
11	10.94	1.15	10.93	1.20	10.93	1.25	10.92	1.29	11
12	11.93	1.25	11.93	1.31	11.92	1.36	11.92	1.41	12
13	12.93	1.36	12.92	1.42	12.92	1.47	12.91	1.53	13
14	13.92	1.46	13.92	1.52	13.91	1.59	13.90	1.65	14
15	14.92	1.57	14.91	1.63	14.90	1.70	14.90	1.76	15
16	15.91	1.67	15.90	1.74	15.90	1.81	15.89	1.88	16
17	16.91	1.78	16.90	1.85	16.89	1.92	16.88	2.00	17
18	17.90	1.88	17.89	1.96	17.88	2.04	17.88	2.12	18
19	18.90	1.99	18.89	2.07	18.88	2.15	18.87	2.23	19
20	19.89	2.09	19.88	2.18	19.87	2.26	19.86	2.35	20
21	20.88	2.20	20.88	2.29	20.87	2.38	20.85	2.47	21
22	21.88	2.30	21.87	2.40	21.86	2.49	21.85	2.59	22
23	22.87	2.40	22.86	2.50	22.85	2.60	22.84	2.70	23
24	23.87	2.51	23.86	2.61	23.85	2.72	23.83	2.82	24
25	24.86	2.61	24.85	2.72	24.84	2.83	24.83	2.94	25
26	25.86	2.72	25.85	2.83	25.83	2.94	25.82	3.06	26
27	26.85	2.82	26.84	2.94	26.83	3.06	26.81	3.17	27
28	27.85	2.93	27.83	3.05	27.82	3.17	27.81	3.29	28
29	28.84	3.03	28.83	3.16	28.81	3.28	28.80	3.41	29
30	29.84	3.14	29.82	3.27	29.81	3.40	29.79	3.53	30
31	30.83	3.24	30.82	3.37	30.80	3.51	30.79	3.64	31
32	31.82	3.34	31.81	3.48	31.79	3.62	31.78	3.76	32
33	32.82	3.45	32.80	3.59	32.79	3.74	32.77	3.88	33
34	33.81	3.55	33.80	3.70	33.78	3.85	33.76	4.00	34
35	34.81	3.66	34.79	3.81	34.78	3.96	34.76	4.11	35
36	35.80	3.76	35.79	3.92	35.77	4.08	35.75	4.23	36
37	36.80	3.87	36.78	4.03	36.76	4.19	36.75	4.35	37
38	37.79	3.97	37.77	4.14	37.76	4.30	37.74	4.47	38
39	38.79	4.08	38.77	4.25	38.75	4.41	38.73	4.58	39
40	39.78	4.18	39.76	4.35	39.74	4.53	39.72	4.70	40
41	40.78	4.29	40.76	4.46	40.74	4.64	40.72	4.82	41
42	41.77	4.39	41.75	4.57	41.73	4.76	41.71	4.94	42
43	42.76	4.49	42.74	4.68	42.72	4.87	42.70	5.05	43
44	43.76	4.60	43.74	4.79	43.72	4.98	43.70	5.17	44
45	44.75	4.70	44.73	4.90	44.71	5.09	44.69	5.29	45
46	45.75	4.81	45.73	5.01	45.70	5.21	45.68	5.41	46
47	46.74	4.91	46.72	5.12	46.70	5.32	46.67	5.52	47
48	47.74	5.02	47.71	5.23	47.69	5.43	47.67	5.64	48
49	48.73	5.12	48.71	5.34	48.69	5.55	48.66	5.76	49
50	49.73	5.23	49.70	5.44	49.68	5.66	49.65	5.88	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	84 Deg.		83½ Deg.		83¼ Deg.		83¼ Deg.		



Distance.	6 Deg.		6¼ Deg.		6½ Deg.		6¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.72	5.33	50.70	5.55	50.67	5.77	50.65	5.99	51
52	51.72	5.44	51.69	5.66	51.67	5.89	51.64	6.11	52
53	52.71	5.54	52.68	5.77	52.66	6.00	52.63	6.23	53
54	53.70	5.64	53.68	5.88	53.65	6.11	53.63	6.35	54
55	54.70	5.75	54.67	5.99	54.65	6.23	54.62	6.46	55
56	55.69	5.85	55.67	6.10	55.64	6.34	55.61	6.58	56
57	56.69	5.96	56.66	6.21	56.63	6.45	56.60	6.70	57
58	57.68	6.06	57.66	6.31	57.63	6.57	57.60	6.82	58
59	58.68	6.17	58.65	6.42	58.62	6.68	58.59	6.93	59
60	59.67	6.27	59.64	6.53	59.61	6.79	59.58	7.05	60
61	60.67	6.38	60.64	6.64	60.61	6.91	60.58	7.17	61
62	61.66	6.48	61.63	6.75	61.60	7.02	61.57	7.29	62
63	62.65	6.59	62.63	6.86	62.60	7.13	62.56	7.40	63
64	63.65	6.69	63.62	6.97	63.59	7.25	63.56	7.52	64
65	64.64	6.79	64.61	7.08	64.58	7.36	64.55	7.64	65
66	65.64	6.90	65.61	7.19	65.58	7.47	65.54	7.76	66
67	66.63	7.00	66.60	7.29	66.57	7.58	66.54	7.88	67
68	67.63	7.11	67.60	7.40	67.56	7.70	67.53	7.99	68
69	68.62	7.21	68.59	7.51	68.56	7.81	68.52	8.11	69
70	69.62	7.32	69.58	7.62	69.55	7.92	69.51	8.23	70
71	70.61	7.42	70.58	7.73	70.54	8.04	70.51	8.35	71
72	71.61	7.53	71.57	7.84	71.54	8.15	71.50	8.46	72
73	72.60	7.63	72.57	7.95	72.53	8.26	72.49	8.58	73
74	73.59	7.74	73.56	8.06	73.52	8.38	73.49	8.70	74
75	74.59	7.84	74.55	8.17	74.52	8.49	74.48	8.82	75
76	75.58	7.94	75.55	8.27	75.51	8.60	75.47	8.93	76
77	76.58	8.05	76.54	8.38	76.51	8.72	76.47	9.05	77
78	77.57	8.15	77.54	8.49	77.50	8.83	77.46	9.17	78
79	78.57	8.26	78.53	8.60	78.49	8.94	78.45	9.29	79
80	79.56	8.36	79.53	8.71	79.49	9.06	79.45	9.40	80
81	80.56	8.47	80.52	8.82	80.48	9.17	80.44	9.52	81
82	81.55	8.57	81.51	8.93	81.47	9.28	81.43	9.64	82
83	82.55	8.68	82.51	9.04	82.47	9.40	82.42	9.76	83
84	83.54	8.78	83.50	9.14	83.46	9.51	83.42	9.87	84
85	84.53	8.88	84.50	9.25	84.45	9.62	84.41	9.99	85
86	85.53	8.99	85.49	9.36	85.45	9.74	85.40	10.11	86
87	86.52	9.09	86.48	9.47	86.44	9.85	86.40	10.23	87
88	87.52	9.20	87.48	9.58	87.43	9.96	87.39	10.34	88
89	88.51	9.30	88.47	9.69	88.43	10.08	88.38	10.46	89
90	89.51	9.41	89.47	9.80	89.42	10.19	89.38	10.58	90
91	90.50	9.51	90.46	9.91	90.42	10.30	90.37	10.70	91
92	91.50	9.62	91.45	10.02	91.41	10.41	91.36	10.81	92
93	92.49	9.72	92.45	10.12	92.40	10.53	92.36	10.93	93
94	93.49	9.83	93.44	10.23	93.40	10.64	93.35	11.05	94
95	94.48	9.93	94.44	10.34	94.39	10.75	94.34	11.17	95
96	95.47	10.03	95.43	10.45	95.38	10.87	95.33	11.28	96
97	96.47	10.14	96.42	10.56	96.38	10.99	96.33	11.40	97
98	97.46	10.24	97.42	10.67	97.37	11.09	97.32	11.52	98
99	98.46	10.35	98.41	10.78	98.36	11.21	98.31	11.64	99
100	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	84 Deg.		83¾ Deg.		83½ Deg.		83¼ Deg.		

Distance.	7 Deg.		7¼ Deg.		7½ Deg.		7¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.99	0.12	0.99	0.13	0.99	0.13	0.99	0.13	1
2	1.99	0.24	1.98	0.25	1.98	0.26	1.98	0.27	2
3	2.98	0.37	2.98	0.38	2.97	0.39	2.97	0.40	3
4	3.97	0.49	3.97	0.50	3.97	0.52	3.96	0.54	4
5	4.96	0.61	4.96	0.63	4.96	0.65	4.95	0.67	5
6	5.96	0.73	5.95	0.76	5.95	0.78	5.95	0.81	6
7	6.95	0.85	6.94	0.88	6.94	0.91	6.94	0.94	7
8	7.94	0.97	7.94	1.01	7.93	1.04	7.93	1.08	8
9	8.93	1.10	8.93	1.14	8.92	1.17	8.92	1.21	9
10	9.93	1.22	9.92	1.26	9.91	1.31	9.91	1.35	10
11	10.92	1.34	10.91	1.39	10.91	1.44	10.90	1.48	11
12	11.91	1.46	11.90	1.51	11.90	1.57	11.89	1.62	12
13	12.90	1.58	12.90	1.64	12.89	1.70	12.88	1.75	13
14	13.90	1.71	13.89	1.77	13.88	1.83	13.87	1.89	14
15	14.89	1.83	14.88	1.89	14.87	1.96	14.86	2.02	15
16	15.88	1.95	15.87	2.02	15.86	2.09	15.85	2.16	16
17	16.87	2.07	16.86	2.15	16.85	2.22	16.84	2.29	17
18	17.87	2.19	17.86	2.27	17.85	2.35	17.84	2.43	18
19	18.86	2.32	18.85	2.40	18.84	2.48	18.83	2.56	19
20	19.85	2.44	19.84	2.52	19.83	2.61	19.82	2.70	20
21	20.84	2.56	20.83	2.65	20.82	2.74	20.81	2.83	21
22	21.84	2.68	21.82	2.78	21.81	2.87	21.80	2.97	22
23	22.83	2.80	22.82	2.90	22.80	3.00	22.79	3.10	23
24	23.82	2.92	23.81	3.03	23.79	3.13	23.78	3.24	24
25	24.81	3.05	24.80	3.15	24.79	3.26	24.77	3.37	25
26	25.81	3.17	25.79	3.28	25.78	3.39	25.76	3.51	26
27	26.80	3.29	26.78	3.41	26.77	3.52	26.75	3.64	27
28	27.79	3.41	27.78	3.53	27.76	3.65	27.74	3.78	28
29	28.78	3.53	28.77	3.66	28.75	3.79	28.74	3.91	29
30	29.78	3.66	29.76	3.79	29.74	3.92	29.73	4.05	30
31	30.77	3.78	30.75	3.91	30.73	4.05	30.72	4.18	31
32	31.76	3.90	31.74	4.04	31.73	4.18	31.71	4.32	32
33	32.75	4.02	32.74	4.16	32.72	4.31	32.70	4.45	33
34	33.75	4.14	33.73	4.29	33.71	4.44	33.69	4.58	34
35	34.74	4.27	34.72	4.42	34.70	4.57	34.68	4.72	35
36	35.73	4.39	35.71	4.54	35.69	4.70	35.67	4.85	36
37	36.72	4.51	36.70	4.67	36.68	4.83	36.66	4.99	37
38	37.72	4.63	37.70	4.80	37.67	4.96	37.65	5.12	38
39	38.71	4.75	38.69	4.92	38.67	5.09	38.64	5.26	39
40	39.70	4.87	39.68	5.05	39.66	5.22	39.63	5.39	40
41	40.70	5.00	40.67	5.17	40.65	5.35	40.63	5.53	41
42	41.69	5.12	41.66	5.30	41.64	5.48	41.62	5.66	42
43	42.68	5.24	42.66	5.43	42.63	5.61	42.61	5.80	43
44	43.67	5.36	43.65	5.55	43.62	5.74	43.60	5.93	44
45	44.67	5.48	44.64	5.68	44.62	5.87	44.59	6.07	45
46	45.66	5.61	45.63	5.81	45.61	6.00	45.58	6.20	46
47	46.65	5.73	46.62	5.93	46.60	6.13	46.57	6.34	47
48	47.64	5.85	47.62	6.06	47.59	6.27	47.56	6.47	48
49	48.63	5.97	48.61	6.18	48.58	6.40	48.55	6.61	49
50	49.63	6.09	49.60	6.31	49.57	6.53	49.54	6.74	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	83 Deg.		82¾ Deg.		82½ Deg.		82¼ Deg.		

Distance.	7 Deg.		7¼ Deg.		7½ Deg.		7¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.62	6.22	50.59	6.44	50.56	6.66	50.53	6.88	51
52	51.61	6.34	51.58	6.56	51.56	6.79	51.53	7.01	52
53	52.60	6.46	52.58	6.69	52.55	6.92	52.52	7.15	53
54	53.60	6.58	53.57	6.81	53.54	7.05	53.51	7.28	54
55	54.59	6.70	54.56	6.94	54.53	7.18	54.50	7.42	55
56	55.58	6.82	55.55	7.07	55.52	7.31	55.49	7.55	56
57	56.58	6.95	56.54	7.19	56.51	7.44	56.48	7.69	57
58	57.57	7.07	57.54	7.32	57.50	7.57	57.47	7.82	58
59	58.56	7.19	58.53	7.45	58.50	7.70	58.46	7.96	59
60	59.55	7.31	59.52	7.57	59.49	7.83	59.45	8.09	60
61	60.55	7.43	60.51	7.70	60.48	7.96	60.44	8.23	61
62	61.54	7.56	61.50	7.82	61.47	8.09	61.43	8.36	62
63	62.53	7.68	62.50	7.95	62.46	8.22	62.42	8.50	63
64	63.52	7.80	63.49	8.08	63.45	8.35	63.42	8.63	64
65	64.52	7.92	64.48	8.20	64.44	8.48	64.41	8.77	65
66	65.51	8.04	65.47	8.33	65.44	8.61	65.40	8.90	66
67	66.50	8.17	66.46	8.46	66.43	8.75	66.39	9.04	67
68	67.49	8.29	67.46	8.58	67.42	8.88	67.38	9.17	68
69	68.49	8.41	68.45	8.71	68.41	9.01	68.37	9.30	69
70	69.48	8.53	69.44	8.83	69.40	9.14	69.36	9.44	70
71	70.47	8.65	70.43	8.96	70.39	9.27	70.35	9.57	71
72	71.46	8.77	71.42	9.09	71.38	9.40	71.34	9.71	72
73	72.46	8.90	72.42	9.21	72.38	9.53	72.33	9.84	73
74	73.45	9.02	73.41	9.34	73.37	9.66	73.32	9.98	74
75	74.44	9.14	74.40	9.46	74.36	9.79	74.31	10.11	75
76	75.43	9.26	75.39	9.59	75.35	9.92	75.31	10.25	76
77	76.43	9.38	76.38	9.72	76.34	10.05	76.30	10.38	77
78	77.42	9.51	77.38	9.84	77.33	10.18	77.29	10.52	78
79	78.41	9.63	78.37	9.97	78.32	10.31	78.28	10.65	79
80	79.40	9.75	79.36	10.10	79.32	10.44	79.27	10.79	80
81	80.40	9.87	80.35	10.22	80.31	10.57	80.26	10.92	81
82	81.39	9.99	81.34	10.35	81.30	10.70	81.25	11.06	82
83	82.38	10.12	82.34	10.47	82.29	10.83	82.24	11.19	83
84	83.37	10.24	83.33	10.60	83.28	10.96	83.23	11.33	84
85	84.37	10.36	84.32	10.73	84.27	11.09	84.22	11.46	85
86	85.36	10.48	85.31	10.85	85.26	11.23	85.21	11.60	86
87	86.35	10.60	86.30	10.98	86.26	11.36	86.21	11.73	87
88	87.34	10.72	87.30	11.11	87.25	11.49	87.20	11.87	88
89	88.34	10.85	88.29	11.23	88.24	11.62	88.19	12.00	89
90	89.33	10.97	89.28	11.36	89.23	11.75	89.18	12.14	90
91	90.32	11.09	90.27	11.48	90.22	11.88	90.17	12.27	91
92	91.31	11.21	91.26	11.61	91.21	12.01	91.16	12.41	92
93	92.31	11.33	92.26	11.74	92.20	12.14	92.15	12.54	93
94	93.30	11.46	93.25	11.86	93.20	12.27	93.14	12.68	94
95	94.29	11.58	94.24	11.99	94.19	12.40	94.13	12.81	95
96	95.28	11.70	95.23	12.12	95.18	12.53	95.12	12.95	96
97	96.28	11.82	96.22	12.24	96.17	12.66	96.11	13.08	97
98	97.27	11.94	97.22	12.37	97.16	12.79	97.10	13.22	98
99	98.26	12.07	98.21	12.49	98.15	12.92	98.10	13.35	99
100	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	83 Deg.		82¾ Deg.		82½ Deg.		82¼ Deg.		

Distance.	8 Deg.		8¼ Deg.		8½ Deg.		8¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.99	0.14	0.99	0.14	0.99	0.15	0.99	0.15	1
2	1.98	0.28	1.98	0.29	1.98	0.30	1.98	0.30	2
3	2.97	0.42	2.97	0.43	2.97	0.44	2.97	0.46	3
4	3.96	0.56	3.96	0.57	3.96	0.59	3.95	0.61	4
5	4.95	0.70	4.95	0.72	4.95	0.74	4.94	0.76	5
6	5.94	0.84	5.94	0.86	5.93	0.89	5.93	0.91	6
7	6.93	0.97	6.93	1.00	6.92	1.03	6.92	1.06	7
8	7.92	1.11	7.92	1.15	7.91	1.18	7.91	1.22	8
9	8.91	1.25	8.91	1.29	8.90	1.33	8.90	1.37	9
10	9.90	1.39	9.90	1.43	9.89	1.48	9.88	1.52	10
11	10.89	1.53	10.89	1.58	10.88	1.63	10.87	1.67	11
12	11.88	1.67	11.88	1.72	11.87	1.77	11.86	1.83	12
13	12.87	1.81	12.87	1.87	12.86	1.92	12.85	1.98	13
14	13.86	1.95	13.86	2.01	13.85	2.07	13.84	2.13	14
15	14.85	2.09	14.85	2.15	14.84	2.22	14.83	2.28	15
16	15.84	2.23	15.84	2.30	15.82	2.36	15.81	2.43	16
17	16.83	2.37	16.83	2.44	16.81	2.51	16.80	2.59	17
18	17.82	2.51	17.81	2.58	17.80	2.66	17.79	2.74	18
19	18.82	2.64	18.80	2.73	18.79	2.81	18.78	2.89	19
20	19.81	2.78	19.79	2.87	19.78	2.96	19.77	3.04	20
21	20.80	2.92	20.78	3.01	20.77	3.10	20.76	3.19	21
22	21.79	3.06	21.77	3.16	21.76	3.25	21.74	3.35	22
23	22.78	3.20	22.76	3.30	22.75	3.40	22.73	3.50	23
24	23.77	3.34	23.75	3.44	23.74	3.55	23.72	3.65	24
25	24.76	3.48	24.74	3.59	24.73	3.70	24.71	3.80	25
26	25.75	3.62	25.73	3.73	25.71	3.84	25.70	3.96	26
27	26.74	3.76	26.72	3.87	26.70	3.99	26.69	4.11	27
28	27.73	3.90	27.71	4.02	27.69	4.14	27.67	4.26	28
29	28.72	4.04	28.70	4.16	28.68	4.29	28.66	4.41	29
30	29.71	4.18	29.69	4.30	29.67	4.43	29.65	4.56	30
31	30.70	4.31	30.68	4.45	30.66	4.58	30.64	4.72	31
32	31.69	4.45	31.67	4.59	31.65	4.73	31.63	4.87	32
33	32.68	4.59	32.66	4.74	32.64	4.88	32.62	5.02	33
34	33.67	4.73	33.65	4.88	33.63	5.03	33.60	5.17	34
35	34.66	4.87	34.64	5.02	34.62	5.17	34.59	5.32	35
36	35.65	5.01	35.63	5.17	35.60	5.32	35.58	5.48	36
37	36.64	5.15	36.62	5.31	36.59	5.47	36.57	5.63	37
38	37.63	5.29	37.61	5.45	37.58	5.62	37.56	5.78	38
39	38.62	5.43	38.60	5.60	38.57	5.76	38.55	5.93	39
40	39.61	5.57	39.59	5.74	39.56	5.91	39.53	6.08	40
41	40.60	5.71	40.58	5.88	40.55	6.06	40.52	6.24	41
42	41.59	5.85	41.57	6.03	41.54	6.21	41.51	6.39	42
43	42.58	5.98	42.56	6.17	42.53	6.36	42.50	6.54	43
44	43.57	6.12	43.54	6.31	43.52	6.50	43.49	6.69	44
45	44.56	6.26	44.53	6.46	44.51	6.65	44.48	6.85	45
46	45.55	6.40	45.52	6.60	45.49	6.80	45.46	7.00	46
47	46.54	6.54	46.51	6.74	46.48	6.95	46.45	7.15	47
48	47.53	6.68	47.50	6.89	47.47	7.09	47.44	7.30	48
49	48.52	6.82	48.49	7.03	48.46	7.24	48.43	7.45	49
50	49.51	6.96	49.48	7.17	49.45	7.39	49.42	7.61	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	82 Deg.		81¼ Deg.		81½ Deg.		81¾ Deg.		

Distance.	8 Deg.		8¼ Deg.		8½ Deg.		8¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.50	7.10	50.47	7.32	50.44	7.54	50.41	7.76	51
52	51.49	7.24	51.46	7.46	51.43	7.69	51.39	7.91	52
53	52.48	7.38	52.45	7.61	52.42	7.83	52.38	8.06	53
54	53.47	7.52	53.44	7.75	53.41	7.98	53.37	8.21	54
55	54.46	7.65	54.43	7.89	54.40	8.13	54.36	8.37	55
56	55.46	7.79	55.42	8.04	55.38	8.28	55.35	8.52	56
57	56.45	7.93	56.41	8.18	56.37	8.43	56.34	8.67	57
58	57.44	8.07	57.40	8.32	57.36	8.57	57.32	8.82	58
59	58.43	8.21	58.39	8.47	58.35	8.72	58.31	8.98	59
60	59.42	8.35	59.38	8.61	59.34	8.87	59.30	9.13	60
61	60.41	8.49	60.37	8.75	60.33	9.02	60.29	9.28	61
62	61.40	8.63	61.36	8.90	61.32	9.16	61.28	9.43	62
63	62.39	8.77	62.35	9.04	62.31	9.31	62.27	9.58	63
64	63.38	8.91	63.34	9.18	63.30	9.46	63.26	9.74	64
65	64.37	9.05	64.33	9.33	64.29	9.61	64.24	9.89	65
66	65.36	9.19	65.32	9.47	65.28	9.76	65.23	10.04	66
67	66.35	9.32	66.31	9.61	66.26	9.90	66.22	10.19	67
68	67.34	9.46	67.30	9.76	67.25	10.05	67.21	10.34	68
69	68.33	9.60	68.29	9.90	68.24	10.20	68.20	10.50	69
70	69.32	9.74	69.28	10.04	69.23	10.35	69.19	10.65	70
71	70.31	9.88	70.27	10.19	70.22	10.49	70.17	10.80	71
72	71.30	10.02	71.25	10.33	71.21	10.64	71.16	10.95	72
73	72.29	10.16	72.24	10.47	72.20	10.79	72.15	11.10	73
74	73.28	10.30	73.23	10.62	73.19	10.94	73.14	11.26	74
75	74.27	10.44	74.22	10.76	74.18	11.09	74.13	11.41	75
76	75.26	10.58	75.21	10.91	75.17	11.23	75.12	11.56	76
77	76.25	10.72	76.20	11.05	76.15	11.38	76.10	11.71	77
78	77.24	10.86	77.19	11.19	77.14	11.53	77.09	11.87	78
79	78.23	10.99	78.18	11.34	78.13	11.68	78.08	12.02	79
80	79.22	11.13	79.17	11.48	79.12	11.82	79.07	12.17	80
81	80.21	11.27	80.16	11.62	80.11	11.97	80.06	12.32	81
82	81.20	11.41	81.15	11.77	81.10	12.12	81.05	12.47	82
83	82.19	11.55	82.14	11.91	82.09	12.27	82.03	12.63	83
84	83.18	11.69	83.13	12.05	83.08	12.42	83.02	12.78	84
85	84.17	11.83	84.12	12.20	84.07	12.56	84.01	12.93	85
86	85.16	11.97	85.11	12.34	85.06	12.71	85.00	13.08	86
87	86.15	12.11	86.10	12.48	86.04	12.86	85.99	13.23	87
88	87.14	12.25	87.09	12.63	87.03	13.01	86.98	13.39	88
89	88.13	12.39	88.08	12.77	88.02	13.16	87.96	13.54	89
90	89.12	12.53	89.07	12.91	89.01	13.30	88.95	13.69	90
91	90.11	12.66	90.06	13.06	90.00	13.45	89.94	13.84	91
92	91.10	12.80	91.05	13.20	90.99	13.60	90.93	14.00	92
93	92.09	12.94	92.04	13.34	91.98	13.75	91.92	14.15	93
94	93.09	13.08	93.03	13.49	92.97	13.89	92.91	14.30	94
95	94.08	13.22	94.02	13.63	93.96	14.04	93.89	14.45	95
96	95.07	13.36	95.01	13.78	94.95	14.19	94.88	14.60	96
97	96.06	13.50	96.00	13.92	95.93	14.34	95.87	14.76	97
98	97.05	13.64	96.99	14.06	96.92	14.49	96.86	14.91	98
99	98.04	13.78	97.98	14.21	97.91	14.63	97.85	15.06	99
100	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	82 Deg.		81¾ Deg.		81½ Deg.		81¼ Deg.		

Distance.	9 Deg.		9¼ Deg.		9½ Deg.		9¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.99	0.16	0.99	0.16	0.99	0.17	0.99	0.17	1
2	1.98	0.31	1.97	0.32	1.97	0.33	1.97	0.34	2
3	2.96	0.47	2.96	0.48	2.96	0.50	2.96	0.51	3
4	3.95	0.63	3.95	0.64	3.95	0.66	3.94	0.68	4
5	4.94	0.78	4.93	0.80	4.93	0.83	4.93	0.85	5
6	5.93	0.94	5.92	0.96	5.92	0.99	5.91	1.02	6
7	6.91	1.10	6.91	1.13	6.90	1.16	6.90	1.19	7
8	7.90	1.25	7.90	1.29	7.89	1.32	7.88	1.35	8
9	8.89	1.41	8.88	1.45	8.88	1.49	8.87	1.52	9
10	9.88	1.56	9.87	1.61	9.86	1.65	9.86	1.69	10
11	10.86	1.72	10.86	1.77	10.85	1.82	10.84	1.86	11
12	11.85	1.88	11.84	1.93	11.84	1.98	11.83	2.03	12
13	12.84	2.03	12.83	2.09	12.82	2.15	12.81	2.20	13
14	13.83	2.19	13.82	2.25	13.81	2.31	13.80	2.37	14
15	14.82	2.35	14.80	2.41	14.79	2.48	14.78	2.54	15
16	15.80	2.50	15.79	2.57	15.78	2.64	15.77	2.71	16
17	16.79	2.66	16.78	2.73	16.77	2.81	16.75	2.88	17
18	17.78	2.82	17.77	2.89	17.75	2.97	17.74	3.05	18
19	18.77	2.97	18.75	3.05	18.74	3.14	18.73	3.22	19
20	19.75	3.13	19.74	3.21	19.73	3.30	19.71	3.39	20
21	20.74	3.29	20.73	3.38	20.71	3.47	20.70	3.56	21
22	21.73	3.44	21.71	3.54	21.70	3.63	21.68	3.73	22
23	22.72	3.60	22.70	3.70	22.68	3.80	22.67	3.90	23
24	23.70	3.75	23.69	3.86	23.67	3.96	23.65	4.06	24
25	24.69	3.91	24.67	4.02	24.66	4.13	24.64	4.23	25
26	25.68	4.07	25.66	4.18	25.64	4.29	25.62	4.40	26
27	26.67	4.22	26.65	4.34	26.63	4.46	26.61	4.57	27
28	27.66	4.38	27.64	4.50	27.62	4.62	27.60	4.74	28
29	28.64	4.54	28.62	4.66	28.60	4.79	28.58	4.91	29
30	29.63	4.69	29.61	4.82	29.59	4.95	29.57	5.08	30
31	30.62	4.85	30.60	4.98	30.57	5.12	30.55	5.25	31
32	31.61	5.01	31.58	5.14	31.56	5.28	31.54	5.42	32
33	32.59	5.16	32.57	5.30	32.55	5.45	32.52	5.59	33
34	33.58	5.32	33.56	5.47	33.53	5.61	33.51	5.76	34
35	34.57	5.48	34.54	5.63	34.52	5.78	34.49	5.93	35
36	35.56	5.63	35.53	5.79	35.51	5.94	35.48	6.10	36
37	36.54	5.79	36.52	5.95	36.49	6.11	36.47	6.27	37
38	37.53	5.94	37.51	6.11	37.48	6.27	37.45	6.44	38
39	38.52	6.10	38.49	6.27	38.47	6.44	38.44	6.60	39
40	39.51	6.26	39.48	6.43	39.45	6.60	39.42	6.77	40
41	40.50	6.41	40.47	6.59	40.44	6.77	40.41	6.94	41
42	41.48	6.57	41.45	6.75	41.42	6.92	41.39	7.11	42
43	42.47	6.73	42.44	6.91	42.41	7.10	42.38	7.28	43
44	43.46	6.88	43.43	7.07	43.40	7.26	43.36	7.45	44
45	44.45	7.04	44.41	7.23	44.38	7.43	44.35	7.62	45
46	45.43	7.20	45.40	7.39	45.37	7.59	45.34	7.79	46
47	46.42	7.35	46.39	7.55	46.36	7.76	46.32	7.96	47
48	47.41	7.51	47.38	7.72	47.34	7.92	47.31	8.13	48
49	48.40	7.67	48.36	7.88	48.33	8.09	48.29	8.30	49
50	49.38	7.82	49.35	8.04	49.32	8.25	49.28	8.47	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	81 Deg.		80¾ Deg.		80½ Deg.		80¼ Deg.		

Distance.	9 Deg.		9¼ Deg.		9½ Deg.		9¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.37	7.98	50.34	8.20	50.30	8.42	50.26	8.64	51
52	51.36	8.13	51.32	8.36	51.29	8.58	51.25	8.81	52
53	52.35	8.29	52.31	8.52	52.27	8.75	52.23	8.98	53
54	53.34	8.45	53.30	8.68	53.26	8.91	53.22	9.14	54
55	54.32	8.60	54.28	8.84	54.25	9.08	54.21	9.31	55
56	55.31	8.76	55.27	9.00	55.23	9.24	55.19	9.48	56
57	56.30	8.92	56.26	9.16	56.22	9.41	56.18	9.65	57
58	57.29	9.07	57.25	9.32	57.20	9.57	57.16	9.82	58
59	58.27	9.23	58.23	9.48	58.19	9.74	58.15	9.99	59
60	59.26	9.39	59.22	9.64	59.18	9.90	59.13	10.16	60
61	60.25	9.54	60.21	9.81	60.16	10.07	60.12	10.33	61
62	61.24	9.70	61.19	9.97	61.15	10.23	61.10	10.50	62
63	62.22	9.86	62.18	10.13	62.14	10.40	62.09	10.67	63
64	63.21	10.01	63.17	10.29	63.12	10.56	63.08	10.84	64
65	64.20	10.17	64.15	10.45	64.11	10.73	64.06	11.01	65
66	65.19	10.32	65.14	10.61	65.09	10.89	65.05	11.18	66
67	66.18	10.48	66.13	10.77	66.08	11.06	66.03	11.35	67
68	67.16	10.64	67.12	10.93	67.07	11.22	67.02	11.52	68
69	68.15	10.79	68.10	11.09	68.05	11.39	68.00	11.69	69
70	69.14	10.95	69.09	11.25	69.04	11.55	68.99	11.85	70
71	70.13	11.11	70.08	11.41	70.03	11.72	69.97	12.02	71
72	71.11	11.26	71.06	11.57	71.01	11.88	70.96	12.19	72
73	72.10	11.42	72.05	11.73	72.00	12.05	71.95	12.36	73
74	73.09	11.58	73.04	11.89	72.99	12.21	72.93	12.53	74
75	74.08	11.73	74.02	12.06	73.97	12.38	73.92	12.70	75
76	75.06	11.89	75.01	12.22	74.96	12.54	74.90	12.87	76
77	76.05	12.05	76.00	12.38	75.94	12.71	75.89	13.04	77
78	77.04	12.20	76.99	12.54	76.93	12.87	76.87	13.21	78
79	78.03	12.36	77.97	12.70	77.92	13.04	77.86	13.38	79
80	79.02	12.51	78.96	12.86	78.90	13.20	78.84	13.55	80
81	80.00	12.67	79.95	13.02	79.89	13.37	79.83	13.72	81
82	80.99	12.83	80.93	13.18	80.88	13.53	80.82	13.89	82
83	81.98	12.98	81.92	13.34	81.86	13.70	81.80	14.06	83
84	82.97	13.14	82.91	13.50	82.85	13.86	82.79	14.23	84
85	83.95	13.30	83.89	13.66	83.83	14.03	83.77	14.39	85
86	84.94	13.45	84.88	13.82	84.82	14.19	84.76	14.56	86
87	85.93	13.61	85.87	13.98	85.81	14.36	85.74	14.73	87
88	86.92	13.77	86.86	14.15	86.79	14.52	86.73	14.90	88
89	87.90	13.92	87.84	14.31	87.78	14.69	87.71	15.07	89
90	88.89	14.08	88.83	14.47	88.77	14.85	88.70	15.24	90
91	89.88	14.24	89.82	14.63	89.75	15.02	89.69	15.41	91
92	90.87	14.39	90.80	14.79	90.74	15.18	90.67	15.58	92
93	91.86	14.55	91.79	14.95	91.72	15.35	91.66	15.75	93
94	92.84	14.70	92.78	15.11	92.71	15.51	92.64	15.92	94
95	93.83	14.86	93.76	15.27	93.70	15.68	93.63	16.09	95
96	94.82	15.02	94.75	15.43	94.68	15.84	94.61	16.26	96
97	95.81	15.17	95.74	15.59	95.67	16.01	95.60	16.43	97
98	96.79	15.33	96.73	15.75	96.66	16.17	96.58	16.60	98
99	97.78	15.49	97.71	15.91	97.64	16.34	97.57	16.77	99
100	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	81 Deg.		80¾ Deg.		80½ Deg.		80¼ Deg.		

Distance.	10 Deg.		10 $\frac{1}{4}$ Deg.		10 $\frac{1}{2}$ Deg.		10 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.98	0.17	0.98	0.18	0.98	0.18	0.98	0.19	1
2	1.97	0.35	1.97	0.36	1.97	0.36	1.96	0.37	2
3	2.95	0.52	2.95	0.53	2.95	0.55	2.95	0.56	3
4	3.94	0.69	3.94	0.71	3.93	0.73	3.93	0.75	4
5	4.92	0.87	4.92	0.89	4.92	0.91	4.91	0.93	5
6	5.91	1.04	5.90	1.07	5.90	1.09	5.89	1.12	6
7	6.89	1.22	6.89	1.25	6.88	1.28	6.88	1.31	7
8	7.88	1.39	7.87	1.42	7.87	1.46	7.86	1.49	8
9	8.86	1.56	8.86	1.60	8.85	1.64	8.84	1.68	9
10	9.85	1.74	9.84	1.78	9.83	1.82	9.82	1.87	10
11	10.83	1.91	10.82	1.96	10.82	2.00	10.81	2.05	11
12	11.82	2.08	11.81	2.14	11.80	2.19	11.79	2.24	12
13	12.80	2.26	12.79	2.31	12.78	2.37	12.77	2.42	13
14	13.79	2.43	13.78	2.49	13.77	2.55	13.75	2.61	14
15	14.77	2.60	14.76	2.67	14.75	2.73	14.74	2.80	15
16	15.76	2.78	15.74	2.85	15.73	2.92	15.72	2.98	16
17	16.74	2.95	16.73	3.03	16.72	3.10	16.70	3.17	17
18	17.73	3.13	17.71	3.20	17.70	3.28	17.68	3.36	18
19	18.71	3.30	18.70	3.38	18.68	3.46	18.67	3.54	19
20	19.70	3.47	19.68	3.56	19.67	3.64	19.65	3.73	20
21	20.68	3.65	20.66	3.74	20.65	3.83	20.63	3.92	21
22	21.67	3.82	21.65	3.91	21.63	4.01	21.61	4.10	22
23	22.65	3.99	22.63	4.09	22.61	4.19	22.60	4.29	23
24	23.64	4.17	23.62	4.27	23.60	4.37	23.58	4.48	24
25	24.62	4.34	24.60	4.45	24.58	4.56	24.56	4.66	25
26	25.61	4.51	25.59	4.63	25.56	4.74	25.54	4.85	26
27	26.59	4.69	26.57	4.80	26.55	4.92	26.53	5.04	27
28	27.57	4.86	27.55	4.98	27.53	5.10	27.51	5.22	28
29	28.56	5.04	28.54	5.16	28.51	5.28	28.49	5.41	29
30	29.54	5.21	29.52	5.34	29.50	5.47	29.47	5.60	30
31	30.53	5.38	30.51	5.52	30.48	5.65	30.46	5.78	31
32	31.51	5.56	31.49	5.69	31.46	5.83	31.44	5.97	32
33	32.50	5.73	32.47	5.87	32.45	6.01	32.42	6.16	33
34	33.48	5.90	33.46	6.05	33.43	6.20	33.40	6.34	34
35	34.47	6.08	34.44	6.23	34.41	6.38	34.39	6.53	35
36	35.45	6.25	35.43	6.41	35.40	6.56	35.37	6.71	36
37	36.44	6.42	36.41	6.58	36.38	6.74	36.35	6.90	37
38	37.42	6.60	37.39	6.76	37.36	6.92	37.33	7.09	38
39	38.41	6.77	38.38	6.94	38.35	7.11	38.32	7.27	39
40	39.39	6.95	39.36	7.12	39.33	7.29	39.30	7.46	40
41	40.38	7.12	40.35	7.30	40.31	7.47	40.28	7.65	41
42	41.36	7.29	41.33	7.47	41.30	7.65	41.26	7.83	42
43	42.35	7.47	42.31	7.65	42.28	7.84	42.25	8.02	43
44	43.33	7.64	43.30	7.83	43.26	8.02	43.23	8.21	44
45	44.32	7.81	44.28	8.01	44.25	8.20	44.21	8.39	45
46	45.30	7.99	45.27	8.19	45.23	8.38	45.19	8.58	46
47	46.29	8.16	46.25	8.36	46.21	8.57	46.18	8.77	47
48	47.27	8.34	47.23	8.54	47.20	8.75	47.16	8.95	48
49	48.26	8.51	48.22	8.72	48.18	8.93	48.14	9.14	49
50	49.24	8.68	49.20	8.90	49.16	9.11	49.12	9.33	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	80 Deg.		79 $\frac{3}{4}$ Deg.		79 $\frac{1}{2}$ Deg.		79 $\frac{1}{4}$ Deg.		



Distance.	10 Deg.		10½ Deg.		10¾ Deg.		10¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.23	8.86	50.19	9.08	50.15	9.29	50.10	9.51	51
52	51.21	9.03	51.17	9.25	51.13	9.48	51.09	9.70	52
53	52.19	9.20	52.15	9.43	52.11	9.66	52.07	9.89	53
54	53.18	9.38	53.14	9.61	53.10	9.84	53.05	10.07	54
55	54.16	9.55	54.12	9.79	54.08	10.02	54.03	10.26	55
56	55.15	9.72	55.11	9.96	55.06	10.21	55.02	10.45	56
57	56.13	9.90	56.09	10.14	56.05	10.39	56.00	10.63	57
58	57.12	10.07	57.07	10.32	57.03	10.57	56.98	10.82	58
59	58.10	10.25	58.06	10.50	58.01	10.75	57.96	11.00	59
60	59.09	10.42	59.04	10.68	59.00	10.93	58.95	11.19	60
61	60.07	10.59	60.03	10.85	59.98	11.12	59.93	11.38	61
62	61.06	10.77	61.01	11.03	60.96	11.30	60.91	11.56	62
63	62.04	10.94	61.99	11.21	61.95	11.48	61.89	11.75	63
64	63.03	11.11	62.98	11.39	62.93	11.66	62.88	11.94	64
65	64.01	11.29	63.96	11.57	63.91	11.85	63.86	12.12	65
66	65.00	11.46	64.95	11.74	64.89	12.03	64.84	12.31	66
67	65.98	11.63	65.93	11.92	65.88	12.21	65.82	12.50	67
68	66.97	11.81	66.91	12.10	66.86	12.39	66.81	12.68	68
69	67.95	11.98	67.90	12.28	67.84	12.57	67.79	12.87	69
70	68.94	12.16	68.88	12.46	68.83	12.76	68.77	13.06	70
71	69.92	12.33	69.87	12.63	69.81	12.94	69.75	13.24	71
72	70.91	12.50	70.85	12.81	70.79	13.12	70.74	13.43	72
73	71.89	12.68	71.83	12.99	71.78	13.30	71.72	13.62	73
74	72.88	12.85	72.82	13.17	72.76	13.49	72.70	13.80	74
75	73.86	13.02	73.80	13.35	73.74	13.67	73.68	13.99	75
76	74.85	13.20	74.79	13.52	74.73	13.85	74.67	14.18	76
77	75.83	13.37	75.77	13.70	75.71	14.03	75.65	14.36	77
78	76.82	13.54	76.76	13.88	76.69	14.21	76.63	14.55	78
79	77.80	13.72	77.74	14.06	77.68	14.40	77.61	14.74	79
80	78.78	13.89	78.72	14.24	78.66	14.58	78.60	14.92	80
81	79.77	14.07	79.71	14.41	79.64	14.76	79.58	15.11	81
82	80.75	14.24	80.69	14.59	80.63	14.94	80.56	15.29	82
83	81.74	14.41	81.68	14.77	81.61	15.13	81.54	15.48	83
84	82.72	14.59	82.66	14.95	82.59	15.31	82.53	15.67	84
85	83.71	14.76	83.64	15.13	83.58	15.49	83.51	15.85	85
86	84.69	14.93	84.63	15.30	84.56	15.67	84.49	16.04	86
87	85.68	15.11	85.61	15.48	85.54	15.85	85.47	16.23	87
88	86.66	15.28	86.60	15.66	86.53	16.04	86.46	16.41	88
89	87.65	15.45	87.58	15.84	87.51	16.22	87.44	16.60	89
90	88.63	15.63	88.56	16.01	88.49	16.40	88.42	16.79	90
91	89.62	15.80	89.55	16.19	89.48	16.58	89.40	16.97	91
92	90.60	15.98	90.53	16.37	90.46	16.77	90.39	17.16	92
93	91.59	16.15	91.52	16.55	91.44	16.95	91.37	17.35	93
94	92.57	16.32	92.50	16.73	92.43	17.13	92.35	17.53	94
95	93.56	16.50	93.48	16.90	93.41	17.31	93.33	17.72	95
96	94.54	16.67	94.47	17.08	94.39	17.49	94.32	17.91	96
97	95.53	16.84	95.45	17.26	95.38	17.68	95.30	18.09	97
98	96.51	17.02	96.44	17.44	96.36	17.86	96.28	18.28	98
99	97.50	17.19	97.42	17.62	97.34	18.04	97.26	18.47	99
100	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	80 Deg.		79¾ Deg.		79½ Deg.		79¼ Deg.		

Distance.	11 Deg.		11¼ Deg.		11½ Deg.		11¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.98	0.19	0.98	0.20	0.98	0.20	0.98	0.20	1
2	1.96	0.38	1.96	0.39	1.96	0.40	1.96	0.41	2
3	2.94	0.57	2.94	0.59	2.94	0.60	2.94	0.61	3
4	3.93	0.76	3.92	0.78	3.92	0.80	3.92	0.82	4
5	4.91	0.95	4.90	0.98	4.90	1.00	4.90	1.02	5
6	5.89	1.14	5.88	1.17	5.88	1.20	5.87	1.22	6
7	6.87	1.34	6.87	1.37	6.86	1.40	6.85	1.43	7
8	7.85	1.53	7.85	1.56	7.84	1.59	7.83	1.63	8
9	8.83	1.72	8.83	1.76	8.82	1.79	8.81	1.83	9
10	9.82	1.91	9.81	1.95	9.80	1.99	9.79	2.04	10
11	10.80	2.10	10.79	2.15	10.78	2.19	10.77	2.24	11
12	11.78	2.29	11.77	2.34	11.76	2.39	11.75	2.44	12
13	12.76	2.48	12.75	2.54	12.74	2.59	12.73	2.65	13
14	13.74	2.67	13.73	2.73	13.72	2.79	13.71	2.85	14
15	14.72	2.86	14.71	2.93	14.70	2.99	14.69	3.06	15
16	15.71	3.05	15.69	3.12	15.68	3.19	15.66	3.26	16
17	16.69	3.24	16.67	3.32	16.66	3.39	16.64	3.46	17
18	17.67	3.43	17.65	3.51	17.64	3.59	17.62	3.66	18
19	18.65	3.63	18.63	3.71	18.62	3.79	18.60	3.87	19
20	19.63	3.82	19.62	3.90	19.60	3.99	19.58	4.07	20
21	20.61	4.01	20.60	4.10	20.58	4.19	20.56	4.28	21
22	21.60	4.20	21.58	4.29	21.56	4.39	21.54	4.48	22
23	22.58	4.39	22.56	4.49	22.54	4.59	22.52	4.68	23
24	23.56	4.58	23.54	4.68	23.52	4.78	23.50	4.89	24
25	24.54	4.77	24.52	4.88	24.50	4.98	24.48	5.09	25
26	25.52	4.96	25.50	5.07	25.48	5.18	25.46	5.30	26
27	26.50	5.15	26.48	5.27	26.46	5.38	26.43	5.50	27
28	27.49	5.34	27.46	5.46	27.44	5.58	27.41	5.70	28
29	28.47	5.53	28.44	5.66	28.42	5.78	28.39	5.91	29
30	29.45	5.72	29.42	5.85	29.40	5.98	29.37	6.11	30
31	30.43	5.92	30.40	6.05	30.38	6.18	30.35	6.31	31
32	31.41	6.11	31.39	6.24	31.36	6.38	31.33	6.52	32
33	32.39	6.30	32.37	6.44	32.34	6.58	32.31	6.72	33
34	33.38	6.49	33.35	6.63	33.32	6.78	33.29	6.92	34
35	34.36	6.68	34.33	6.83	34.30	6.98	34.27	7.13	35
36	35.34	6.87	35.31	7.02	35.28	7.18	35.25	7.33	36
37	36.32	7.06	36.29	7.22	36.26	7.38	36.22	7.53	37
38	37.30	7.25	37.27	7.41	37.24	7.58	37.20	7.74	38
39	38.28	7.44	38.25	7.61	38.22	7.78	38.18	7.94	39
40	39.27	7.63	39.23	7.80	39.20	7.97	39.16	8.15	40
41	40.25	7.82	40.21	8.00	40.18	8.17	40.14	8.35	41
42	41.23	8.01	41.19	8.19	41.16	8.37	41.12	8.55	42
43	42.21	8.20	42.17	8.39	42.14	8.57	42.10	8.76	43
44	43.19	8.40	43.15	8.58	43.12	8.77	43.08	8.96	44
45	44.17	8.59	44.14	8.78	44.10	8.97	44.06	9.16	45
46	45.15	8.78	45.12	8.97	45.08	9.17	45.04	9.37	46
47	46.14	8.97	46.10	9.17	46.06	9.37	46.02	9.57	47
48	47.12	9.16	47.08	9.36	47.04	9.57	46.99	9.78	48
49	48.10	9.35	48.06	9.56	48.02	9.77	47.97	9.98	49
50	49.08	9.54	49.04	9.75	49.00	9.97	48.95	10.18	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	79 Deg.		78¾ Deg.		78½ Deg.		78¼ Deg.		

Distance	11 Deg.		11¼ Deg.		11½ Deg.		11¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.06	9.73	50.02	9.95	49.98	10.17	49.93	10.39	51
52	51.04	9.92	51.00	10.14	50.96	10.37	50.91	10.59	52
53	52.03	10.11	51.98	10.34	51.94	10.57	51.89	10.79	53
54	53.01	10.30	52.96	10.53	52.92	10.77	52.87	11.00	54
55	53.99	10.49	53.94	10.73	53.90	10.97	53.85	11.20	55
56	54.97	10.69	54.92	10.93	54.88	11.16	54.83	11.40	56
57	55.95	10.88	55.90	11.12	55.86	11.36	55.81	11.61	57
58	56.93	11.07	56.89	11.32	56.84	11.56	56.78	11.81	58
59	57.92	11.26	57.87	11.51	57.82	11.76	57.76	12.01	59
60	58.90	11.45	58.85	11.71	58.80	11.96	58.74	12.22	60
61	59.88	11.64	59.83	11.90	59.78	12.16	59.72	12.42	61
62	60.86	11.83	60.81	12.10	60.76	12.36	60.70	12.63	62
63	61.84	12.02	61.79	12.29	61.74	12.56	61.68	12.83	63
64	62.82	12.21	62.77	12.49	62.72	12.76	62.66	13.03	64
65	63.81	12.40	63.75	12.68	63.70	12.96	63.64	13.24	65
66	64.79	12.59	64.73	12.88	64.68	13.16	64.62	13.44	66
67	65.77	12.78	65.71	13.07	65.66	13.36	65.60	13.64	67
68	66.75	12.98	66.69	13.27	66.63	13.56	66.58	13.85	68
69	67.73	13.17	67.67	13.46	67.61	13.76	67.55	14.05	69
70	68.71	13.36	68.66	13.66	68.59	13.96	68.53	14.25	70
71	69.70	13.55	69.64	13.85	69.57	14.16	69.51	14.46	71
72	70.68	13.74	70.62	14.05	70.55	14.35	70.49	14.66	72
73	71.66	13.93	71.60	14.24	71.53	14.55	71.47	14.87	73
74	72.64	14.12	72.58	14.44	72.51	14.75	72.45	15.07	74
75	73.62	14.31	73.56	14.63	73.49	14.95	73.43	15.27	75
76	74.60	14.50	74.54	14.83	74.47	15.15	74.41	15.48	76
77	75.59	14.69	75.52	15.02	75.45	15.35	75.39	15.68	77
78	76.57	14.88	76.50	15.22	76.43	15.55	76.37	15.88	78
79	77.55	15.07	77.48	15.41	77.41	15.75	77.34	16.09	79
80	78.53	15.26	78.46	15.61	78.39	15.95	78.32	16.29	80
81	79.51	15.46	79.44	15.80	79.37	16.15	79.30	16.49	81
82	80.49	15.65	80.42	16.00	80.35	16.35	80.28	16.70	82
83	81.48	15.84	81.41	16.19	81.33	16.55	81.26	16.90	83
84	82.46	16.03	82.39	16.39	82.31	16.75	82.24	17.11	84
85	83.44	16.22	83.37	16.58	83.29	16.95	83.22	17.31	85
86	84.42	16.41	84.35	16.78	84.27	17.15	84.20	17.51	86
87	85.40	16.60	85.33	16.97	85.25	17.35	85.18	17.72	87
88	86.38	16.79	86.31	17.17	86.23	17.54	86.16	17.92	88
89	87.36	16.98	87.29	17.36	87.21	17.74	87.14	18.12	89
90	88.35	17.17	88.27	17.56	88.19	17.94	88.11	18.33	90
91	89.33	17.36	89.25	17.75	89.17	18.14	89.09	18.53	91
92	90.31	17.55	90.23	17.95	90.15	18.34	90.07	18.74	92
93	91.29	17.75	91.21	18.14	91.13	18.54	91.05	18.94	93
94	92.27	17.94	92.19	18.34	92.11	18.74	92.03	19.14	94
95	93.25	18.13	93.17	18.53	93.09	18.94	93.01	19.35	95
96	94.24	18.32	94.16	18.73	94.07	19.14	93.99	19.55	96
97	95.22	18.51	95.14	18.92	95.05	19.34	94.97	19.75	97
98	96.20	18.70	96.12	19.12	96.03	19.54	95.95	19.96	98
99	97.18	18.89	97.10	19.31	97.01	19.74	96.93	20.16	99
100	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	79 Deg.		78¼ Deg.		78½ Deg.		78¾ Deg.		

Distance.	12 Deg		12¼ Deg.		12½ Deg.		12¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.98	0.21	0.98	0.21	0.98	0.22	0.98	0.22	1
2	1.96	0.42	1.95	0.42	1.95	0.43	1.95	0.44	2
3	2.93	0.62	2.93	0.64	2.93	0.65	2.93	0.66	3
4	3.91	0.83	3.91	0.85	3.91	0.87	3.90	0.88	4
5	4.89	1.04	4.89	1.06	4.88	1.08	4.88	1.10	5
6	5.87	1.25	5.86	1.27	5.86	1.30	5.85	1.32	6
7	6.85	1.46	6.84	1.49	6.83	1.52	6.83	1.54	7
8	7.83	1.66	7.82	1.70	7.81	1.73	7.80	1.77	8
9	8.80	1.87	8.80	1.91	8.79	1.95	8.78	1.99	9
10	9.78	2.08	9.77	2.12	9.76	2.16	9.75	2.21	10
11	10.76	2.29	10.75	2.33	10.74	2.38	10.73	2.43	11
12	11.74	2.49	11.73	2.55	11.72	2.60	11.70	2.65	12
13	12.72	2.70	12.70	2.76	12.69	2.81	12.68	2.87	13
14	13.69	2.91	13.68	2.97	13.67	3.03	13.65	3.09	14
15	14.67	3.12	14.66	3.18	14.64	3.25	14.63	3.31	15
16	15.65	3.33	15.64	3.39	15.62	3.46	15.61	3.53	16
17	16.63	3.53	16.61	3.61	16.60	3.68	16.58	3.75	17
18	17.61	3.74	17.59	3.82	17.57	3.90	17.56	3.97	18
19	18.58	3.95	18.57	4.03	18.55	4.11	18.53	4.19	19
20	19.56	4.16	19.54	4.24	19.53	4.33	19.51	4.41	20
21	20.54	4.37	20.52	4.46	20.50	4.55	20.48	4.63	21
22	21.52	4.57	21.50	4.67	21.48	4.76	21.46	4.86	22
23	22.50	4.78	22.48	4.88	22.45	4.98	22.43	5.08	23
24	23.48	4.99	23.45	5.09	23.43	5.19	23.41	5.30	24
25	24.45	5.20	24.43	5.30	24.41	5.41	24.38	5.52	25
26	25.43	5.41	25.41	5.52	25.38	5.63	25.36	5.74	26
27	26.41	5.61	26.39	5.73	26.36	5.84	26.33	5.96	27
28	27.39	5.82	27.36	5.94	27.34	6.06	27.31	6.18	28
29	28.37	6.03	28.34	6.15	28.31	6.28	28.28	6.40	29
30	29.34	6.24	29.32	6.37	29.29	6.49	29.26	6.62	30
31	30.32	6.45	30.29	6.58	30.27	6.71	30.24	6.84	31
32	31.30	6.65	31.27	6.79	31.24	6.93	31.21	7.06	32
33	32.28	6.86	32.25	7.00	32.22	7.14	32.19	7.28	33
34	33.26	7.07	33.23	7.21	33.19	7.36	33.16	7.50	34
35	34.24	7.28	34.20	7.43	34.17	7.58	34.14	7.72	35
36	35.21	7.48	35.18	7.64	35.15	7.79	35.11	7.95	36
37	36.19	7.69	36.16	7.85	36.12	8.01	36.09	8.17	37
38	37.17	7.90	37.13	8.06	37.10	8.22	37.06	8.39	38
39	38.15	8.11	38.11	8.27	38.08	8.44	38.04	8.61	39
40	39.13	8.32	39.09	8.49	39.05	8.66	39.01	8.83	40
41	40.10	8.52	40.07	8.70	40.03	8.87	39.99	9.05	41
42	41.08	8.73	41.04	8.91	41.00	9.09	40.96	9.27	42
43	42.06	8.94	42.02	9.12	41.98	9.31	41.94	9.49	43
44	43.04	9.15	43.00	9.34	42.96	9.52	42.92	9.71	44
45	44.02	9.36	43.98	9.55	43.93	9.74	43.89	9.93	45
46	44.99	9.56	44.95	9.76	44.91	9.96	44.87	10.15	46
47	45.97	9.77	45.93	9.97	45.89	10.17	45.84	10.37	47
48	46.95	9.98	46.91	10.18	46.86	10.39	46.82	10.59	48
49	47.93	10.19	47.88	10.40	47.84	10.61	47.79	10.81	49
50	48.91	10.40	48.86	10.61	48.81	10.82	48.77	11.03	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	78 Deg.		77¾ Deg.		77½ Deg.		77¼ Deg.		

Distance.	12 Deg.		12 $\frac{1}{4}$ Deg.		12 $\frac{1}{2}$ Deg.		12 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.89	10.60	49.84	10.82	49.79	11.04	49.74	11.26	51
52	50.86	10.81	50.82	11.03	50.77	11.25	50.72	11.48	52
53	51.84	11.02	51.79	11.25	51.74	11.47	51.69	11.70	53
54	52.82	11.23	52.77	11.46	52.72	11.69	52.67	11.92	54
55	53.80	11.44	53.75	11.67	53.70	11.90	53.64	12.14	55
56	54.78	11.64	54.72	11.88	54.67	12.12	54.62	12.36	56
57	55.75	11.85	55.70	12.09	55.65	12.34	55.59	12.58	57
58	56.73	12.06	56.68	12.31	56.63	12.55	56.57	12.80	58
59	57.71	12.27	57.66	12.52	57.60	12.77	57.55	13.02	59
60	58.69	12.47	58.63	12.73	58.58	12.99	58.52	13.24	60
61	59.67	12.68	59.61	12.94	59.55	13.20	59.50	13.46	61
62	60.65	12.89	60.59	13.16	60.53	13.42	60.47	13.68	62
63	61.62	13.10	61.57	13.37	61.51	13.64	61.45	13.90	63
64	62.60	13.31	62.54	13.58	62.48	13.85	62.42	14.12	64
65	63.58	13.51	63.52	13.79	63.46	14.07	63.40	14.35	65
66	64.56	13.72	64.50	14.00	64.44	14.29	64.37	14.57	66
67	65.54	13.93	65.47	14.22	65.41	14.50	65.35	14.79	67
68	66.51	14.14	66.45	14.43	66.39	14.72	66.32	15.01	68
69	67.49	14.35	67.43	14.64	67.36	14.93	67.30	15.23	69
70	68.47	14.55	68.41	14.85	68.34	15.15	68.27	15.45	70
71	69.45	14.76	69.38	15.06	69.32	15.37	69.25	15.67	71
72	70.43	14.97	70.36	15.28	70.29	15.58	70.22	15.89	72
73	71.49	15.18	71.34	15.49	71.27	15.80	71.20	16.11	73
74	72.38	15.39	72.32	15.70	72.25	16.02	72.18	16.33	74
75	73.36	15.59	73.29	15.91	73.22	16.23	73.15	16.55	75
76	74.34	15.80	74.27	16.13	74.20	16.45	74.13	16.77	76
77	75.32	16.01	75.25	16.34	75.17	16.67	75.10	16.99	77
78	76.30	16.22	76.22	16.55	76.15	16.88	76.08	17.21	78
79	77.27	16.43	77.20	16.76	77.13	17.10	77.05	17.44	79
80	78.25	16.63	78.18	16.97	78.10	17.32	78.03	17.66	80
81	79.23	16.84	79.16	17.19	79.08	17.53	79.00	17.88	81
82	80.21	17.05	80.13	17.40	80.06	17.75	79.98	18.10	82
83	81.19	17.26	81.11	17.61	81.03	17.96	80.95	18.32	83
84	82.16	17.46	82.09	17.82	82.01	18.18	81.93	18.54	84
85	83.14	17.67	83.06	18.04	82.99	18.40	82.90	18.76	85
86	84.12	17.88	84.04	18.25	83.96	18.61	83.88	18.98	86
87	85.10	18.09	85.02	18.46	84.94	18.83	84.85	19.20	87
88	86.08	18.30	86.00	18.67	85.91	19.05	85.83	19.42	88
89	87.06	18.50	86.97	18.88	86.89	19.26	86.81	19.64	89
90	88.03	18.71	87.95	19.10	87.87	19.48	87.78	19.86	90
91	89.01	18.92	88.93	19.31	88.84	19.70	88.76	20.08	91
92	89.99	19.13	89.91	19.52	89.82	19.91	89.73	20.30	92
93	90.97	19.34	90.88	19.73	90.80	20.13	90.71	20.52	93
94	91.95	19.54	91.86	19.94	91.77	20.35	91.68	20.75	94
95	92.92	19.75	92.84	20.16	92.75	20.56	92.66	20.97	95
96	93.90	19.96	93.81	20.37	93.72	20.78	93.63	21.19	96
97	94.88	20.17	94.79	20.58	94.70	20.99	94.61	21.41	97
98	95.86	20.38	95.77	20.79	95.68	21.21	95.58	21.63	98
99	96.84	20.58	96.75	21.01	96.65	21.43	96.56	21.85	99
100	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	78 Deg.		77 $\frac{3}{4}$ Deg		77 $\frac{1}{2}$ Deg.		77 $\frac{1}{4}$ Deg.		

TRAVERSE TABLE.

Distance.	13 Deg.		13 $\frac{1}{4}$ Deg.		13 $\frac{1}{2}$ Deg.		13 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.97	0.23	0.97	0.23	0.97	0.23	0.97	0.24	1
2	1.95	0.45	1.95	0.46	1.95	0.47	1.94	0.48	2
3	2.92	0.67	2.92	0.69	2.92	0.70	2.91	0.71	3
4	3.90	0.90	3.89	0.92	3.89	0.93	3.89	0.95	4
5	4.87	1.12	4.87	1.15	4.86	1.17	4.86	1.19	5
6	5.85	1.35	5.84	1.38	5.83	1.40	5.83	1.43	6
7	6.82	1.57	6.81	1.60	6.81	1.63	6.80	1.66	7
8	7.80	1.80	7.79	1.83	7.78	1.87	7.77	1.90	8
9	8.77	2.02	8.76	2.06	8.75	2.10	8.74	2.14	9
10	9.74	2.25	9.73	2.29	9.72	2.33	9.71	2.38	10
11	10.72	2.47	10.71	2.52	10.70	2.57	10.68	2.61	11
12	11.69	2.70	11.68	2.75	11.67	2.80	11.66	2.85	12
13	12.67	2.92	12.65	2.98	12.64	3.03	12.63	3.09	13
14	13.64	3.15	13.63	3.21	13.61	3.27	13.60	3.33	14
15	14.62	3.37	14.60	3.44	14.59	3.50	14.57	3.57	15
16	15.59	3.60	15.57	3.67	15.56	3.74	15.54	3.80	16
17	16.57	3.82	16.55	3.90	16.53	3.97	16.51	4.04	17
18	17.54	4.05	17.52	4.13	17.50	4.20	17.48	4.28	18
19	18.51	4.27	18.49	4.35	18.48	4.44	18.46	4.52	19
20	19.49	4.50	19.47	4.58	19.45	4.67	19.43	4.75	20
21	20.46	4.72	20.44	4.81	20.42	4.90	20.40	4.99	21
22	21.44	4.95	21.41	5.04	21.39	5.14	21.37	5.23	22
23	22.41	5.17	22.39	5.27	22.36	5.37	22.34	5.47	23
24	23.38	5.40	23.36	5.50	23.34	5.60	23.31	5.70	24
25	24.36	5.62	24.33	5.73	24.31	5.84	24.28	5.94	25
26	25.33	5.85	25.31	5.96	25.28	6.07	25.25	6.18	26
27	26.31	6.07	26.28	6.19	26.25	6.30	26.23	6.42	27
28	27.28	6.30	27.25	6.42	27.23	6.54	27.20	6.66	28
29	28.26	6.52	28.23	6.65	28.20	6.77	28.17	6.89	29
30	29.23	6.75	29.20	6.88	29.17	7.00	29.14	7.13	30
31	30.21	6.97	30.17	7.11	30.14	7.24	30.11	7.37	31
32	31.18	7.20	31.15	7.33	31.12	7.47	31.08	7.61	32
33	32.15	7.42	32.12	7.56	32.09	7.70	32.05	7.84	33
34	33.13	7.65	33.09	7.79	33.06	7.94	33.03	8.08	34
35	34.10	7.87	34.07	8.02	34.03	8.17	34.00	8.32	35
36	35.08	8.10	35.04	8.25	35.01	8.40	34.97	8.56	36
37	36.05	8.32	36.02	8.48	35.98	8.64	35.94	8.79	37
38	37.03	8.55	36.99	8.71	36.95	8.87	36.91	9.03	38
39	38.00	8.77	37.96	8.94	37.92	9.10	37.88	9.27	39
40	38.97	9.00	38.94	9.17	38.89	9.34	38.85	9.51	40
41	39.95	9.22	39.91	9.40	39.87	9.57	39.83	9.75	41
42	40.92	9.45	40.88	9.63	40.84	9.80	40.80	9.98	42
43	41.90	9.67	41.86	9.86	41.81	10.04	41.77	10.22	43
44	42.87	9.90	42.83	10.08	42.78	10.27	42.74	10.46	44
45	43.85	10.12	43.80	10.31	43.76	10.51	43.71	10.70	45
46	44.82	10.35	44.78	10.54	44.73	10.74	44.68	10.93	46
47	45.80	10.57	45.75	10.77	45.70	10.97	45.65	11.17	47
48	46.77	10.80	46.72	11.00	46.67	11.21	46.62	11.41	48
49	47.74	11.02	47.70	11.23	47.65	11.44	47.60	11.65	49
50	48.72	11.25	48.67	11.46	48.62	11.67	48.57	11.88	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	77 Deg.		76 $\frac{3}{4}$ Deg.		76 $\frac{1}{2}$ Deg.		76 $\frac{1}{4}$ Deg.		

Distance.	13 Deg.		13 $\frac{1}{4}$ Deg.		13 $\frac{1}{2}$ Deg.		13 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.69	11.47	49.64	11.69	49.59	11.91	49.54	12.12	51
52	50.67	11.70	50.62	11.92	50.56	12.14	50.51	12.36	52
53	51.64	11.92	51.59	12.15	51.54	12.37	51.48	12.60	53
54	52.62	12.15	52.56	12.38	52.51	12.61	52.45	12.84	54
55	53.59	12.37	53.54	12.61	53.48	12.84	53.42	13.07	55
56	54.56	12.60	54.51	12.84	54.45	13.07	54.40	13.31	56
57	55.54	12.82	55.48	13.06	55.43	13.31	55.37	13.55	57
58	56.51	13.05	56.46	13.29	56.40	13.54	56.34	13.79	58
59	57.49	13.27	57.43	13.52	57.37	13.77	57.31	14.02	59
60	58.46	13.50	58.40	13.75	58.34	14.01	58.28	14.26	60
61	59.44	13.72	59.38	13.98	59.31	14.24	59.25	14.50	61
62	60.41	13.95	60.35	14.21	60.29	14.47	60.22	14.74	62
63	61.39	14.17	61.32	14.44	61.26	14.71	61.19	14.97	63
64	62.36	14.40	62.30	14.67	62.23	14.94	62.17	15.21	64
65	63.33	14.62	63.27	14.90	63.20	15.17	63.14	15.45	65
66	64.31	14.85	64.24	15.13	64.18	15.41	64.11	15.69	66
67	65.28	15.07	65.22	15.36	65.15	15.64	65.08	15.93	67
68	66.26	15.30	66.19	15.59	66.12	15.87	66.05	16.16	68
69	67.23	15.52	67.16	15.81	67.09	16.11	67.02	16.40	69
70	68.21	15.75	68.14	16.04	68.07	16.34	67.99	16.64	70
71	69.18	15.97	69.11	16.27	69.04	16.57	68.97	16.88	71
72	70.15	16.20	70.08	16.50	70.01	16.81	69.94	17.11	72
73	71.13	16.42	71.06	16.73	70.98	17.04	70.91	17.35	73
74	72.10	16.65	72.03	16.96	71.96	17.28	71.88	17.59	74
75	73.08	16.87	73.00	17.19	72.93	17.50	72.85	17.83	75
76	74.05	17.10	73.98	17.42	73.90	17.74	73.82	18.06	76
77	75.03	17.32	74.95	17.65	74.87	17.98	74.79	18.30	77
78	76.00	17.55	75.92	17.88	75.84	18.21	75.76	18.54	78
79	76.98	17.77	76.90	18.11	76.82	18.44	76.74	18.78	79
80	77.95	18.00	77.87	18.34	77.79	18.68	77.71	19.01	80
81	78.92	18.22	78.84	18.57	78.76	18.91	78.68	19.25	81
82	79.90	18.45	79.82	18.79	79.73	19.14	79.65	19.49	82
83	80.87	18.67	80.79	19.02	80.71	19.38	80.62	19.73	83
84	81.85	18.90	81.76	19.25	81.68	19.61	81.59	19.97	84
85	82.82	19.12	82.74	19.48	82.65	19.84	82.56	20.20	85
86	83.80	19.35	83.71	19.71	83.62	20.08	83.54	20.44	86
87	84.77	19.57	84.68	19.94	84.60	20.31	84.51	20.68	87
88	85.74	19.80	85.66	20.17	85.57	20.54	85.48	20.92	88
89	86.72	20.02	86.63	20.40	86.54	20.78	86.45	21.15	89
90	87.69	20.25	87.60	20.63	87.51	21.01	87.42	21.39	90
91	88.67	20.47	88.58	20.86	88.49	21.24	88.39	21.63	91
92	89.64	20.70	89.55	21.09	89.46	21.48	89.36	21.87	92
93	90.62	20.92	90.52	21.32	90.43	21.71	90.33	22.10	93
94	91.59	21.15	91.50	21.54	91.40	21.94	91.31	22.34	94
95	92.57	21.37	92.47	21.77	92.38	22.18	92.28	22.58	95
96	93.54	21.60	93.44	22.00	93.35	22.41	93.25	22.82	96
97	94.51	21.82	94.42	22.23	94.32	22.64	94.22	23.06	97
98	95.49	22.05	95.39	22.46	95.29	22.88	95.19	23.29	98
99	96.46	22.27	96.36	22.69	96.26	23.11	96.16	23.53	99
100	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	77 Deg.		76 $\frac{3}{4}$ Deg.		76 $\frac{1}{2}$ Deg.		76 $\frac{1}{4}$ Deg.		

Distance.	14 Deg.		14 $\frac{1}{4}$ Deg.		14 $\frac{1}{2}$ Deg.		14 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.97	0.24	0.97	0.25	0.97	0.25	0.97	0.25	1
2	1.94	0.48	1.94	0.49	1.94	0.50	1.93	0.51	2
3	2.91	0.73	2.91	0.74	2.90	0.75	2.90	0.76	3
4	3.88	0.97	3.88	0.98	3.87	1.00	3.87	1.02	4
5	4.85	1.21	4.85	1.23	4.84	1.25	4.84	1.27	5
6	5.82	1.45	5.82	1.48	5.81	1.50	5.80	1.53	6
7	6.79	1.69	6.78	1.72	6.78	1.75	6.77	1.78	7
8	7.76	1.94	7.75	1.97	7.75	2.00	7.74	2.04	8
9	8.73	2.18	8.72	2.22	8.71	2.25	8.70	2.29	9
10	9.70	2.42	9.69	2.46	9.68	2.50	9.67	2.55	10
11	10.67	2.66	10.66	2.71	10.65	2.75	10.64	2.80	11
12	11.64	2.90	11.63	2.95	11.62	3.00	11.60	3.06	12
13	12.61	3.15	12.60	3.20	12.59	3.25	12.57	3.31	13
14	13.58	3.39	13.57	3.45	13.55	3.51	13.54	3.56	14
15	14.55	3.63	14.54	3.69	14.52	3.76	14.51	3.82	15
16	15.52	3.87	15.51	3.94	15.49	4.01	15.47	4.07	16
17	16.50	4.11	16.48	4.18	16.46	4.26	16.44	4.33	17
18	17.47	4.35	17.45	4.43	17.43	4.51	17.41	4.58	18
19	18.44	4.60	18.42	4.68	18.39	4.76	18.37	4.84	19
20	19.41	4.84	19.38	4.92	19.36	5.01	19.34	5.09	20
21	20.38	5.08	20.35	5.17	20.33	5.26	20.31	5.35	21
22	21.35	5.32	21.32	5.42	21.30	5.51	21.28	5.60	22
23	22.32	5.56	22.29	5.66	22.27	5.76	22.24	5.86	23
24	23.29	5.81	23.26	5.91	23.24	6.01	23.21	6.11	24
25	24.26	6.05	24.23	6.15	24.20	6.26	24.18	6.37	25
26	25.23	6.29	25.20	6.40	25.17	6.51	25.14	6.62	26
27	26.20	6.53	26.17	6.65	26.14	6.76	26.11	6.87	27
28	27.17	6.77	27.14	6.89	27.11	7.01	27.08	7.13	28
29	28.14	7.02	28.11	7.14	28.08	7.26	28.04	7.38	29
30	29.11	7.26	29.08	7.38	29.04	7.51	29.01	7.64	30
31	30.08	7.50	30.05	7.63	30.01	7.76	29.98	7.89	31
32	31.05	7.74	31.02	7.88	30.98	8.01	30.95	8.15	32
33	32.02	7.98	31.98	8.12	31.95	8.26	31.91	8.40	33
34	32.99	8.23	32.95	8.37	32.92	8.51	32.88	8.66	34
35	33.96	8.47	33.92	8.62	33.89	8.76	33.85	8.91	35
36	34.93	8.71	34.89	8.86	34.85	9.01	34.81	9.17	36
37	35.90	8.95	35.86	9.11	35.82	9.26	35.78	9.42	37
38	36.87	9.19	36.83	9.35	36.79	9.51	36.75	9.67	38
39	37.84	9.44	37.80	9.60	37.76	9.76	37.71	9.93	39
40	38.81	9.68	38.77	9.85	38.73	10.02	38.68	10.18	40
41	39.78	9.92	39.74	10.09	39.69	10.27	39.65	10.44	41
42	40.75	10.16	40.71	10.34	40.66	10.52	40.62	10.69	42
43	41.72	10.40	41.68	10.58	41.63	10.77	41.58	10.95	43
44	42.69	10.64	42.65	10.83	42.60	11.02	42.55	11.20	44
45	43.66	10.89	43.62	11.08	43.57	11.27	43.52	11.46	45
46	44.63	11.13	44.58	11.32	44.53	11.52	44.48	11.71	46
47	45.60	11.37	45.55	11.57	45.50	11.77	45.45	11.97	47
48	46.57	11.61	46.52	11.82	46.47	12.02	46.42	12.22	48
49	47.54	11.85	47.49	12.06	47.44	12.27	47.39	12.48	49
50	48.51	12.10	48.46	12.31	48.41	12.52	48.35	12.73	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	76 Deg.		75 $\frac{3}{4}$ Deg.		75 $\frac{1}{2}$ Deg.		75 $\frac{1}{4}$ Deg.		



Distance.	14 Deg.		14 $\frac{1}{4}$ Deg.		14 $\frac{1}{2}$ Deg.		14 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.49	12.34	49.43	12.55	49.38	12.77	49.32	12.98	51
52	50.46	12.58	50.40	12.80	50.34	13.02	50.29	13.24	52
53	51.43	12.82	51.37	13.05	51.31	13.27	51.25	13.49	53
54	52.40	13.06	52.34	13.29	52.28	13.52	52.22	13.75	54
55	53.37	13.31	53.31	13.54	53.25	13.77	53.19	14.00	55
56	54.34	13.55	54.28	13.78	54.22	14.02	54.15	14.26	56
57	55.31	13.79	55.25	14.03	55.18	14.27	55.12	14.51	57
58	56.28	14.03	56.22	14.28	56.15	14.52	56.09	14.77	58
59	57.25	14.27	57.18	14.52	57.12	14.77	57.06	15.02	59
60	58.22	14.52	58.15	14.77	58.09	15.02	58.02	15.28	60
61	59.19	14.76	59.12	15.02	59.06	15.27	58.99	15.53	61
62	60.16	15.00	60.09	15.26	60.03	15.52	59.96	15.79	62
63	61.13	15.24	61.06	15.51	60.99	15.77	60.92	16.04	63
64	62.10	15.48	62.03	15.75	61.96	16.02	61.89	16.29	64
65	63.07	15.72	63.00	16.00	62.93	16.27	62.86	16.55	65
66	64.04	15.97	63.97	16.25	63.90	16.53	63.83	16.80	66
67	65.01	16.21	64.94	16.49	64.87	16.78	64.79	17.06	67
68	65.98	16.45	65.91	16.74	65.83	17.03	65.76	17.31	68
69	66.95	16.69	66.88	16.98	66.80	17.28	66.73	17.57	69
70	67.92	16.93	67.85	17.23	67.77	17.53	67.69	17.82	70
71	68.89	17.18	68.82	17.48	68.74	17.78	68.66	18.08	71
72	69.86	17.42	69.78	17.72	69.71	18.03	69.63	18.33	72
73	70.83	17.66	70.75	17.97	70.67	18.28	70.59	18.59	73
74	71.80	17.90	71.72	18.22	71.64	18.53	71.56	18.84	74
75	72.77	18.14	72.69	18.46	72.61	18.78	72.53	19.10	75
76	73.74	18.39	73.66	18.71	73.58	19.03	73.50	19.35	76
77	74.71	18.63	74.63	18.95	74.55	19.28	74.46	19.60	77
78	75.68	18.87	75.60	19.20	75.52	19.53	75.43	19.86	78
79	76.65	19.11	76.57	19.45	76.48	19.78	76.40	20.11	79
80	77.62	19.35	77.54	19.69	77.45	20.03	77.36	20.37	80
81	78.59	19.60	78.51	19.94	78.42	20.28	78.33	20.62	81
82	79.56	19.84	79.48	20.18	79.39	20.53	79.30	20.88	82
83	80.53	20.08	80.45	20.43	80.36	20.78	80.26	21.13	83
84	81.50	20.32	81.42	20.68	81.32	21.03	81.23	21.39	84
85	82.48	20.56	82.38	20.92	82.29	21.28	82.20	21.64	85
86	83.45	20.81	83.35	21.17	83.26	21.53	83.17	21.90	86
87	84.42	21.05	84.32	21.42	84.23	21.78	84.13	22.15	87
88	85.39	21.29	85.29	21.66	85.20	22.03	85.10	22.41	88
89	86.36	21.53	86.26	21.91	86.17	22.28	86.07	22.66	89
90	87.33	21.77	87.23	22.15	87.13	22.53	87.03	22.91	90
91	88.30	22.01	88.20	22.40	88.10	22.78	88.00	23.17	91
92	89.27	22.26	89.17	22.65	89.07	23.04	88.97	23.42	92
93	90.24	22.50	90.14	22.89	90.04	23.29	89.94	23.68	93
94	91.21	22.74	91.11	23.14	91.01	23.54	90.90	23.93	94
95	92.18	22.98	92.08	23.38	91.97	23.79	91.87	24.19	95
96	93.15	23.22	93.05	23.63	92.94	24.04	92.84	24.44	96
97	94.12	23.47	94.02	23.88	93.91	24.29	93.80	24.70	97
98	95.09	23.71	94.98	24.12	94.88	24.54	94.77	24.95	98
99	96.06	23.95	95.95	24.37	95.85	24.79	95.74	25.21	99
100	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	76 Deg.		75 $\frac{3}{4}$ Deg		75 $\frac{1}{2}$ Deg.		75 $\frac{1}{4}$ Deg		

TRAVERSE TABLE.

Distance.	15 Deg.		15½ Deg.		15¾ Deg.		15¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.97	0.26	0.96	0.26	0.96	0.27	0.96	0.27	1
2	1.93	0.52	1.93	0.53	1.93	0.53	1.92	0.54	2
3	2.90	0.78	2.89	0.79	2.89	0.80	2.89	0.81	3
4	3.86	1.04	3.86	1.05	3.85	1.07	3.85	1.09	4
5	4.83	1.29	4.82	1.32	4.82	1.34	4.81	1.36	5
6	5.80	1.55	5.79	1.58	5.78	1.60	5.77	1.63	6
7	6.76	1.81	6.75	1.84	6.75	1.87	6.74	1.90	7
8	7.73	2.07	7.72	2.10	7.71	2.14	7.70	2.17	8
9	8.69	2.33	8.68	2.37	8.67	2.41	8.66	2.44	9
10	9.66	2.59	9.65	2.63	9.64	2.67	9.62	2.71	10
11	10.63	2.85	10.61	2.89	10.60	2.94	10.59	2.99	11
12	11.59	3.11	11.58	3.16	11.56	3.21	11.55	3.26	12
13	12.56	3.36	12.54	3.42	12.53	3.47	12.51	3.53	13
14	13.52	3.62	13.51	3.68	13.49	3.74	13.47	3.80	14
15	14.49	3.88	14.47	3.95	14.45	4.01	14.44	4.07	15
16	15.45	4.14	15.44	4.21	15.42	4.28	15.40	4.34	16
17	16.42	4.40	16.40	4.47	16.38	4.54	16.36	4.61	17
18	17.39	4.66	17.37	4.73	17.35	4.81	17.32	4.89	18
19	18.35	4.92	18.33	5.00	18.31	5.08	18.29	5.16	19
20	19.32	5.18	19.30	5.26	19.27	5.34	19.25	5.43	20
21	20.28	5.44	20.26	5.52	20.24	5.61	20.21	5.70	21
22	21.25	5.69	21.23	5.79	21.20	5.88	21.17	5.97	22
23	22.22	5.95	22.19	6.05	22.16	6.15	22.14	6.24	23
24	23.18	6.21	23.15	6.31	23.13	6.41	23.10	6.51	24
25	24.15	6.47	24.12	6.58	24.09	6.68	24.06	6.79	25
26	25.11	6.73	25.08	6.84	25.05	6.95	25.02	7.06	26
27	26.08	6.99	26.05	7.10	26.02	7.22	25.99	7.33	27
28	27.05	7.25	27.01	7.36	26.98	7.48	26.95	7.60	28
29	28.01	7.51	27.98	7.63	27.95	7.75	27.91	7.87	29
30	28.98	7.76	28.94	7.89	28.91	8.02	28.87	8.14	30
31	29.94	8.02	29.91	8.15	29.87	8.28	29.84	8.41	31
32	30.91	8.28	30.87	8.42	30.84	8.55	30.80	8.69	32
33	31.88	8.54	31.84	8.68	31.80	8.82	31.76	8.96	33
34	32.84	8.80	32.80	8.94	32.76	9.09	32.72	9.23	34
35	33.81	9.06	33.77	9.21	33.73	9.35	33.69	9.50	35
36	34.77	9.32	34.73	9.47	34.69	9.62	34.65	9.77	36
37	35.74	9.58	35.70	9.73	35.65	9.89	35.61	10.04	37
38	36.71	9.84	36.66	10.00	36.62	10.16	36.57	10.31	38
39	37.67	10.09	37.63	10.26	37.58	10.42	37.54	10.59	39
40	38.64	10.35	38.59	10.52	38.55	10.69	38.50	10.86	40
41	39.60	10.61	39.56	10.78	39.51	10.96	39.46	11.13	41
42	40.57	10.87	40.52	11.05	40.47	11.22	40.42	11.40	42
43	41.53	11.13	41.49	11.31	41.44	11.49	41.39	11.67	43
44	42.50	11.39	42.45	11.57	42.40	11.76	42.35	11.94	44
45	43.47	11.65	43.42	11.84	43.36	12.03	43.31	12.21	45
46	44.43	11.91	44.38	12.10	44.33	12.29	44.27	12.49	46
47	45.40	12.16	45.35	12.36	45.29	12.56	45.24	12.76	47
48	46.36	12.42	46.31	12.63	46.25	12.83	46.20	13.03	48
49	47.33	12.68	47.27	12.89	47.22	13.09	47.16	13.30	49
50	48.30	12.94	48.24	13.15	48.18	13.36	48.12	13.57	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	75 Deg.		74½ Deg.		74¼ Deg.		74¼ Deg.		

Distance.	15 Deg.		15½ Deg.		15½ Deg.		15¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.26	13.20	49.20	13.41	49.15	13.63	49.09	13.84	51
52	50.23	13.46	50.17	13.68	50.11	13.90	50.05	14.11	52
53	51.19	13.72	51.13	13.94	51.07	14.16	51.01	14.39	53
54	52.16	13.98	52.10	14.20	52.04	14.43	51.97	14.66	54
55	53.13	14.24	53.06	14.47	53.00	14.70	52.94	14.93	55
56	54.09	14.49	54.03	14.73	53.96	14.97	53.90	15.20	56
57	55.06	14.75	54.99	14.99	54.93	15.23	54.86	15.47	57
58	56.02	15.01	55.96	15.26	55.89	15.50	55.82	15.74	58
59	56.99	15.27	56.92	15.52	56.85	15.77	56.78	16.01	59
60	57.96	15.53	57.89	15.78	57.82	16.03	57.75	16.29	60
61	58.92	15.79	58.85	16.04	58.78	16.30	58.71	16.56	61
62	59.89	16.05	59.82	16.31	59.75	16.57	59.67	16.83	62
63	60.85	16.31	60.78	16.57	60.71	16.84	60.63	17.10	63
64	61.82	16.56	61.75	16.83	61.67	17.10	61.60	17.37	64
65	62.79	16.82	62.71	17.10	62.64	17.37	62.56	17.64	65
66	63.75	17.08	63.68	17.35	63.60	17.64	63.52	17.92	66
67	64.72	17.34	64.64	17.62	64.56	17.90	64.48	18.19	67
68	65.68	17.60	65.61	17.89	65.53	18.17	65.45	18.46	68
69	66.65	17.86	66.57	18.15	66.49	18.44	66.41	18.73	69
70	67.61	18.12	67.54	18.41	67.45	18.71	67.37	19.00	70
71	68.58	18.38	68.50	18.68	68.42	18.97	68.33	19.27	71
72	69.55	18.63	69.46	18.94	69.38	19.24	69.30	19.54	72
73	70.51	18.89	70.43	19.20	70.35	19.51	70.26	19.82	73
74	71.48	19.15	71.39	19.46	71.31	19.78	71.22	20.09	74
75	72.44	19.41	72.36	19.73	72.27	20.04	72.18	20.36	75
76	73.41	19.67	73.32	19.99	73.24	20.31	73.15	20.63	76
77	74.38	19.93	74.29	20.25	74.20	20.58	74.11	20.90	77
78	75.34	20.19	75.25	20.52	75.16	20.84	75.07	21.17	78
79	76.31	20.45	76.22	20.78	76.13	21.11	76.03	21.44	79
80	77.27	20.71	77.18	21.04	77.09	21.38	77.00	21.72	80
81	78.24	20.96	78.15	21.31	78.05	21.65	77.96	21.99	81
82	79.21	21.22	79.11	21.57	79.02	21.91	78.92	22.26	82
83	80.17	21.48	80.08	21.83	79.98	22.18	79.88	22.53	83
84	81.14	21.74	81.04	22.09	80.94	22.45	80.85	22.80	84
85	82.10	22.00	82.01	22.36	81.91	22.72	81.81	23.07	85
86	83.07	22.26	82.97	22.62	82.87	22.98	82.77	23.34	86
87	84.04	22.52	83.94	22.88	83.84	23.25	83.73	23.62	87
88	85.00	22.78	84.90	23.15	84.80	23.52	84.70	23.89	88
89	85.97	23.03	85.87	23.41	85.76	23.78	85.66	24.16	89
90	86.93	23.29	86.83	23.67	86.73	24.05	86.62	24.43	90
91	87.90	23.55	87.80	23.94	87.69	24.32	87.58	24.70	91
92	88.87	23.81	88.76	24.20	88.65	24.59	88.55	24.97	92
93	89.83	24.07	89.73	24.46	89.62	24.85	89.51	25.24	93
94	90.80	24.33	90.69	24.72	90.58	25.12	90.47	25.52	94
95	91.76	24.59	91.65	24.99	91.54	25.39	91.43	25.79	95
96	92.73	24.85	92.62	25.25	92.51	25.65	92.40	26.06	96
97	93.69	25.11	93.58	25.51	93.47	25.92	93.36	26.33	97
98	94.66	25.36	94.55	25.78	94.44	26.19	94.32	26.60	98
99	95.63	25.62	95.51	26.04	95.40	26.46	95.28	26.87	99
100	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	75 Deg.		74¾ Deg.		74½ Deg.		74¼ Deg.		

Distance.	16 Deg.		16¼ Deg.		16½ Deg.		16¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.96	0.28	0.96	0.28	0.96	0.28	0.96	0.29	1
2	1.92	0.55	1.92	0.56	1.92	0.57	1.92	0.58	2
3	2.88	0.83	2.88	0.84	2.88	0.85	2.87	0.86	3
4	3.85	1.10	3.84	1.12	3.84	1.14	3.83	1.15	4
5	4.81	1.38	4.80	1.40	4.79	1.42	4.79	1.44	5
6	5.77	1.65	5.76	1.68	5.75	1.70	5.75	1.73	6
7	6.73	1.93	6.72	1.96	6.71	1.99	6.70	2.02	7
8	7.69	2.21	7.68	2.24	7.67	2.27	7.66	2.31	8
9	8.65	2.48	8.64	2.52	8.63	2.56	8.62	2.59	9
10	9.61	2.76	9.60	2.80	9.59	2.84	9.58	2.88	10
11	10.57	3.03	10.56	3.08	10.55	3.12	10.53	3.17	11
12	11.54	3.31	11.52	3.36	11.51	3.41	11.49	3.46	12
13	12.50	3.58	12.48	3.64	12.46	3.69	12.45	3.75	13
14	13.46	3.86	13.44	3.92	13.42	3.98	13.41	4.03	14
15	14.42	4.13	14.40	4.20	14.38	4.26	14.36	4.32	15
16	15.38	4.41	15.36	4.48	15.34	4.54	15.32	4.61	16
17	16.34	4.69	16.32	4.76	16.30	4.83	16.28	4.90	17
18	17.30	4.96	17.28	5.04	17.26	5.11	17.24	5.19	18
19	18.26	5.24	18.24	5.32	18.22	5.40	18.19	5.48	19
20	19.23	5.51	19.20	5.60	19.18	5.68	19.15	5.76	20
21	20.19	5.79	20.16	5.88	20.14	5.96	20.11	6.05	21
22	21.15	6.06	21.12	6.16	21.09	6.25	21.07	6.34	22
23	22.11	6.34	22.08	6.44	22.05	6.53	22.02	6.63	23
24	23.07	6.62	23.04	6.72	23.01	6.82	22.98	6.92	24
25	24.03	6.89	24.00	7.00	23.97	7.10	23.94	7.20	25
26	24.99	7.17	24.96	7.28	24.93	7.38	24.90	7.49	26
27	25.95	7.44	25.92	7.56	25.89	7.67	25.85	7.78	27
28	26.92	7.72	26.88	7.84	26.85	7.95	26.81	8.07	28
29	27.88	7.99	27.84	8.11	27.81	8.24	27.77	8.36	29
30	28.84	8.27	28.80	8.39	28.76	8.52	28.73	8.65	30
31	29.80	8.54	29.76	8.67	29.72	8.80	29.68	8.93	31
32	30.76	8.82	30.72	8.95	30.68	9.09	30.64	9.22	32
33	31.72	9.10	31.68	9.23	31.64	9.37	31.60	9.51	33
34	32.68	9.37	32.64	9.51	32.60	9.66	32.56	9.80	34
35	33.64	9.65	33.60	9.79	33.56	9.94	33.51	10.09	35
36	34.61	9.92	34.56	10.07	34.52	10.22	34.47	10.38	36
37	35.57	10.20	35.52	10.35	35.48	10.51	35.43	10.66	37
38	36.53	10.47	36.48	10.63	36.44	10.79	36.39	10.95	38
39	37.49	10.75	37.44	10.91	37.39	11.08	37.35	11.24	39
40	38.45	11.03	38.40	11.19	38.35	11.36	38.30	11.53	40
41	39.41	11.30	39.36	11.47	39.31	11.64	39.26	11.82	41
42	40.37	11.58	40.32	11.75	40.27	11.93	40.22	12.10	42
43	41.33	11.85	41.28	12.03	41.23	12.21	41.18	12.39	43
44	42.30	12.13	42.24	12.31	42.19	12.50	42.13	12.68	44
45	43.26	12.40	43.20	12.59	43.15	12.78	43.09	12.97	45
46	44.22	12.68	44.16	12.87	44.11	13.06	44.05	13.26	46
47	45.18	12.95	45.12	13.15	45.06	13.35	45.01	13.55	47
48	46.14	13.23	46.08	13.43	46.02	13.63	45.96	13.83	48
49	47.10	13.51	47.04	13.71	46.98	13.92	46.92	14.12	49
50	48.06	13.78	48.00	13.99	47.94	14.20	47.88	14.41	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	74 Deg.		73¾ Deg.		73½ Deg.		73¼ Deg.		

Distance.	16 Deg.		16 $\frac{1}{4}$ Deg.		16 $\frac{1}{2}$ Deg.		16 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.62	14.06	48.96	14.27	48.90	14.48	48.84	14.70	51
52	49.99	14.33	49.92	14.55	49.86	14.77	49.79	14.99	52
53	50.95	14.61	50.88	14.83	50.82	15.05	50.75	15.27	53
54	51.91	14.88	51.84	15.11	51.78	15.34	51.71	15.56	54
55	52.87	15.16	52.80	15.39	52.74	15.62	52.67	15.85	55
56	53.83	15.44	53.76	15.67	53.69	15.90	53.62	16.14	56
57	54.79	15.71	54.72	15.95	54.65	16.19	54.58	16.43	57
58	55.75	15.99	55.68	16.23	55.61	16.47	55.54	16.72	58
59	56.71	16.26	56.64	16.51	56.57	16.76	56.50	17.00	59
60	57.68	16.54	57.60	16.79	57.53	17.04	57.45	17.29	60
61	58.64	16.81	58.56	17.07	58.49	17.32	58.41	17.58	61
62	59.60	17.09	59.52	17.35	59.45	17.61	59.37	17.87	62
63	60.56	17.37	60.48	17.63	60.41	17.89	60.33	18.16	63
64	61.52	17.64	61.44	17.91	61.36	18.18	61.28	18.44	64
65	62.48	17.92	62.40	18.19	62.32	18.46	62.24	18.73	65
66	63.44	18.19	63.36	18.47	63.28	18.74	63.20	19.02	66
67	64.40	18.47	64.32	18.75	64.24	19.03	64.16	19.31	67
68	65.37	18.74	65.28	19.03	65.20	19.31	65.11	19.60	68
69	66.33	19.02	66.24	19.31	66.16	19.60	66.07	19.89	69
70	67.29	19.29	67.20	19.59	67.12	19.88	67.03	20.17	70
71	68.25	19.57	68.16	19.87	68.08	20.17	67.99	20.46	71
72	69.21	19.85	69.12	20.15	69.03	20.45	68.95	20.75	72
73	70.17	20.12	70.08	20.43	69.99	20.73	69.90	21.04	73
74	71.13	20.40	71.04	20.71	70.95	21.02	70.86	21.33	74
75	72.09	20.67	72.00	20.99	71.91	21.30	71.82	21.61	75
76	73.06	20.95	72.96	21.27	72.87	21.59	72.78	21.90	76
77	74.02	21.22	73.92	21.55	73.83	21.87	73.73	22.19	77
78	74.98	21.50	74.88	21.83	74.79	22.15	74.69	22.48	78
79	75.94	21.78	75.84	22.11	75.75	22.44	75.65	22.77	79
80	76.90	22.05	76.80	22.39	76.71	22.72	76.61	23.06	80
81	77.86	22.33	77.76	22.67	77.66	23.01	77.56	23.34	81
82	78.82	22.60	78.72	22.95	78.62	23.29	78.52	23.63	82
83	79.78	22.88	79.68	23.23	79.58	23.57	79.48	23.92	83
84	80.75	23.15	80.64	23.51	80.54	23.86	80.44	24.21	84
85	81.71	23.43	81.60	23.79	81.50	24.14	81.39	24.50	85
86	82.67	23.70	82.56	24.07	82.46	24.43	82.35	24.78	86
87	83.63	23.98	83.52	24.35	83.42	24.71	83.31	25.07	87
88	84.59	24.26	84.48	24.62	84.38	24.99	84.27	25.36	88
89	85.55	24.53	85.44	24.90	85.33	25.28	85.22	25.65	89
90	86.51	24.81	86.40	25.18	86.29	25.56	86.18	25.94	90
91	87.47	25.08	87.36	25.46	87.25	25.85	87.14	26.23	91
92	88.44	25.36	88.32	25.74	88.21	26.13	88.10	26.51	92
93	89.40	25.63	89.28	26.02	89.17	26.41	89.05	26.80	93
94	90.36	25.91	90.24	26.30	90.13	26.70	90.01	27.09	94
95	91.32	26.19	91.20	26.58	91.09	26.98	90.97	27.38	95
96	92.28	26.46	92.16	26.86	92.05	27.27	91.93	27.67	96
97	93.24	26.74	93.12	27.14	93.01	27.55	92.88	27.95	97
98	94.20	27.01	94.08	27.42	93.96	27.83	93.84	28.24	98
99	95.16	27.29	95.04	27.70	94.92	28.12	94.80	28.53	99
100	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	74 Deg.		73 $\frac{3}{4}$ Deg.		73 $\frac{1}{2}$ Deg.		73 $\frac{1}{4}$ Deg.		

Distance.	17 Deg.		17¼ Deg.		17½ Deg.		17¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.96	0.29	0.95	0.30	0.95	0.30	0.95	0.30	1
2	1.91	0.58	1.91	0.59	1.91	0.60	1.90	0.61	2
3	2.87	0.88	2.87	0.89	2.86	0.90	2.86	0.91	3
4	3.83	1.17	3.82	1.19	3.81	1.20	3.81	1.22	4
5	4.78	1.46	4.78	1.48	4.77	1.50	4.76	1.52	5
6	5.74	1.75	5.73	1.78	5.72	1.80	5.71	1.83	6
7	6.69	2.05	6.69	2.08	6.68	2.10	6.67	2.13	7
8	7.65	2.34	7.64	2.37	7.63	2.41	7.62	2.44	8
9	8.61	2.63	8.60	2.67	8.58	2.71	8.57	2.74	9
10	9.56	2.92	9.55	2.97	9.54	3.01	9.52	3.05	10
11	10.52	3.22	10.51	3.26	10.49	3.31	10.48	3.35	11
12	11.48	3.51	11.46	3.56	11.44	3.61	11.43	3.66	12
13	12.43	3.80	12.42	3.85	12.40	3.91	12.38	3.96	13
14	13.39	4.09	13.37	4.15	13.35	4.21	13.33	4.27	14
15	14.34	4.39	14.33	4.45	14.31	4.51	14.29	4.57	15
16	15.30	4.68	15.28	4.74	15.26	4.81	15.24	4.88	16
17	16.26	4.97	16.24	5.04	16.21	5.11	16.19	5.18	17
18	17.21	5.26	17.19	5.34	17.17	5.41	17.14	5.49	18
19	18.17	5.56	18.15	5.63	18.12	5.71	18.10	5.79	19
20	19.13	5.85	19.10	5.93	19.07	6.01	19.05	6.10	20
21	20.08	6.14	20.06	6.23	20.03	6.31	20.00	6.40	21
22	21.04	6.43	21.01	6.52	20.98	6.62	20.95	6.71	22
23	21.99	6.72	21.97	6.82	21.94	6.92	21.91	7.01	23
24	22.95	7.02	22.92	7.12	22.89	7.22	22.86	7.32	24
25	23.91	7.31	23.88	7.41	23.84	7.52	23.81	7.62	25
26	24.86	7.60	24.83	7.71	24.80	7.82	24.76	7.93	26
27	25.82	7.89	25.79	8.01	25.75	8.12	25.71	8.23	27
28	26.78	8.19	26.74	8.30	26.70	8.42	26.67	8.54	28
29	27.73	8.48	27.70	8.60	27.66	8.72	27.62	8.84	29
30	28.69	8.77	28.65	8.90	28.61	9.02	28.57	9.15	30
31	29.65	9.06	29.61	9.19	29.57	9.32	29.52	9.45	31
32	30.60	9.36	30.56	9.49	30.52	9.62	30.48	9.76	32
33	31.56	9.65	31.52	9.79	31.47	9.92	31.43	10.06	33
34	32.51	9.94	32.47	10.08	32.43	10.22	32.38	10.37	34
35	33.47	10.23	33.43	10.38	33.38	10.52	33.33	10.67	35
36	34.43	10.53	34.38	10.68	34.33	10.83	34.29	10.98	36
37	35.38	10.82	35.34	10.97	35.29	11.13	35.24	11.28	37
38	36.34	11.11	36.29	11.27	36.24	11.43	36.19	11.58	38
39	37.30	11.40	37.25	11.57	37.19	11.73	37.14	11.89	39
40	38.25	11.69	38.20	11.86	38.15	12.03	38.10	12.19	40
41	39.21	11.99	39.16	12.16	39.10	12.33	39.05	12.50	41
42	40.16	12.28	40.11	12.45	40.06	12.63	40.00	12.80	42
43	41.12	12.57	41.07	12.75	41.01	12.93	40.95	13.11	43
44	42.08	12.86	42.02	13.05	41.96	13.23	41.91	13.41	44
45	43.03	13.16	42.98	13.34	42.92	13.53	42.86	13.72	45
46	43.99	13.45	43.93	13.64	43.87	13.83	43.81	14.02	46
47	44.95	13.74	44.89	13.94	44.82	14.13	44.76	14.33	47
48	45.90	14.03	45.84	14.23	45.78	14.43	45.71	14.63	48
49	46.86	14.33	46.80	14.53	46.73	14.73	46.67	14.94	49
50	47.82	14.62	47.75	14.83	47.69	15.04	47.62	15.24	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	73 Deg.		72¾ Deg.		72½ Deg.		72¼ Deg.		

Distance.	17 Deg.		17 $\frac{1}{4}$ Deg.		17 $\frac{1}{2}$ Deg.		17 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	48.77	14.91	48.71	15.12	48.64	15.34	48.57	15.55	51
52	49.73	15.20	49.66	15.42	49.59	15.64	49.52	15.85	52
53	50.68	15.50	50.62	15.72	50.55	15.94	50.48	16.16	53
54	51.64	15.79	51.57	16.01	51.50	16.24	51.43	16.46	54
55	52.60	16.08	52.53	16.31	52.45	16.54	52.38	16.77	55
56	53.55	16.37	53.48	16.61	53.41	16.84	53.33	17.07	56
57	54.51	16.67	54.44	16.90	54.36	17.14	54.29	17.38	57
58	55.47	16.96	55.39	17.20	55.32	17.44	55.24	17.68	58
59	56.42	17.25	56.35	17.50	56.27	17.74	56.10	17.99	59
60	57.38	17.54	57.30	17.79	57.22	18.04	57.14	18.29	60
61	58.33	17.83	58.26	18.09	58.18	18.34	58.10	18.60	61
62	59.29	18.13	59.21	18.39	59.13	18.64	59.05	18.90	62
63	60.25	18.42	60.17	18.68	60.08	18.94	60.00	19.21	63
64	61.20	18.71	61.12	18.98	61.04	19.25	60.95	19.51	64
65	62.16	19.00	62.08	19.28	61.99	19.55	61.91	19.82	65
66	63.12	19.30	63.03	19.57	62.95	19.35	62.86	20.12	66
67	64.07	19.59	63.99	19.87	63.90	20.15	63.81	20.43	67
68	65.03	19.88	64.94	20.16	64.85	20.45	64.76	20.73	68
69	65.99	20.17	65.90	20.46	65.81	20.75	65.72	21.04	69
70	66.94	20.47	66.85	20.75	66.76	21.05	66.67	21.34	70
71	67.90	20.76	67.81	21.05	67.71	21.35	67.62	21.65	71
72	68.85	21.05	68.76	21.35	68.67	21.65	68.57	21.95	72
73	69.81	21.34	69.72	21.65	69.62	21.95	69.52	22.26	73
74	70.77	21.64	70.67	21.94	70.58	22.25	70.48	22.56	74
75	71.72	21.93	71.63	22.24	71.53	22.55	71.43	22.86	75
76	72.68	22.22	72.58	22.54	72.48	22.85	72.38	23.17	76
77	73.64	22.51	73.54	22.83	73.44	23.15	73.33	23.47	77
78	74.59	22.80	74.49	23.13	74.39	23.46	74.29	23.78	78
79	75.55	23.10	75.45	23.43	75.34	23.76	75.24	24.08	79
80	76.50	23.39	76.40	23.72	76.30	24.06	76.19	24.39	80
81	77.46	23.68	77.36	24.02	77.25	24.36	77.14	24.69	81
82	78.42	23.97	78.31	24.32	78.20	24.66	78.10	25.00	82
83	79.37	24.27	79.27	24.61	79.16	25.96	79.05	25.30	83
84	80.33	24.56	80.22	24.91	80.11	25.26	80.00	25.61	84
85	81.29	24.85	81.18	25.21	81.07	25.56	80.95	25.91	85
86	82.24	25.14	82.13	25.50	82.02	25.86	81.91	26.22	86
87	83.20	25.44	83.09	25.80	82.97	26.16	82.86	26.52	87
88	84.15	25.73	84.04	26.10	83.93	26.46	83.81	26.83	88
89	85.11	26.02	85.00	26.39	84.88	26.76	84.76	27.13	89
90	86.07	26.31	85.95	26.69	85.83	27.06	85.72	27.44	90
91	87.02	26.61	86.91	26.99	86.79	27.36	86.67	27.74	91
92	87.98	26.90	87.86	27.28	87.74	27.66	87.62	28.05	92
93	88.94	27.19	88.82	27.58	88.70	27.97	88.57	28.35	93
94	89.89	27.48	89.77	27.87	89.65	28.27	89.53	28.66	94
95	90.85	27.78	90.73	28.17	90.60	28.57	90.48	28.96	95
96	91.81	28.07	91.68	28.47	91.56	28.87	91.43	29.27	96
97	92.76	28.36	92.64	28.76	92.51	29.17	92.38	29.57	97
98	93.72	28.65	93.59	29.06	93.46	29.47	93.33	29.88	98
99	94.67	28.94	94.55	29.36	94.42	29.77	94.29	30.18	99
100	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	73 Deg.		72 $\frac{3}{4}$ Deg.		72 $\frac{1}{2}$ Deg.		72 $\frac{1}{4}$ Deg.		

Distance.	18 Deg.		18¼ Deg.		18½ Deg.		18¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.95	0.31	0.95	0.31	0.95	0.32	0.95	0.32	1
2	1.90	0.62	1.90	0.63	1.90	0.63	1.89	0.64	2
3	2.85	0.93	2.85	0.94	2.84	0.95	2.84	0.96	3
4	3.80	1.24	3.80	1.25	3.79	1.27	3.79	1.29	4
5	4.76	1.55	4.75	1.57	4.74	1.59	4.73	1.61	5
6	5.71	1.85	5.70	1.88	5.69	1.90	5.68	1.93	6
7	6.66	2.16	6.65	2.19	6.64	2.22	6.63	2.25	7
8	7.61	2.47	7.60	2.51	7.59	2.54	7.58	2.57	8
9	8.56	2.78	8.55	2.82	8.53	2.86	8.52	2.89	9
10	9.51	3.09	9.50	3.13	9.48	3.17	9.47	3.21	10
11	10.46	3.40	10.45	3.44	10.43	3.49	10.42	3.54	11
12	11.41	3.71	11.40	3.76	11.38	3.81	11.36	3.86	12
13	12.36	4.02	12.35	4.07	12.33	4.12	12.31	4.18	13
14	13.31	4.33	13.30	4.38	13.28	4.44	13.26	4.50	14
15	14.27	4.64	14.25	4.70	14.22	4.76	14.20	4.82	15
16	15.22	4.94	15.20	5.01	15.17	5.08	15.15	5.14	16
17	16.17	5.25	16.14	5.32	16.12	5.39	16.10	5.46	17
18	17.12	5.56	17.09	5.64	17.07	5.71	17.04	5.79	18
19	18.07	5.87	18.04	5.95	18.02	6.03	17.99	6.11	19
20	19.02	6.18	18.99	6.26	18.97	6.35	18.94	6.43	20
21	19.97	6.49	19.94	6.58	19.91	6.66	19.89	6.75	21
22	20.92	6.80	20.89	6.89	20.86	6.98	20.83	7.07	22
23	21.87	7.11	21.84	7.20	21.81	7.30	21.78	7.39	23
24	22.83	7.42	22.79	7.52	22.76	7.62	22.73	7.71	24
25	23.78	7.73	23.74	7.83	23.71	7.93	23.67	8.04	25
26	24.73	8.03	24.69	8.14	24.66	8.25	24.62	8.36	26
27	25.68	8.34	25.64	8.46	25.60	8.57	25.57	8.68	27
28	26.63	8.65	26.59	8.77	26.55	8.88	26.51	9.00	28
29	27.58	8.96	27.54	9.08	27.50	9.20	27.46	9.32	29
30	28.53	9.27	28.49	9.39	28.45	9.52	28.41	9.64	30
31	29.48	9.58	29.44	9.71	29.40	9.84	29.35	9.96	31
32	30.43	9.89	30.39	10.02	30.35	10.15	30.30	10.29	32
33	31.38	10.20	31.34	10.33	31.29	10.47	31.25	10.61	33
34	32.34	10.51	32.29	10.65	32.24	10.79	32.20	10.93	34
35	33.29	10.82	33.24	10.96	33.19	11.11	33.14	11.25	35
36	34.24	11.12	34.19	11.27	34.14	11.42	34.09	11.57	36
37	35.19	11.43	35.14	11.59	35.09	11.74	35.04	11.89	37
38	36.14	11.74	36.09	11.90	36.04	12.06	35.98	12.21	38
39	37.09	12.05	37.04	12.21	36.98	12.37	36.93	12.54	39
40	38.04	12.36	37.99	12.53	37.93	12.69	37.88	12.86	40
41	38.99	12.67	38.94	12.84	38.88	13.01	38.82	13.18	41
42	39.94	12.98	39.89	13.15	39.83	13.33	39.77	13.50	42
43	40.90	13.29	40.84	13.47	40.78	13.64	40.72	13.82	43
44	41.85	13.60	41.79	13.78	41.73	13.96	41.66	14.14	44
45	42.80	13.91	42.74	14.09	42.67	14.28	42.61	14.46	45
46	43.75	14.21	43.69	14.41	43.62	14.60	43.56	14.79	46
47	44.70	14.52	44.64	14.72	44.57	14.91	44.51	15.11	47
48	45.65	14.83	45.59	15.03	45.52	15.23	45.45	15.43	48
49	46.60	15.14	46.54	15.35	46.47	15.55	46.40	15.75	49
50	47.55	15.45	47.48	15.66	47.42	15.87	47.35	16.07	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	72 Deg.		71¾ Deg.		71½ Deg.		71¼ Deg.		



Distance.	18 Deg.		18¼ Deg.		18½ Deg.		18¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	18.50	15.76	48.43	15.97	48.36	16.18	48.29	16.39	51
52	49.45	16.07	49.38	16.28	49.31	16.50	49.24	16.71	52
53	50.41	16.38	50.33	16.60	50.26	16.82	50.19	17.04	53
54	51.36	16.69	51.28	16.91	51.21	17.13	51.13	17.36	54
55	52.31	17.00	52.23	17.22	52.16	17.45	52.08	17.68	55
56	53.26	17.30	53.18	17.54	53.11	17.77	53.03	18.00	56
57	54.21	17.61	54.13	17.85	54.05	18.09	53.98	18.32	57
58	55.16	17.92	55.08	18.16	55.00	18.40	54.92	18.64	58
59	56.11	18.23	56.03	18.48	55.95	18.72	55.87	18.96	59
60	57.06	18.54	56.98	18.79	56.90	19.04	56.82	19.29	60
61	58.01	18.85	57.93	19.10	57.85	19.36	57.76	19.61	61
62	58.97	19.16	58.88	19.42	58.80	19.67	58.71	19.93	62
63	59.92	19.47	59.83	19.73	59.74	19.99	59.66	20.25	63
64	60.87	19.78	60.78	20.04	60.69	20.31	60.60	20.57	64
65	61.82	20.09	61.73	20.36	61.64	20.62	61.55	20.89	65
66	62.77	20.40	62.68	20.67	62.59	20.94	62.50	21.22	66
67	63.72	20.70	63.63	20.98	63.54	21.26	63.44	21.54	67
68	64.67	21.01	64.58	21.30	64.49	21.58	64.39	21.86	68
69	65.62	21.32	65.53	21.61	65.43	21.89	65.34	22.18	69
70	66.57	21.63	66.48	21.92	66.38	22.21	66.29	22.50	70
71	67.53	21.94	67.43	22.23	67.33	22.53	67.23	22.82	71
72	68.48	22.25	68.38	22.55	68.28	22.85	68.18	23.14	72
73	69.43	22.56	69.33	22.86	69.23	23.16	69.13	23.47	73
74	70.38	22.87	70.28	23.17	70.18	23.48	70.07	23.79	74
75	71.33	23.18	71.23	23.49	71.12	23.80	71.02	24.11	75
76	72.28	23.49	72.18	23.80	72.07	24.12	71.97	24.43	76
77	73.23	23.79	73.13	24.11	73.02	24.43	72.91	24.75	77
78	74.18	24.10	74.08	24.43	73.97	24.75	73.86	25.07	78
79	75.13	24.41	75.03	24.74	74.92	25.07	74.81	25.39	79
80	76.08	24.72	75.98	25.05	75.87	25.38	75.75	25.72	80
81	77.04	25.03	76.93	25.37	76.81	25.70	76.70	26.04	81
82	77.99	25.34	77.88	25.68	77.76	26.02	77.65	26.36	82
83	78.94	25.65	78.83	25.99	78.71	26.34	78.60	26.68	83
84	79.89	25.96	79.77	26.31	79.66	26.65	79.54	27.00	84
85	80.84	26.27	80.72	26.62	80.61	26.97	80.49	27.32	85
86	81.79	26.58	81.67	26.93	81.56	27.29	81.44	27.64	86
87	82.74	26.88	82.62	27.25	82.50	27.61	82.38	27.97	87
88	83.69	27.19	83.57	27.56	83.45	27.92	83.33	28.29	88
89	84.64	27.50	84.52	27.87	84.40	28.24	84.28	28.61	89
90	85.60	27.81	85.47	28.18	85.35	28.56	85.22	28.93	90
91	86.55	28.12	86.42	28.50	86.30	28.87	86.17	29.25	91
92	87.50	28.43	87.37	28.81	87.25	29.19	87.12	29.57	92
93	88.45	28.74	88.32	29.12	88.19	29.51	88.06	29.89	93
94	89.40	29.05	89.27	29.44	89.14	29.83	89.01	30.22	94
95	90.35	29.36	90.22	29.75	90.09	30.14	89.96	30.54	95
96	91.30	29.67	91.17	30.06	91.04	30.46	90.91	30.86	96
97	92.25	29.97	92.12	30.38	91.99	30.78	91.85	31.18	97
98	93.20	30.28	93.07	30.69	92.94	31.10	92.80	31.50	98
99	94.15	30.59	94.02	31.00	93.88	31.41	93.75	31.82	99
100	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	72 Deg.		71¾ Deg.		71½ Deg.		71¼ Deg.		

Distance.	19 Deg.		19 $\frac{1}{4}$ Deg.		19 $\frac{1}{2}$ Deg.		19 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.95	0.33	0.94	0.33	0.94	0.33	0.94	0.34	1
2	1.89	0.65	1.89	0.66	1.89	0.67	1.88	0.68	2
3	2.84	0.98	2.83	0.99	2.83	1.00	2.82	1.01	3
4	3.78	1.30	3.78	1.32	3.77	1.34	3.76	1.35	4
5	4.73	1.63	4.72	1.65	4.71	1.67	4.71	1.69	5
6	5.67	1.95	5.66	1.98	5.66	2.00	5.65	2.03	6
7	6.62	2.28	6.61	2.31	6.60	2.34	6.59	2.37	7
8	7.56	2.60	7.55	2.64	7.54	2.67	7.53	2.70	8
9	8.51	2.93	8.50	2.97	8.48	3.00	8.47	3.04	9
10	9.46	3.26	9.44	3.30	9.43	3.34	9.41	3.38	10
11	10.40	3.58	10.38	3.63	10.37	3.67	10.35	3.72	11
12	11.35	3.91	11.33	3.96	11.31	4.01	11.29	4.06	12
13	12.29	4.23	12.27	4.29	12.25	4.34	12.24	4.39	13
14	13.24	4.56	13.22	4.62	13.20	4.67	13.18	4.73	14
15	14.18	4.88	14.16	4.95	14.14	5.01	14.12	5.07	15
16	15.13	5.21	15.11	5.28	15.08	5.34	15.06	5.41	16
17	16.07	5.53	16.05	5.60	16.02	5.67	16.00	5.74	17
18	17.02	5.86	16.99	5.93	16.97	6.01	16.94	6.08	18
19	17.96	6.19	17.94	6.26	17.91	6.34	17.88	6.42	19
20	18.91	6.51	18.88	6.59	18.85	6.68	18.82	6.76	20
21	19.86	6.84	19.83	6.92	19.80	7.01	19.76	7.10	21
22	20.80	7.16	20.77	7.25	20.74	7.34	20.71	7.43	22
23	21.75	7.49	21.71	7.58	21.68	7.68	21.65	7.77	23
24	22.69	7.81	22.66	7.91	22.62	8.01	22.59	8.11	24
25	23.64	8.14	23.60	8.24	23.57	8.35	23.53	8.45	25
26	24.58	8.46	24.55	8.57	24.51	8.68	24.47	8.79	26
27	25.53	8.79	25.49	8.90	25.45	9.01	25.41	9.12	27
28	26.47	9.12	26.43	9.23	26.39	9.35	26.35	9.46	28
29	27.42	9.44	27.38	9.56	27.34	9.68	27.29	9.80	29
30	28.37	9.77	28.32	9.89	28.28	10.01	28.24	10.14	30
31	29.31	10.09	29.27	10.22	29.22	10.35	29.18	10.48	31
32	30.26	10.42	30.21	10.55	30.16	10.68	30.12	10.81	32
33	31.20	10.74	31.15	10.88	31.11	11.02	31.06	11.15	33
34	32.15	11.07	32.10	11.21	32.05	11.35	32.00	11.49	34
35	33.09	11.39	33.04	11.54	32.99	11.68	32.94	11.83	35
36	34.04	11.72	33.99	11.87	33.94	12.02	33.88	12.17	36
37	34.98	12.05	34.93	12.20	34.88	12.35	34.82	12.50	37
38	35.93	12.37	35.88	12.53	35.82	12.68	35.76	12.84	38
39	36.88	12.70	36.82	12.86	36.76	13.02	36.71	13.18	39
40	37.82	13.02	37.76	13.19	37.71	13.35	37.65	13.52	40
41	38.77	13.35	38.71	13.52	38.65	13.69	38.59	13.85	41
42	39.71	13.67	39.65	13.85	39.59	14.02	39.53	14.19	42
43	40.66	14.00	40.60	14.18	40.53	14.35	40.47	14.53	43
44	41.60	14.32	41.54	14.51	41.48	14.69	41.41	14.87	44
45	42.55	14.65	42.48	14.84	42.42	15.02	42.35	15.21	45
46	43.49	14.98	43.43	15.17	43.36	15.36	43.29	15.54	46
47	44.44	15.30	44.37	15.50	44.30	15.69	44.24	15.88	47
48	45.38	15.63	45.32	15.83	45.25	16.02	45.18	16.22	48
49	46.33	15.95	46.26	16.15	46.19	16.36	46.12	16.56	49
50	47.28	16.28	47.20	16.48	47.13	16.69	47.06	16.90	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	71 Deg.		70 $\frac{3}{4}$ Deg.		70 $\frac{1}{2}$ Deg.		70 $\frac{1}{4}$ Deg.		

Distance.	19 Deg.		19½ Deg.		19½ Deg.		19¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	48.22	16.60	48.15	16.81	48.07	17.02	48.00	17.23	51
52	49.17	16.93	49.09	17.14	49.02	17.36	48.94	17.57	52
53	50.11	17.26	50.04	17.47	49.96	17.69	49.88	17.91	53
54	51.06	17.58	50.98	17.80	50.90	18.03	50.82	18.25	54
55	52.00	17.91	51.92	18.13	51.85	18.36	51.76	18.59	55
56	52.95	18.23	52.87	18.46	52.79	18.69	52.71	18.92	56
57	53.89	18.56	53.81	18.79	53.73	19.03	53.65	19.26	57
58	54.84	18.88	54.76	19.12	54.67	19.36	54.59	19.60	58
59	55.79	19.21	55.70	19.45	55.62	19.69	55.53	19.94	59
60	56.73	19.53	56.65	19.78	56.56	20.03	56.47	20.27	60
61	57.68	19.86	57.59	20.11	57.50	20.36	57.41	20.61	61
62	58.62	20.19	58.53	20.44	58.44	20.70	58.35	20.95	62
63	59.57	20.51	59.48	20.77	59.39	21.03	59.29	21.29	63
64	60.51	20.84	60.42	21.10	60.33	21.36	60.24	21.63	64
65	61.46	21.16	61.37	21.43	61.27	21.70	61.18	21.96	65
66	62.40	21.49	62.31	21.76	62.21	22.03	62.12	22.30	66
67	63.35	21.81	63.25	22.09	63.16	22.37	63.06	22.64	67
68	64.30	22.14	64.20	22.42	64.10	22.70	64.00	22.98	68
69	65.24	22.46	65.14	22.75	65.04	23.03	64.94	23.32	69
70	66.19	22.79	66.09	23.08	65.98	23.37	65.88	23.65	70
71	67.13	23.12	67.03	23.41	66.93	23.70	66.82	23.99	71
72	68.08	23.44	67.97	23.74	67.87	24.03	67.76	24.33	72
73	69.02	23.77	68.92	24.07	68.81	24.37	68.71	24.67	73
74	69.97	24.09	69.86	24.40	69.76	24.70	69.65	25.01	74
75	70.91	24.42	70.81	24.73	70.70	25.04	70.59	25.34	75
76	71.86	24.74	71.75	25.06	71.64	25.37	71.53	25.68	76
77	72.80	25.07	72.69	25.39	72.58	25.70	72.47	26.02	77
78	73.75	25.39	73.64	25.72	73.53	26.04	73.41	26.36	78
79	74.70	25.72	74.58	26.05	74.47	26.37	74.35	26.70	79
80	75.64	26.05	75.53	26.38	75.41	26.70	75.29	27.03	80
81	76.59	26.37	76.47	26.70	76.35	27.04	76.24	27.37	81
82	77.53	26.70	77.42	27.03	77.30	27.37	77.18	27.71	82
83	78.48	27.02	78.36	27.36	78.24	27.71	78.12	28.05	83
84	79.42	27.35	79.30	27.69	79.18	28.04	79.06	28.39	84
85	80.37	27.67	80.25	28.02	80.12	28.37	80.00	28.72	85
86	81.31	28.00	81.19	28.35	81.07	28.71	80.94	29.06	86
87	82.26	28.32	82.14	28.68	82.01	29.04	81.88	29.40	87
88	83.21	28.65	83.08	29.01	92.95	29.37	82.82	29.74	88
89	84.15	28.98	84.02	29.34	83.90	29.71	83.76	30.07	89
90	85.10	29.30	84.97	29.67	84.84	30.04	84.71	30.41	90
91	86.04	29.63	85.91	30.00	85.78	30.38	85.65	30.75	91
92	86.99	29.95	86.86	30.33	86.72	30.71	86.59	31.09	92
93	87.93	30.28	87.80	30.66	87.67	31.04	87.53	31.43	93
94	88.88	30.60	88.74	30.99	88.61	31.38	88.47	31.76	94
95	89.82	30.93	89.69	31.32	89.55	31.71	89.41	32.10	95
96	90.77	31.25	90.63	31.65	90.49	32.05	90.35	32.44	96
97	91.72	31.58	91.58	31.98	91.44	32.38	91.29	32.78	97
98	92.66	31.91	92.52	32.31	92.38	32.71	92.24	33.12	98
99	93.61	32.23	93.46	32.64	93.32	33.05	93.18	33.45	99
100	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	71 Deg.		70¾ Deg.		70½ Deg.		70¼ Deg.		

Distance.	20 Deg.		20 $\frac{1}{4}$ Deg.		20 $\frac{1}{2}$ Deg.		20 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.94	0.34	0.94	0.35	0.94	0.35	0.94	0.35	1
2	1.88	0.68	1.88	0.69	1.87	0.70	1.87	0.71	2
3	2.82	1.03	2.81	1.04	2.81	1.05	2.81	1.06	3
4	3.76	1.37	3.75	1.38	3.75	1.40	3.74	1.42	4
5	4.70	1.71	4.69	1.73	4.68	1.75	4.68	1.77	5
6	5.64	2.05	5.63	2.08	5.62	2.10	5.61	2.13	6
7	6.58	2.39	6.57	2.42	6.56	2.45	6.55	2.48	7
8	7.52	2.74	7.51	2.77	7.49	2.80	7.48	2.83	8
9	8.46	3.08	8.44	3.12	8.43	3.15	8.42	3.19	9
10	9.40	3.42	9.38	3.46	9.37	3.50	9.35	3.54	10
11	10.34	3.76	10.32	3.81	10.30	3.85	10.29	3.90	11
12	11.28	4.10	11.26	4.15	11.24	4.20	11.22	4.25	12
13	12.22	4.45	12.20	4.50	12.18	4.55	12.16	4.61	13
14	13.16	4.79	13.13	4.85	13.11	4.90	13.09	4.96	14
15	14.10	5.13	14.07	5.19	14.05	5.25	14.03	5.31	15
16	15.04	5.47	15.01	5.54	14.99	5.60	14.96	5.67	16
17	15.97	5.81	15.95	5.88	15.92	5.95	15.90	6.02	17
18	16.91	6.16	16.89	6.23	16.86	6.30	16.83	6.38	18
19	17.85	6.50	17.83	6.58	17.80	6.65	17.77	6.73	19
20	18.79	6.84	18.76	6.92	18.73	7.00	18.70	7.09	20
21	19.73	7.18	19.70	7.27	19.67	7.35	19.64	7.44	21
22	20.67	7.52	20.64	7.61	20.61	7.70	20.57	7.79	22
23	21.61	7.87	21.58	7.96	21.54	8.05	21.51	8.15	23
24	22.55	8.21	22.52	8.31	22.48	8.40	22.44	8.50	24
25	23.49	8.55	23.45	8.65	23.42	8.76	23.38	8.86	25
26	24.43	8.89	24.39	9.00	24.35	9.11	24.31	9.21	26
27	25.37	9.23	25.33	9.35	25.29	9.46	25.25	9.57	27
28	26.31	9.58	26.27	9.69	26.23	9.81	26.18	9.92	28
29	27.25	9.92	27.21	10.04	27.16	10.16	27.12	10.27	29
30	28.19	10.26	28.15	10.38	28.10	10.51	28.05	10.63	30
31	29.13	10.60	29.08	10.73	29.04	10.86	28.99	10.98	31
32	30.07	10.94	30.02	11.08	29.97	11.21	29.92	11.34	32
33	31.01	11.29	30.96	11.42	30.91	11.56	30.86	11.69	33
34	31.95	11.63	31.90	11.77	31.85	11.91	31.79	12.05	34
35	32.89	11.97	32.84	12.11	32.78	12.26	32.73	12.40	35
36	33.83	12.31	33.77	12.46	33.72	12.61	33.66	12.75	36
37	34.77	12.65	34.71	12.81	34.66	12.96	34.60	13.11	37
38	35.71	13.00	35.65	13.15	35.59	13.31	35.54	13.46	38
39	36.65	13.34	36.59	13.50	36.53	13.66	36.47	13.82	39
40	37.59	13.68	37.53	13.84	37.47	14.01	37.41	14.17	40
41	38.53	14.02	38.47	14.19	38.40	14.36	38.34	14.53	41
42	39.47	14.36	39.40	14.54	39.34	14.71	39.28	14.88	42
43	40.41	14.71	40.34	14.88	40.28	15.06	40.21	15.23	43
44	41.35	15.05	41.28	15.23	41.21	15.41	41.15	15.59	44
45	42.29	15.39	42.22	15.58	42.15	15.76	42.08	15.94	45
46	43.23	15.73	43.16	15.92	43.09	16.11	43.02	16.30	46
47	44.17	16.07	44.09	16.27	44.02	16.46	43.95	16.65	47
48	45.11	16.42	45.03	16.61	44.96	16.81	44.89	17.01	48
49	46.04	16.76	45.97	16.96	45.90	17.16	45.82	17.36	49
50	46.98	17.10	46.91	17.31	46.83	17.51	46.76	17.71	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	70 Deg.		69 $\frac{3}{4}$ Deg.		69 $\frac{1}{2}$ Deg.		69 $\frac{1}{4}$ Deg.		

Distance.	20 Deg.		20 $\frac{1}{4}$ Deg.		20 $\frac{1}{2}$ Deg.		20 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	47.92	17.44	47.35	17.65	47.77	17.86	47.69	18.07	51
52	48.86	17.79	48.79	18.00	48.71	18.21	48.63	18.42	52
53	49.80	18.13	49.72	18.34	49.64	18.56	49.56	18.78	53
54	50.74	18.47	50.66	18.69	50.58	18.91	50.50	19.13	54
55	51.68	18.81	51.60	19.04	51.52	19.26	51.43	19.49	55
56	52.62	19.15	52.54	19.38	52.45	19.61	52.37	19.84	56
57	53.56	19.50	53.48	19.73	53.39	19.96	53.30	20.19	57
58	54.50	19.84	54.42	20.07	54.33	20.31	54.24	20.55	58
59	55.44	20.18	55.35	20.42	55.26	20.66	55.17	20.90	59
60	56.38	20.52	56.29	20.77	56.20	21.01	56.11	21.26	60
61	57.32	20.86	57.23	21.11	57.14	21.36	57.04	21.61	61
62	58.26	21.21	58.17	21.46	58.07	21.71	57.98	21.97	62
63	59.20	21.55	59.11	21.81	59.01	22.06	58.91	22.32	63
64	60.14	21.89	60.04	22.15	59.95	22.41	59.85	22.67	64
65	61.08	22.23	60.93	22.50	60.88	22.76	60.78	23.03	65
66	62.02	22.57	61.92	22.84	61.82	23.11	61.72	23.38	66
67	62.96	22.92	62.86	23.19	62.76	23.46	62.65	23.74	67
68	63.90	23.26	63.80	23.54	63.69	23.81	63.59	24.09	68
69	64.84	23.60	64.74	23.88	64.63	24.16	64.52	24.45	69
70	65.78	23.94	65.67	24.23	65.57	24.51	65.46	24.80	70
71	66.72	24.28	66.61	24.57	66.50	24.86	66.39	25.15	71
72	67.66	24.63	67.55	24.92	67.44	25.21	67.33	25.51	72
73	68.60	24.97	68.49	25.27	68.33	25.57	68.26	25.86	73
74	69.54	25.31	69.43	25.61	69.31	25.92	69.20	26.22	74
75	70.48	25.65	70.36	25.96	70.25	26.27	70.14	26.57	75
76	71.42	25.99	71.30	26.30	71.19	26.62	71.07	26.93	76
77	72.36	26.34	72.24	26.65	72.12	26.97	72.01	27.28	77
78	73.30	26.68	73.18	27.00	73.06	27.32	72.94	27.63	78
79	74.24	27.02	74.12	27.34	74.00	27.67	73.88	27.99	79
80	75.18	27.36	75.06	27.69	74.93	28.02	74.81	28.34	80
81	76.12	27.70	75.99	28.04	75.87	28.37	75.75	28.70	81
82	77.05	28.05	76.93	28.38	76.81	28.72	76.68	29.05	82
83	77.99	28.39	77.87	28.73	77.74	29.07	77.62	29.41	83
84	78.93	28.73	78.81	29.07	78.68	29.42	78.55	29.76	84
85	79.87	29.07	79.75	29.42	79.62	29.77	79.49	30.11	85
86	80.81	29.41	80.68	29.77	80.55	30.12	80.42	30.47	86
87	81.75	29.76	81.62	30.11	81.49	30.47	81.36	30.82	87
88	82.69	30.10	82.56	30.46	82.43	30.82	82.29	31.18	88
89	83.63	30.44	83.50	30.80	83.36	31.17	83.23	31.53	89
90	84.57	30.78	84.44	31.15	84.30	31.52	84.16	31.89	90
91	85.51	31.12	85.33	31.50	85.24	31.87	85.10	32.24	91
92	86.45	31.47	86.31	31.84	86.17	32.22	86.03	32.59	92
93	87.39	31.81	87.25	32.19	87.11	32.57	86.97	32.95	93
94	88.33	32.15	88.19	32.54	88.05	32.92	87.90	33.30	94
95	89.27	32.49	89.13	32.88	88.98	33.27	88.84	33.66	95
96	90.21	32.83	90.07	33.23	89.92	33.62	89.77	34.01	96
97	91.15	33.18	91.00	33.57	90.86	33.97	90.71	34.37	97
98	92.09	33.52	91.94	33.92	91.79	34.32	91.64	34.72	98
99	93.03	33.86	92.88	34.27	92.73	34.67	92.58	35.07	99
100	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	70 Deg.		69 $\frac{3}{4}$ Deg.		69 $\frac{1}{2}$ Deg.		69 $\frac{1}{4}$ Deg.		

Distance.	21 Deg.		21½ Deg.		21½ Deg.		21¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.93	0.36	0.93	0.36	0.93	0.37	0.93	0.37	1
2	1.87	0.72	1.86	0.72	1.86	0.73	1.86	0.74	2
3	2.80	1.08	2.80	1.09	2.79	1.10	2.79	1.11	3
4	3.73	1.43	3.73	1.45	3.72	1.47	3.72	1.48	4
5	4.67	1.79	4.66	1.81	4.65	1.83	4.64	1.85	5
6	5.60	2.15	5.59	2.17	5.58	2.20	5.57	2.22	6
7	6.54	2.51	6.52	2.54	6.51	2.57	6.50	2.59	7
8	7.47	2.87	7.46	2.90	7.44	2.93	7.43	2.96	8
9	8.40	3.23	8.39	3.26	8.37	3.30	8.36	3.34	9
10	9.34	3.58	9.32	3.62	9.30	3.67	9.29	3.71	10
11	10.27	3.94	10.25	3.99	10.23	4.03	10.22	4.08	11
12	11.20	4.30	11.18	4.35	11.17	4.40	11.15	4.45	12
13	12.14	4.66	12.12	4.71	12.10	4.76	12.07	4.82	13
14	13.07	5.02	13.05	5.07	13.03	5.13	13.00	5.19	14
15	14.00	5.38	13.98	5.44	13.96	5.50	13.93	5.56	15
16	14.94	5.73	14.91	5.80	14.89	5.86	14.86	5.93	16
17	15.87	6.09	15.84	6.16	15.82	6.23	15.79	6.30	17
18	16.80	6.45	16.78	6.52	16.75	6.60	16.72	6.67	18
19	17.74	6.81	17.71	6.89	17.68	6.96	17.65	7.04	19
20	18.67	7.17	18.64	7.25	18.61	7.33	18.58	7.41	20
21	19.61	7.53	19.57	7.61	19.54	7.70	19.50	7.78	21
22	20.54	7.88	20.50	7.97	20.47	8.06	20.43	8.15	22
23	21.47	8.24	21.44	8.34	21.40	8.43	21.36	8.52	23
24	22.41	8.60	22.37	8.70	22.33	8.80	22.29	8.89	24
25	23.34	8.96	23.30	9.06	23.26	9.16	23.22	9.26	25
26	24.27	9.32	24.23	9.42	24.19	9.53	24.15	9.63	26
27	25.21	9.68	25.16	9.79	25.12	9.90	25.08	10.01	27
28	26.14	10.03	26.10	10.15	26.05	10.26	26.01	10.38	28
29	27.07	10.39	27.03	10.51	26.98	10.63	26.94	10.75	29
30	28.01	10.75	27.96	10.87	27.91	11.00	27.86	11.12	30
31	28.94	11.11	28.89	11.24	28.84	11.36	28.79	11.49	31
32	29.87	11.47	29.82	11.60	29.77	11.73	29.72	11.86	32
33	30.81	11.83	30.76	11.96	30.70	12.09	30.65	12.23	33
34	31.74	12.18	31.69	12.32	31.63	12.46	31.58	12.60	34
35	32.68	12.54	32.62	12.69	32.56	12.83	32.51	12.97	35
36	33.61	12.90	33.55	13.05	33.50	13.19	33.44	13.34	36
37	34.54	13.26	34.48	13.41	34.43	13.56	34.37	13.71	37
38	35.48	13.62	35.42	13.77	35.36	13.93	35.29	14.08	38
39	36.41	13.98	36.35	14.14	36.29	14.29	36.22	14.45	39
40	37.34	14.33	37.28	14.50	37.22	14.66	37.15	14.82	40
41	38.28	14.69	38.21	14.86	38.15	15.03	38.08	15.19	41
42	39.21	15.05	39.14	15.22	39.08	15.39	39.01	15.56	42
43	40.14	15.41	40.08	15.58	40.01	15.76	39.94	15.93	43
44	41.08	15.77	41.01	15.95	40.94	16.13	40.87	16.30	44
45	42.01	16.13	41.94	16.31	41.87	16.49	41.80	16.68	45
46	42.94	16.48	42.87	16.67	42.80	16.86	42.73	17.05	46
47	43.88	16.84	43.80	17.03	43.73	17.23	43.65	17.42	47
48	44.81	17.20	44.74	17.40	44.66	17.59	44.58	17.79	48
49	45.75	17.56	45.67	17.76	45.59	17.96	45.51	18.16	49
50	46.68	17.92	46.60	18.12	46.52	18.33	46.44	18.53	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	69 Deg.		68¾ Deg.		68½ Deg.		68¼ Deg.		

Distance.	21 Deg.		21 $\frac{1}{4}$ Deg.		21 $\frac{1}{2}$ Deg.		21 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	47.61	18.28	47.53	18.48	47.45	18.69	47.37	18.90	51
52	48.55	18.64	48.46	18.85	48.38	19.06	48.30	19.27	52
53	49.48	18.99	49.40	19.21	49.31	19.42	49.23	19.64	53
54	50.41	19.35	50.33	19.57	50.24	19.79	50.16	20.01	54
55	51.35	19.71	51.26	19.93	51.17	20.16	51.08	20.38	55
56	52.28	20.07	52.19	20.30	52.10	20.52	52.01	20.75	56
57	53.21	20.43	53.12	20.66	53.03	20.89	52.94	21.12	57
58	54.15	20.79	54.06	21.02	53.96	21.26	53.87	21.49	58
59	55.08	21.14	54.99	21.38	54.89	21.62	54.80	21.86	59
60	56.01	21.50	55.92	21.75	55.83	21.99	55.73	22.23	60
61	56.95	21.86	56.85	22.11	56.76	22.36	56.66	22.60	61
62	57.88	22.22	57.78	22.47	57.69	22.72	57.59	22.97	62
63	58.82	22.58	58.72	22.83	58.62	23.09	58.52	23.35	63
64	59.75	22.94	59.65	23.20	59.55	23.46	59.44	23.72	64
65	60.68	23.29	60.58	23.56	60.48	23.82	60.37	24.09	65
66	61.62	23.65	61.51	23.92	61.41	24.19	61.30	24.46	66
67	62.55	24.01	62.44	24.28	62.34	24.56	62.23	24.83	67
68	63.48	24.37	63.38	24.65	63.27	24.92	63.16	25.20	68
69	64.42	24.73	64.31	25.01	64.20	25.29	64.09	25.57	69
70	65.35	25.09	65.24	25.37	65.13	25.66	65.02	25.94	70
71	66.28	25.44	66.17	25.73	66.06	26.02	65.95	26.31	71
72	67.22	25.80	67.10	26.10	66.99	26.39	66.87	26.68	72
73	68.15	26.16	68.04	26.46	67.92	26.75	67.80	27.05	73
74	69.08	26.52	68.97	26.82	68.85	27.12	68.73	27.42	74
75	70.02	26.88	69.90	27.18	69.78	27.49	69.66	27.79	75
76	70.95	27.24	70.83	27.55	70.71	27.85	70.59	28.16	76
77	71.89	27.59	71.76	27.91	71.64	28.22	71.52	28.53	77
78	72.82	27.95	72.70	28.27	72.57	28.59	72.45	28.90	78
79	73.75	28.31	73.63	28.63	73.50	28.95	73.38	29.27	79
80	74.69	28.67	74.56	29.00	74.43	29.32	74.30	29.64	80
81	75.62	29.03	75.49	29.36	75.36	29.69	75.23	30.02	81
82	76.55	29.39	76.42	29.72	76.29	30.05	76.16	30.39	82
83	77.49	29.74	77.36	30.08	77.22	30.42	77.09	30.76	83
84	78.42	30.10	78.29	30.44	78.16	30.79	78.02	31.13	84
85	79.35	30.46	79.22	30.81	79.09	31.15	78.95	31.50	85
86	80.29	30.82	80.15	31.17	80.02	31.52	79.88	31.87	86
87	81.22	31.18	81.08	31.53	80.95	31.89	80.81	32.24	87
88	82.16	31.54	82.02	31.89	81.88	32.25	81.74	32.61	88
89	83.09	31.89	82.95	32.26	82.81	32.62	82.66	32.98	89
90	84.02	32.25	83.88	32.62	83.74	32.99	83.59	33.35	90
91	84.96	32.61	84.81	32.98	84.67	33.35	84.52	33.72	91
92	85.89	32.97	85.74	33.34	85.60	33.72	85.45	34.09	92
93	86.82	33.33	86.68	33.71	86.53	34.08	86.38	34.46	93
94	87.76	33.69	87.61	34.07	87.46	34.45	87.31	34.83	94
95	88.69	34.04	88.54	34.43	88.39	34.82	88.24	35.20	95
96	89.62	34.40	89.47	34.79	89.32	35.18	89.17	35.57	96
97	90.56	34.76	90.40	35.16	90.25	35.55	90.09	35.94	97
98	91.49	35.12	91.34	35.52	91.18	35.92	91.02	36.31	98
99	92.42	35.48	92.27	35.88	92.11	36.28	91.95	36.69	99
100	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	69 Deg.		68 $\frac{3}{4}$ Deg.		68 $\frac{1}{2}$ Deg.		68 $\frac{1}{4}$ Deg.		

Distance.	22 Deg.		22 $\frac{1}{4}$ Deg.		22 $\frac{1}{2}$ Deg.		22 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.93	0.37	0.93	0.38	0.92	0.38	0.92	0.39	1
2	1.85	0.75	1.85	0.76	1.85	0.77	1.84	0.77	2
3	2.78	1.12	2.78	1.14	2.77	1.15	2.77	1.16	3
4	3.71	1.50	3.70	1.51	3.70	1.53	3.69	1.55	4
5	4.64	1.87	4.63	1.89	4.62	1.91	4.61	1.93	5
6	5.56	2.25	5.55	2.27	5.54	2.30	5.53	2.32	6
7	6.49	2.62	6.48	2.65	6.47	2.68	6.46	2.71	7
8	7.42	3.00	7.40	3.03	7.39	3.06	7.38	3.09	8
9	8.34	3.37	8.33	3.41	8.31	3.44	8.30	3.48	9
10	9.27	3.75	9.26	3.79	9.24	3.83	9.22	3.87	10
11	10.20	4.12	10.18	4.17	10.16	4.21	10.14	4.25	11
12	11.13	4.50	11.11	4.54	11.09	4.59	11.07	4.64	12
13	12.05	4.87	12.03	4.92	12.01	4.97	11.99	5.03	13
14	12.98	5.24	12.96	5.30	12.93	5.36	12.91	5.41	14
15	13.91	5.62	13.88	5.68	13.86	5.74	13.83	5.80	15
16	14.83	5.99	14.81	6.06	14.78	6.12	14.76	6.19	16
17	15.76	6.37	15.73	6.44	15.71	6.51	15.68	6.57	17
18	16.69	6.74	16.66	6.82	16.63	6.89	16.60	6.96	18
19	17.62	7.12	17.59	7.19	17.55	7.27	17.52	7.35	19
20	18.54	7.49	18.51	7.57	18.48	7.65	18.44	7.73	20
21	19.47	7.87	19.44	7.95	19.40	8.04	19.37	8.12	21
22	20.40	8.24	20.36	8.33	20.33	8.42	20.29	8.51	22
23	21.33	8.62	21.29	8.71	21.25	8.80	21.21	8.89	23
24	22.25	8.99	22.21	9.09	22.17	9.18	22.13	9.28	24
25	23.18	9.37	23.14	9.47	23.10	9.57	23.05	9.67	25
26	24.11	9.74	24.06	9.84	24.02	9.95	23.98	10.05	26
27	25.03	10.11	24.99	10.22	24.94	10.33	24.90	10.44	27
28	25.96	10.49	25.92	10.60	25.87	10.72	25.82	10.83	28
29	26.89	10.86	26.84	10.98	26.79	11.10	26.74	11.21	29
30	27.82	11.24	27.77	11.36	27.72	11.48	27.67	11.60	30
31	28.74	11.61	28.69	11.74	28.64	11.86	28.59	11.99	31
32	29.67	11.99	29.62	12.12	29.56	12.25	29.51	12.37	32
33	30.60	12.36	30.54	12.50	30.49	12.63	30.43	12.76	33
34	31.52	12.74	31.47	12.87	31.41	13.01	31.35	13.15	34
35	32.45	13.11	32.39	13.25	32.34	13.39	32.28	13.53	35
36	33.38	13.49	33.32	13.63	33.26	13.78	33.20	13.92	36
37	34.31	13.86	34.24	14.01	34.18	14.16	34.12	14.31	37
38	35.23	14.24	35.17	14.39	35.11	14.54	35.04	14.70	38
39	36.16	14.61	36.10	14.77	36.03	14.92	35.97	15.08	39
40	37.09	14.98	37.02	15.15	36.96	15.31	36.89	15.47	40
41	38.01	15.36	37.95	15.52	37.88	15.69	37.81	15.86	41
42	38.94	15.73	38.87	15.90	38.80	16.07	38.73	16.24	42
43	39.87	16.11	39.80	16.28	39.73	16.46	39.65	16.63	43
44	40.80	16.48	40.72	16.66	40.65	16.84	40.58	17.02	44
45	41.72	16.86	41.65	17.04	41.57	17.22	41.50	17.40	45
46	42.65	17.23	42.57	17.42	42.50	17.60	42.42	17.79	46
47	43.58	17.61	43.50	17.80	43.42	17.99	43.34	18.18	47
48	44.50	17.98	44.43	18.18	44.35	18.37	44.27	18.56	48
49	45.43	18.36	45.35	18.55	45.27	18.75	45.19	18.95	49
50	46.36	18.73	46.28	18.93	46.19	19.13	46.11	19.34	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	68 Deg.		67 $\frac{1}{4}$ Deg.		67 $\frac{1}{2}$ Deg.		67 $\frac{3}{4}$ Deg.		



Distance.	22 Deg.		22½ Deg.		22½ Deg.		22¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	47.29	19.10	47.20	19.31	47.12	19.52	47.03	19.72	51
52	48.21	19.48	48.13	19.69	48.04	19.90	47.95	20.11	52
53	49.14	19.85	49.05	20.07	48.97	20.28	48.88	20.50	53
54	50.07	20.23	49.98	20.45	49.89	20.66	49.80	20.88	54
55	51.00	20.60	50.90	20.83	50.81	21.05	50.72	21.27	55
56	51.92	20.98	51.83	21.20	51.74	21.43	51.64	21.66	56
57	52.85	21.35	52.76	21.58	52.66	21.81	52.57	22.04	57
58	53.78	21.73	53.68	21.96	53.59	22.20	53.49	22.43	58
59	54.70	22.10	54.61	22.34	54.51	22.58	54.41	22.82	59
60	55.63	22.48	55.53	22.72	55.43	22.96	55.33	23.20	60
61	56.56	22.85	56.47	23.10	56.36	23.34	56.25	23.59	61
62	57.49	23.23	57.38	23.48	57.28	23.73	57.18	23.98	62
63	58.41	23.60	58.31	23.85	58.20	24.11	58.10	24.36	63
64	59.34	23.97	59.23	24.23	59.13	24.49	59.02	24.75	64
65	60.27	24.35	60.16	24.61	60.05	24.87	59.94	25.14	65
66	61.19	24.72	61.09	24.99	60.98	25.26	60.87	25.52	66
67	62.12	25.10	62.01	25.37	61.90	25.64	61.79	25.91	67
68	63.05	25.47	62.94	25.75	62.82	26.02	62.71	26.30	68
69	63.98	25.85	63.86	26.13	63.75	26.41	63.63	26.68	69
70	64.90	26.22	64.79	26.51	64.67	26.79	64.55	27.07	70
71	65.83	26.60	65.71	26.88	65.60	27.17	65.48	27.46	71
72	66.76	26.97	66.64	27.26	66.52	27.55	66.40	27.84	72
73	67.68	27.35	67.56	27.64	67.44	27.94	67.32	28.23	73
74	68.61	27.72	68.49	28.02	68.37	28.32	68.24	28.62	74
75	69.54	28.10	69.42	28.40	69.29	28.70	69.17	29.00	75
76	70.47	28.47	70.34	28.78	70.21	29.08	70.09	29.39	76
77	71.39	28.84	71.27	29.16	71.14	29.47	71.01	29.78	77
78	72.32	29.22	72.19	29.53	72.06	29.85	71.93	30.16	78
79	73.25	29.59	73.12	29.91	72.99	30.23	72.85	30.55	79
80	74.17	29.97	74.04	30.29	73.91	30.61	73.78	30.94	80
81	75.10	30.34	74.97	30.67	74.83	31.00	74.70	31.32	81
82	76.03	30.72	75.89	31.05	75.76	31.38	75.62	31.71	82
83	76.96	31.09	76.82	31.43	76.68	31.76	76.54	32.10	83
84	77.88	31.47	77.75	31.81	77.61	32.15	77.46	32.48	84
85	78.81	31.84	78.67	32.19	78.53	32.53	78.39	32.87	85
86	79.74	32.22	79.60	32.56	79.45	32.91	79.31	33.26	86
87	80.66	32.59	80.52	32.94	80.38	33.29	80.23	33.64	87
88	81.59	32.97	81.45	33.32	81.30	33.68	81.15	34.03	88
89	82.52	33.34	82.37	33.70	82.23	34.06	82.08	34.42	89
90	83.45	33.71	83.30	34.08	83.15	34.44	83.00	34.80	90
91	84.37	34.09	84.22	34.46	84.07	34.82	83.92	35.19	91
92	85.30	34.46	85.15	34.84	85.00	35.21	84.84	35.58	92
93	86.23	34.84	86.08	35.21	85.92	35.59	85.76	35.96	93
94	87.16	35.21	87.00	35.59	86.84	35.97	86.69	36.35	94
95	88.08	35.59	87.93	35.97	87.77	36.35	87.61	36.74	95
96	89.01	35.96	88.85	36.35	88.69	36.74	88.53	37.12	96
97	89.94	36.34	89.78	36.73	89.62	37.12	89.45	37.51	97
98	90.86	36.71	90.70	37.11	90.54	37.50	90.38	37.90	98
99	91.79	37.09	91.63	37.49	91.46	37.89	91.30	38.28	99
100	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	100

Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
		68 Deg.		67¾ Deg.		67½ Deg.		67¼ Deg.	

Distance.	23 Deg.		23 $\frac{1}{4}$ Deg.		23 $\frac{1}{2}$ Deg.		23 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.92	0.39	0.92	0.39	0.92	0.40	0.92	0.40	1
2	1.84	0.78	1.84	0.79	1.83	0.80	1.83	0.81	2
3	2.76	1.17	2.76	1.18	2.75	1.20	2.75	1.21	3
4	3.68	1.56	3.68	1.58	3.67	1.59	3.66	1.61	4
5	4.60	1.95	4.59	1.97	4.59	1.99	4.58	2.01	5
6	5.52	2.34	5.51	2.37	5.50	2.39	5.49	2.42	6
7	6.44	2.74	6.43	2.76	6.42	2.79	6.41	2.82	7
8	7.36	3.13	7.35	3.16	7.34	3.19	7.32	3.22	8
9	8.28	3.52	8.27	3.55	8.25	3.59	8.24	3.62	9
10	9.20	3.91	9.19	3.95	9.17	3.99	9.15	4.03	10
11	10.13	4.30	10.11	4.34	10.09	4.39	10.07	4.43	11
12	11.05	4.69	11.03	4.74	11.00	4.78	10.98	4.83	12
13	11.97	5.08	11.94	5.13	11.92	5.18	11.90	5.24	13
14	12.89	5.47	12.86	5.53	12.84	5.58	12.81	5.64	14
15	13.81	5.86	13.78	5.92	13.76	5.98	13.73	6.04	15
16	14.73	6.25	14.70	6.32	14.67	6.38	14.64	6.44	16
17	15.65	6.64	15.62	6.71	15.59	6.78	15.56	6.85	17
18	16.57	7.03	16.54	7.11	16.51	7.18	16.48	7.25	18
19	17.49	7.42	17.46	7.50	17.42	7.58	17.39	7.65	19
20	18.41	7.81	18.38	7.89	18.34	7.97	18.31	8.05	20
21	19.33	8.21	19.29	8.29	19.26	8.37	19.22	8.46	21
22	20.25	8.60	20.21	8.68	20.18	8.77	20.14	8.86	22
23	21.17	8.99	21.13	9.08	21.09	9.17	21.05	9.26	23
24	22.09	9.38	22.05	9.47	22.01	9.57	21.97	9.67	24
25	23.01	9.77	22.97	9.87	22.93	9.97	22.88	10.07	25
26	23.93	10.16	23.89	10.26	23.84	10.37	23.80	10.47	26
27	24.85	10.55	24.81	10.66	24.76	10.77	24.71	10.87	27
28	25.77	10.94	25.73	11.05	25.68	11.16	25.63	11.28	28
29	26.69	11.33	26.64	11.45	26.59	11.56	26.54	11.68	29
30	27.62	11.72	27.56	11.84	27.51	11.96	27.46	12.08	30
31	28.54	12.11	28.48	12.24	28.43	12.36	28.37	12.49	31
32	29.46	12.50	29.40	12.63	29.35	12.76	29.29	12.89	32
33	30.38	12.89	30.32	13.03	30.26	13.16	30.21	13.29	33
34	31.30	13.28	31.24	13.42	31.18	13.56	31.12	13.69	34
35	32.22	13.68	32.16	13.82	32.10	13.96	32.04	14.10	35
36	33.14	14.07	33.08	14.21	33.01	14.35	32.95	14.50	36
37	34.06	14.46	34.00	14.61	33.93	14.75	33.87	14.90	37
38	34.98	14.85	34.91	15.00	34.85	15.15	34.78	15.30	38
39	35.90	15.24	35.83	15.39	35.77	15.55	35.70	15.71	39
40	36.82	15.63	36.75	15.79	36.68	15.95	36.61	16.11	40
41	37.74	16.02	37.67	16.18	37.60	16.35	37.53	16.51	41
42	38.66	16.41	38.59	16.58	38.52	16.75	38.44	16.92	42
43	39.58	16.80	39.51	16.97	39.43	17.15	39.36	17.32	43
44	40.50	17.19	40.43	17.37	40.35	17.54	40.27	17.72	44
45	41.42	17.58	41.35	17.76	41.27	17.94	41.19	18.12	45
46	42.34	17.97	42.26	18.16	42.18	18.34	42.10	18.53	46
47	43.26	18.36	43.18	18.55	43.10	18.74	43.02	18.93	47
48	44.18	18.76	44.10	18.95	44.02	19.14	43.93	19.33	48
49	45.10	19.15	45.02	19.34	44.94	19.54	44.85	19.73	49
50	46.03	19.54	45.94	19.74	45.85	19.94	45.77	20.14	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	67 Deg		66 $\frac{3}{4}$ Deg.		66 $\frac{1}{2}$ Deg.		66 $\frac{1}{4}$ Deg.		

Distance.	23 Deg.		23 $\frac{1}{4}$ Deg.		23 $\frac{1}{2}$ Deg.		23 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	46.95	19.93	46.86	20.13	46.77	20.34	46.68	20.54	51
52	47.87	20.32	47.78	20.53	47.69	20.73	47.60	20.94	52
53	48.79	20.71	48.70	20.92	48.60	21.13	48.51	21.35	53
54	49.71	21.10	49.61	21.32	49.52	21.53	49.43	21.75	54
55	50.63	21.49	50.53	21.71	50.44	21.93	50.34	22.15	55
56	51.55	21.88	51.45	22.11	51.36	22.33	51.26	22.55	56
57	52.47	22.27	52.37	22.50	52.27	22.73	52.17	22.96	57
58	53.39	22.66	53.29	22.90	53.19	23.13	53.09	23.36	58
59	54.31	23.05	54.21	23.29	54.11	23.53	54.00	23.76	59
60	55.23	23.44	55.13	23.68	55.02	23.92	54.92	24.16	60
61	56.15	23.83	56.05	24.03	55.94	24.32	55.83	24.57	61
62	57.07	24.23	56.97	24.47	56.86	24.72	56.75	24.97	62
63	57.99	24.62	57.88	24.87	57.77	25.12	57.66	25.37	63
64	58.91	25.01	58.80	25.26	58.69	25.52	58.58	25.78	64
65	59.83	25.40	59.72	25.66	59.61	25.92	59.50	26.18	65
66	60.75	25.79	60.64	26.05	60.53	26.32	60.41	26.58	66
67	61.67	26.18	61.56	26.45	61.44	26.72	61.33	26.98	67
68	62.59	26.57	62.48	26.84	62.36	27.11	62.24	27.39	68
69	63.51	26.96	63.40	27.24	63.28	27.51	63.16	27.79	69
70	64.44	27.35	64.32	27.63	64.19	27.91	64.07	28.19	70
71	65.36	27.74	65.23	28.03	65.11	28.31	64.99	28.59	71
72	66.28	28.13	66.15	28.42	66.03	28.71	65.90	29.00	72
73	67.20	28.52	67.07	28.82	66.95	29.11	66.82	29.40	73
74	68.12	28.91	67.99	29.21	67.86	29.51	67.73	29.80	74
75	69.04	29.30	68.91	29.61	68.78	29.91	68.65	30.21	75
76	69.96	29.70	69.83	30.00	69.70	30.30	69.56	30.61	76
77	70.88	30.09	70.75	30.40	70.61	30.70	70.48	31.01	77
78	71.80	30.48	71.67	30.79	71.53	31.10	71.39	31.41	78
79	72.72	30.87	72.58	31.18	72.45	31.50	72.31	31.82	79
80	73.64	31.26	73.50	31.58	73.36	31.90	73.22	32.22	80
81	74.56	31.65	74.42	31.97	74.28	32.30	74.14	32.62	81
82	75.48	32.04	75.34	32.37	75.20	32.70	75.06	33.03	82
83	76.40	32.43	76.26	32.76	76.12	33.10	75.97	33.43	83
84	77.32	32.82	77.18	33.16	77.03	33.49	76.89	33.83	84
85	78.24	33.21	78.10	33.55	77.95	33.89	77.80	34.23	85
86	79.16	33.60	79.02	33.95	78.87	34.29	78.72	34.64	86
87	80.08	33.99	79.93	34.34	79.78	34.69	79.63	35.04	87
88	81.00	34.38	80.85	34.74	80.70	35.09	80.55	35.44	88
89	81.92	34.78	81.77	35.13	81.62	35.49	81.46	35.84	89
90	82.85	35.17	82.69	35.53	82.54	35.89	82.38	36.25	90
91	83.77	35.56	83.61	35.92	83.45	36.29	83.29	36.65	91
92	84.69	35.95	84.53	36.32	84.37	36.68	84.21	37.05	92
93	85.61	36.34	85.45	36.71	85.29	37.08	85.12	37.46	93
94	86.53	36.73	86.37	37.11	86.20	37.48	86.04	37.86	94
95	87.45	37.12	87.29	37.50	87.12	37.88	86.95	38.26	95
96	88.37	37.51	88.20	37.90	88.04	38.28	87.87	38.66	96
97	89.29	37.90	89.12	38.29	88.95	38.68	88.79	39.07	97
98	90.21	38.29	90.04	38.68	89.87	39.08	89.70	39.47	98
99	91.13	38.68	90.96	39.08	90.79	39.48	90.62	39.87	99
100	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	67 Deg.		66 $\frac{3}{4}$ Deg.		66 $\frac{1}{2}$ Deg.		66 $\frac{1}{4}$ Deg.		

Distance.	24 Deg.		24 $\frac{1}{4}$ Deg.		24 $\frac{1}{2}$ Deg.		24 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.91	0.41	0.91	0.41	0.91	0.41	0.91	0.42	1
2	1.83	0.81	1.82	0.82	1.82	0.83	1.82	0.84	2
3	2.74	1.22	2.74	1.23	2.73	1.24	2.72	1.26	3
4	3.65	1.63	3.65	1.64	3.64	1.66	3.63	1.67	4
5	4.57	2.03	4.56	2.05	4.55	2.07	4.54	2.09	5
6	5.48	2.44	5.47	2.46	5.46	2.49	5.45	2.51	6
7	6.39	2.85	6.38	2.87	6.37	2.90	6.36	2.93	7
8	7.31	3.25	7.29	3.29	7.28	3.32	7.27	3.35	8
9	8.22	3.66	8.21	3.70	8.19	3.73	8.17	3.77	9
10	9.14	4.07	9.12	4.11	9.10	4.15	9.08	4.19	10
11	10.05	4.47	10.03	4.52	10.01	4.56	9.99	4.61	11
12	10.96	4.88	10.94	4.93	10.92	4.98	10.90	5.02	12
13	11.88	5.29	11.85	5.34	11.83	5.39	11.81	5.44	13
14	12.79	5.69	12.76	5.75	12.74	5.81	12.71	5.86	14
15	13.70	6.10	13.68	6.16	13.65	6.22	13.62	6.28	15
16	14.62	6.51	14.59	6.57	14.56	6.64	14.53	6.70	16
17	15.53	6.92	15.50	6.98	15.47	7.05	15.44	7.12	17
18	16.44	7.32	16.41	7.39	16.38	7.46	16.35	7.54	18
19	17.36	7.73	17.32	7.80	17.29	7.88	17.25	7.95	19
20	18.27	8.13	18.24	8.21	18.20	8.29	18.16	8.37	20
21	19.18	8.54	19.15	8.63	19.11	8.71	19.07	8.79	21
22	20.10	8.95	20.06	9.04	20.02	9.12	19.98	9.21	22
23	21.01	9.35	20.97	9.45	20.93	9.54	20.89	9.63	23
24	21.93	9.76	21.88	9.86	21.84	9.95	21.80	10.05	24
25	22.84	10.17	22.79	10.27	22.75	10.37	22.70	10.47	25
26	23.75	10.58	23.71	10.68	23.66	10.78	23.61	10.89	26
27	24.67	10.98	24.62	11.09	24.57	11.20	24.52	11.30	27
28	25.58	11.39	25.53	11.50	25.48	11.61	25.43	11.72	28
29	26.49	11.80	26.44	11.91	26.39	12.03	26.34	12.14	29
30	27.41	12.20	27.35	12.32	27.30	12.44	27.24	12.56	30
31	28.32	12.61	28.26	12.73	28.21	12.86	28.15	12.98	31
32	29.23	13.02	29.18	13.14	29.12	13.27	29.06	13.40	32
33	30.15	13.42	30.09	13.55	30.03	13.68	29.97	13.82	33
34	31.06	13.83	31.00	13.96	30.94	14.10	30.88	14.23	34
35	31.97	14.24	31.91	14.38	31.85	14.51	31.78	14.65	35
36	32.89	14.64	32.82	14.79	32.76	14.93	32.69	15.07	36
37	33.80	15.05	33.74	15.20	33.67	15.34	33.60	15.49	37
38	34.71	15.46	34.65	15.61	34.58	15.76	34.51	15.91	38
39	35.63	15.86	35.56	16.02	35.49	16.17	35.42	16.33	39
40	36.54	16.27	36.47	16.43	36.40	16.59	36.33	16.75	40
41	37.46	16.68	37.38	16.84	37.31	17.00	37.23	17.16	41
42	38.37	17.08	38.29	17.25	38.22	17.42	38.14	17.58	42
43	39.28	17.49	39.21	17.66	39.13	17.83	39.05	18.00	43
44	40.20	17.90	40.12	18.07	40.04	18.25	39.96	18.42	44
45	41.11	18.30	41.03	18.48	40.95	18.66	40.87	18.84	45
46	42.02	18.71	41.94	18.89	41.86	19.08	41.77	19.26	46
47	42.94	19.12	42.85	19.30	42.77	19.49	42.68	19.68	47
48	43.85	19.52	43.76	19.71	43.68	19.91	43.59	20.10	48
49	44.76	19.93	44.68	20.13	44.59	20.32	44.50	20.51	49
50	45.68	20.34	45.59	20.54	45.50	20.73	45.41	20.93	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	66 Deg.		65 $\frac{3}{4}$ Deg.		65 $\frac{1}{2}$ Deg.		65 $\frac{1}{4}$ Deg.		

Distance.	24 Deg.		24 $\frac{1}{4}$ Deg.		24 $\frac{1}{2}$ Deg.		24 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	46.59	20.74	46.50	20.95	46.41	21.15	46.32	21.35	51
52	47.50	21.15	47.41	21.36	47.32	21.56	47.22	21.77	52
53	48.42	21.56	48.32	21.77	48.23	21.98	48.13	22.19	53
54	49.33	21.96	49.24	22.18	49.14	22.39	49.04	22.61	54
55	50.24	22.37	50.15	22.59	50.05	22.81	49.95	23.03	55
56	51.16	22.78	51.06	23.00	50.96	23.22	50.86	23.44	56
57	52.07	23.18	51.97	23.41	51.87	23.64	51.76	23.86	57
58	52.99	23.59	52.88	23.82	52.78	24.05	52.67	24.28	58
59	53.90	24.00	53.79	24.23	53.69	24.47	53.58	24.70	59
60	54.81	24.40	54.71	24.64	54.60	24.88	54.49	25.12	60
61	55.73	24.81	55.62	25.05	55.51	25.30	55.40	25.54	61
62	56.64	25.22	56.53	25.46	56.42	25.71	56.30	25.96	62
63	57.55	25.62	57.44	25.88	57.33	26.13	57.21	26.38	63
64	58.47	26.03	58.35	26.29	58.24	26.54	58.12	26.79	64
65	59.38	26.44	59.26	26.70	59.15	26.96	59.03	27.21	65
66	60.29	26.84	60.18	27.11	60.06	27.37	59.94	27.63	66
67	61.21	27.25	61.09	27.52	60.97	27.78	60.85	28.05	67
68	62.12	27.66	62.00	27.93	61.88	28.20	61.75	28.47	68
69	63.03	28.06	62.91	28.34	62.79	28.61	62.66	28.89	69
70	63.95	28.47	63.82	28.75	63.70	29.03	63.57	29.31	70
71	64.86	28.88	64.74	29.16	64.61	29.44	64.48	29.72	71
72	65.78	29.28	65.65	29.57	65.52	29.86	65.39	30.14	72
73	66.69	29.69	66.56	29.98	66.43	30.27	66.29	30.56	73
74	67.60	30.10	67.47	30.39	67.34	30.69	67.20	30.98	74
75	68.52	30.51	68.38	30.80	68.25	31.10	68.11	31.40	75
76	69.43	30.91	69.29	31.21	69.16	31.52	69.02	31.82	76
77	70.34	31.32	70.21	31.63	70.07	31.93	69.93	32.24	77
78	71.26	31.73	71.12	32.04	70.98	32.35	70.84	32.66	78
79	72.17	32.13	72.03	32.45	71.89	32.76	71.74	33.07	79
80	73.08	32.54	72.94	32.86	72.80	33.18	72.65	33.49	80
81	74.00	32.95	73.85	33.27	73.71	33.59	73.56	33.91	81
82	74.91	33.35	74.76	33.68	74.62	34.00	74.47	34.33	82
83	75.82	33.76	75.68	34.09	75.53	34.42	75.38	34.75	83
84	76.74	34.17	76.59	34.50	76.44	34.83	76.28	35.17	84
85	77.65	34.57	77.50	34.91	77.35	35.25	77.19	35.59	85
86	78.56	34.98	78.41	35.32	78.26	35.66	78.10	36.00	86
87	79.48	35.39	79.32	35.73	79.17	36.08	79.01	36.42	87
88	80.39	35.79	80.24	36.14	80.08	36.49	79.92	36.84	88
89	81.31	36.20	81.15	36.55	80.99	36.91	80.82	37.26	89
90	82.22	36.61	82.06	36.96	81.90	37.32	81.73	37.68	90
91	83.13	37.01	82.97	37.38	82.81	37.74	82.64	38.10	91
92	84.05	37.42	83.88	37.79	83.72	38.15	83.55	38.52	92
93	84.96	37.83	84.79	38.20	84.63	38.57	84.46	38.94	93
94	85.87	38.23	85.71	38.61	85.54	38.98	85.37	39.35	94
95	86.79	38.64	86.62	39.02	86.45	39.40	86.27	39.77	95
96	87.70	39.05	87.53	39.43	87.36	39.81	87.18	40.19	96
97	88.61	39.45	88.44	39.84	88.27	40.23	88.09	40.61	97
98	89.53	39.86	89.35	40.25	89.18	40.64	89.00	41.03	98
99	90.44	40.27	90.26	40.66	90.09	41.05	89.91	41.45	99
100	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	66 Deg.		65 $\frac{3}{4}$ Deg.		65 $\frac{1}{2}$ Deg.		65 $\frac{1}{4}$ Deg.		

Distance.	25 Deg.		25 $\frac{1}{4}$ Deg.		25 $\frac{1}{2}$ Deg.		25 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.91	0.42	0.90	0.43	0.90	0.43	0.90	0.43	1
2	1.81	0.85	1.81	0.85	1.81	0.86	1.80	0.87	2
3	2.72	1.27	2.71	1.28	2.71	1.29	2.70	1.30	3
4	3.63	1.69	3.62	1.71	3.61	1.72	3.60	1.74	4
5	4.53	2.11	4.52	2.13	4.51	2.15	4.50	2.17	5
6	5.44	2.54	5.43	2.56	5.42	2.58	5.40	2.61	6
7	6.34	2.96	6.33	2.99	6.32	3.01	6.30	3.04	7
8	7.25	3.38	7.24	3.41	7.22	3.44	7.21	3.48	8
9	8.16	3.80	8.14	3.84	8.12	3.87	8.11	3.91	9
10	9.06	4.23	9.04	4.27	9.03	4.31	9.01	4.34	10
11	9.97	4.65	9.95	4.69	9.93	4.74	9.91	4.78	11
12	10.88	5.07	10.85	5.12	10.83	5.17	10.81	5.21	12
13	11.78	5.49	11.76	5.55	11.73	5.60	11.71	5.65	13
14	12.69	5.92	12.66	5.97	12.64	6.03	12.61	6.08	14
15	13.59	6.34	13.57	6.40	13.54	6.46	13.51	6.52	15
16	14.50	6.76	14.47	6.83	14.44	6.89	14.41	6.95	16
17	15.41	7.18	15.38	7.25	15.34	7.32	15.31	7.39	17
18	16.31	7.61	16.28	7.68	16.25	7.75	16.21	7.82	18
19	17.22	8.03	17.18	8.10	17.15	8.18	17.11	8.25	19
20	18.13	8.45	18.09	8.53	18.05	8.61	18.01	8.69	20
21	19.03	8.87	18.99	8.96	18.95	9.04	18.91	9.12	21
22	19.94	9.30	19.90	9.38	19.86	9.47	19.82	9.56	22
23	20.85	9.72	20.80	9.81	20.76	9.90	20.72	9.99	23
24	21.75	10.14	21.71	10.24	21.66	10.33	21.62	10.43	24
25	22.66	10.57	22.61	10.66	22.56	10.76	22.52	10.86	25
26	23.56	10.99	23.52	11.09	23.47	11.19	23.42	11.30	26
27	24.47	11.41	24.42	11.52	24.37	11.62	24.32	11.73	27
28	25.38	11.83	25.32	11.94	25.27	12.05	25.22	12.16	28
29	26.28	12.26	26.23	12.37	26.17	12.48	26.12	12.60	29
30	27.19	12.68	27.13	12.80	27.08	12.92	27.02	13.03	30
31	28.10	13.10	28.04	13.22	27.98	13.35	27.92	13.47	31
32	29.00	13.52	28.94	13.65	28.88	13.78	28.82	13.90	32
33	29.91	13.95	29.85	14.08	29.79	14.21	29.72	14.34	33
34	30.81	14.37	30.75	14.50	30.69	14.64	30.62	14.77	34
35	31.72	14.79	31.66	14.93	31.59	15.07	31.52	15.21	35
36	32.63	15.21	32.56	15.36	32.49	15.50	32.43	15.64	36
37	33.53	15.64	33.46	15.78	33.40	15.93	33.33	16.07	37
38	34.44	16.06	34.37	16.21	34.30	16.36	34.23	16.51	38
39	35.35	16.48	35.27	16.64	35.20	16.79	35.13	16.94	39
40	36.25	16.90	36.18	17.06	36.10	17.22	36.03	17.38	40
41	37.16	17.33	37.08	17.49	37.01	17.65	36.93	17.81	41
42	38.06	17.75	37.99	17.92	37.91	18.08	37.83	18.25	42
43	38.97	18.17	38.89	18.34	38.81	18.51	38.73	18.68	43
44	39.88	18.60	39.80	18.77	39.71	18.94	39.63	19.12	44
45	40.78	19.02	40.70	19.20	40.62	19.37	40.53	19.55	45
46	41.69	19.44	41.60	19.62	41.52	19.80	41.43	19.98	46
47	42.60	19.86	42.51	20.05	42.42	20.23	42.33	20.42	47
48	43.50	20.29	43.41	20.48	43.32	20.66	43.23	20.85	48
49	44.41	20.71	44.32	20.90	44.23	21.10	44.13	21.29	49
50	45.32	21.13	45.22	21.33	45.13	21.53	45.03	21.72	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	65 Deg.		64 $\frac{3}{4}$ Deg.		64 $\frac{1}{2}$ Deg.		64 $\frac{1}{4}$ Deg.		

Distance.	25 Deg.		25½ Deg.		25¾ Deg.		25¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	46.22	21.55	46.13	21.75	46.03	21.96	45.94	22.16	51
52	47.13	21.98	47.03	22.18	46.93	22.39	46.84	22.59	52
53	48.03	22.40	47.94	22.61	47.84	22.82	47.74	23.03	53
54	48.94	22.82	48.84	23.03	48.74	23.25	48.64	23.46	54
55	49.85	23.24	49.74	23.46	49.64	23.68	49.54	23.89	55
56	50.75	23.67	50.65	23.89	50.54	24.11	50.44	24.33	56
57	51.66	24.09	51.55	24.31	51.45	24.54	51.34	24.76	57
58	52.57	24.51	52.46	24.74	52.35	24.97	52.24	25.20	58
59	53.47	24.93	53.36	25.17	53.25	25.40	53.14	25.63	59
60	54.38	25.36	54.27	25.59	54.16	25.83	54.04	26.07	60
61	55.28	25.78	55.17	26.02	55.06	26.26	54.94	26.50	61
62	56.19	26.20	56.08	26.45	55.96	26.69	55.84	26.91	62
63	57.10	26.62	56.98	26.87	56.86	27.12	56.74	27.37	63
64	58.00	27.05	57.89	27.30	57.77	27.55	57.64	27.80	64
65	58.91	27.47	58.79	27.73	58.67	27.98	58.55	28.24	65
66	59.82	27.89	59.69	28.15	59.57	28.41	59.45	28.67	66
67	60.72	28.32	60.60	28.58	60.47	28.84	60.35	29.11	67
68	61.63	28.74	61.50	29.01	61.38	29.27	61.25	29.54	68
69	62.54	29.16	62.41	29.43	62.28	29.71	62.15	29.98	69
70	63.44	29.58	63.31	29.86	63.18	30.14	63.05	30.41	70
71	64.35	30.01	64.22	30.29	64.08	30.57	63.95	30.85	71
72	65.25	30.43	65.12	30.71	64.99	31.00	64.85	31.28	72
73	66.16	30.85	66.03	31.14	65.89	31.43	65.75	31.71	73
74	67.07	31.27	66.93	31.57	66.79	31.86	66.65	32.15	74
75	67.97	31.70	67.83	31.99	67.69	32.29	67.55	32.58	75
76	68.88	32.12	68.74	32.42	68.60	32.72	68.45	33.02	76
77	69.79	32.54	69.64	32.85	69.50	33.15	69.35	33.45	77
78	70.69	32.96	70.55	33.27	70.40	33.58	70.25	33.89	78
79	71.60	33.39	71.45	33.70	71.30	34.01	71.16	34.32	79
80	72.50	33.81	72.36	34.13	72.21	34.44	72.06	34.76	80
81	73.41	34.23	73.26	34.55	73.11	34.87	72.96	35.19	81
82	74.32	34.65	74.17	34.98	74.01	35.30	73.86	35.62	82
83	75.22	35.08	75.07	35.41	74.91	35.73	74.76	36.06	83
84	76.13	35.50	75.97	35.83	75.82	36.16	75.66	36.49	84
85	77.04	35.92	76.88	36.26	76.72	36.59	76.56	36.93	85
86	77.94	36.35	77.78	36.68	77.62	37.02	77.46	37.36	86
87	78.85	36.77	78.69	37.11	78.52	37.45	78.36	37.80	87
88	79.76	37.19	79.59	37.54	79.43	37.88	79.26	38.23	88
89	80.66	37.61	80.50	37.96	80.33	38.32	80.16	38.67	89
90	81.57	38.04	81.40	38.39	81.23	38.75	81.06	39.10	90
91	82.47	38.46	82.31	38.82	82.14	39.18	81.96	39.53	91
92	83.38	38.88	83.21	39.24	83.04	39.61	82.86	39.97	92
93	84.29	39.30	84.11	39.67	83.94	40.04	83.76	40.40	93
94	85.19	39.73	85.02	40.10	84.84	40.47	84.67	40.84	94
95	86.10	40.15	85.92	40.52	85.75	40.90	85.57	41.27	95
96	87.01	40.57	86.83	40.95	86.65	41.33	86.47	41.71	96
97	87.91	40.99	87.73	41.38	87.55	41.76	87.37	42.14	97
98	88.82	41.42	88.64	41.80	88.45	42.19	88.27	42.58	98
99	89.72	41.84	89.54	42.23	89.36	42.62	89.17	43.01	99
100	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	65 Deg.		64¾ Deg.		64½ Deg.		64¼ Deg.		

TRAVERSE TABLE.

Distance.	26 Deg.		26¼ Deg.		26½ Deg.		26¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.90	0.44	0.90	0.44	0.89	0.45	0.89	0.45	1
2	1.80	0.88	1.79	0.88	1.79	0.89	1.79	0.90	2
3	2.70	1.32	2.69	1.33	2.68	1.34	2.68	1.35	3
4	3.60	1.75	3.59	1.77	3.58	1.78	3.57	1.80	4
5	4.49	2.19	4.48	2.21	4.47	2.23	4.46	2.25	5
6	5.39	2.63	5.38	2.65	5.37	2.63	5.36	2.70	6
7	6.29	3.07	6.28	3.10	6.26	3.12	6.25	3.15	7
8	7.19	3.51	7.17	3.54	7.16	3.57	7.14	3.60	8
9	8.09	3.95	8.07	3.98	8.05	4.02	8.04	4.05	9
10	8.99	4.38	8.97	4.42	8.95	4.46	8.93	4.50	10
11	9.89	4.82	9.87	4.87	9.84	4.91	9.82	4.95	11
12	10.79	5.26	10.76	5.31	10.74	5.35	10.72	5.40	12
13	11.68	5.70	11.66	5.75	11.63	5.80	11.61	5.85	13
14	12.58	6.14	12.56	6.19	12.53	6.25	12.50	6.30	14
15	13.48	6.58	13.45	6.63	13.42	6.69	13.39	6.75	15
16	14.38	7.01	14.35	7.08	14.32	7.14	14.29	7.20	16
17	15.28	7.45	15.25	7.52	15.21	7.59	15.18	7.65	17
18	16.18	7.89	16.14	7.96	16.11	8.03	16.07	8.10	18
19	17.08	8.33	17.04	8.40	17.00	8.48	16.97	8.55	19
20	17.98	8.77	17.94	8.85	17.90	8.92	17.86	9.00	20
21	18.87	9.21	18.83	9.29	18.79	9.37	18.75	9.45	21
22	19.77	9.64	19.73	9.73	19.69	9.82	19.65	9.90	22
23	20.67	10.08	20.63	10.17	20.58	10.26	20.54	10.35	23
24	21.57	10.52	21.52	10.61	21.48	10.71	21.43	10.80	24
25	22.47	10.96	22.42	11.06	22.37	11.15	22.32	11.25	25
26	23.37	11.40	23.32	11.50	23.27	11.60	23.22	11.70	26
27	24.27	11.84	24.22	11.94	24.16	12.05	24.11	12.15	27
28	25.17	12.27	25.11	12.38	25.06	12.49	25.00	12.60	28
29	26.06	12.71	26.01	12.83	25.95	12.94	25.90	13.05	29
30	26.96	13.15	26.91	13.27	26.85	13.39	26.79	13.50	30
31	27.86	13.59	27.80	13.71	27.74	13.83	27.68	13.95	31
32	28.76	14.03	28.70	14.15	28.64	14.28	28.58	14.40	32
33	29.66	14.47	29.60	14.60	29.53	14.72	29.47	14.85	33
34	30.56	14.90	30.49	15.04	30.43	15.17	30.36	15.30	34
35	31.46	15.34	31.39	15.48	31.32	15.62	31.25	15.75	35
36	32.36	15.78	32.29	15.92	32.22	16.06	32.15	16.20	36
37	33.26	16.22	33.18	16.36	33.11	16.51	33.04	16.65	37
38	34.15	16.66	34.08	16.81	34.01	16.96	33.93	17.10	38
39	35.05	17.10	34.98	17.25	34.90	17.40	34.83	17.55	39
40	35.95	17.53	35.87	17.69	35.80	17.85	35.72	18.00	40
41	36.85	17.97	36.77	18.13	36.69	18.29	36.61	18.45	41
42	37.75	18.41	37.67	18.58	37.59	18.74	37.51	18.90	42
43	38.65	18.85	38.57	19.02	38.48	19.19	38.40	19.35	43
44	39.55	19.29	39.46	19.46	39.38	19.63	39.29	19.80	44
45	40.45	19.73	40.36	19.90	40.27	20.08	40.18	20.25	45
46	41.34	20.17	41.26	20.35	41.17	20.53	41.08	20.70	46
47	42.24	20.60	42.15	20.79	42.06	20.97	41.97	21.15	47
48	43.14	21.04	43.05	21.23	42.96	21.42	42.86	21.60	48
49	44.04	21.48	43.95	21.67	43.85	21.86	43.76	22.05	49
50	44.94	21.92	44.84	22.11	44.75	22.31	44.65	22.50	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	64 Deg.		63¾ Deg.		63½ Deg.		63¼ Deg.		



Distance.	26 Deg.		26¼ Deg.		26½ Deg.		26¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	45.84	22.36	45.74	22.56	45.64	22.76	45.54	22.96	51
52	46.74	22.80	46.64	23.00	46.54	23.20	46.43	23.41	52
53	47.64	23.23	47.53	23.44	47.43	23.65	47.33	23.86	53
54	48.53	23.67	48.43	23.88	48.33	24.09	48.22	24.31	54
55	49.43	24.11	49.33	24.33	49.22	24.54	49.11	24.76	55
56	50.33	24.55	50.22	24.77	50.12	24.99	50.01	25.21	56
57	51.23	24.99	51.12	25.21	51.01	25.43	50.90	25.66	57
58	52.13	25.43	52.02	25.65	51.91	25.88	51.79	26.11	58
59	53.03	25.86	52.92	26.09	52.80	26.33	52.69	26.56	59
60	53.93	26.30	53.81	26.54	53.70	26.77	53.58	27.01	60
61	54.83	26.74	54.71	26.98	54.59	27.22	54.47	27.46	61
62	55.73	27.18	55.61	27.42	55.49	27.66	55.36	27.91	62
63	56.62	27.62	56.50	27.86	56.38	28.11	56.26	28.36	63
64	57.52	28.06	57.40	28.31	57.28	28.56	57.15	28.81	64
65	58.42	28.49	58.30	28.75	58.17	29.00	58.04	29.26	65
66	59.32	28.93	59.19	29.19	59.07	29.45	58.94	29.71	66
67	60.22	29.37	60.09	29.63	59.96	29.90	59.83	30.16	67
68	61.12	29.81	60.99	30.08	60.86	30.34	60.72	30.61	68
69	62.02	30.25	61.88	30.52	61.75	30.79	61.62	31.06	69
70	62.92	30.69	62.78	30.96	62.65	31.23	62.51	31.51	70
71	63.81	31.12	63.68	31.40	63.54	31.68	63.40	31.96	71
72	64.71	31.56	64.57	31.84	64.44	32.13	64.29	32.41	72
73	65.61	32.00	65.47	32.29	65.33	32.57	65.19	32.86	73
74	66.51	32.44	66.37	32.73	66.23	33.02	66.08	33.31	74
75	67.41	32.88	67.27	33.17	67.12	33.46	66.97	33.76	75
76	68.31	33.32	68.16	33.61	68.01	33.91	67.87	34.21	76
77	69.21	33.75	69.06	34.06	68.91	34.36	68.76	34.66	77
78	70.11	34.19	69.96	34.50	69.80	34.80	69.65	35.11	78
79	71.00	34.63	70.85	34.94	70.70	35.25	70.55	35.56	79
80	71.90	35.07	71.75	35.38	71.59	35.70	71.44	36.01	80
81	72.80	35.51	72.65	35.83	72.49	36.14	72.33	36.46	81
82	73.70	35.95	73.54	36.27	73.38	36.59	73.22	36.91	82
83	74.60	36.38	74.44	36.71	74.28	37.03	74.12	37.36	83
84	75.50	36.82	75.34	37.15	75.17	37.48	75.01	37.81	84
85	76.40	37.26	76.23	37.59	76.07	37.93	75.90	38.26	85
86	77.30	37.70	77.13	38.04	76.96	38.37	76.80	38.71	86
87	78.20	38.14	78.03	38.48	77.86	38.82	77.69	39.16	87
88	79.09	38.58	78.92	38.92	78.75	39.27	78.58	39.61	88
89	79.99	39.01	79.82	39.36	79.65	39.71	79.48	40.06	89
90	80.89	39.45	80.72	39.81	80.54	40.16	80.37	40.51	90
91	81.79	39.89	81.62	40.25	81.44	40.60	81.26	40.96	91
92	82.69	40.33	82.51	40.69	82.33	41.05	82.15	41.41	92
93	83.59	40.77	83.41	41.13	83.23	41.50	83.05	41.86	93
94	84.49	41.21	84.31	41.58	84.12	41.94	83.94	42.31	94
95	85.39	41.65	85.20	42.02	85.02	42.39	84.83	42.76	95
96	86.28	42.08	86.10	42.46	85.91	42.83	85.73	43.21	96
97	87.18	42.52	87.00	42.90	86.81	43.28	86.62	43.66	97
98	88.08	42.96	87.89	43.34	87.70	43.73	87.51	44.11	98
99	88.98	43.40	88.79	43.79	88.60	44.17	88.40	44.56	99
100	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	64 Deg.		63¾ Deg.		63½ Deg.		63¼ Deg.		

Distance.	27 Deg.		27 $\frac{1}{4}$ Deg.		27 $\frac{1}{2}$ Deg.		27 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.89	0.45	0.89	0.46	0.89	0.46	0.88	0.47	1
2	1.78	0.91	1.78	0.92	1.77	0.92	1.77	0.93	2
3	2.67	1.36	2.67	1.37	2.66	1.39	2.65	1.40	3
4	3.56	1.82	3.56	1.83	3.55	1.85	3.54	1.86	4
5	4.45	2.27	4.45	2.29	4.44	2.31	4.42	2.33	5
6	5.35	2.72	5.33	2.75	5.32	2.77	5.31	2.79	6
7	6.24	3.18	6.22	3.21	6.21	3.23	6.19	3.26	7
8	7.13	3.63	7.11	3.66	7.10	3.69	7.08	3.72	8
9	8.02	4.09	8.00	4.12	7.98	4.16	7.96	4.19	9
10	8.91	4.54	8.89	4.58	8.87	4.62	8.85	4.66	10
11	9.80	4.99	9.78	5.04	9.76	5.08	9.73	5.12	11
12	10.69	5.45	10.67	5.49	10.64	5.54	10.62	5.59	12
13	11.58	5.90	11.56	5.95	11.53	6.00	11.50	6.05	13
14	12.47	6.36	12.45	6.41	12.42	6.46	12.39	6.52	14
15	13.37	6.81	13.34	6.87	13.31	6.93	13.27	6.98	15
16	14.26	7.26	14.22	7.33	14.19	7.39	14.16	7.45	16
17	15.15	7.72	15.11	7.78	15.08	7.85	15.04	7.92	17
18	16.04	8.17	16.00	8.24	15.97	8.31	15.93	8.38	18
19	16.93	8.63	16.89	8.70	16.85	8.77	16.81	8.85	19
20	17.82	9.08	17.78	9.16	17.74	9.23	17.70	9.31	20
21	18.71	9.53	18.67	9.62	18.63	9.70	18.58	9.78	21
22	19.60	9.99	19.56	10.07	19.51	10.16	19.47	10.24	22
23	20.49	10.44	20.45	10.53	20.40	10.62	20.35	10.71	23
24	21.38	10.90	21.34	10.99	21.29	11.08	21.24	11.17	24
25	22.28	11.35	22.23	11.45	22.18	11.54	22.12	11.64	25
26	23.17	11.80	23.11	11.90	23.06	12.01	23.01	12.11	26
27	24.06	12.26	24.00	12.36	23.95	12.47	23.89	12.57	27
28	24.95	12.71	24.89	12.82	24.84	12.93	24.78	13.04	28
29	25.84	13.17	25.78	13.28	25.72	13.39	25.66	13.50	29
30	26.73	13.62	26.67	13.74	26.61	13.85	26.55	13.97	30
31	27.62	14.07	27.56	14.19	27.50	14.31	27.43	14.43	31
32	28.51	14.53	28.45	14.65	28.38	14.78	28.32	14.90	32
33	29.40	14.98	29.34	15.11	29.27	15.24	29.20	15.37	33
34	30.29	15.44	30.23	15.57	30.16	15.70	30.09	15.83	34
35	31.19	15.89	31.12	16.03	31.05	16.16	30.97	16.30	35
36	32.08	16.34	32.00	16.48	31.93	16.62	31.86	16.76	36
37	32.97	16.80	32.89	16.94	32.82	17.08	32.74	17.23	37
38	33.86	17.25	33.78	17.40	33.71	17.55	33.63	17.69	38
39	34.75	17.71	34.67	17.86	34.59	18.01	34.51	18.16	39
40	35.64	18.16	35.56	18.31	35.48	18.47	35.40	18.62	40
41	36.53	18.61	36.45	18.77	36.37	18.93	36.28	19.09	41
42	37.42	19.07	37.34	19.23	37.25	19.39	37.17	19.56	42
43	38.31	19.52	38.23	19.69	38.14	19.86	38.05	20.02	43
44	39.20	19.98	39.12	20.15	39.03	20.32	38.94	20.49	44
45	40.10	20.43	40.01	20.60	39.92	20.78	39.82	20.95	45
46	40.99	20.88	40.89	21.06	40.80	21.24	40.71	21.42	46
47	41.88	21.34	41.78	21.52	41.69	21.70	41.59	21.88	47
48	42.77	21.79	42.67	21.98	42.58	22.16	42.48	22.35	48
49	43.66	22.25	43.56	22.44	43.46	22.63	43.36	22.82	49
50	44.55	22.70	44.45	22.89	44.35	23.09	44.25	23.28	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	63 Deg.		62 $\frac{3}{4}$ Deg.		62 $\frac{1}{2}$ Deg.		62 $\frac{1}{4}$ Deg.		

Distance.	27 Deg.		27 $\frac{1}{4}$ Deg.		27 $\frac{1}{2}$ Deg.		27 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	45.44	23.15	45.34	23.35	45.24	23.55	45.13	23.75	51
52	46.33	23.61	46.23	23.81	46.12	24.01	46.02	24.21	52
53	47.22	24.06	47.12	24.27	47.01	24.47	46.90	24.68	53
54	48.11	24.52	48.01	24.73	47.90	24.93	47.79	25.14	54
55	49.01	24.97	48.90	25.18	48.79	25.40	48.67	25.61	55
56	49.90	25.42	49.78	25.64	49.67	25.86	49.56	26.07	56
57	50.79	25.88	50.67	26.10	50.56	26.32	50.44	26.54	57
58	51.68	26.33	51.56	26.56	51.45	26.78	51.33	27.01	58
59	52.57	26.79	52.45	27.01	52.33	27.24	52.21	27.47	59
60	53.46	27.24	53.34	27.47	53.22	27.70	53.10	27.94	60
61	54.35	27.69	54.23	27.93	54.11	28.17	53.98	28.40	61
62	55.24	28.15	55.12	28.39	54.99	28.63	54.87	28.87	62
63	56.13	28.60	56.01	28.85	55.88	29.09	55.75	29.33	63
64	57.02	29.06	56.90	29.30	56.77	29.55	56.64	29.80	64
65	57.92	29.51	57.79	29.76	57.66	30.01	57.52	30.26	65
66	58.81	29.96	58.68	30.22	58.54	30.48	58.41	30.73	66
67	59.70	30.42	59.56	30.68	59.43	30.94	59.29	31.20	67
68	60.59	30.87	60.45	31.14	60.32	31.40	60.18	31.66	68
69	61.48	31.33	61.34	31.59	61.20	31.86	61.06	32.13	69
70	62.37	31.78	62.23	32.05	62.09	32.32	61.95	32.59	70
71	63.26	32.23	63.12	32.51	62.98	32.78	62.83	33.06	71
72	64.15	32.69	64.01	32.97	63.86	33.25	63.72	33.52	72
73	65.04	33.14	64.90	33.42	64.75	33.71	64.60	33.99	73
74	65.93	33.60	65.79	33.88	65.64	34.17	65.49	34.46	74
75	66.83	34.05	66.68	34.34	66.53	34.63	66.37	34.92	75
76	67.72	34.50	67.57	34.80	67.41	35.09	67.26	35.39	76
77	68.61	34.96	68.45	35.26	68.30	35.55	68.14	35.85	77
78	69.50	35.41	69.34	35.71	69.19	36.02	69.03	36.32	78
79	70.39	35.87	70.23	36.17	70.07	36.48	69.91	36.78	79
80	71.28	36.32	71.12	36.63	70.96	36.94	70.80	37.25	80
81	72.17	36.77	72.01	37.09	71.85	37.40	71.68	37.71	81
82	73.06	37.23	72.90	37.55	72.73	37.86	72.57	38.18	82
83	73.95	37.68	73.79	38.00	73.62	38.33	73.45	38.65	83
84	74.84	38.14	74.68	38.46	74.51	38.79	74.34	39.11	84
85	75.74	38.59	75.57	38.92	75.40	39.25	75.22	39.58	85
86	76.63	39.04	76.46	39.38	76.28	39.71	76.11	40.04	86
87	77.52	39.50	77.34	39.83	77.17	40.17	76.99	40.51	87
88	78.41	39.95	78.23	40.29	78.06	40.63	77.88	40.97	88
89	79.30	40.41	79.12	40.75	78.94	41.10	78.76	41.44	89
90	80.19	40.86	80.01	41.21	79.83	41.56	79.65	41.91	90
91	81.08	41.31	80.90	41.67	80.72	42.02	80.53	42.37	91
92	81.97	41.77	81.79	42.12	81.60	42.48	81.42	42.84	92
93	82.86	42.22	82.68	42.58	82.49	42.94	82.30	43.30	93
94	83.75	42.68	83.57	43.04	83.38	43.40	83.19	43.77	94
95	84.65	43.13	84.46	43.50	84.27	43.87	84.07	44.23	95
96	85.54	43.58	85.35	43.96	85.15	44.33	84.96	44.70	96
97	86.43	44.04	86.23	44.41	86.04	44.79	85.84	45.16	97
98	87.32	44.49	87.12	44.87	86.93	45.25	86.73	45.63	98
99	88.21	44.95	88.01	45.33	87.81	45.71	87.61	46.10	99
100	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	100

Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
		63 Deg.		62 $\frac{3}{4}$ Deg.		62 $\frac{1}{2}$ Deg.		62 $\frac{1}{4}$ Deg.	

Distance.	28 Deg.		28½ Deg.		28½ Deg.		28¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.88	0.47	0.88	0.47	0.88	0.48	0.88	0.48	1
2	1.77	0.94	1.76	0.95	1.76	0.95	1.75	0.96	2
3	2.65	1.41	2.64	1.42	2.64	1.43	2.63	1.44	3
4	3.53	1.88	3.52	1.89	3.52	1.91	3.51	1.92	4
5	4.41	2.35	4.40	2.37	4.39	2.39	4.38	2.40	5
6	5.30	2.82	5.29	2.84	5.27	2.86	5.26	2.89	6
7	6.18	3.29	6.17	3.31	6.15	3.34	6.14	3.37	7
8	7.06	3.76	7.05	3.79	7.03	3.82	7.01	3.85	8
9	7.95	4.23	7.93	4.26	7.91	4.29	7.89	4.33	9
10	8.83	4.69	8.81	4.73	8.79	4.77	8.77	4.81	10
11	9.71	5.16	9.69	5.21	9.67	5.25	9.64	5.29	11
12	10.60	5.63	10.57	5.68	10.55	5.73	10.52	5.77	12
13	11.48	6.10	11.45	6.15	11.42	6.20	11.40	6.25	13
14	12.36	6.57	12.33	6.63	12.30	6.68	12.27	6.73	14
15	13.24	7.04	13.21	7.10	13.18	7.16	13.15	7.21	15
16	14.13	7.51	14.09	7.57	14.06	7.63	14.03	7.70	16
17	15.01	7.98	14.98	8.05	14.94	8.11	14.90	8.18	17
18	15.89	8.45	15.86	8.52	15.82	8.59	15.78	8.66	18
19	16.78	8.92	16.74	8.99	16.70	9.07	16.66	9.14	19
20	17.66	9.39	17.62	9.47	17.58	9.54	17.53	9.62	20
21	18.54	9.86	18.50	9.94	18.46	10.02	18.41	10.10	21
22	19.42	10.33	19.38	10.41	19.33	10.50	19.29	10.58	22
23	20.31	10.80	20.26	10.89	20.21	10.97	20.16	11.06	23
24	21.19	11.27	21.14	11.36	21.09	11.45	21.04	11.54	24
25	22.07	11.74	22.02	11.83	21.97	11.93	21.92	12.02	25
26	22.96	12.21	22.90	12.31	22.85	12.41	22.79	12.51	26
27	23.84	12.68	23.78	12.78	23.73	12.88	23.67	12.99	27
28	24.72	13.15	24.66	13.25	24.61	13.36	24.55	13.47	28
29	25.61	13.61	25.55	13.73	25.49	13.84	25.43	13.95	29
30	26.49	14.08	26.43	14.20	26.36	14.31	26.30	14.43	30
31	27.37	14.55	27.31	14.67	27.24	14.79	27.18	14.91	31
32	28.25	15.02	28.19	15.15	28.12	15.27	28.06	15.39	32
33	29.14	15.49	29.07	15.62	29.00	15.75	28.93	15.87	33
34	30.02	15.96	29.95	16.09	29.88	16.22	29.81	16.35	34
35	30.90	16.43	30.83	16.57	30.76	16.70	30.69	16.83	35
36	31.79	16.90	31.71	17.04	31.64	17.18	31.56	17.32	36
37	32.67	17.37	32.59	17.51	32.52	17.65	32.44	17.80	37
38	33.55	17.84	33.47	17.99	33.39	18.13	33.32	18.28	38
39	34.43	18.31	34.35	18.46	34.27	18.61	34.19	18.76	39
40	35.32	18.78	35.24	18.93	35.15	19.09	35.07	19.24	40
41	36.20	19.25	36.12	19.41	36.03	19.56	35.95	19.72	41
42	37.08	19.72	37.00	19.88	36.91	20.04	36.82	20.20	42
43	37.97	20.19	37.88	20.35	37.79	20.52	37.70	20.68	43
44	38.85	20.66	38.76	20.83	38.67	20.99	38.58	21.16	44
45	39.73	21.13	39.64	21.30	39.55	21.47	39.45	21.64	45
46	40.62	21.60	40.52	21.77	40.43	21.95	40.33	22.13	46
47	41.50	22.07	41.40	22.25	41.30	22.43	41.21	22.61	47
48	42.38	22.53	42.28	22.72	42.18	22.90	42.08	23.09	48
49	43.26	23.00	43.16	23.19	43.06	23.38	42.96	23.57	49
50	44.15	23.47	44.04	23.67	43.94	23.86	43.84	24.05	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	62 Deg.		61¾ Deg.		61½ Deg.		61¼ Deg.		

Distance.	23 Deg.		23 $\frac{1}{4}$ Deg.		23 $\frac{1}{2}$ Deg.		23 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	45.03	23.94	44.93	24.14	44.82	24.34	44.71	24.53	51
52	45.91	24.41	45.81	24.61	45.70	24.81	45.59	25.01	52
53	46.80	24.88	46.69	25.09	46.58	25.29	46.47	25.49	53
54	47.68	25.35	47.57	25.56	47.46	25.77	47.34	25.97	54
55	48.56	25.82	48.45	26.03	48.33	26.24	48.22	26.45	55
56	49.45	26.29	49.33	26.51	49.21	26.72	49.10	26.94	56
57	50.33	26.76	50.21	26.98	50.09	27.20	49.97	27.42	57
58	51.21	27.23	51.09	27.45	50.97	27.68	50.85	27.90	58
59	52.09	27.70	51.97	27.93	51.85	28.15	51.73	28.38	59
60	52.93	28.17	52.85	28.40	52.73	28.63	52.60	28.86	60
61	53.86	28.64	53.73	28.87	53.61	29.11	53.48	29.34	61
62	54.74	29.11	54.62	29.35	54.49	29.58	54.36	29.82	62
63	55.63	29.58	55.50	29.82	55.37	30.06	55.23	30.30	63
64	56.51	30.05	56.38	30.29	56.24	30.54	56.11	30.78	64
65	57.39	30.52	57.26	30.77	57.12	31.02	56.99	31.26	65
66	58.27	30.99	58.14	31.24	58.00	31.49	57.86	31.75	66
67	59.16	31.45	59.02	31.71	58.88	31.97	58.74	32.23	67
68	60.04	31.92	59.90	32.19	59.76	32.45	59.62	32.71	68
69	60.92	32.39	60.78	32.66	60.64	32.92	60.49	33.19	69
70	61.81	32.86	61.66	33.13	61.52	33.40	61.37	33.67	70
71	62.69	33.33	62.54	33.61	62.40	33.88	62.25	34.15	71
72	63.57	33.80	63.42	34.08	63.27	34.36	63.12	34.63	72
73	64.46	34.27	64.30	34.55	64.15	34.83	64.00	35.11	73
74	65.34	34.74	65.19	35.03	65.03	35.31	64.88	35.59	74
75	66.22	35.21	66.07	35.50	65.91	35.79	65.75	36.07	75
76	67.10	35.68	66.95	35.97	66.79	36.26	66.63	36.56	76
77	67.99	36.15	67.83	36.45	67.67	36.74	67.51	37.04	77
78	68.87	36.62	68.71	36.92	68.55	37.22	68.38	37.52	78
79	69.75	37.09	69.59	37.39	69.43	37.70	69.26	38.00	79
80	70.64	37.56	70.47	37.87	70.31	38.17	70.14	38.48	80
81	71.52	38.03	71.35	38.34	71.18	38.65	71.01	38.96	81
82	72.40	38.50	72.23	38.81	72.06	39.13	71.89	39.44	82
83	73.28	38.97	73.11	39.29	72.94	39.60	72.77	39.92	83
84	74.17	39.44	73.99	39.76	73.82	40.08	73.64	40.40	84
85	75.05	39.91	74.88	40.23	74.70	40.56	74.52	40.88	85
86	75.93	40.37	75.76	40.71	75.58	41.04	75.40	41.36	86
87	76.82	40.84	76.64	41.18	76.46	41.51	76.28	41.85	87
88	77.70	41.31	77.52	41.65	77.34	41.99	77.15	42.33	88
89	78.58	41.78	78.40	42.13	78.21	42.47	78.03	42.81	89
90	79.47	42.25	79.28	42.60	79.09	42.94	78.91	43.29	90
91	80.35	42.72	80.16	43.07	79.97	43.42	79.78	43.77	91
92	81.23	43.19	81.04	43.55	80.85	43.90	80.66	44.25	92
93	82.11	43.66	81.92	44.02	81.73	44.38	81.54	44.73	93
94	83.00	44.13	82.80	44.49	82.61	44.85	82.41	45.21	94
95	83.88	44.60	83.68	44.97	83.49	45.33	83.29	45.69	95
96	84.76	45.07	84.57	45.44	84.37	45.81	84.17	46.17	96
97	85.65	45.54	85.45	45.91	85.25	46.28	85.04	46.66	97
98	86.53	46.01	86.33	46.39	86.12	46.76	85.92	47.14	98
99	87.41	46.48	87.21	46.86	87.00	47.24	86.80	47.62	99
100	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	62 Deg.		61 $\frac{3}{4}$ Deg.		61 $\frac{1}{2}$ Deg.		61 $\frac{1}{4}$ Deg.		

Distance.	29 Deg.		29 $\frac{1}{4}$ Deg.		29 $\frac{1}{2}$ Deg.		29 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.87	0.48	0.87	0.49	0.87	0.49	0.87	0.50	1
2	1.75	0.97	1.74	0.98	1.74	0.98	1.74	0.99	2
3	2.62	1.45	2.62	1.47	2.61	1.48	2.60	1.49	3
4	3.50	1.94	3.49	1.95	3.48	1.97	3.47	1.98	4
5	4.37	2.42	4.36	2.44	4.35	2.46	4.34	2.48	5
6	5.25	2.91	5.23	2.93	5.22	2.95	5.21	2.98	6
7	6.12	3.39	6.11	3.42	6.09	3.45	6.08	3.47	7
8	7.00	3.88	6.98	3.91	6.96	3.94	6.95	3.97	8
9	7.87	4.36	7.85	4.40	7.83	4.43	7.81	4.47	9
10	8.75	4.85	8.72	4.89	8.70	4.92	8.68	4.96	10
11	9.62	5.33	9.60	5.37	9.57	5.42	9.55	5.46	11
12	10.50	5.82	10.47	5.86	10.44	5.91	10.42	5.95	12
13	11.37	6.30	11.34	6.35	11.31	6.40	11.29	6.45	13
14	12.24	6.79	12.21	6.84	12.18	6.89	12.15	6.95	14
15	13.12	7.27	13.09	7.33	13.06	7.39	13.02	7.44	15
16	13.99	7.76	13.96	7.82	13.93	7.88	13.89	7.94	16
17	14.87	8.24	14.83	8.31	14.80	8.37	14.76	8.44	17
18	15.74	8.73	15.70	8.80	15.67	8.86	15.63	8.93	18
19	16.62	9.21	16.58	9.28	16.54	9.36	16.50	9.43	19
20	17.49	9.70	17.45	9.77	17.41	9.85	17.36	9.92	20
21	18.37	10.18	18.32	10.26	18.28	10.34	18.23	10.42	21
22	19.24	10.67	19.19	10.75	19.15	10.83	19.10	10.92	22
23	20.12	11.15	20.07	11.24	20.02	11.33	19.97	11.41	23
24	20.99	11.64	20.94	11.73	20.89	11.82	20.84	11.91	24
25	21.87	12.12	21.81	12.22	21.76	12.31	21.70	12.41	25
26	22.74	12.60	22.68	12.70	22.63	12.80	22.57	12.90	26
27	23.61	13.09	23.56	13.19	23.50	13.30	23.44	13.40	27
28	24.49	13.57	24.43	13.68	24.37	13.79	24.31	13.89	28
29	25.36	14.06	25.30	14.17	25.24	14.28	25.18	14.39	29
30	26.24	14.54	26.17	14.66	26.11	14.77	26.05	14.89	30
31	27.11	15.03	27.05	15.15	26.98	15.27	26.91	15.38	31
32	27.99	15.51	27.92	15.64	27.85	15.76	27.78	15.88	32
33	28.86	16.00	28.79	16.12	28.72	16.25	28.65	16.38	33
34	29.74	16.48	29.66	16.61	29.59	16.74	29.52	16.87	34
35	30.61	16.97	30.54	17.10	30.46	17.23	30.39	17.37	35
36	31.49	17.45	31.41	17.59	31.33	17.73	31.26	17.86	36
37	32.36	17.94	32.28	18.08	32.20	18.22	32.12	18.36	37
38	33.24	18.42	33.15	18.57	33.07	18.71	32.99	18.86	38
39	34.11	18.91	34.03	19.06	33.94	19.20	33.86	19.35	39
40	34.98	19.39	34.90	19.54	34.81	19.70	34.73	19.85	40
41	35.86	19.88	35.77	20.03	35.68	20.19	35.60	20.34	41
42	36.73	20.36	36.64	20.52	36.55	20.68	36.46	20.84	42
43	37.61	20.85	37.52	21.01	37.43	21.17	37.33	21.34	43
44	38.48	21.33	38.39	21.50	38.30	21.67	38.20	21.83	44
45	39.36	21.82	39.26	21.99	39.17	22.16	39.07	22.33	45
46	40.23	22.30	40.13	22.48	40.04	22.65	39.94	22.83	46
47	41.11	22.79	41.01	22.97	40.91	23.14	40.81	23.32	47
48	41.98	23.27	41.88	23.45	41.78	23.63	41.67	23.82	48
49	42.86	23.76	42.75	23.94	42.65	24.13	42.54	24.31	49
50	43.73	24.24	43.62	24.43	43.52	24.62	43.41	24.81	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	61 Deg.		60 $\frac{3}{4}$ Deg.		60 $\frac{1}{2}$ Deg.		60 $\frac{1}{4}$ Deg.		

Distance.	29 Deg.		29¼ Deg.		29½ Deg.		29¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	44.61	24.73	44.50	24.92	44.39	25.11	44.28	25.31	51
52	45.48	25.21	45.37	25.41	45.26	25.61	45.15	25.80	52
53	46.35	25.69	46.24	25.90	46.13	26.10	46.01	26.30	53
54	47.23	26.18	47.11	26.39	47.00	26.59	46.88	26.80	54
55	48.10	26.66	47.99	26.87	47.87	27.08	47.75	27.29	55
56	48.98	27.15	48.86	27.36	48.74	27.58	48.62	27.79	56
57	49.85	27.63	49.73	27.85	49.61	28.07	49.49	28.28	57
58	50.73	28.12	50.60	28.34	50.48	28.56	50.36	28.78	58
59	51.60	28.60	51.48	28.83	51.35	29.05	51.22	29.28	59
60	52.48	29.09	52.35	29.32	52.22	29.55	52.09	29.77	60
61	53.35	29.57	53.22	29.81	53.09	30.04	52.96	30.27	61
62	54.23	30.06	54.09	30.29	53.96	30.53	53.83	30.77	62
63	55.10	30.54	54.97	30.78	54.83	31.02	54.70	31.26	63
64	55.98	31.03	55.84	31.27	55.70	31.52	55.56	31.76	64
65	56.85	31.51	56.71	31.76	56.57	32.01	56.43	32.25	65
66	57.72	32.00	57.58	32.25	57.44	32.50	57.30	32.75	66
67	58.60	32.48	58.46	32.74	58.31	32.99	58.17	33.25	67
68	59.47	32.97	59.33	33.23	59.18	33.48	59.04	33.74	68
69	60.35	33.45	60.20	33.71	60.05	33.98	59.91	34.24	69
70	61.22	33.94	61.07	34.20	60.92	34.47	60.77	34.74	70
71	62.10	34.42	61.95	34.69	61.80	34.96	61.64	35.23	71
72	62.97	34.91	62.82	35.18	62.67	35.45	62.51	35.73	72
73	63.85	35.39	63.69	35.67	63.54	35.95	63.38	36.22	73
74	64.72	35.88	64.56	36.16	64.41	36.44	64.25	36.72	74
75	65.60	36.36	65.44	36.65	65.28	36.93	65.11	37.22	75
76	66.47	36.85	66.31	37.14	66.15	37.42	65.98	37.71	76
77	67.35	37.33	67.18	37.62	67.02	37.92	66.85	38.21	77
78	68.22	37.82	68.05	38.11	67.89	38.41	67.72	38.70	78
79	69.09	38.30	68.93	38.60	68.76	38.90	68.59	39.20	79
80	69.97	38.78	69.80	39.09	69.63	39.39	69.46	39.70	80
81	70.84	39.27	70.67	39.58	70.50	39.89	70.32	40.19	81
82	71.72	39.75	71.54	40.07	71.37	40.38	71.19	40.69	82
83	72.59	40.24	72.42	40.56	72.24	40.87	72.06	41.19	83
84	73.47	40.72	73.29	41.04	73.11	41.36	72.93	41.68	84
85	74.34	41.21	74.16	41.53	73.98	41.86	73.80	42.18	85
86	75.22	41.69	75.03	42.02	74.85	42.35	74.67	42.67	86
87	76.09	42.18	75.91	42.51	75.72	42.84	75.53	43.17	87
88	76.97	42.63	76.78	43.00	76.59	43.33	76.40	43.67	88
89	77.84	43.15	77.65	43.49	77.46	43.83	77.27	44.16	89
90	78.72	43.63	78.52	43.98	78.33	44.32	78.14	44.66	90
91	79.59	44.12	79.40	44.46	79.20	44.81	79.01	45.16	91
92	80.46	44.60	80.27	44.95	80.07	45.30	79.87	45.65	92
93	81.34	45.09	81.14	45.44	80.94	45.80	80.74	46.15	93
94	82.21	45.57	82.01	45.93	81.81	46.29	81.61	46.64	94
95	83.09	46.06	82.89	46.42	82.68	46.78	82.48	47.14	95
96	83.96	46.54	83.76	46.91	83.55	47.27	83.35	47.64	96
97	84.84	47.03	84.63	47.40	84.42	47.77	84.22	48.13	97
98	85.71	47.51	85.50	47.88	85.29	48.26	85.08	48.63	98
99	86.59	48.00	86.38	48.37	86.17	48.75	85.95	49.13	99
100	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	61 Deg.		60¾ Deg.		60½ Deg.		60¼ Deg.		

Distance.	30 Deg.		30¼ Deg.		30½ Deg.		30¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.87	0.50	0.86	0.50	0.86	0.51	0.86	0.51	1
2	1.73	1.00	1.73	1.01	1.72	1.02	1.72	1.02	2
3	2.60	1.50	2.59	1.51	2.58	1.52	2.58	1.53	3
4	3.46	2.00	3.46	2.02	3.45	2.03	3.44	2.05	4
5	4.33	2.50	4.32	2.52	4.31	2.54	4.30	2.56	5
6	5.20	3.00	5.18	3.02	5.17	3.05	5.16	3.07	6
7	6.06	3.50	6.05	3.53	6.03	3.55	6.02	3.58	7
8	6.93	4.00	6.91	4.03	6.89	4.06	6.88	4.09	8
9	7.79	4.50	7.77	4.53	7.75	4.57	7.73	4.60	9
10	8.66	5.00	8.64	5.04	8.62	5.08	8.59	5.11	10
11	9.53	5.50	9.50	5.54	9.48	5.58	9.45	5.62	11
12	10.39	6.00	10.37	6.05	10.34	6.09	10.31	6.14	12
13	11.26	6.50	11.23	6.55	11.20	6.60	11.17	6.65	13
14	12.12	7.00	12.09	7.05	12.06	7.11	12.03	7.16	14
15	12.99	7.50	12.96	7.56	12.92	7.61	12.89	7.67	15
16	13.86	8.00	13.82	8.06	13.79	8.12	13.75	8.18	16
17	14.72	8.50	14.69	8.56	14.65	8.63	14.61	8.69	17
18	15.59	9.00	15.55	9.07	15.51	9.14	15.47	9.20	18
19	16.45	9.50	16.41	9.57	16.37	9.64	16.33	9.71	19
20	17.32	10.00	17.28	10.08	17.23	10.15	17.19	10.23	20
21	18.19	10.50	18.14	10.58	18.09	10.66	18.05	10.74	21
22	19.05	11.00	19.00	11.08	18.96	11.17	18.91	11.25	22
23	19.92	11.50	19.87	11.59	19.82	11.67	19.77	11.76	23
24	20.78	12.00	20.73	12.09	20.68	12.18	20.63	12.27	24
25	21.65	12.50	21.60	12.59	21.54	12.69	21.49	12.78	25
26	22.52	13.00	22.46	13.10	22.40	13.20	22.34	13.29	26
27	23.38	13.50	23.32	13.60	23.26	13.70	23.20	13.80	27
28	24.25	14.00	24.19	14.11	24.13	14.21	24.06	14.32	28
29	25.11	14.50	25.05	14.61	24.99	14.72	24.92	14.83	29
30	25.98	15.00	25.92	15.11	25.85	15.23	25.78	15.34	30
31	26.85	15.50	26.78	15.62	26.71	15.73	26.64	15.85	31
32	27.71	16.00	27.64	16.12	27.57	16.24	27.50	16.36	32
33	28.58	16.50	28.51	16.62	28.43	16.75	28.36	16.87	33
34	29.44	17.00	29.37	17.13	29.30	17.26	29.22	17.38	34
35	30.31	17.50	30.23	17.63	30.16	17.76	30.08	17.90	35
36	31.18	18.00	31.10	18.14	31.02	18.27	30.94	18.41	36
37	32.04	18.50	31.96	18.64	31.88	18.78	31.80	18.92	37
38	32.91	19.00	32.83	19.14	32.74	19.29	32.66	19.43	38
39	33.77	19.50	33.69	19.65	33.60	19.79	33.52	19.94	39
40	34.64	20.00	34.55	20.15	34.47	20.30	34.38	20.45	40
41	35.51	20.50	35.42	20.65	35.33	20.81	35.24	20.96	41
42	36.37	21.00	36.28	21.16	36.19	21.32	36.10	21.47	42
43	37.24	21.50	37.14	21.66	37.05	21.82	36.95	21.99	43
44	38.11	22.00	38.01	22.17	37.91	22.33	37.81	22.50	44
45	38.97	22.50	38.87	22.67	38.77	22.84	38.67	23.01	45
46	39.84	23.00	39.74	23.17	39.63	23.35	39.53	23.52	46
47	40.70	23.50	40.60	23.68	40.50	23.85	40.39	24.03	47
48	41.57	24.00	41.46	24.18	41.36	24.36	41.25	24.54	48
49	42.44	24.50	42.33	24.68	42.22	24.87	42.11	25.05	49
50	43.30	25.00	43.19	25.19	43.08	25.38	42.97	25.56	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	60 Deg.		59¾ Deg.		59½ Deg.		59¼ Deg.		



Distance.	30 Deg.		30¼ Deg.		30½ Deg.		30¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	44.17	25.50	44.06	25.69	43.94	25.88	43.83	26.08	51
52	45.03	26.00	44.92	26.20	44.80	26.39	44.69	26.59	52
53	45.90	26.50	45.78	26.70	45.67	26.90	45.55	27.10	53
54	46.77	27.00	46.65	27.20	46.53	27.41	46.41	27.61	54
55	47.63	27.50	47.51	27.71	47.39	27.91	47.27	28.12	55
56	48.50	28.00	48.37	28.21	48.25	28.42	48.13	28.63	56
57	49.36	28.50	49.24	28.72	49.11	28.93	48.99	29.14	57
58	50.23	29.00	50.10	29.23	49.97	29.44	49.85	29.65	58
59	51.10	29.50	50.97	29.72	50.84	29.94	50.70	30.17	59
60	51.96	30.00	51.83	30.23	51.70	30.45	51.56	30.68	60
61	52.83	30.50	52.69	30.73	52.56	30.96	52.42	31.19	61
62	53.69	31.00	53.56	31.23	53.42	31.47	53.28	31.70	62
63	54.56	31.50	54.42	31.74	54.28	31.97	54.14	32.21	63
64	55.43	32.00	55.29	32.24	55.14	32.48	55.00	32.72	64
65	56.29	32.50	56.15	32.75	56.01	32.99	55.86	33.23	65
66	57.16	33.00	57.01	33.25	56.87	33.50	56.72	33.75	66
67	58.02	33.50	57.88	33.75	57.73	34.01	57.58	34.26	67
68	58.89	34.00	58.74	34.26	58.59	34.51	58.44	34.77	68
69	59.76	34.50	59.60	34.76	59.45	35.02	59.30	35.28	69
70	60.62	35.00	60.47	35.26	60.31	35.53	60.16	35.79	70
71	61.49	35.50	61.33	35.77	61.18	36.04	61.02	36.30	71
72	62.35	36.00	62.20	36.27	62.04	36.54	61.88	36.81	72
73	63.22	36.50	63.06	36.78	62.90	37.05	62.74	37.32	73
74	64.09	37.00	63.92	37.28	63.76	37.56	63.60	37.84	74
75	64.95	37.50	64.79	37.78	64.62	38.07	64.46	38.35	75
76	65.82	38.00	65.65	38.29	65.48	38.57	65.31	38.86	76
77	66.68	38.50	66.52	38.79	66.35	39.08	66.17	39.37	77
78	67.55	39.00	67.38	39.29	67.21	39.59	67.03	39.88	78
79	68.42	39.50	68.24	39.80	68.07	40.10	67.89	40.39	79
80	69.28	40.00	69.11	40.30	68.93	40.60	68.75	40.90	80
81	70.15	40.50	69.97	40.81	69.79	41.11	69.61	41.41	81
82	71.01	41.00	70.83	41.31	70.65	41.62	70.47	41.93	82
83	71.88	41.50	71.70	41.81	71.52	42.13	71.33	42.44	83
84	72.75	42.00	72.56	42.32	72.38	42.63	72.19	42.95	84
85	73.61	42.50	73.43	42.82	73.24	43.14	73.05	43.46	85
86	74.48	43.00	74.29	43.32	74.10	43.65	73.91	43.97	86
87	75.34	43.50	75.15	43.83	74.96	44.16	74.77	44.48	87
88	76.21	44.00	76.02	44.33	75.82	44.66	75.63	44.99	88
89	77.08	44.50	76.88	44.84	76.68	45.17	76.49	45.51	89
90	77.94	45.00	77.75	45.34	77.55	45.68	77.35	46.02	90
91	78.81	45.50	78.61	45.84	78.41	46.19	78.21	46.53	91
92	79.67	46.00	79.47	46.35	79.27	46.69	79.07	47.04	92
93	80.54	46.50	80.34	46.85	80.13	47.20	79.92	47.55	93
94	81.41	47.00	81.20	47.35	80.99	47.71	80.78	48.06	94
95	82.27	47.50	82.06	47.86	81.85	48.22	81.64	48.57	95
96	83.14	48.00	82.93	48.36	82.72	48.72	82.50	49.08	96
97	84.00	48.50	83.79	48.87	83.58	49.23	83.36	49.60	97
98	84.87	49.00	84.66	49.37	84.44	49.74	84.22	50.11	98
99	85.74	49.50	85.52	49.87	85.30	50.25	85.08	50.62	99
100	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	60 Deg.		59¾ Deg.		59½ Deg.		59¼ Deg.		

Distance.	31 Deg.		31½ Deg.		31¾ Deg.		31¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.86	0.51	0.85	0.52	0.85	0.52	0.85	0.53	1
2	1.71	1.03	1.71	1.04	1.71	1.04	1.70	1.05	2
3	2.57	1.55	2.56	1.56	2.56	1.57	2.55	1.58	3
4	3.43	2.06	3.42	2.08	3.41	2.09	3.40	2.10	4
5	4.29	2.58	4.27	2.59	4.26	2.61	4.25	2.63	5
6	5.14	3.09	5.13	3.11	5.12	3.13	5.10	3.16	6
7	6.00	3.61	5.98	3.63	5.97	3.66	5.95	3.68	7
8	6.86	4.12	6.84	4.15	6.82	4.18	6.80	4.21	8
9	7.71	4.64	7.69	4.67	7.67	4.70	7.65	4.74	9
10	8.57	5.15	8.55	5.19	8.53	5.22	8.50	5.26	10
11	9.43	5.67	9.40	5.71	9.38	5.75	9.35	5.79	11
12	10.29	6.18	10.26	6.23	10.23	6.27	10.20	6.31	12
13	11.14	6.70	11.11	6.74	11.08	6.79	11.05	6.84	13
14	12.00	7.21	11.97	7.26	11.94	7.31	11.90	7.37	14
15	12.86	7.73	12.82	7.78	12.79	7.84	12.76	7.89	15
16	13.71	8.24	13.68	8.30	13.64	8.36	13.61	8.42	16
17	14.57	8.76	14.53	8.82	14.49	8.88	14.46	8.95	17
18	15.43	9.27	15.39	9.34	15.35	9.40	15.31	9.47	18
19	16.29	9.79	16.24	9.86	16.20	9.93	16.16	10.00	19
20	17.14	10.30	17.10	10.38	17.05	10.45	17.01	10.52	20
21	18.00	10.82	17.95	10.89	17.91	10.97	17.86	11.05	21
22	18.86	11.33	18.81	11.41	18.76	11.49	18.71	11.58	22
23	19.71	11.85	19.66	11.93	19.61	12.02	19.56	12.10	23
24	20.57	12.36	20.52	12.45	20.46	12.54	20.41	12.63	24
25	21.43	12.88	21.37	12.97	21.32	13.06	21.26	13.16	25
26	22.29	13.39	22.23	13.49	22.17	13.58	22.11	13.68	26
27	23.14	13.91	23.08	14.01	23.02	14.11	22.96	14.21	27
28	24.00	14.42	23.94	14.53	23.87	14.63	23.81	14.73	28
29	24.86	14.94	24.79	15.04	24.73	15.15	24.66	15.26	29
30	25.71	15.45	25.65	15.56	25.58	15.67	25.51	15.79	30
31	26.57	15.97	26.50	16.08	26.43	16.20	26.36	16.31	31
32	27.43	16.48	27.36	16.60	27.28	16.72	27.21	16.84	32
33	28.29	17.00	28.21	17.12	28.14	17.24	28.06	17.37	33
34	29.14	17.51	29.07	17.64	28.99	17.76	28.91	17.89	34
35	30.00	18.03	29.92	18.16	29.84	18.29	29.76	18.42	35
36	30.86	18.54	30.78	18.68	30.70	18.81	30.61	18.94	36
37	31.72	19.06	31.63	19.19	31.55	19.33	31.46	19.47	37
38	32.57	19.57	32.49	19.71	32.40	19.85	32.31	20.00	38
39	33.43	20.09	33.34	20.23	33.25	20.38	33.16	20.52	39
40	34.29	20.60	34.20	20.75	34.11	20.90	34.01	21.05	40
41	35.14	21.12	35.05	21.27	34.96	21.42	34.86	21.57	41
42	36.00	21.63	35.91	21.79	35.81	21.94	35.71	22.10	42
43	36.86	22.15	36.76	22.31	36.66	22.47	36.57	22.63	43
44	37.72	22.66	37.62	22.83	37.52	22.99	37.42	23.15	44
45	38.57	23.18	38.47	23.34	38.37	23.51	38.27	23.68	45
46	39.43	23.69	39.33	23.86	39.22	24.03	39.12	24.21	46
47	40.29	24.21	40.18	24.38	40.07	24.56	39.97	24.73	47
48	41.14	24.72	41.04	24.90	40.93	25.08	40.82	25.26	48
49	42.00	25.24	41.89	25.42	41.78	25.60	41.67	25.78	49
50	42.86	25.75	42.75	25.94	42.63	26.12	42.52	26.31	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	59 Deg.		58½ Deg.		58½ Deg.		58½ Deg.		

Distance.	31 Deg.		31¼ Deg.		31½ Deg.		31¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	43.72	26.27	43.60	26.46	43.48	26.65	43.37	26.84	51
52	44.57	26.78	44.46	26.98	44.34	27.17	44.22	27.36	52
53	45.43	27.30	45.31	27.49	45.19	27.69	45.07	27.89	53
54	46.29	27.81	46.17	28.01	46.04	28.21	45.92	28.42	54
55	47.14	28.33	47.02	28.53	46.90	28.74	46.77	28.94	55
56	48.00	28.84	47.88	29.05	47.75	29.26	47.62	29.47	56
57	48.86	29.36	48.73	29.57	48.60	29.78	48.47	29.99	57
58	49.72	29.87	49.58	30.09	49.45	30.30	49.32	30.52	58
59	50.57	30.39	50.44	30.61	50.31	30.83	50.17	31.05	59
60	51.43	30.90	51.29	31.13	51.16	31.35	51.02	31.57	60
61	52.29	31.42	52.15	31.65	52.01	31.87	51.87	32.10	61
62	53.14	31.93	53.00	32.16	52.86	32.39	52.72	32.63	62
63	54.00	32.45	53.86	32.68	53.72	32.92	53.57	33.15	63
64	54.86	32.96	54.71	33.20	54.57	33.44	54.42	33.68	64
65	55.72	33.48	55.57	33.72	55.42	33.96	55.27	34.20	65
66	56.57	33.99	56.42	34.24	56.27	34.48	56.12	34.73	66
67	57.43	34.51	57.28	34.76	57.13	35.01	56.98	35.26	67
68	58.29	35.02	58.13	35.28	57.98	35.53	57.82	35.78	68
69	59.14	35.54	58.99	35.80	58.83	36.05	58.67	36.31	69
70	60.00	36.05	59.84	36.31	59.68	36.57	59.52	36.83	70
71	60.86	36.57	60.70	36.83	60.54	37.10	60.37	37.36	71
72	61.72	37.08	61.55	37.35	61.39	37.62	61.23	37.89	72
73	62.57	37.60	62.41	37.87	62.24	38.14	62.08	38.41	73
74	63.43	38.11	63.26	38.39	63.10	38.66	62.93	38.94	74
75	64.29	38.63	64.12	38.91	63.95	39.19	63.78	39.47	75
76	65.14	39.14	64.97	39.43	64.80	39.71	64.63	39.99	76
77	66.00	39.66	65.83	39.95	65.65	40.23	65.48	40.52	77
78	66.86	40.17	66.68	40.46	66.51	40.75	66.33	41.04	78
79	67.72	40.69	67.54	40.98	67.36	41.28	67.18	41.57	79
80	68.57	41.20	68.39	41.50	68.21	41.80	68.03	42.10	80
81	69.43	41.72	69.25	42.02	69.06	42.32	68.88	42.62	81
82	70.29	42.23	70.10	42.54	69.92	42.84	69.73	43.15	82
83	71.14	42.75	70.96	43.06	70.77	43.37	70.58	43.68	83
84	72.00	43.26	71.81	43.58	71.62	43.89	71.43	44.20	84
85	72.86	43.78	72.67	44.10	72.47	44.41	72.28	44.73	85
86	73.72	44.29	73.52	44.61	73.33	44.93	73.13	45.25	86
87	74.57	44.81	74.38	45.13	74.18	45.46	73.98	45.78	87
88	75.43	45.32	75.23	45.65	75.03	45.98	74.83	46.31	88
89	76.29	45.84	76.09	46.17	75.88	46.50	75.68	46.83	89
90	77.15	46.35	76.94	46.69	76.74	47.02	76.53	47.36	90
91	78.00	46.87	77.80	47.21	77.59	47.55	77.38	47.89	91
92	78.86	47.38	78.65	47.73	78.44	48.07	78.23	48.41	92
93	79.72	47.90	79.51	48.25	79.30	48.59	79.08	48.94	93
94	80.57	48.41	80.36	48.76	80.15	49.11	79.93	49.47	94
95	81.43	48.93	81.22	49.28	81.00	49.64	80.78	49.99	95
96	82.29	49.44	82.07	49.80	81.85	50.16	81.63	50.52	96
97	83.15	49.96	82.93	50.32	82.71	50.68	82.48	51.04	97
98	84.00	50.47	83.78	50.84	83.56	51.20	83.33	51.57	98
99	84.86	50.99	84.64	51.36	84.41	51.73	84.18	52.10	99
100	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	59 Deg.		58¾ Deg.		58½ Deg.		58¼ Deg.		

Distance.	32 Deg.		32 $\frac{1}{4}$ Deg.		32 $\frac{1}{2}$ Deg.		32 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.85	0.53	0.85	0.53	0.84	0.54	0.84	0.54	1
2	1.70	1.06	1.69	1.07	1.69	1.07	1.68	1.08	2
3	2.54	1.59	2.54	1.60	2.53	1.61	2.52	1.62	3
4	3.39	2.12	3.38	2.13	3.37	2.15	3.36	2.16	4
5	4.24	2.65	4.23	2.67	4.22	2.69	4.21	2.70	5
6	5.09	3.18	5.07	3.20	5.06	3.22	5.05	3.25	6
7	5.94	3.71	5.92	3.74	5.90	3.76	5.89	3.79	7
8	6.78	4.24	6.77	4.27	6.75	4.30	6.73	4.33	8
9	7.63	4.77	7.61	4.80	7.59	4.84	7.57	4.87	9
10	8.48	5.30	8.46	5.34	8.43	5.37	8.41	5.41	10
11	9.33	5.83	9.30	5.87	9.28	5.91	9.25	5.95	11
12	10.18	6.36	10.15	6.40	10.12	6.45	10.09	6.49	12
13	11.02	6.89	10.99	6.94	10.96	6.98	10.93	7.03	13
14	11.87	7.42	11.84	7.47	11.81	7.52	11.77	7.57	14
15	12.72	7.95	12.69	8.00	12.65	8.06	12.62	8.11	15
16	13.57	8.48	13.53	8.54	13.49	8.60	13.46	8.66	16
17	14.42	9.01	14.38	9.07	14.34	9.13	14.30	9.20	17
18	15.26	9.54	15.22	9.61	15.18	9.67	15.14	9.74	18
19	16.11	10.07	16.07	10.14	16.02	10.21	15.98	10.28	19
20	16.96	10.60	16.91	10.67	16.87	10.75	16.82	10.82	20
21	17.81	11.13	17.76	11.21	17.71	11.28	17.66	11.36	21
22	18.66	11.66	18.61	11.74	18.55	11.82	18.50	11.90	22
23	19.51	12.19	19.45	12.27	19.40	12.36	19.34	12.44	23
24	20.35	12.72	20.30	12.81	20.24	12.90	20.18	12.98	24
25	21.20	13.25	21.14	13.34	21.08	13.43	21.03	13.52	25
26	22.05	13.78	21.99	13.87	21.93	13.97	21.87	14.07	26
27	22.90	14.31	22.83	14.41	22.77	14.51	22.71	14.61	27
28	23.75	14.84	23.68	14.94	23.61	15.04	23.55	15.15	28
29	24.59	15.37	24.53	15.47	24.46	15.58	24.39	15.69	29
30	25.44	15.90	25.37	16.01	25.30	16.12	25.23	16.23	30
31	26.29	16.43	26.22	16.54	26.15	16.66	26.07	16.77	31
32	27.14	16.96	27.06	17.08	26.99	17.19	26.91	17.31	32
33	27.99	17.49	27.91	17.61	27.83	17.73	27.75	17.85	33
34	28.83	18.02	28.75	18.14	28.68	18.27	28.60	18.39	34
35	29.68	18.55	29.60	18.68	29.52	18.81	29.44	18.93	35
36	30.53	19.08	30.45	19.21	30.36	19.34	30.28	19.48	36
37	31.38	19.61	31.29	19.74	31.21	19.88	31.12	20.02	37
38	32.23	20.14	32.14	20.28	32.05	20.42	31.96	20.56	38
39	33.07	20.67	32.98	20.81	32.89	20.95	32.80	21.10	39
40	33.92	21.20	33.83	21.34	33.74	21.49	33.64	21.64	40
41	34.77	21.73	34.67	21.88	34.58	22.03	34.48	22.18	41
42	35.62	22.26	35.52	22.41	35.42	22.57	35.32	22.72	42
43	36.47	22.79	36.37	22.95	36.27	23.10	36.16	23.26	43
44	37.31	23.32	37.21	23.48	37.11	23.64	37.01	23.80	44
45	38.16	23.85	38.06	24.01	37.95	24.18	37.85	24.34	45
46	39.01	24.38	38.90	24.55	38.80	24.72	38.69	24.88	46
47	39.86	24.91	39.75	25.08	39.64	25.25	39.53	25.43	47
48	40.71	25.44	40.59	25.61	40.48	25.79	40.37	25.97	48
49	41.55	25.97	41.44	26.15	41.33	26.33	41.21	26.51	49
50	42.40	26.50	42.29	26.68	42.17	26.86	42.05	27.05	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	58 Deg.		57 $\frac{3}{4}$ Deg.		57 $\frac{1}{2}$ Deg.		57 $\frac{1}{4}$ Deg.		

Distance.	32 Deg.		32½ Deg.		32¾ Deg.		33¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	43.25	27.03	43.13	27.21	43.01	27.40	42.89	27.59	51
52	44.10	27.56	43.98	27.75	43.86	27.94	43.73	28.13	52
53	44.95	28.09	44.82	28.28	44.70	28.48	44.58	28.67	53
54	45.79	28.62	45.67	28.82	45.54	29.01	45.42	29.21	54
55	46.64	29.15	46.51	29.35	46.39	29.55	46.26	29.75	55
56	47.49	29.68	47.36	29.88	47.23	30.09	47.10	30.29	56
57	48.34	30.21	48.21	30.42	48.07	30.63	47.94	30.84	57
58	49.19	30.74	49.05	30.95	48.92	31.16	48.78	31.38	58
59	50.03	31.27	49.90	31.48	49.76	31.70	49.62	31.92	59
60	50.88	31.80	50.74	32.02	50.60	32.24	50.46	32.46	60
61	51.73	32.33	51.59	32.55	51.45	32.78	51.30	33.00	61
62	52.58	32.85	52.44	33.08	52.29	33.31	52.14	33.54	62
63	53.43	33.38	53.28	33.62	53.13	33.85	52.99	34.08	63
64	54.28	33.91	54.13	34.15	53.98	34.39	53.83	34.62	64
65	55.12	34.44	54.97	34.68	54.82	34.92	54.67	35.16	65
66	55.97	34.97	55.82	35.22	55.66	35.46	55.51	35.70	66
67	56.82	35.50	56.66	35.75	56.51	36.00	56.35	36.25	67
68	57.67	36.03	57.51	36.29	57.35	36.54	57.19	36.79	68
69	58.52	36.56	58.36	36.82	58.19	37.07	58.03	37.33	69
70	59.36	37.09	59.20	37.35	59.04	37.61	58.87	37.87	70
71	60.21	37.62	60.05	37.89	59.88	38.15	59.71	38.41	71
72	61.06	38.15	60.89	38.42	60.72	38.69	60.55	38.95	72
73	61.91	38.68	61.74	38.95	61.57	39.22	61.40	39.49	73
74	62.76	39.21	62.58	39.49	62.41	39.76	62.24	40.03	74
75	63.60	39.74	63.43	40.02	63.25	40.30	63.08	40.57	75
76	64.45	40.27	64.28	40.55	64.10	40.83	63.92	41.11	76
77	65.30	40.80	65.12	41.09	64.94	41.37	64.76	41.65	77
78	66.15	41.33	65.97	41.62	65.78	41.91	65.60	42.20	78
79	67.00	41.86	66.81	42.16	66.63	42.45	66.44	42.74	79
80	67.84	42.39	67.66	42.69	67.47	42.98	67.28	43.28	80
81	68.69	42.92	68.50	43.22	68.31	43.52	68.12	43.82	81
82	69.54	43.45	69.35	43.76	69.16	44.06	68.97	44.36	82
83	70.39	43.98	70.20	44.29	70.00	44.60	69.81	44.90	83
84	71.24	44.51	71.04	44.82	70.84	45.13	70.65	45.44	84
85	72.08	45.04	71.89	45.36	71.69	45.67	71.49	45.98	85
86	72.93	45.57	72.73	45.89	72.53	46.21	72.33	46.52	86
87	73.78	46.10	73.58	46.42	73.38	46.75	73.17	47.06	87
88	74.63	46.63	74.42	46.96	74.22	47.28	74.01	47.61	88
89	75.48	47.16	75.27	47.49	75.06	47.82	74.85	48.15	89
90	76.32	47.69	76.12	48.03	75.91	48.36	75.69	48.69	90
91	77.17	48.22	76.96	48.56	76.75	48.89	76.53	49.23	91
92	78.02	48.75	77.81	49.09	77.59	49.43	77.38	49.77	92
93	78.87	49.28	78.65	49.63	78.44	49.97	78.22	50.31	93
94	79.72	49.81	79.50	50.16	79.28	50.51	79.06	50.85	94
95	80.56	50.34	80.34	50.69	80.12	51.04	79.90	51.39	95
96	81.41	50.87	81.19	51.23	80.97	51.58	80.74	51.93	96
97	82.26	51.40	82.04	51.76	81.81	52.12	81.58	52.47	97
98	83.11	51.93	82.88	52.29	82.65	52.66	82.42	53.02	98
99	83.96	52.46	83.73	52.83	83.50	53.19	83.26	53.56	99
100	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	58 Deg.		57¾ Deg.		57½ Deg.		57¼ Deg.		

Distance.	33 Deg.		33 $\frac{1}{4}$ Deg.		33 $\frac{1}{2}$ Deg.		33 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.84	0.54	0.84	0.55	0.83	0.55	0.83	0.56	1
2	1.68	1.09	1.67	1.10	1.67	1.10	1.66	1.11	2
3	2.52	1.63	2.51	1.64	2.50	1.66	2.49	1.67	3
4	3.35	2.18	3.35	2.19	3.34	2.21	3.33	2.22	4
5	4.19	2.72	4.18	2.74	4.17	2.76	4.16	2.78	5
6	5.03	3.27	5.02	3.29	5.00	3.31	4.99	3.23	6
7	5.87	3.81	5.85	3.84	5.84	3.86	5.82	3.89	7
8	6.71	4.36	6.69	4.39	6.67	4.42	6.65	4.44	8
9	7.55	4.90	7.53	4.93	7.50	4.97	7.48	5.00	9
10	8.39	5.45	8.36	5.48	8.34	5.52	8.31	5.56	10
11	9.23	5.99	9.20	6.03	9.17	6.07	9.15	6.11	11
12	10.06	6.54	10.04	6.58	10.01	6.62	9.98	6.67	12
13	10.90	7.08	10.87	7.13	10.84	7.18	10.81	7.22	13
14	11.74	7.62	11.71	7.68	11.67	7.73	11.64	7.78	14
15	12.58	8.17	12.54	8.22	12.51	8.28	12.47	8.33	15
16	13.42	8.71	13.38	8.77	13.34	8.83	13.30	8.89	16
17	14.26	9.26	14.22	9.32	14.18	9.38	14.13	9.44	17
18	15.10	9.80	15.05	9.87	15.01	9.93	14.97	10.00	18
19	15.93	10.35	15.89	10.42	15.84	10.49	15.80	10.56	19
20	16.77	10.89	16.73	10.97	16.68	11.04	16.63	11.11	20
21	17.61	11.44	17.56	11.51	17.51	11.59	17.46	11.67	21
22	18.45	11.98	18.40	12.06	18.35	12.14	18.29	12.22	22
23	19.29	12.53	19.23	12.61	19.18	12.69	19.12	12.78	23
24	20.13	13.07	20.07	13.16	20.01	13.25	19.96	13.33	24
25	20.97	13.62	20.91	13.71	20.85	13.80	20.79	13.89	25
26	21.81	14.16	21.74	14.26	21.68	14.35	21.62	14.44	26
27	22.64	14.71	22.58	14.80	22.51	14.90	22.45	15.00	27
28	23.48	15.25	23.42	15.35	23.35	15.45	23.28	15.56	28
29	24.32	15.79	24.25	15.90	24.18	16.01	24.11	16.11	29
30	25.16	16.34	25.09	16.45	25.02	16.56	24.94	16.67	30
31	26.00	16.88	25.92	17.00	25.85	17.11	25.78	17.22	31
32	26.84	17.43	26.76	17.55	26.68	17.66	26.61	17.78	32
33	27.68	17.97	27.60	18.09	27.52	18.21	27.44	18.33	33
34	28.51	18.52	28.43	18.64	28.35	18.77	28.27	18.89	34
35	29.35	19.06	29.27	19.19	29.19	19.32	29.10	19.44	35
36	30.19	19.61	30.11	19.74	30.02	19.87	29.93	20.00	36
37	31.03	20.15	30.94	20.29	30.85	20.42	30.76	20.56	37
38	31.87	20.70	31.78	20.84	31.69	20.97	31.60	21.11	38
39	32.71	21.24	32.62	21.38	32.52	21.53	32.43	21.67	39
40	33.55	21.79	33.45	21.93	33.36	22.08	33.26	22.22	40
41	34.39	22.33	34.29	22.48	34.19	22.63	34.09	22.78	41
42	35.22	22.87	35.12	23.03	35.02	23.18	34.92	23.33	42
43	36.06	23.42	35.96	23.58	35.86	23.73	35.75	23.89	43
44	36.90	23.96	36.80	24.12	36.69	24.29	36.58	24.45	44
45	37.74	24.51	37.63	24.67	37.52	24.84	37.42	25.00	45
46	38.58	25.05	38.47	25.22	38.36	25.39	38.25	25.56	46
47	39.42	25.60	39.31	25.77	39.19	25.94	39.08	26.11	47
48	40.26	26.14	40.14	26.32	40.03	26.49	39.91	26.67	48
49	41.09	26.69	40.98	26.87	40.86	27.04	40.74	27.22	49
50	41.93	27.23	41.81	27.41	41.69	27.60	41.57	27.78	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	57 Deg.		56 $\frac{3}{4}$ Deg.		56 $\frac{1}{2}$ Deg.		56 $\frac{1}{4}$ Deg.		

Distance.	33 Deg.		33 $\frac{1}{4}$ Deg.		33 $\frac{1}{2}$ Deg.		33 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	42.77	27.78	42.65	27.96	42.53	28.15	42.40	28.33	51
52	43.61	28.32	43.49	28.51	43.36	28.70	43.24	28.89	52
53	44.45	28.87	44.32	29.06	44.20	29.25	44.07	29.45	53
54	45.29	29.41	45.16	29.61	45.03	29.80	44.90	30.00	54
55	46.13	29.96	46.00	30.16	45.86	30.36	45.73	30.56	55
56	46.97	30.50	46.83	30.70	46.70	30.91	46.56	31.11	56
57	47.80	31.04	47.67	31.25	47.53	31.46	47.39	31.67	57
58	48.64	31.59	48.50	31.80	48.37	32.01	48.23	32.22	58
59	49.48	32.13	49.34	32.35	49.20	32.56	49.06	32.78	59
60	50.32	32.68	50.18	32.90	50.03	33.12	49.89	33.33	60
61	51.16	33.22	51.01	33.45	50.87	33.67	50.72	33.89	61
62	52.00	33.77	51.85	33.99	51.70	34.22	51.55	34.45	62
63	52.84	34.31	52.69	34.54	52.53	34.77	52.38	35.00	63
64	53.67	34.86	53.52	35.09	53.37	35.32	53.21	35.56	64
65	54.51	35.40	54.36	35.64	54.20	35.88	54.05	36.11	65
66	55.35	35.95	55.19	36.19	55.04	36.43	54.88	36.67	66
67	56.19	36.49	56.03	36.74	55.87	36.98	55.71	37.22	67
68	57.03	37.04	56.87	37.28	56.70	37.53	56.54	37.78	68
69	57.87	37.58	57.70	37.83	57.54	38.08	57.37	38.33	69
70	58.71	38.12	58.54	38.38	58.37	38.64	58.20	38.89	70
71	59.55	38.67	59.38	38.93	59.21	39.19	59.03	39.45	71
72	60.38	39.21	60.21	39.48	60.04	39.74	59.87	40.00	72
73	61.22	39.76	61.05	40.03	60.87	40.29	60.70	40.56	73
74	62.06	40.30	61.89	40.57	61.71	40.84	61.53	41.11	74
75	62.90	40.85	62.72	41.12	62.54	41.40	62.36	41.67	75
76	63.74	41.39	63.56	41.67	63.38	41.95	63.19	42.22	76
77	64.58	41.94	64.39	42.22	64.21	42.50	64.02	42.78	77
78	65.42	42.48	65.23	42.77	65.04	43.05	64.85	43.33	78
79	66.25	43.03	66.07	43.32	65.88	43.60	65.69	43.89	79
80	67.09	43.57	66.90	43.86	66.71	44.15	66.52	44.45	80
81	67.93	44.12	67.74	44.41	67.54	44.71	67.35	45.00	81
82	68.77	44.66	68.58	44.96	68.38	45.26	68.18	45.56	82
83	69.61	45.20	69.41	45.51	69.21	45.81	69.01	46.11	83
84	70.45	45.75	70.25	46.06	70.05	46.36	69.84	46.67	84
85	71.29	46.29	71.08	46.60	70.88	46.91	70.67	47.22	85
86	72.13	46.84	71.92	47.15	71.71	47.47	71.51	47.78	86
87	72.96	47.38	72.76	47.70	72.55	48.02	72.34	48.33	87
88	73.80	47.93	73.59	48.25	73.38	48.57	73.17	48.89	88
89	74.64	48.47	74.43	48.80	74.22	49.12	74.00	49.45	89
90	75.48	49.02	75.27	49.35	75.05	49.67	74.83	50.00	90
91	76.32	49.56	76.10	49.89	75.88	50.23	75.66	50.56	91
92	77.16	50.11	76.94	50.44	76.72	50.78	76.50	51.11	92
93	78.00	50.65	77.77	50.99	77.55	51.33	77.33	51.67	93
94	78.83	51.20	78.61	51.54	78.39	51.88	78.16	52.22	94
95	79.67	51.74	79.45	52.09	79.22	52.43	78.99	52.78	95
96	80.51	52.29	80.28	52.64	80.05	52.99	79.82	53.33	96
97	81.35	52.83	81.12	53.18	80.89	53.54	80.65	53.89	97
98	82.19	53.37	81.96	53.73	81.72	54.09	81.48	54.45	98
99	83.03	53.92	82.79	54.28	82.55	54.64	82.32	55.00	99
100	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	57 Deg.		56 $\frac{3}{4}$ Deg.		56 $\frac{1}{2}$ Deg.		56 $\frac{1}{4}$ Deg.		

Distance.	34 Deg.		34 $\frac{1}{4}$ Deg.		34 $\frac{1}{2}$ Deg.		34 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.83	0.56	0.83	0.56	0.82	0.57	0.82	0.57	1
2	1.66	1.12	1.65	1.13	1.65	1.13	1.64	1.14	2
3	2.49	1.68	2.48	1.69	2.47	1.70	2.46	1.71	3
4	3.32	2.24	3.31	2.25	3.30	2.27	3.29	2.28	4
5	4.15	2.80	4.13	2.81	4.12	2.83	4.11	2.85	5
6	4.97	3.36	4.96	3.38	4.94	3.40	4.93	3.42	6
7	5.80	3.91	5.79	3.94	5.77	3.96	5.75	3.99	7
8	6.63	4.47	6.61	4.50	6.59	4.53	6.57	4.56	8
9	7.46	5.03	7.44	5.07	7.42	5.10	7.39	5.13	9
10	8.29	5.59	8.27	5.63	8.24	5.66	8.22	5.70	10
11	9.12	6.15	9.09	6.19	9.07	6.23	9.04	6.27	11
12	9.95	6.71	9.92	6.75	9.89	6.80	9.86	6.84	12
13	10.78	7.27	10.75	7.32	10.71	7.36	10.68	7.41	13
14	11.61	7.83	11.57	7.88	11.54	7.93	11.50	7.98	14
15	12.44	8.39	12.40	8.44	12.36	8.50	12.32	8.55	15
16	13.26	8.95	13.23	9.00	13.19	9.06	13.15	9.12	16
17	14.09	9.51	14.05	9.57	14.01	9.63	13.97	9.69	17
18	14.92	10.07	14.88	10.13	14.83	10.20	14.79	10.26	18
19	15.75	10.62	15.71	10.69	15.66	10.76	15.61	10.83	19
20	16.58	11.18	16.53	11.26	16.48	11.33	16.43	11.40	20
21	17.41	11.74	17.36	11.82	17.31	11.89	17.25	11.97	21
22	18.24	12.30	18.18	12.38	18.13	12.46	18.08	12.54	22
23	19.07	12.86	19.01	12.94	18.95	13.03	18.90	13.11	23
24	19.90	13.42	19.84	13.51	19.78	13.59	19.72	13.68	24
25	20.73	13.98	20.66	14.07	20.60	14.16	20.54	14.25	25
26	21.55	14.54	21.49	14.63	21.43	14.73	21.36	14.82	26
27	22.38	15.10	22.32	15.20	22.25	15.29	22.18	15.39	27
28	23.21	15.66	23.14	15.76	23.08	15.86	23.01	15.96	28
29	24.04	16.22	23.97	16.32	23.90	16.43	23.83	16.53	29
30	24.87	16.78	24.80	16.88	24.72	16.99	24.65	17.10	30
31	25.70	17.33	25.62	17.45	25.55	17.56	25.47	17.67	31
32	26.53	17.89	26.45	18.01	26.37	18.12	26.29	18.24	32
33	27.36	18.45	27.28	18.57	27.20	18.69	27.11	18.81	33
34	28.19	19.01	28.10	19.14	28.02	19.26	27.94	19.38	34
35	29.02	19.57	28.93	19.70	28.84	19.82	28.76	19.95	35
36	29.85	20.13	29.76	20.26	29.67	20.39	29.58	20.52	36
37	30.67	20.69	30.58	20.82	30.49	20.96	30.40	21.09	37
38	31.50	21.25	31.41	21.39	31.32	21.52	31.22	21.66	38
39	32.33	21.81	32.24	21.95	32.14	22.09	32.04	22.23	39
40	33.16	22.37	33.06	22.51	32.97	22.66	32.87	22.80	40
41	33.99	22.93	33.89	23.07	33.79	23.22	33.69	23.37	41
42	34.82	23.49	34.72	23.64	34.61	23.79	34.51	23.94	42
43	35.65	24.05	35.54	24.20	35.44	24.36	35.33	24.51	43
44	36.48	24.60	36.37	24.76	36.26	24.92	36.15	25.08	44
45	37.31	25.16	37.20	25.33	37.09	25.49	36.97	25.65	45
46	38.14	25.72	38.02	25.89	37.91	26.05	37.80	26.22	46
47	38.96	26.28	38.85	26.45	38.73	26.62	38.62	26.79	47
48	39.79	26.84	39.68	27.01	39.56	27.19	39.44	27.36	48
49	40.62	27.40	40.50	27.58	40.38	27.75	40.26	27.93	49
50	41.45	27.96	41.33	28.14	41.21	28.32	41.08	28.50	50
Distance.	56 Deg.		55 $\frac{3}{4}$ Deg.		55 $\frac{1}{2}$ Deg.		55 $\frac{1}{4}$ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	



Distance.	34 Deg.		34½ Deg.		34½ Deg.		34¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	42.23	28.52	42.16	28.70	42.03	28.89	41.90	29.07	51
52	43.11	29.08	42.98	29.27	42.85	29.45	42.73	29.64	52
53	43.94	29.64	43.81	29.83	43.68	30.02	43.55	30.21	53
54	44.77	30.20	44.64	30.39	44.50	30.59	44.37	30.78	54
55	45.60	30.76	45.46	30.95	45.33	31.15	45.19	31.35	55
56	46.43	31.31	46.29	31.52	46.15	31.72	46.01	31.92	56
57	47.26	31.87	47.12	32.08	46.98	32.29	46.83	32.49	57
58	48.08	32.43	47.94	32.64	47.80	32.85	47.66	33.06	58
59	48.91	32.99	48.77	33.21	48.62	33.42	48.48	33.63	59
60	49.74	33.55	49.60	33.77	49.45	33.98	49.30	34.20	60
61	50.57	34.11	50.42	34.33	50.27	34.55	50.12	34.77	61
62	51.40	34.67	51.25	34.89	51.10	35.12	50.94	35.34	62
63	52.23	35.23	52.08	35.46	51.92	35.68	51.76	35.91	63
64	53.06	35.79	52.90	36.02	52.74	36.25	52.59	36.48	64
65	53.89	36.35	53.73	36.58	53.57	36.82	53.41	37.05	65
66	54.72	36.91	54.55	37.15	54.39	37.38	54.23	37.62	66
67	55.55	37.46	55.38	37.71	55.22	37.95	55.05	38.19	67
68	56.37	38.03	56.21	38.27	56.04	38.52	55.87	38.76	68
69	57.20	38.58	57.03	38.83	56.86	39.08	56.69	39.33	69
70	58.03	39.14	57.86	39.40	57.69	39.65	57.52	39.90	70
71	58.86	39.70	58.69	39.96	58.51	40.21	58.34	40.47	71
72	59.69	40.26	59.51	40.52	59.34	40.78	59.16	41.04	72
73	60.52	40.82	60.34	41.08	60.16	41.35	59.98	41.61	73
74	61.35	41.38	61.17	41.65	60.99	41.91	60.80	42.18	74
75	62.18	41.94	61.99	42.21	61.81	42.48	61.62	42.75	75
76	63.01	42.50	62.82	42.77	62.63	43.05	62.45	43.32	76
77	63.84	43.06	63.65	43.34	63.46	43.61	63.27	43.89	77
78	64.66	43.62	64.47	43.90	64.28	44.18	64.09	44.46	78
79	65.49	44.18	65.30	44.46	65.11	44.75	64.91	45.03	79
80	66.32	44.74	66.13	45.02	65.93	45.31	65.73	45.60	80
81	67.15	45.29	66.95	45.59	66.75	45.88	66.55	46.17	81
82	67.98	45.85	67.78	46.15	67.58	46.45	67.37	46.74	82
83	68.81	46.41	68.61	46.71	68.40	47.01	68.20	47.31	83
84	69.64	46.97	69.43	47.28	69.23	47.58	69.02	47.88	84
85	70.47	47.53	70.26	47.84	70.05	48.14	69.84	48.45	85
86	71.30	48.09	71.09	48.40	70.87	48.71	70.66	49.02	86
87	72.13	48.65	71.91	48.96	71.70	49.28	71.48	49.59	87
88	72.96	49.21	72.74	49.53	72.52	49.84	72.30	50.16	88
89	73.78	49.77	73.57	50.09	73.35	50.41	73.13	50.73	89
90	74.61	50.33	74.39	50.65	74.17	50.98	73.95	51.30	90
91	75.44	50.89	75.22	51.22	75.00	51.54	74.77	51.87	91
92	76.27	51.45	76.05	51.78	75.82	52.11	75.59	52.44	92
93	77.10	52.00	76.87	52.34	76.64	52.68	76.41	53.01	93
94	77.93	52.56	77.70	52.90	77.47	53.24	77.23	53.58	94
95	78.76	53.12	78.53	53.47	78.29	53.81	78.06	54.15	95
96	79.59	53.68	79.35	54.03	79.12	54.37	78.88	54.72	96
97	80.42	54.24	80.18	54.59	79.94	54.94	79.70	55.29	97
98	81.25	54.80	81.01	55.15	80.76	55.51	80.52	55.86	98
99	82.07	55.36	81.83	55.72	81.59	56.07	81.34	56.43	99
100	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	100
Distance.	56 Deg.		55¾ Deg.		55½ Deg.		55¼ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

Distance.	35 Deg.		35 $\frac{1}{4}$ Deg.		35 $\frac{1}{2}$ Deg.		35 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.82	0.57	0.82	0.58	0.81	0.58	0.81	0.58	1
2	1.64	1.15	1.63	1.15	1.63	1.16	1.62	1.17	2
3	2.46	1.72	2.45	1.73	2.44	1.74	2.43	1.75	3
4	3.28	2.29	3.27	2.31	3.26	2.32	3.25	2.34	4
5	4.10	2.87	4.08	2.89	4.07	2.90	4.06	2.92	5
6	4.91	3.44	4.90	3.46	4.88	3.48	4.87	3.51	6
7	5.73	4.01	5.72	4.04	5.70	4.06	5.68	4.09	7
8	6.55	4.59	6.53	4.62	6.51	4.65	6.49	4.67	8
9	7.37	5.16	7.35	5.19	7.33	5.23	7.30	5.26	9
10	8.19	5.74	8.17	5.77	8.14	5.81	8.12	5.84	10
11	9.01	6.31	8.98	6.35	8.96	6.39	8.93	6.43	11
12	9.83	6.88	9.80	6.93	9.77	6.97	9.74	7.01	12
13	10.65	7.46	10.62	7.50	10.58	7.55	10.55	7.60	13
14	11.47	8.03	11.43	8.08	11.40	8.13	11.36	8.18	14
15	12.29	8.60	12.25	8.66	12.21	8.71	12.17	8.76	15
16	13.11	9.18	13.07	9.23	13.03	9.29	12.99	9.35	16
17	13.93	9.75	13.88	9.81	13.84	9.87	13.80	9.93	17
18	14.74	10.32	14.70	10.39	14.65	10.45	14.61	10.52	18
19	15.56	10.90	15.52	10.97	15.47	11.03	15.42	11.10	19
20	16.38	11.47	16.33	11.54	16.28	11.61	16.23	11.68	20
21	17.20	12.05	17.15	12.12	17.10	12.19	17.04	12.27	21
22	18.02	12.62	17.97	12.70	17.91	12.78	17.85	12.85	22
23	18.84	13.19	18.78	13.27	18.72	13.36	18.67	13.44	23
24	19.66	13.77	19.60	13.85	19.54	13.94	19.48	14.02	24
25	20.48	14.34	20.42	14.43	20.35	14.52	20.29	14.61	25
26	21.30	14.91	21.23	15.01	21.17	15.10	21.10	15.19	26
27	22.12	15.49	22.05	15.58	21.98	15.68	21.91	15.77	27
28	22.94	16.06	22.87	16.16	22.80	16.26	22.72	16.36	28
29	23.76	16.63	23.68	16.74	23.61	16.84	23.54	16.94	29
30	24.57	17.21	24.50	17.51	24.42	17.42	24.35	17.53	30
31	25.39	17.78	25.32	17.89	25.24	18.00	25.16	18.11	31
32	26.21	18.35	26.13	18.47	26.05	18.58	25.97	18.70	32
33	27.03	18.93	26.95	19.05	26.87	19.16	26.78	19.28	33
34	27.85	19.50	27.77	19.62	27.68	19.74	27.59	19.86	34
35	28.67	20.08	28.58	20.20	28.49	20.32	28.41	20.45	35
36	29.49	20.65	29.40	20.78	29.31	20.91	29.22	21.03	36
37	30.31	21.22	30.22	21.35	30.12	21.49	30.03	21.62	37
38	31.13	21.80	31.03	21.93	30.94	22.07	30.84	22.20	38
39	31.95	22.37	31.85	22.51	31.75	22.65	31.65	22.79	39
40	32.77	22.94	32.67	23.09	32.56	23.23	32.46	23.37	40
41	33.59	23.52	33.48	23.66	33.38	23.81	33.27	23.95	41
42	34.40	24.09	34.30	24.24	34.19	24.39	34.09	24.54	42
43	35.22	24.66	35.12	24.82	35.01	24.97	34.90	25.12	43
44	36.04	25.24	35.93	25.39	35.82	25.55	35.71	25.71	44
45	36.86	25.81	36.75	25.97	36.64	26.13	36.52	26.29	45
46	37.68	26.38	37.57	26.55	37.45	26.71	37.33	26.88	46
47	38.50	26.96	38.38	27.13	38.26	27.29	38.14	27.46	47
48	39.32	27.53	39.20	27.70	39.08	27.87	38.96	28.04	48
49	40.14	28.11	40.02	28.28	39.89	28.45	39.77	28.63	49
50	40.96	28.68	40.83	28.86	40.71	29.04	40.58	29.21	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	55 Deg.		54 $\frac{3}{4}$ Deg.		54 $\frac{1}{2}$ Deg.		54 $\frac{1}{4}$ Deg.		

Distance.	35 Deg.		35½ Deg.		35¾ Deg.		35¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	41.78	29.25	41.65	29.43	41.52	29.62	41.39	29.80	51
52	42.60	29.83	42.47	30.01	42.33	30.20	42.20	30.38	52
53	43.42	30.40	43.28	30.59	43.15	30.78	43.01	30.97	53
54	44.23	30.97	44.10	31.17	43.96	31.36	43.82	31.55	54
55	45.05	31.55	44.92	31.74	44.78	31.94	44.64	32.13	55
56	45.87	32.12	45.73	32.32	45.59	32.52	45.45	32.72	56
57	46.69	32.69	46.55	32.90	46.40	33.10	46.26	33.30	57
58	47.51	33.27	47.37	33.47	47.22	33.68	47.07	33.89	58
59	48.33	33.84	48.18	34.05	48.03	34.26	47.88	34.47	59
60	49.15	34.41	49.00	34.63	48.85	34.84	48.69	35.05	60
61	49.97	34.99	49.82	35.21	49.66	35.42	49.51	35.64	61
62	50.79	35.56	50.63	35.78	50.48	36.00	50.32	36.22	62
63	51.61	36.14	51.45	36.36	51.29	36.58	51.13	36.81	63
64	52.43	36.71	52.27	36.94	52.10	37.16	51.94	37.39	64
65	53.24	37.28	53.08	37.51	52.92	37.75	52.75	37.98	65
66	54.06	37.86	53.90	38.09	53.73	38.33	53.56	38.56	66
67	54.88	38.43	54.71	38.67	54.55	38.91	54.38	39.14	67
68	55.70	39.00	55.53	39.25	55.36	39.49	55.19	39.73	68
69	56.52	39.58	56.35	39.82	56.17	40.07	56.00	40.31	69
70	57.34	40.15	57.16	40.40	56.99	40.65	56.81	40.90	70
71	58.16	40.72	57.98	40.98	57.80	41.23	57.62	41.48	71
72	58.98	41.30	58.80	41.55	58.62	41.81	58.43	42.07	72
73	59.80	41.87	59.61	42.13	59.43	42.39	59.24	42.65	73
74	60.62	42.44	60.43	42.71	60.24	42.97	60.05	43.23	74
75	61.44	43.02	61.25	43.29	61.06	43.55	60.87	43.82	75
76	62.26	43.59	62.06	43.86	61.87	44.13	61.68	44.40	76
77	63.07	44.17	62.88	44.44	62.69	44.71	62.49	44.99	77
78	63.89	44.74	63.70	45.02	63.50	45.29	63.30	45.57	78
79	64.71	45.31	64.51	45.59	64.32	45.88	64.11	46.16	79
80	65.53	45.89	65.33	46.17	65.13	46.46	64.93	46.74	80
81	66.35	46.46	66.15	46.75	65.94	47.04	65.74	47.32	81
82	67.17	47.03	66.96	47.33	66.76	47.62	66.55	47.91	82
83	67.99	47.61	67.78	47.90	67.57	48.20	67.36	48.49	83
84	68.81	48.18	68.60	48.48	68.39	48.78	68.17	49.08	84
85	69.63	48.75	69.41	49.06	69.20	49.36	68.98	49.66	85
86	70.45	49.33	70.23	49.63	70.01	49.94	69.80	50.25	86
87	71.27	49.90	71.05	50.21	70.83	50.52	70.61	50.83	87
88	72.09	50.47	71.86	50.79	71.64	51.10	71.42	51.41	88
89	72.90	51.05	72.68	51.37	72.46	51.68	72.23	52.00	89
90	73.72	51.62	73.50	51.94	73.27	52.26	73.04	52.58	90
91	74.54	52.20	74.31	52.52	74.08	52.84	73.85	53.17	91
92	75.36	52.77	75.13	53.10	74.90	53.42	74.66	53.75	92
93	76.18	53.34	75.95	53.67	75.71	54.01	75.48	54.34	93
94	77.00	53.92	76.76	54.25	76.53	54.59	76.29	54.92	94
95	77.82	54.49	77.58	54.83	77.34	55.17	77.10	55.50	95
96	78.64	55.06	78.40	55.41	78.16	55.75	77.91	56.09	96
97	79.46	55.64	79.21	55.98	78.97	56.33	78.72	56.67	97
98	80.28	56.21	80.03	56.56	79.78	56.91	79.53	57.26	98
99	81.10	56.78	80.85	57.14	80.60	57.49	80.35	57.84	99
100	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	55 Deg.		54¾ Deg.		54½ Deg.		54¼ Deg.		

Distance.	36 Deg.		36¼ Deg.		36½ Deg.		36¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.81	0.59	0.81	0.59	0.80	0.59	0.80	0.60	1
2	1.62	1.18	1.61	1.18	1.61	1.19	1.60	1.20	2
3	2.43	1.76	2.42	1.77	2.41	1.78	2.40	1.79	3
4	3.24	2.35	3.23	2.37	3.22	2.38	3.20	2.39	4
5	4.05	2.94	4.03	2.96	4.02	2.97	4.01	2.99	5
6	4.85	3.53	4.84	3.55	4.82	3.57	4.81	3.59	6
7	5.66	4.11	5.65	4.14	5.63	4.16	5.61	4.19	7
8	6.47	4.70	6.45	4.73	6.43	4.76	6.41	4.79	8
9	7.28	5.29	7.26	5.32	7.23	5.35	7.21	5.38	9
10	8.09	5.88	8.06	5.91	8.04	5.95	8.01	5.98	10
11	8.90	6.47	8.87	6.50	8.84	6.54	8.81	6.58	11
12	9.71	7.05	9.68	7.10	9.65	7.14	9.61	7.18	12
13	10.52	7.64	10.48	7.69	10.45	7.73	10.42	7.78	13
14	11.33	8.23	11.29	8.28	11.25	8.33	11.22	8.38	14
15	12.14	8.82	12.10	8.87	12.06	8.92	12.02	8.97	15
16	12.94 <sup>6</sup>	9.40	12.90	9.46	12.86	9.52	12.82	9.57	16
17	13.75	9.99	13.71	10.05	13.67	10.11	13.62	10.17	17
18	14.56	10.58	14.52	10.64	14.47	10.71	14.42	10.77	18
19	15.37	11.17	15.32	11.23	15.27	11.30	15.22	11.37	19
20	16.18	11.76	16.13	11.83	16.08	11.90	16.03	11.97	20
21	16.99	12.34	16.94	12.42	16.88	12.49	16.83	12.56	21
22	17.80	12.93	17.74	13.01	17.68	13.09	17.63	13.16	22
23	18.61	13.52	18.55	13.60	18.49	13.68	18.43	13.76	23
24	19.42	14.11	19.35	14.19	19.29	14.28	19.23	14.36	24
25	20.23	14.69	20.16	14.78	20.10	14.87	20.03	14.96	25
26	21.03	15.28	20.97	15.37	20.90	15.47	20.83	15.56	26
27	21.84	15.87	21.77	15.97	21.70	16.06	21.63	16.15	27
28	22.65	16.46	22.58	16.56	22.51	16.65	22.44	16.75	28
29	23.46	17.05	23.39	17.15	23.31	17.25	23.24	17.35	29
30	24.27	17.63	24.19	17.74	24.12	17.84	24.04	17.95	30
31	25.08	18.22	25.00	18.33	24.92	18.44	24.84	18.55	31
32	25.89	18.81	25.81	18.92	25.72	19.03	25.64	19.15	32
33	26.70	19.40	26.61	19.51	26.53	19.63	26.44	19.74	33
34	27.51	19.98	27.42	20.10	27.33	20.22	27.24	20.34	34
35	28.32	20.57	28.23	20.70	28.13	20.82	28.04	20.94	35
36	29.12	21.16	29.03	21.29	28.94	21.41	28.85	21.54	36
37	29.93	21.75	29.84	21.88	29.74	22.01	29.65	22.14	37
38	30.74	22.34	30.64	22.47	30.55	22.60	30.45	22.74	38
39	31.55	22.92	31.45	23.06	31.35	23.20	31.25	23.33	39
40	32.36	23.51	32.26	23.65	32.15	23.79	32.05	23.93	40
41	33.17	24.10	33.06	24.24	32.96	24.39	32.85	24.53	41
42	33.98	24.69	33.87	24.83	33.76	24.98	33.65	25.13	42
43	34.79	25.27	34.68	25.43	34.57	25.58	34.45	25.73	43
44	35.60	25.86	35.48	26.02	35.37	26.17	35.26	26.33	44
45	36.41	26.45	36.29	26.61	36.17	26.77	36.06	26.92	45
46	37.21	27.04	37.10	27.20	36.98	27.36	36.86	27.52	46
47	38.02	27.63	37.90	27.79	37.78	27.96	37.66	28.12	47
48	38.83	28.21	38.71	28.38	38.59	28.55	38.46	28.72	48
49	39.64	28.80	39.52	28.97	39.39	29.15	39.26	29.32	49
50	40.45	29.39	40.32	29.57	40.19	29.74	40.06	29.92	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	54 Deg.		53¼ Deg.		53½ Deg.		53¾ Deg.		

Distance.	36 Deg.		36½ Deg.		36¾ Deg.		36¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	41.26	29.98	41.13	30.16	41.00	30.34	40.86	30.51	51
52	42.07	30.56	41.94	30.75	41.80	30.93	41.67	31.11	52
53	42.88	31.15	42.74	31.34	42.60	31.53	42.47	31.71	53
54	43.69	31.74	43.55	31.93	43.41	32.12	43.27	32.31	54
55	44.50	32.33	44.35	32.52	44.21	32.72	44.07	32.91	55
56	45.30	32.92	45.16	33.11	45.02	33.31	44.87	33.51	56
57	46.11	33.50	45.97	33.70	45.82	33.90	45.67	34.10	57
58	46.92	34.09	46.77	34.30	46.62	34.50	46.47	34.70	58
59	47.73	34.68	47.58	34.89	47.43	35.09	47.27	35.30	59
60	48.54	35.27	48.39	35.48	48.23	35.69	48.08	35.90	60
61	49.35	35.85	49.19	36.07	49.04	36.28	48.88	36.50	61
62	50.16	36.44	50.00	36.66	49.84	36.88	49.68	37.10	62
63	50.97	37.03	50.81	37.25	50.64	37.47	50.48	37.69	63
64	51.78	37.62	51.61	37.84	51.45	38.07	51.28	38.29	64
65	52.59	38.21	52.42	38.44	52.25	38.66	52.08	38.89	65
66	53.40	38.79	53.23	39.03	53.05	39.26	52.88	39.49	66
67	54.20	39.38	54.03	39.62	53.86	39.85	53.68	40.09	67
68	55.01	39.97	54.84	40.21	54.66	40.45	54.49	40.69	68
69	55.82	40.56	55.64	40.80	55.47	41.04	55.29	41.28	69
70	56.63	41.14	56.45	41.39	56.27	41.64	56.09	41.88	70
71	57.44	41.73	57.26	41.98	57.07	42.23	56.89	42.48	71
72	58.25	42.32	58.06	42.57	57.88	42.83	57.69	43.08	72
73	59.06	42.91	58.87	43.17	58.68	43.42	58.49	43.68	73
74	59.87	43.50	59.68	43.76	59.49	44.02	59.29	44.28	74
75	60.68	44.08	60.48	44.35	60.29	44.61	60.09	44.87	75
76	61.49	44.67	61.29	44.94	61.09	45.21	60.90	45.47	76
77	62.29	45.26	62.10	45.53	61.90	45.80	61.70	46.07	77
78	63.10	45.85	62.90	46.12	62.70	46.40	62.50	46.67	78
79	63.91	46.43	63.71	46.71	63.50	46.99	63.30	47.27	79
80	64.72	47.02	64.52	47.30	64.31	47.59	64.10	47.87	80
81	65.53	47.61	65.32	47.90	65.11	48.18	64.90	48.46	81
82	66.34	48.20	66.13	48.49	65.92	48.78	65.70	49.06	82
83	67.15	48.79	66.93	49.08	66.72	49.37	66.50	49.66	83
84	67.96	49.37	67.74	49.67	67.52	49.97	67.31	50.26	84
85	68.77	49.96	68.55	50.26	68.33	50.56	68.11	50.86	85
86	69.58	50.55	69.35	50.85	69.13	51.15	68.91	51.46	86
87	70.38	51.14	70.16	51.44	69.94	51.75	69.71	52.05	87
88	71.19	51.73	70.97	52.04	70.74	52.34	70.51	52.65	88
89	72.00	52.31	71.77	52.63	71.54	52.94	71.31	53.25	89
90	72.81	52.90	72.58	53.22	72.35	53.53	72.11	53.85	90
91	73.62	53.49	73.39	53.81	73.15	54.13	72.91	54.45	91
92	74.43	54.08	74.19	54.40	73.95	54.72	73.72	55.05	92
93	75.24	54.66	75.00	54.99	74.76	55.32	74.52	55.64	93
94	76.05	55.25	75.81	55.58	75.56	55.91	75.32	56.24	94
95	76.86	55.84	76.61	56.17	76.37	56.51	76.12	56.84	95
96	77.67	56.43	77.42	56.77	77.17	57.10	76.92	57.44	96
97	78.47	57.02	78.23	57.36	77.97	57.70	77.72	58.04	97
98	79.28	57.60	79.03	57.95	78.78	58.29	78.52	58.64	98
99	80.09	58.19	79.84	58.54	79.58	58.89	79.32	59.23	99
100	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	54 Deg.		53¾ Deg.		53½ Deg.		53¼ Deg.		

Distance.	37 Deg.		37 $\frac{1}{4}$ Deg.		37 $\frac{1}{2}$ Deg.		37 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.80	0.60	0.80	0.61	0.79	0.61	0.79	0.61	1
2	1.60	1.20	1.59	1.21	1.59	1.22	1.58	1.22	2
3	2.40	1.81	2.39	1.82	2.38	1.83	2.37	1.84	3
4	3.19	2.41	3.18	2.42	3.17	2.43	3.16	2.45	4
5	3.99	3.01	3.98	3.03	3.97	3.04	3.95	3.06	5
6	4.79	3.61	4.78	3.63	4.76	3.65	4.74	3.67	6
7	5.59	4.21	5.57	4.24	5.55	4.26	5.53	4.29	7
8	6.39	4.81	6.37	4.84	6.35	4.87	6.33	4.90	8
9	7.19	5.42	7.16	5.45	7.14	5.48	7.12	5.51	9
10	7.99	6.02	7.96	6.05	7.93	6.09	7.91	6.12	10
11	8.78	6.62	8.76	6.66	8.73	6.70	8.70	6.73	11
12	9.58	7.22	9.55	7.26	9.52	7.31	9.49	7.35	12
13	10.38	7.82	10.35	7.87	10.31	7.91	10.28	7.96	13
14	11.18	8.43	11.14	8.47	11.11	8.52	11.07	8.57	14
15	11.98	9.03	11.94	9.08	11.90	9.13	11.86	9.18	15
16	12.78	9.63	12.74	9.68	12.69	9.74	12.65	9.80	16
17	13.58	10.23	13.53	10.29	13.49	10.35	13.44	10.41	17
18	14.38	10.83	14.33	10.90	14.28	10.96	14.23	11.02	18
19	15.17	11.43	15.12	11.50	15.07	11.57	15.02	11.63	19
20	15.97	12.04	15.92	12.11	15.87	12.18	15.81	12.24	20
21	16.77	12.64	16.72	12.71	16.66	12.78	16.60	12.86	21
22	17.57	13.24	17.51	13.32	17.45	13.39	17.40	13.47	22
23	18.37	13.84	18.31	13.92	18.25	14.00	18.19	14.08	23
24	19.17	14.44	19.10	14.53	19.04	14.61	18.98	14.69	24
25	19.97	15.05	19.90	15.13	19.83	15.22	19.77	15.31	25
26	20.76	15.65	20.70	15.74	20.63	15.83	20.56	15.92	26
27	21.56	16.25	21.49	16.34	21.42	16.44	21.35	16.53	27
28	22.36	16.85	22.29	16.95	22.21	17.05	22.14	17.14	28
29	23.16	17.45	23.08	17.55	23.01	17.65	22.93	17.75	29
30	23.96	18.05	23.88	18.16	23.80	18.26	23.72	18.37	30
31	24.76	18.66	24.68	18.76	24.59	18.87	24.51	18.98	31
32	25.56	19.26	25.47	19.37	25.39	19.48	25.30	19.59	32
33	26.35	19.86	26.27	19.97	26.18	20.09	26.09	20.20	33
34	27.15	20.46	27.06	20.58	26.97	20.70	26.88	20.82	34
35	27.95	21.06	27.86	21.19	27.77	21.31	27.67	21.43	35
36	28.75	21.67	28.66	21.79	28.56	21.92	28.46	22.04	36
37	29.55	22.27	29.45	22.40	29.35	22.52	29.26	22.65	37
38	30.35	22.87	30.25	23.00	30.15	23.13	30.05	23.26	38
39	31.15	23.47	31.04	23.61	30.94	23.74	30.84	23.88	39
40	31.95	24.07	31.84	24.21	31.73	24.35	31.63	24.49	40
41	32.74	24.67	32.64	24.82	32.53	24.96	32.42	25.10	41
42	33.54	25.28	33.43	25.42	33.32	25.57	33.21	25.71	42
43	34.34	25.88	34.23	26.03	34.11	26.18	34.00	26.33	43
44	35.14	26.48	35.02	26.63	34.91	26.79	34.79	26.94	44
45	35.94	27.08	35.82	27.24	35.70	27.39	35.58	27.55	45
46	36.74	27.68	36.62	27.84	36.49	28.00	36.37	28.16	46
47	37.54	28.29	37.41	28.45	37.29	28.61	37.16	28.77	47
48	38.33	28.89	38.21	29.05	38.08	29.22	37.95	29.39	48
49	39.13	29.49	39.00	29.66	38.87	29.83	38.74	30.00	49
50	39.93	30.09	39.80	30.26	39.67	30.44	39.53	30.61	50
Distance.	53 Deg.		52 $\frac{3}{4}$ Deg.		52 $\frac{1}{2}$ Deg.		52 $\frac{1}{4}$ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

Distance.	37 Deg.		37 $\frac{1}{4}$ Deg.		37 $\frac{1}{2}$ Deg.		37 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	40.73	30.69	40.60	30.87	40.46	31.05	40.33	31.22	51
52	41.53	31.29	41.39	31.48	41.25	31.66	41.12	31.84	52
53	42.33	31.90	42.19	32.08	42.05	32.26	41.91	32.45	53
54	43.13	32.50	42.98	32.69	42.84	32.87	42.70	33.06	54
55	43.92	33.10	43.78	33.29	43.63	33.48	43.49	33.67	55
56	44.72	33.70	44.58	33.90	44.43	34.09	44.28	34.28	56
57	45.52	34.30	45.37	34.50	45.22	34.70	45.07	34.90	57
58	46.32	34.91	46.17	35.11	46.01	35.31	45.86	35.51	58
59	47.12	35.51	46.96	35.71	46.81	35.92	46.65	36.12	59
60	47.92	36.11	47.76	36.32	47.60	36.53	47.44	36.73	60
61	48.72	36.71	48.56	36.92	48.39	37.13	48.23	37.35	61
62	49.52	37.31	49.35	37.53	49.19	37.74	49.02	37.96	62
63	50.31	37.91	50.15	38.13	49.98	38.35	49.81	38.57	63
64	51.11	38.52	50.94	38.74	50.77	38.96	50.60	39.18	64
65	51.91	39.12	51.74	39.34	51.57	39.57	51.39	39.79	65
66	52.71	39.72	52.54	39.95	52.36	40.18	52.19	40.41	66
67	53.51	40.32	53.33	40.55	53.15	40.79	52.98	41.02	67
68	54.31	40.92	54.13	41.16	53.95	41.40	53.77	41.63	68
69	55.11	41.53	54.92	41.77	54.74	42.00	54.56	42.24	69
70	55.90	42.13	55.72	42.37	55.53	42.61	55.35	42.86	70
71	56.70	42.73	56.52	42.98	56.33	43.22	56.14	43.47	71
72	57.50	43.33	57.31	43.58	57.12	43.83	56.93	44.08	72
73	58.30	43.93	58.11	44.19	57.91	44.44	57.72	44.69	73
74	59.10	44.53	58.90	44.79	58.71	45.05	58.51	45.30	74
75	59.90	45.14	59.70	45.40	59.50	45.66	59.30	45.92	75
76	60.70	45.74	60.50	46.00	60.29	46.27	60.09	46.53	76
77	61.49	46.34	61.29	46.61	61.09	46.87	60.88	47.14	77
78	62.29	46.94	62.09	47.21	61.88	47.48	61.67	47.75	78
79	63.09	47.54	62.88	47.82	62.67	48.09	62.46	48.37	79
80	63.89	48.15	63.68	48.42	63.47	48.70	63.26	48.98	80
81	64.69	48.75	64.48	49.03	64.26	49.31	64.05	49.59	81
82	65.49	49.35	65.27	49.63	65.05	49.92	64.84	50.20	82
83	66.29	49.95	66.07	50.24	65.85	50.53	65.63	50.81	83
84	67.09	50.55	66.86	50.84	66.64	51.14	66.42	51.43	84
85	67.88	51.15	67.66	51.45	67.43	51.74	67.21	52.04	85
86	68.68	51.76	68.46	52.06	68.23	52.35	68.00	52.65	86
87	69.48	52.36	69.25	52.66	69.02	52.96	68.79	53.26	87
88	70.28	52.96	70.05	53.27	69.82	53.57	69.58	53.88	88
89	71.08	53.56	70.84	53.87	70.61	54.18	70.37	54.49	89
90	71.88	54.16	71.64	54.48	71.40	54.79	71.16	55.10	90
91	72.68	54.77	72.44	55.08	72.20	55.40	71.95	55.71	91
92	73.47	55.37	73.23	55.69	72.99	56.01	72.74	56.32	92
93	74.27	55.97	74.03	56.29	73.78	56.61	73.53	56.94	93
94	75.07	56.57	74.82	56.90	74.58	57.22	74.32	57.55	94
95	75.87	57.17	75.62	57.50	75.37	57.83	75.12	58.16	95
96	76.67	57.77	76.42	58.11	76.16	58.44	75.91	58.77	96
97	77.47	58.38	77.21	58.71	76.96	59.05	76.70	59.39	97
98	78.27	58.98	78.01	59.32	77.75	59.66	77.49	60.00	98
99	79.06	59.58	78.80	59.92	78.54	60.27	78.28	60.61	99
100	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	53 Deg.		52 $\frac{3}{4}$ Deg.		52 $\frac{1}{2}$ Deg.		52 $\frac{1}{4}$ Deg.		

Distance.	38 Deg.		38½ Deg.		38½ Deg.		38¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.79	0.62	0.79	0.62	0.78	0.62	0.78	0.63	1
2	1.58	1.23	1.57	1.24	1.57	1.24	1.56	1.25	2
3	2.36	1.85	2.36	1.86	2.35	1.87	2.34	1.88	3
4	3.15	2.46	3.14	2.48	3.13	2.49	3.12	2.50	4
5	3.94	3.08	3.93	3.10	3.91	3.11	3.90	3.13	5
6	4.73	3.69	4.71	3.71	4.70	3.74	4.68	3.76	6
7	5.52	4.31	5.50	4.33	5.48	4.36	5.46	4.38	7
8	6.30	4.93	6.28	4.95	6.26	4.98	6.24	5.01	8
9	7.09	5.54	7.07	5.57	7.04	5.60	7.02	5.63	9
10	7.88	6.16	7.85	6.19	7.83	6.23	7.80	6.26	10
11	8.67	6.77	8.64	6.81	8.61	6.85	8.58	6.89	11
12	9.46	7.39	9.42	7.43	9.39	7.47	9.36	7.51	12
13	10.24	8.00	10.21	8.05	10.17	8.09	10.14	8.14	13
14	11.03	8.62	10.99	8.67	10.96	8.72	10.92	8.76	14
15	11.82	9.23	11.78	9.29	11.74	9.34	11.70	9.39	15
16	12.61	9.85	12.57	9.91	12.52	9.96	12.48	10.01	16
17	13.40	10.47	13.35	10.52	13.30	10.58	13.26	10.64	17
18	14.18	11.08	14.14	11.14	14.09	11.21	14.04	11.27	18
19	14.97	11.70	14.92	11.76	14.87	11.83	14.82	11.89	19
20	15.76	12.31	15.71	12.38	15.65	12.45	15.60	12.52	20
21	16.55	12.93	16.49	13.00	16.43	13.07	16.38	13.14	21
22	17.34	13.54	17.28	13.62	17.22	13.70	17.16	13.77	22
23	18.12	14.16	18.06	14.24	18.00	14.32	17.94	14.40	23
24	18.91	14.78	18.85	14.86	18.78	14.94	18.72	15.02	24
25	19.70	15.39	19.63	15.48	19.57	15.56	19.50	15.65	25
26	20.49	16.01	20.42	16.10	20.35	16.19	20.28	16.27	26
27	21.28	16.62	21.20	16.72	21.13	16.81	21.06	16.90	27
28	22.06	17.24	21.99	17.33	21.91	17.43	21.84	17.53	28
29	22.85	17.85	22.77	17.95	22.70	18.05	22.62	18.15	29
30	23.64	18.47	23.56	18.57	23.48	18.68	23.40	18.78	30
31	24.43	19.09	24.34	19.19	24.26	19.30	24.18	19.40	31
32	25.22	19.70	25.13	19.81	25.04	19.92	24.96	20.03	32
33	26.00	20.32	25.92	20.43	25.83	20.54	25.74	20.66	33
34	26.79	20.93	26.70	21.05	26.61	21.17	26.52	21.28	34
35	27.58	21.55	27.49	21.67	27.39	21.79	27.30	21.91	35
36	28.37	22.16	28.27	22.29	28.17	22.41	28.08	22.53	36
37	29.16	22.78	29.06	22.91	28.96	23.03	28.86	23.16	37
38	29.94	23.40	29.84	23.53	29.74	23.66	29.64	23.79	38
39	30.73	24.01	30.63	24.14	30.52	24.28	30.42	24.41	39
40	31.52	24.63	31.41	24.76	31.30	24.90	31.20	25.04	40
41	32.31	25.24	32.20	25.38	32.09	25.52	31.98	25.66	41
42	33.10	25.86	32.98	26.00	32.87	26.15	32.76	26.29	42
43	33.88	26.47	33.77	26.62	33.65	26.77	33.53	26.91	43
44	34.67	27.09	34.55	27.24	34.43	27.39	34.31	27.54	44
45	35.46	27.70	35.34	27.86	35.22	28.01	35.09	28.17	45
46	36.25	28.32	36.12	28.48	36.00	28.64	35.87	28.79	46
47	37.04	28.94	36.91	29.10	36.78	29.26	36.65	29.42	47
48	37.82	29.55	37.70	29.72	37.57	29.88	37.43	30.04	48
49	38.61	30.17	38.48	30.34	38.35	30.50	38.21	30.67	49
50	39.40	30.78	39.27	30.95	39.13	31.13	38.99	31.30	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	52 Deg.		51¾ Deg.		51½ Deg.		51¼ Deg.		



Distance.	38 Deg.		38½ Deg.		38¾ Deg.		39¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	40.19	31.40	40.05	31.57	39.91	31.75	39.77	31.92	51
52	40.98	32.01	40.84	32.19	40.70	32.37	40.55	32.55	52
53	41.76	32.63	41.62	32.81	41.48	32.99	41.33	33.17	53
54	42.55	33.25	42.41	33.43	42.26	33.62	42.11	33.89	54
55	43.34	33.86	43.19	34.05	43.04	34.24	42.89	34.43	55
56	44.13	34.48	43.98	34.67	43.83	34.86	43.67	35.05	56
57	44.92	35.09	44.76	35.29	44.61	35.48	44.45	35.68	57
58	45.70	35.71	45.55	35.91	45.39	36.11	45.23	36.30	58
59	46.49	36.32	46.33	36.53	46.17	36.73	46.01	36.93	59
60	47.28	36.94	47.12	37.15	46.96	37.35	46.79	37.56	60
61	48.07	37.56	47.90	37.76	47.74	37.97	47.57	38.18	61
62	48.86	38.17	48.69	38.38	48.52	38.60	48.35	38.81	62
63	49.64	38.79	49.47	39.00	49.30	39.22	49.13	39.43	63
64	50.43	39.40	50.26	39.62	50.09	39.84	49.91	40.06	64
65	51.22	40.02	51.05	40.24	50.87	40.46	50.69	40.68	65
66	52.01	40.63	51.83	40.86	51.65	41.09	51.47	41.31	66
67	52.80	41.25	52.62	41.48	52.43	41.71	52.25	41.94	67
68	53.58	41.86	53.40	42.10	53.22	42.33	53.03	42.56	68
69	54.37	42.48	54.19	42.72	54.00	42.95	53.81	43.19	69
70	55.16	43.10	54.97	43.34	54.78	43.58	54.59	43.81	70
71	55.95	43.71	55.76	43.96	55.57	44.20	55.37	44.44	71
72	56.74	44.33	56.54	44.57	56.35	44.82	56.15	45.07	72
73	57.52	44.94	57.33	45.19	57.13	45.44	56.93	45.69	73
74	58.31	45.56	58.11	45.81	57.91	46.07	57.71	46.32	74
75	59.10	46.17	58.90	46.43	58.70	46.69	58.49	46.94	75
76	59.89	46.79	59.68	47.05	59.48	47.31	59.27	47.57	76
77	60.68	47.41	60.47	47.67	60.26	47.93	60.05	48.20	77
78	61.46	48.02	61.25	48.29	61.04	48.56	60.83	48.82	78
79	62.25	48.64	62.04	48.91	61.83	49.18	61.61	49.45	79
80	63.04	49.25	62.83	49.53	62.61	49.80	62.39	50.07	80
81	63.83	49.87	63.61	50.15	63.39	50.42	63.17	50.70	81
82	64.62	50.48	64.40	50.77	64.17	51.05	63.95	51.33	82
83	65.40	51.10	65.18	51.38	64.96	51.67	64.73	51.95	83
84	66.19	51.72	65.97	52.00	65.74	52.29	65.51	52.58	84
85	66.98	52.33	66.75	52.62	66.52	52.91	66.29	53.20	85
86	67.77	52.95	67.54	53.24	67.30	53.54	67.07	53.83	86
87	68.56	53.56	68.32	53.86	68.09	54.16	67.85	54.46	87
88	69.34	54.18	69.11	54.48	68.87	54.78	68.63	55.08	88
89	70.13	54.79	69.89	55.10	69.65	55.40	69.41	55.71	89
90	70.92	55.41	70.68	55.72	70.43	56.03	70.19	56.33	90
91	71.71	56.03	71.46	56.34	71.22	56.65	70.97	56.96	91
92	72.50	56.64	72.25	56.96	72.00	57.27	71.75	57.58	92
93	73.28	57.26	73.03	57.58	72.78	57.89	72.53	58.21	93
94	74.07	57.87	73.82	58.19	73.57	58.52	73.31	58.84	94
95	74.86	58.49	74.61	58.81	74.35	59.14	74.09	59.46	95
96	75.65	59.10	75.39	59.43	75.13	59.76	74.87	60.09	96
97	76.44	59.72	76.18	60.05	75.91	60.38	75.65	60.71	97
98	77.22	60.33	76.96	60.67	76.70	61.01	76.43	61.34	98
99	78.01	60.95	77.75	61.29	77.48	61.63	77.21	61.97	99
100	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	52 Deg.		51½ Deg.		51¼ Deg.		51¼ Deg.		

Distance.	39 Deg.		39 $\frac{1}{4}$ Deg.		39 $\frac{1}{2}$ Deg.		39 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.78	0.63	0.77	0.63	0.77	0.64	0.77	0.64	1
2	1.55	1.26	1.55	1.27	1.54	1.27	1.54	1.28	2
3	2.33	1.89	2.32	1.90	2.31	1.91	2.31	1.92	3
4	3.11	2.52	3.10	2.53	3.09	2.54	3.08	2.56	4
5	3.89	3.15	3.87	3.16	3.86	3.18	3.84	3.20	5
6	4.66	3.78	4.65	3.80	4.63	3.82	4.61	3.84	6
7	5.44	4.41	5.42	4.43	5.40	4.45	5.38	4.48	7
8	6.22	5.03	6.20	5.06	6.17	5.09	6.15	5.12	8
9	6.99	5.66	6.97	5.69	6.94	5.72	6.92	5.75	9
10	7.77	6.29	7.74	6.33	7.72	6.36	7.69	6.39	10
11	8.55	6.92	8.52	6.96	8.49	7.00	8.46	7.03	11
12	9.33	7.55	9.29	7.59	9.26	7.63	9.23	7.67	12
13	10.10	8.18	10.07	8.23	10.03	8.27	9.99	8.31	13
14	10.88	8.81	10.84	8.86	10.80	8.91	10.76	8.95	14
15	11.66	9.44	11.62	9.49	11.57	9.54	11.53	9.59	15
16	12.43	10.07	12.39	10.12	12.35	10.18	12.30	10.23	16
17	13.21	10.70	13.16	10.76	13.12	10.81	13.07	10.87	17
18	13.99	11.33	13.94	11.39	13.89	11.45	13.84	11.51	18
19	14.77	11.96	14.71	12.02	14.66	12.09	14.61	12.15	19
20	15.54	12.59	15.49	12.65	15.43	12.72	15.38	12.79	20
21	16.32	13.22	16.26	13.29	16.20	13.36	16.15	13.43	21
22	17.10	13.84	17.04	13.92	16.98	13.99	16.91	14.07	22
23	17.87	14.47	17.81	14.55	17.75	14.63	17.68	14.71	23
24	18.65	15.10	18.59	15.18	18.52	15.27	18.45	15.35	24
25	19.43	15.73	19.36	15.82	19.29	15.90	19.22	15.99	25
26	20.21	16.36	20.13	16.45	20.06	16.54	19.99	16.63	26
27	20.98	16.99	20.91	17.08	20.83	17.17	20.76	17.26	27
28	21.76	17.62	21.68	17.72	21.61	17.81	21.53	17.90	28
29	22.54	18.25	22.46	18.35	22.38	18.45	22.30	18.54	29
30	23.31	18.88	23.23	18.98	23.15	19.08	23.07	19.18	30
31	24.09	19.51	24.01	19.61	23.92	19.72	23.83	19.82	31
32	24.87	20.14	24.78	20.25	24.69	20.35	24.60	20.46	32
33	25.65	20.77	25.55	20.88	25.46	20.99	25.37	21.10	33
34	26.42	21.40	26.33	21.51	26.24	21.63	26.14	21.74	34
35	27.20	22.03	27.10	22.14	27.01	22.26	26.91	22.33	35
36	27.98	22.66	27.88	22.78	27.78	22.90	27.68	23.02	36
37	28.75	23.28	28.65	23.41	28.55	23.53	28.45	23.66	37
38	29.53	23.91	29.43	24.04	29.32	24.17	29.22	24.30	38
39	30.31	24.54	30.20	24.68	30.09	24.81	29.98	24.94	39
40	31.09	25.17	30.98	25.31	30.86	25.44	30.75	25.58	40
41	31.86	25.80	31.75	25.94	31.64	26.08	31.52	26.22	41
42	32.64	26.43	32.52	26.57	32.41	26.72	32.29	26.86	42
43	33.42	27.06	33.30	27.21	33.18	27.35	33.06	27.50	43
44	34.19	27.69	34.07	27.84	33.95	27.99	33.83	28.14	44
45	34.97	28.32	34.85	28.47	34.72	28.62	34.60	28.77	45
46	35.75	28.95	35.62	29.10	35.49	29.26	35.37	29.41	46
47	36.53	29.58	36.40	29.74	36.27	29.90	36.14	30.05	47
48	37.30	30.21	37.17	30.37	37.04	30.53	36.90	30.69	48
49	38.08	30.84	37.95	31.00	37.81	31.17	37.67	31.33	49
50	38.86	31.47	38.72	31.64	38.58	31.80	38.44	31.97	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	51 Deg.		50 $\frac{1}{4}$ Deg.		50 $\frac{1}{2}$ Deg.		50 $\frac{3}{4}$ Deg.		

Distance.	39 Deg.		39 $\frac{1}{4}$ Deg.		39 $\frac{1}{2}$ Deg.		39 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	39.63	32.10	39.49	32.27	39.35	32.44	39.21	32.61	51
52	40.41	32.72	40.27	32.90	40.12	33.08	39.98	33.25	52
53	41.19	33.35	41.04	33.53	40.90	33.71	40.75	33.89	53
54	41.97	33.98	41.82	34.17	41.67	34.35	41.52	34.53	54
55	42.74	34.61	42.59	34.80	42.44	34.98	42.29	35.17	55
56	43.52	35.24	43.37	35.43	43.21	35.62	43.06	35.81	56
57	44.30	35.87	44.14	36.06	43.98	36.26	43.82	36.45	57
58	45.07	36.50	44.91	36.70	44.75	36.89	44.59	37.09	58
59	45.85	37.13	45.69	37.33	45.53	37.53	45.36	37.73	59
60	46.63	37.76	46.46	37.96	46.30	38.16	46.13	38.37	60
61	47.41	38.39	47.24	38.60	47.07	38.80	46.90	39.01	61
62	48.18	39.02	48.01	39.23	47.84	39.44	47.67	39.65	62
63	48.96	39.65	48.79	39.86	48.61	40.07	48.44	40.28	63
64	49.74	40.28	49.56	40.49	49.38	40.71	49.21	40.92	64
65	50.51	40.91	50.34	41.13	50.16	41.35	49.97	41.56	65
66	51.29	41.54	51.11	41.76	50.93	41.98	50.74	42.20	66
67	52.07	42.16	51.88	42.39	51.70	42.62	51.51	42.84	67
68	52.85	42.79	52.66	43.02	52.47	43.25	52.28	43.48	68
69	53.52	43.42	53.43	43.66	53.24	43.89	53.05	44.12	69
70	54.40	44.05	54.21	44.29	54.01	44.53	53.82	44.76	70
71	55.18	44.68	54.98	44.92	54.79	45.16	54.59	45.40	71
72	55.95	45.31	55.76	45.55	55.56	45.80	55.36	46.04	72
73	56.73	45.94	56.53	46.19	56.33	46.43	56.13	46.68	73
74	57.51	46.57	57.31	46.82	57.10	47.07	56.89	47.32	74
75	58.29	47.20	58.08	47.45	57.87	47.71	57.66	47.96	75
76	59.06	47.83	58.85	48.09	58.64	48.34	58.43	48.60	76
77	59.84	48.46	59.63	48.72	59.42	48.98	59.20	49.24	77
78	60.62	49.09	60.40	49.35	60.19	49.61	59.97	49.88	78
79	61.39	49.72	61.18	49.98	60.96	50.25	60.74	50.52	79
80	62.17	50.35	61.95	50.62	61.73	50.89	61.51	51.16	80
81	62.95	50.97	62.73	51.25	62.50	51.52	62.28	51.79	81
82	63.73	51.60	63.50	51.88	63.27	52.16	63.04	52.43	82
83	64.50	52.23	64.27	52.51	64.04	52.79	63.81	53.07	83
84	65.28	52.86	65.05	53.15	64.82	53.43	64.58	53.71	84
85	66.06	53.49	65.82	53.78	65.59	54.07	65.35	54.35	85
86	66.83	54.12	66.60	54.41	66.36	54.70	66.12	54.99	86
87	67.61	54.75	67.37	55.05	67.13	55.34	66.89	55.63	87
88	68.39	55.38	68.15	55.68	67.90	55.97	67.66	56.27	88
89	69.17	56.01	68.92	56.32	68.67	56.61	68.43	56.91	89
90	69.94	56.64	69.70	56.94	69.45	57.25	69.20	57.55	90
91	70.72	57.27	70.47	57.58	70.22	57.88	69.96	58.19	91
92	71.50	57.90	71.24	58.21	70.99	58.52	70.73	58.83	92
93	72.27	58.53	72.02	58.84	71.76	59.16	71.50	59.47	93
94	73.05	59.16	72.79	59.47	72.53	59.79	72.27	60.11	94
95	73.83	59.79	73.57	60.11	73.30	60.43	73.04	60.75	95
96	74.61	60.41	74.34	60.74	74.08	61.06	73.81	61.39	96
97	75.38	61.04	75.12	61.37	74.85	61.70	74.58	62.03	97
98	76.16	61.67	75.89	62.01	75.62	62.34	75.35	62.66	98
99	76.94	62.30	76.66	62.64	76.39	62.97	76.12	63.30	99
100	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	51 Deg.		50 $\frac{3}{4}$ Deg.		50 $\frac{1}{2}$ Deg.		50 $\frac{1}{4}$ Deg.		

## TRAVERSE TABLE

Distance.	40 Deg.		40½ Deg.		40¾ Deg.		40¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.77	0.64	0.76	0.65	0.76	0.65	0.76	0.65	1
2	1.53	1.29	1.53	1.29	1.52	1.30	1.52	1.31	2
3	2.30	1.93	2.29	1.94	2.28	1.95	2.27	1.96	3
4	3.06	2.57	3.05	2.58	3.04	2.60	3.03	2.61	4
5	3.83	3.21	3.82	3.23	3.80	3.25	3.79	3.26	5
6	4.60	3.86	4.58	3.88	4.56	3.90	4.55	3.92	6
7	5.36	4.50	5.34	4.52	5.32	4.55	5.30	4.57	7
8	6.13	5.14	6.11	5.17	6.08	5.20	6.06	5.22	8
9	6.89	5.79	6.87	5.82	6.84	5.84	6.82	5.87	9
10	7.66	6.43	7.63	6.46	7.60	6.49	7.58	6.53	10
11	8.43	7.07	8.40	7.11	8.36	7.14	8.33	7.18	11
12	9.19	7.71	9.16	7.75	9.12	7.79	9.09	7.83	12
13	9.96	8.36	9.92	8.40	9.89	8.44	9.85	8.49	13
14	10.72	9.00	10.69	9.05	10.65	9.09	10.61	9.14	14
15	11.49	9.64	11.45	9.69	11.41	9.74	11.36	9.79	15
16	12.26	10.28	12.21	10.34	12.17	10.39	12.12	10.44	16
17	13.02	10.93	12.97	10.98	12.93	11.04	12.88	11.10	17
18	13.79	11.57	13.74	11.63	13.69	11.69	13.64	11.75	18
19	14.55	12.21	14.50	12.28	14.45	12.34	14.39	12.40	19
20	15.32	12.86	15.26	12.92	15.21	12.99	15.15	13.06	20
21	16.09	13.50	16.03	13.57	15.97	13.64	15.91	13.71	21
22	16.85	14.14	16.79	14.21	16.73	14.29	16.67	14.36	22
23	17.62	14.78	17.55	14.86	17.49	14.94	17.42	15.01	23
24	18.39	15.43	18.32	15.51	18.25	15.59	18.18	15.67	24
25	19.15	16.07	19.08	16.15	19.01	16.24	18.94	16.32	25
26	19.92	16.71	19.84	16.80	19.77	16.89	19.70	16.97	26
27	20.68	17.36	20.61	17.45	20.53	17.54	20.45	17.62	27
28	21.45	18.00	21.37	18.09	21.29	18.18	21.21	18.28	28
29	22.22	18.64	22.13	18.74	22.05	18.83	21.97	18.93	29
30	22.98	19.28	22.90	19.38	22.81	19.48	22.73	19.58	30
31	23.75	19.93	23.66	20.03	23.57	20.13	23.48	20.24	31
32	24.51	20.57	24.42	20.68	24.33	20.78	24.24	20.89	32
33	25.28	21.21	25.19	21.32	25.09	21.43	25.00	21.54	33
34	26.05	21.85	25.95	21.97	25.85	22.08	25.76	22.19	34
35	26.81	22.50	26.71	22.61	26.61	22.73	26.51	22.85	35
36	27.58	23.14	27.48	23.26	27.37	23.38	27.27	23.50	36
37	28.34	23.78	28.24	23.91	28.13	24.03	28.03	24.15	37
38	29.11	24.43	29.00	24.55	28.90	24.68	28.79	24.80	38
39	29.88	25.07	29.77	25.20	29.66	25.33	29.54	25.46	39
40	30.64	25.71	30.53	25.84	30.42	25.98	30.30	26.11	40
41	31.41	26.35	31.29	26.49	31.18	26.63	31.06	26.76	41
42	32.17	27.00	32.06	27.14	31.94	27.28	31.82	27.42	42
43	32.94	27.64	32.82	27.78	32.70	27.93	32.58	28.07	43
44	33.71	28.28	33.58	28.43	33.46	28.58	33.33	28.72	44
45	34.47	28.93	34.35	29.08	34.22	29.23	34.09	29.37	45
46	35.24	29.57	35.11	29.72	34.98	29.87	34.85	30.03	46
47	36.00	30.21	35.87	30.37	35.74	30.52	35.61	30.68	47
48	36.77	30.85	36.64	31.01	36.50	31.17	36.36	31.33	48
49	37.54	31.50	37.40	31.66	37.26	31.82	37.12	31.99	49
50	38.30	32.14	38.16	32.31	38.02	32.47	37.88	32.64	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	50 Deg.		49¾ Deg.		49½ Deg.		49¼ Deg.		

Distance.	40 Deg.		40 $\frac{1}{4}$ Deg.		40 $\frac{1}{2}$ Deg.		40 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	39.07	32.78	38.92	32.95	38.78	33.12	38.64	33.29	51
52	39.83	33.42	39.69	33.60	39.54	33.77	39.39	33.94	52
53	40.60	34.07	40.45	34.24	40.30	34.42	40.15	34.60	53
54	41.37	34.71	41.21	34.89	41.06	35.07	40.91	35.25	54
55	42.13	35.35	41.98	35.54	41.82	35.72	41.67	35.90	55
56	42.90	36.00	42.74	36.18	42.58	36.37	42.42	36.55	56
57	43.66	36.64	43.50	36.83	43.34	37.02	43.18	37.21	57
58	44.43	37.28	44.27	37.48	44.10	37.67	43.94	37.86	58
59	45.20	37.92	45.03	38.12	44.86	38.32	44.70	38.51	59
60	45.96	38.57	45.79	38.77	45.62	38.97	45.45	39.17	60
61	46.73	39.21	46.56	39.41	46.38	39.62	46.21	39.82	61
62	47.49	39.85	47.32	40.06	47.15	40.27	46.97	40.47	62
63	48.26	40.50	48.08	40.71	47.91	40.92	47.73	41.12	63
64	49.03	41.14	48.85	41.35	48.67	41.56	48.48	41.78	64
65	49.79	41.78	49.61	42.00	49.43	42.21	49.24	42.43	65
66	50.56	42.42	50.37	42.64	50.19	42.86	50.00	43.08	66
67	51.32	43.07	51.14	43.29	50.95	43.51	50.76	43.73	67
68	52.09	43.71	51.90	43.94	51.71	44.16	51.51	44.39	68
69	52.86	44.35	52.66	44.58	52.47	44.81	52.27	45.04	69
70	53.62	45.00	53.43	45.23	53.23	45.46	53.03	45.69	70
71	54.39	45.64	54.19	45.87	53.99	46.11	53.79	46.35	71
72	55.16	46.28	54.95	46.52	54.75	46.76	54.54	47.00	72
73	55.92	46.92	55.72	47.17	55.51	47.41	55.30	47.65	73
74	56.69	47.57	56.48	47.81	56.27	48.06	56.06	48.30	74
75	57.45	48.21	57.24	48.46	57.03	48.71	56.82	48.96	75
76	58.22	48.85	58.01	49.11	57.79	49.36	57.57	49.61	76
77	58.99	49.49	58.77	49.75	58.55	50.01	58.33	50.26	77
78	59.75	50.14	59.53	50.40	59.31	50.66	59.09	50.92	78
79	60.52	50.78	60.30	51.04	60.07	51.31	59.85	51.57	79
80	61.28	51.42	61.06	51.69	60.83	51.96	60.61	52.22	80
81	62.05	52.07	61.82	52.34	61.59	52.61	61.36	52.87	81
82	62.82	52.71	62.59	52.98	62.35	53.25	62.12	53.53	82
83	63.58	53.35	63.35	53.63	63.11	53.90	62.88	54.18	83
84	64.35	53.99	64.11	54.27	63.87	54.55	63.64	54.83	84
85	65.11	54.64	64.87	54.92	64.63	55.20	64.39	55.48	85
86	65.88	55.28	65.64	55.57	65.39	55.85	65.15	56.14	86
87	66.65	55.92	66.40	56.21	66.16	56.50	65.91	56.79	87
88	67.41	56.57	67.16	56.86	66.92	57.15	66.67	57.44	88
89	68.18	57.21	67.93	57.50	67.68	57.80	67.42	58.10	89
90	68.94	57.85	68.69	58.15	68.44	58.45	68.18	58.75	90
91	69.71	58.49	69.45	58.80	69.20	59.10	68.94	59.40	91
92	70.48	59.14	70.22	59.44	69.96	59.75	69.70	60.05	92
93	71.24	59.78	70.98	60.09	70.72	60.40	70.45	60.71	93
94	72.01	60.42	71.74	60.74	71.48	61.05	71.21	61.36	94
95	72.77	61.06	72.51	61.38	72.24	61.70	71.97	62.01	95
96	73.54	61.71	73.27	62.03	73.00	62.35	72.73	62.66	96
97	74.31	62.35	74.03	62.67	73.76	63.00	73.48	63.32	97
98	75.07	62.99	74.80	63.32	74.52	63.65	74.24	63.97	98
99	75.84	63.64	75.56	63.97	75.28	64.30	75.00	64.62	99
100	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	100
Distance.	50 Deg.		49 $\frac{3}{4}$ Deg.		49 $\frac{1}{2}$ Deg.		49 $\frac{1}{4}$ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

Distance.	41 Deg.		41 $\frac{1}{4}$ Deg.		41 $\frac{1}{2}$ Deg.		41 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.75	0.66	0.75	0.66	0.75	0.66	0.75	0.67	1
2	1.51	1.31	1.50	1.32	1.50	1.33	1.49	1.33	2
3	2.26	1.97	2.26	1.98	2.25	1.99	2.24	2.00	3
4	3.02	2.62	3.01	2.64	3.00	2.65	2.98	2.66	4
5	3.77	3.28	3.76	3.30	3.74	3.31	3.73	3.33	5
6	4.53	3.94	4.51	3.96	4.49	3.98	4.48	4.00	6
7	5.28	4.59	5.26	4.62	5.24	4.64	5.22	4.66	7
8	6.04	5.25	6.01	5.27	5.99	5.30	5.97	5.33	8
9	6.79	5.90	6.77	5.93	6.74	5.96	6.71	5.99	9
10	7.55	6.56	7.52	6.59	7.49	6.63	7.46	6.66	10
11	8.30	7.22	8.27	7.25	8.24	7.29	8.21	7.32	11
12	9.06	7.87	9.02	7.91	8.99	7.95	8.95	7.99	12
13	9.81	8.53	9.77	8.57	9.74	8.61	9.70	8.66	13
14	10.57	9.18	10.53	9.23	10.49	9.28	10.44	9.32	14
15	11.32	9.84	11.28	9.89	11.23	9.94	11.19	9.99	15
16	12.08	10.50	12.03	10.55	11.98	10.60	11.94	10.65	16
17	12.83	11.15	12.78	11.21	12.73	11.26	12.68	11.32	17
18	13.58	11.81	13.53	11.87	13.48	11.93	13.43	11.99	18
19	14.34	12.47	14.28	12.53	14.23	12.59	14.18	12.65	19
20	15.09	13.12	15.04	13.19	14.98	13.25	14.92	13.32	20
21	15.85	13.78	15.79	13.85	15.73	13.91	15.67	13.98	21
22	16.60	14.43	16.54	14.51	16.48	14.58	16.41	14.65	22
23	17.36	15.09	17.29	15.16	17.23	15.24	17.16	15.32	23
24	18.11	15.75	18.04	15.82	17.97	15.90	17.91	15.98	24
25	18.87	16.40	18.80	16.48	18.72	16.57	18.65	16.65	25
26	19.62	17.06	19.55	17.14	19.47	17.23	19.40	17.31	26
27	20.38	17.71	20.30	17.80	20.22	17.89	20.14	17.98	27
28	21.13	18.37	21.05	18.46	20.97	18.55	20.89	18.64	28
29	21.89	19.03	21.80	19.12	21.72	19.22	21.64	19.31	29
30	22.64	19.68	22.56	19.78	22.47	19.88	22.38	19.98	30
31	23.40	20.34	23.31	20.44	23.22	20.54	23.13	20.64	31
32	24.15	20.99	24.06	21.10	23.97	21.20	23.87	21.31	32
33	24.91	21.65	24.81	21.76	24.72	21.87	24.62	21.97	33
34	25.66	22.31	25.56	22.42	25.46	22.53	25.37	22.64	34
35	26.41	22.96	26.31	23.08	26.21	23.19	26.11	23.31	35
36	27.17	23.62	27.07	23.74	26.96	23.85	26.86	23.97	36
37	27.92	24.27	27.82	24.40	27.71	24.52	27.60	24.64	37
38	28.68	24.93	28.57	25.06	28.46	25.18	28.35	25.30	38
39	29.43	25.59	29.32	25.71	29.21	25.84	29.10	25.97	39
40	30.19	26.24	30.07	26.37	29.96	26.50	29.84	26.64	40
41	30.94	26.90	30.83	27.03	30.71	27.17	30.59	27.30	41
42	31.70	27.55	31.58	27.69	31.46	27.83	31.33	27.97	42
43	32.45	28.21	32.33	28.35	32.21	28.49	32.08	28.63	43
44	33.21	28.87	33.08	29.01	32.95	29.16	32.83	29.30	44
45	33.96	29.52	33.83	29.67	33.70	29.82	33.57	29.97	45
46	34.72	30.18	34.58	30.33	34.45	30.48	34.32	30.63	46
47	35.47	30.83	35.34	30.99	35.20	31.14	35.06	31.30	47
48	36.23	31.49	36.09	31.65	35.95	31.81	35.81	31.96	48
49	36.98	32.15	36.84	32.31	36.70	32.47	36.56	32.63	49
50	37.74	32.80	37.59	32.97	37.45	33.13	37.30	33.29	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	49 Deg.		48 $\frac{3}{4}$ Deg.		48 $\frac{1}{2}$ Deg.		48 $\frac{1}{4}$ Deg.		

Distance.	41 Deg.		41 $\frac{1}{4}$ Deg.		41 $\frac{1}{2}$ Deg.		41 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	38.49	33.46	38.34	33.63	38.20	33.79	38.05	33.96	51
52	39.24	34.12	39.10	34.29	38.95	34.46	38.79	34.63	52
53	40.00	34.77	39.85	34.95	39.69	35.12	39.54	35.29	53
54	40.75	35.43	40.60	35.60	40.44	35.78	40.29	35.96	54
55	41.51	36.08	41.35	36.26	41.19	36.44	41.03	36.62	55
56	42.26	36.74	42.10	36.92	41.94	37.11	41.78	37.29	56
57	43.02	37.40	42.85	37.58	42.69	37.77	42.53	37.96	57
58	43.77	38.05	43.61	38.24	43.44	38.43	43.27	38.62	58
59	44.53	38.71	44.36	38.90	44.19	39.09	44.02	39.29	59
60	45.28	39.36	45.11	39.56	44.94	39.76	44.76	39.95	60
61	46.04	40.02	45.86	40.22	45.69	40.42	45.51	40.62	61
62	46.79	40.68	46.61	40.88	46.44	41.08	46.26	41.28	62
63	47.55	41.33	47.37	41.54	47.18	41.75	47.00	41.95	63
64	48.30	41.99	48.12	42.20	47.93	42.41	47.75	42.62	64
65	49.06	42.64	48.87	42.86	48.68	43.07	48.49	43.28	65
66	49.81	43.30	49.62	43.52	49.43	43.73	49.24	43.95	66
67	50.57	43.96	50.37	44.18	50.18	44.40	49.99	44.61	67
68	51.32	44.61	51.13	44.84	50.93	45.06	50.73	45.28	68
69	52.07	45.27	51.88	45.49	51.68	45.72	51.48	45.95	69
70	52.83	45.92	52.63	46.15	52.43	46.38	52.22	46.61	70
71	53.58	46.58	53.38	46.81	53.18	47.05	52.97	47.28	71
72	54.34	47.24	54.13	47.47	53.92	47.71	53.72	47.94	72
73	55.09	47.89	54.88	48.13	54.67	48.37	54.46	48.61	73
74	55.85	48.55	55.64	48.79	55.42	49.03	55.21	49.28	74
75	56.60	49.20	56.39	49.45	56.17	49.70	55.95	49.94	75
76	57.36	49.86	57.14	50.11	56.92	50.36	56.70	50.61	76
77	58.11	50.52	57.89	50.77	57.67	51.02	57.45	51.27	77
78	58.87	51.17	58.64	51.43	58.42	51.68	58.19	51.94	78
79	59.62	51.83	59.40	52.09	59.17	52.35	58.94	52.60	79
80	60.38	52.48	60.15	52.75	59.92	53.01	59.68	53.27	80
81	61.13	53.14	60.90	53.41	60.67	53.67	60.43	53.94	81
82	61.89	53.80	61.65	54.07	61.41	54.33	61.18	54.60	82
83	62.64	54.45	62.40	54.73	62.16	55.00	61.92	55.27	83
84	63.40	55.11	63.15	55.38	62.91	55.66	62.67	55.93	84
85	64.15	55.76	63.91	56.04	63.66	56.32	63.41	56.60	85
86	64.90	56.42	64.66	56.70	64.41	56.99	64.16	57.27	86
87	65.66	57.08	65.41	57.36	65.16	57.65	64.91	57.93	87
88	66.41	57.73	66.16	58.02	65.91	58.31	65.65	58.60	88
89	67.17	58.39	66.91	58.68	66.66	58.97	66.40	59.26	89
90	67.92	59.05	67.67	59.34	67.41	59.64	67.15	59.93	90
91	68.68	59.70	68.42	60.00	68.15	60.30	67.89	60.60	91
92	69.43	60.36	69.17	60.66	68.90	60.96	68.64	61.26	92
93	70.19	61.01	69.92	61.32	69.65	61.62	69.38	61.93	93
94	70.94	61.67	70.67	61.98	70.40	62.29	70.13	62.59	94
95	71.70	62.33	71.43	62.64	71.15	62.95	70.88	63.26	95
96	72.45	62.98	72.18	63.30	71.90	63.61	71.62	63.92	96
97	73.21	63.64	72.93	63.96	72.65	64.27	72.37	64.59	97
98	73.96	64.29	73.68	64.62	73.40	64.94	73.11	65.26	98
99	74.72	64.95	74.43	65.28	74.15	65.60	73.86	65.92	99
100	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	49 Deg.		48 $\frac{3}{4}$ Deg.		48 $\frac{1}{2}$ Deg.		48 $\frac{1}{4}$ Deg.		

Distance.	42 Deg.		42 $\frac{1}{4}$ Deg.		42 $\frac{1}{2}$ Deg.		42 $\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.74	0.67	0.74	0.67	0.74	0.68	0.73	0.68	1
2	1.49	1.34	1.48	1.34	1.47	1.35	1.47	1.36	2
3	2.23	2.01	2.22	2.02	2.21	2.03	2.20	2.04	3
4	2.97	2.68	2.96	2.69	2.95	2.70	2.94	2.72	4
5	3.72	3.35	3.70	3.36	3.69	3.38	3.67	3.39	5
6	4.46	4.01	4.44	4.03	4.42	4.05	4.41	4.07	6
7	5.20	4.68	5.18	4.71	5.16	4.73	5.14	4.75	7
8	5.95	5.35	5.92	5.38	5.90	5.40	5.87	5.43	8
9	6.69	6.02	6.66	6.05	6.64	6.08	6.61	6.11	9
10	7.43	6.69	7.40	6.72	7.37	6.76	7.34	6.79	10
11	8.17	7.36	8.14	7.40	8.11	7.43	8.08	7.47	11
12	8.92	8.03	8.88	8.07	8.85	8.11	8.81	8.15	12
13	9.66	8.70	9.62	8.74	9.58	8.78	9.55	8.82	13
14	10.40	9.37	10.36	9.41	10.32	9.46	10.28	9.50	14
15	11.15	10.04	11.10	10.09	11.06	10.13	11.01	10.18	15
16	11.89	10.71	11.84	10.76	11.80	10.81	11.75	10.86	16
17	12.63	11.38	12.58	11.43	12.53	11.48	12.48	11.54	17
18	13.38	12.04	13.32	12.10	13.27	12.16	13.22	12.22	18
19	14.12	12.71	14.06	12.77	14.01	12.84	13.95	12.90	19
20	14.86	13.38	14.80	13.45	14.75	13.51	14.69	13.58	20
21	15.61	14.05	15.54	14.12	15.48	14.19	15.42	14.25	21
22	16.35	14.72	16.28	14.79	16.22	14.86	16.16	14.93	22
23	17.09	15.39	17.02	15.46	16.96	15.54	16.89	15.61	23
24	17.84	16.06	17.77	16.14	17.69	16.21	17.62	16.29	24
25	18.58	16.73	18.51	16.81	18.43	16.89	18.36	16.97	25
26	19.32	17.40	19.25	17.48	19.17	17.57	19.09	17.65	26
27	20.06	18.07	19.99	18.15	19.91	18.24	19.83	18.33	27
28	20.81	18.74	20.73	18.83	20.64	18.92	20.56	19.01	28
29	21.55	19.40	21.47	19.50	21.38	19.59	21.30	19.69	29
30	22.29	20.07	22.21	20.17	22.12	20.27	22.03	20.36	30
31	23.04	20.74	22.95	20.84	22.86	20.94	22.76	21.04	31
32	23.78	21.41	23.69	21.52	23.59	21.62	23.50	21.72	32
33	24.52	22.08	24.43	22.19	24.33	22.29	24.23	22.40	33
34	25.27	22.75	25.17	22.86	25.07	22.97	24.97	23.08	34
35	26.01	23.42	25.91	23.53	25.80	23.65	25.70	23.76	35
36	26.75	24.09	26.65	24.21	26.54	24.32	26.44	24.44	36
37	27.50	24.76	27.39	24.88	27.28	25.00	27.17	25.12	37
38	28.24	25.43	28.13	25.55	28.02	25.67	27.90	25.79	38
39	28.98	26.10	28.87	26.22	28.75	26.35	28.64	26.47	39
40	29.73	26.77	29.61	26.89	29.49	27.02	29.37	27.15	40
41	30.47	27.43	30.35	27.57	30.23	27.70	30.11	27.83	41
42	31.21	28.10	31.09	28.24	30.97	28.37	30.84	28.51	42
43	31.96	28.77	31.83	28.91	31.70	29.05	31.58	29.19	43
44	32.70	29.44	32.57	29.58	32.44	29.73	32.31	29.87	44
45	33.44	30.11	33.31	30.26	33.18	30.40	33.04	30.55	45
46	34.18	30.78	34.05	30.93	33.91	31.08	33.78	31.22	46
47	34.93	31.45	34.79	31.60	34.65	31.75	34.51	31.90	47
48	35.67	32.12	35.53	32.27	35.39	32.43	35.25	32.58	48
49	36.41	32.79	36.27	32.95	36.13	33.10	35.98	33.26	49
50	37.16	33.46	37.01	33.62	36.86	33.78	36.72	33.94	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	48 Deg.		47 $\frac{3}{4}$ Deg.		47 $\frac{1}{2}$ Deg.		47 $\frac{1}{4}$ Deg.		



Distance.	42 Deg.		42½ Deg.		42¾ Deg.		42¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	37.90	34.13	37.75	34.29	37.60	34.46	37.45	34.62	51
52	38.64	34.79	38.49	34.96	38.34	35.13	38.18	35.30	52
53	39.39	35.46	39.23	35.64	39.08	35.81	38.92	35.98	53
54	40.13	36.13	39.97	36.31	39.81	36.48	39.65	36.66	54
55	40.87	36.80	40.71	36.98	40.55	37.16	40.39	37.33	55
56	41.62	37.47	41.45	37.65	41.29	37.83	41.12	38.01	56
57	42.36	38.14	42.19	38.32	42.02	38.51	41.86	38.69	57
58	43.10	38.81	42.93	39.00	42.76	39.18	42.59	39.37	58
59	43.85	39.48	43.67	39.67	43.50	39.86	43.32	40.05	59
60	44.59	40.15	44.41	40.34	44.24	40.54	44.06	40.73	60
61	45.33	40.82	45.15	41.01	44.97	41.21	44.79	41.41	61
62	46.07	41.49	45.89	41.69	45.71	41.89	45.53	42.09	62
63	46.82	42.16	46.63	42.36	46.45	42.56	46.26	42.76	63
64	47.56	42.82	47.37	43.03	47.19	43.24	47.00	43.44	64
65	48.30	43.49	48.11	43.70	47.92	43.91	47.73	44.12	65
66	49.05	44.16	48.85	44.38	48.66	44.59	48.47	44.80	66
67	49.79	44.83	49.59	45.05	49.40	45.26	49.20	45.48	67
68	50.53	45.50	50.33	45.72	50.13	45.94	49.93	46.16	68
69	51.28	46.17	51.07	46.39	50.87	46.62	50.67	46.84	69
70	52.02	46.84	51.82	47.07	51.61	47.29	51.40	47.52	70
71	52.76	47.51	52.56	47.74	52.35	47.97	52.14	48.19	71
72	53.51	48.18	53.30	48.41	53.08	48.64	52.87	48.87	72
73	54.25	48.85	54.04	49.08	53.82	49.32	53.61	49.55	73
74	54.99	49.52	54.78	49.76	54.56	49.99	54.34	50.23	74
75	55.74	50.18	55.52	50.43	55.30	50.67	55.07	50.91	75
76	56.48	50.85	56.26	51.10	56.03	51.34	55.81	51.59	76
77	57.22	51.52	57.00	51.77	56.77	52.02	56.54	52.27	77
78	57.97	52.19	57.74	52.44	57.51	52.70	57.28	52.95	78
79	58.71	52.86	58.48	53.12	58.24	53.37	58.01	53.63	79
80	59.45	53.53	59.22	53.79	58.98	54.05	58.75	54.30	80
81	60.19	54.20	59.96	54.46	59.72	54.72	59.48	54.98	81
82	60.94	54.87	60.70	55.13	60.46	55.40	60.21	55.66	82
83	61.68	55.54	61.44	55.81	61.19	56.07	60.95	56.34	83
84	62.42	56.21	62.18	56.48	61.93	56.75	61.68	57.02	84
85	63.17	56.88	62.92	57.15	62.67	57.43	62.42	57.70	85
86	63.91	57.55	63.66	57.82	63.41	58.10	63.15	58.38	86
87	64.65	58.21	64.40	58.50	64.14	58.78	63.89	59.06	87
88	65.40	58.88	65.14	59.17	64.88	59.45	64.62	59.73	88
89	66.14	59.55	65.88	59.84	65.62	60.13	65.35	60.41	89
90	66.88	60.22	66.62	60.51	66.35	60.80	66.09	61.09	90
91	67.63	60.89	67.36	61.19	67.09	61.48	66.82	61.77	91
92	68.37	61.56	68.10	61.86	67.83	62.15	67.56	62.45	92
93	69.11	62.23	68.84	62.53	68.57	62.83	68.29	63.13	93
94	69.86	62.90	69.58	63.20	69.30	63.51	69.03	63.81	94
95	70.60	63.57	70.32	63.87	70.04	64.18	69.76	64.49	95
96	71.34	64.24	71.06	64.55	70.78	64.86	70.49	65.16	96
97	72.08	64.91	71.80	65.22	71.52	65.53	71.23	65.84	97
98	72.83	65.57	72.54	65.89	72.25	66.21	71.96	66.52	98
99	73.57	66.24	73.28	66.56	72.99	66.88	72.70	67.20	99
100	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	48 Deg.		47¾ Deg.		47½ Deg.		47¼ Deg.		

Distance.	43 Deg.		43¼ Deg.		43½ Deg.		43¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.73	0.68	0.73	0.69	0.73	0.69	0.72	0.69	1
2	1.46	1.36	1.46	1.37	1.45	1.38	1.44	1.38	2
3	2.19	2.05	2.19	2.06	2.18	2.07	2.17	2.07	3
4	2.93	2.73	2.91	2.74	2.90	2.75	2.89	2.77	4
5	3.66	3.41	3.64	3.43	3.63	3.44	3.61	3.46	5
6	4.39	4.09	4.37	4.11	4.35	4.13	4.33	4.15	6
7	5.12	4.77	5.10	4.80	5.08	4.82	5.06	4.84	7
8	5.85	5.46	5.83	5.48	5.80	5.51	5.78	5.53	8
9	6.58	6.14	6.56	6.17	6.53	6.20	6.50	6.22	9
10	7.31	6.82	7.28	6.85	7.25	6.88	7.22	6.92	10
11	8.04	7.50	8.01	7.54	7.98	7.57	7.95	7.61	11
12	8.78	8.18	8.74	8.22	8.70	8.26	8.67	8.30	12
13	9.51	8.87	9.47	8.91	9.43	8.95	9.39	8.99	13
14	10.24	9.55	10.20	9.59	10.16	9.64	10.11	9.68	14
15	10.97	10.23	10.93	10.28	10.88	10.33	10.84	10.37	15
16	11.70	10.91	11.65	10.96	11.61	11.01	11.56	11.06	16
17	12.43	11.59	12.38	11.65	12.33	11.70	12.28	11.76	17
18	13.16	12.28	13.11	12.33	13.06	12.39	13.00	12.45	18
19	13.90	12.96	13.84	13.02	13.78	13.08	13.72	13.14	19
20	14.63	13.64	14.57	13.70	14.51	13.77	14.45	13.83	20
21	15.36	14.32	15.30	14.39	15.23	14.46	15.17	14.52	21
22	16.09	15.00	16.02	15.07	15.96	15.14	15.89	15.21	22
23	16.82	15.69	16.75	15.76	16.68	15.83	16.61	15.90	23
24	17.55	16.37	17.48	16.44	17.41	16.52	17.34	16.60	24
25	18.28	17.05	18.21	17.13	18.13	17.21	18.06	17.29	25
26	19.02	17.73	18.94	17.81	18.86	17.90	18.78	17.98	26
27	19.75	18.41	19.67	18.50	19.59	18.59	19.50	18.67	27
28	20.48	19.10	20.39	19.19	20.31	19.27	20.23	19.36	28
29	21.21	19.78	21.12	19.87	21.04	19.96	20.95	20.05	29
30	21.94	20.46	21.85	20.56	21.76	20.65	21.67	20.75	30
31	22.67	21.14	22.58	21.24	22.49	21.34	22.39	21.44	31
32	23.40	21.82	23.31	21.93	23.21	22.03	23.12	22.13	32
33	24.13	22.51	24.04	22.61	23.94	22.72	23.84	22.82	33
34	24.87	23.19	24.76	23.30	24.66	23.40	24.56	23.51	34
35	25.60	23.87	25.49	23.98	25.39	24.09	25.28	24.20	35
36	26.33	24.55	26.22	24.67	26.11	24.78	26.01	24.89	36
37	27.06	25.23	26.95	25.35	26.84	25.47	26.73	25.59	37
38	27.79	25.92	27.68	26.04	27.56	26.16	27.45	26.28	38
39	28.52	26.60	28.41	26.72	28.29	26.85	28.17	26.97	39
40	29.25	27.28	29.13	27.41	29.01	27.53	28.89	27.66	40
41	29.99	27.96	29.86	28.09	29.74	28.22	29.62	28.35	41
42	30.72	28.64	30.59	28.78	30.47	28.91	30.34	29.04	42
43	31.45	29.33	31.32	29.46	31.19	29.60	31.06	29.74	43
44	32.18	30.01	32.05	30.15	31.92	30.29	31.78	30.43	44
45	32.91	30.69	32.78	30.83	32.64	30.98	32.51	31.12	45
46	33.64	31.37	33.51	31.52	33.37	31.66	33.23	31.81	46
47	34.37	32.05	34.23	32.20	34.09	32.35	33.95	32.50	47
48	35.10	32.74	34.96	32.89	34.82	33.04	34.67	33.19	48
49	35.84	33.42	35.69	33.57	35.54	33.73	35.40	33.88	49
50	36.57	34.10	36.42	34.26	36.27	34.42	36.12	34.58	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	47 Deg.		46¾ Deg.		46½ Deg.		46¼ Deg.		



Distance.	44 Deg.		44½ Deg.		44¾ Deg.		45 Deg.		Distance.		
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.			
1	0.72	0.69	0.72	0.70	0.71	0.70	0.71	0.71	1		
2	1.44	1.39	1.43	1.40	1.43	1.40	1.42	1.41	2		
3	2.16	2.08	2.15	2.09	2.14	2.10	2.13	2.11	3		
4	2.88	2.78	2.87	2.79	2.85	2.80	2.84	2.82	4		
5	3.60	3.47	3.58	3.49	3.57	3.50	3.55	3.52	5		
6	4.32	4.17	4.30	4.19	4.28	4.21	4.26	4.22	6		
7	5.04	4.86	5.01	4.88	4.99	4.91	4.97	4.93	7		
8	5.75	5.56	5.73	5.58	5.71	5.61	5.68	5.63	8		
9	6.47	6.25	6.45	6.28	6.42	6.31	6.39	6.34	9		
10	7.19	6.95	7.16	6.98	7.13	7.01	7.10	7.04	10		
11	7.91	7.64	7.88	7.68	7.85	7.71	7.81	7.74	11		
12	8.63	8.34	8.60	8.37	8.56	8.41	8.52	8.45	12		
13	9.35	9.03	9.31	9.07	9.27	9.11	9.23	9.15	13		
14	10.07	9.73	10.03	9.77	9.99	9.81	9.94	9.86	14		
15	10.79	10.42	10.74	10.47	10.70	10.51	10.65	10.56	15		
16	11.51	11.11	11.46	11.16	11.41	11.21	11.36	11.26	16		
17	12.23	11.81	12.18	11.86	12.13	11.92	12.07	11.97	17		
18	12.95	12.50	12.89	12.56	12.84	12.62	12.78	12.67	18		
19	13.67	13.20	13.61	13.26	13.55	13.32	13.49	13.38	19		
20	14.39	13.89	14.33	13.96	14.26	14.02	14.20	14.08	20		
21	15.11	14.59	15.04	14.65	14.98	14.72	14.91	14.78	21		
22	15.83	15.28	15.76	15.35	15.69	15.42	15.62	15.49	22		
23	16.54	15.98	16.47	16.05	16.40	16.12	16.33	16.19	23		
24	17.26	16.67	17.19	16.75	17.12	16.82	17.04	16.90	24		
25	17.98	17.37	17.91	17.44	17.83	17.52	17.75	17.60	25		
26	18.70	18.06	18.62	18.14	18.54	18.22	18.46	18.30	26		
27	19.42	18.76	19.34	18.84	19.26	18.92	19.17	19.01	27		
28	20.14	19.45	20.06	19.54	19.97	19.63	19.89	19.71	28		
29	20.86	20.15	20.77	20.24	20.68	20.33	20.60	20.42	29		
30	21.58	20.84	21.49	20.93	21.40	21.03	21.31	21.12	30		
31	22.30	21.53	22.21	21.63	22.11	21.73	22.02	21.82	31		
32	23.02	22.23	22.92	22.33	22.82	22.43	22.73	22.53	32		
33	23.74	22.92	23.64	23.03	23.54	23.13	23.44	23.23	33		
34	24.46	23.62	24.35	23.72	24.25	23.83	24.15	23.94	34		
35	25.18	24.31	25.07	24.42	24.96	24.53	24.86	24.64	35		
36	25.90	25.01	25.79	25.12	25.68	25.23	25.57	25.34	36		
37	26.62	25.70	26.50	25.82	26.39	25.93	26.28	26.05	37		
38	27.33	26.40	27.22	26.52	27.10	26.63	26.99	26.75	38		
39	28.05	27.09	27.94	27.21	27.82	27.34	27.70	27.46	39		
40	28.77	27.79	28.65	27.91	28.53	28.04	28.41	28.16	40		
41	29.49	28.48	29.37	28.61	29.24	28.74	29.12	28.86	41		
42	30.21	29.18	30.08	29.31	29.96	29.44	29.83	29.57	42		
43	30.93	29.87	30.80	30.00	30.67	30.14	30.54	30.27	43		
44	31.65	30.56	31.52	30.70	31.38	30.84	31.25	30.98	44		
45	32.37	31.26	32.23	31.40	32.10	31.54	31.96	31.68	45		
46	33.09	31.95	32.95	32.10	32.81	32.24	32.67	32.38	46		
47	33.81	32.65	33.67	32.80	33.52	32.94	33.38	33.09	47		
48	34.53	33.34	34.38	33.49	34.24	33.64	34.09	33.79	48		
49	35.25	34.04	35.10	34.19	34.95	34.34	34.80	34.50	49		
50	35.97	34.73	35.82	34.89	35.66	35.05	35.51	35.20	50		
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	46 Deg.		45¾ Deg.		45½ Deg.		45¼ Deg.		45 Deg.		

TRAVERSE TABLE.

Distance.	44 Deg.		44¼ Deg.		44½ Deg.		44¾ Deg.		45 Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	36.69	35.43	36.53	35.59	36.38	35.75	36.22	35.90	36.06	36.06	51
52	37.41	36.12	37.25	36.29	37.09	36.45	36.93	36.61	36.77	36.77	52
53	38.12	36.82	37.96	36.98	37.80	37.15	37.64	37.31	37.48	37.48	53
54	38.84	37.51	38.68	37.68	38.52	37.85	38.35	38.02	38.18	38.18	54
55	39.56	38.21	39.40	38.38	39.23	38.55	39.06	38.72	38.89	38.89	55
56	40.28	38.90	40.11	39.08	39.94	39.25	39.77	39.42	39.60	39.60	56
57	41.00	39.60	40.83	39.77	40.66	39.95	40.48	40.13	40.31	40.31	57
58	41.72	40.29	41.55	40.47	41.37	40.65	41.19	40.83	41.01	41.01	58
59	42.44	40.98	42.26	41.17	42.08	41.35	41.90	41.54	41.72	41.72	59
60	43.16	41.68	42.98	41.87	42.79	42.05	42.61	42.24	42.43	42.43	60
61	43.88	42.37	43.69	42.57	43.51	42.76	43.32	42.94	43.13	43.13	61
62	44.60	43.07	44.41	43.26	44.22	43.46	44.03	43.65	43.84	43.84	62
63	45.32	43.76	45.13	43.96	44.93	44.16	44.74	44.35	44.55	44.55	63
64	46.04	44.46	45.84	44.66	45.65	44.86	45.45	45.06	45.25	45.25	64
65	46.76	45.15	46.56	45.36	46.36	45.56	46.16	45.76	45.96	45.96	65
66	47.48	45.85	47.28	46.05	47.07	46.26	46.87	46.46	46.67	46.67	66
67	48.20	46.54	47.99	46.75	47.79	46.96	47.58	47.17	47.38	47.38	67
68	48.92	47.24	48.71	47.45	48.50	47.66	48.29	47.87	48.08	48.08	68
69	49.63	47.93	49.42	48.15	49.21	48.36	49.00	48.58	48.79	48.79	69
70	50.35	48.63	50.14	48.85	49.93	49.06	49.71	49.28	49.50	49.50	70
71	51.07	49.32	50.86	49.54	50.64	49.76	50.42	49.93	50.20	50.20	71
72	51.79	50.02	51.57	50.24	51.35	50.47	51.13	50.69	50.91	50.91	72
73	52.51	50.71	52.29	50.94	52.07	51.17	51.84	51.39	51.62	51.62	73
74	53.23	51.40	53.01	51.64	52.78	51.87	52.55	52.10	52.33	52.33	74
75	53.95	52.10	53.72	52.33	53.49	52.57	53.26	52.80	53.03	53.03	75
76	54.67	52.79	54.44	53.03	54.21	53.27	53.97	53.51	53.74	53.74	76
77	55.39	53.49	55.16	53.73	54.92	53.97	54.68	54.21	54.45	54.45	77
78	56.11	54.18	55.87	54.43	55.63	54.67	55.39	54.91	55.15	55.15	78
79	56.83	54.88	56.59	55.13	56.35	55.37	56.10	55.62	55.86	55.86	79
80	57.55	55.57	57.30	55.82	57.06	56.07	56.81	56.32	56.57	56.57	80
81	58.27	56.27	58.02	56.52	57.77	56.77	57.52	57.03	57.28	57.28	81
82	58.99	56.96	58.74	57.22	58.49	57.47	58.24	57.73	57.98	57.98	82
83	59.71	57.66	59.45	57.92	59.20	58.18	58.95	58.43	58.69	58.69	83
84	60.42	58.35	60.17	58.61	59.91	58.88	59.66	59.14	59.40	59.40	84
85	61.14	59.05	60.89	59.31	60.63	59.58	60.37	59.84	60.10	60.10	85
86	61.86	59.74	61.60	60.01	61.34	60.28	61.08	60.55	60.81	60.81	86
87	62.58	60.44	62.32	60.71	62.05	60.98	61.79	61.25	61.52	61.52	87
88	63.30	61.13	63.03	61.41	62.77	61.68	62.50	61.95	62.23	62.23	88
89	64.02	61.82	63.75	62.10	63.48	62.38	63.21	62.66	62.93	62.93	89
90	64.74	62.52	64.47	62.80	64.19	63.08	63.92	63.36	63.64	63.64	90
91	65.46	63.21	65.18	63.50	64.91	63.78	64.63	64.07	64.35	64.35	91
92	66.18	63.91	65.90	64.20	65.62	64.48	65.34	64.77	65.05	65.05	92
93	66.90	64.60	66.62	64.89	66.33	65.18	66.05	65.47	65.76	65.76	93
94	67.62	65.30	67.33	65.59	67.05	65.89	66.76	66.18	66.47	66.47	94
95	68.34	65.99	68.05	66.29	67.76	66.59	67.47	66.88	67.18	67.18	95
96	69.06	66.69	68.76	66.99	68.47	67.29	68.18	67.59	67.88	67.88	96
97	69.78	67.38	69.48	67.69	69.19	67.99	68.89	68.29	68.59	68.59	97
98	70.50	68.08	70.20	68.38	69.90	68.69	69.60	68.99	69.30	69.30	98
99	71.21	68.77	70.91	69.08	70.61	69.39	70.31	69.70	70.00	70.00	99
100	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	70.71	70.71	100

Distance.	46 Deg.		45¾ Deg.		45½ Deg.		45¼ Deg.		45 Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

## A TABLE OF RHUMBS.

SHOWING

THE DEGREES, MINUTES, AND SECONDS, THAT EVERY POINT AND QUARTER POINT OF THE COMPASS MAKES WITH THE MERIDIAN.

NORTH.		Pts.	qr.	o	/	//	Pts.	qr.	SOUTH.	
		0	1	2	48	45	0	1		
		1	2	5	37	30	0	2		
		0	3	8	26	15	0	3		
N by E.	N. by W.	1	0	11	15	0	1	0	S. by E.	S. by W.
		1	1	14	3	45	1	1		
		1	2	16	52	30	1	2		
		1	3	19	41	15	1	3		
N.N.E.	N.N.W.	2	0	22	30	0	2	0	S.S.E.	S.S.W.
		2	1	25	18	45	2	1		
		2	2	28	7	30	2	2		
		2	3	30	56	15	2	3		
N.E. by N.	N.W. by N.	3	0	33	45	0	3	0	S.E. by S.	S.W. by S.
		3	1	35	33	45	3	1		
		3	2	39	22	30	3	2		
		3	3	42	11	15	3	3		
N.E.	N.W.	4	0	45	0	0	4	0	S.E.	S.W.
		4	1	47	48	45	4	1		
		4	2	50	37	30	4	2		
		4	3	53	26	15	4	3		
N.E. by E.	N.W. by W.	5	0	56	15	0	5	0	S.E. by E.	S.W. by W.
		5	1	59	3	45	5	1		
		5	2	61	52	30	5	2		
		5	3	64	41	15	5	3		
E.N.E.	W.N.W.	6	0	67	30	0	6	0	E.S.E.	W S.W.
		6	1	70	18	45	6	1		
		6	2	73	7	30	6	2		
		6	3	75	56	15	6	3		
E. by N.	W. by N.	7	0	78	45	0	7	0	E. by S.	W. by S.
		7	1	81	33	45	7	1		
		7	2	84	22	30	7	2		
		7	3	87	11	15	7	3		
East.	West.	8	0	90	0	0	8	0	East.	West.

Mid. Lat.	30	40	50	60	70	80	90	100	110
0	0 02	0 03	0 04	0 06	0 09	0 12	0 15	0 19	0 23
15	0 02	0 03	0 04	0 06	0 09	0 12	0 15	0 18	0 22
16	0 02	0 03	0 04	0 06	0 08	0 11	0 14	0 17	0 21
17	0 02	0 03	0 04	0 06	0 08	0 11	0 14	0 17	0 20
18	0 02	0 03	0 04	0 06	0 07	0 10	0 13	0 16	0 19
19	0 02	0 03	0 04	0 06	0 07	0 09	0 12	0 15	0 18
20	0 02	0 03	0 04	0 06	0 07	0 09	0 12	0 15	0 18
21	0 02	0 03	0 04	0 06	0 07	0 09	0 12	0 15	0 17
22	0 02	0 03	0 04	0 06	0 07	0 09	0 12	0 15	0 17
23	0 02	0 03	0 04	0 06	0 07	0 09	0 11	0 14	0 16
24	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
25	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
26	0 02	0 03	0 04	0 05	0 07	0 08	0 11	0 14	0 16
27	0 02	0 03	0 04	0 05	0 07	0 08	0 11	0 14	0 16
28	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
29	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
30	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
31	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
32	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
33	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
34	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
35	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
36	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
37	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
38	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
39	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
40	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
41	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
42	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
43	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
44	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
45	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
46	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
47	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
48	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
49	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 17
50	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 17
51	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 17
52	0 02	0 03	0 04	0 05	0 07	0 09	0 12	0 15	0 18
53	0 02	0 03	0 04	0 06	0 07	0 09	0 12	0 15	0 18
54	0 02	0 03	0 04	0 06	0 08	0 10	0 13	0 16	0 19
55	0 02	0 03	0 04	0 06	0 08	0 10	0 13	0 16	0 19
56	0 02	0 03	0 04	0 06	0 08	0 10	0 13	0 16	0 20
57	0 02	0 03	0 04	0 06	0 08	0 11	0 14	0 17	0 20
58	0 02	0 03	0 04	0 06	0 09	0 11	0 14	0 17	0 21
59	0 02	0 03	0 04	0 06	0 09	0 12	0 15	0 18	0 22
60	0 02	0 03	0 04	0 06	0 09	0 12	0 15	0 19	0 23
61	0 02	0 03	0 05	0 07	0 09	0 12	0 15	0 19	0 23
62	0 02	0 03	0 05	0 07	0 09	0 12	0 16	0 20	0 24
63	0 02	0 04	0 05	0 07	0 09	0 13	0 16	0 20	0 24
64	0 02	0 04	0 06	0 08	0 09	0 13	0 17	0 21	0 25
65	0 02	0 04	0 06	0 08	0 10	0 13	0 17	0 21	0 25
66	0 02	0 04	0 06	0 08	0 10	0 14	0 18	0 22	0 26
67	0 02	0 04	0 06	0 08	0 11	0 15	0 18	0 23	0 27
68	0 02	0 04	0 06	0 08	0 11	0 15	0 19	0 24	0 28
69	0 02	0 05	0 06	0 09	0 12	0 16	0 20	0 25	0 30
70	0 03	0 05	0 06	0 09	0 13	0 17	0 21	0 26	0 31
71	0 04	0 06	0 07	0 09	0 13	0 18	0 22	0 27	0 33
72	0 04	0 06	0 08	0 10	0 14	0 19	0 23	0 29	0 35

94 WORKMAN'S TABLE, FOR CORRECTING THE MIDDLE LATITUDE.

Mil. Lat.	120	130	140	150	160	170	180	190	200
0	0 /	0 /	0 /	0 /	0 /	0 /	0 /	0 /	0 /
15	0 27	0 31	0 35	0 40	0 45	0 51	0 58	1 06	1 14
16	0 26	0 30	0 34	0 38	0 43	0 49	0 56	1 03	1 11
17	0 25	0 28	0 32	0 37	0 42	0 48	0 54	1 01	1 08
18	0 24	0 27	0 31	0 36	0 41	0 46	0 52	0 58	1 06
19	0 23	0 26	0 30	0 34	0 40	0 45	0 50	0 56	1 03
20	0 22	0 25	0 29	0 33	0 38	0 43	0 48	0 54	1 00
21	0 21	0 25	0 29	0 33	0 37	0 42	0 47	0 53	0 58
22	0 20	0 24	0 28	0 32	0 36	0 41	0 46	0 51	0 56
23	0 20	0 24	0 28	0 32	0 36	0 40	0 45	0 50	0 55
24	0 19	0 23	0 27	0 31	0 35	0 39	0 44	0 48	0 53
25	0 19	0 23	0 27	0 31	0 35	0 39	0 43	0 47	0 52
26	0 19	0 22	0 26	0 30	0 34	0 38	0 42	0 47	0 52
27	0 19	0 22	0 26	0 30	0 33	0 38	0 42	0 46	0 51
28	0 18	0 21	0 25	0 29	0 33	0 37	0 41	0 46	0 51
29	0 18	0 21	0 25	0 29	0 32	0 36	0 41	0 45	0 50
30	0 18	0 21	0 25	0 28	0 32	0 36	0 41	0 45	0 50
31	0 18	0 21	0 25	0 28	0 32	0 36	0 41	0 45	0 50
32	0 18	0 21	0 25	0 28	0 31	0 36	0 41	0 45	0 50
33	0 18	0 21	0 24	0 27	0 31	0 35	0 40	0 44	0 49
34	0 18	0 21	0 24	0 27	0 31	0 35	0 40	0 44	0 49
35	0 18	0 21	0 24	0 27	0 31	0 35	0 40	0 44	0 49
36	0 18	0 21	0 24	0 27	0 31	0 35	0 40	0 44	0 49
37	0 18	0 21	0 24	0 27	0 31	0 35	0 40	0 44	0 49
38	0 18	0 21	0 24	0 27	0 31	0 36	0 40	0 45	0 50
39	0 18	0 21	0 25	0 28	0 32	0 36	0 41	0 45	0 50
40	0 18	0 22	0 25	0 28	0 32	0 36	0 41	0 45	0 50
41	0 18	0 22	0 25	0 28	0 32	0 37	0 41	0 45	0 50
42	0 18	0 22	0 26	0 29	0 33	0 37	0 42	0 46	0 51
43	0 19	0 23	0 26	0 30	0 34	0 38	0 42	0 46	0 51
44	0 19	0 23	0 27	0 30	0 34	0 38	0 43	0 47	0 52
45	0 19	0 23	0 27	0 31	0 35	0 39	0 43	0 47	0 52
46	0 19	0 23	0 27	0 31	0 35	0 39	0 44	0 48	0 53
47	0 20	0 23	0 27	0 31	0 35	0 40	0 44	0 49	0 54
48	0 20	0 23	0 27	0 31	0 35	0 40	0 45	0 50	0 55
49	0 21	0 24	0 28	0 32	0 36	0 41	0 45	0 51	0 57
50	0 21	0 24	0 28	0 32	0 36	0 41	0 46	0 52	0 58
51	0 21	0 24	0 28	0 32	0 37	0 42	0 47	0 53	0 59
52	0 22	0 25	0 29	0 33	0 37	0 42	0 48	0 54	1 00
53	0 22	0 25	0 29	0 33	0 38	0 43	0 49	0 55	1 01
54	0 23	0 26	0 30	0 34	0 39	0 44	0 50	0 56	1 02
55	0 23	0 26	0 30	0 35	0 40	0 45	0 51	0 57	1 03
56	0 24	0 27	0 31	0 36	0 41	0 46	0 52	0 58	1 04
57	0 24	0 28	0 32	0 37	0 42	0 48	0 54	1 00	1 06
58	0 25	0 29	0 33	0 38	0 44	0 50	0 55	1 02	1 08
59	0 26	0 30	0 34	0 39	0 45	0 51	0 57	1 04	1 10
60	0 27	0 31	0 35	0 40	0 46	0 52	0 59	1 06	1 13
61	0 27	0 31	0 36	0 41	0 47	0 54	1 01	1 08	1 15
62	0 28	0 32	0 37	0 42	0 49	0 56	1 03	1 10	1 18
63	0 29	0 33	0 39	0 44	0 51	0 58	1 05	1 12	1 21
64	0 29	0 34	0 40	0 46	0 53	1 00	1 07	1 14	1 24
65	0 30	0 35	0 41	0 48	0 55	1 02	1 09	1 17	1 27
66	0 31	0 37	0 43	0 50	0 58	1 05	1 12	1 21	1 31
67	0 33	0 38	0 45	0 53	1 00	1 07	1 16	1 25	1 35
68	0 34	0 40	0 48	0 55	1 02	1 10	1 19	1 30	1 39
69	0 36	0 42	0 50	0 58	1 05	1 13	1 23	1 34	1 44
70	0 38	0 44	0 52	1 00	1 08	1 17	1 28	1 39	1 50
71	0 40	0 46	0 55	1 03	1 12	1 22	1 32	1 44	1 56
72	0 42	0 49	0 58	1 06	1 16	1 27	1 38	1 50	2 04



M.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°
0	0	60	120	180	240	300	361	421	482	542	603	664	725	787
1	1	61	121	181	241	301	362	422	483	543	604	665	726	788
2	2	62	122	182	242	302	363	423	484	544	605	666	727	789
3	3	63	123	183	243	303	364	424	485	545	606	667	728	790
4	4	64	124	184	244	304	365	425	486	546	607	668	729	791
5	5	65	125	185	245	305	366	426	487	547	608	669	730	792
6	6	66	126	186	246	306	367	427	488	548	609	670	731	793
7	7	67	127	187	247	307	368	428	489	549	610	671	732	794
8	8	68	128	188	248	308	369	429	490	550	611	672	733	795
9	9	69	129	189	249	309	370	430	491	551	612	673	735	796
10	10	70	130	190	250	310	371	431	492	552	613	664	736	797
11	11	71	131	191	251	311	372	432	493	553	614	675	737	798
12	12	72	132	192	252	312	373	433	494	554	615	676	738	799
13	13	73	133	193	253	313	374	434	495	555	616	677	739	800
14	14	74	134	194	254	314	375	435	496	556	617	678	740	801
15	15	75	135	195	255	315	376	436	497	557	618	679	741	802
16	16	76	136	196	256	316	377	437	498	558	619	680	742	803
17	17	77	137	197	257	317	378	438	499	559	620	681	743	804
18	18	78	138	198	258	318	379	439	500	560	621	682	744	805
19	19	79	139	199	259	319	380	440	501	561	622	683	745	806
20	20	80	140	200	260	320	381	441	502	562	623	684	746	807
21	21	81	141	201	261	321	382	442	503	563	624	685	747	808
22	22	82	142	202	262	322	383	443	504	564	625	687	748	809
23	23	83	143	203	263	323	384	444	505	565	626	688	749	810
24	24	84	144	204	264	324	385	445	506	566	627	689	750	811
25	25	85	145	205	265	325	386	446	507	567	628	690	751	812
26	26	86	146	206	266	326	387	447	508	568	629	691	752	813
27	27	87	147	207	267	327	388	448	509	570	631	692	753	815
28	28	88	148	208	268	328	389	449	510	571	632	693	754	816
29	29	89	149	209	269	330	390	450	511	572	633	694	755	817
30	30	90	150	210	270	331	391	451	512	573	634	695	756	818
31	31	91	151	211	271	332	392	452	513	574	635	696	757	819
32	32	92	152	212	272	333	393	453	514	575	636	697	758	820
33	33	93	153	213	273	334	394	454	515	576	637	698	759	821
34	34	94	154	214	274	335	395	455	516	577	638	699	760	822
35	35	95	155	215	275	336	396	456	517	578	639	700	761	823
36	36	96	156	216	276	337	397	457	518	579	640	701	762	824
37	37	97	157	217	277	338	398	458	519	580	641	702	763	825
38	38	98	158	218	278	339	399	459	520	581	642	703	764	826
39	39	99	159	219	279	340	400	460	521	582	643	704	765	827
40	40	100	160	220	280	341	401	461	522	583	644	705	766	828
41	41	101	161	221	281	342	402	462	523	584	645	706	767	829
42	42	102	162	222	282	343	403	463	524	585	646	707	768	830
43	43	103	163	223	283	344	404	464	525	586	647	708	769	831
44	44	104	164	224	284	345	405	465	526	587	648	709	770	832
45	45	105	165	225	285	346	406	466	527	588	649	710	771	833
46	46	106	166	226	286	347	407	467	528	589	650	711	772	834
47	47	107	167	227	287	348	408	468	529	590	651	712	773	835
48	48	108	168	228	288	349	409	469	530	591	652	713	774	836
49	49	109	169	229	289	350	410	470	531	592	653	714	775	837
50	50	110	170	230	290	351	411	471	532	593	654	715	777	838
51	51	111	171	231	291	352	412	472	533	594	655	716	778	839
52	52	112	172	232	292	353	413	473	534	595	656	717	779	840
53	53	113	173	233	293	354	414	474	535	596	657	718	780	841
54	54	114	174	234	294	355	415	476	536	597	658	719	781	842
55	55	115	175	235	295	356	416	477	537	598	659	720	782	843
56	56	116	176	236	296	357	417	478	538	599	660	721	783	844
57	57	117	177	237	297	358	418	479	539	600	661	722	784	845
58	58	118	178	238	298	359	419	480	540	601	662	723	785	846
59	59	119	179	239	299	360	420	481	541	602	663	724	786	847

TABLE OF MERIDIONAL PARTS.

M.	140	150	160	170	180	190	200	210	220	230	240	250	260	270
0	848	910	973	1035	1098	1161	1225	1289	1354	1419	1484	1550	1616	1684
.1	850	911	974	36	99	63	26	90	55	20	85	51	18	85
2	851	913	975	37	1100	64	27	91	56	21	86	52	19	86
3	852	914	976	38	01	65	28	92	57	22	87	53	20	87
4	853	915	977	39	02	66	29	93	58	23	88	54	21	88
5	854	916	978	41	03	67	30	95	59	24	90	56	22	89
6	855	917	979	42	05	68	32	96	60	25	91	57	23	90
7	856	918	980	43	06	69	33	97	61	26	92	58	24	91
8	857	919	981	44	07	70	34	98	62	27	93	59	25	93
9	858	920	982	45	08	71	35	99	63	28	94	60	26	94
10	859	921	983	1046	1109	1172	1236	1300	1364	1430	1495	1561	1628	1695
11	860	922	984	47	10	73	37	01	66	31	96	62	29	96
12	861	923	985	48	11	74	38	02	67	32	97	63	30	97
13	862	924	986	49	12	75	39	03	68	33	98	64	31	98
14	863	925	987	50	13	76	40	04	69	34	99	65	32	99
15	864	926	988	51	14	77	41	05	70	35	1500	67	33	1700
16	865	927	989	52	15	78	42	06	71	36	02	68	34	01
17	866	928	990	53	16	79	43	07	72	37	03	69	35	03
18	867	929	991	54	17	81	44	08	73	38	04	70	37	04
19	868	930	993	55	18	82	45	10	74	39	05	71	38	05
20	869	931	994	1056	1119	1183	1246	1311	1375	1440	1506	1572	1639	1706
21	870	932	995	57	20	84	48	12	76	41	07	73	40	07
22	871	933	996	58	21	85	49	13	77	43	08	74	41	08
23	872	934	997	59	22	86	50	14	79	44	09	75	42	09
24	873	935	998	60	23	87	51	15	80	45	10	77	43	11
25	874	936	999	61	25	88	52	16	81	46	11	78	44	12
26	875	937	1000	63	26	89	53	17	82	47	13	79	45	13
27	876	938	1001	64	27	90	54	18	83	48	14	80	47	14
28	877	939	1002	65	28	91	55	19	84	49	15	81	48	15
29	878	941	1003	66	29	92	56	20	85	50	16	82	49	16
30	879	942	1004	1067	1130	1193	1257	1321	1386	1451	1517	1583	1650	1717
31	880	943	05	68	31	94	58	22	87	52	18	84	51	18
32	882	944	06	69	32	95	59	24	88	53	19	85	52	20
33	883	945	07	70	33	96	60	25	89	55	20	86	53	21
34	884	946	08	71	34	98	61	26	90	56	21	88	54	22
35	885	947	09	72	35	99	62	27	92	57	22	89	56	23
36	886	948	10	73	36	1200	64	28	93	58	24	90	57	24
37	887	949	11	74	37	01	65	29	94	59	25	91	58	25
38	888	950	12	75	38	02	66	30	95	60	26	92	59	26
39	889	951	13	76	39	03	67	31	96	61	27	93	60	27
40	890	952	1014	1077	1140	1204	1268	1332	1397	1462	1528	1594	1661	1729
41	891	953	15	78	41	05	69	33	98	63	29	96	62	30
42	892	954	16	79	42	06	70	34	99	64	30	97	63	31
43	893	955	18	80	44	07	71	35	1400	65	31	98	64	32
44	894	956	19	81	45	08	72	36	01	67	32	99	66	33
45	895	957	20	82	46	09	73	38	02	68	33	1600	67	34
46	896	958	21	84	47	10	74	39	03	69	35	01	68	35
47	897	959	22	85	48	11	75	40	05	70	36	02	69	36
48	898	960	23	86	49	12	76	41	06	71	37	03	70	38
49	899	961	24	87	50	13	77	42	07	72	38	04	71	39
50	900	962	1025	1088	1151	1215	1278	1343	1408	1473	1539	1605	1672	1740
51	901	963	26	89	52	16	80	44	09	74	40	06	73	41
52	902	964	27	90	53	17	81	45	10	75	41	08	75	42
53	903	965	28	91	54	18	82	46	11	76	42	09	76	43
54	904	966	29	92	55	19	83	47	12	77	43	10	77	44
55	905	968	30	93	56	20	84	48	13	79	44	11	78	46
56	906	969	31	94	57	21	85	49	14	80	46	12	79	47
57	907	970	32	95	58	22	86	50	15	81	47	13	80	48
58	908	971	33	96	59	23	87	52	16	82	48	14	81	49
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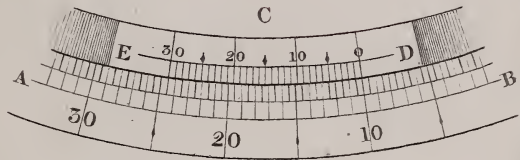
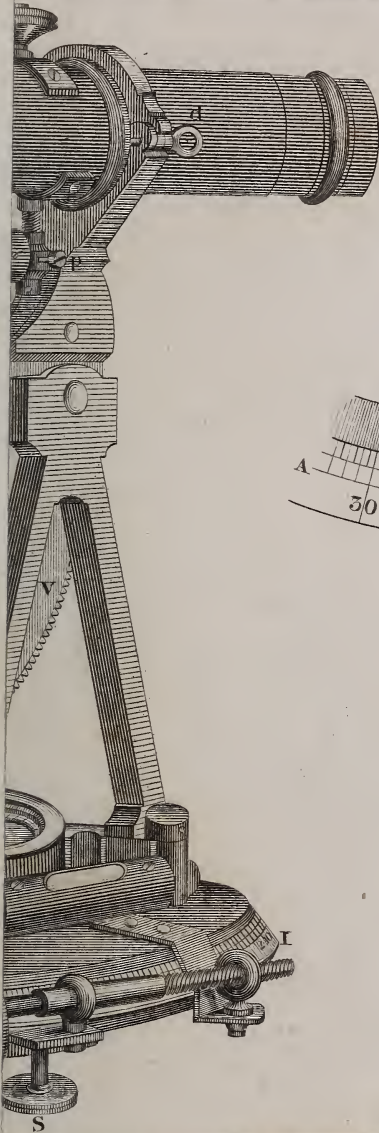
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3	55	23	92	62	32	03	75	48	22	96	72	49	27	06
4	56	24	93	63	33	04	76	49	23	98	73	50	28	07
5	57	25	94	64	34	05	78	50	24	99	75	51	29	08
6	58	26	95	65	35	07	79	52	25	2400	76	53	31	10
7	59	27	96	66	37	08	80	53	27	01	77	54	32	11
8	60	29	98	67	38	09	81	54	28	03	78	55	33	12
9	61	30	99	69	39	10	82	55	29	04	80	57	34	14
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13	66	34	03	73	44	15	87	60	34	09	85	62	40	19
14	67	35	05	74	45	16	88	61	35	10	86	63	41	20
15	68	37	06	76	46	17	90	63	37	11	87	64	42	22
16	69	38	07	77	47	19	91	64	38	13	89	66	44	23
17	70	39	08	78	48	20	92	65	39	14	90	67	45	24
18	72	40	09	79	50	21	93	66	40	15	91	68	46	26
19	73	41	10	80	51	22	94	68	42	16	92	69	48	27
20	1774	1842	1912	1981	2052	2123	2196	2269	2343	2418	2494	2571	2649	2728
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22	76	45	14	84	54	26	98	71	45	20	96	73	51	31
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26	81	49	18	88	59	31	03	76	50	25	01	78	57	36
27	82	50	20	90	60	32	04	77	51	27	03	80	58	37
28	83	52	21	91	61	33	05	79	53	28	04	81	59	39
29	84	53	22	92	63	34	07	80	54	29	05	82	61	40
30	1785	1854	1923	1993	2064	2135	2208	2281	2355	2430	2506	2584	2662	2742
31	86	55	24	94	65	37	09	82	56	32	08	85	63	43
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33	89	57	27	97	67	39	11	85	59	34	10	88	66	46
34	90	58	28	98	69	40	13	86	60	35	12	89	67	47
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36	92	61	30	2000	71	43	15	88	63	38	14	91	70	50
37	93	62	31	01	72	44	16	90	64	39	15	93	71	51
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39	95	64	34	04	75	46	19	92	66	42	18	95	74	54
40	1797	1865	1935	2005	2076	2147	2220	2293	2368	2443	2519	2597	2675	2755
41	98	66	36	06	77	49	21	95	69	44	21	98	76	56
42	99	68	37	07	78	50	22	96	70	45	22	99	78	58
43	1800	69	38	08	79	51	24	97	71	47	23	2600	79	59
44	01	70	39	10	80	52	25	98	73	48	24	02	80	60
45	02	71	41	11	82	53	26	99	74	49	26	03	82	62
46	03	72	42	12	83	55	27	2301	75	51	27	04	83	63
47	05	73	43	13	84	56	28	02	76	52	28	06	84	64
48	06	75	44	14	85	57	30	03	78	53	30	07	86	66
49	07	76	45	15	86	58	31	04	79	54	31	08	87	67
50	1808	1877	1946	2017	2088	2159	2232	2306	2380	2456	2532	2610	2688	2768
51	09	78	48	18	89	61	33	07	81	57	33	11	90	70
52	10	79	49	19	90	62	35	08	83	58	35	12	91	71
53	11	80	50	20	91	63	36	09	84	59	36	14	92	72
54	13	81	51	21	92	64	37	11	85	61	37	15	94	74
55	14	83	52	22	94	65	38	12	86	62	38	16	95	75
56	15	84	53	24	95	67	39	13	88	63	40	17	96	76
57	16	85	55	25	96	68	41	14	89	64	41	19	98	78
58	17	86	56	26	97	69	42	16	90	66	42	20	99	79
59	18	87	57	27	98	70	43	17	91	67	44	21	2700	80

## TABLE OF MERIDIONAL PARTS.

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2	84	66	49	33	18	06	95	85	78	72	68	67	68	71
3	86	67	50	34	20	07	96	87	79	74	70	69	70	73
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5	88	70	53	37	23	10	99	90	82	77	73	72	73	77
6	90	71	54	38	24	12	3301	91	84	78	75	74	75	78
7	91	73	56	40	26	13	02	93	85	80	77	75	77	80
8	92	74	57	41	27	14	03	94	87	82	78	77	78	82
9	94	75	58	43	29	16	05	96	88	83	80	79	80	84
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11	97	78	61	46	31	19	08	99	92	86	83	82	83	87
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13	99	81	64	48	34	22	11	02	95	90	86	85	87	91
14	2801	82	65	50	36	23	12	03	96	91	88	87	89	92
15	02	84	67	51	37	25	14	05	98	93	90	89	90	94
16	03	85	68	53	39	26	16	07	99	94	91	90	92	96
17	05	86	70	54	40	28	17	08	3501	96	93	92	94	98
18	06	88	71	55	42	29	19	10	03	98	95	94	95	99
19	07	89	72	57	43	31	20	11	04	99	96	95	97	4001
20	2809	2891	2974	3058	3144	3232	3322	3413	3506	3601	3698	3797	3899	4003
21	10	92	75	60	46	34	24	14	07	02	99	99	3901	05
22	11	93	76	61	47	35	25	16	09	04	3701	3800	02	06
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25	15	97	81	65	52	40	29	20	14	09	06	06	07	12
26	17	99	82	67	53	41	31	22	15	10	07	07	09	14
27	18	2900	83	68	55	42	32	23	17	12	09	09	11	15
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29	21	03	86	71	57	45	35	27	20	15	13	12	14	19
30	2822	2904	2988	3073	3159	3247	3337	3428	3521	3617	3714	3814	3916	4021
31	24	06	89	74	60	48	38	30	23	18	16	16	18	22
32	25	07	91	75	62	50	40	31	25	20	17	17	19	24
33	26	08	92	77	63	51	41	33	26	22	19	19	21	26
34	28	10	93	78	65	53	43	34	28	23	21	21	22	28
35	29	11	95	80	66	54	44	36	29	25	22	22	25	29
36	30	13	96	81	68	56	46	37	31	26	24	24	26	31
37	32	14	98	83	69	57	47	39	32	28	26	26	28	33
38	33	15	99	84	71	59	49	40	34	30	27	27	30	35
39	34	17	3000	85	72	60	50	42	36	31	29	29	32	37
40	2836	2918	3002	3087	3173	3262	3352	3443	3537	3633	3731	3831	3933	4038
41	37	19	03	88	75	63	53	45	39	34	32	32	35	40
42	39	21	05	90	76	65	55	47	40	36	34	34	37	42
43	40	22	06	91	78	66	56	48	42	38	36	36	38	44
44	41	24	07	93	79	68	58	50	43	39	37	37	40	45
45	43	25	09	94	81	69	59	51	45	41	39	39	42	47
46	44	26	10	95	82	71	61	53	47	43	41	41	44	49
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48	47	29	13	98	85	74	64	56	50	46	44	44	47	52
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56	58	40	24	10	97	86	76	68	62	59	57	58	61	67
57	59	42	26	11	98	87	78	70	64	60	59	60	63	69
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M.	56°	57°	58°	59°	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°
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2	77	86	98	13	31	53	79	09	44	84	28	79	36	5800
3	79	88	4300	15	33	55	81	12	46	86	31	82	39	03
4	81	90	02	17	35	57	84	14	49	88	33	84	42	06
5	83	92	04	19	37	60	86	16	51	91	36	87	44	09
6	85	94	06	21	39	62	88	18	53	93	38	89	47	11
7	86	95	08	23	41	64	90	20	55	95	41	92	50	14
8	88	97	09	25	43	66	92	23	58	98	43	95	52	17
9	90	99	11	27	45	68	94	25	60	5200	46	97	55	20
10	4092	4201	4313	4429	4547	4670	4796	4927	5062	5203	5348	5500	5658	5823
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21	12	21	34	50	70	93	20	51	88	29	76	28	87	54
22	13	23	36	52	72	95	22	54	90	31	78	31	90	56
23	15	25	38	54	74	97	24	56	92	34	80	33	93	59
24	17	27	40	56	76	99	26	58	95	36	83	36	95	62
25	19	29	42	58	78	4701	29	60	97	38	85	39	98	65
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27	22	32	46	62	82	05	33	65	5102	43	90	44	04	71
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33	33	44	57	74	94	18	46	78	15	58	06	59	20	88
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35	37	47	61	78	98	22	50	83	20	63	11	65	25	94
36	39	49	63	80	4600	24	52	85	22	65	13	67	28	96
37	41	51	65	82	02	26	55	87	25	67	16	70	31	99
38	42	53	67	84	04	28	57	90	27	70	18	73	34	5902
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41	48	59	72	90	10	35	63	96	34	77	26	80	42	11
42	50	60	74	92	12	37	65	99	36	80	28	83	45	14
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47	59	70	84	4501	23	47	76	10	48	92	41	96	58	28
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52	68	79	94	11	33	58	87	21	60	04	54	10	72	43
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57	77	89	03	21	43	69	98	33	72	16	66	23	86	57
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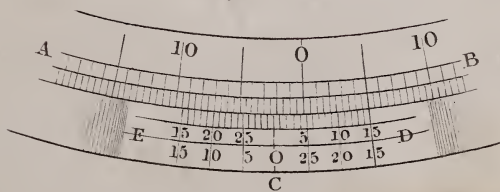
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2	72	52	41	41	53	78	18	76	54	56	87	52	60	22
3	75	55	45	45	57	82	22	81	59	61	93	58	67	31
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6	84	64	54	55	68	94	35	94	74	77	10	78	89	55
7	86	67	58	58	71	97	39	98	78	83	16	84	96	64
8	89	70	61	62	75	7001	43	7503	83	88	22	91	9203	72
9	92	73	64	65	79	05	47	07	88	93	27	97	11	81
10	5995	6177	6367	6569	6782	7009	7252	7512	7793	8099	8433	8804	9218	9689
11	98	80	71	72	86	13	56	16	98	8104	39	10	25	97
12	6001	83	74	76	90	17	60	21	7803	09	45	17	33	9706
13	04	86	77	79	93	21	64	25	08	15	51	23	40	14
14	07	89	80	83	97	25	68	30	13	20	57	30	48	23
15	10	92	84	86	6801	29	73	35	17	25	63	36	55	31
16	13	95	87	90	04	33	77	39	22	31	69	43	62	40
17	16	98	90	93	08	37	81	44	27	36	74	49	70	48
18	19	6201	94	96	12	41	85	48	32	41	80	56	77	57
19	22	05	97	6600	15	45	89	53	37	47	86	63	85	65
20	6025	6208	6400	6603	6819	7049	7294	7557	7842	8152	8492	8869	9292	9774
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22	31	14	07	10	26	56	7302	66	52	63	8504	83	07	91
23	34	17	10	14	30	60	06	71	57	68	10	89	15	9800
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27	46	30	23	28	45	76	23	89	77	90	34	16	45	35
28	49	33	27	31	49	80	28	94	82	96	40	23	53	44
29	52	36	30	35	53	84	32	98	87	8201	46	30	60	52
30	6055	6239	6433	6639	6856	7088	7336	7603	7892	8207	8552	8936	9368	9861
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32	61	45	40	46	64	96	45	12	7902	18	64	50	83	79
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35	70	55	50	56	75	08	58	26	17	34	83	70	9407	9906
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38	79	64	60	67	86	20	71	40	32	51	8601	91	30	33
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43	94	80	77	85	05	40	92	64	58	79	32	25	69	78
44	97	83	80	88	09	45	97	68	63	84	38	32	77	87
45	6100	87	83	92	13	49	7401	73	68	90	44	39	85	9996
46	04	90	87	95	17	53	06	78	73	95	51	46	93	10005
47	06	93	90	99	20	57	10	83	78	8301	57	53	9501	10015
48	09	96	94	6702	24	61	14	87	83	07	63	60	09	10024
49	12	99	97	06	28	65	19	92	89	12	69	67	17	10033
50	6115	6303	6500	6710	6932	7169	7423	7697	7994	8318	8676	9074	9525	10043
51	18	06	04	13	36	73	27	7702	99	24	82	81	33	10052
52	21	09	07	17	40	77	32	06	8004	29	88	88	41	10061
53	24	12	11	20	43	81	36	11	09	25	93	96	49	10071
54	27	15	14	24	47	85	41	16	14	41	8701	9103	57	10080
55	30	19	17	28	51	89	45	21	20	47	07	10	65	10089
56	33	22	21	31	55	94	49	25	25	52	14	17	73	10099
57	36	25	24	35	59	98	54	30	30	58	20	24	81	10108
58	40	28	28	38	63	7202	58	35	35	64	26	31	89	10118
59	43	32	31	42	66	06	63	40	40	69	33	38	96	10127



*Fig. 2.*



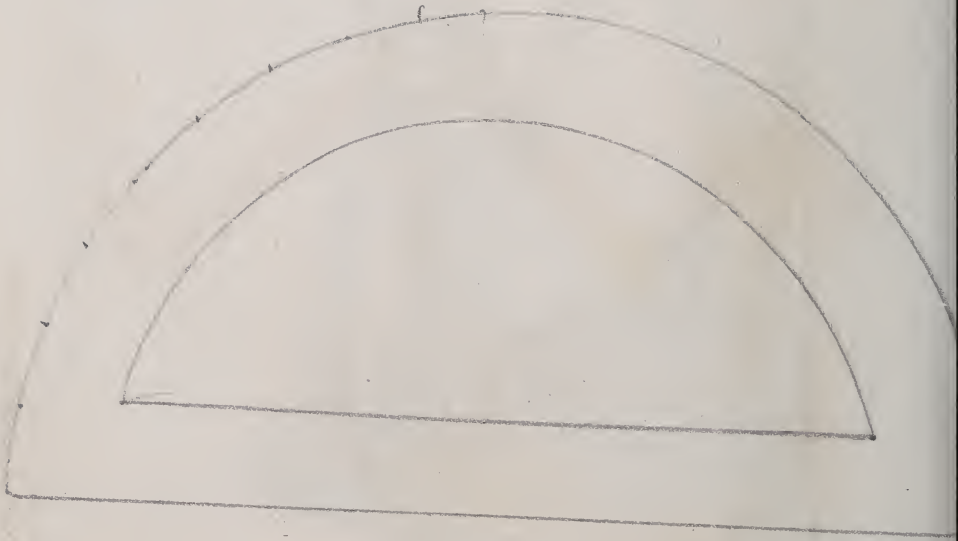
*Fig. 3.*

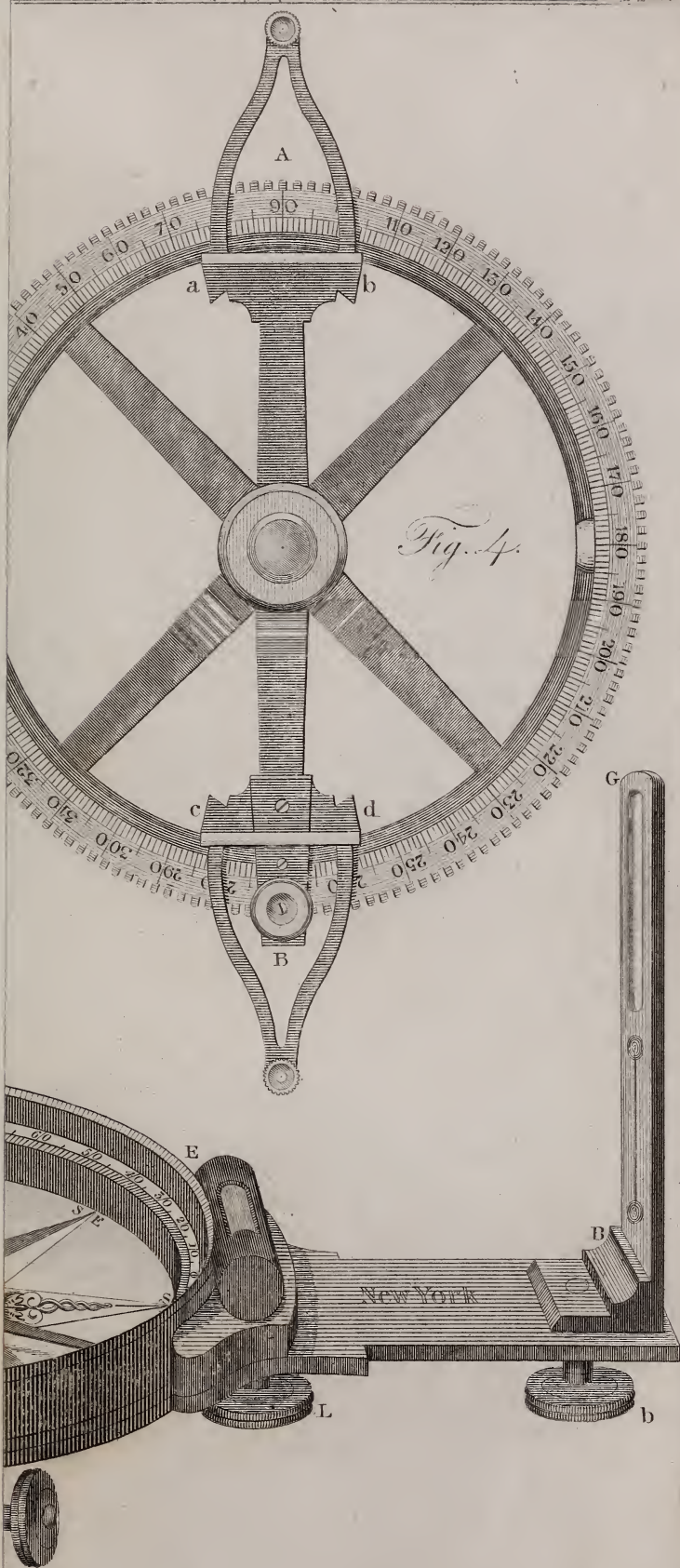






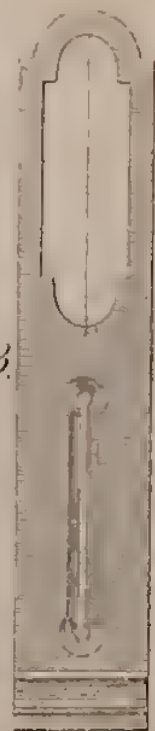




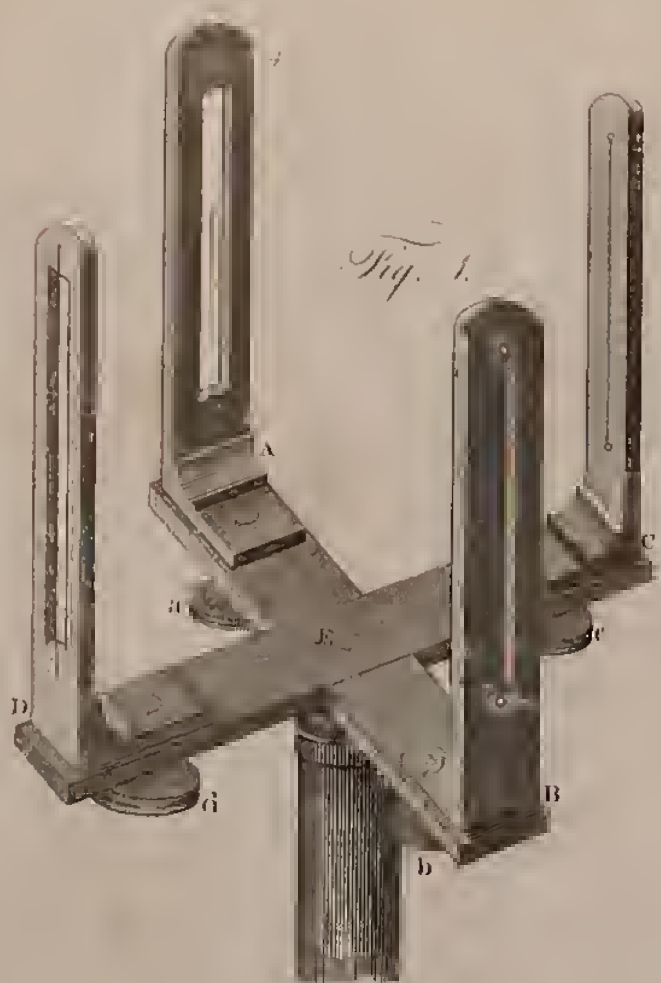




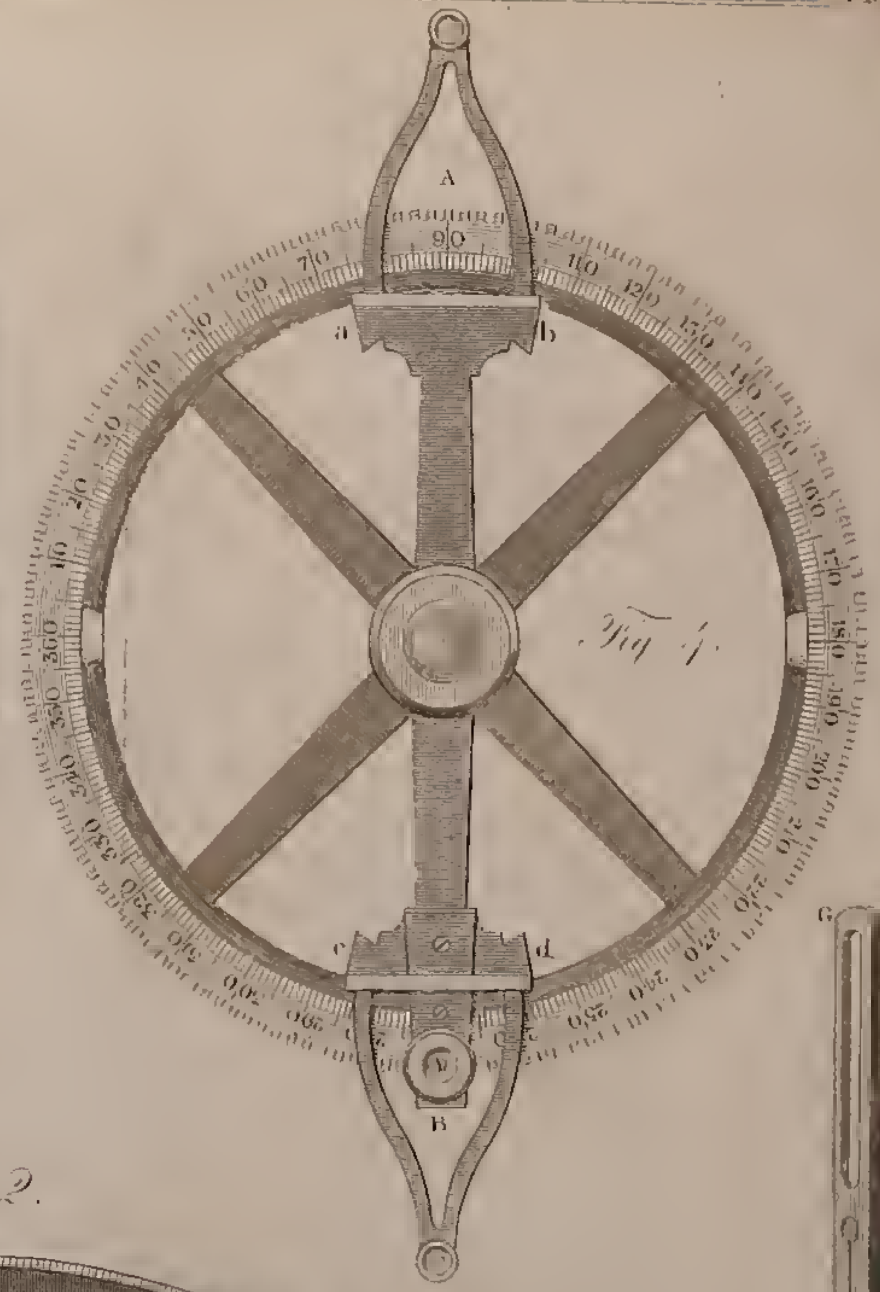
*Fig. 3.*



*Fig. 1.*

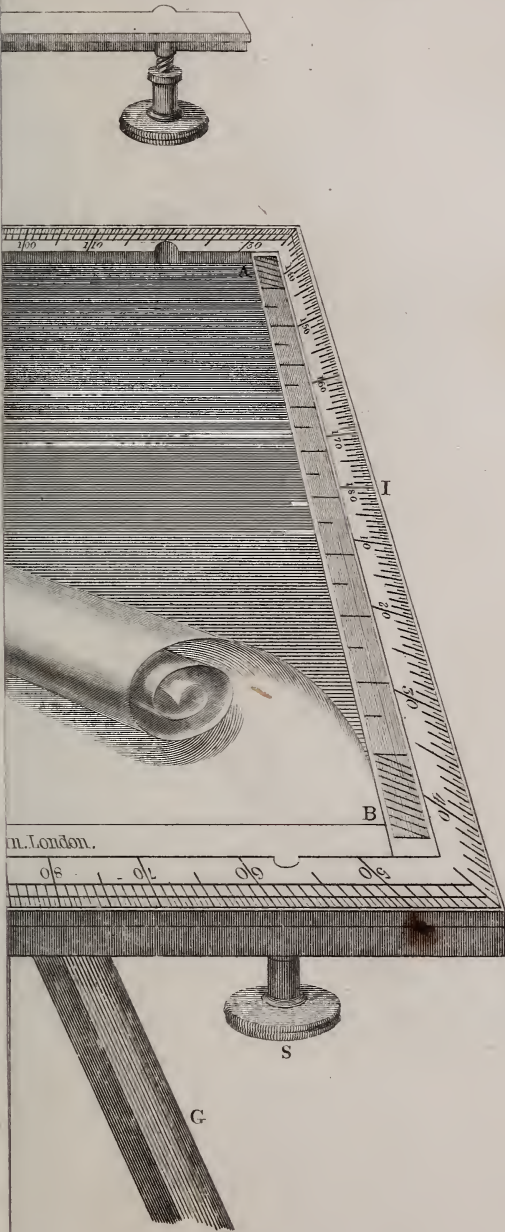


*Fig. 2.*





9.



n. London.

ndon.



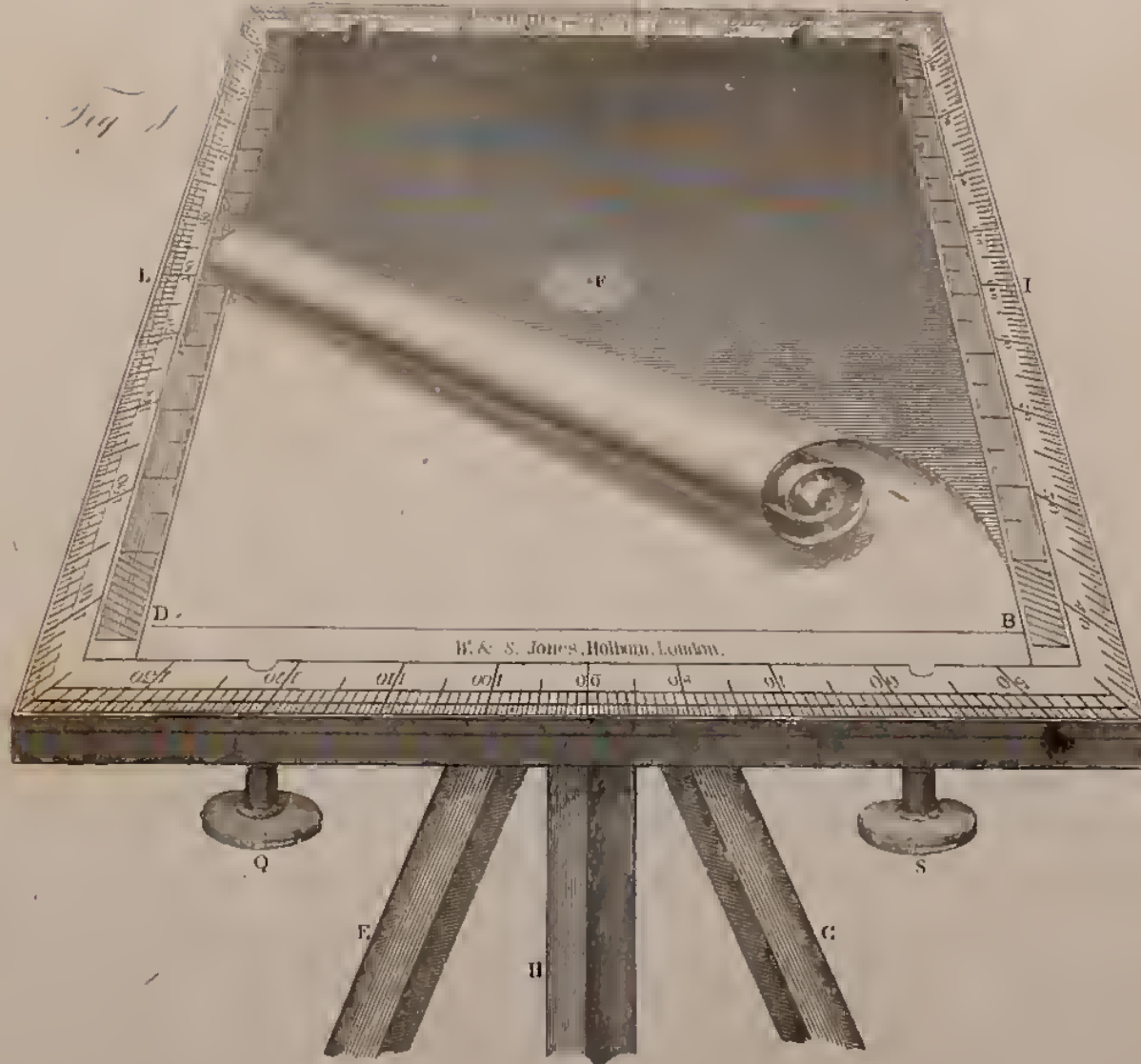




*Fig. 3.*

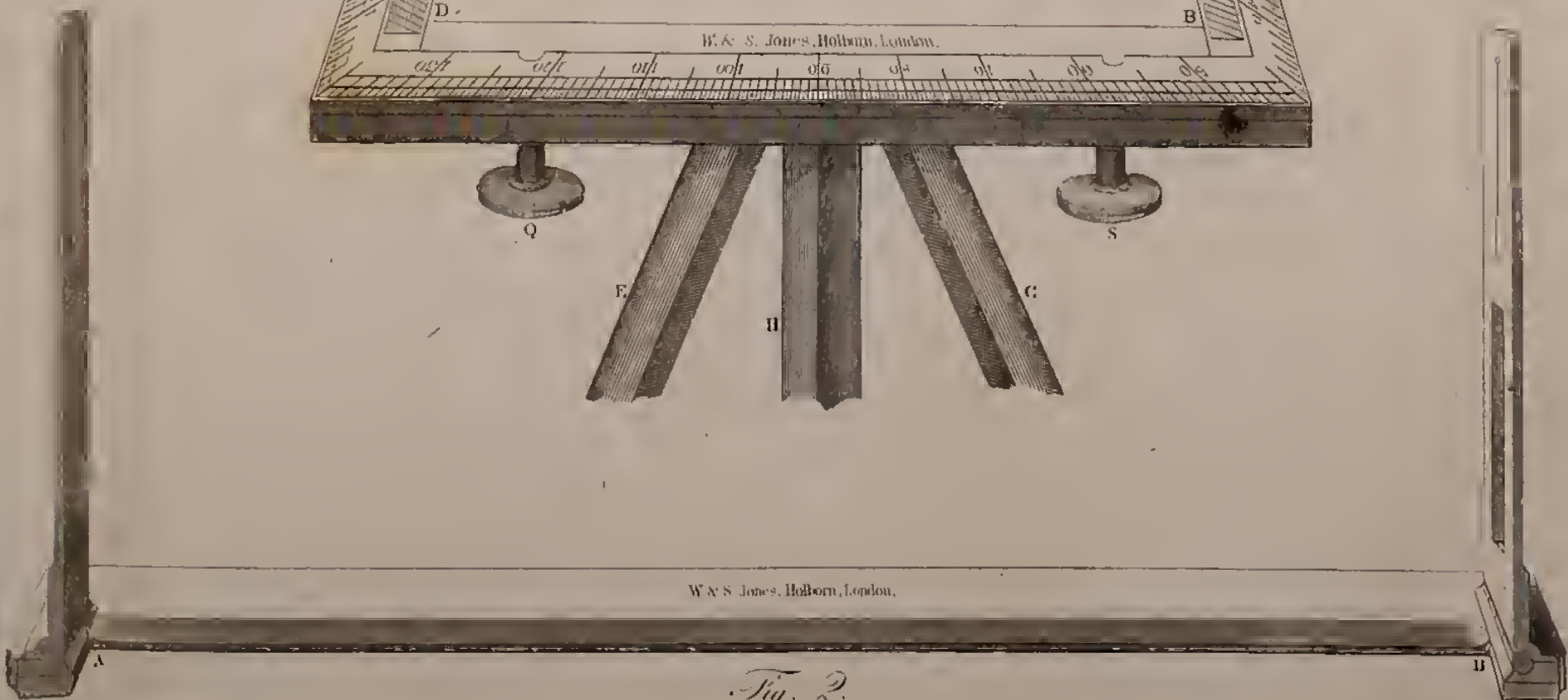


*Fig. 1.*

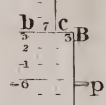
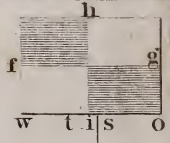
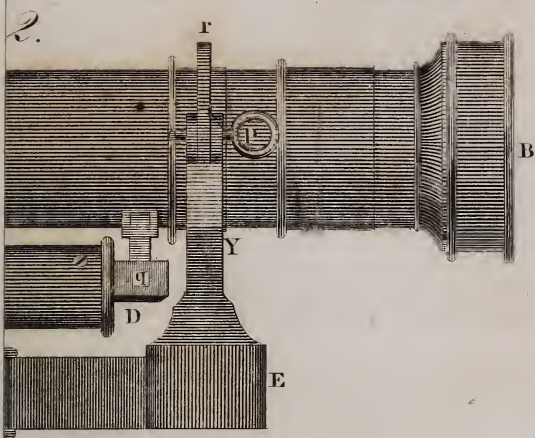


W & S. Jones, Holborn, London.

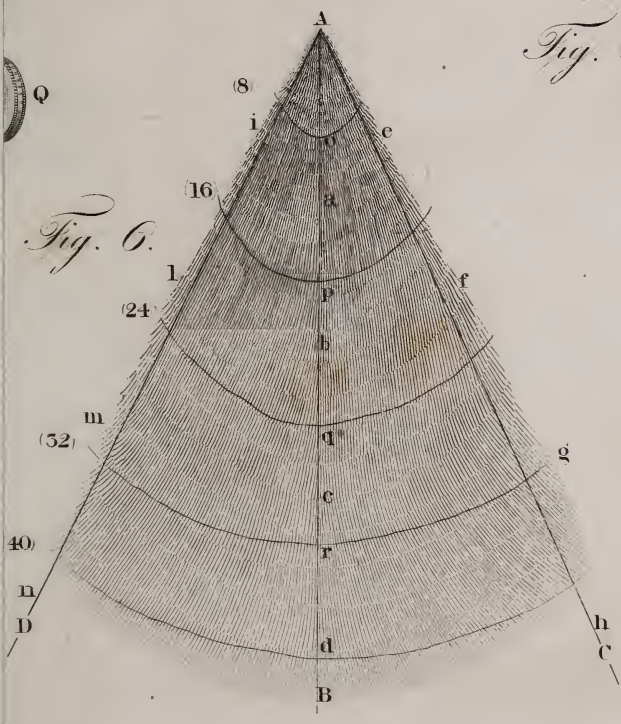
*Fig. 2.*



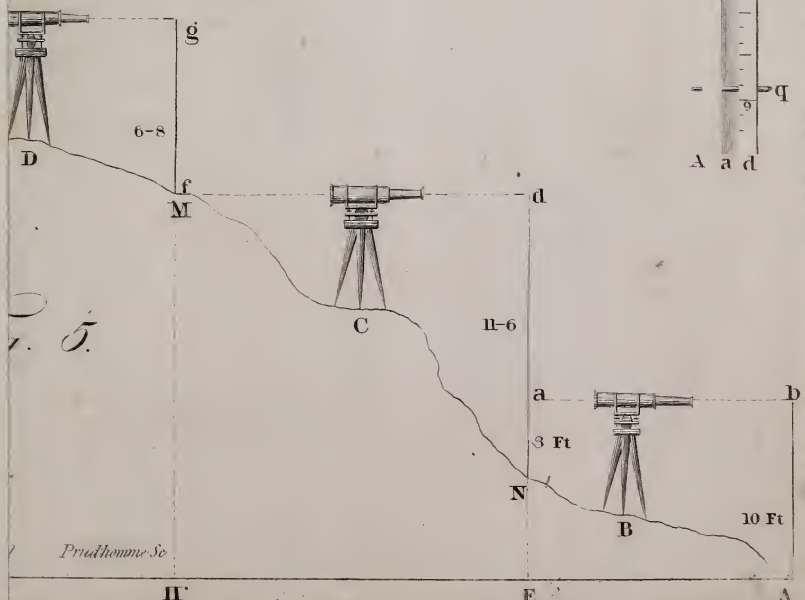
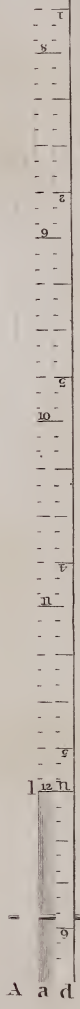




*Fig. 3.*



*Fig. 6.*



*Fig. 5.*

Prudhomme So



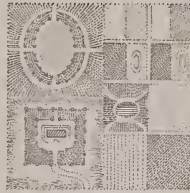




Rice Plant<sup>n</sup>



Gardens



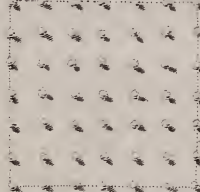
Cotton P.



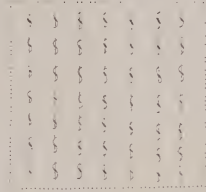
Ploughed L.



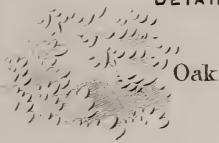
Orchards



Vine yard



DETAILS OF LEAVES



Oak



Fruit



Chestnut

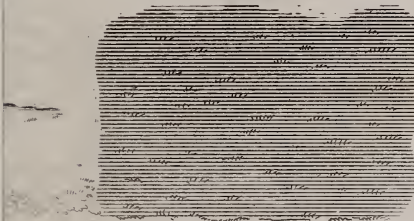
Heath



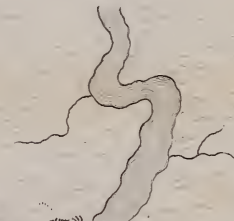
Oak Woods



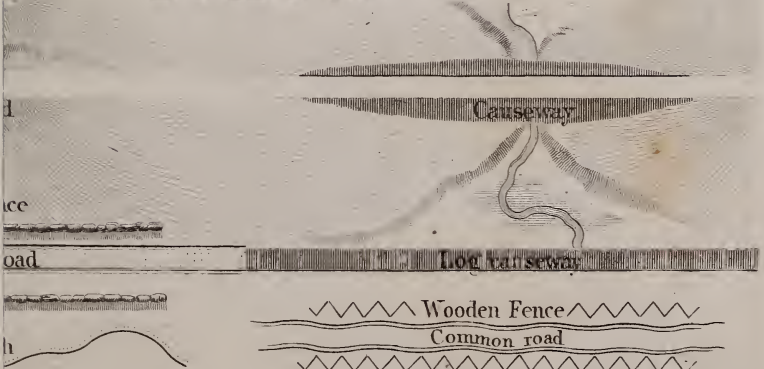
Salt Marsh



Meadows



ROADS &c.



Causeway



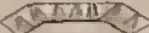
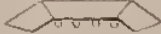












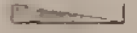









Log Causeway

Wooden Fence


Common road



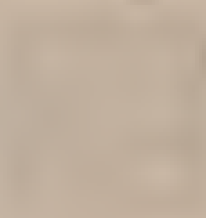


- Million* 
- Artillery Park* 
- Battery for Cannon* 
- Battery for Mortars* 
- Cemetery* 
- Givcery* 
- Cart House* 
- Cotton Factory* 
- Tavern* 
- Barn* 
- Glass Factory* 
- Church of a Village* 
- Do. Detached* 
- Foundry* 
- Forge* 
- Cavalry* 
- Industry* 
- House* 
- Mill, Wind* 
- Do. Water* 
- Do. Steam* 
- Do. of Stone* 
- Do. of Wood* 
- Post Office* 
- Trigonometrical Point* 
- Telegraph* 


**Tobacco P.**



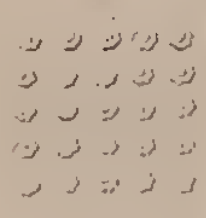
**Rice Plant<sup>g</sup>**



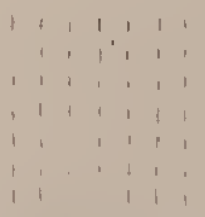
**Gardens**



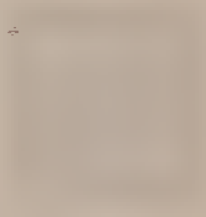
**Cotton P.**




**Sugar P.**




**Ploughed L.**



**Orchards**




**Vine yard**




**DETAILS OF LEAVES**


**Pine**




**Oak**




**Fruit**



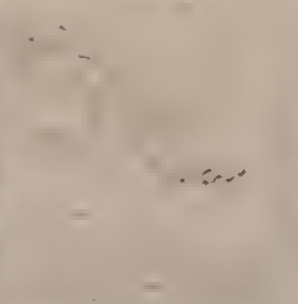
**Chesnut**




**Pine Woods**




**Heath**




**Oak Woods**




**Fresh Marsh**



**Salt Marsh**




**Meadows**




**ROADS &c.**

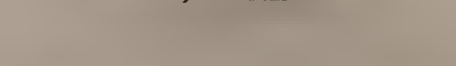
**Scarp road**



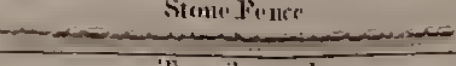
**Causeway**



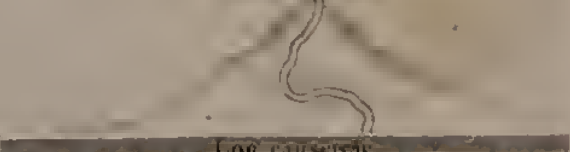
**Stone Fence**



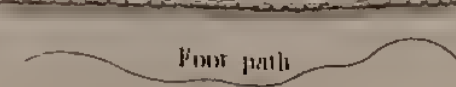
**Turnpike road**



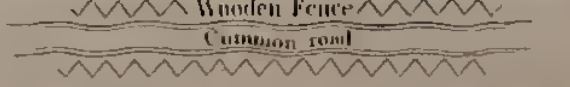
**Loe causeway**




**Foot path**



**Wooden Fence**

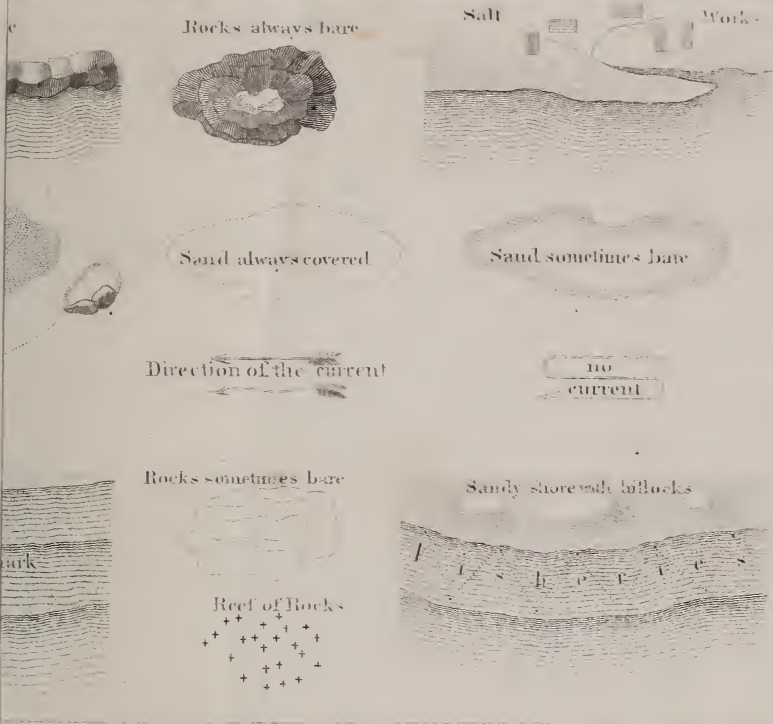


**Common road**









Drawn by S. J.






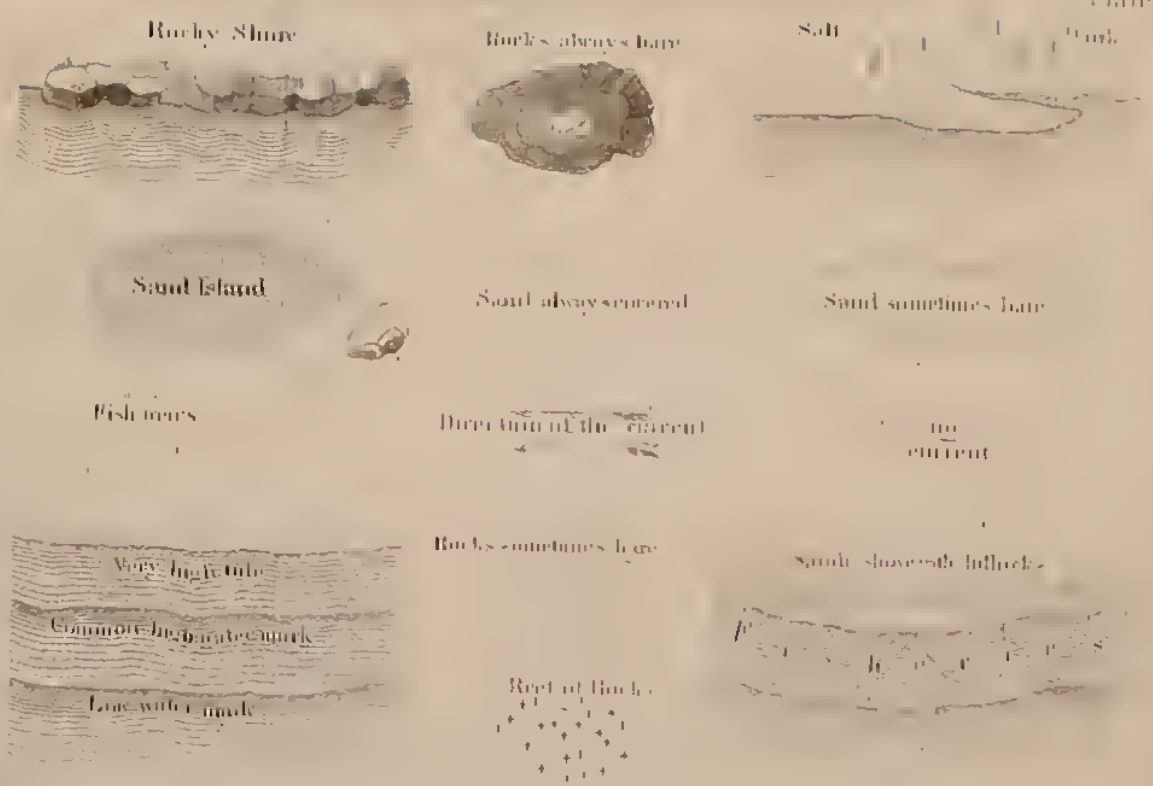
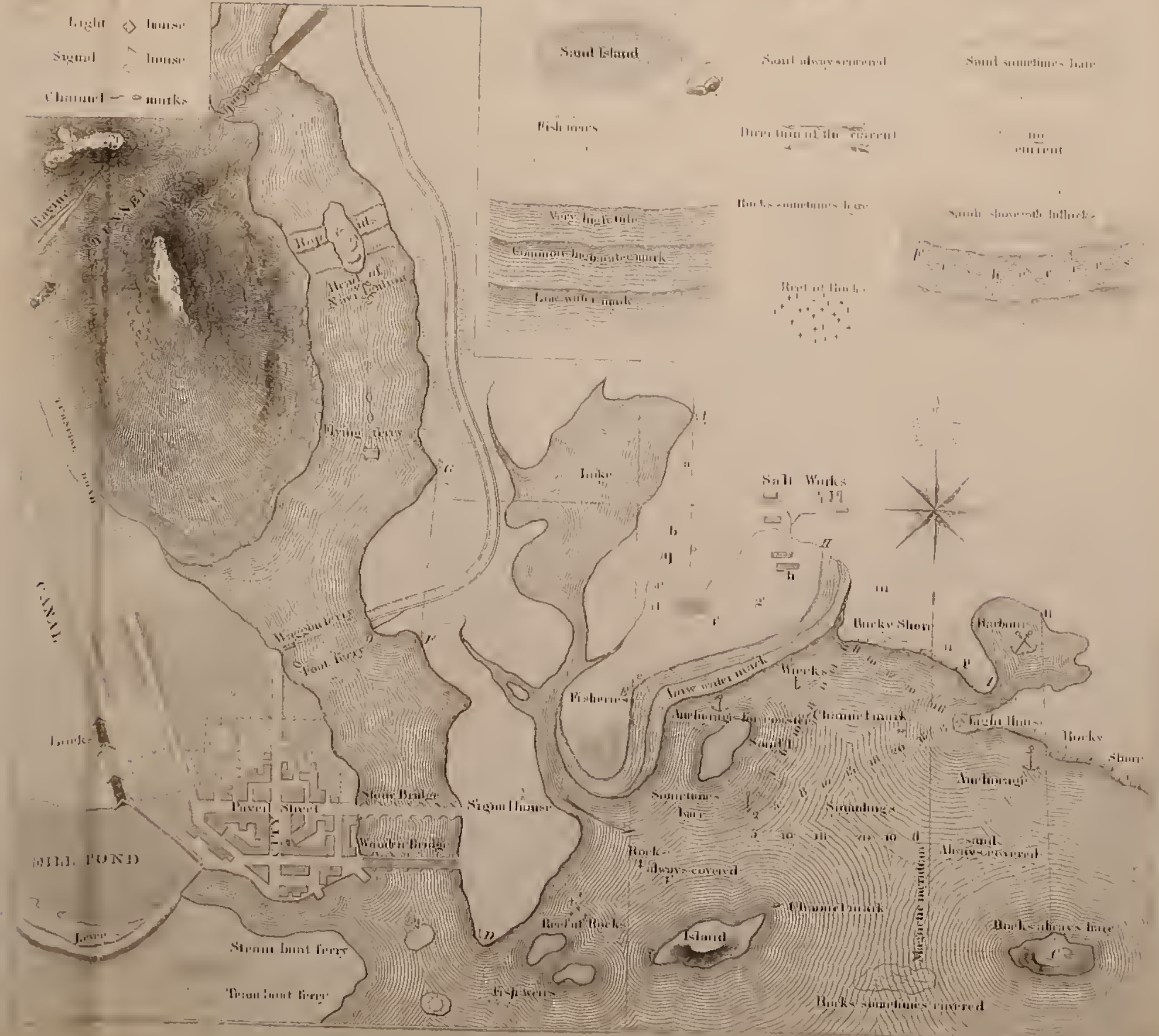




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 Anchorage for Boats   
 Rocks always covered 

Buoys   
 Wrecks   
 Harbours 

Light  house  
 Signal  house  
 Channel  marks













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