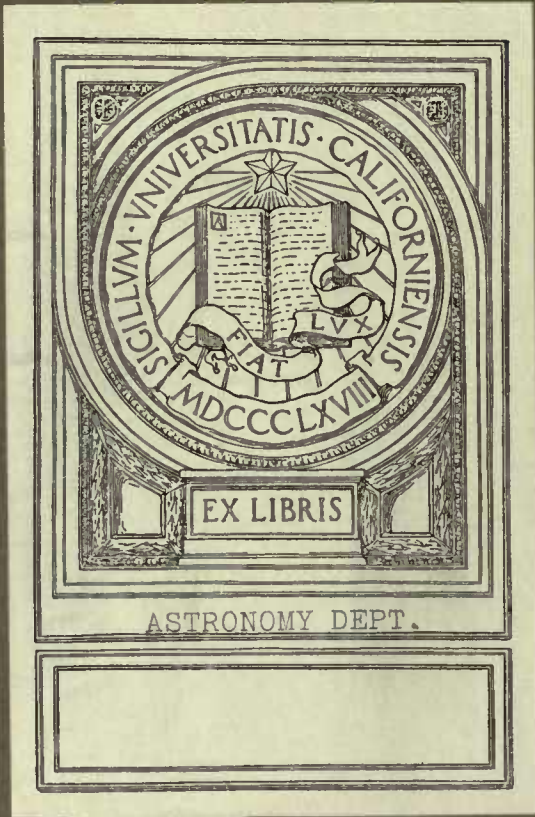


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INVESTIGATION OF INEQUALITIES IN THE
MOTION OF THE MOON PRODUCED BY
THE ACTION OF THE PLANETS

BY

SIMON NEWCOMB

ASSISTED BY

FRANK E. ROSS



WASHINGTON, D. C.:

PUBLISHED BY THE CARNEGIE INSTITUTION OF WASHINGTON

JUNE, 1907

TABLE III.—*Concluded.*

MUTUAL PERIODIC PERTURBATIONS OF VENUS AND THE EARTH.

The term of long period is omitted. The tabular unit is σ'' .01 in δu and $\delta v'$, and 10^{-8} in $\delta \rho$ and $\delta \rho'$.

| <i>i</i> | System 9. | | | | System 10. | | | | System 11. | | | |
|----------|------------|-------------|---------------|----------------|------------|-------------|---------------|----------------|------------|-------------|---------------|----------------|
| | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ |
| 0 | -598 | +447 | +196 | +563 | -548 | +407 | +300 | +495 | -205 | +158 | +341 | +471 |
| 1 | -544 | +318 | +174 | +583 | -616 | +355 | +295 | +500 | -371 | +169 | +372 | +454 |
| 2 | -482 | +176 | +237 | +552 | -660 | +285 | +355 | +409 | -540 | +175 | +468 | +393 |
| 3 | -444 | +36 | +357 | +487 | -698 | +200 | +465 | +398 | -718 | +179 | +591 | +306 |
| 4 | -446 | -90 | +493 | +394 | -747 | +109 | +579 | +301 | -897 | +176 | +700 | +207 |
| 5 | -493 | -196 | +613 | +285 | -811 | +19 | +673 | +193 | -1066 | +165 | +767 | +103 |
| 6 | -576 | -278 | +699 | +162 | -889 | -62 | +727 | +82 | -1208 | +141 | +783 | +0 |
| 7 | -690 | -338 | +744 | +26 | -980 | -127 | +732 | -32 | -1321 | +109 | +757 | -104 |
| 8 | -828 | -370 | +736 | -121 | -1073 | -171 | +681 | -142 | -1409 | +77 | +662 | -205 |
| 9 | -981 | -371 | +667 | -272 | -1164 | -194 | +577 | -254 | -1470 | +51 | +516 | -300 |
| 10 | -1138 | -335 | +522 | -420 | -1249 | -193 | +416 | -364 | -1497 | +39 | +342 | -384 |
| 11 | -1274 | -260 | +298 | -553 | -1290 | -166 | +203 | -472 | -1484 | +41 | +114 | -456 |
| 12 | -1360 | -147 | -3 | -661 | -1310 | -113 | -60 | -569 | -1423 | +59 | -147 | -517 |
| 13 | -1372 | -1 | -351 | -740 | -1274 | -29 | -364 | -648 | -1314 | +95 | -427 | -566 |
| 14 | -1288 | +164 | -715 | -783 | -1176 | +83 | -693 | -699 | -1154 | +147 | -711 | -603 |
| 15 | -1106 | +339 | -1055 | -786 | -1000 | +222 | -1015 | -716 | -938 | +220 | -987 | -624 |
| 16 | -835 | +504 | -1328 | -753 | -741 | +374 | -1301 | -605 | -669 | +311 | -1237 | -620 |
| 17 | -493 | +654 | -1520 | -682 | -415 | +530 | -1511 | -637 | -346 | +420 | -1438 | -583 |
| 18 | -106 | +779 | -1609 | -576 | -40 | +671 | -1617 | -549 | +19 | +536 | -1561 | -510 |
| 19 | +308 | +876 | -1582 | -440 | +353 | +791 | -1605 | -431 | +413 | +651 | -1579 | -403 |
| 20 | +710 | +938 | -1438 | -282 | +726 | +878 | -1469 | -293 | +793 | +749 | -1470 | -270 |
| 21 | +1072 | +964 | -1180 | -108 | +1049 | +933 | -1225 | -135 | +1126 | +821 | -1260 | -116 |
| 22 | +1359 | +948 | -820 | +68 | +1323 | +949 | -880 | +33 | +1387 | +862 | -940 | +40 |
| 23 | +1532 | +899 | -399 | +242 | +1501 | +927 | -467 | +207 | +1547 | +867 | -544 | +202 |
| 24 | +1580 | +816 | +54 | +405 | +1572 | +853 | -13 | +376 | +1600 | +835 | -101 | +359 |
| 25 | +1493 | +711 | +494 | +551 | +1525 | +765 | +446 | +530 | +1546 | +769 | +355 | +509 |
| 26 | +1278 | +592 | +885 | +677 | +1353 | +632 | +659 | +1379 | +667 | +791 | +644 | |
| 27 | +957 | +466 | +1210 | +778 | +1070 | +479 | +1221 | +759 | +1116 | +533 | +1174 | +757 |
| 28 | +558 | +336 | +1436 | +849 | +701 | +316 | +1471 | +833 | +766 | +372 | +1460 | +841 |
| 29 | +106 | +205 | +1545 | +884 | +271 | +153 | +1600 | +874 | +353 | +192 | +1627 | +837 |
| 30 | -355 | +73 | +1534 | +883 | -179 | -1 | +1609 | +886 | -84 | +6 | +1659 | +806 |
| 31 | -791 | -59 | +1404 | +848 | -621 | -142 | +1501 | +867 | -515 | -171 | +1565 | +870 |
| 32 | -1164 | -183 | +1169 | +780 | -1026 | -270 | +1278 | +815 | -909 | -330 | +1357 | +814 |
| 33 | -1439 | -297 | +851 | +660 | -1358 | -383 | +961 | +733 | -1234 | -466 | +1050 | +735 |
| 34 | -1594 | -393 | +497 | +581 | -1592 | -477 | +574 | +621 | -1476 | -573 | +673 | +632 |
| 35 | -1633 | -471 | +134 | +465 | -1704 | -550 | +154 | +491 | -1629 | -652 | +250 | +511 |
| 36 | -1560 | -537 | -225 | +345 | -1684 | -602 | -256 | +351 | -1601 | -707 | -183 | +370 |
| 37 | -1402 | -594 | -544 | +226 | -1549 | -630 | -620 | +209 | -1579 | -733 | -596 | +216 |
| 38 | -1173 | -645 | -818 | +115 | -1317 | -639 | -923 | +77 | -1384 | -730 | -959 | +60 |
| 39 | -879 | -694 | -1058 | +11 | -1017 | -637 | -1149 | -43 | -1098 | -703 | -1232 | -82 |
| 40 | -540 | -740 | -1237 | -84 | -674 | -631 | -1301 | -150 | -752 | -654 | -1403 | -219 |
| 41 | -159 | -783 | -1347 | -169 | -303 | -627 | -1384 | -244 | -375 | -595 | -1473 | -324 |
| 42 | +244 | -813 | -1390 | -245 | +80 | -626 | -1396 | -324 | +3 | -532 | -1450 | -403 |
| 43 | +651 | -838 | -1365 | -315 | +405 | -626 | -1342 | -391 | +304 | -477 | -1357 | -462 |
| 44 | +1039 | -849 | -1275 | -383 | +835 | -623 | -1225 | -442 | +697 | -432 | -1208 | -504 |
| 45 | +1399 | -845 | -1121 | -449 | +1181 | -617 | -1049 | -478 | +1001 | -396 | -1009 | -531 |
| 46 | +1708 | -821 | -911 | -509 | +1482 | -607 | -832 | -502 | +1264 | -368 | -778 | -542 |
| 47 | +1946 | -768 | -642 | -562 | +1728 | -591 | -580 | -517 | +1480 | -346 | -520 | -536 |
| 48 | +2089 | -681 | -322 | -601 | +1908 | -566 | -303 | -526 | +1640 | -328 | -248 | -515 |
| 49 | +2122 | -555 | +27 | -621 | +2014 | -524 | -15 | -527 | +1743 | -312 | +17 | -481 |
| 50 | +2026 | -393 | +372 | -611 | +2027 | -460 | +276 | -514 | +1784 | -298 | +265 | -434 |
| 51 | +1803 | -207 | +678 | -570 | +1939 | -371 | +548 | -479 | +1761 | -283 | +487 | -378 |
| 52 | +1482 | -11 | +912 | -469 | +1744 | -254 | +779 | -418 | +1679 | -259 | +673 | -314 |
| 53 | +1093 | +178 | +1054 | -396 | +1454 | -116 | +942 | -327 | +1528 | -221 | +813 | -236 |
| 54 | +679 | +344 | +1097 | -269 | +1097 | +27 | +1017 | -213 | +1313 | -169 | +895 | -145 |
| 55 | +279 | +477 | +1042 | -117 | +709 | +166 | +995 | -80 | +1044 | -101 | +900 | -31 |
| 56 | -71 | +569 | +906 | +49 | +331 | +284 | +884 | +66 | +743 | -27 | +825 | +30 |
| 57 | -344 | +612 | +710 | +217 | +3 | +371 | -716 | +209 | +451 | +43 | +686 | +234 |
| 58 | -523 | +603 | +497 | +370 | -254 | +418 | +536 | +337 | +189 | +99 | +525 | +354 |
| 59 | -601 | +548 | +312 | +489 | -434 | +430 | +385 | +437 | -27 | +137 | +397 | +437 |

TABLE IV_a.
PERTURBATIONS OF THE G-COÖRDINATE X OF VENUS.

The tabular unit is 10⁻⁸.

| System <i>i</i> | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------------|------|------|------|------|------|------|------|------|------|------|------|------|
| 0 | + 47 | + 57 | + 92 | +137 | +181 | +217 | +218 | +184 | +142 | +107 | + 71 | + 52 |
| 1 | + 37 | + 50 | + 81 | +118 | +159 | +197 | +212 | +183 | +140 | + 92 | + 52 | + 30 |
| 2 | - 11 | + 11 | + 41 | + 71 | +109 | +149 | +176 | +158 | +114 | + 59 | + 8 | - 23 |
| 3 | - 92 | - 59 | - 24 | + 5 | + 39 | + 75 | +112 | +111 | + 72 | + 9 | - 52 | - 97 |
| 4 | -193 | -154 | -111 | - 79 | - 50 | - 14 | + 26 | + 46 | + 14 | - 48 | -122 | -183 |
| 5 | -305 | -269 | -217 | -183 | -156 | -122 | - 79 | - 41 | - 55 | -111 | -191 | -268 |
| 6 | -412 | -396 | -338 | -290 | -267 | -237 | -197 | -146 | -136 | -179 | -261 | -348 |
| 7 | -506 | -519 | -405 | -405 | -380 | -354 | -318 | -263 | -230 | -251 | -326 | -421 |
| 8 | -581 | -628 | -586 | -519 | -487 | -468 | -437 | -384 | -331 | -330 | -386 | -482 |
| 9 | -636 | -715 | -696 | -629 | -583 | -569 | -546 | -502 | -437 | -410 | -443 | -530 |
| 10 | -668 | -763 | -780 | -718 | -661 | -650 | -636 | -599 | -539 | -488 | -494 | -565 |
| 11 | -674 | -777 | -827 | -783 | -718 | -699 | -697 | -672 | -619 | -556 | -534 | -582 |
| 12 | -660 | -759 | -828 | -814 | -745 | -714 | -722 | -710 | -669 | -606 | -561 | -580 |
| 13 | -621 | -710 | -790 | -803 | -745 | -699 | -707 | -712 | -682 | -625 | -569 | -560 |
| 14 | -559 | -639 | -713 | -749 | -709 | -652 | -652 | -671 | -659 | -610 | -552 | -523 |
| 15 | -479 | -541 | -614 | -659 | -640 | -580 | -564 | -591 | -596 | -559 | -507 | -466 |
| 16 | -383 | -431 | -495 | -542 | -540 | -487 | -452 | -475 | -496 | -476 | -432 | -389 |
| 17 | -279 | -308 | -364 | -410 | -417 | -374 | -325 | -337 | -368 | -366 | -331 | -298 |
| 18 | -171 | -183 | -231 | -273 | -283 | -251 | -195 | -187 | -221 | -236 | -213 | -187 |
| 19 | - 54 | - 61 | - 98 | -137 | -149 | -123 | - 68 | - 38 | - 66 | - 95 | - 84 | - 64 |
| 20 | + 60 | + 56 | + 25 | - 13 | - 26 | - 1 | + 48 | + 93 | + 80 | + 46 | + 41 | + 58 |
| 21 | +170 | +160 | +136 | +100 | + 82 | +106 | +151 | +203 | +209 | +179 | +155 | +171 |
| 22 | +269 | +253 | +229 | +197 | +174 | +192 | +236 | +288 | +312 | +291 | +262 | +266 |
| 23 | +350 | +330 | +305 | +275 | +249 | +259 | +299 | +350 | +384 | +377 | +348 | +342 |
| 24 | +406 | +392 | +363 | +333 | +307 | +306 | +341 | +387 | +430 | +434 | +412 | +398 |
| 25 | +441 | +436 | +407 | +373 | +347 | +338 | +367 | +412 | +451 | +466 | +456 | +437 |
| 26 | +461 | +460 | +435 | +400 | +374 | +361 | +378 | +418 | +457 | +475 | +476 | +464 |
| 27 | +468 | +471 | +451 | +417 | +388 | +372 | +380 | +418 | +454 | +478 | +483 | +478 |
| 28 | +476 | +475 | +459 | +426 | +394 | +381 | +379 | +411 | +447 | +472 | +481 | +484 |
| 29 | +480 | +475 | +403 | +432 | +397 | +381 | +379 | +405 | +440 | +465 | +475 | +485 |
| 30 | +484 | +479 | +467 | +438 | +401 | +380 | +380 | +401 | +434 | +459 | +473 | +479 |
| 31 | +490 | +484 | +476 | +445 | +406 | +380 | +380 | +397 | +431 | +457 | +470 | +476 |
| 32 | +491 | +492 | +483 | +455 | +414 | +380 | +379 | +392 | +426 | +456 | +469 | +473 |
| 33 | +485 | +497 | +488 | +460 | +417 | +379 | +375 | +387 | +419 | +451 | +467 | +466 |
| 34 | +468 | +492 | +489 | +463 | +420 | +377 | +362 | +375 | +403 | +437 | +456 | +456 |
| 35 | +439 | +468 | +479 | +458 | +414 | +366 | +341 | +354 | +377 | +411 | +432 | +436 |
| 36 | +397 | +426 | +448 | +437 | +392 | +342 | +310 | +314 | +338 | +368 | +391 | +399 |
| 37 | +340 | +360 | +394 | +396 | +353 | +301 | +262 | +260 | +282 | +311 | +331 | +343 |
| 38 | +263 | +270 | +309 | +327 | +293 | +240 | +196 | +184 | +208 | +236 | +255 | +264 |
| 39 | +167 | +166 | +199 | +230 | +211 | +155 | +109 | + 90 | +112 | +141 | +161 | +166 |
| 40 | + 56 | + 47 | + 69 | +107 | +104 | + 51 | + 2 | - 20 | - 4 | + 33 | + 55 | + 57 |
| 41 | - 67 | - 80 | - 74 | - 38 | - 22 | - 67 | -121 | -145 | -127 | - 90 | - 59 | - 58 |
| 42 | -188 | -206 | -215 | -188 | -161 | -192 | -254 | -283 | -265 | -222 | -180 | -172 |
| 43 | -301 | -325 | -344 | -336 | -306 | -310 | -381 | -420 | -407 | -357 | -304 | -282 |
| 44 | -397 | -430 | -459 | -464 | -443 | -438 | -494 | -549 | -543 | -486 | -423 | -385 |
| 45 | -473 | -510 | -545 | -568 | -557 | -544 | -589 | -656 | -665 | -609 | -534 | -475 |
| 46 | -528 | -560 | -605 | -634 | -638 | -626 | -655 | -729 | -760 | -712 | -628 | -555 |
| 47 | -566 | -578 | -626 | -665 | -681 | -678 | -694 | -764 | -818 | -791 | -702 | -617 |
| 48 | -585 | -574 | -611 | -660 | -685 | -692 | -703 | -759 | -833 | -833 | -749 | -657 |
| 49 | -588 | -547 | -566 | -619 | -653 | -668 | -679 | -723 | -805 | -838 | -775 | -675 |
| 50 | -572 | -508 | -506 | -549 | -588 | -609 | -627 | -659 | -737 | -796 | -766 | -668 |
| 51 | -539 | -457 | -431 | -454 | -499 | -525 | -545 | -571 | -639 | -716 | -723 | -639 |
| 52 | -491 | -401 | -347 | -350 | -391 | -423 | -447 | -470 | -525 | -605 | -644 | -589 |
| 53 | -431 | -339 | -268 | -248 | -276 | -311 | -333 | -357 | -401 | -477 | -535 | -518 |
| 54 | -362 | -274 | -193 | -152 | -162 | -197 | -222 | -247 | -281 | -346 | -414 | -428 |
| 55 | -283 | -205 | -122 | - 69 | - 58 | - 88 | -111 | -137 | -167 | -219 | -286 | -324 |
| 56 | -199 | -134 | - 58 | + 2 | + 31 | + 14 | - 14 | - 37 | - 64 | -106 | -164 | -211 |
| 57 | -114 | - 67 | - 3 | + 60 | +101 | +102 | + 73 | + 48 | + 20 | - 14 | - 60 | -105 |
| 58 | - 38 | - 8 | + 44 | +104 | +151 | +167 | +144 | +115 | + 85 | + 54 | + 16 | - 18 |
| 59 | + 19 | + 36 | + 78 | +130 | +179 | +208 | +194 | +161 | +128 | + 94 | + 59 | + 36 |

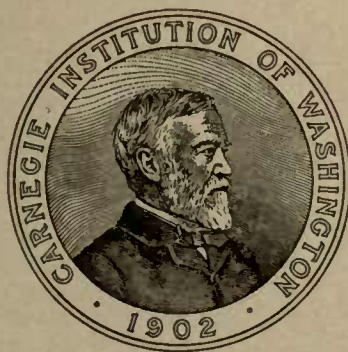
INVESTIGATION OF INEQUALITIES IN THE
MOTION OF THE MOON PRODUCED BY
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WASHINGTON, D. C.:
PUBLISHED BY THE CARNEGIE INSTITUTION OF WASHINGTON
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LANCASTER, PA.

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PREFACE.

THE immediate incentive to the present work was the hope of explaining by gravitational theory the observed variations in the mean longitude of the Moon, shown by more than two centuries of observation to exist, but not yet satisfactorily accounted for. The author has published a number of papers and memoirs on this subject during the last forty years, terminating with a summary of the case, which appeared in the *Monthly Notices of the Royal Astronomical Society* for March, 1904. The deviations in question offer the greatest enigma yet encountered in explaining the motions of the heavenly bodies, and the present paper may be regarded as a contribution to the study of the problem thus offered.

While the work was in progress the completing chapter of Professor Brown's *Theory of the Moon's Motion* appeared. The actual work being based on Delaunay's theory, it seemed to be desirable to revise and correct it by Brown's results. In doing this the imperfections of Delaunay's theory as a basis became so evident, and the later theory proved to be so much better adapted to the purpose of the investigation, that the completed work gradually became step by step practically based upon Brown's theory, except in those parts requiring derivatives which could not be readily obtained except from Delaunay's literal expressions. Acknowledgment is due to Professor Brown for courteous advice and assistance which facilitated the use of his work for the purpose.

The theory of the action of the planets on the Moon being, in several points, the most intricate with which the mathematical astronomer has to deal, it is important that its development should be presented in a form to render as easy as possible the detection of errors or imperfections. In the arrangement of the work this end has been kept constantly in view. It is hoped that any investigator desiring to test the processes will find few difficulties except those necessarily inherent in the nature of the work.

To form a general conception of the arrangement it may be stated that the work naturally divides itself into four parts. One of these treats of the theory of the subject, including under this head not only the general equations, but the numerical details on which all the computations are based. In this part the fundamental quantities are reduced to products of two factors, one of which depends upon the coördinates of the planet; the other upon the geocentric coördinates of the Moon. The first factors, termed planetary, are numerically developed in Part II. This development falls into two parts, one treating the direct action of the planet, the other the indirect action through the Sun. In Part III is found the numerical

development of the factors depending upon the Moon alone, and of their partial derivatives as to the lunar elements. In Part IV is presented the combinations of these two factors and the final results of the work.

A more complete summary in detail is found in the table of contents. An effort has been made to lessen the trouble of finding the definitions of the symbols used by collecting in the introduction definitions or references to these symbols as to the meaning of which doubt might be felt.

A word may be added as to the part taken by the author's assistant. At an early stage in the work Dr. Ross made a practically independent computation of the principal periodic inequalities, using the methods of Hill and Radau. In doing this he discovered the error of the Jovian evection as computed by them, which arose from the omission of what we may call the side-terms in the indirect action. His result for the coefficient was $1''.16$, in exact agreement with that originally found by Mr. Neville. In this early stage of the work the writer did not intend to do much more than revise these computations, and make a thorough investigation of the terms of long period. But he found the theory of the subject so interesting, and the opportunity for recasting the methods so attractive, that he was led to carry the work through, with Dr. Ross's assistance, on the basis of his own developments.

The next step in logical order is the rediscussion of the moon's mean longitude since 1650, as derived from occultations of stars, with a view of learning what modifications will be produced by the use of the more rigorous data now available, and the addition of thirty years to the period of available observations. This rediscussion will, the writer hopes, be his next contribution to the subject of the motion of the Moon.

It remains to add that the work has been prosecuted under the auspices of the Carnegie Institution of Washington, without the help of which it could not have been undertaken.

SIMON NEWCOMB.

WASHINGTON, MAY, 1907.

UNIVERSITY OF
CALIFORNIA

ACTION OF THE PLANETS ON THE MOON.

INTRODUCTION.

MORE than thirty years ago the author proposed to treat the action of the planets on the Moon by using the Lagrangian differential equations for the variation of the elements by considering as simultaneously variable, not only what are commonly called the elements of the Moon, but those of the orbit of the centre of mass of the Earth-Moon around the Sun also.* Twelve elements would thus come in, and the coördinates both of the Moon and of the Sun would be expressed in terms of the osculating values of all these elements.

Notwithstanding the favorable opinion of this method expressed at the time by Professor Cayley, and later, as to some of its processes, by Professor E. W. Brown, the author found that, in applying it unmodified, which he did during the years 1872-77, very long and complex computations were required in its application. The result was that the work, so far as it was carried, remained unpublished for nearly twenty years. Hoping that the general developments of the work and some of the details might be of use to subsequent investigators, the incomplete work was finally published in 1895.

About the same time with the publication of this work appeared the very elaborate one of Radau.† This work contains a seemingly exhaustive enumeration of possible inequalities of long period, and the numerical computation of a great number of lunar inequalities due to the action of the planets which had not previously been suspected.

On recommencing the work in 1904 it became very clear to the author that its completion by his former method, unmodified, would be impracticable, and that satisfactory results could best be reached by regarding the solar elements as constants, or known variables from the beginning. In the present investigation, therefore, the method has been modified so that the final values of the coördinates of the Moon, instead of being expressed as functions of the instantaneous elements of the Earth's disturbed motion, are expressed as functions of the mean elements. As thus modified it is substantially a continuation of that of Delaunay, as applied

* *Liouville, Journal des Mathématiques*, 1871, March.

† *Annales de l'Observatoire de Paris, Mémoires*, vol. xx1.

first by Hill and then by Radau. In this method the coördinates of the Sun, relative to the centre of gravity of the Earth and Moon, are regarded as known functions of the time. Then, when the action of the Sun alone is considered, the coördinates of the Moon relative to the Earth are found by the method of Delaunay, completed if necessary, as functions of six purely arbitrary constants.

This solution of the problem of three bodies is supposed to be complete in advance. When the action of the planets is then taken into consideration, the only elements whose variations are to be determined by the Lagrangian equations are the six final elements of the Moon's motion. The variations in the coördinates of the Sun, due to the same action, are derived with great ease, and enter into the differential equations. In this way a system of six differential equations for the determination of the changes in the lunar elements is all that is necessary.

In setting forth the subject it is deemed unnecessary to repeat the derivation of the equations already found in astronomical literature. For this branch of the subject, reference may be had to Hill's paper in the *American Journal of Mathematics*, Vol. VI, and to Chapter XIII of the *Treatise on the Lunar Theory* by E. W. Brown. It is deemed necessary only to explain fully, at each point, the application of the method, and the meaning of the symbols introduced.

PART I.

DEVELOPMENT OF THE THEORY.

CHAPTER I.

FUNDAMENTAL DIFFERENTIAL EQUATIONS.

§ 1. *Notation.* The following notation is mostly used in this work:

G, when designating a point, centre of mass of Earth and Moon; m' , mass of the Sun; m_2 , mass of the Earth; m_3 , mass of the Moon; m_4 , mass of the Planet.

$$\mu = m_2 + m_3 \qquad \mu' = m' + \mu$$

x, y, z, r , geocentric coördinates and radius vector of the Moon, referred to the moving ecliptic;

x', y', z', r' , coördinates and radius vector of the Sun, referred to the point G and the moving ecliptic;

ξ, η, ζ , and ρ , the ratios of x, y, z , and r of the Moon to the mean distance of the latter: $x = a\xi$, etc. When unmarked the coördinates are referred to a moving X -axis directed toward the mean Sun;

x_1, y_1 , Moon coördinates referred to the mean Moon as the X -axis;

Δ , distance of the Planet from G;

S , cosine of angle between r and r' ;

S' , cosine of angle between r and Δ ;

P_0 , potential function of mutual action of Earth and Moon;

Ω , potential function for action of Sun on Moon;

R , potential function for action of Planet on Moon;

l, π, θ , mean longitude, longitude of perigee, longitude of node of Moon;

π_1, θ_1 , motions of π and θ in unit of time (quantities of dimensions T^{-1});

N , motion of argument in unit of time;

n , ratio of motion of an argument to n , the mean motion of the Moon;

ν , the integrating factor, generally $= n/N$;

a, e, g , defined in (43), § 22;

K, C, D , planetary coefficients for the direct action, defined in § 20;

p, q, κ_4 , lunar coefficients, § 20 Eq. (36);

G, J, I , planetary coefficients for the indirect action, defined in § 24;

G is also used for a combined lunar and planetary argument;

a , logarithm of a , the Moon's mean distance;

v, m, j, s , the mean longitudes of the respective planets, Venus, Mars, Jupiter, and Saturn measured, in each case, from the Earth's perihelion: π' for 1800=99.°5.

The abbreviation "Action" has been used to designate the previous work of the author on this subject — "Theory of the Inequalities in the motion of the Moon produced by the Action of the Planets"; forming Part III of *Astronomical Papers of the American Ephemeris*, Vol. V.

§ 2. *Dimensions of quantities.* In this subject it will be found helpful to the reader and investigator to have, in the case of the principal equations, a statement of their dimensions in terms of the fundamental units of Mass, Time, and Length. In strictness an independent unit of mass is not necessary in gravitational astronomy, because the most convenient unit is that mass which, on an equal mass at unit distance, exerts a unit force of gravitation. But it is still sometimes convenient to use this unit in the equations, although it is a derived one.

In the case of each system of equations which are regarded as fundamental will be found the dimensions of the terms which form its members, the signification being as follows:

$$T, \text{ Time}; \quad L, \text{ Length}; \quad M, \text{ Mass.}$$

The definition of the unit of mass just given leads to the relation

$$M = L^3 T^{-2}$$

In this way it will be much easier than it would be without this help to appreciate the degree of magnitude of small quantities. Considered by itself, no concrete quantity can be regarded as small or great; it is so only when compared with other quantities of the same kind, or, to speak more accurately, of the same dimensions in fundamental quantities. The ratios of two fundamental quantities of the same kind are pure numbers, and these may be large or small to any extent.

§ 3. *Fundamental differential equations.*

Putting

x_1, y_1, z_1 , the geocentric coördinates of the Moon referred to any system of fixed axes,

P , the total potential

the differential equations to be integrated may be written

$$D_t^2 x_1 = \frac{\partial P}{\partial x_1} \quad D_t^2 y_1 = \frac{\partial P}{\partial y_1} \quad D_t^2 z_1 = \frac{\partial P}{\partial z_1} \quad [\text{Dimensions} = ML^{-1} = LT^{-2}] \quad (1)$$

§ 4. *Transformation to the moving ecliptic.* In the preceding equations the coördinates are referred to fixed axes. In astronomical practice the coördinates of the heavenly bodies are referred to the moving ecliptic. The latter carries the plane of the Moon's orbit with it in its motion. It therefore seems desirable to refer the motion, in the first place, to the moving ecliptic.

To do this let us put

x, y, z , coördinates referred to the moving ecliptic;

κ , the speed of motion of the plane of the ecliptic;

Π , the longitude of the ascending node of the moving on the fixed ecliptic, or of the instantaneous axis of rotation of the ecliptic. At the present time we have $\Pi = 173^\circ$, nearly.

Then, regarding κt as infinitesimal, the expression for the moving coördinates in terms of the fixed ones will be

$$x = x_1 - z_1 \kappa \sin \Pi$$

$$y = y_1 + z_1 \kappa \cos \Pi$$

$$z = z_1 + x_1 \kappa \sin \Pi - y_1 \kappa \cos \Pi$$

Putting for brevity

$$p = \kappa \sin \Pi \quad q = \kappa \cos \Pi \quad [\text{Dim. of } p, q, \text{ and } \kappa = T^{-1}],$$

these expressions become

$$x = x_1 - pz_1 t$$

$$y = y_1 + qz_1 t \tag{2}$$

$$z = z_1 + px_1 t - qy_1 t$$

Differentiating them twice as to the time, regarding p and q as constant, we have

$$D_t^2 x = D_t^2 x_1 - pt D_t^2 z_1 - 2p D_t z_1$$

$$D_t^2 y = D_t^2 y_1 + qt D_t^2 z_1 + 2q D_t z_1 \tag{3}$$

$$D_t^2 z = D_t^2 z_1 + pt D_t^2 x_1 - qt D_t^2 y_1 + 2p D_t x_1 - 2q D_t y_1$$

Regarding P , originally a function of x_1, y_1 , and z_1 , as becoming a function of x, y , and z through the substitution (2) we have

$$\frac{\partial P}{\partial x_1} = \frac{\partial P}{\partial x} + pt \frac{\partial P}{\partial z} \quad \frac{\partial P}{\partial y_1} = \frac{\partial P}{\partial y} - qt \frac{\partial P}{\partial z} \quad \frac{\partial P}{\partial z_1} = \frac{\partial P}{\partial z} - pt \frac{\partial P}{\partial x} + qt \frac{\partial P}{\partial y}$$

Substituting these expressions for $D_t^2 x_1, D_t^2 y_1$, and $D_t^2 z_1$ in (3) and dropping terms of the second order in pt and qt we find

$$D_t^2 x = \frac{\partial P}{\partial x} - 2p D_t z_1$$

$$D_t^2 y = \frac{\partial P}{\partial y} + 2q D_t z_1 \tag{4}$$

$$D_t^2 z = \frac{\partial P}{\partial z} + 2p D_t x_1 - 2q D_t y_1$$

Equations of this form were used by Hill for the same purpose.*

* *Annals of Mathematics*, vol. 1, 1890.

It follows that if we add to P the terms

$$\Delta R = 2p(zD_t x_1 - xD_t z_1) + 2q(yD_t z_1 - zD_t y_1) \quad (5)$$

so that the potential shall become

$$P + \Delta R \quad [\text{Dim.} = ML^{-1} = L^2 T^{-2}]$$

the fundamental differential equations in x , y , and z , will retain the form (1) unchanged, and the coördinates referred to the moving ecliptic will be determined by the general equations

$$D_t^2 x = \frac{\partial P}{\partial x} \quad D_t^2 y = \frac{\partial P}{\partial y} \quad D_t^2 z = \frac{\partial P}{\partial z} \quad (6)$$

In ΔR the symbols x_1 , y_1 , and z_1 have the same meanings as x , y , and z , but they are to be regarded as constant when ΔR is differentiated as to the lunar elements.

§ 5. *Preliminary form of the potential function.*

We put Ω for the part of the potential P due to the action of the Sun. This part is developed in a series proceeding according to the powers of r/r' in the well-known form

$$\Omega = \frac{m' r^2}{2r'^3} (3S^2 - 1) + \frac{m' r^3}{2r'^4} \cdot \frac{m_2 - m_3}{\mu} (5S^3 - 3S) + \dots \quad (7)$$

where S , the cosine of the angle between the radii vectores of the Moon and Sun from the point G, is determined by the equation

$$rr'S = xx' + yy' + zz'$$

When we assign to x' , y' , z' , and r' their elliptic values, we have what may be called the Delaunay part of the potential. We put

Ω_0 , the Delaunay part of Ω .

Ω_p , the increment of Ω_0 produced by the action of the planets on the Earth.

The part R of P , due to the direct action of the planet in changing the coördinates of the Earth relative to the Moon, may be formed from Ω in (7) by replacing

$$m', r', x', y', \text{ and } z'$$

by

$$m_4, \Delta, X, Y, \text{ and } Z$$

where m_4 is the mass of the planet, and Δ , X , Y , and Z its distance and coördinates relative to the point G. Putting R for this part we have for its principal term

$$R = \frac{m_4 r^2}{2\Delta^3} (3S'^2 - 1) \quad (7a)$$

where S' is determined by the equation

$$r\Delta S' = (x' + x_4)x + (y' + y_4)y + (z' + z_4)z$$

$x_4, y_4,$ and z_4 being the heliocentric coördinates of the planet.

We have thus separated the potential of all the actions changing the coördinates of the Moon relative to the Earth into the following five parts.

A. The part generated by the mutual action of the Earth and Moon, $P_0 = \mu/r$, which taken alone would give rise to an undisturbed elliptic motion of the Moon around the Earth.

B. The part Ω_0 generated by the action of the Sun, assuming the point G to move in an elliptic orbit.

C. The part Ω_p , the increment of Ω_0 due to the action of the planets on the point G .

D. The part R due to the direct action of the planet. Developed in the same way as the highest term of Ω the principal term of this part is formed from Ω by replacing $m', x', y',$ and z' by the mass and G-coördinates of the planet. The value of its principal term is given in (7a).

E. The part ΔR arising from the reference of the coördinates to the moving ecliptic.

The complete value of P thus becomes

$$P = P_0 + \Omega_0 + \Omega_p + R + \Delta R \tag{8}$$

and we are to consider this expression as replacing P in the equations (6).

§ 6. *Reduction of the terms of the potential function for the indirect action.*

By substituting for S in (7) its value, the first and principal term of Ω becomes a linear function of the six squares and products of the lunar coördinates $x, y,$ and z , which we may write

$$\Omega = T_1x^2 + T_2y^2 + T_3z^2 + 2T_4xy + 2T_5xz + 2T_6yz \tag{9}$$

Moreover, since we form the part Ω_p of the potential by assigning increments to T , and the part R by making T a function of the elements of the planet, it follows that both of these parts as well as Ω are of this same form.

For the first and principal term of Ω_0 in which the higher powers of r/r' are dropped we have

$$\begin{aligned} T_1 &= \frac{m'}{r'^3} \left(\frac{3}{2} \frac{x'^2}{r'^2} - \frac{1}{2} \right) & T_4 &= \frac{3}{2} \frac{m'}{r'^3} \cdot \frac{x'y'}{r'^2} \\ T_2 &= \frac{m'}{r'^3} \left(\frac{3}{2} \frac{y'^2}{r'^2} - \frac{1}{2} \right) & T_5 &= \frac{3}{2} \frac{m'}{r'^3} \cdot \frac{x'z'}{r'^2} \\ T_3 &= \frac{m'}{r'^3} \left(\frac{3}{2} \frac{z'^2}{r'^2} - \frac{1}{2} \right) & T_6 &= \frac{3}{2} \frac{m'}{r'^3} \cdot \frac{y'z'}{r'^2} \end{aligned} \quad [\text{Dim.} = ML^{-1}] \tag{10}$$

The study of the second term, which it may be advisable to examine for sensible results, is postponed, and Ω is taken as equal to its principal part. The value of Ω_p is then found by adding to the preceding values of T_i their increments produced by the action of the planets upon the coördinates x' , y' , and z' of the Sun. If we put

$$v', \text{ the longitude of the Sun}$$

and take the moving ecliptic as the plane of reference, we may regard z' , the periodic perturbations of the latitude, as infinitesimal and write

$$x' = r' \cos v' \quad y' = r' \sin v' \quad z' = r' \sin \beta'$$

where β' is the Sun's latitude, a minute purely periodic quantity.

Substituting these values in (10), the expressions for the coefficients T become

$$\begin{aligned} T_1 &= \frac{m'}{r'^3} \left(\frac{1}{2} + \frac{3}{4} \cos 2v' \right) & T_2 &= \frac{m'}{r'^3} \left(\frac{1}{2} - \frac{3}{4} \cos 2v' \right) & T_3 &= -\frac{m'}{2r'^3} \\ T_4 &= \frac{3}{4} \frac{m'}{r'^3} \sin 2v' & T_5 &= \frac{3}{2} \frac{m' \sin \beta' \cos v'}{r'^3} & T_6 &= \frac{3}{2} \frac{m' \sin \beta' \sin v'}{r'^3} \end{aligned} \quad (10a)$$

If we assign to these quantities their elliptic values, (7) will become Ω_0 for which the integration is assumed in advance. We have now to assign to v' and r' the increments $\delta v'$ and $r' \delta \rho'$, ρ' being the Napierian logarithm of r' . The resulting increments of the coefficients are

$$\begin{aligned} \delta T_1 &= \frac{3m'}{4r'^3} \{ -2 \sin 2v' \delta v' - 3 \cos 2v' \delta \rho' - \delta \rho' \} & \delta T_2 &= \frac{3m'}{4r'^3} \{ 2 \sin 2v' \delta v' + 3 \cos 2v' \delta \rho' - \delta \rho' \} \\ \delta T_3 &= \frac{3m'}{2r'^3} \delta \rho' & \delta T_4 &= \frac{3m'}{4r'^3} \{ 2 \cos 2v' \delta v' - 3 \sin 2v' \delta \rho' \} \end{aligned} \quad (11)$$

The values of δT_5 and δT_6 will be the original values (9) of T_5 and T_6 as they are due wholly to the action of the planet. With them the expression for Ω_p derived from (9) becomes

$$\Omega_p = \delta T_1 x^2 + \delta T_2 y^2 + \delta T_3 z^2 + 2\delta T_4 xy + 2T_5 xz + 2T_6 yz \quad (12)$$

§ 7. Reduction of R , the potential of direct action.

By substituting for S' in the principal term (7a) of R its expression in terms of the G-coördinates of the planet we shall have

$$R = \frac{3}{2} m_4 R_2 \quad (13)$$

where

$$R_2 = Ax^2 + By^2 + Cz^2 + 2Dxy + 2Exz + 2Fyz \quad [\text{Dim.} = L^{-1}]$$

the values of the coefficients being

$$\begin{aligned}
 A &= \frac{(x' + x_4)^2}{\Delta^5} - \frac{1}{3} \frac{1}{\Delta^3} & D &= \frac{(x' + x_4)(y' + y_4)}{\Delta^5} \\
 B &= \frac{(y' + y_4)^2}{\Delta^5} - \frac{1}{3} \frac{1}{\Delta^3} & E &= \frac{(x' + x_4)(z' + z_4)}{\Delta^5} \quad [\text{Dim.} = L^{-2}] \quad (14) \\
 C &= \frac{(z' + z_4)^2}{\Delta^5} - \frac{1}{3} \frac{1}{\Delta^3} & F &= \frac{(y' + y_4)(z' + z_4)}{\Delta^5}
 \end{aligned}$$

It should be noted that these coefficients require the factor $\frac{2}{3}$ to make them directly comparable with T_1, T_2 , etc., in (10).

§ 8. *Complete form of the fundamental equations.*

Comparing the expressions (12) to (14) we see that Ω_p and R are of the same form, and that the principal terms of each are products of two factors, of which one depends solely on the heliocentric coördinates of the Sun and planet, and the other is a square or product of the coördinates of the Moon. Moreover, if we put, for brevity,

$$P_1 = \Omega_p + R + \Delta R \quad (15)$$

the fundamental differential equations may be written

$$D_t^2 x = \frac{\partial(P_0 + \Omega_0)}{\partial x} + \frac{\partial P_1}{\partial x} \quad D_t^2 y = \frac{\partial(P_0 + \Omega_0)}{\partial y} + \frac{\partial P_1}{\partial y} \quad D_t^2 z = \frac{\partial(P_0 + \Omega_0)}{\partial z} + \frac{\partial P_1}{\partial z} \quad (16)$$

where x, y , and z are coördinates referred to the moving ecliptic as the fundamental plane.

We shall now consider these differential equations as solved for the case when P_1 is dropped from the second members. The problem will then be that of the solution when P_1 is included; and this problem will be attacked by the Lagrangian method of variation of elements.

CHAPTER II.

DEVELOPMENT AND INTEGRATION OF THE DIFFERENTIAL EQUATIONS FOR THE VARIATION OF THE ELEMENTS.

§ 9. The problem being to integrate equations (16), we shall regard as known quantities the coördinates x', y', z' of the Sun, which enter implicitly into the equations, as well as those of the planets relative to the Sun. The problem then is to express the values of $x, y,$ and z in terms of the fundamental constants implicitly contained in the differential equations, and six other arbitrary constants which we regard as elements of the Moon's motion.

The solution of the equations is separated into two parts by applying the Lagrangian method of the variation of elements. We have first the Delaunay solution, in which P_1 is dropped. This solution gives the orbit of the Moon around the Earth under the influence of the Sun's and Earth's attraction alone. From it we are to pass, by the method of variation of elements, to a solution when P_1 is taken account of.

We accept the results of Delaunay, as found in his work, as forming the basis of the first solution, the results needing only certain modifications in the terms depending on the Sun's parallax, arising from the fact that he did not take into account the mass of the Moon, and certain reductions, to reduce them to the required form. This being done we have values of the Moon's coördinates satisfying the differential equations in the case $P = \mu/r + \Omega_0$ and expressed as functions of six arbitrary constants

$$a, e, \gamma, l_0, \pi_0, \theta_0$$

and of the time t . The latter enters only through the quantities $l, \pi,$ and $\theta,$ named and defined thus

$$\text{Mean longitude: } l = l_0 + nt \quad \text{Long. of perigee: } \pi = \pi_0 + \pi_1 t \quad \text{Long. of node: } \theta = \theta_0 + \theta_1 t \quad (17)$$

where $n, \pi_1,$ and θ_1 are functions of $a, e,$ and $\gamma.$

I use the quantities $l, \pi,$ and θ instead of Delaunay's $l, g,$ and $h,$ which are the mean anomaly, the angle node to perigee, and the longitude of the node. The expressions for the symbols used here in terms of those used by Delaunay are therefore

$$l \equiv \text{Delaunay's } h + g + l \quad \pi \equiv \text{Delaunay's } h + g \quad \theta \equiv \text{Delaunay's } h \quad (18)$$

The fundamental idea of the Lagrangian method, which we propose to apply to the present problem, is that the six arbitrary elements are to become such functions of the time that the solution which satisfies (16) when $P_1 = 0$ shall still satisfy it when the variable values of the elements are substituted for the constant values in the expressions for the coördinates. The derivatives of the elements as to the time may be formed by known processes, but the details of these processes are unnecessary, because Delaunay gives their results in a form most convenient for our purpose.

§ 10. *Canonical form of the differential equations.*

We see from (5), (12), (13), and (15) that P_1 is a function of given quantities and of the Moon's coördinates. By substituting for the latter their expressions in terms of the six arbitrary constants of the first integration, P_1 becomes a function of $a, e, \gamma, l, \pi,$ and θ . The differential variations of the elements are then expressed in the most condensed form by replacing $a, e,$ and γ by three other quantities $c_1, c_2,$ and $c_3,$ functions of $a, e, \gamma,$ so chosen that the differential equations to be solved shall be

$$\begin{aligned} D_t c_1 &= \frac{\partial P_1}{\partial l} & D_t l_0 &= -\frac{\partial P_1}{\partial c_1} \\ D_t c_2 &= \frac{\partial P_1}{\partial \pi} & D_t \pi_0 &= -\frac{\partial P_1}{\partial c_2} \\ D_t c_3 &= \frac{\partial P_1}{\partial \theta} & D_t \theta_0 &= -\frac{\partial P_1}{\partial c_3} \end{aligned} \quad [\text{Dim.} = ML^{-1}] \quad (19)$$

The variable elements $c_1, c_2,$ and c_3 are functions of Delaunay's L, G, H .

$$\begin{aligned} c_1 &= L & c_2 &= G - L & c_3 &= H - G \\ [\text{Dim.} = L^{\frac{1}{2}} M^{\frac{1}{2}} = L^{\frac{1}{2}} T^{-1}] & & & & & \end{aligned} \quad (20)$$

§ 11. *Transformation of the canonical elements.*

The canonical elements $c_1, c_2,$ and c_3 can not be used explicitly in the processes of solution. We have therefore to express them in terms of $a, e,$ and γ . The values of $L, G,$ and H are not given by Delaunay in terms of the final $a, e,$ and $\gamma,$ but of preliminary ones from which the required expressions are to be derived as follows:

1. In Vol. II, pp. 235-236, Delaunay gives the expressions for $L, G,$ and H in terms of the $a, e,$ and γ which resulted immediately from his processes of integration.

2. On p. 800 he gives the transformation of these $a, e, \gamma,$ into the final values of these quantities which appear in the expression for the Moon's coördinates, which are those we are to use.

To find from these data the expressions for the derivatives of L, G, H in terms of the final a, e, γ , I shall write a, e, g, n , for the quantities a, e, γ, n , as found on pp. 235-236 of Delaunay, Vol. II, and shall also put

$$m = \frac{n'}{n}$$

The forms which we have to use are:

$$L, G, H = f(a, e, g, m) \quad a, e, g = f(a, e, \gamma, m) \quad (21)$$

Noticing that m is a function of a and m of a , we shall then have

$$\frac{\partial L}{\partial a} = \left(\frac{\partial L}{\partial a} + \frac{\partial L}{\partial m} \frac{\partial m}{\partial a} \right) \frac{\partial a}{\partial a} + \frac{\partial L}{\partial e} \frac{\partial e}{\partial a} + \frac{\partial L}{\partial g} \frac{\partial g}{\partial a} \quad (22)$$

with similar forms for G and H .

§ 12. *Form of the partial derivatives.* Two points in the use of the partial derivatives are these:

α . In taking the partial derivatives I use the logarithm of a and of a instead of these quantities as the variables with respect to which derivatives are to be formed. Homogeneity in the equations is thus secured, the variables being all pure numbers, or quantities of dimensions 0. We put

$$\alpha = \log a \quad \text{whence} \quad a = e^\alpha$$

β . The quantities n and n are defined as functions of a and of a respectively by the equations

$$a^3 n^2 = a^3 n^2 = \mu$$

It follows that if we have an expression M developed in powers of m or m ,

$$M = a^i (M_0 + M_1 m + M_2 m^2 + \dots)$$

we shall have

$$\frac{\partial M}{\partial \alpha} = a^i (i M_0 + (i + \frac{3}{2}) M_1 m + (i + \frac{6}{2}) M_2 m^2 + \dots) \quad (23)$$

§ 13. *Numerical values of the fundamental quantities.*

Instead of effecting the preceding transformations analytically, to put the equations (21) into numbers, we use the numerical values of e, γ , and m given by Delaunay in his Vol. II, pp. 801-802, namely

$$e = .054 \ 8993 \quad \gamma = .044 \ 8866 \quad m = .074 \ 8013 \quad (24)$$

We then find from his expressions on p. 800

$$\begin{aligned} a &= 0.996\ 493a = [9.998\ 474]a \\ an &= 1.001\ 758an = [0.000\ 763]an \\ a^2n &= 0.998\ 245a^2n = [9.999\ 237]a^2n \\ m &= 0.994\ 743m = [9.997\ 711]m = 0.074\ 4082 \\ e &= 0.054\ 867 \qquad g = 0.044\ 993 \end{aligned}$$

We also find, from these numbers, the following values of the required partial derivatives for the numerical transformation

$$\begin{aligned} \frac{\partial a}{\partial \alpha} &= 0.986\ 691a & \frac{\partial e}{\partial \alpha} &= -0.007\ 37e = -0.000\ 404 & \frac{\partial g}{\partial \alpha} &= +0.006\ 85\gamma = 0.000\ 308 \\ \frac{\partial a}{\partial e} &= -0.001\ 375a & \frac{\partial e}{\partial e} &= +0.999\ 61 & \frac{\partial g}{\partial e} &= +0.000\ 202 \\ \frac{\partial a}{\partial \gamma} &= +0.001\ 353a & \frac{\partial e}{\partial \gamma} &= -0.001\ 22e = -0.000\ 067 & \frac{\partial g}{\partial \gamma} &= +1.002\ 324 \end{aligned}$$

Then, from Delaunay, II, p. 236, we find

$$\begin{aligned} L &= 1.000\ 197a^2n & G &= 0.998\ 586a^2n & H &= 0.994\ 549a^2n \\ a \frac{\partial L}{\partial a} &= 0.500\ 158a^2n & a \frac{\partial G}{\partial a} &= 0.499\ 697a^2n & a \frac{\partial H}{\partial a} &= 0.497\ 696a^2n \\ \frac{\partial L}{\partial e} &= -0.000\ 088a^2n & \frac{\partial G}{\partial e} &= -0.052\ 410a^2n & \frac{\partial H}{\partial e} &= -0.052\ 185a^2n \\ \frac{\partial L}{\partial g} &= -0.000\ 007a^2n & \frac{\partial G}{\partial g} &= -0.000\ 035a^2n & \frac{\partial H}{\partial g} &= -0.179\ 474a^2n \end{aligned}$$

§ 14. *Formation of the transformed differential equations.*

Let us now return to the equations (19), in which we have to replace c_1 , c_2 , and c_3 by a , e , and γ . We have, for any c ,

$$\frac{dc}{dt} = \frac{dc}{d\alpha} \frac{d\alpha}{dt} + \frac{dc}{de} \frac{de}{dt} + \frac{dc}{dg} \frac{dg}{dt}$$

and

$$\frac{dc}{d\alpha} = \frac{dc}{da} \frac{da}{d\alpha} + \frac{dc}{de} \frac{de}{d\alpha} + \frac{dc}{dg} \frac{dg}{d\alpha}$$

In the case of c_1 we have from (20)

$$\frac{dc_1}{da} = \frac{dL}{da}$$

so that the numerical expressions need not be repeated. For the derivatives of c_2 and c_3 we find

$$\begin{aligned} a \frac{\partial c_2}{\partial a} &= -0.000461a^2n & \frac{\partial c_2}{\partial e} &= -0.052322a^2n & \frac{\partial c_2}{\partial g} &= -0.000028a^2n \\ a \frac{\partial c_3}{\partial a} &= -0.002001a^2n & \frac{\partial c_3}{\partial e} &= +0.000225a^2n & \frac{\partial c_3}{\partial g} &= -0.179436a^2n \end{aligned}$$

By substitution in the form (22) we now find

$$\begin{aligned} \frac{\partial c_1}{\partial a} &= 0.494369a^2n & \frac{\partial c_1}{\partial e} &= -0.000777a^2n & \frac{\partial c_1}{\partial \gamma} &= 0.000671a^2n \\ \frac{\partial c_2}{\partial a} &= -0.000435a^2n & \frac{\partial c_2}{\partial e} &= -0.052209a^2n & \frac{\partial c_2}{\partial \gamma} &= -0.000025a^2n \\ \frac{\partial c_3}{\partial a} &= -0.002033a^2n & \frac{\partial c_3}{\partial e} &= 0.000191a^2n & \frac{\partial c_3}{\partial \gamma} &= -0.179538a^2n \end{aligned} \quad (25)$$

We now have the data for transforming the equations (19), p. 14, so as to express the differential variations of α , e , and γ instead of c_1 , c_2 , and c_3 , and to express those of l_0 , π_0 , and θ_0 in terms of the partial derivatives of R as to α , e , and γ . For this purpose we need the nine partial derivatives of α , e , and γ as to c_1 , c_2 , and c_3 . We shall express these nine derivatives by means of the nine numerical factors

$$\alpha_i, e_i, \gamma_i, \dots (i = 1 : 2 : 3)$$

defined by the equations

$$\alpha_i = a^2n \frac{\partial \alpha}{\partial c_i} \quad e_i = a^2n \frac{\partial e}{\partial c_i} \quad \gamma_i = a^2n \frac{\partial \gamma}{\partial c_i}$$

The numerical values of these coefficients are most expeditiously found in the following way. Multiplying the first three equations (19) in order by the respective factors

$$\frac{\partial \alpha}{\partial c_1}, \quad \frac{\partial \alpha}{\partial c_2}, \quad \text{and} \quad \frac{\partial \alpha}{\partial c_3}$$

we have

$$D_i \alpha = \frac{\partial \alpha}{\partial c_1} \frac{\partial P_1}{\partial l} + \frac{\partial \alpha}{\partial c_2} \frac{\partial P_1}{\partial \pi} + \frac{\partial \alpha}{\partial c_3} \frac{\partial P_1}{\partial \theta}$$

with similar equations in $D_i e$ and $D_i \gamma$. From the same three equations we have

$$\frac{\partial c_1}{\partial \alpha} D_i \alpha + \frac{\partial c_1}{\partial e} D_i e + \frac{\partial c_1}{\partial \gamma} D_i \gamma = \frac{\partial P_1}{\partial l}$$

$$\frac{\partial c_2}{\partial \alpha} D_i \alpha + \frac{\partial c_2}{\partial e} D_i e + \frac{\partial c_2}{\partial \gamma} D_i \gamma = \frac{\partial P_1}{\partial \pi}$$

$$\frac{\partial c_3}{\partial \alpha} D_i \alpha + \frac{\partial c_3}{\partial e} D_i e + \frac{\partial c_3}{\partial \gamma} D_i \gamma = \frac{\partial P_1}{\partial \theta}$$

It follows that if we solve these three equations for $D_i \alpha$, $D_i e$, and $D_i \gamma$ the nine partial derivatives required will be the coefficients of the second members in the

solution. Replacing the coefficients of the unknowns by their numerical values (25), we may reduce the solution to that of three numerical equations

$$\begin{aligned} 0.494369X - .000777Y + .000671Z &= P \\ - .000435X - .052209Y - .000025Z &= Q \\ - .002033X + .000191Y - .179538Z &= R \end{aligned}$$

The solution of these equations so as to express X , Y , and Z as linear functions of P , Q , and R gives the following values of the factors which we seek. Along with these values is given for comparison the values found in *Action of Planets*, p. 196, where the numbers are the coefficients of $\frac{an}{m_2 m_3}$. The two determinations are completely independent, in that the earlier one is derived from the analytic expressions for the coördinates of the Moon, while these last have been obtained from Delaunay's expressions of the canonical elements $L G H$ in terms of a, e, γ .

| | | |
|-----------------------|------------------------|----------|
| $\alpha_1 = + 2.0228$ | Former value: + 2.0225 | |
| $\alpha_2 = - 0.0301$ | | - 0.0293 |
| $\alpha_3 = + 0.0075$ | | + 0.0075 |
| $e_1 = - 0.0168$ | | - 0.0169 |
| $e_2 = - 19.1534$ | | - 19.151 |
| $e_3 = + 0.0026$ | | + 0.0017 |
| $\gamma_1 = - 0.0229$ | | - 0.0233 |
| $\gamma_2 = - 0.0200$ | | - 0.0216 |
| $\gamma_3 = - 5.5700$ | | - 5.5704 |

(26)

The fundamental differential equations for the variations of the elements now become

$$\begin{aligned} a^2 n D_t \alpha &= \alpha_1 \frac{\partial P_1}{\partial l} + \alpha_2 \frac{\partial P_1}{\partial \pi} + \alpha_3 \frac{\partial P_1}{\partial \theta} \\ a^2 n D_t e &= e_1 \frac{\partial P_1}{\partial l} + e_2 \frac{\partial P_1}{\partial \pi} + e_3 \frac{\partial P_1}{\partial \theta} \\ a^2 n D_t \gamma &= \gamma_1 \frac{\partial P_1}{\partial l} + \gamma_2 \frac{\partial P_1}{\partial \pi} + \gamma_3 \frac{\partial P_1}{\partial \theta} \\ a^2 n D_t l_0 &= -\alpha_1 \frac{\partial P_1}{\partial \alpha} - e_1 \frac{\partial P_1}{\partial e} - \gamma_1 \frac{\partial P_1}{\partial \gamma} \\ a^2 n D_t \pi_0 &= -\alpha_2 \frac{\partial P_1}{\partial \alpha} - e_2 \frac{\partial P_1}{\partial e} - \gamma_2 \frac{\partial P_1}{\partial \gamma} \\ a^2 n D_t \theta_0 &= -\alpha_3 \frac{\partial P_1}{\partial \alpha} - e_3 \frac{\partial P_1}{\partial e} - \gamma_3 \frac{\partial P_1}{\partial \gamma} \end{aligned}$$

[Dim. = ML^{-1}]

(27)

In order that we may, so far as possible, handle only pure numbers, with specifications of the units as concrete quantities, we shall substitute nt , the total motion of the Moon in mean longitude, and therefore a pure number, as the independent variable. The first numbers will then take the form $a^2 n^2 D_n a$, etc.

Since

$$a^2 n^2 = \frac{\mu}{a}$$

the equations will now give

$$D_n \alpha = \frac{a}{\mu} \left(\alpha_1 \frac{\partial P_1}{\partial l} + \alpha_2 \frac{\partial P_1}{\partial \pi} + \alpha_3 \frac{\partial P_1}{\partial \theta} \right) \quad (28)$$

[Dim. = 0]

with five others formed in the same way from (27) which need not be written.

§ 15. *Elimination of t from the partial derivatives of l , π , and θ .*

An important remark at this point is that since P_1 is a function of l , π , and θ , the three quantities a , e , and γ enter into P_1 not only explicitly but implicitly through n , π , and θ , so that the complete differential variations of these functions are

$$\frac{dl}{dt} = \frac{dl_0}{dt} + n + t \frac{dn}{dt} \quad \frac{d\pi}{dt} = \frac{d\pi_0}{dt} + \pi_1 + t \frac{d\pi_1}{dt} \quad \frac{d\theta}{dt} = \frac{d\theta_0}{dt} + \theta_1 + t \frac{d\theta_1}{dt}$$

P_1 being a function of the six quantities

$$a, e, \gamma, l_0 + nt, \pi_0 + \pi_1 t, \theta_0 + \theta_1 t$$

its complete derivatives as to a , e , and γ are

$$\frac{\partial P_1}{\partial a} = \left(\frac{\partial P_1}{\partial a} \right) + t \left(\frac{\partial P_1}{\partial l} \frac{\partial n}{\partial a} + \frac{\partial P_1}{\partial \pi} \frac{\partial \pi_1}{\partial a} + \frac{\partial P_1}{\partial \theta} \frac{\partial \theta_1}{\partial a} \right)$$

with similar expressions for $\partial P_1 / \partial e$ and $\partial P_1 / \partial \gamma$. Thus we have for any canonical element c

$$\frac{\partial P_1}{\partial c} = \left(\frac{\partial P_1}{\partial c} \right) + t \left(\frac{\partial P_1}{\partial l} \frac{\partial n}{\partial c} + \frac{\partial P_1}{\partial \pi} \frac{\partial \pi_1}{\partial c} + \frac{\partial P_1}{\partial \theta} \frac{\partial \theta_1}{\partial c} \right)$$

The complete derivatives of l , π , and θ are therefore

$$\begin{aligned}\frac{dl}{dt} &= \frac{dl_0}{dt} + n + t \left(\frac{dn}{dt} - \frac{\partial P_1}{\partial l} \frac{\partial n}{\partial c_1} - \frac{\partial P_1}{\partial \pi} \frac{\partial \pi_1}{\partial c_1} - \frac{\partial P_1}{\partial \theta} \frac{\partial \theta_1}{\partial c_1} \right) \\ \frac{d\pi}{dt} &= \frac{d\pi_0}{dt} + \pi_1 + t \left(\frac{d\pi_1}{dt} - \frac{\partial P_1}{\partial l} \frac{\partial n}{\partial c_2} - \frac{\partial P_1}{\partial \pi} \frac{\partial \pi_1}{\partial c_2} - \frac{\partial P_1}{\partial \theta} \frac{\partial \theta_1}{\partial c_2} \right) \\ \frac{d\theta}{dt} &= \frac{d\theta_0}{dt} + \theta_1 + t \left(\frac{d\theta_1}{dt} - \frac{\partial P_1}{\partial l} \frac{\partial n}{\partial c_3} - \frac{\partial P_1}{\partial \pi} \frac{\partial \pi_1}{\partial c_3} - \frac{\partial P_1}{\partial \theta} \frac{\partial \theta_1}{\partial c_3} \right)\end{aligned}$$

It is a fundamental theorem of the development of the planetary coördinates in periodic series that the terms of these equations containing t as a factor all vanish.* The values of l , π , and θ are therefore

$$l = l_0 + \int n dt \qquad \pi = \pi_0 + \int \pi_1 dt \qquad \theta = \theta_0 + \int \theta_1 dt \qquad (29)$$

* A demonstration of this theorem in the most general case is found in the author's paper *On the General Integrals of Planetary Motion: Smithsonian Contributions to Knowledge*, 1874.

CHAPTER III.

DEFINITIVE FORM OF THE DIFFERENTIAL VARIATIONS OF THE ELEMENTS.

§ 16. The differential equations (27) in the form (28) are the fundamental ones of our problem, the integration of which is to be effected. This need be done only to terms of the first order as to the disturbing function. This amounts to saying that we regard the second members of the equation as known functions of the time, and that the required integration is to be performed by simple quadrature.

We begin by studying the general form of the function P_1 . Besides ΔR , this function consists of two parts, one, R , arising from the direct action shown in § 7, and the other Ω_p , arising from the indirect action. We have reduced both these parts to the general form

$$Ax^2 + By^2 + Cz^2 + 2Dxy + 2Exz + 2Fyz$$

The coefficients, A, B , etc., are functions of the heliocentric coördinates of two points: the centre of gravity G of the Earth and Moon, and that of the planet. They are, therefore, regarded as independent of the elements of the Moon's orbit. The variables x^2, y^2 , etc., being functions of the geocentric coördinates of the Moon, are independent of the position of the planet, and contain, besides the six lunar elements proper, the major axis and eccentricity of the Earth's orbit around the Sun. The arguments on which the coefficients A, B , etc., depend are g_1 and g' . The coördinates x^2, y^2 , etc., depend on the four arguments l, π, θ , and g' . It follows that the terms of P_1 depend on the five arguments

$$l, \pi, \theta, g', g_1$$

Although the two actions, the direct and indirect, admit of being treated together by combining the corresponding coefficients of x^2, y^2 , etc., yet the coefficients are so different in their form and origin that it will be better to treat them separately.

§ 17. *Reduction of the equations for the direct action.*

We begin with the development of R , as given by (13) and (14). Since

$$x^2, y^2, \text{ etc., each} = \text{a pure number} \times a^2$$

$$A, B, C, \text{ etc., each} = \text{a pure number} \div a'^3$$

it follows that R may be developed in the form

$$R = \frac{3}{2} m_4 \frac{a^2}{a'^3} H \quad (30)$$

H being a pure number.

When the fundamental equations are taken in the form (28), and P_1 is replaced by R expressed in terms of H , the second members will all take the common constant numerical factor

$$\frac{3}{2} \frac{m_4}{\mu} \frac{a^3}{a'^3}$$

This factor may be simplified by the fundamental relations

$$a^3 n^2 = \mu \quad a'^3 n'^2 = m' + \mu$$

where μ and m' are the respective masses of Earth + Moon and of the Sun.

Owing to the minuteness of μ relative to m' (1:330000 +) we may drop it from the quotient, thus obtaining

$$\frac{m'}{\mu} \frac{a^3}{a'^3} = \frac{n'^2}{n^2} = m^2$$

The factor thus reduces to the pure number

$$\frac{3}{2} \frac{m_4}{m'} m^2$$

The ratio $m_4 : m'$ is what is commonly taken as the numerical expression of the mass of the planet. We shall write

$$M = \frac{3}{2} \frac{m_4}{m'} m^2 = 0.008 \ 392 \ 86 \frac{m_4}{m'}$$

The numerical values of M for the four planets whose action is to be determined are as follows:

| | $\frac{m'}{m_4}$ | M |
|---------|------------------|--------------|
| Venus | 408 000 | 0'' .004 242 |
| Mars | 3 093 500 | 0 .000 560 |
| Jupiter | 1047.35 | 1 .653 |
| Saturn | 3500 | 0 .4947 |

We have next to consider H and its derivatives. As this quantity has been above introduced we have

$$H = a'^3 A \frac{x^2}{a^2} + a'^3 B \frac{y^2}{a^2} + a'^3 C \frac{z^2}{a} + 2a'^3 D \frac{xy}{a} \quad (31)$$

The terms in E and F are omitted here, owing to their minuteness.

We have now to deal with two sets of factors:

1. The planetary factors, $a'^3 A$, $a'^3 B$, etc.
2. The lunar factors

$$\frac{x^2}{a^2}, \frac{y^2}{a^2}, \frac{z^2}{a^2}, \frac{2xy}{a^2}, \text{ etc.}$$

for which we use

$$\xi^2, \eta^2, \zeta^2, 2\xi\eta, \text{ respectively}$$

§ 18. *Notation of the Planetary Factors.* The development of these requires numerical processes which, owing to their length and their distinctive character, are given in Part II. We shall therefore assume this development to be effected, referring to Part II for the methods and numerical results. Considering the latter in their general form, we remark that these coefficients being of dimensions L^{-3} , if we compute their values, taking the Earth's mean distance as unity, the numbers obtained for the several coefficients A, B , etc., will readily be the values of $a'^3 A, a'^3 B$, etc. We shall therefore put

$$\begin{aligned} a'^3 A &= \Sigma (A_e \cos N_4 + A_s \sin N_4) \\ a'^3 B &= \Sigma (B_e \cos N_4 + B_s \sin N_4) \\ a'^3 C &= \Sigma (C_e \cos N_4 + C_s \sin N_4) \\ &\dots \dots \dots \end{aligned} \tag{33}$$

where each argument is of the general form

$$N_4 = kl_4 + k'g'$$

l_4 being the mean longitude of the planet, measured from a point which we shall take as that corresponding to the earth's perihelion.

§ 19. *Notation of the lunar factors.* We have shown in *Action*, Chapter II, how, from Delaunay's results, the squares and products of the Moon's coördinates may be developed in the general form

$$\begin{aligned} \frac{x^2}{a^2} = \xi^2 &= \Sigma \kappa_1 \cos N & \frac{y^2}{a^2} = \eta^2 &= \Sigma \kappa_2 \cos N & \frac{z^2}{a^2} = \zeta^2 &= \Sigma \kappa_3 \cos N \\ 2\xi\eta &= \Sigma \kappa_4 \sin N & 2\xi\zeta &= \Sigma \kappa_5 \sin N & 2\eta\zeta &= \Sigma \kappa_6 \cos N \end{aligned} \tag{34}$$

Here the κ are functions of $a, e, \gamma, a',$ and e' , and the arguments N may be expressed in the general form

$$N = il + i'\pi + i''\theta + jg'$$

These developments comprise all the quantities necessary to the formation of R and its derivatives.

§ 20. *Numerical form of the fundamental coefficients.* The condition

$$A + B + C = 0$$

enables us to reduce by one the number of terms in H , and at the same time to simplify the computation. We have the identity

$$A\xi^2 + B\eta^2 = \frac{1}{2}(A + B)(\xi^2 + \eta^2) + \frac{1}{2}(A - B)(\xi^2 - \eta^2)$$

Replacing $A + B$ by $-C$ there results

$$A\xi^2 + B\eta^2 + C\xi^2 = \frac{1}{2}(A - B)(\xi^2 - \eta^2) - \frac{1}{2}C(\xi^2 + \eta^2 - 2\xi^2)$$

Putting, for brevity,

$$K = \frac{1}{2}a'^3(A - B) \quad C_1 = a'^3C \quad \rho^2 = \frac{r^2}{a^2} = \xi^2 + \eta^2 + \zeta^2 \quad D_1 = a'^3D$$

which will make K , C_1 , and D_1 pure numbers, we shall have

$$H = K(\xi^2 - \eta^2) - \frac{1}{2}C_1(\rho^2 - 3\xi^2) + 2D_1\xi\eta$$

The planetary factors, K , C_1 , and D_1 are taken as developed in a double trigonometric series from the equations (33), by putting

$$K_c = \frac{1}{2}(A_c - B_c) \quad K_s = \frac{1}{2}(A_s - B_s)$$

We shall then have for H the double trigonometric series

$$\begin{aligned} H = & \Sigma(K_c \cos N_4 + K_s \sin N_4)(\kappa_1 - \kappa_2) \cos N \\ & - \Sigma(\frac{1}{2}C_c \cos N_4 + \frac{1}{2}C_s \sin N_4)(\kappa_1 + \kappa_2 - 2\kappa_3) \cos N \\ & + \Sigma(D_c \cos N_4 + D_s \sin N_4)\kappa_4 \sin N \end{aligned} \quad (35)$$

Introducing, for brevity,

$$p = \frac{1}{2}(\kappa_1 - \kappa_2) \quad q = \frac{1}{2}(\kappa_1 + \kappa_2) - \kappa_3 \quad (36)$$

the terms of the lunar factors will be expressed by

$$(\xi^2 - \eta^2) = 2p \cos N \quad \rho^2 - 3\xi^2 = 2q \cos N \quad 2\xi\eta = \kappa_4 \sin N.$$

Every combination of a planetary argument N_4 with a lunar argument N will give rise to a set of terms in H of the form

$$H = h_c \cos(N + N_4) + h_s \sin(N + N_4) + h'_c \cos(N - N_4) + h'_s \sin(N - N_4) \quad (37)$$

where

$$\begin{aligned} h_c &= K_c p - \frac{1}{2}C_c q - \frac{1}{2}D_c \kappa_4 & h'_c &= -K_c p - \frac{1}{2}C_c q + \frac{1}{2}D_c \kappa_4 \\ h_s &= K_s p - \frac{1}{2}C_s q + \frac{1}{2}D_s \kappa_4 & h'_s &= -K_s p + \frac{1}{2}C_s q + \frac{1}{2}D_s \kappa_4 \end{aligned} \quad (38)$$

The partial derivatives of H as to α , e , and γ are to be found from

$$\begin{aligned} Dh_c &= K_c Dp - \frac{1}{2} C_c Dq - \frac{1}{2} D_c D\kappa_4 \\ \frac{\partial h_c}{\partial e} &= K_c \frac{\partial p}{\partial e} - \frac{1}{2} C_c \frac{\partial q}{\partial e} - \frac{1}{2} D_c \frac{\partial \kappa_4}{\partial e} \\ \frac{\partial h_c}{\partial \gamma} &= K_c \frac{\partial p}{\partial \gamma} - \frac{1}{2} C_c \frac{\partial q}{\partial \gamma} - \frac{1}{2} D_c \frac{\partial \kappa_4}{\partial \gamma} \end{aligned} \quad (39)$$

with three other sets formed by replacing p , q , and κ_4 in (38) by their partial derivatives. These derivatives of h_c , h_s , h'_c , and h'_s being substituted in (37) give the required partial derivatives of H . In forming the derivatives as to l , π , and θ we note that these quantities enter only through the arguments N , in which they have the respective coefficients

$$i; \quad i'; \quad i''$$

Their formation is therefore a simple algebraic process after H is developed.

The elements e and γ also enter R only through H . But α appears both in H , which is a function of m , and in the factor a^2/a'^3 . We therefore have from (30)

$$\frac{\partial R}{\partial \alpha} = \frac{3}{2} m_4 \frac{a^2}{a'^3} \left(2H + \frac{\partial H}{\partial \alpha} \right)$$

For consistency in form and notation we shall put

$$D'H = 2H + \frac{\partial H}{\partial \alpha} \quad (40)$$

It may be remarked that the formation of $D'H$ may be effected by the general operation indicated in (23), by supposing H developed in powers of m and putting

$$M = a^2 H$$

so that

$$i = 2$$

We then have

$$H = M_0 + M_1 m + M_2 m^2 + \dots$$

and

$$\frac{\partial H}{\partial \alpha} = \frac{3}{2} M_1 m + \frac{6}{2} M_2 m^2 + \dots$$

The sum of this $+2H$ gives $D'H$ as above expressed. In forming this sum we need not use the analytic development of $2H$, which is necessary to form $\partial H/\partial \alpha$, but may use the numerical development when it is more accurate.

The partial derivatives of R as to α , e , and γ are

$$\frac{\partial R}{\partial \alpha} = \frac{3}{2} m_4 \frac{a^2}{a'^3} D'H \quad \frac{\partial R}{\partial e} = \frac{3}{2} m_4 \frac{a^2}{a'^3} \frac{\partial H}{\partial e} \quad \frac{\partial R}{\partial \gamma} = \frac{3}{2} m_4 \frac{a^2}{a'^3} \frac{\partial H}{\partial \gamma}$$

§ 21. The fundamental equations in the form (28) for the direct action now become

$$\begin{aligned} D_{nt}\alpha &= M \left(\alpha_1 \frac{\partial H}{\partial l} + \alpha_2 \frac{\partial H}{\partial \pi} + \alpha_3 \frac{\partial H}{\partial \theta} \right) \\ D_{nt}e &= M \left(e_1 \frac{\partial H}{\partial l} + e_2 \frac{\partial H}{\partial \pi} + e_3 \frac{\partial H}{\partial \theta} \right) \end{aligned} \quad (41)$$

$$\begin{aligned} D_{nt}\gamma &= M \left(\gamma_1 \frac{\partial H}{\partial l} + \gamma_2 \frac{\partial H}{\partial \pi} + \gamma_3 \frac{\partial H}{\partial \theta} \right) \\ -D_{nt}l_0 &= M \left(\alpha_1 D' H + e_1 \frac{\partial H}{\partial e} + \gamma_1 \frac{\partial H}{\partial \gamma} \right) \\ -D_{nt}\pi_0 &= M \left(\alpha_2 D' H + e_2 \frac{\partial H}{\partial e} + \gamma_2 \frac{\partial H}{\partial \gamma} \right) \\ -D_{nt}\theta_0 &= M \left(\alpha_3 D' H + e_3 \frac{\partial H}{\partial e} + \gamma_3 \frac{\partial H}{\partial \gamma} \right) \end{aligned} \quad (42)$$

§ 22. We have next to show how the second members of these equations may be most readily reduced to numbers. There being a certain number of lunar arguments N and also a certain number of planetary arguments N_4 , it will conduce to simplicity to carry forward the quantities depending on the argument of each class as far as possible before making the combination.

Each lunar argument being of the general form

$$N = il + i'\pi + i''\theta + jg'$$

and each planetary one of the form

$$N_4 = k'g' + kl_4$$

it follows that by putting G for the general value of the combined final argument, $N \pm N_4$,

$$G = il + i'\pi + i''\theta + (j \pm k')g' \pm kl_4$$

the general form (37) of H may be written

$$H = \Sigma(h_c \cos G + h_s \sin G)$$

The derivatives of H as to l , π , and θ are

$$\frac{\partial H}{\partial l} = \Sigma(-ih_c \sin G + ih_s \cos G) \quad \frac{\partial H}{\partial \pi} = \Sigma(-i'h_c \sin G + i'h_s \cos G)$$

$$\frac{\partial H}{\partial \theta} = \Sigma(-i''h_c \sin G + i''h_s \cos G)$$

Substituting these values in (41) and putting

$$a = i\alpha_1 + i'\alpha_2 + i''\alpha_3 \quad e = ie_1 + i'e_2 + i''e_3 \quad g = i\gamma_1 + i'\gamma_2 + i''\gamma_3 \quad (43)$$

the equations (41) become

$$\begin{aligned} D_{ni}\alpha &= M(ah_c \cos G - ah_c \sin G) \\ D_{ni}e &= M(eh_c \cos G - eh_c \sin G) \\ D_{ni}\gamma &= M(gh_c \cos G - gh_c \sin G) \end{aligned} \quad (44)$$

Every combination of a lunar argument N with a planetary argument N_4 gives rise in each derivative of an element to four terms, which we shall express in the form

$$D_{ni}\alpha = h_{a,c} \cos(N + N_4) + h_{a,s} \sin(N + N_4) + h_{a,s'} \cos(N - N_4) + h_{a,s'} \sin(N - N_4) \quad (45)$$

Replacing h_s and h_c in (44) by their values (38) we have for each combination

$$\begin{aligned} h_{a,c} &= +MK_a p - \frac{1}{2}MC_a q + \frac{1}{2}MD_a \kappa_4 \\ h_{a,c'} &= -MK_a p + \frac{1}{2}MC_a q + \frac{1}{2}MD_a \kappa_4 \\ h_{a,s} &= -MK_c p + \frac{1}{2}MC_c q + \frac{1}{2}MD_c \kappa_4 \end{aligned} \quad (46)$$

$$\begin{aligned} h_{a,s'} &= -MK_c p + \frac{1}{2}MC_c q - \frac{1}{2}MD_c \kappa_4 \\ h_{e,c} &= +MK_e p - \frac{1}{2}MC_e q + \frac{1}{2}MD_e \kappa_4 \\ h_{e,c'} &= -MK_e p + \frac{1}{2}MC_e q + \frac{1}{2}MD_e \kappa_4 \\ h_{e,s} &= -MK_c p + \frac{1}{2}MC_c q + \frac{1}{2}MD_c \kappa_4 \end{aligned} \quad (47)$$

$$\begin{aligned} h_{e,s'} &= -MK_c p + \frac{1}{2}MC_c q - \frac{1}{2}MD_c \kappa_4 \\ h_{\gamma,c} &= +MK_g p - \frac{1}{2}MC_g q + \frac{1}{2}MD_g \kappa_4 \\ h_{\gamma,c'} &= -MK_g p + \frac{1}{2}MC_g q + \frac{1}{2}MD_g \kappa_4 \\ h_{\gamma,s} &= -MK_c p + \frac{1}{2}MC_c q + \frac{1}{2}MD_c \kappa_4 \end{aligned} \quad (48)$$

$$h_{\gamma,s'} = -MK_c p + \frac{1}{2}MC_c q - \frac{1}{2}MD_c \kappa_4$$

§ 23. We now reduce in a similar way the group (42). We have for each argument,

$$D'H = D'h_c \cos G + D'h_s \sin G \quad \frac{\partial H}{\partial c} = \frac{\partial h_c}{\partial c} \cos G + \frac{\partial h_s}{\partial c} \sin G \quad \frac{\partial H}{\partial \gamma} = \frac{\partial h_c}{\partial \gamma} \cos G + \frac{\partial h_s}{\partial \gamma} \sin G$$

Replacing h_c and h_s by their values (38) and substituting the resulting partial derivatives in (42) we have results which we may write in the form

$$\begin{aligned} -D_{ni}l_0 &= h_{l,c} \cos(N + N_4) + h_{l,s} \sin(N + N_4) + h_{l,c'} \cos(N - N_4) + h_{l,s'} \sin(N - N_4) \\ -D_{ni}\pi_0 &= h_{\pi,c} \cos(N + N_4) + h_{\pi,s} \sin(N + N_4) + h_{\pi,c'} \cos(N - N_4) + h_{\pi,s'} \sin(N - N_4) \\ -D_{ni}\theta_0 &= h_{\theta,c} \cos(N + N_4) + h_{\theta,s} \sin(N + N_4) + h_{\theta,c'} \cos(N - N_4) + h_{\theta,s'} \sin(N - N_4) \end{aligned} \quad (49)$$

where the values of the coefficients are found by the following computation. For each lunar argument we form

$$\begin{aligned}
 L' &= \alpha_1 D' p + e_1 \frac{\partial p}{\partial e} + \gamma_1 \frac{\partial p}{\partial \gamma} & L'' &= \alpha_1 D' q + e_1 \frac{\partial q}{\partial e} + \gamma_1 \frac{\partial q}{\partial \gamma} & L_4 &= \alpha_1 D' \kappa_4 + e_1 \frac{\partial \kappa_4}{\partial e} + \gamma_1 \frac{\partial \kappa_4}{\partial \gamma} \\
 P' &= \alpha_2 D' p + e_2 \frac{\partial p}{\partial e} + \gamma_2 \frac{\partial p}{\partial \gamma} & P'' &= \alpha_2 D' q + e_2 \frac{\partial q}{\partial e} + \gamma_2 \frac{\partial q}{\partial \gamma} & P_4 &= \alpha_2 D' \kappa_4 + e_2 \frac{\partial \kappa_4}{\partial e} + \gamma_2 \frac{\partial \kappa_4}{\partial \gamma} \\
 R' &= \alpha_3 D' p + e_3 \frac{\partial p}{\partial e} + \gamma_3 \frac{\partial p}{\partial \gamma} & R'' &= \alpha_3 D' q + e_3 \frac{\partial q}{\partial e} + \gamma_3 \frac{\partial q}{\partial \gamma} & R_4 &= \alpha_3 D' \kappa_4 + e_3 \frac{\partial \kappa_4}{\partial e} + \gamma_3 \frac{\partial \kappa_4}{\partial \gamma}
 \end{aligned} \tag{50}$$

Then for each pair of arguments

$$\begin{aligned}
 h_{i,c} &= MK_c L' - \frac{1}{2} MC_c L'' - \frac{1}{2} MD_c L_4 & h_{i,c}' &= + MK_c L' - \frac{1}{2} MC_c L'' + \frac{1}{2} MD_c L_4 \\
 h_{i,s} &= MK_s L' - \frac{1}{2} MC_s L'' + \frac{1}{2} MD_s L_4 & h_{i,s}' &= - MK_s L' + \frac{1}{2} MC_s L'' + \frac{1}{2} MD_s L_4 \\
 h_{\pi,c} &= MK_c P' - \frac{1}{2} MC_c P'' - \frac{1}{2} MD_c P_4 & h_{\pi,c}' &= + MK_c P' - \frac{1}{2} MC_c P'' + \frac{1}{2} MD_c P_4 \\
 h_{\pi,s} &= MK_s P' - \frac{1}{2} MC_s P'' + \frac{1}{2} MD_s P_4 & h_{\pi,s}' &= - MK_s P' + \frac{1}{2} MC_s P'' + \frac{1}{2} MD_s P_4 \\
 h_{\theta,c} &= MK_c R' - \frac{1}{2} MC_c R'' - \frac{1}{2} MD_c R_4 & h_{\theta,c}' &= + MK_c R' - \frac{1}{2} MC_c R'' + \frac{1}{2} MD_c R_4 \\
 h_{\theta,s} &= MK_s R' - \frac{1}{2} MC_s R'' + \frac{1}{2} MD_s R_4 & h_{\theta,s}' &= - MK_s R' + \frac{1}{2} MC_s R'' + \frac{1}{2} MD_s R_4
 \end{aligned} \tag{51}$$

§ 24. *Development of the indirect action.*

The fundamental equations for the indirect action are found from (28) by replacing P_1 by the function Ω_p defined in (12). We first replace the coefficients δT by the following:

$$A' = a'^3 \delta T_1 \quad B' = a'^3 \delta T_2, \text{ etc.}$$

Taking, as we do throughout this work, the mean Sun as the origin of longitudes, the true longitude, v' , will be replaced by the Sun's equation of the centre $\equiv E$. We also put

$$r_1 = \frac{r'}{a'}$$

With these substitutions the equations (11) will be replaced by others which may be written thus: Put

$$\begin{aligned}
 G &= \frac{3}{2} r_1^{-3} \sin 2E \delta v' + \frac{9}{4} r_1^{-3} \cos 2E \delta \rho' \\
 J &= \frac{3}{4} r_1^{-3} \delta \rho'
 \end{aligned} \tag{52}$$

$$I = \frac{3}{2} r_1^{-3} \cos 2E \delta v' - \frac{9}{4} r_1^{-3} \sin 2E \delta \rho'$$

Then

$$\begin{aligned}
 A' &= -G - J & B' &= G - J & C' &= 2J & D' &= I \\
 E' &= \frac{3}{2} r_1^{-3} \cos E \sin \beta' & F' &= \frac{3}{2} r_1^{-3} \sin E \sin \beta'
 \end{aligned} \tag{53}$$

These substitutions lead to the replacement of expression (12) by

$$\Omega_p = \frac{m' a^2}{a'^3} H' \quad (54)$$

where

$$H' = A'\xi^2 + B'\eta^2 + C'\xi\eta + 2D'\xi\eta + \dots \quad (55)$$

This function H' , a pure number in dimensions, will hereafter be used as a fundamental quantity instead of Ω_p .

By replacing P_1 by this value of Ω_p in (27) the second members in the form (28) take the common factor

$$\frac{m' a^3}{\mu a'^3} = m^2$$

and the differential variations of the elements become

$$\begin{aligned} D_{n'}\alpha &= m^2 \left(\alpha_1 \frac{\partial H'}{\partial l} + \alpha_2 \frac{\partial H'}{\partial \pi} + \alpha_3 \frac{\partial H'}{\partial \theta} \right) \\ D_{n'}e &= m^2 \left(e_1 \frac{\partial H'}{\partial l} + e_2 \frac{\partial H'}{\partial \pi} + e_3 \frac{\partial H'}{\partial \theta} \right) \\ D_{n'}\gamma &= m^2 \left(\gamma_1 \frac{\partial H'}{\partial l} + \gamma_2 \frac{\partial H'}{\partial \pi} + \gamma_3 \frac{\partial H'}{\partial \theta} \right) \\ -D_{n'}J_0 &= m^2 \left(\alpha_1 D' H' + e_1 \frac{\partial H'}{\partial e} + \gamma_1 \frac{\partial H'}{\partial \gamma} \right) \\ -D_{n'}\pi_0 &= m^2 \left(\alpha_2 D' H' + e_2 \frac{\partial H'}{\partial e} + \gamma_2 \frac{\partial H'}{\partial \gamma} \right) \\ -D_{n'}\theta_0 &= m^2 \left(\alpha_3 D' H' + e_3 \frac{\partial H'}{\partial e} + \gamma_3 \frac{\partial H'}{\partial \gamma} \right) \end{aligned} \quad (56)$$

We have next to develop the values (52) of G , J , and I in terms of the mean anomaly g' . This may be done by means of Cayley's tables in the *Memoirs of the Royal Astronomical Society*, Vol. XXIX, or the development given by Leverrier in *Annales de l'Observatoire de Paris*, Vol. I. Dropping unnecessary terms and powers of e' we have

$$\begin{aligned} r_1^{-3} \cos 2E &= 1 - \frac{5}{2}e'^2 + (3e' - \frac{9}{8}e'^3) \cos g' + \frac{1}{2}e'^2 \cos 2g' \\ r_1^{-3} \sin 2E &= (4e' - \frac{3}{4}e'^3) \sin g' + \frac{1}{2}e'^2 \sin 2g' \\ r_1^{-3} &= 1 + \frac{3}{2}e'^2 + (3e' + \frac{2}{8}e'^3) \cos g' + \frac{9}{2}e'^2 \cos 2g' \\ r_1^{-3} \cos E &= 1 + 3e' \cos g' \\ r_1^{-3} \sin E &= 2e' \sin g' \end{aligned} \quad (58)$$

The expressions for G , J , and I thus become

$$\begin{aligned}
 G &= \{(6e' - \frac{9}{8}e'^3) \sin g' + \frac{5}{4}e'^2 \sin 2g'\} \delta v' \\
 &\quad + \{\frac{9}{4} - \frac{45}{8}e'^2 + (\frac{27}{4}e' - \frac{5}{32}e'^3) \cos g' + \frac{15}{8}e'^2 \cos 2g'\} \delta \rho' \\
 J &= -\{\frac{3}{4} + \frac{9}{8}e'^2 + (\frac{9}{4}e' + \frac{81}{32}e'^3) \cos g' + \frac{27}{8}e'^2 \cos 2g'\} \delta \rho' \\
 I &= \{\frac{3}{2} - \frac{15}{4}e'^2 + (\frac{9}{2}e' - \frac{15}{16}e'^3) \cos g' + \frac{5}{4}e'^2 \cos 2g'\} \delta v' \\
 &\quad - \{(9e' - \frac{27}{16}e'^3) \sin g' + \frac{15}{8}e'^2 \sin 2g'\} \delta \rho'
 \end{aligned} \tag{59}$$

In reducing these expressions to numbers I take, with Delaunay and Brown, the value of e' for 1850

$$e' = .016\ 771$$

With this datum the expressions for G , J , etc., become

$$\begin{aligned}
 G &= (0.10058 \sin g' + 0.00359 \sin 2g') \delta v' \\
 &\quad + (2.24842 + 0.11313 \cos g' + 0.00538 \cos 2g') \delta \rho' \\
 J &= (0.75032 + 0.03775 \cos g' + 0.00095 \cos 2g') \delta \rho' \\
 I &= (1.49895 + 0.07542 \cos g' + 0.00359 \cos 2g') \delta v' \\
 &\quad - (0.15087 \sin g' + 0.00538 \sin 2g') \delta \rho'
 \end{aligned} \tag{60}$$

§ 25. *Abbreviated coefficients for the indirect action.* Since

$$A' + B' + C' = 0$$

we have, as in the direct action,

$$H' = \frac{1}{2}(A' - B')(\xi^2 - \eta^2) - \frac{1}{2}C'(\xi^2 + \eta^2 - 2\zeta^2) + 2D'\xi\eta$$

Replacing A' , B' , and C' by their values (53)

$$H' = -G(\xi^2 - \eta^2) - J(\xi^2 + \eta^2 - 2\zeta^2) + 2I\xi\eta + 2E'\xi\zeta + 2F'\eta\zeta$$

As the last two terms of H' are important only in some exceptional cases, we postpone their development to Part IV.

With the notation of (36), we have for each lunar argument

$$H' = (-2Gp \cos N - 2Jq \cos N + I\kappa_4 \sin N) \tag{61}$$

The planetary factors, G , J , and I are to be developed in a periodic series of the same form as that for A , B , and C , so that, for each planetary argument N_4 we shall have

$$G = G_c \cos N_4 + G_s \sin N_4 \quad J = J_c \cos N_4 + J_s \sin N_4 \quad I = I_c \cos N_4 + I_s \sin N_4 \tag{62}$$

With these values we shall have H' developed in a double series in which for each pair of arguments N and N_4 , H' will have the four terms

$$H' = h_c \cos(N + N_4) + h_c' \cos(N - N_4) + h_s \sin(N + N_4) + h_s' \sin(N - N_4) \quad (63)$$

where

$$h_c = -G_c p - J_c q - \frac{1}{2} I_c \kappa_4 \quad h_c' = -G_c p - J_c q + \frac{1}{2} I_c \kappa_4$$

$$h_s = -G_c p - J_c q + \frac{1}{2} I_c \kappa_4 \quad h_s' = G_c p + J_c q + \frac{1}{2} I_c \kappa_4$$

Expressing the differential variations of the elements in the same form as before we shall find

$$h_{a,c} = m^2(-G_c a p - J_c a q + \frac{1}{2} I_c a \kappa_4) \quad h_{a,c'} = m^2(G_c a p + J_c a q + \frac{1}{2} I_c a \kappa_4) \quad (64)$$

$$h_{a,s} = m^2(G_c a p + J_c a q + \frac{1}{2} I_c a \kappa_4) \quad h_{a,s'} = m^2(G_c a p + J_c a q - \frac{1}{2} I_c a \kappa_4)$$

with two other sets of equations found by replacing a and a by e and e for the set in e , and by γ and g for the set in γ . Also,

$$h_{1,c} = m^2(-G_c L' - J_c L'' - \frac{1}{2} I_c L_4) \quad h_{1,c'} = m^2(-G_c L' - J_c L'' + \frac{1}{2} I_c L_4) \quad (65)$$

$$h_{1,s} = m^2(-G_c L' - J_c L'' + \frac{1}{2} I_c L_4) \quad h_{1,s'} = m^2(G_c L' + J_c L'' + \frac{1}{2} I_c L_4)$$

with two other sets formed by replacing l and L by π and P , for the set in π , and by θ and R for the set in θ .

Comparing these with the corresponding coefficients (51) for the direct action we see that the equations for the indirect action may be formed from those of the direct action by replacing

$$K, \frac{1}{2}C \text{ and } D \text{ by } -G, J, \text{ and } I; \text{ and also } M \text{ by } m^2$$

It also follows that the two actions may be combined by replacing in the expressions for the coefficients h , given in (46), (47), (48) and (51),

$$MK \text{ by } MK - m^2 G; \quad \frac{1}{2}MC \text{ by } \frac{1}{2}MC + m^2 J; \quad MD \text{ by } MD + m^2 I \quad (66)$$

We shall make this combination to save labor in the formation of the products, but shall give the separate parts of the coefficients, so that the parts of each term due to the respective actions may be readily found.

§ 26. *Integration of the equations.* The integration is effected by multiplying each coefficient by the quotient of the mean motion of the Moon by the motion of the argument itself, which factor is

$$v = \frac{n}{in + i'\pi_1 + i''\theta_1 \pm (j + k')n' \pm kn_4} \quad (67)$$

The reciprocal of this factor, which we may use as a divisor, is

$$\frac{1}{\nu} = i + i' \frac{\pi_1}{n} + i'' \frac{\theta_1}{n} \pm (j + k') \frac{n'}{n} \pm k \frac{n_4}{n}$$

a form most convenient for numerical computation.

We shall thus have for the perturbations of the elements corresponding to each pair of lunar and planetary arguments

$$\begin{aligned} \delta\alpha &= \nu h_{\alpha,e} \sin(N \pm N_4) - \nu h_{\alpha,s} \cos(N \pm N_4) \\ \delta e &= \nu h_{e,e} \sin(N \pm N_4) - \nu h_{e,s} \cos(N \pm N_4) \end{aligned} \quad (68)$$

$$\delta\gamma = \nu h_{\gamma,e} \sin(N \pm N_4) - \nu h_{\gamma,s} \cos(N \pm N_4)$$

$$\delta l_0 = -\nu h_{l,e} \sin(N \pm N_4) + \nu h_{l,s} \cos(N \pm N_4)$$

$$\delta\pi_0 = -\nu h_{\pi,e} \sin(N \pm N_4) + \nu h_{\pi,s} \cos(N \pm N_4) \quad (69)$$

$$\delta\theta_0 = -\nu h_{\theta,e} \sin(N \pm N_4) + \nu h_{\theta,s} \cos(N \pm N_4)$$

Practically we use the perturbation of n , the mean motion, instead of α . From the relation of § 12, β , we have

$$D_t n = -\frac{3}{2} n D_t \alpha$$

Thus the first equation (68) is replaced by

$$\delta n = -\frac{3}{2} \nu h_{\alpha,e} \sin(N \pm N_4) + \frac{3}{2} \nu h_{\alpha,s} \cos(N \pm N_4) \quad (70)$$

§ 27. We pass next to the inequalities of the actual mean longitude, l , and of the perigee and node, π and θ . Taking the equations (29) for these quantities

$$l = l_0 + \int n dt \quad \pi = \pi_0 + \int \pi_1 dt \quad \theta = \theta_0 + \int \theta_1 dt$$

the complete expressions are

$$\delta l = \delta l_0 + \int \delta n dt \quad \delta \pi = \delta \pi_0 + \int \delta \pi_1 dt \quad \delta \theta = \delta \theta_0 + \int \delta \theta_1 dt \quad (71)$$

The motions n , π_1 , and θ_1 are functions of the elements a (or α), e , and γ . n is given by the relation $a^3 n^2 = \mu$, while π_1 and θ_1 have been developed by Delaunay, whose results are found in *Comptes Rendus*, Vol. LXXIV, 1872, I, and are reproduced in part in *Action*, p. 190.

$$\delta \pi_1 = \frac{\partial \pi_1}{\partial n} \delta n + \frac{\partial \pi_1}{\partial e} \delta e + \frac{\partial \pi_1}{\partial \gamma} \delta \gamma \quad \delta \theta_1 = \frac{\partial \theta_1}{\partial n} \delta n + \frac{\partial \theta_1}{\partial e} \delta e + \frac{\partial \theta_1}{\partial \gamma} \delta \gamma$$

From (70) and (71) we thus have, in the variation of l , the terms

$$D_{n_1} \delta l = -\frac{3}{2} \nu h_{\alpha,e} \sin(N \pm N_4) + \frac{3}{2} \nu h_{\alpha,s} \cos(N \pm N_4) \quad (72)$$

arising from the variation of n . Integrating and including the value of δl_0 we shall have for the complete perturbation of the mean longitude

$$\delta l = l_c \cos(N \pm N_4) + l_s \sin(N \pm N_4)$$

where

$$l_c = \frac{3}{2}v^2 h_{a,c} + v h_{l,s} = v(\frac{3}{2}v h_{a,c} + h_{l,s}) \quad l_s = \frac{3}{2}v^2 h_{a,s} - v h_{l,s} = v(\frac{3}{2}v h_{a,s} - h_{l,s}) \quad (73)$$

From the Delaunay developments in powers of m are found

$$\begin{aligned} \frac{\partial \pi_1}{\partial n} &= - .01480 & \frac{\partial \pi_1}{\partial e} &= - .001042n & \frac{\partial \pi_1}{\partial \gamma} &= - .004331n \\ \frac{\partial \theta_1}{\partial n} &= + .00377 & \frac{\partial \theta_1}{\partial e} &= - .001292n & \frac{\partial \theta_1}{\partial \gamma} &= + .000665n \end{aligned} \quad (74)$$

Substituting these values and the values (68) and (70) we find that by putting

$$\begin{aligned} \pi_{1,c} &= .02220h_{a,c} - .00104h_{e,c} - .00433h_{\gamma,c} & \pi_{1,s} &= .02220h_{a,s} - .00104h_{e,s} - .00433h_{\gamma,s} \\ \theta_{1,c} &= - .00566h_{a,c} - .00129h_{e,c} + .00066h_{\gamma,c} & \theta_{1,s} &= - .00566h_{a,s} - .00129h_{e,s} + .00066h_{\gamma,s} \end{aligned} \quad (75)$$

we shall have

$$\begin{aligned} \delta \pi_1 &= v n \{ \pi_{1,c} \sin(N \pm N_4) - \pi_{1,s} \cos(N \pm N_4) \} \\ \delta \theta_1 &= v n \{ \theta_{1,c} \sin(N \pm N_4) - \theta_{1,s} \cos(N \pm N_4) \} \end{aligned}$$

Then by integrating we have the terms

$$\begin{aligned} \delta \pi &= - v^2 \pi_{1,c} \cos(N \pm N_4) - v^2 \pi_{1,s} \sin(N \pm N_4) \\ \delta \theta &= - v^2 \theta_{1,c} \cos(N \pm N_4) - v^2 \theta_{1,s} \sin(N \pm N_4) \end{aligned} \quad (76)$$

Adding the values (69) we have the complete periodic perturbations of π and θ expressed in the form

$$\delta \pi = \pi_c \cos(N \pm N_4) + \pi_s \sin(N \pm N_4) \quad \delta \theta = \theta_c \cos(N \pm N_4) + \theta_s \sin(N \pm N_4)$$

where

$$\begin{aligned} \pi_c &= v h_{\pi,s} - v^2 \pi_{1,c} = v(h_{\pi,s} - v \pi_{1,c}) & \pi_s &= - v h_{\pi,c} - v^2 \pi_{1,s} = - v(h_{\pi,c} + v \pi_{1,s}) \\ \theta_c &= v h_{\theta,s} - v^2 \theta_{1,c} = v(h_{\theta,s} - v \theta_{1,c}) & \theta_s &= - v h_{\theta,c} - v^2 \theta_{1,s} = - v(h_{\theta,c} + v \theta_{1,s}) \end{aligned} \quad (77)$$

§ 28. Treatment of the non-periodic terms in R .

In the preceding integration we have supposed all the arguments to be of the form $G_0 + n t$. We have now to consider the special case in which n vanishes. In the case of the direct action this occurs when, in the pair of arguments which form G ,

$$i = i' = i'' = k = 0 \quad j \pm k' = 0$$

We shall then have in H a term, $H = \Sigma h_c$, which we shall call h_c simply. It will be affected by a minute secular variation which we need not consider at present,

In the case of the indirect action we note that the coefficients of $\delta v'$, $\delta \rho'$, and $\delta \beta'$, as found in (59), are developed in the general form $\Sigma k_i \sin ig'$ or $k_i \cos ig'$, in which k_0 , being a function of the eccentricity of the Earth's orbit, is a function of the time. The coefficients of all the terms arising from the indirect action are therefore affected by a secular variation.

The perturbations $\delta v'$ and $\delta \rho'$ contain terms independent of the mean longitude of the disturbing planet, which may be treated separately, namely:

- (1) A constant term in $\delta \rho'$.
- (2) Terms of the form $c \frac{\sin}{\cos} ig'$ in $\delta v'$ and $\delta \rho'$.
- (3) The secular variation of e' and of ρ' .

Omitting for the present the powers of t above the first, we shall have in $\delta v'$ and $\delta \rho'$ terms of the general form

$$(c + c't) \frac{\sin}{\cos} ig'$$

The product of these into (59) gives rise to terms of G , J , and I of the same form. When we form the products of these terms by ξ^2 , η^2 , etc., we shall have in H' terms of the form

$$h + h'nt + \dots$$

Substituting the derivatives of the non-periodic direct term in (41) and (42), and of the indirect term in (56) and (57), omitting terms in t , and putting for brevity

$$P_0 = Mh_c + m^2h$$

we find

$$\begin{aligned} D_{nt}\alpha &= D_{nt}e = D_{nt}\gamma = 0 \\ -D_{nt}l_0 &= \alpha_1 D'P_0 + e_1 \frac{\partial P_0}{\partial e} + \gamma_1 \frac{\partial P_0}{\partial \gamma} \equiv h_0 \\ -D_{nt}\pi_0 &= \alpha_2 D'P_0 + e_2 \frac{\partial P_0}{\partial e} + \gamma_2 \frac{\partial P_0}{\partial \gamma} \equiv h'_0 \\ -D_{nt}\theta_0 &= \alpha_3 D'P_0 + e_3 \frac{\partial P_0}{\partial e} + \gamma_3 \frac{\partial P_0}{\partial \gamma} \equiv h''_0 \end{aligned} \tag{78}$$

Adding in the terms multiplied by nt , these three equations may be written

$$D_{nt}l_0 = -h_0 - h_1nt \quad D_{nt}\pi_0 = -h'_0 - h'_1nt \quad D_{nt}\theta_0 = -h''_0 - h''_1nt \tag{78'}$$

The integration of (78) and (78') will give

$$\begin{aligned} \delta\alpha &= \delta_0\alpha; & \delta l_0 &= \delta_0 l_0 - h_0nt - \frac{1}{2}h_1n^2t^2 \\ \delta e &= \delta_0e; & \delta\pi_0 &= \delta_0\pi_0 - h'_0nt - \frac{1}{2}h'_1n^2t^2 \\ \delta\gamma &= \delta_0\gamma; & \delta\theta_0 &= \delta_0\theta_0 - h''_0nt - \frac{1}{2}h''_1n^2t^2 \end{aligned} \tag{78''}$$

δ_0 designating, in each case, the arbitrary constant of integration.

The completed expressions for l , π , and θ are to be found by the equations

$$\delta n = \frac{\partial n}{\partial \alpha} \delta \alpha \quad \delta \pi_1 = \frac{\partial \pi_1}{\partial \alpha} \delta \alpha + \frac{\partial \pi_1}{\partial e} \delta e + \frac{\partial \pi_1}{\partial \gamma} \delta \gamma \quad \delta \theta_1 = \frac{\partial \theta_1}{\partial \alpha} \delta \alpha + \frac{\partial \theta_1}{\partial e} \delta e + \frac{\partial \theta_1}{\partial \gamma} \delta \gamma \quad (79)$$

$$\delta l = \delta l_0 + \int \delta n dt \quad \delta \pi = \delta \pi_0 + \int \delta \pi_1 dt \quad \delta \theta = \delta \theta_0 + \int \delta \theta_1 dt \quad (80)$$

In these equations the perturbations (78'') are to be substituted. In doing this the arbitrary constants δl_0 , $\delta_0 \pi_0$, and $\delta_0 \theta_0$, being merely constant corrections to l , π , and θ , may be dropped as unimportant to the theory. We shall then have from (78'') and (80)

$$\begin{aligned} \delta l &= \left(\frac{\partial n}{\partial \alpha} \delta_0 \alpha - h_0 n \right) t - \frac{1}{2} h_1 n^2 t^2 \\ \delta \pi &= \left(\frac{\partial \pi_1}{\partial \alpha} \delta_0 \alpha + \frac{\partial \pi_1}{\partial e} \delta_0 e + \frac{\partial \pi_1}{\partial \gamma} \delta_0 \gamma - h_0' n \right) t - \frac{1}{2} h_1' n^2 t^2 \\ \delta \theta &= \left(\frac{\partial \theta_1}{\partial \alpha} \delta_0 \alpha + \frac{\partial \theta_1}{\partial e} \delta_0 e + \frac{\partial \theta_1}{\partial \gamma} \delta_0 \gamma - h_0'' n \right) t - \frac{1}{2} h_1'' n^2 t^2 \end{aligned} \quad (81)$$

§ 29. *Adjustment of the arbitrary constants.* Values are next to be assigned to the arbitrary constants $\delta_0 \alpha$, $\delta_0 e$, and $\delta_0 \gamma$. We shall do this so as to satisfy the conditions that the coefficient of t in δl , of $\sin g$ in the mean longitude, and of $\sin(l - \theta)$ in the latitude, shall all remain unchanged. The first of these conditions gives

$$-\frac{2}{3} n \delta_0 \alpha = h_0 n \quad \text{or} \quad \delta_0 \alpha = -\frac{2}{3} h_0 \quad (82)$$

We thus have

$$\delta l = -\frac{1}{2} h_1 n^2 t^2$$

The determination of $\delta_0 e$ and $\delta_0 \gamma$ must await the computation of the periodic terms depending on the arguments g and $l - \theta$, which is found in Part IV. The increments in the motions of π and θ now become

$$\begin{aligned} \delta \pi_1 &= n \left(\frac{\partial \pi_1}{\partial n} h_0 - h_0' \right) + \frac{\partial \pi_1}{\partial e} \delta_0 e + \frac{\partial \pi_1}{\partial \gamma} \delta_0 \gamma \\ \delta \theta_1 &= n \left(\frac{\partial \theta_1}{\partial n} h_0 - h_0'' \right) + \frac{\partial \theta_1}{\partial e} \delta_0 e + \frac{\partial \theta_1}{\partial \gamma} \delta_0 \gamma \end{aligned} \quad (83)$$

§ 30. *Opposite secular effects of the direct and indirect action of a planet near the Sun.*

An important theorem of the planetary action on the Moon is that as the planet is nearer the Sun, not only does each form of action become smaller, but the two forms tend to cancel each other, so that when the mass of the planet can be considered as simply added to that of the Sun, the non-parallactic perturbations vanish.

To find the effect of the direct action in this case, let the values of x_4 , y_4 , and z_4 in (14) be so small that they may be neglected in comparison with x' , y' , and z' . Then Δ will merge into r' and we shall have

$$R = \frac{m_4 r'^2}{2r'^3} (3S^2 - 1)$$

For the indirect action we remark that the only effect of the action of the planet on the position of the Earth, after so adjusting the constants of integration that the mean motion shall remain unaltered, is to increase the mean distance, so that instead of

$$a'^3 n'^2 = m'$$

we shall have

$$a'^3 n'^2 = m' + m_4$$

This gives, for the perturbation of a'

$$3a'^2 n'^2 \delta a' = m_4$$

and the eccentricity e' being unaltered

$$\delta \rho' = \frac{m_4}{3m'}$$

The corresponding part of Ω_p is found from (7) by assigning the increment $r' \delta \rho'$ to r' . We thus have

$$\Omega_p = -\frac{3m' r'^2 \delta \rho'}{2r'^3} (3S^2 - 1) = -\frac{m_4 r'^2}{2r'^3} (3S^2 - 1)$$

This cancels the value of R found above.

PART II.

NUMERICAL DEVELOPMENT OF THE PLANETARY
COEFFICIENTS.

that we could not be sure of this point without actual computation. In the case of the Hansenian inequality of long period due to the action of Venus it was shown that the perturbations in question, considered individually, were nearly of the same order of magnitude as the coefficients to be determined. This proceeded from the fact that, even when we consider only the formulæ of the elliptic motion, the coefficients of the term in question are in the nature of minute residual differences of large quantities. In view of the undoubted fact of some apparent inequalities of long period in the motion of the Moon of which theory has yet given no explanation, it seems necessary to exhaustively discuss every possible mode of action which might affect the result.

The most effective and certain way which the author could devise to overcome this difficulty was to employ the purely numerical development sometimes called "mechanical quadratures," but, more exactly, that of induction of general formulæ from special values. It is true that the numerical computations required by this method would be very voluminous, possibly more so than those by other methods. But the use of the method has the great advantage that the computations are made on a simple and uniform plan, which can be executed by routine computers, and in which the complexity incident to the analytic treatment does not enter at all. Another important advantage of this purely numerical method is that the mutual periodic perturbations of Venus and the Earth can be taken account of from the beginning. This will readily be seen by a statement of the method.

The values of the planetary coefficients A, B , etc., being functions of the geocentric coördinates of Venus, can be computed for any assigned mean longitude of the Earth and Venus. They are therefore to be computed for a certain number of equidistant values of the mean longitude of each planet. For each of these values there will be a definite perturbation of the coördinates of each planet, which may be computed and applied in advance. Thus the first computation gives at once numerical values of the coefficients in which the effect of periodic perturbation is included. From these are developed by well-known formulæ the coefficients of the sines and cosines of the multiples of the mean longitudes.

The perturbations of Mars are so small that it was assumed that undisturbed values of the coefficients would suffice. But the same method was used owing to its simplicity in theory.

In the case of Jupiter the analytic development would not have involved the difficulty which I have pointed out. But it was so convenient to apply the numerical method that it was adopted for this planet also.

The action of Saturn is so minute that a very simple development suffices. It was therefore unnecessary to employ the numerical method in this case.

A. ACTION OF VENUS.

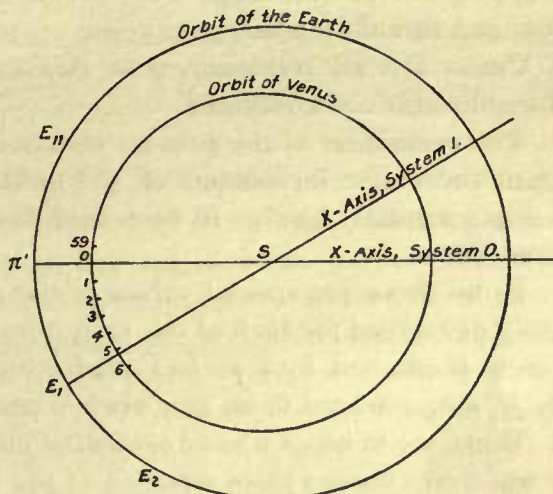
§ 32. We shall now show how the computations were arranged in the case of Venus. Let us first suppose that the orbits of both planets are circular. Then assume the Earth to be in zero of longitude. We assign in succession 60 equidistant longitudes to Venus, 6° apart. For each of these positions we compute the values of the four principal coefficients. Numerical induction from these special values will then give the values of A , B , etc., in a series proceeding according to the cosines of the multiples of the differences of the mean longitudes.

Now assign to the Earth a mean longitude equal to any multiple of 6° . If we start with Venus at inferior conjunction we shall have the same series of values of the coefficients as before, provided that we now take the line joining the Sun and Earth as the axis of X . Supposing all our coördinates referred to this axis we should then have A , B , etc., developed according to cosines of multiples of the difference of the mean longitudes.

It follows that in the actual case of the two orbits having a small eccentricity and inclination the other terms which we require will be of the order of magnitude of these quantities and will therefore be smaller than these principal terms. It is therefore not necessary to divide the circle into so many parts in order to obtain them.

The actual process was to take the direction of the solar perigee for 1800 as the initial line, or axis of X . The way in which the coördinates were defined will then be seen by the diagram. Here on the left, π' marks the position of the Earth's perihelion. The positive direction of X passes through the Sun and is therefore directed toward the solar perigee. The Earth being in this fixed position, the coördinates of Venus are computed for 60 equidistant values of the mean longitude of Venus differing by increments of 6° . The initial or zero value corresponds to the mean inferior conjunction of Venus, marked 0 in the figure, which determines all the other values; a few of the others are numbered in order.

For each of these mean longitudes, the actual coördinates of Venus, including the effect of perturbations by the Earth, were computed. The position of the Earth at π' , corresponding to the 6° positions of Venus, was then corrected in each of the 60 cases by the periodic perturbations due to each position of Venus. With these coördinates 60 numerical values of the A -coefficients are computed. I



Arrangement of Coördinate Axes, in Systems 0, 1, etc., for Venus.

designate this system of 60 values, corresponding, perturbations aside, to one position of the Earth, by the number 0; and I distinguish the values by 60 indices 0, 1, 2, . . . 59.

In the next system, called system 1, the Earth has moved through 30° of mean longitude, or mean anomaly, to the position E_1 . The set of 60 heliocentric coördinates of Venus to be used will be the same as before, except for the perturbations, which will now be those for E_1 , or for $g=30^\circ$. But the position corresponding to the inferior conjunction in this system will be that corresponding to the index 5 in system 0. A new axis of X is now adopted, again passing through the mean Sun, and therefore making an angle of 30° with the initial axis. The coördinates of Venus are all transformed to this axis, and another set of 60 values of the A -coefficients are computed.

The remainder of the process consists in assigning to the mean longitude of the Earth successive increments of 30° until it is brought around to the position E_{11} , in mean anomaly 330° . In each case the axis of X is taken to pass through the mean Sun.

From these 720 special values of the A -coefficients the general values are separately developed for each of the 12 systems. Then the general development for any system is effected by a second quadrature. The final result will be the values of A , B , etc., referred to an axis always passing through the mean Sun.

Were we to adopt a fixed system of coördinate axes, it would now be necessary to transform these values referred to the moving axis, to the adopted fixed system. But the necessity of this transformation is avoided by referring all the coördinates, those of the Moon as well as of the planet, to the mean Sun from the beginning. This is fully as simple as, perhaps even simpler than, referring them to a fixed axis. The ease of doing it is all the greater from the fact that, in the actual computation of the lunar coördinates, they are first referred to the mean Moon. The transformation from the mean Moon to the mean Sun is probably simpler than the transformation to a fixed axis.

§ 33. *Development of the A-coefficients for Venus.*

The computations relating to Venus are shown in tabular form in Tables I-VIII, and will now be explained. To obtain the 12 undisturbed values of the Sun's coördinates, we derive the equation of the centre and the logarithm of the radius vector from the tables of the Sun found in *Astronomical Papers*, Vol. VI.

For the argument of mean anomaly of the Sun the initial value is

$$M_0 = 5.37018$$

corresponding to $g' = 0^\circ$. The increment for each 30° is

$$\Delta M = 30.43830$$

resulting in the value 188.0000 for $g' = 180^\circ$.

With the 12 values of M thus found are taken the equation of the centre, E , for 1800, and $\log r'$. Then

$$x' = r' \cos E \qquad y' = r' \sin E$$

The resulting values of x' and y' are shown in Table I.

For Venus, we have

$$\text{Initial mean longitude} = 99^\circ 30' 7''$$

this being the longitude of the Earth's perihelion for 1800. For the same epoch we have

$$\text{Longitude of perihelion of Venus} = 128^\circ 45' 17''.4$$

$$\text{Initial mean anomaly of Venus} = 330^\circ 44' 50''.2$$

To find the tabular argument corresponding to this mean anomaly we proceed thus: Adding 5 increments of 6° , we have

$$\text{Mean anomaly of Venus for index 5} = 0^\circ 44' 50''.25$$

For this mean anomaly the precepts of *Tables of Venus*, pp. 278-279, give

$$\text{Tabular Arg. } K; K_0 = 1.11601$$

$$\text{Increment of } K \text{ for } 6^\circ = 3.745014$$

We now add one period to K and subtract 5 increments

$$\begin{array}{r} K_0 = \quad 1.11601 \\ P = \quad 224.70084 \\ \quad \quad 225.81685 \\ 5 \text{ increments} \quad 18.72507 \\ \text{Initial } K, \quad \underline{207.09178} \end{array}$$

which corresponds to the inferior conjunction of Venus in system o.

The resulting values of K are found in Table II. With the values of K thus formed the equation of the centre and $\log r$ in the elliptic orbit of 1800 are taken from the tables.

The data for the rectangular coördinates are:

$$\text{Node of Venus, 1800} \qquad \Omega = 74^\circ 52' 48''.75$$

$$\text{Perihelion of Earth} \qquad \pi = 99^\circ 30' 7''.6$$

$$\text{Node referred to Perihelion} \quad \theta = 335^\circ 22' 41''.2$$

$$\text{Inclination for 1800} \qquad \gamma = 3^\circ 23' 33''.45$$

The values of the coördinates x , y , and z in the initial system are now computed by the formulæ

$$u = \text{Eq. Cent.} + 24^\circ 37' 18''.80 \qquad m \sin M = \cos \gamma \sin \theta \qquad m \cos M = \cos \theta$$

$$m' \sin M' = \sin \theta \qquad m' \cos M' = \cos \gamma \cos \theta$$

leading to

$$M = 24^\circ 35' 1''.84 \qquad M' = 24^\circ 39' 35''.91$$

$$\log m = 9.9998680 \qquad \log m' = 9.9993706$$

$$x = mr \cos (M + u) \qquad y = m'r \sin (M' + u) \qquad z = r \sin \gamma \sin u$$

Designating the systems by suffixes, and putting $c = \cos 30^\circ$, these coördinates were transformed to the axes of the other 11 systems by the formulæ

$$\begin{aligned} x_1 &= cx_0 + \frac{1}{2}y_0 & y_1 &= cy_0 - \frac{1}{2}x_0 \\ x_2 &= \frac{1}{2}x_0 + cy_0 & y_2 &= \frac{1}{2}y_0 - cx_0 \\ x_3 &= y_0 & y_3 &= -x_0 \\ x_4 &= y_1 & y_4 &= -x_1 \\ x_5 &= y_2 & y_5 &= -x_2 \\ \text{and then, in general,} & & x_n &= -x_{n-6} & y_n &= -y_{n-6} \end{aligned}$$

§ 34. *Explanation of the tables.* The periodic perturbations of the longitudes of the Earth and Venus, and of the logarithms of their radii vectores, omitting terms of long period, are now to be found.

TABLE III: *Mutual periodic perturbations.*

For the perturbations of Venus by the Earth, δu and $\delta \rho$, the arguments of the double entry Tables VIII and XVII are:

$$\begin{aligned} \text{Hor. Arg. } g &= K - 0^d.650 = 206^d.44 + 3.745i \\ \text{Vert. Arg. II for System } 0 &\text{ and } i = 0, 104.35 \\ \text{Increment of II for each system } \Delta \text{II} &= 20 \\ \text{“ “ “ “ “ index } \Delta_2 \text{II} &= -2.461 \end{aligned}$$

For the single entry Tables XI and XX we have

$$\begin{aligned} \text{Arg. } A &= 1.62203(g - g') \\ \text{For the index } i & \quad g = 330^\circ.75 + 6^\circ i \\ \text{For the } j\text{th system } & \quad g' = 30^\circ j \\ \text{Hence, for } i = 0, j = 0, & \quad \text{Arg. } A = 536.49 \\ \text{Increment for each unit of } i, & \quad \Delta A = +9.732 \\ \text{“ “ “ “ “ } j, & \quad \Delta' A = -48.661 \end{aligned}$$

With the values of the arguments thus formed the periodic perturbations of Venus by the Earth are taken from the Tables VIII, XVII, XI, and XX.

For the corresponding perturbations of the Earth by Venus, we have

$$\begin{aligned} \text{Hor. Arg. } g &= 30.4383j \\ \text{Vert. Arg. II for } j = 0; & \quad i = 0 \dots 165.375 \\ \text{Increment for each unit of } i; & \quad \frac{1}{2}\Delta g = 3 \\ \text{“ “ “ “ “ } j; & \quad -24.383 \end{aligned}$$

Argument A has the same value as in the *Tables of Venus*.

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TABLE IV α AND IV b . The perturbations in Table III are transformed into increments of the rectangular coördinates of Venus and the Earth.

Neglecting the cosine of the inclination we have for Venus when referred to the initial system of axes

$$\Delta x_0 = -y \sin i'' \delta u + x \delta \rho \quad \Delta y_0 = x \sin i'' \delta u + y \delta \rho$$

the tabular $\delta \rho$ being multiplied by the modulus of logarithms. For the other systems the transformation is made by the formulæ for the transformation of the coördinates themselves. The results are given in full, in units of the 8th place of decimals, in Table IV. Applying them to the undisturbed coördinates, we have the coördinates of Venus for each position of the two bodies.

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TABLE VI. With the perturbations of latitude in the different systems the disturbed geocentric coördinate Z was computed and tabulated.

With these geocentric coördinates are computed the 720 values of the four coefficients A , B , C , and D defined in § 7. Since

$$A + B + C = 0$$

the computation of C might have been dispensed with. It was, however, carried through as an additional check on the accuracy of the work. The latter was, however, done in duplicate, the check being incomplete.

TABLE VII gives the values of the coefficients thus computed.

The coefficients E and F lead to appreciable inequalities only in the case of the argument θ , and have been treated separately. Their special values were computed for six systems and thirty indices only, and are found in Table VIII.

§ 35. The process of developing the general value of each coefficient in a periodic series is given by Brünnow in his *Sphärischen Astronomie*. Taking A as an example we first develop the value for each system in the form

$$A_k = \Sigma (a_k \cos iL + b_k \sin iL)$$

where k is the number of the system and L the difference of the mean longitudes of Venus and the Earth,

$$L = v - g'$$

We thus have 12 values of each of the coefficients a_k and b_k , one corresponding to each value of g' . These values are then again developed in the form

$$a_k = \Sigma (a_{k,j} \cos jg' + b_{k,j} \sin jg') \quad b_k = \Sigma (a_{k,j'} \cos ig' + b_{k,j'} \sin jg')$$

Designating the systems by suffixes, and putting $c = \cos 30^\circ$, these coördinates were transformed to the axes of the other 11 systems by the formulæ

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We thus have 12 values of each of the coefficients a_k and b_k , one corresponding to each value of g' . These values are then again developed in the form

$$a_k = \Sigma (a_{k,j} \cos jg' + b_{k,j} \sin jg') \quad b_k = \Sigma (a_{k,j}' \cos ig' + b_{k,j}' \sin jg')$$

These being substituted in the general expression given above for A_k gives the value of A itself in the form

$$A = \Sigma \Sigma [a \cos (iL + jg') + b \sin (iL + jg')]$$

The development was effected in this way up to $i = 8$ only, this being the limit for possible sensible terms other than the Hansenian term of long period depending on the argument

$$18L + 2g' - g$$

§ 36. *The Hansenian Venus-term of long period.* The computation of this inequality requires the determination of the coefficients for $i = 18$, which we obtain from the general formulæ thus. Putting, in any one system,

$$A_0, A_1, A_2, \dots, A_{59}$$

for the 60 values of A , and

$$A_c \cos 18L + A_s \sin 18L$$

for the pair of terms depending on the argument $18L$, the general formulæ give

$$30A_c = A_0 + A_1 \cos 108^\circ + A_2 \cos 216^\circ + \dots$$

$$30A_s = A_1 \sin 108^\circ + A_2 \sin 216^\circ + \dots$$

the angles increasing by 108° in each term. The fifth angle will be $180^\circ + 2\pi$, so that the only numerically different values of the coefficients which enter into the series besides 1 and 0 are

$$\sin 18^\circ, \cos 18^\circ, \sin 36^\circ, \text{ and } \cos 36^\circ.$$

For example, we have

$$30A_c = A_0 - A_1 \sin 18^\circ - A_2 \cos 36^\circ + A_3 \cos 36^\circ + A_4 \sin 18^\circ + \dots$$

$$30A_s = A_1 \cos 18^\circ - A_2 \sin 36^\circ - A_3 \sin 36^\circ + A_4 \cos 18^\circ + \dots$$

From the cyclic order of the coefficients the method of computing A_c and A_s is as follows:

With the 60 values of any one coefficient, say A , in any one system,

$$A_0, A_1, A_2, \dots, A_{59}$$

compute

$$A_0' = A_0 + A_{10} + A_{20} + \dots + A_{50}$$

$$A_1' = A_1 + A_{11} + A_{21} + \dots + A_{51}$$

$$A_2' = A_2 + A_{12} + A_{22} + \dots + A_{52}$$

$$\vdots$$

$$A_9' = A_9 + A_{19} + A_{29} + \dots + A_{59}$$

Next:

$$A_0'' = A_0' - A_5' \quad A_1'' = A_1' - A_6' \quad A_2'' = A_2' - A_7' \quad A_3'' = A_3' - A_8' \quad A_4'' = A_4' - A_9'$$

Next:

$$A_{e,1} = A_4'' + A_1'' \quad A_{e,1} = A_4'' - A_1'' \quad A_{s,1} = A'' + A_2'' \quad A_{e,2} = A_3'' - A_2''$$

We then have, in each system

$$30A_c = A_0'' + A_{e,1} \sin 18^\circ + A_{e,2} \cos 36^\circ \quad 30A_s = A_{s,1} \cos 18^\circ - A_{e,2} \sin 36^\circ$$

with similar values for B , C , and D .

The numerical results of these processes for each system are shown in Table IX.

The next step is to develop each set of numerical values of any one pair of coefficients, say A_c , and A_s in the form

$$\begin{aligned} 30A_c &= \alpha_0 + \alpha_1 \cos g' + \alpha_2 \cos 2g' + \beta_1 \sin g' + \beta_2 \sin 2g' \\ 30A_s &= \alpha_0' + \alpha_1' \cos g' + \alpha_2' \cos 2g' + \beta_1' \sin g' + \beta_2' \sin 2g' \end{aligned} \quad (a)$$

These are to be substituted in the general form

$$A = A_c \cos 18L + A_s \sin 18L$$

Retaining only terms which may be wanted for our purpose, we shall have

$$\begin{aligned} 30A &= \alpha_0 \cos 18L + \alpha_0' \sin 18L \\ &+ \frac{1}{2}(\alpha_1 - \beta_1') \cos (18L + g') + \frac{1}{2}(\alpha_1' + \beta_1) \sin (18L + g') \\ &+ \frac{1}{2}(\alpha_2 - \beta_2') \cos (18L + 2g') + \frac{1}{2}(\alpha_2' + \beta_2) \sin (18L + 2g') \\ &+ \frac{1}{2}(\alpha_3 - \beta_3') \cos (18L + 3g') + \frac{1}{2}(\alpha_3' + \beta_3) \sin (18L + 3g') \end{aligned} \quad (b)$$

TABLE I.

SUN'S GEOCENTRIC COÖRDINATES IN THE MEAN ORBIT OF 1800,
REFERRED TO MEAN SUN AS DIRECTION OF AXIS OF X.

| System. | g' | x' | y' |
|---------|------|-------------|-------------|
| 0 | 0 | +0.983 2075 | 0.000 0000 |
| 1 | 30 | +0.985 3853 | +0.016 8542 |
| 2 | 60 | +0.991 3897 | +0.029 1452 |
| 3 | 90 | +0.999 7183 | +0.033 5823 |
| 4 | 120 | +1.008 1877 | +0.029 0233 |
| 5 | 150 | +1.014 4741 | +0.016 7321 |
| 6 | 180 | +1.016 7929 | 0.000 0000 |
| 7 | 210 | +1.014 4741 | -0.016 7321 |
| 8 | 240 | +1.008 1877 | -0.029 0233 |
| 9 | 270 | +0.999 7183 | -0.033 5823 |
| 10 | 300 | +0.991 3897 | -0.029 1452 |
| 11 | 330 | +0.985 3853 | -0.016 8542 |

TABLE II.

COMPUTATION OF RECTANGULAR COÖRDINATES OF VENUS IN THE ELLIPTIC ORBIT OF 1800, REFERRED TO SOLAR PERIGEE AS AXIS OF X.

| <i>i</i> | Arg. K. | Eq. Cent. | log. <i>r</i> | log. <i>x</i> | log. <i>y</i> | log. <i>z</i> |
|----------|----------|-----------|---------------|---------------|---------------|---------------|
| 0 | 207.0918 | -23 15.02 | 9.856 7321 | -0.856 5920 | +7.726 9130 | +8.242 1742 |
| 1 | 210.8368 | -18 47.49 | 9.856 5914 | -0.854 2879 | -8.849 0901 | +8.331 7492 |
| 2 | 214.5818 | -14 7.30 | 9.856 4812 | -0.847 0688 | -9.163 8652 | +8.401 8640 |
| 3 | 218.3268 | -9 17.60 | 9.856 4028 | -0.834 7638 | -9.341 2292 | +8.457 9729 |
| 4 | 222.0718 | -4 21.63 | 9.856 3570 | -0.817 0717 | -9.463 1513 | +8.503 3027 |
| 5 | 1.1160 | + 0 37.28 | 9.856 3445 | -0.793 5309 | -9.554 3215 | +8.539 9034 |
| 6 | 4.8610 | + 5 35.76 | 9.856 3653 | -0.793 4657 | -9.625 5304 | +8.569 1404 |
| 7 | 8.6060 | +10 30.48 | 9.856 4193 | -0.725 9000 | -9.682 4522 | +8.591 9486 |
| 8 | 12.3510 | +15 18.10 | 9.856 5057 | -0.679 4042 | -9.728 4252 | +8.608 9752 |
| 9 | 16.0961 | +19 55.43 | 9.856 6236 | -0.621 8221 | -9.765 5624 | +8.620 6617 |
| 10 | 19.8411 | +24 19.34 | 9.856 7717 | -0.549 7350 | -9.795 2686 | +8.627 2934 |
| 11 | 23.5861 | +28 26.93 | 9.856 9481 | -0.457 3022 | -9.818 5057 | +8.629 0280 |
| 12 | 27.3311 | +32 15.39 | 9.857 1509 | -0.333 3365 | -9.835 9401 | +8.625 9108 |
| 13 | 31.0761 | +35 42.29 | 9.857 3778 | -0.151 9096 | -9.848 0289 | +8.617 8781 |
| 14 | 34.8211 | +38 45.29 | 9.857 6261 | -0.824 3320 | -9.855 0707 | +8.604 7511 |
| 15 | 38.5661 | +41 22.44 | 9.857 8931 | +7.961 5592 | -9.857 2356 | +8.586 2194 |
| 16 | 42.3112 | +43 32.07 | 9.858 1756 | +8.929 0946 | -9.854 5813 | +8.561 8070 |
| 17 | 46.0562 | +45 12.78 | 9.858 4706 | +9.203 5288 | -9.847 0574 | +8.530 8192 |
| 18 | 49.8012 | +46 23.54 | 9.858 7747 | +9.367 1085 | -9.834 5015 | +8.492 2492 |
| 19 | 53.5462 | +47 3.66 | 9.859 0846 | +9.482 0030 | -9.816 6224 | +8.444 6187 |
| 20 | 57.2912 | +47 12.78 | 9.859 3968 | +9.568 8886 | -9.792 9712 | +8.385 6881 |
| 21 | 61.0362 | +46 50.89 | 9.859 7079 | +9.637 2113 | -9.762 8896 | +8.311 8851 |
| 22 | 64.7812 | +45 58.29 | 9.860 0146 | +9.692 0696 | -9.725 4250 | +8.217 0551 |
| 23 | 68.5263 | +44 35.65 | 9.860 3134 | +9.736 5149 | -9.679 1841 | +8.089 2497 |
| 24 | 72.2713 | +42 43.92 | 9.860 6011 | +9.772 5022 | -9.622 0691 | +7.900 1224 |
| 25 | 76.0163 | +40 24.44 | 9.860 8748 | +9.801 3428 | -9.550 7649 | +7.546 9461 |
| 26 | 79.7613 | +37 38.73 | 9.861 1314 | +9.823 9406 | -9.459 6400 | -6.971 8246 |
| 27 | 83.5063 | +34 28.65 | 9.861 3684 | +9.840 9243 | -9.338 0001 | -7.731 3881 |
| 28 | 87.2513 | +30 56.31 | 9.861 5830 | +9.852 7264 | -9.161 4423 | -7.990 3231 |
| 29 | 90.9963 | +27 4.01 | 9.861 7733 | +9.859 6294 | -8.849 5051 | -8.148 1795 |
| 30 | 94.7414 | +22 54.28 | 9.861 9370 | +9.861 7933 | +7.639 3795 | -8.260 1046 |
| 31 | 98.4864 | +18 29.84 | 9.862 0726 | +9.859 2710 | +8.899 7388 | -8.345 1900 |
| 32 | 102.2314 | +13 53.52 | 9.862 1786 | +9.852 0116 | +9.186 2719 | -8.412 3233 |
| 33 | 105.9764 | +9 8.29 | 9.862 2540 | +9.839 8567 | +9.354 2638 | -8.466 3544 |
| 34 | 109.7214 | +4 17.19 | 9.862 2779 | +9.822 5254 | +9.471 5502 | -8.510 2060 |
| 35 | 113.4664 | - 0 36.64 | 9.862 3099 | +9.799 5863 | +9.560 0170 | -8.545 7583 |
| 36 | 117.2114 | - 5 30.07 | 9.862 2899 | +9.770 4104 | +9.629 5228 | -8.574 2757 |
| 37 | 120.9564 | -10 20.01 | 9.862 2381 | +9.734 0928 | +9.685 3431 | -8.596 6294 |
| 38 | 124.7015 | -15 3.29 | 9.862 1550 | +9.689 3188 | +9.730 6171 | -8.613 4244 |
| 39 | 128.4465 | -19 36.93 | 9.862 0415 | +9.634 1256 | +9.767 3464 | -8.625 0747 |
| 40 | 132.1915 | -23 57.98 | 9.861 8988 | +9.565 4464 | +9.796 8687 | -8.631 8465 |
| 41 | 135.9365 | -28 3.60 | 9.861 7283 | +9.478 1499 | +9.820 1022 | -8.633 8851 |
| 42 | 139.6815 | -31 51.16 | 9.861 5318 | +9.362 7126 | +9.837 6839 | -8.631 2325 |
| 43 | 143.4265 | -35 18.17 | 9.861 3113 | +9.198 2317 | +9.850 0500 | -8.623 8210 |
| 44 | 147.1715 | -38 22.35 | 9.861 0693 | +8.921 4921 | +9.857 4837 | -8.611 4784 |
| 45 | 150.9166 | -41 1.70 | 9.860 8081 | +7.912 5788 | +9.860 1443 | -8.593 9051 |
| 46 | 154.6616 | -43 14.42 | 9.860 5307 | -8.827 3540 | +9.858 0817 | -8.570 6520 |
| 47 | 158.4066 | -44 58.99 | 9.860 2398 | -9.151 8035 | +9.851 2413 | -8.541 0589 |
| 48 | 162.1516 | -46 14.23 | 9.859 9388 | -9.332 3188 | +9.839 4597 | -8.504 1837 |
| 49 | 165.8966 | -46 59.22 | 9.859 6307 | -9.455 9020 | +9.822 4495 | -8.458 6539 |
| 50 | 169.6416 | -47 13.42 | 9.859 3190 | -9.548 1734 | +9.799 7714 | -8.402 4145 |
| 51 | 173.3866 | -46 56.56 | 9.859 0071 | -9.620 2216 | +9.770 7859 | -8.332 2360 |
| 52 | 177.1317 | -46 8.76 | 9.858 6983 | -9.677 8438 | +9.734 5737 | -8.242 6677 |
| 53 | 180.8767 | -44 50.45 | 9.858 3962 | -9.724 4363 | +9.689 7990 | -8.123 4525 |
| 54 | 184.6217 | -43 2.43 | 9.858 1040 | -9.762 1421 | +9.634 4660 | -7.951 5304 |
| 55 | 188.3667 | -40 45.82 | 9.857 8250 | -9.792 3808 | +9.565 4593 | -7.653 3423 |
| 56 | 192.1117 | -38 2.06 | 9.857 5624 | -9.816 1217 | +9.477 5085 | -4.949 3707 |
| 57 | 195.8567 | -34 52.90 | 9.857 3192 | -9.834 0339 | +9.300 8616 | +7.651 6300 |
| 58 | 199.6017 | -31 20.43 | 9.857 0981 | -9.846 5740 | +9.193 8645 | +7.950 6732 |
| 59 | 203.3468 | -27 26.94 | 9.856 9016 | -9.854 0381 | +8.909 8324 | +8.122 8613 |

TABLE III.

MUTUAL PERIODIC PERTURBATIONS OF VENUS AND THE EARTH.

The term of long period is omitted. The tabular unit is $0''.01$ in δu and $\delta v'$, and 10^{-8} in $\delta \rho$ and $\delta \rho'$.

| <i>i</i> | System o. | | | | System 1. | | | | System 2. | | | |
|----------|------------|-------------|---------------|----------------|------------|-------------|---------------|----------------|------------|-------------|---------------|----------------|
| | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ |
| 0 | + 239 | -169 | + 347 | +464 | + 534 | -390 | + 321 | +472 | + 543 | -402 | + 229 | +537 |
| 1 | + 65 | -151 | + 394 | +440 | + 432 | -423 | + 308 | +424 | + 545 | -507 | + 331 | +467 |
| 2 | - 146 | -116 | + 515 | +365 | + 267 | -423 | + 540 | +334 | + 479 | -573 | + 514 | +349 |
| 3 | - 406 | - 65 | + 675 | +254 | + 23 | -379 | + 716 | +214 | + 315 | -590 | + 724 | +203 |
| 4 | - 705 | + 4 | + 814 | +126 | - 295 | -303 | + 880 | + 78 | + 58 | -558 | + 910 | + 42 |
| 5 | -1018 | + 82 | + 897 | + 0 | - 662 | -194 | + 988 | - 62 | - 276 | -477 | +1045 | -117 |
| 6 | -1304 | +158 | + 898 | -111 | -1052 | - 62 | +1023 | -194 | - 659 | -357 | +1093 | -261 |
| 7 | -1541 | +219 | + 823 | -206 | -1420 | + 80 | + 941 | -308 | -1058 | -204 | +1044 | -388 |
| 8 | -1702 | +264 | + 687 | -284 | -1728 | +221 | + 779 | -397 | -1435 | - 27 | + 895 | -489 |
| 9 | -1796 | +289 | + 501 | -352 | -1941 | +348 | + 551 | -459 | -1760 | +161 | + 658 | -562 |
| 10 | -1820 | +301 | + 281 | -414 | -2049 | +449 | + 273 | -495 | -1991 | +348 | + 349 | -602 |
| 11 | -1777 | +307 | + 26 | -468 | -2047 | +522 | - 21 | -514 | -2103 | +517 | + 5 | -612 |
| 12 | -1674 | +313 | - 234 | -510 | -1950 | +566 | - 316 | -518 | -2089 | +657 | - 343 | -594 |
| 13 | -1508 | +325 | - 506 | -538 | -1767 | +589 | - 596 | -515 | -1956 | +757 | - 661 | -557 |
| 14 | -1286 | +343 | - 767 | -549 | -1517 | +599 | - 851 | -504 | -1721 | +818 | - 935 | -506 |
| 15 | -1013 | +370 | -1002 | -544 | -1211 | +605 | -1066 | -485 | -1417 | +847 | -1146 | -447 |
| 16 | - 695 | +403 | -1205 | -524 | - 857 | -1236 | -454 | -307 | -1057 | +850 | -1298 | -337 |
| 17 | - 350 | +446 | -1361 | -436 | - 475 | +610 | -1348 | -406 | - 666 | +836 | -1386 | -322 |
| 18 | + 19 | +498 | -1462 | -433 | - 77 | +611 | -1399 | -346 | - 260 | +812 | -1407 | -255 |
| 19 | + 407 | +559 | -1486 | -353 | + 320 | +613 | -1382 | -269 | + 149 | +781 | -1357 | -181 |
| 20 | + 787 | +622 | -1417 | -247 | + 701 | +614 | -1302 | -178 | + 535 | +741 | -1236 | - 99 |
| 21 | +1139 | +681 | -1244 | -113 | +1047 | +616 | -1148 | - 72 | + 883 | +695 | -1053 | - 6 |
| 22 | +1431 | +723 | - 966 | + 40 | +1351 | +617 | - 921 | + 50 | +1182 | +643 | - 825 | + 96 |
| 23 | +1629 | +740 | - 597 | +205 | +1586 | +611 | - 619 | +189 | +1417 | +586 | - 541 | +209 |
| 24 | +1709 | +725 | - 180 | +307 | +1725 | +590 | - 248 | +338 | +1578 | +524 | - 226 | +328 |
| 25 | +1660 | +682 | + 263 | +516 | +1748 | +550 | + 164 | +489 | +1652 | +458 | + 121 | +453 |
| 26 | +1489 | +606 | + 694 | +646 | +1636 | +484 | + 586 | +630 | +1623 | +380 | +488 | +578 |
| 27 | +1215 | +504 | +1074 | +752 | +1394 | +395 | + 973 | +750 | +1478 | +288 | + 846 | +695 |
| 28 | + 854 | +376 | +1381 | +836 | +1045 | +285 | +1287 | +844 | +1212 | +179 | +1162 | +799 |
| 29 | + 438 | +226 | +1583 | +890 | + 616 | +160 | +1503 | +900 | + 842 | + 56 | +1399 | +875 |
| 30 | - 9 | + 58 | +1667 | +912 | + 148 | + 24 | +1608 | +922 | + 397 | - 77 | +1532 | +918 |
| 31 | - 451 | -122 | +1616 | +898 | - 321 | -122 | +1596 | +909 | - 79 | -214 | +1544 | +923 |
| 32 | - 859 | -301 | +1439 | +843 | - 764 | -272 | +1463 | +853 | - 549 | -342 | +1437 | +887 |
| 33 | -1197 | -468 | +1142 | +755 | -1145 | -426 | +1210 | +784 | - 971 | -467 | +1213 | +815 |
| 34 | -1440 | -610 | + 765 | +637 | -1429 | -571 | + 860 | +673 | -1309 | -581 | + 896 | +709 |
| 35 | -1577 | -718 | + 336 | +502 | -1598 | -700 | + 436 | +536 | -1540 | -684 | + 501 | +576 |
| 36 | -1605 | -793 | - 103 | +355 | -1636 | -803 | - 14 | +377 | -1643 | -777 | + 66 | +420 |
| 37 | -1529 | -833 | - 524 | +204 | -1557 | -870 | - 453 | +206 | -1610 | -849 | - 378 | +247 |
| 38 | -1357 | -837 | - 911 | + 51 | -1360 | -898 | - 856 | + 33 | -1443 | -893 | - 797 | + 67 |
| 39 | -1098 | -811 | -1221 | -102 | -1085 | -889 | -1183 | -132 | -1163 | -907 | -1148 | -115 |
| 40 | - 770 | -755 | -1440 | -248 | - 747 | -844 | -1422 | -284 | - 800 | -883 | -1404 | -288 |
| 41 | - 393 | -675 | -1548 | -380 | - 370 | -770 | -1557 | -418 | - 389 | -824 | -1551 | -443 |
| 42 | - 8 | -575 | -1540 | -485 | + 19 | -669 | -1579 | -532 | + 31 | -733 | -1578 | -573 |
| 43 | + 360 | -467 | -1430 | -559 | + 395 | -547 | -1491 | -620 | + 426 | -620 | -1503 | -673 |
| 44 | + 681 | -359 | -1243 | -599 | + 730 | -410 | -1303 | -678 | + 780 | -487 | -1328 | -741 |
| 45 | + 950 | -264 | -1003 | -608 | +1002 | -269 | -1035 | -702 | +1068 | -340 | -1067 | -775 |
| 46 | +1160 | -187 | - 739 | -593 | +1192 | -135 | - 731 | -688 | +1273 | -188 | - 750 | -772 |
| 47 | +1318 | -130 | - 463 | -561 | +1302 | - 20 | - 415 | -641 | +1383 | - 38 | - 403 | -732 |
| 48 | +1424 | - 92 | - 186 | -518 | +1347 | + 68 | - 106 | -566 | +1399 | + 99 | - 59 | -656 |
| 49 | +1485 | - 69 | + 72 | -465 | +1334 | +127 | + 148 | -476 | +1335 | +212 | + 240 | -552 |
| 50 | +1497 | - 59 | + 304 | -398 | +1284 | +155 | + 367 | -374 | +1212 | +291 | + 472 | -422 |
| 51 | +1467 | - 61 | + 490 | -319 | +1206 | +160 | + 537 | -268 | +1066 | +331 | + 627 | -277 |
| 52 | +1401 | - 74 | + 641 | -232 | +1111 | +148 | + 655 | -163 | + 904 | +336 | + 709 | -129 |
| 53 | +1306 | - 95 | + 739 | -136 | +1007 | +116 | + 719 | - 55 | + 757 | +308 | + 739 | + 14 |
| 54 | +1191 | -122 | + 783 | - 38 | + 903 | + 65 | + 731 | + 52 | + 634 | +254 | + 701 | +144 |
| 55 | +1050 | -147 | + 777 | + 63 | + 799 | + 1 | + 688 | +161 | + 535 | +182 | + 627 | +264 |
| 56 | + 889 | -165 | + 717 | +168 | + 728 | - 76 | + 603 | +267 | + 467 | + 92 | + 504 | +371 |
| 57 | + 723 | -175 | + 611 | +272 | + 670 | -162 | + 494 | +362 | + 443 | - 17 | + 390 | +401 |
| 58 | + 556 | -179 | + 488 | +307 | + 630 | -251 | + 388 | +435 | + 462 | -142 | + 276 | +527 |
| 59 | + 398 | -177 | + 387 | +436 | + 591 | -329 | + 320 | +474 | + 501 | -274 | + 212 | +556 |

TABLE III.—Continued.

MUTUAL PERIODIC PERTURBATIONS OF VENUS AND THE EARTH.

The term of long period is omitted. The tabular unit is $0''.01$ in δu and $\delta v'$, and 10^{-8} in $\delta \rho$ and $\delta \rho'$.

| i | System 3. | | | | System 4. | | | | System 5. | | | |
|-----|------------|-------------|---------------|----------------|------------|-------------|---------------|----------------|------------|-------------|---------------|----------------|
| | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ |
| 0 | + 391 | - 295 | + 106 | +639 | + 249 | - 194 | - 20 | +749 | + 110 | - 87 | - 121 | +839 |
| 1 | + 452 | - 431 | + 220 | +555 | + 326 | - 337 | + 89 | +669 | + 223 | - 253 | - 31 | +777 |
| 2 | + 456 | - 543 | + 424 | +419 | + 349 | - 457 | + 293 | +533 | + 273 | - 391 | + 170 | +649 |
| 3 | + 375 | - 619 | + 667 | +251 | + 299 | - 548 | + 547 | +357 | + 245 | - 493 | + 424 | +477 |
| 4 | + 197 | - 647 | + 893 | + 66 | + 170 | - 604 | + 802 | +156 | + 128 | - 556 | + 665 | +277 |
| 5 | - 68 | - 623 | +1059 | -118 | - 38 | - 621 | +1008 | - 53 | - 65 | - 579 | + 903 | + 6 |
| 6 | - 393 | - 551 | +1132 | -287 | - 310 | - 596 | +1132 | -251 | - 314 | - 568 | +1053 | -144 |
| 7 | - 744 | - 435 | +1106 | -436 | - 614 | - 529 | +1145 | -430 | - 595 | - 524 | +1111 | -344 |
| 8 | -1097 | - 283 | + 977 | -557 | - 924 | - 421 | +1042 | -576 | - 882 | - 447 | +1062 | -523 |
| 9 | -1424 | - 103 | + 760 | -646 | -1208 | - 278 | + 838 | -688 | -1148 | - 339 | + 902 | -672 |
| 10 | -1690 | + 97 | + 463 | -701 | -1441 | - 108 | + 547 | -761 | -1362 | - 202 | + 637 | -781 |
| 11 | -1876 | + 305 | + 109 | -720 | -1604 | + 79 | + 200 | -799 | -1499 | - 44 | + 293 | -845 |
| 12 | -1958 | + 507 | - 271 | -702 | -1688 | + 276 | - 180 | -799 | -1545 | + 126 | - 95 | -863 |
| 13 | -1919 | + 692 | - 647 | -654 | -1681 | + 476 | - 563 | -765 | -1501 | + 303 | - 489 | -844 |
| 14 | -1761 | + 843 | - 977 | -578 | -1582 | + 667 | - 921 | -695 | -1372 | + 478 | - 859 | -788 |
| 15 | -1505 | + 952 | -1226 | -487 | -1393 | + 839 | -1219 | -594 | -1174 | + 648 | -1171 | -701 |
| 16 | -1173 | +1014 | -1378 | -388 | -1120 | + 979 | -1433 | -471 | - 914 | + 805 | -1412 | -588 |
| 17 | - 800 | +1035 | -1458 | -287 | - 787 | +1078 | -1541 | -332 | - 610 | + 944 | -1554 | -449 |
| 18 | - 412 | +1019 | -1448 | -188 | - 429 | +1127 | -1539 | -194 | - 284 | +1051 | -1588 | -291 |
| 19 | - 23 | + 980 | -1366 | - 95 | - 69 | +1129 | -1431 | - 62 | + 45 | +1121 | -1503 | -125 |
| 20 | + 344 | + 922 | -1219 | - 5 | + 260 | +1089 | -1245 | + 56 | + 347 | +1143 | -1313 | + 37 |
| 21 | + 679 | + 853 | -1014 | + 84 | + 547 | +1021 | - 999 | +162 | + 595 | +1120 | -1036 | +188 |
| 22 | + 967 | + 774 | - 758 | +172 | + 788 | + 931 | - 713 | +254 | + 778 | +1056 | - 706 | +313 |
| 23 | +1195 | + 682 | - 466 | +262 | + 975 | + 827 | - 403 | +340 | + 893 | + 959 | - 356 | +416 |
| 24 | +1349 | + 582 | - 151 | +353 | +1102 | + 712 | - 81 | +419 | + 942 | + 841 | - 7 | +495 |
| 25 | +1428 | + 477 | + 171 | +446 | +1161 | + 587 | + 241 | +492 | + 936 | + 710 | + 322 | +557 |
| 26 | +1427 | + 364 | + 489 | +542 | +1148 | + 449 | + 546 | +558 | + 875 | + 569 | + 623 | +609 |
| 27 | +1339 | + 248 | + 786 | +635 | +1067 | + 307 | + 817 | +617 | + 765 | + 422 | + 879 | +650 |
| 28 | +1164 | + 126 | +1059 | +726 | + 920 | + 163 | +1043 | +674 | + 608 | + 258 | +1086 | +684 |
| 29 | + 993 | - 4 | +1273 | +804 | + 719 | + 13 | +1208 | +726 | + 412 | + 107 | +1216 | +707 |
| 30 | + 562 | - 143 | +1416 | +860 | + 473 | - 138 | +1313 | +770 | + 194 | - 56 | +1278 | +720 |
| 31 | + 160 | - 288 | +1454 | +886 | + 185 | - 290 | +1341 | +803 | - 36 | - 219 | +1263 | +726 |
| 32 | - 273 | - 429 | +1379 | +876 | - 137 | - 442 | +1282 | +814 | - 269 | - 379 | +1177 | +720 |
| 33 | - 692 | - 562 | +1183 | +829 | - 472 | - 591 | +1117 | +796 | - 491 | - 536 | +1003 | +707 |
| 34 | -1052 | - 675 | + 887 | +743 | - 781 | - 730 | + 854 | +742 | - 692 | - 685 | + 773 | +676 |
| 35 | -1325 | - 764 | + 514 | +625 | -1038 | - 848 | + 500 | +652 | - 857 | - 824 | + 461 | +624 |
| 36 | -1484 | - 832 | + 96 | +479 | -1206 | - 937 | + 94 | +526 | - 966 | - 948 | + 93 | +540 |
| 37 | -1523 | - 878 | - 334 | +311 | -1269 | - 991 | - 329 | +376 | -1002 | -1047 | - 309 | +425 |
| 38 | -1427 | - 902 | - 751 | +129 | -1221 | -1007 | - 740 | +207 | - 945 | -1106 | - 718 | +281 |
| 39 | -1212 | - 906 | -1112 | - 59 | -1065 | - 991 | -1095 | + 26 | - 797 | -1124 | -1082 | +114 |
| 40 | - 888 | - 884 | -1392 | -244 | - 809 | - 946 | -1376 | -158 | - 564 | -1095 | -1373 | - 65 |
| 41 | - 482 | - 837 | -1560 | -417 | - 477 | - 880 | -1558 | -339 | - 267 | -1026 | -1562 | -242 |
| 42 | - 44 | - 759 | -1603 | -567 | - 89 | - 793 | -1622 | -507 | + 61 | - 920 | -1635 | -411 |
| 43 | + 392 | - 655 | -1524 | -689 | + 322 | - 685 | -1563 | -654 | + 408 | - 791 | -1586 | -564 |
| 44 | + 778 | - 530 | -1338 | -777 | + 715 | - 558 | -1385 | -769 | + 743 | - 643 | -1428 | -696 |
| 45 | +1095 | - 388 | -1067 | -828 | +1054 | - 418 | -1106 | -846 | +1043 | - 484 | -1159 | -800 |
| 46 | +1319 | - 240 | - 749 | -841 | +1304 | - 268 | - 762 | -880 | +1279 | - 319 | - 819 | -869 |
| 47 | +1445 | - 89 | - 392 | -815 | +1453 | - 114 | - 384 | -872 | +1429 | - 151 | - 427 | -896 |
| 48 | +1474 | + 57 | - 33 | -751 | +1495 | + 33 | - 5 | -824 | +1481 | + 12 | - 22 | -876 |
| 49 | +1405 | + 194 | + 292 | -651 | +1438 | + 170 | + 338 | -740 | +1430 | + 164 | + 349 | -813 |
| 50 | +1256 | + 311 | + 561 | -516 | +1297 | + 292 | + 618 | -620 | +1288 | + 296 | + 661 | -706 |
| 51 | +1048 | + 398 | + 741 | -354 | +1085 | + 392 | + 829 | -467 | +1078 | + 404 | + 886 | -565 |
| 52 | + 820 | + 446 | + 825 | -177 | + 836 | + 468 | + 930 | -286 | + 829 | + 484 | +1011 | -395 |
| 53 | + 609 | + 452 | + 819 | + 4 | + 575 | + 511 | + 932 | - 87 | + 564 | + 534 | +1031 | -205 |
| 54 | + 432 | + 414 | + 734 | +177 | + 342 | + 511 | + 839 | +116 | + 313 | + 551 | + 955 | - 3 |
| 55 | + 398 | + 342 | + 600 | +330 | + 159 | + 468 | + 672 | +313 | + 97 | + 534 | + 790 | +206 |
| 56 | + 237 | + 245 | + 451 | +463 | + 51 | + 385 | + 465 | +490 | - 55 | + 479 | + 556 | +411 |
| 57 | + 219 | + 127 | + 292 | +569 | + 26 | + 264 | + 246 | +629 | - 125 | + 384 | + 297 | +597 |
| 58 | + 247 | - 6 | + 161 | +640 | + 66 | + 119 | + 72 | +726 | - 105 | + 249 | + 66 | +742 |
| 59 | + 312 | - 148 | + 89 | +665 | + 151 | - 38 | - 26 | +768 | - 15 | + 87 | - 89 | +827 |

TABLE III.—Continued.

MUTUAL PERIODIC PERTURBATIONS OF VENUS AND THE EARTH.

The term of long period is omitted. The tabular unit is $0''.01$ in δu and $\delta v'$, and 10^{-8} in $\delta \rho$ and $\delta \rho'$.

| <i>i</i> | System 6. | | | | System 7. | | | | System 8. | | | |
|----------|------------|-------------|---------------|----------------|------------|-------------|---------------|----------------|------------|-------------|---------------|----------------|
| | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ |
| 0 | - 57 | + 45 | - 130 | +838 | - 225 | + 170 | - 33 | +759 | - 422 | + 319 | + 73 | +655 |
| 1 | + 73 | - 129 | - 94 | +826 | - 110 | + 5 | - 39 | +773 | - 316 | + 156 | + 59 | +682 |
| 2 | + 166 | - 292 | + 58 | +741 | - 12 | - 155 | + 56 | +726 | - 226 | - 3 | + 134 | +654 |
| 3 | + 186 | - 426 | + 296 | +596 | + 38 | - 301 | + 231 | +620 | - 177 | - 148 | + 272 | +581 |
| 4 | + 113 | - 519 | + 558 | +406 | + 21 | - 422 | + 446 | +487 | - 179 | - 273 | + 434 | +471 |
| 5 | - 55 | - 565 | + 794 | +195 | - 82 | - 509 | + 663 | +312 | - 238 | - 375 | + 596 | +334 |
| 6 | - 294 | - 565 | + 961 | - 23 | - 266 | - 552 | + 840 | +115 | - 353 | - 449 | + 733 | +178 |
| 7 | - 573 | - 526 | +1039 | -232 | - 511 | - 547 | + 943 | - 94 | - 522 | - 490 | + 827 | + 5 |
| 8 | - 860 | - 453 | +1017 | -421 | - 790 | - 493 | + 950 | -298 | - 735 | - 490 | + 845 | -175 |
| 9 | -1128 | - 351 | + 892 | -588 | -1066 | - 400 | + 855 | -483 | - 973 | - 442 | + 776 | -349 |
| 10 | -1349 | - 228 | + 668 | -723 | -1302 | - 275 | + 651 | -639 | -1201 | - 348 | + 605 | -518 |
| 11 | -1496 | - 88 | + 361 | -823 | -1470 | - 131 | + 368 | -758 | -1378 | - 217 | + 343 | -659 |
| 12 | -1549 | + 64 | - 9 | -879 | -1549 | + 23 | + 23 | -836 | -1480 | - 62 | + 13 | -762 |
| 13 | -1494 | + 223 | - 405 | -893 | -1524 | + 182 | - 352 | -876 | -1481 | + 107 | - 350 | -828 |
| 14 | -1335 | + 381 | - 790 | -860 | -1390 | + 339 | - 732 | -875 | -1378 | + 277 | - 714 | -850 |
| 15 | -1089 | + 533 | -1125 | -788 | -1150 | + 489 | -1076 | -834 | -1178 | + 440 | -1048 | -831 |
| 16 | - 775 | + 671 | -1382 | -682 | - 815 | + 624 | -1355 | -757 | - 875 | + 588 | -1327 | -774 |
| 17 | - 427 | + 796 | -1541 | -547 | - 419 | + 742 | -1534 | -640 | - 500 | + 718 | -1521 | -680 |
| 18 | - 73 | + 902 | -1592 | -396 | + 2 | + 833 | -1595 | -496 | - 75 | + 821 | -1606 | -555 |
| 19 | + 266 | + 987 | -1528 | -231 | + 409 | + 901 | -1538 | -328 | + 370 | + 895 | -1567 | -406 |
| 20 | + 563 | +1046 | -1357 | - 59 | + 759 | + 944 | -1364 | -151 | + 782 | + 934 | -1402 | -238 |
| 21 | + 799 | +1073 | -1083 | +114 | +1030 | + 966 | -1098 | + 29 | +1124 | + 941 | -1126 | - 58 |
| 22 | + 957 | +1062 | - 731 | +277 | +1205 | + 967 | - 754 | +203 | +1362 | + 920 | - 766 | +123 |
| 23 | +1023 | +1009 | - 349 | +425 | +1274 | + 943 | - 359 | +366 | +1479 | + 876 | - 356 | +298 |
| 24 | +1001 | + 919 | + 47 | +544 | +1232 | + 890 | + 40 | +512 | +1467 | + 812 | + 70 | +459 |
| 25 | + 890 | + 801 | + 412 | +632 | +1087 | + 809 | + 461 | +634 | +1333 | + 735 | + 486 | +599 |
| 26 | + 737 | + 663 | + 726 | +687 | + 842 | + 696 | + 816 | +726 | +1083 | + 641 | + 861 | +713 |
| 27 | + 540 | + 517 | + 962 | +716 | + 541 | + 565 | +1090 | +784 | + 742 | + 531 | +1165 | +795 |
| 28 | + 318 | + 366 | +1142 | +729 | + 207 | + 419 | +1266 | +809 | + 340 | + 406 | +1368 | +846 |
| 29 | + 90 | + 213 | +1251 | +728 | - 121 | + 270 | +1339 | +802 | - 91 | + 268 | +1457 | +861 |
| 30 | - 139 | + 57 | +1282 | +721 | - 422 | + 121 | +1321 | +772 | - 498 | + 126 | +1428 | +843 |
| 31 | - 359 | - 102 | +1236 | +705 | - 677 | - 23 | +1230 | +727 | - 849 | - 11 | +1294 | +796 |
| 32 | - 562 | - 262 | +1118 | +679 | - 884 | - 164 | +1071 | +673 | -1126 | - 140 | +1084 | +726 |
| 33 | - 731 | - 422 | + 926 | +645 | -1037 | - 306 | + 855 | +615 | -1312 | - 260 | + 813 | +642 |
| 34 | - 852 | - 574 | + 675 | +599 | -1128 | - 445 | + 589 | +553 | -1406 | - 370 | + 510 | +548 |
| 35 | - 923 | - 718 | + 374 | +545 | -1153 | - 579 | + 284 | +487 | -1418 | - 474 | + 187 | +453 |
| 36 | - 935 | - 852 | + 39 | +480 | -1108 | - 709 | - 40 | +414 | -1346 | - 577 | - 136 | +357 |
| 37 | - 886 | - 972 | - 315 | +399 | - 991 | - 828 | - 365 | +334 | -1202 | - 676 | - 449 | +265 |
| 38 | - 773 | -1071 | - 683 | +300 | - 803 | - 933 | - 688 | +246 | - 982 | - 767 | - 743 | +177 |
| 39 | - 589 | -1143 | -1024 | +178 | - 558 | -1024 | - 983 | +150 | - 697 | - 850 | - 997 | + 88 |
| 40 | - 335 | -1177 | -1317 | + 33 | - 262 | -1093 | -1240 | + 45 | - 362 | - 920 | -1203 | - 3 |
| 41 | - 28 | -1165 | -1526 | -130 | + 79 | -1139 | -1436 | - 72 | + 12 | - 977 | -1354 | - 96 |
| 42 | + 313 | -1100 | -1622 | -297 | + 450 | -1147 | -1550 | -201 | + 407 | -1017 | -1438 | -192 |
| 43 | + 650 | - 989 | -1599 | -458 | + 825 | -1112 | -1556 | -337 | + 808 | -1036 | -1454 | -291 |
| 44 | + 959 | - 837 | -1456 | -600 | +1172 | -1024 | -1451 | -473 | +1190 | -1024 | -1381 | -393 |
| 45 | +1215 | - 658 | -1207 | -717 | +1462 | - 887 | -1233 | -599 | +1535 | - 974 | -1213 | -491 |
| 46 | +1400 | - 466 | - 881 | -801 | +1660 | - 709 | - 930 | -703 | +1805 | - 878 | - 961 | -581 |
| 47 | +1505 | - 269 | - 406 | -850 | +1753 | - 502 | - 564 | -773 | +1974 | - 737 | - 629 | -655 |
| 48 | +1524 | - 77 | - 87 | -863 | +1738 | - 285 | - 167 | -807 | +2021 | - 555 | - 248 | -705 |
| 49 | +1454 | + 106 | + 307 | -837 | +1629 | - 67 | + 222 | -803 | +1941 | - 342 | + 135 | -725 |
| 50 | +1268 | + 270 | + 651 | -769 | +1433 | + 137 | + 576 | -758 | +1741 | - 125 | + 488 | -706 |
| 51 | +1070 | + 407 | + 909 | -653 | +1168 | + 319 | + 866 | -675 | +1450 | + 91 | + 785 | -650 |
| 52 | + 802 | + 513 | +1062 | -500 | + 861 | + 471 | +1063 | -556 | +1100 | + 287 | + 998 | -555 |
| 53 | + 521 | + 582 | +1101 | -316 | + 534 | + 586 | +1151 | -403 | + 720 | + 454 | +1118 | -425 |
| 54 | + 256 | + 610 | +1045 | -117 | + 225 | + 654 | +1129 | -225 | + 346 | + 580 | +1138 | -271 |
| 55 | + 34 | + 599 | + 890 | + 93 | - 43 | + 677 | + 988 | - 27 | + 7 | + 662 | +1051 | - 97 |
| 56 | - 135 | + 553 | + 671 | +299 | - 239 | + 651 | + 773 | +180 | - 266 | + 693 | + 875 | + 90 |
| 57 | - 224 | + 472 | + 414 | +491 | - 348 | + 579 | + 520 | +379 | - 446 | + 670 | + 639 | +273 |
| 58 | - 237 | + 356 | + 163 | +656 | - 371 | + 467 | + 272 | +552 | - 522 | + 592 | + 392 | +440 |
| 59 | - 174 | + 212 | - 33 | +776 | - 322 | + 328 | + 76 | +683 | - 504 | + 471 | + 188 | +572 |

TABLE III.—*Concluded.*

MUTUAL PERIODIC PERTURBATIONS OF VENUS AND THE EARTH.

The term of long period is omitted. The tabular unit is $0''.01$ in δu and $\delta v'$, and 10^{-8} in $\delta \rho$ and $\delta \rho'$.

| <i>i</i> | System 9. | | | | System 10. | | | | System 11. | | | |
|----------|------------|-------------|---------------|----------------|------------|-------------|---------------|----------------|------------|-------------|---------------|----------------|
| | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ | δu | $\delta v'$ | $\delta \rho$ | $\delta \rho'$ |
| 0 | - 598 | +447 | + 196 | +563 | - 548 | +407 | + 300 | +495 | - 205 | +158 | + 341 | +471 |
| 1 | - 544 | +318 | + 174 | +583 | - 616 | +355 | + 295 | +506 | - 371 | +169 | + 372 | +454 |
| 2 | - 482 | +176 | + 237 | +552 | - 660 | +285 | + 355 | +469 | - 540 | +175 | + 468 | +393 |
| 3 | - 444 | + 36 | + 357 | +487 | - 698 | +200 | + 465 | +398 | - 718 | +179 | + 591 | +366 |
| 4 | - 446 | - 90 | + 493 | +394 | - 747 | +109 | + 579 | +301 | - 897 | +176 | + 700 | +207 |
| 5 | - 493 | -196 | + 613 | +285 | - 811 | + 19 | + 673 | +193 | -1066 | +165 | + 767 | +103 |
| 6 | - 576 | -278 | + 699 | +162 | - 889 | - 62 | + 727 | + 82 | -1208 | +141 | + 783 | + 0 |
| 7 | - 690 | -338 | + 744 | + 26 | - 980 | -127 | + 732 | - 32 | -1321 | +109 | + 757 | -104 |
| 8 | - 828 | -370 | + 736 | -121 | -1073 | -171 | + 681 | -142 | -1409 | + 77 | + 662 | -205 |
| 9 | - 981 | -371 | + 667 | -272 | -1104 | -194 | + 577 | -254 | -1470 | + 51 | + 516 | -300 |
| 10 | -1138 | -335 | + 522 | -420 | -1249 | -193 | + 416 | -364 | -1497 | + 39 | + 342 | -384 |
| 11 | -1274 | -260 | + 298 | -553 | -1290 | -166 | + 203 | -472 | -1484 | + 41 | + 114 | -456 |
| 12 | -1360 | -147 | - 3 | -661 | -1310 | -113 | - 60 | -569 | -1423 | + 59 | - 147 | -517 |
| 13 | -1372 | - 1 | - 351 | -740 | -1274 | - 29 | - 364 | -648 | -1314 | + 95 | - 427 | -566 |
| 14 | -1288 | +164 | - 715 | -783 | -1176 | + 83 | - 693 | -699 | -1154 | +147 | - 711 | -603 |
| 15 | -1106 | +339 | -1055 | -786 | -1000 | +222 | -1015 | -716 | - 938 | +220 | - 987 | -624 |
| 16 | - 835 | +504 | -1328 | -753 | - 741 | +374 | -1301 | -695 | - 669 | +311 | -1237 | -620 |
| 17 | - 493 | +654 | -1520 | -682 | - 415 | +530 | -1511 | -637 | - 346 | +420 | -1438 | -583 |
| 18 | - 106 | +779 | -1609 | -576 | - 40 | +671 | -1617 | -549 | + 19 | +536 | -1561 | -510 |
| 19 | + 308 | +876 | -1582 | -440 | + 353 | +791 | -1605 | -431 | + 413 | +651 | -1579 | -403 |
| 20 | + 710 | +938 | -1438 | -282 | + 726 | +878 | -1469 | -293 | + 793 | +749 | -1479 | -270 |
| 21 | +1072 | +964 | -1180 | -108 | +1049 | +933 | -1225 | -135 | +1126 | +821 | -1260 | -116 |
| 22 | +1359 | +948 | - 820 | + 68 | +1323 | +949 | - 880 | + 33 | +1387 | +862 | - 940 | + 40 |
| 23 | +1532 | +899 | - 399 | +242 | +1501 | +927 | - 467 | +207 | +1547 | +867 | - 544 | +202 |
| 24 | +1580 | +816 | + 54 | +405 | +1572 | +863 | - 13 | +376 | +1600 | +835 | - 101 | +359 |
| 25 | +1493 | +711 | + 494 | +551 | +1525 | +765 | + 446 | +530 | +1546 | +769 | + 355 | +509 |
| 26 | +1278 | +592 | + 885 | +677 | +1353 | +632 | + 872 | +659 | +1379 | +667 | + 791 | +644 |
| 27 | + 957 | +466 | +1210 | +778 | +1070 | +479 | +1221 | +759 | +1116 | +533 | +1174 | +757 |
| 28 | + 558 | +336 | +1436 | +849 | + 701 | +316 | +1471 | +833 | + 766 | +372 | +1460 | +841 |
| 29 | + 106 | +205 | +1545 | +884 | + 271 | +153 | +1600 | +874 | + 353 | +192 | +1627 | +837 |
| 30 | - 355 | + 73 | +1534 | +883 | - 179 | - 1 | +1609 | +886 | - 84 | + 6 | +1659 | +896 |
| 31 | - 791 | - 59 | +1404 | +848 | - 621 | -142 | +1501 | +867 | - 515 | -171 | +1565 | +870 |
| 32 | -1164 | -183 | +1169 | +780 | -1026 | -270 | +1278 | +815 | - 909 | -330 | +1357 | +814 |
| 33 | -1439 | -297 | + 861 | +660 | -1358 | -383 | + 961 | +733 | -1234 | -466 | +1050 | +735 |
| 34 | -1594 | -393 | + 497 | +581 | -1592 | -477 | + 574 | +621 | -1476 | -573 | + 673 | +632 |
| 35 | -1633 | -471 | + 134 | +465 | -1704 | -550 | + 154 | +491 | -1629 | -652 | + 250 | +511 |
| 36 | -1560 | -537 | - 225 | +345 | -1684 | -602 | - 256 | +351 | -1661 | -707 | - 183 | +370 |
| 37 | -1402 | -594 | - 544 | +226 | -1549 | -630 | - 620 | +209 | -1579 | -733 | - 596 | +216 |
| 38 | -1173 | -645 | - 818 | +115 | -1317 | -639 | - 923 | + 77 | -1384 | -730 | - 959 | + 60 |
| 39 | - 879 | -694 | -1058 | + 11 | -1017 | -637 | -1149 | - 43 | -1098 | -703 | -1232 | - 89 |
| 40 | - 540 | -740 | -1237 | - 84 | - 674 | -631 | -1301 | -150 | - 752 | -654 | -1403 | -219 |
| 41 | - 159 | -783 | -1347 | -169 | - 303 | -627 | -1384 | -244 | - 375 | -595 | -1473 | -324 |
| 42 | + 244 | -813 | -1390 | -245 | + 80 | -626 | -1396 | -324 | + 3 | -532 | -1450 | -403 |
| 43 | + 651 | -838 | -1365 | -315 | + 465 | -626 | -1342 | -391 | + 364 | -477 | -1357 | -462 |
| 44 | +1039 | -849 | -1275 | -383 | + 835 | -623 | -1225 | -442 | + 697 | -432 | -1208 | -504 |
| 45 | +1399 | -845 | -1121 | -449 | +1181 | -617 | -1049 | -478 | +1001 | -366 | -1009 | -531 |
| 46 | +1708 | -821 | - 911 | -509 | +1482 | -607 | - 832 | -502 | +1264 | -368 | - 778 | -542 |
| 47 | +1946 | -768 | - 642 | -562 | +1728 | -591 | - 580 | -517 | +1480 | -346 | - 520 | -536 |
| 48 | +2089 | -681 | - 322 | -601 | +1908 | -566 | - 303 | -526 | +1640 | -328 | - 248 | -515 |
| 49 | +2122 | -555 | + 27 | -621 | +2014 | -524 | - 15 | -527 | +1743 | -312 | + 17 | -481 |
| 50 | +2026 | -393 | + 372 | -611 | +2027 | -460 | + 276 | -514 | +1784 | -298 | + 265 | -434 |
| 51 | +1803 | -207 | + 678 | -570 | +1939 | -371 | + 548 | -479 | +1761 | -283 | + 487 | -378 |
| 52 | +1482 | - 11 | + 912 | -499 | +1744 | -254 | + 779 | -418 | +1679 | -259 | + 673 | -314 |
| 53 | +1093 | +178 | +1054 | -396 | +1454 | -116 | + 942 | -327 | +1528 | -221 | + 813 | -236 |
| 54 | + 679 | +344 | +1097 | -269 | +1097 | + 27 | +1017 | -213 | +1313 | -169 | + 895 | -145 |
| 55 | + 279 | +477 | +1042 | -117 | + 709 | +166 | + 995 | - 80 | +1044 | -101 | + 900 | - 31 |
| 56 | - 71 | +569 | + 906 | + 49 | + 331 | +284 | + 884 | + 66 | + 743 | - 27 | + 825 | +100 |
| 57 | - 344 | +612 | + 710 | +217 | + 3 | +371 | - 716 | +209 | + 451 | + 43 | + 685 | +234 |
| 58 | - 523 | +603 | + 497 | +370 | - 254 | +418 | + 536 | +337 | + 189 | + 99 | + 525 | +354 |
| 59 | - 601 | +548 | + 312 | +489 | - 434 | +430 | + 385 | +437 | - 27 | +137 | + 397 | +437 |

TABLE IVa.
PERTURBATIONS OF THE G-COÖRDINATE X OF VENUS.

The tabular unit is 10⁻⁸.

| System <i>i</i> | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------------|------|------|------|------|------|------|------|------|------|------|------|------|
| 0 | + 47 | + 57 | + 92 | +137 | +181 | +217 | +218 | +184 | +142 | +107 | + 71 | + 52 |
| 1 | + 37 | + 50 | + 81 | +118 | +159 | +197 | +212 | +183 | +140 | + 92 | + 52 | + 30 |
| 2 | - 11 | + 11 | + 41 | + 71 | +109 | +149 | +176 | +158 | +114 | + 59 | + 8 | - 23 |
| 3 | - 92 | - 59 | - 24 | + 5 | + 39 | + 75 | +112 | +111 | + 72 | + 9 | - 52 | - 97 |
| 4 | -193 | -154 | -111 | - 79 | - 50 | - 14 | + 26 | + 46 | + 14 | - 48 | -122 | -183 |
| 5 | -305 | -269 | -217 | -183 | -156 | -122 | - 79 | - 41 | - 55 | -111 | -191 | -268 |
| 6 | -412 | -396 | -338 | -290 | -267 | -237 | -197 | -146 | -136 | -179 | -261 | -348 |
| 7 | -506 | -519 | -465 | -405 | -380 | -354 | -318 | -263 | -230 | -251 | -326 | -421 |
| 8 | -581 | -628 | -586 | -519 | -487 | -468 | -437 | -384 | -331 | -330 | -386 | -482 |
| 9 | -636 | -715 | -696 | -629 | -583 | -569 | -546 | -502 | -437 | -410 | -443 | -530 |
| 10 | -668 | -763 | -780 | -718 | -661 | -650 | -636 | -599 | -539 | -488 | -494 | -565 |
| 11 | -674 | -777 | -827 | -783 | -718 | -699 | -697 | -672 | -619 | -556 | -534 | -582 |
| 12 | -660 | -759 | -828 | -814 | -745 | -714 | -722 | -710 | -669 | -606 | -561 | -580 |
| 13 | -621 | -710 | -790 | -803 | -745 | -699 | -707 | -712 | -682 | -625 | -569 | -560 |
| 14 | -559 | -639 | -713 | -749 | -709 | -652 | -652 | -671 | -659 | -610 | -552 | -523 |
| 15 | -479 | -541 | -614 | -659 | -640 | -580 | -564 | -591 | -596 | -559 | -507 | -466 |
| 16 | -383 | -431 | -495 | -542 | -540 | -487 | -452 | -475 | -496 | -476 | -432 | -389 |
| 17 | -279 | -308 | -364 | -410 | -417 | -374 | -325 | -337 | -368 | -366 | -331 | -298 |
| 18 | -171 | -183 | -231 | -273 | -283 | -251 | -195 | -187 | -221 | -236 | -213 | -187 |
| 19 | - 54 | - 61 | - 98 | -137 | -149 | -123 | - 68 | - 38 | - 66 | - 95 | - 84 | - 64 |
| 20 | + 60 | + 56 | + 25 | - 13 | - 26 | - 1 | + 48 | + 93 | + 80 | + 46 | + 41 | + 58 |
| 21 | +170 | +160 | +136 | +100 | + 82 | +106 | +151 | +203 | +209 | +179 | +155 | +171 |
| 22 | +269 | +253 | +229 | +197 | +174 | +192 | +236 | +288 | +312 | +291 | +262 | +266 |
| 23 | +350 | +330 | +305 | +275 | +249 | +259 | +299 | +350 | +384 | +377 | +348 | +342 |
| 24 | +406 | +392 | +363 | +333 | +307 | +306 | +341 | +387 | +430 | +434 | +412 | +398 |
| 25 | +441 | +436 | +407 | +373 | +347 | +338 | +367 | +412 | +451 | +466 | +456 | +437 |
| 26 | +461 | +460 | +435 | +400 | +374 | +361 | +378 | +418 | +457 | +475 | +476 | +464 |
| 27 | +468 | +471 | +451 | +417 | +388 | +372 | +380 | +418 | +454 | +478 | +483 | +478 |
| 28 | +476 | +475 | +459 | +426 | +394 | +381 | +379 | +411 | +447 | +472 | +481 | +484 |
| 29 | +480 | +475 | +463 | +432 | +397 | +381 | +379 | +405 | +440 | +465 | +475 | +485 |
| 30 | +484 | +479 | +467 | +438 | +401 | +380 | +380 | +401 | +434 | +459 | +473 | +479 |
| 31 | +490 | +484 | +476 | +445 | +406 | +380 | +380 | +397 | +431 | +457 | +470 | +476 |
| 32 | +491 | +492 | +483 | +455 | +414 | +380 | +379 | +392 | +426 | +456 | +469 | +473 |
| 33 | +485 | +497 | +488 | +460 | +417 | +379 | +375 | +387 | +419 | +451 | +467 | +466 |
| 34 | +468 | +492 | +489 | +463 | +420 | +377 | +362 | +375 | +403 | +437 | +456 | +456 |
| 35 | +439 | +468 | +479 | +458 | +414 | +366 | +341 | +354 | +377 | +411 | +432 | +436 |
| 36 | +397 | +426 | +448 | +437 | +392 | +342 | +310 | +314 | +338 | +368 | +391 | +399 |
| 37 | +340 | +360 | +394 | +396 | +353 | +301 | +262 | +260 | +282 | +311 | +331 | +343 |
| 38 | +263 | +270 | +309 | +327 | +293 | +240 | +196 | +184 | +208 | +236 | +255 | +264 |
| 39 | +167 | +166 | +199 | +230 | +211 | +155 | +109 | + 90 | +112 | +141 | +161 | +166 |
| 40 | + 56 | + 47 | + 69 | +107 | +104 | + 51 | + 2 | - 20 | - 4 | + 33 | + 55 | + 57 |
| 41 | - 67 | - 80 | - 74 | - 38 | - 22 | - 67 | -121 | -145 | -127 | - 90 | - 59 | - 58 |
| 42 | -188 | -206 | -215 | -188 | -161 | -192 | -254 | -283 | -265 | -222 | -180 | -172 |
| 43 | -301 | -325 | -344 | -336 | -306 | -310 | -381 | -420 | -407 | -357 | -304 | -282 |
| 44 | -397 | -430 | -459 | -404 | -443 | -438 | -494 | -549 | -543 | -486 | -423 | -385 |
| 45 | -473 | -510 | -545 | -568 | -557 | -544 | -589 | -656 | -665 | -609 | -534 | -475 |
| 46 | -528 | -560 | -605 | -634 | -638 | -626 | -655 | -729 | -760 | -712 | -628 | -555 |
| 47 | -566 | -578 | -626 | -665 | -681 | -678 | -694 | -764 | -818 | -791 | -702 | -617 |
| 48 | -585 | -574 | -611 | -660 | -685 | -692 | -703 | -759 | -833 | -833 | -749 | -657 |
| 49 | -588 | -547 | -566 | -619 | -653 | -668 | -679 | -723 | -805 | -838 | -775 | -675 |
| 50 | -572 | -508 | -506 | -549 | -588 | -609 | -627 | -659 | -737 | -796 | -766 | -668 |
| 51 | -539 | -457 | -431 | -454 | -499 | -525 | -545 | -571 | -639 | -716 | -723 | -639 |
| 52 | -491 | -401 | -347 | -350 | -391 | -423 | -447 | -470 | -525 | -605 | -644 | -589 |
| 53 | -431 | -339 | -268 | -248 | -276 | -311 | -333 | -357 | -401 | -477 | -535 | -518 |
| 54 | -362 | -274 | -193 | -152 | -162 | -197 | -222 | -247 | -281 | -346 | -414 | -428 |
| 55 | -283 | -205 | -122 | - 69 | - 58 | - 88 | -111 | -137 | -167 | -219 | -286 | -324 |
| 56 | -199 | -134 | - 58 | + 2 | + 31 | + 14 | - 14 | - 37 | - 64 | -106 | -164 | -211 |
| 57 | -114 | - 67 | - 3 | + 60 | +101 | +102 | + 73 | + 48 | + 20 | - 14 | - 60 | -105 |
| 58 | - 38 | - 8 | + 44 | +104 | +151 | +167 | +144 | +115 | + 85 | + 54 | + 16 | - 18 |
| 59 | + 19 | + 36 | + 78 | +130 | +179 | +208 | +194 | +161 | +128 | + 94 | + 59 | + 36 |

TABLE IVb.

PERTURBATIONS OF THE G-COÖRDINATE Y OF VENUS.

The tabular unit is 10^{-8} .

| Sys- tem <i>i</i> | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| 0 | -164 | -370 | -379 | -274 | -176 | -78 | +42 | +160 | +300 | +423 | +385 | +146 |
| 1 | -100 | -357 | -436 | -365 | -275 | -199 | -87 | +39 | +181 | +337 | +377 | +202 |
| 2 | -22 | -310 | -454 | -430 | -350 | -290 | -203 | -77 | +68 | +239 | +348 | +251 |
| 3 | +70 | -224 | -424 | -458 | -394 | -345 | -287 | -175 | -30 | +145 | +304 | +294 |
| 4 | +172 | -111 | -350 | -438 | -405 | -360 | -330 | -246 | -108 | +65 | +252 | +324 |
| 5 | +273 | +22 | -236 | -373 | -378 | -341 | -328 | -281 | -162 | +3 | +200 | +339 |
| 6 | +355 | +164 | -97 | -272 | -318 | -294 | -289 | -277 | -190 | -38 | +154 | +334 |
| 7 | +410 | +298 | +53 | -148 | -231 | -228 | -225 | -239 | -193 | -65 | +115 | +313 |
| 8 | +435 | +406 | +202 | -11 | -124 | -146 | -144 | -171 | -167 | -72 | +89 | +286 |
| 9 | +436 | +481 | +340 | +131 | -6 | -54 | -59 | -87 | -114 | -62 | +73 | +258 |
| 10 | +415 | +523 | +452 | +267 | +114 | +46 | +32 | +7 | -38 | -31 | +70 | +232 |
| 11 | +389 | +531 | +533 | +390 | +230 | +146 | +120 | +98 | +49 | +19 | +78 | +214 |
| 12 | +361 | +519 | +583 | +490 | +339 | +244 | +205 | +185 | +139 | +86 | +101 | +205 |
| 13 | +339 | +495 | +602 | +571 | +442 | +338 | +290 | +267 | +227 | +165 | +142 | +207 |
| 14 | +331 | +472 | +600 | +626 | +533 | +429 | +372 | +348 | +315 | +254 | +201 | +229 |
| 15 | +339 | +457 | +590 | +660 | +610 | +515 | +454 | +427 | +399 | +348 | +279 | +268 |
| 16 | +363 | +457 | +579 | +673 | +673 | +597 | +536 | +508 | +484 | +440 | +371 | +329 |
| 17 | +406 | +472 | +575 | +679 | +721 | +673 | +615 | +588 | +568 | +534 | +473 | +409 |
| 18 | +469 | +502 | +582 | +678 | +749 | +738 | +690 | +667 | +650 | +624 | +579 | +505 |
| 19 | +550 | +548 | +602 | +680 | +760 | +787 | +757 | +735 | +729 | +710 | +675 | +610 |
| 20 | +639 | +606 | +629 | +685 | +759 | +812 | +809 | +792 | +793 | +786 | +761 | +710 |
| 21 | +729 | +668 | +660 | +692 | +747 | +814 | +837 | +832 | +837 | +845 | +829 | +795 |
| 22 | +804 | +729 | +691 | +698 | +729 | +788 | +835 | +847 | +858 | +877 | +875 | +855 |
| 23 | +848 | +779 | +715 | +696 | +704 | +743 | +799 | +830 | +846 | +875 | +888 | +880 |
| 24 | +854 | +801 | +725 | +681 | +671 | +681 | +729 | +778 | +801 | +833 | +861 | +864 |
| 25 | +812 | +786 | +717 | +653 | +621 | +606 | +630 | +683 | +717 | +752 | +792 | +809 |
| 26 | +723 | +722 | +676 | +602 | +552 | +517 | +510 | +551 | +594 | +632 | +676 | +710 |
| 27 | +594 | +609 | +593 | +531 | +405 | +416 | +383 | +397 | +441 | +478 | +522 | +567 |
| 28 | +428 | +455 | +467 | +428 | +360 | +297 | +248 | +228 | +262 | +301 | +341 | +390 |
| 29 | +237 | +269 | +301 | +295 | +239 | +174 | +113 | +66 | +70 | +106 | +138 | +187 |
| 30 | +26 | +67 | +107 | +132 | +100 | +40 | -22 | -90 | -116 | -92 | -65 | -27 |
| 31 | -187 | -142 | -099 | -54 | -51 | -98 | -155 | -227 | -280 | -283 | -261 | -235 |
| 32 | -388 | -340 | -300 | -250 | -216 | -237 | -284 | -346 | -416 | -449 | -440 | -424 |
| 33 | -565 | -523 | -484 | -439 | -389 | -375 | -403 | -451 | -520 | -580 | -589 | -582 |
| 34 | -702 | -673 | -637 | -602 | -547 | -505 | -509 | -538 | -594 | -667 | -702 | -703 |
| 35 | -796 | -785 | -754 | -729 | -685 | -625 | -601 | -609 | -644 | -711 | -770 | -787 |
| 36 | -846 | -852 | -835 | -814 | -789 | -728 | -679 | -664 | -675 | -723 | -788 | -829 |
| 37 | -857 | -875 | -872 | -860 | -850 | -807 | -743 | -704 | -691 | -712 | -774 | -830 |
| 38 | -832 | -857 | -869 | -867 | -809 | -850 | -791 | -729 | -695 | -688 | -729 | -794 |
| 39 | -779 | -810 | -833 | -840 | -850 | -858 | -820 | -749 | -690 | -659 | -669 | -729 |
| 40 | -704 | -741 | -769 | -787 | -802 | -835 | -827 | -761 | -685 | -631 | -608 | -647 |
| 41 | -613 | -659 | -690 | -713 | -736 | -778 | -810 | -767 | -682 | -607 | -554 | -551 |
| 42 | -518 | -568 | -601 | -629 | -655 | -704 | -766 | -763 | -680 | -589 | -512 | -483 |
| 43 | -428 | -475 | -513 | -539 | -568 | -618 | -702 | -743 | -685 | -582 | -484 | -421 |
| 44 | -350 | -383 | -426 | -452 | -478 | -528 | -622 | -705 | -689 | -586 | -468 | -379 |
| 45 | -289 | -299 | -341 | -369 | -393 | -435 | -530 | -645 | -681 | -597 | -469 | -353 |
| 46 | -249 | -226 | -260 | -291 | -310 | -344 | -432 | -569 | -659 | -612 | -480 | -345 |
| 47 | -227 | -168 | -183 | -214 | -229 | -254 | -329 | -472 | -610 | -618 | -499 | -352 |
| 48 | -220 | -126 | -111 | -139 | -152 | -166 | -223 | -360 | -532 | -606 | -521 | -363 |
| 49 | -227 | -103 | -47 | -64 | -77 | -79 | -116 | -235 | -425 | -566 | -535 | -387 |
| 50 | -240 | -94 | -3 | +9 | -2 | +8 | -10 | -104 | -295 | -488 | -530 | -410 |
| 51 | -258 | -96 | +25 | +75 | +74 | +88 | +97 | +30 | -148 | -377 | -497 | -424 |
| 52 | -278 | -105 | +40 | +124 | +143 | +163 | +192 | +160 | +8 | -235 | -427 | -427 |
| 53 | -297 | -124 | +35 | +151 | +200 | +226 | +270 | +276 | +161 | -77 | -324 | -407 |
| 54 | -314 | -150 | +13 | +151 | +234 | +272 | +327 | +368 | +299 | +84 | -194 | -359 |
| 55 | -319 | -184 | -21 | +124 | +237 | +298 | +358 | +428 | +409 | +235 | -49 | -285 |
| 56 | -311 | -226 | -68 | +74 | +205 | +291 | +360 | +449 | +483 | +351 | +92 | -192 |
| 57 | -290 | -273 | -132 | +8 | +136 | +247 | +329 | +427 | +509 | +448 | +215 | -94 |
| 58 | -257 | -319 | -212 | -77 | +42 | +164 | +264 | +365 | +481 | +487 | +305 | +1 |
| 59 | -215 | -355 | -298 | -173 | -66 | +50 | +165 | +274 | +407 | +477 | +361 | +81 |

TABLE V.

RECTANGULAR G-COÖRDINATES X AND Y OF VENUS, REFERRED, IN EACH SYSTEM, TO AN AXIS OF X PASSING THROUGH THE MEAN SUN.

| <i>i</i> | System 0. | | System 1. | | System 2. | |
|----------|-------------|-------------|-------------|-------------|-------------|-------------|
| | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> |
| 0 | +0.264 4388 | +0.005 3159 | +0.267 8642 | +0.017 2810 | +0.273 5960 | +0.024 1368 |
| 1 | +0.268 2411 | -0.070 6564 | +0.271 9461 | -0.058 8025 | +0.277 8772 | -0.051 8927 |
| 2 | +0.280 0227 | -0.145 8383 | +0.284 0031 | -0.134 0369 | +0.290 1029 | -0.127 0162 |
| 3 | +0.299 6585 | -0.219 3893 | +0.303 8978 | -0.207 5810 | +0.310 1265 | -0.200 3988 |
| 4 | +0.326 9346 | -0.290 4863 | +0.331 4038 | -0.278 6154 | +0.337 7133 | -0.271 2285 |
| 5 | +0.361 5487 | -0.358 3344 | +0.366 2082 | -0.346 3496 | +0.372 5452 | -0.338 7248 |
| 6 | +0.403 1159 | -0.422 1763 | +0.407 9159 | -0.410 0328 | +0.414 2234 | -0.402 1483 |
| 7 | +0.451 1712 | -0.481 2993 | +0.456 0557 | -0.468 9619 | +0.462 2754 | -0.460 8077 |
| 8 | +0.505 1754 | -0.535 0445 | +0.510 0841 | -0.522 4898 | +0.516 1594 | -0.514 0671 |
| 9 | +0.564 5219 | -0.582 8139 | +0.569 3924 | -0.570 0313 | +0.575 2710 | -0.561 3528 |
| 10 | +0.628 5438 | -0.624 0792 | +0.633 3160 | -0.611 0692 | +0.638 9518 | -0.602 1602 |
| 11 | +0.696 5229 | -0.658 3852 | +0.701 1382 | -0.645 1617 | +0.706 4955 | -0.636 0564 |
| 12 | +0.767 6965 | -0.685 3576 | +0.772 1023 | -0.671 9440 | +0.777 1566 | -0.662 6856 |
| 13 | +0.841 2692 | -0.704 7061 | +0.845 4198 | -0.691 1353 | +0.850 1572 | -0.681 7730 |
| 14 | +0.916 4199 | -0.716 2270 | +0.920 2784 | -0.702 5389 | +0.924 6978 | -0.693 1251 |
| 15 | +0.992 3125 | -0.719 8055 | +0.995 8539 | -0.706 0456 | +0.999 9648 | -0.696 6325 |
| 16 | +1.068 1057 | -0.715 4169 | +1.071 3157 | -0.701 6335 | +1.075 1404 | -0.692 2716 |
| 17 | +1.142 9619 | -0.703 1247 | +1.145 8394 | -0.689 3674 | +1.149 4106 | -0.680 1025 |
| 18 | +1.216 0577 | -0.683 0801 | +1.218 6136 | -0.669 3977 | +1.221 9735 | -0.660 2691 |
| 19 | +1.286 5933 | -0.655 5200 | +1.288 8493 | -0.641 9577 | +1.292 0488 | -0.632 9963 |
| 20 | +1.353 7991 | -0.620 7640 | +1.355 7887 | -0.607 3599 | +1.358 8839 | -0.598 5883 |
| 21 | +1.416 9464 | -0.579 2086 | +1.418 7118 | -0.565 9943 | +1.421 7633 | -0.557 4240 |
| 22 | +1.475 3529 | -0.531 3238 | +1.476 9448 | -0.518 3206 | +1.480 0138 | -0.509 9523 |
| 23 | +1.528 3911 | -0.477 6470 | +1.529 8660 | -0.464 8651 | +1.533 0133 | -0.456 6884 |
| 24 | +1.575 4942 | -0.418 7748 | +1.576 9123 | -0.406 2148 | +1.580 1954 | -0.398 2084 |
| 25 | +1.616 1628 | -0.355 3577 | +1.617 5843 | -0.343 0090 | +1.621 0558 | -0.335 1418 |
| 26 | +1.649 9691 | -0.288 0919 | +1.651 4516 | -0.275 9346 | +1.655 1564 | -0.268 1673 |
| 27 | +1.676 5593 | -0.217 7116 | +1.678 1568 | -0.205 7162 | +1.682 1302 | -0.198 0049 |
| 28 | +1.695 6592 | -0.144 9820 | +1.697 4188 | -0.133 1099 | +1.701 6857 | -0.125 4065 |
| 29 | +1.707 0734 | -0.070 6903 | +1.709 0351 | -0.058 8960 | +1.713 6087 | -0.051 1511 |
| 30 | +1.710 6894 | +0.004 3615 | +1.712 8842 | +0.016 1297 | +1.717 7659 | +0.023 9552 |
| 31 | +1.706 4775 | +0.079 3664 | +1.708 9249 | +0.091 1628 | +1.714 1050 | +0.099 1360 |
| 32 | +1.694 4891 | +0.153 5190 | +1.697 1090 | +0.165 3988 | +1.702 6556 | +0.173 5529 |
| 33 | +1.674 8587 | +0.226 0244 | +1.677 8288 | +0.238 0408 | +1.683 5308 | +0.246 4124 |
| 34 | +1.647 8008 | +0.296 1060 | +1.651 0177 | +0.308 3085 | +1.656 9253 | +0.316 9261 |
| 35 | +1.613 6080 | +0.363 0127 | +1.617 0473 | +0.375 4452 | +1.623 1144 | +0.384 3269 |
| 36 | +1.572 6476 | +0.426 0265 | +1.576 2761 | +0.438 7253 | +1.582 4506 | +0.447 8781 |
| 37 | +1.525 3583 | +0.484 4694 | +1.529 1350 | +0.497 4622 | +1.535 3622 | +0.506 8825 |
| 38 | +1.472 2450 | +0.537 7122 | +1.476 1240 | +0.551 0155 | +1.482 3484 | +0.560 6879 |
| 39 | +1.413 8753 | +0.585 1789 | +1.417 8080 | +0.598 7973 | +1.423 9759 | +0.608 6959 |
| 40 | +1.350 8731 | +0.626 3539 | +1.354 8096 | +0.640 2802 | +1.360 8720 | +0.650 3687 |
| 41 | +1.283 9122 | +0.660 7876 | +1.287 8040 | +0.675 0020 | +1.293 7184 | +0.685 2350 |
| 42 | +1.213 7108 | +0.688 0995 | +1.217 5124 | +0.702 5721 | +1.223 2454 | +0.712 8968 |
| 43 | +1.141 0227 | +0.707 9845 | +1.144 6940 | +0.722 6753 | +1.150 2220 | +0.733 0331 |
| 44 | +1.066 6304 | +0.720 2157 | +1.070 1388 | +0.735 0768 | +1.075 5484 | +0.745 4066 |
| 45 | +0.991 3369 | +0.724 6478 | +0.994 6591 | +0.739 6239 | +0.999 7488 | +0.749 8650 |
| 46 | +0.915 9571 | +0.721 2182 | +0.919 0806 | +0.736 2498 | +0.923 9587 | +0.746 3434 |
| 47 | +0.841 3093 | +0.709 9494 | +0.844 2332 | +0.724 9743 | +0.848 9201 | +0.734 8666 |
| 48 | +0.768 2082 | +0.690 9488 | +0.770 9409 | +0.705 9042 | +0.775 4674 | +0.715 5486 |
| 49 | +0.697 4541 | +0.664 4077 | +0.700 0152 | +0.679 2337 | +0.704 4196 | +0.688 5925 |
| 50 | +0.629 8261 | +0.630 6012 | +0.632 2439 | +0.645 2428 | +0.636 5703 | +0.654 2871 |
| 51 | +0.566 0715 | +0.589 8843 | +0.568 3830 | +0.604 2938 | +0.572 6800 | +0.613 0068 |
| 52 | +0.506 8987 | +0.542 6896 | +0.509 1472 | +0.556 8286 | +0.513 4653 | +0.565 2062 |
| 53 | +0.452 9685 | +0.489 5225 | +0.455 2029 | +0.503 3636 | +0.459 5903 | +0.511 4133 |
| 54 | +0.404 8861 | +0.430 9573 | +0.407 1576 | +0.444 4847 | +0.411 6602 | +0.452 2270 |
| 55 | +0.363 1948 | +0.367 6314 | +0.365 5549 | +0.380 8404 | +0.370 2130 | +0.388 3082 |
| 56 | +0.328 3680 | +0.300 2365 | +0.330 8664 | +0.313 1351 | +0.335 7125 | +0.320 3708 |
| 57 | +0.300 8042 | +0.229 5127 | +0.303 4856 | +0.242 1210 | +0.308 5436 | +0.249 1751 |
| 58 | +0.280 8207 | +0.156 2403 | +0.283 7236 | +0.168 5895 | +0.289 0073 | +0.175 5176 |
| 59 | +0.268 6504 | +0.081 2302 | +0.271 8049 | +0.093 3621 | +0.277 3170 | +0.100 2240 |

TABLE V.—Continued.

RECTANGULAR G-COÖRDINATES X AND Y OF VENUS, REFERRED, IN EACH SYSTEM, TO AN AXIS OF X PASSING THROUGH THE MEAN SUN.

| <i>i</i> | System 3. | | System 4. | | System 5. | |
|----------|-------------|-------------|-------------|-------------|-------------|-------------|
| | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> |
| 0 | +0.279 8926 | +0.024 4020 | +0.285 2603 | +0.018 4830 | +0.288 6591 | +0.008 0878 |
| 1 | +0.284 2769 | -0.051 3907 | +0.289 6702 | -0.056 9777 | +0.293 0191 | -0.067 0880 |
| 2 | +0.296 5601 | -0.126 2430 | +0.301 9298 | -0.131 4966 | +0.305 1838 | -0.141 3542 |
| 3 | +0.316 5918 | -0.199 3308 | +0.321 8895 | -0.204 2627 | +0.325 0091 | -0.213 9093 |
| 4 | +0.344 1354 | -0.269 8527 | +0.349 3160 | -0.274 4873 | +0.352 2710 | -0.283 9728 |
| 5 | +0.378 8721 | -0.337 0406 | +0.383 8974 | -0.341 4123 | +0.386 6655 | -0.350 7937 |
| 6 | +0.420 4078 | -0.400 1668 | +0.425 2457 | -0.404 3190 | +0.427 8152 | -0.413 6573 |
| 7 | +0.468 2736 | -0.458 5510 | +0.472 9020 | -0.462 5340 | +0.475 2721 | -0.471 8919 |
| 8 | +0.521 9346 | -0.511 5674 | +0.526 3418 | -0.515 4368 | +0.528 5222 | -0.524 8756 |
| 9 | +0.580 7952 | -0.558 6507 | +0.584 9803 | -0.562 4651 | +0.586 9911 | -0.572 0427 |
| 10 | +0.644 2076 | -0.599 3022 | +0.648 1798 | -0.603 1207 | +0.650 0504 | -0.612 8887 |
| 11 | +0.711 4758 | -0.633 0942 | +0.715 2540 | -0.636 9740 | +0.717 0241 | -0.646 9765 |
| 12 | +0.781 8059 | -0.659 6737 | +0.785 4819 | -0.663 6672 | +0.787 1933 | -0.673 9389 |
| 13 | +0.854 6132 | -0.678 7647 | +0.858 1036 | -0.682 9185 | +0.859 8058 | -0.693 4842 |
| 14 | +0.928 9294 | -0.690 1730 | +0.932 3397 | -0.694 5257 | +0.934 0825 | -0.705 3977 |
| 15 | +1.004 0113 | -0.693 7852 | +1.007 3925 | -0.698 3667 | +1.009 2254 | -0.709 5459 |
| 16 | +1.079 0492 | -0.689 5714 | +1.082 4565 | -0.694 4006 | +1.084 4261 | -0.705 8759 |
| 17 | +1.153 2351 | -0.677 5823 | +1.156 7246 | -0.682 6691 | +1.158 8744 | -0.694 4182 |
| 18 | +1.225 7719 | -0.657 9526 | +1.229 3983 | -0.663 2956 | +1.231 7646 | -0.675 2864 |
| 19 | +1.295 8808 | -0.630 8962 | +1.299 6944 | -0.636 4839 | +1.302 3064 | -0.648 6759 |
| 20 | +1.362 8093 | -0.596 7058 | +1.366 8546 | -0.602 5160 | +1.369 7311 | -0.614 8635 |
| 21 | +1.425 8394 | -0.555 7489 | +1.430 1522 | -0.561 7502 | +1.433 3011 | -0.574 2026 |
| 22 | +1.484 2931 | -0.508 4647 | +1.488 9006 | -0.514 6175 | +1.492 3178 | -0.527 1222 |
| 23 | +1.537 5412 | -0.455 3593 | +1.542 4596 | -0.461 6180 | +1.546 1296 | -0.474 1214 |
| 24 | +1.585 0084 | -0.397 0007 | +1.590 2425 | -0.403 3157 | +1.594 1387 | -0.415 7661 |
| 25 | +1.626 1801 | -0.334 0124 | +1.631 7225 | -0.340 3342 | +1.635 8083 | -0.352 6827 |
| 26 | +1.660 6072 | -0.267 0689 | +1.666 4388 | -0.273 3482 | +1.670 6690 | -0.285 5523 |
| 27 | +1.687 9113 | -0.196 8867 | +1.694 0012 | -0.203 0779 | +1.698 3230 | -0.215 1035 |
| 28 | +1.707 7882 | -0.124 2202 | +1.714 0957 | -0.130 2819 | +1.718 4514 | -0.142 1049 |
| 29 | +1.720 0122 | -0.049 8508 | +1.726 4883 | -0.055 7493 | +1.730 8162 | -0.067 3551 |
| 30 | +1.724 4388 | +0.025 4188 | +1.731 0274 | +0.019 7085 | +1.735 2660 | +0.008 3225 |
| 31 | +1.721 0059 | +0.100 7745 | +1.727 6465 | +0.095 2669 | +1.731 7363 | +0.084 0928 |
| 32 | +1.709 7359 | +0.175 3989 | +1.716 3660 | +0.170 0960 | +1.720 2518 | +0.159 1154 |
| 33 | +1.690 7351 | +0.248 4792 | +1.697 2920 | +0.243 3714 | +1.700 9265 | +0.232 5558 |
| 34 | +1.664 1950 | +0.319 2167 | +1.670 6195 | +0.314 2840 | +1.673 9638 | +0.303 5951 |
| 35 | +1.630 3893 | +0.386 8336 | +1.636 6271 | +0.382 0454 | +1.639 6529 | +0.371 4384 |
| 36 | +1.589 6721 | +0.450 5830 | +1.595 6761 | +0.445 9010 | +1.598 3674 | +0.435 3259 |
| 37 | +1.542 4753 | +0.509 7560 | +1.548 2079 | +0.505 1363 | +1.550 5612 | +0.494 5411 |
| 38 | +1.489 3032 | +0.563 6915 | +1.494 7388 | +0.559 0849 | +1.496 7627 | +0.548 4197 |
| 39 | +1.430 7300 | +0.611 7835 | +1.435 8543 | +0.607 1386 | +1.437 5701 | +0.596 3565 |
| 40 | +1.367 3923 | +0.653 4880 | +1.372 2027 | +0.648 7530 | +1.373 6443 | +0.637 8131 |
| 41 | +1.299 9821 | +0.688 3306 | +1.304 4890 | +0.683 4552 | +1.305 6998 | +0.672 3257 |
| 42 | +1.229 2412 | +0.715 9113 | +1.233 4657 | +0.710 8508 | +1.234 4980 | +0.699 5075 |
| 43 | +1.155 9507 | +0.735 9114 | +1.159 9243 | +0.730 6274 | +1.160 8358 | +0.719 0571 |
| 44 | +1.080 9236 | +0.748 0961 | +1.084 6868 | +0.742 5595 | +1.085 5389 | +0.730 7598 |
| 45 | +1.004 9938 | +0.752 3188 | +1.008 5958 | +0.746 5108 | +1.009 4492 | +0.734 4915 |
| 46 | +0.929 0085 | +0.748 5233 | +0.932 5029 | +0.742 4365 | +0.933 4172 | +0.730 2183 |
| 47 | +0.853 8157 | +0.736 7446 | +0.857 2595 | +0.730 3837 | +0.858 2903 | +0.717 9976 |
| 48 | +0.780 2560 | +0.717 1082 | +0.783 7664 | +0.710 4897 | +0.784 6033 | +0.697 9763 |
| 49 | +0.709 1529 | +0.689 8295 | +0.712 6639 | +0.682 9817 | +0.714 0686 | +0.670 3895 |
| 50 | +0.641 3017 | +0.655 2115 | +0.644 9229 | +0.648 1733 | +0.646 5668 | +0.635 5557 |
| 51 | +0.577 4611 | +0.613 6402 | +0.581 2344 | +0.606 4605 | +0.583 1378 | +0.593 8734 |
| 52 | +0.518 3431 | +0.565 5804 | +0.522 3027 | +0.558 3153 | +0.524 4736 | +0.545 8162 |
| 53 | +0.464 6055 | +0.511 5714 | +0.468 7755 | +0.504 2817 | +0.471 2105 | +0.491 9264 |
| 54 | +0.416 8456 | +0.452 2194 | +0.421 2379 | +0.444 9681 | +0.423 9224 | +0.432 8084 |
| 55 | +0.375 5907 | +0.388 1916 | +0.380 2062 | +0.381 0400 | +0.383 1147 | +0.369 1218 |
| 56 | +0.341 2944 | +0.320 2069 | +0.346 1218 | +0.313 2132 | +0.349 2206 | +0.301 5727 |
| 57 | +0.314 3366 | +0.240 0281 | +0.319 3477 | +0.242 2440 | +0.322 5952 | +0.230 9071 |
| 58 | +0.294 0887 | +0.175 4508 | +0.300 1638 | +0.168 9220 | +0.303 5124 | +0.157 9020 |
| 59 | +0.283 4712 | +0.100 2967 | +0.288 7653 | +0.094 0597 | +0.292 1646 | +0.083 3577 |

TABLE V.—Continued.

RECTANGULAR G-COÖRDINATES X AND Y OF VENUS, REFERRED, IN EACH SYSTEM, TO AN AXIS OF X PASSING THROUGH THE MEAN SUN.

| <i>i</i> | System 6. | | System 7. | | System 8. | |
|----------|-------------|-------------|-------------|-------------|-------------|-------------|
| | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> |
| 0 | +0.289 3812 | -0.004 3547 | +0.287 0415 | -0.015 0849 | +0.281 8724 | -0.023 8026 |
| 1 | +0.293 5931 | -0.079 3938 | +0.291 0012 | -0.091 0510 | +0.285 5340 | -0.099 0059 |
| 2 | +0.305 5780 | -0.153 5781 | +0.302 7254 | -0.165 3184 | +0.290 9815 | -0.173 4542 |
| 3 | +0.325 2014 | -0.226 1096 | +0.322 0914 | -0.237 0885 | +0.316 1026 | -0.246 3419 |
| 4 | +0.352 2490 | -0.296 2092 | +0.348 8955 | -0.308 2783 | +0.342 7024 | -0.316 8787 |
| 5 | +0.386 4284 | -0.363 1251 | +0.382 8548 | -0.375 4297 | +0.376 5054 | -0.384 2966 |
| 6 | +0.427 3728 | -0.426 1400 | +0.423 6113 | -0.438 7161 | +0.417 1580 | -0.447 8587 |
| 7 | +0.474 6443 | -0.484 5776 | +0.470 7341 | -0.497 4515 | +0.464 2316 | -0.506 8671 |
| 8 | +0.527 7380 | -0.537 8098 | +0.523 7240 | -0.550 9962 | +0.517 2268 | -0.560 6666 |
| 9 | +0.586 0872 | -0.585 2627 | +0.582 0178 | -0.598 7649 | +0.575 5777 | -0.608 6687 |
| 10 | +0.649 0693 | -0.626 4213 | +0.644 9946 | -0.640 2315 | +0.638 6584 | -0.650 3275 |
| 11 | +0.716 0118 | -0.660 8369 | +0.711 9802 | -0.674 9360 | +0.705 7897 | -0.685 1772 |
| 12 | +0.786 1086 | -0.688 1308 | +0.782 2554 | -0.702 4883 | +0.776 2436 | -0.712 8211 |
| 13 | +0.858 8769 | -0.707 9983 | +0.855 0617 | -0.722 5740 | +0.849 2528 | -0.732 9398 |
| 14 | +0.933 2651 | -0.720 2135 | +0.929 6105 | -0.734 9582 | +0.924 0172 | -0.745 2958 |
| 15 | +1.008 5598 | -0.724 6313 | +1.005 0902 | -0.739 4890 | +0.999 7145 | -0.749 7373 |
| 16 | +1.083 9453 | -0.721 1895 | +1.080 6753 | -0.736 0995 | +1.075 5085 | -0.746 1991 |
| 17 | +1.158 6020 | -0.709 9106 | +1.155 5347 | -0.724 8102 | +1.150 5579 | -0.734 7062 |
| 18 | +1.231 7142 | -0.690 9018 | +1.228 8424 | -0.705 7280 | +1.224 0268 | -0.715 3728 |
| 19 | +1.302 4807 | -0.664 3547 | +1.299 7857 | -0.679 0484 | +1.295 0946 | -0.688 4024 |
| 20 | +1.370 1219 | -0.630 5443 | +1.367 5740 | -0.645 0509 | +1.362 0645 | -0.654 0862 |
| 21 | +1.433 8901 | -0.589 8264 | +1.431 4510 | -0.604 0981 | +1.426 8752 | -0.612 7987 |
| 22 | +1.493 0762 | -0.542 6339 | +1.490 7009 | -0.556 6323 | +1.486 1086 | -0.564 9945 |
| 23 | +1.547 0187 | -0.489 4723 | +1.544 6576 | -0.503 1709 | +1.539 9987 | -0.511 2033 |
| 24 | +1.595 1122 | -0.430 9158 | +1.592 7131 | -0.444 2998 | +1.587 9409 | -0.452 0237 |
| 25 | +1.636 8140 | -0.367 6003 | +1.634 3252 | -0.380 6684 | +1.629 3973 | -0.388 1167 |
| 26 | +1.671 6503 | -0.300 2166 | +1.669 0214 | -0.312 9805 | +1.663 9048 | -0.320 1963 |
| 27 | +1.699 2228 | -0.229 5034 | +1.696 4089 | -0.241 0865 | +1.691 0789 | -0.249 0223 |
| 28 | +1.719 2138 | -0.156 2412 | +1.716 1761 | -0.168 4765 | +1.710 6192 | -0.175 3907 |
| 29 | +1.731 3898 | -0.081 2404 | +1.728 0986 | -0.093 2689 | +1.722 3122 | -0.100 1249 |
| 30 | +1.735 6043 | -0.005 3345 | +1.732 0410 | -0.017 2049 | +1.726 0340 | -0.024 0644 |
| 31 | +1.731 8010 | +0.070 6309 | +1.727 9580 | +0.058 8662 | +1.721 7514 | +0.051 9430 |
| 32 | +1.720 0145 | +0.145 8077 | +1.715 8666 | +0.134 0934 | +1.709 5212 | +0.127 0511 |
| 33 | +1.700 3702 | +0.219 3560 | +1.695 9944 | +0.207 6356 | +1.689 4904 | +0.200 4263 |
| 34 | +1.673 0827 | +0.290 4526 | +1.668 4777 | +0.278 6726 | +1.661 8933 | +0.271 2560 |
| 35 | +1.638 4553 | +0.358 3016 | +1.633 6597 | +0.346 4130 | +1.627 0482 | +0.338 7587 |
| 36 | +1.596 8743 | +0.422 1439 | +1.591 9353 | +0.410 1049 | +1.585 3540 | +0.402 1930 |
| 37 | +1.548 8048 | +0.481 2659 | +1.543 7778 | +0.469 0434 | +1.537 2837 | +0.460 8658 |
| 38 | +1.494 7865 | +0.535 0089 | +1.489 7309 | +0.522 5796 | +1.483 3802 | +0.514 1397 |
| 39 | +1.435 4258 | +0.582 7755 | +1.430 4045 | +0.570 1266 | +1.424 2480 | +0.561 4397 |
| 40 | +1.371 3900 | +0.624 0380 | +1.366 4651 | +0.611 1675 | +1.360 5472 | +0.602 2588 |
| 41 | +1.303 3980 | +0.658 3431 | +1.298 6290 | +0.645 2602 | +1.292 9865 | +0.636 1634 |
| 42 | +1.232 2125 | +0.685 3171 | +1.227 6529 | +0.672 0417 | +1.222 3115 | +0.662 7978 |
| 43 | +1.158 6310 | +0.704 6698 | +1.154 3266 | +0.691 2326 | +1.149 3005 | +0.681 8865 |
| 44 | +1.083 4752 | +0.716 1979 | +1.079 4622 | +0.702 6377 | +1.074 7540 | +0.693 2381 |
| 45 | +1.007 5811 | +0.719 7864 | +1.003 8858 | +0.706 1489 | +0.999 4847 | +0.696 7453 |
| 46 | +0.931 7909 | +0.715 4100 | +0.928 4277 | +0.701 7444 | +0.924 3115 | +0.692 3855 |
| 47 | +0.856 9412 | +0.703 1324 | +0.853 9128 | +0.689 4895 | +0.850 0486 | +0.680 2209 |
| 48 | +0.783 8553 | +0.683 1047 | +0.781 1516 | +0.669 5340 | +0.777 4975 | +0.660 3960 |
| 49 | +0.713 3338 | +0.655 5634 | +0.710 9317 | +0.642 1111 | +0.707 4383 | +0.633 1359 |
| 50 | +0.646 1446 | +0.620 8269 | +0.644 0104 | +0.607 5322 | +0.640 6223 | +0.598 7436 |
| 51 | +0.583 0165 | +0.579 2912 | +0.581 1065 | +0.566 1862 | +0.577 7638 | +0.557 5971 |
| 52 | +0.524 6297 | +0.531 4234 | +0.522 8929 | +0.518 5316 | +0.519 5340 | +0.510 1441 |
| 53 | +0.471 6110 | +0.477 7588 | +0.469 9907 | +0.465 0927 | +0.466 5545 | +0.456 8979 |
| 54 | +0.424 5246 | +0.418 8929 | +0.422 0616 | +0.406 4538 | +0.419 3902 | +0.398 4327 |
| 55 | +0.383 8706 | +0.355 4747 | +0.382 3050 | +0.343 2525 | +0.378 5456 | +0.335 3763 |
| 56 | +0.350 0760 | +0.288 2002 | +0.348 4501 | +0.276 1738 | +0.344 4581 | +0.268 4051 |
| 57 | +0.323 4952 | +0.217 8039 | +0.321 7545 | +0.205 9419 | +0.317 4943 | +0.198 2368 |
| 58 | +0.304 4032 | +0.145 0512 | +0.302 4996 | +0.133 3140 | +0.297 0461 | +0.125 6232 |
| 59 | +0.292 9944 | +0.070 7305 | +0.290 8879 | +0.059 0724 | +0.286 0278 | +0.051 3438 |

TABLE V.—*Concluded.*

RECTANGULAR G-COÖRDINATES X AND Y OF VENUS, REFERRED, IN EACH SYSTEM, TO AN AXIS OF X PASSING THROUGH THE MEAN SUN.

| <i>i</i> | System 9. | | System 10. | | System 11. | |
|----------|-------------|-------------|-------------|-------------|-------------|-------------|
| | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> |
| 0 | +0.275 0523 | -0.025 3633 | +0.268 5973 | -0.019 7819 | +0.264 6365 | -0.008 4260 |
| 1 | +0.278 4844 | -0.100 7462 | +0.271 9768 | -0.095 3562 | +0.268 1640 | -0.084 2045 |
| 2 | +0.289 7521 | -0.175 4000 | +0.283 2537 | -0.170 2047 | +0.279 6432 | -0.159 2361 |
| 3 | +0.308 7484 | -0.248 5086 | +0.302 3220 | -0.243 5018 | +0.298 9610 | -0.232 6860 |
| 4 | +0.335 2831 | -0.319 2704 | +0.328 9878 | -0.314 4354 | +0.325 9149 | -0.303 7353 |
| 5 | +0.369 0820 | -0.386 9062 | +0.362 9727 | -0.382 2158 | +0.360 2162 | -0.371 5891 |
| 6 | +0.409 7903 | -0.450 6682 | +0.403 9145 | -0.446 0864 | +0.401 4913 | -0.435 4874 |
| 7 | +0.450 9758 | -0.509 8485 | +0.451 3723 | -0.505 3317 | +0.449 2861 | -0.494 7126 |
| 8 | +0.510 1331 | -0.563 7854 | +0.504 8294 | -0.559 2848 | +0.503 0724 | -0.548 5982 |
| 9 | +0.568 6886 | -0.611 8737 | +0.563 7000 | -0.607 3382 | +0.562 2517 | -0.506 5386 |
| 10 | +0.632 0062 | -0.653 5698 | +0.627 3358 | -0.648 9481 | +0.626 1636 | -0.637 9955 |
| 11 | +0.699 3951 | -0.688 4000 | +0.695 0329 | -0.683 6429 | +0.694 0946 | -0.672 5042 |
| 12 | +0.770 1160 | -0.715 9656 | +0.766 0366 | -0.711 0281 | +0.765 2841 | -0.699 6795 |
| 13 | +0.843 3898 | -0.733 9488 | +0.839 5657 | -0.730 7919 | +0.838 9356 | -0.719 2203 |
| 14 | +0.918 4056 | -0.748 1159 | +0.914 7912 | -0.742 7091 | +0.914 2243 | -0.730 9118 |
| 15 | +0.994 3301 | -0.752 3209 | +0.990 8753 | -0.746 6441 | +0.990 3091 | -0.734 6303 |
| 16 | +1.070 3171 | -0.748 5084 | +1.066 9676 | -0.742 5523 | +1.066 3406 | -0.730 3419 |
| 17 | +1.145 5178 | -0.730 7126 | +1.142 2168 | -0.730 4812 | +1.141 4717 | -0.718 1042 |
| 18 | +1.219 0910 | -0.717 0597 | +1.215 7813 | -0.710 5689 | +1.214 8681 | -0.698 0645 |
| 19 | +1.290 2123 | -0.689 7649 | +1.286 8399 | -0.683 0438 | +1.285 7175 | -0.670 4585 |
| 20 | +1.358 0846 | -0.655 1320 | +1.354 5999 | -0.648 2193 | +1.353 2374 | -0.635 6060 |
| 21 | +1.421 9480 | -0.613 5482 | +1.418 3087 | -0.606 4921 | +1.416 6861 | -0.593 9072 |
| 22 | +1.481 0876 | -0.565 4803 | +1.477 2619 | -0.558 3354 | +1.475 3700 | -0.545 8365 |
| 23 | +1.534 8440 | -0.511 4688 | +1.530 8092 | -0.504 2948 | +1.528 6519 | -0.491 9379 |
| 24 | +1.582 6192 | -0.452 1210 | +1.578 3646 | -0.444 9805 | +1.575 9570 | -0.432 8169 |
| 25 | +1.623 8856 | -0.388 1040 | +1.619 4111 | -0.381 0590 | +1.616 7795 | -0.369 1332 |
| 26 | +1.658 1899 | -0.320 1363 | +1.653 5064 | -0.313 2470 | +1.650 6865 | -0.301 5947 |
| 27 | +1.685 1598 | -0.248 9795 | +1.680 2882 | -0.242 3001 | +1.677 3221 | -0.230 9478 |
| 28 | +1.704 5055 | -0.175 4284 | +1.699 4769 | -0.169 0056 | +1.696 4120 | -0.157 9687 |
| 29 | +1.716 0249 | -0.100 3034 | +1.710 8776 | -0.094 1744 | +1.707 7640 | -0.083 4561 |
| 30 | +1.719 6036 | -0.024 4386 | +1.714 3825 | -0.018 6290 | +1.711 2698 | -0.008 2204 |
| 31 | +1.715 2172 | +0.051 3259 | +1.709 9702 | +0.056 8022 | +1.706 9075 | +0.066 9225 |
| 32 | +1.702 9292 | +0.126 1551 | +1.697 7055 | +0.131 2957 | +1.694 7377 | +0.141 1607 |
| 33 | +1.682 8904 | +0.199 2270 | +1.677 7386 | +0.204 0425 | +1.674 9043 | +0.213 6945 |
| 34 | +1.655 3370 | +0.269 7422 | +1.650 3021 | +0.274 2547 | +1.647 6325 | +0.283 7444 |
| 35 | +1.620 5873 | +0.336 9322 | +1.615 7077 | +0.341 1756 | +1.613 2252 | +0.350 5588 |
| 36 | +1.579 0366 | +0.400 0673 | +1.574 3442 | +0.404 0865 | +1.572 0603 | +0.413 4229 |
| 37 | +1.531 1536 | +0.458 4650 | +1.526 6766 | +0.462 3116 | +1.524 5861 | +0.471 6640 |
| 38 | +1.477 4737 | +0.511 4975 | +1.473 2125 | +0.515 2296 | +1.471 3167 | +0.524 6595 |
| 39 | +1.418 5926 | +0.558 5979 | +1.414 5550 | +0.562 2757 | +1.412 8279 | +0.571 8423 |
| 40 | +1.355 1605 | +0.599 2658 | +1.351 3371 | +0.602 9494 | +1.349 7496 | +0.612 7065 |
| 41 | +1.287 8735 | +0.633 0725 | +1.284 2449 | +0.636 8197 | +1.282 7595 | +0.646 8129 |
| 42 | +1.217 4671 | +0.659 6638 | +1.214 0031 | +0.663 5280 | +1.212 5774 | +0.673 7929 |
| 43 | +1.144 7074 | +0.678 7636 | +1.141 3690 | +0.682 7924 | +1.139 9554 | +0.693 3538 |
| 44 | +1.070 3837 | +0.690 1770 | +1.067 1246 | +0.694 4103 | +1.065 6731 | +0.705 2866 |
| 45 | +0.995 2985 | +0.693 7915 | +0.992 0676 | +0.698 2589 | +0.990 5284 | +0.709 4400 |
| 46 | +0.920 2620 | +0.689 5775 | +0.917 0042 | +0.694 2980 | +0.915 3290 | +0.705 7790 |
| 47 | +0.846 0814 | +0.677 5884 | +0.842 7410 | +0.682 5694 | +0.840 8858 | +0.694 3282 |
| 48 | +0.773 5541 | +0.657 9598 | +0.770 0760 | +0.663 1965 | +0.768 0039 | +0.675 2018 |
| 49 | +0.703 4583 | +0.630 9076 | +0.699 7907 | +0.636 3845 | +0.697 4731 | +0.648 5938 |
| 50 | +0.636 5464 | +0.596 7255 | +0.632 6437 | +0.602 4170 | +0.630 0613 | +0.614 7816 |
| 51 | +0.573 5356 | +0.555 7804 | +0.569 3612 | +0.561 6533 | +0.566 5049 | +0.574 1195 |
| 52 | +0.515 1027 | +0.508 5110 | +0.510 6299 | +0.514 5258 | +0.507 5018 | +0.527 0362 |
| 53 | +0.461 8752 | +0.455 4212 | +0.457 0893 | +0.461 5341 | +0.453 7038 | +0.474 0329 |
| 54 | +0.414 4269 | +0.397 0772 | +0.397 3243 | +0.403 2415 | +0.405 7084 | +0.415 6762 |
| 55 | +0.373 2719 | +0.334 1012 | +0.367 8611 | +0.340 2695 | +0.364 0524 | +0.352 5927 |
| 56 | +0.338 8588 | +0.267 1652 | +0.333 1597 | +0.273 2907 | +0.329 2053 | +0.285 4627 |
| 57 | +0.311 5656 | +0.196 9846 | +0.305 6091 | +0.203 0240 | +0.301 5630 | +0.215 0136 |
| 58 | +0.291 6964 | +0.124 3117 | +0.285 5228 | +0.130 2265 | +0.281 4442 | +0.142 0126 |
| 59 | +0.279 4770 | +0.049 9280 | +0.273 1348 | +0.055 6874 | +0.269 0848 | +0.067 2585 |

TABLE VI.
G-COÖRDINATE Z OF VENUS.

| Sys-tem <i>i</i> | 0 | 1 | 2 | 3 | 4 | 5 |
|---------------------|-------------|-------------|-------------|-------------|-------------|-------------|
| 0 | +0.17 4641 | +0.34 6635 | +0.42 3898 | +0.38 5648 | +0.24 3031 | +0.03 5232 |
| 1 | +0.021 4657 | +0.37 0784 | +0.42 5597 | +0.36 4563 | +0.20 5041 | -.000 9384 |
| 2 | +0.025 2276 | +0.39 0785 | +0.42 2557 | +0.33 9453 | +0.16 4810 | -.005 3894 |
| 3 | +0.028 7075 | +0.40 6417 | +0.41 4818 | +0.31 0603 | +0.12 2785 | -.009 7824 |
| 4 | +0.031 8665 | +0.41 7509 | +0.40 2471 | +0.27 8339 | +0.07 9423 | -.014 0692 |
| 5 | +0.034 6689 | +0.42 3939 | +0.38 5664 | +0.24 3022 | +0.03 5202 | -.018 2044 |
| 6 | +0.037 0834 | +0.42 5642 | +0.36 4589 | +0.20 5043 | -.000 9400 | -.022 1436 |
| 7 | +0.039 0828 | +0.42 2603 | +0.33 9486 | +0.16 4824 | -.005 3898 | -.025 8445 |
| 8 | +0.040 6450 | +0.41 4861 | +0.31 0641 | +0.12 2809 | -.009 7816 | -.029 2675 |
| 9 | +0.041 7527 | +0.40 2507 | +0.27 8378 | +0.07 9454 | -.014 0672 | -.032 3763 |
| 10 | +0.042 3943 | +0.38 5690 | +0.24 3057 | +0.03 5235 | -.018 2018 | -.035 1374 |
| 11 | +0.042 5630 | +0.36 4602 | +0.20 5072 | -.000 9368 | -.022 1406 | -.037 5211 |
| 12 | +0.042 2579 | +0.33 9485 | +0.16 4842 | -.005 3871 | -.025 8416 | -.039 5028 |
| 13 | +0.041 4828 | +0.31 0627 | +0.12 2814 | -.009 7798 | -.029 2651 | -.041 0601 |
| 14 | +0.040 2473 | +0.27 8355 | +0.07 9446 | -.014 0665 | -.032 3746 | -.042 1764 |
| 15 | +0.038 5660 | +0.24 3029 | +0.03 5218 | -.018 2022 | -.035 1366 | -.042 8392 |
| 16 | +0.036 4580 | +0.20 5046 | -.000 9389 | -.022 1419 | -.037 5215 | -.043 0410 |
| 17 | +0.033 9476 | +0.16 4822 | -.005 3893 | -.025 8434 | -.039 5037 | -.042 7792 |
| 18 | +0.031 0631 | +0.12 2804 | -.009 7815 | -.029 2671 | -.041 0620 | -.042 0556 |
| 19 | +0.027 8370 | +0.07 9450 | -.014 0675 | -.032 3762 | -.042 1783 | -.040 8775 |
| 20 | +0.024 3054 | +0.03 5233 | -.018 2021 | -.035 1377 | -.042 8411 | -.039 2568 |
| 21 | +0.020 5072 | -.000 9367 | -.022 1407 | -.037 5218 | -.043 0424 | -.037 2103 |
| 22 | +0.016 4847 | -.005 3866 | -.025 8415 | -.039 5032 | -.042 7800 | -.034 7593 |
| 23 | +0.012 2824 | -.009 7789 | -.029 2648 | -.041 0604 | -.042 0556 | -.031 9299 |
| 24 | +0.007 9461 | -.014 0654 | -.032 3739 | -.042 1765 | -.040 8769 | -.028 7515 |
| 25 | +0.003 5237 | -.018 2007 | -.035 1357 | -.042 8391 | -.039 2556 | -.025 2590 |
| 26 | -.000 9370 | -.022 1401 | -.037 5204 | -.043 0406 | -.037 2089 | -.021 4899 |
| 27 | -.005 3875 | -.025 8415 | -.039 5023 | -.042 7786 | -.034 7578 | -.017 4848 |
| 28 | -.009 7799 | -.029 2652 | -.041 0600 | -.042 0548 | -.031 9285 | -.013 2876 |
| 29 | -.014 0663 | -.032 3746 | -.042 1766 | -.040 8766 | -.028 7508 | -.008 9440 |
| 30 | -.018 2014 | -.035 1364 | -.042 8395 | -.039 2557 | -.025 2588 | -.004 5014 |
| 31 | -.022 1404 | -.037 5209 | -.043 0411 | -.037 2091 | -.021 4900 | -.000 0091 |
| 32 | -.025 8416 | -.039 5026 | -.042 7789 | -.034 7581 | -.017 4851 | +0.004 4833 |
| 33 | -.029 2651 | -.041 0601 | -.042 0550 | -.031 9287 | -.013 2878 | +0.008 9260 |
| 34 | -.032 3744 | -.042 1765 | -.040 8765 | -.028 7508 | -.008 9438 | +0.013 2696 |
| 35 | -.035 1363 | -.042 8394 | -.039 2555 | -.025 2585 | -.004 5009 | +0.017 4653 |
| 36 | -.037 5212 | -.043 0411 | -.037 2089 | -.021 4895 | -.000 0084 | +0.021 4663 |
| 37 | -.039 5032 | -.042 7792 | -.034 7581 | -.017 4846 | +0.004 4842 | +0.025 2276 |
| 38 | -.041 0611 | -.042 0556 | -.031 9288 | -.013 2874 | +0.008 9269 | +0.028 7069 |
| 39 | -.042 1777 | -.040 8775 | -.028 7513 | -.008 9438 | +0.013 2702 | +0.031 8651 |
| 40 | -.042 8407 | -.039 2567 | -.025 2594 | -.004 5015 | +0.017 4654 | +0.034 6668 |
| 41 | -.043 0424 | -.037 2103 | -.021 4908 | -.000 0095 | +0.021 4658 | +0.037 0805 |
| 42 | -.042 7801 | -.034 7594 | -.017 4861 | +0.004 4827 | +0.025 2265 | +0.039 0797 |
| 43 | -.042 0559 | -.031 9300 | -.013 2889 | +0.008 9251 | +0.028 7052 | +0.040 6420 |
| 44 | -.040 8771 | -.028 7519 | -.008 9451 | +0.013 2684 | +0.031 8631 | +0.041 7501 |
| 45 | -.039 2555 | -.025 2594 | -.004 5022 | +0.017 4641 | +0.034 6648 | +0.042 3922 |
| 46 | -.037 2085 | -.021 4900 | -.000 0095 | +0.021 4650 | +0.037 0791 | +0.042 5618 |
| 47 | -.034 7572 | -.017 4816 | +0.004 4835 | +0.025 2265 | +0.039 0788 | +0.042 2575 |
| 48 | -.031 9278 | -.013 2869 | +0.008 9269 | +0.028 7061 | +0.040 6418 | +0.041 4834 |
| 49 | -.028 7504 | -.008 9431 | +0.013 2707 | +0.031 8649 | +0.041 7508 | +0.040 2487 |
| 50 | -.025 2588 | -.004 5007 | +0.017 4664 | +0.034 6672 | +0.042 3939 | +0.038 5680 |
| 51 | -.021 4907 | -.000 0088 | +0.021 4671 | +0.037 0818 | +0.042 5641 | +0.036 4606 |
| 52 | -.017 4867 | +0.004 4829 | +0.025 2277 | +0.039 0815 | +0.042 2603 | +0.033 9503 |
| 53 | -.013 2904 | +0.008 9247 | +0.028 7061 | +0.040 6439 | +0.041 4852 | +0.031 0659 |
| 54 | -.008 9473 | +0.013 2672 | +0.031 8635 | +0.041 7518 | +0.040 2511 | +0.027 8396 |
| 55 | -.004 5052 | +0.017 4621 | +0.034 6645 | +0.042 3935 | +0.038 5697 | +0.024 3076 |
| 56 | -.000 0130 | +0.021 4624 | +0.037 0779 | +0.042 5624 | +0.036 4611 | +0.020 5092 |
| 57 | +0.004 4797 | +0.025 2232 | +0.039 0768 | +0.042 2573 | +0.033 9495 | +0.016 4863 |
| 58 | +0.008 9228 | +0.028 7024 | +0.040 6390 | +0.041 4822 | +0.031 0636 | +0.012 2834 |
| 59 | +0.013 2669 | +0.031 8610 | +0.041 7474 | +0.040 2465 | +0.027 8361 | +0.007 9465 |

TABLE VI.—*Concluded.*
G-COÖRDINATE Z OF VENUS.

| System <i>i</i> | 6 | 7 | 8 | 9 | 10 | 11 |
|--------------------|-------------|-------------|-------------|-------------|-------------|-------------|
| 0 | -.018 2000 | -.035 1342 | -.042 8369 | -.039 2532 | -.025 2572 | -.004 5010 |
| 1 | -.022 1401 | -.037 5194 | -.043 0386 | -.037 2062 | -.021 4874 | -.000 0076 |
| 2 | -.025 8423 | -.039 5018 | -.042 7767 | -.034 7550 | -.017 4818 | +0.004 4858 |
| 3 | -.029 2668 | -.041 0601 | -.042 0532 | -.031 9256 | -.013 2840 | +0.008 9294 |
| 4 | -.032 3768 | -.042 1773 | -.040 8754 | -.028 7481 | -.008 9400 | +0.013 2734 |
| 5 | -.035 1389 | -.042 8410 | -.039 2552 | -.025 2564 | -.004 4976 | +0.017 4692 |
| 6 | -.037 5236 | -.043 0430 | -.037 2094 | -.021 4882 | -.000 0058 | +0.021 4697 |
| 7 | -.039 5053 | -.042 7812 | -.034 7591 | -.017 4841 | +0.004 4860 | +0.025 2302 |
| 8 | -.041 0626 | -.042 0571 | -.031 9302 | -.013 2877 | +0.008 9278 | +0.028 7085 |
| 9 | -.042 1786 | -.040 8785 | -.028 7525 | -.008 9446 | +0.013 2704 | +0.031 8658 |
| 10 | -.042 8409 | -.039 2571 | -.025 2602 | -.004 5023 | +0.017 4650 | +0.034 6667 |
| 11 | -.043 0419 | -.037 2100 | -.021 4909 | -.000 0100 | +0.021 4652 | +0.037 0801 |
| 12 | -.042 7792 | -.034 7584 | -.017 4855 | +0.004 4828 | +0.025 2260 | +0.039 0788 |
| 13 | -.042 0547 | -.031 9285 | -.013 2877 | +0.008 9260 | +0.028 7051 | +0.040 6410 |
| 14 | -.040 8759 | -.028 7504 | -.008 9434 | +0.013 2698 | +0.031 8637 | +0.041 7493 |
| 15 | -.039 2548 | -.025 2577 | -.004 5004 | +0.017 4658 | +0.034 6659 | +0.042 3920 |
| 16 | -.037 2083 | -.021 4886 | -.000 0078 | +0.021 4667 | +0.037 0804 | +0.042 5621 |
| 17 | -.034 7576 | -.017 4838 | +0.004 4849 | +0.025 2279 | +0.039 0801 | +0.042 2582 |
| 18 | -.031 9285 | -.013 2868 | +0.008 9276 | +0.028 7070 | +0.040 6429 | +0.041 4843 |
| 19 | -.028 7511 | -.008 9433 | +0.013 2707 | +0.031 8652 | +0.041 7515 | +0.040 2494 |
| 20 | -.025 2591 | -.004 5010 | +0.017 4659 | +0.034 6669 | +0.042 3938 | +0.038 5683 |
| 21 | -.021 4905 | -.000 0089 | +0.021 4663 | +0.37 0806 | +0.042 5634 | +0.036 4601 |
| 22 | -.017 4858 | +0.004 4834 | +0.025 2260 | +0.039 0798 | +0.042 2588 | +0.033 9492 |
| 23 | -.013 2884 | +0.008 9260 | +0.028 7058 | +0.040 6420 | +0.041 4841 | +0.031 0639 |
| 24 | -.008 9445 | +0.013 2693 | +0.031 8639 | +0.041 7503 | +0.040 2485 | +0.027 8371 |
| 25 | -.004 5016 | +0.017 4648 | +0.034 6657 | +0.042 3926 | +0.038 5671 | +0.024 3046 |
| 26 | -.000 0090 | +0.021 4657 | +0.037 0798 | +0.042 5622 | +0.036 4589 | +0.020 5061 |
| 27 | +0.004 4836 | +0.025 2267 | +0.039 0792 | +0.042 2578 | +0.033 9480 | +0.016 4835 |
| 28 | +0.008 9263 | +0.028 7059 | +0.040 6418 | +0.041 4834 | +0.031 0630 | +0.012 2812 |
| 29 | +0.013 2697 | +0.031 8640 | +0.041 7503 | +0.040 2483 | +0.027 8365 | +0.007 9453 |
| 30 | +0.017 4651 | +0.034 6658 | +0.042 3926 | +0.038 5671 | +0.024 3044 | +0.003 5232 |
| 31 | +0.021 4656 | +0.037 0798 | +0.042 5622 | +0.036 4589 | +0.020 5061 | -.000 9372 |
| 32 | +0.025 2265 | +0.039 0790 | +0.042 2577 | +0.033 9481 | +0.016 4835 | -.005 3874 |
| 33 | +0.028 7055 | +0.040 6414 | +0.041 4832 | +0.031 0629 | +0.012 2813 | -.009 7798 |
| 34 | +0.031 8637 | +0.041 7499 | +0.040 2479 | +0.027 8362 | +0.007 9452 | -.014 0663 |
| 35 | +0.034 6657 | +0.042 3924 | +0.038 5666 | +0.024 3039 | +0.003 5227 | -.018 2016 |
| 36 | +0.037 0803 | +0.042 5624 | +0.036 4587 | +0.020 5053 | -.000 9380 | -.022 1410 |
| 37 | +0.039 0800 | +0.042 2582 | +0.033 9481 | +0.016 4829 | -.005 3885 | -.025 8425 |
| 38 | +0.040 6429 | +0.041 4843 | +0.031 0634 | +0.012 2810 | -.009 7809 | -.029 2663 |
| 39 | +0.041 7516 | +0.040 2496 | +0.027 8373 | +0.007 9454 | -.014 0673 | -.032 3757 |
| 40 | +0.042 3941 | +0.038 5686 | +0.024 3059 | +0.003 5236 | -.018 2018 | -.035 1375 |
| 41 | +0.042 5637 | +0.036 4607 | +0.020 5076 | -.000 9364 | -.022 1405 | -.037 5218 |
| 42 | +0.042 2590 | +0.033 9500 | +0.016 4854 | -.005 3861 | -.025 8411 | -.039 5031 |
| 43 | +0.041 4843 | +0.031 0647 | +0.012 2833 | -.009 7782 | -.029 2643 | -.041 0603 |
| 44 | +0.040 2488 | +0.027 8377 | +0.007 9472 | -.014 0645 | -.032 3732 | -.042 1761 |
| 45 | +0.038 5672 | +0.024 3051 | +0.003 5245 | -.018 1997 | -.035 1349 | -.042 8386 |
| 46 | +0.036 4590 | +0.020 5062 | -.000 9367 | -.022 1394 | -.037 5197 | -.043 0401 |
| 47 | +0.033 9480 | +0.016 4835 | -.005 3875 | -.025 8414 | -.039 5020 | -.042 7782 |
| 48 | +0.031 0631 | +0.012 2812 | -.009 7805 | -.029 2657 | -.041 0604 | -.042 0548 |
| 49 | +0.027 8367 | +0.007 9452 | -.014 0671 | -.032 3758 | -.042 1777 | -.040 8770 |
| 50 | +0.024 3049 | +0.003 5231 | -.018 2023 | -.035 1381 | -.042 8413 | -.039 2569 |
| 51 | +0.020 5071 | -.000 9371 | -.022 1413 | -.037 5229 | -.043 0437 | -.037 2112 |
| 52 | +0.016 4852 | -.005 3869 | -.025 8422 | -.039 5045 | -.042 7820 | -.034 7610 |
| 53 | +0.012 2837 | -.009 7786 | -.029 2654 | -.041 0619 | -.042 0581 | -.031 9323 |
| 54 | +0.007 9482 | -.014 0642 | -.032 3741 | -.042 1778 | -.040 8794 | -.028 7548 |
| 55 | +0.003 5264 | -.018 1987 | -.035 1353 | -.042 8401 | -.039 2580 | -.025 2624 |
| 56 | -.000 9340 | -.022 1376 | -.037 5193 | -.043 0411 | -.037 2108 | -.021 4931 |
| 57 | -.005 3844 | -.025 8388 | -.039 5006 | -.042 7784 | -.034 7591 | -.017 4875 |
| 58 | -.009 7771 | -.029 2624 | -.041 0578 | -.042 0538 | -.031 9290 | -.013 2894 |
| 59 | -.014 0642 | -.032 3720 | -.042 1740 | -.040 8748 | -.028 7503 | -.008 9447 |

TABLE VII.

VALUES OF A, B, C, AND D FOR THE ACTION OF VENUS ON THE MOON.

| System o. | | | | | System i. | | | | |
|-----------|-------------|-------------|-------------|-------------|-----------|-------------|------------|-------------|-------------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +35.541 47 | -17.876 47 | -17.664 99 | + 1.074 27 | 0 | +32.593 73 | -16.607 73 | -15.085 99 | + 3.187 45 |
| 1 | +27.684 74 | -12.483 21 | -15.201 55 | -11.369 32 | 1 | +27.372 10 | -13.088 33 | -14.283 78 | - 9.177 80 |
| 2 | +14.109 43 | - 3.818 23 | -10.291 18 | -12.812 04 | 2 | +14.893 21 | - 4.857 17 | -10.036 02 | -11.992 56 |
| 3 | + 6.072 22 | + 0.262 35 | - 6.334 56 | - 9.167 52 | 3 | + 6.704 15 | - 0.374 85 | - 6.329 30 | - 9.064 78 |
| 4 | + 2.039 36 | + 1.251 33 | - 3.890 71 | - 5.857 72 | 4 | + 3.003 34 | + 0.935 15 | - 3.938 50 | - 5.930 21 |
| 5 | + 1.270 90 | + 1.203 98 | - 2.474 87 | - 3.746 92 | 5 | + 1.474 29 | + 1.046 97 | - 2.521 25 | - 3.830 19 |
| 6 | + 0.707 97 | + 0.937 76 | - 1.645 74 | - 2.486 04 | 6 | + 0.827 46 | + 0.853 85 | - 1.681 30 | - 2.549 54 |
| 7 | + 0.459 96 | + 0.682 85 | - 1.142 81 | - 1.722 74 | 7 | + 0.535 00 | + 0.633 64 | - 1.168 65 | - 1.767 04 |
| 8 | + 0.341 13 | + 0.484 05 | - 0.825 17 | - 1.243 31 | 8 | + 0.391 31 | + 0.452 53 | - 0.843 83 | - 1.273 60 |
| 9 | + 0.278 66 | + 0.337 95 | - 0.616 61 | - 0.929 36 | 9 | + 0.314 04 | + 0.316 17 | - 0.630 22 | - 0.950 06 |
| 10 | + 0.242 48 | + 0.232 28 | - 0.474 76 | - 0.715 40 | 10 | + 0.268 52 | + 0.216 33 | - 0.484 84 | - 0.729 59 |
| 11 | + 0.219 41 | + 0.155 84 | - 0.375 25 | - 0.564 21 | 11 | + 0.239 23 | + 0.143 61 | - 0.382 83 | - 0.573 95 |
| 12 | + 0.203 37 | + 0.100 16 | - 0.303 52 | - 0.453 90 | 12 | + 0.218 85 | + 0.090 46 | - 0.309 32 | - 0.460 55 |
| 13 | + 0.191 38 | + 0.059 22 | - 0.250 58 | - 0.371 12 | 13 | + 0.203 73 | + 0.051 35 | - 0.255 07 | - 0.375 58 |
| 14 | + 0.181 90 | + 0.028 81 | - 0.210 71 | - 0.307 44 | 14 | + 0.191 91 | + 0.022 31 | - 0.214 22 | - 0.310 32 |
| 15 | + 0.174 12 | + 0.006 01 | - 0.180 13 | - 0.257 36 | 15 | + 0.182 33 | + 0.000 58 | - 0.182 90 | - 0.259 10 |
| 16 | + 0.167 56 | - 0.011 23 | - 0.156 32 | - 0.217 19 | 16 | + 0.174 35 | - 0.015 82 | - 0.158 53 | - 0.218 09 |
| 17 | + 0.161 93 | - 0.024 38 | - 0.137 55 | - 0.184 39 | 17 | + 0.167 57 | - 0.028 27 | - 0.139 30 | - 0.184 66 |
| 18 | + 0.157 05 | - 0.034 47 | - 0.122 58 | - 0.157 18 | 18 | + 0.161 75 | - 0.037 78 | - 0.123 98 | - 0.156 97 |
| 19 | + 0.152 80 | - 0.042 26 | - 0.110 54 | - 0.134 23 | 19 | + 0.156 72 | - 0.045 08 | - 0.111 65 | - 0.133 68 |
| 20 | + 0.149 09 | - 0.048 31 | - 0.100 78 | - 0.114 61 | 20 | + 0.152 35 | - 0.050 68 | - 0.101 66 | - 0.113 79 |
| 21 | + 0.145 86 | - 0.053 01 | - 0.092 86 | - 0.097 60 | 21 | + 0.148 54 | - 0.055 01 | - 0.093 54 | - 0.095 58 |
| 22 | + 0.143 07 | - 0.056 66 | - 0.086 40 | - 0.082 65 | 22 | + 0.145 24 | - 0.058 33 | - 0.086 92 | - 0.081 48 |
| 23 | + 0.140 67 | - 0.059 51 | - 0.081 17 | - 0.069 33 | 23 | + 0.142 39 | - 0.060 86 | - 0.081 53 | - 0.068 04 |
| 24 | + 0.138 64 | - 0.061 71 | - 0.076 93 | - 0.057 30 | 24 | + 0.139 95 | - 0.062 78 | - 0.077 17 | - 0.055 94 |
| 25 | + 0.136 93 | - 0.063 38 | - 0.073 56 | - 0.046 29 | 25 | + 0.137 89 | - 0.064 20 | - 0.073 68 | - 0.044 87 |
| 26 | + 0.135 58 | - 0.064 64 | - 0.070 94 | - 0.036 05 | 26 | + 0.136 16 | - 0.065 22 | - 0.070 96 | - 0.034 61 |
| 27 | + 0.134 53 | - 0.065 55 | - 0.068 98 | - 0.026 43 | 27 | + 0.134 78 | - 0.065 89 | - 0.068 90 | - 0.024 97 |
| 28 | + 0.133 77 | - 0.066 15 | - 0.067 61 | - 0.017 22 | 28 | + 0.133 71 | - 0.066 26 | - 0.067 44 | - 0.015 78 |
| 29 | + 0.133 30 | - 0.066 49 | - 0.066 82 | - 0.008 27 | 29 | + 0.132 94 | - 0.066 38 | - 0.066 55 | - 0.006 88 |
| 30 | + 0.133 12 | - 0.066 57 | - 0.066 55 | + 0.000 51 | 30 | + 0.132 45 | - 0.066 26 | - 0.066 20 | + 0.001 87 |
| 31 | + 0.133 22 | - 0.066 41 | - 0.066 81 | + 0.009 30 | 31 | + 0.132 25 | - 0.065 89 | - 0.066 35 | + 0.010 60 |
| 32 | + 0.133 61 | - 0.066 00 | - 0.067 60 | + 0.018 23 | 32 | + 0.132 34 | - 0.065 28 | - 0.067 06 | + 0.019 44 |
| 33 | + 0.134 28 | - 0.065 32 | - 0.068 96 | + 0.027 44 | 33 | + 0.132 70 | - 0.064 38 | - 0.068 31 | + 0.028 54 |
| 34 | + 0.135 25 | - 0.064 33 | - 0.070 91 | + 0.037 06 | 34 | + 0.133 34 | - 0.063 19 | - 0.070 16 | + 0.038 03 |
| 35 | + 0.136 51 | - 0.062 99 | - 0.073 53 | + 0.047 28 | 35 | + 0.134 27 | - 0.061 63 | - 0.072 64 | + 0.048 08 |
| 36 | + 0.138 10 | - 0.061 21 | - 0.076 88 | + 0.058 27 | 36 | + 0.135 49 | - 0.059 63 | - 0.075 86 | + 0.058 87 |
| 37 | + 0.140 01 | - 0.058 92 | - 0.081 09 | + 0.070 27 | 37 | + 0.137 02 | - 0.057 10 | - 0.079 91 | + 0.070 63 |
| 38 | + 0.142 27 | - 0.055 97 | - 0.086 30 | + 0.083 55 | 38 | + 0.138 86 | - 0.053 92 | - 0.084 95 | + 0.083 61 |
| 39 | + 0.144 90 | - 0.052 19 | - 0.092 72 | + 0.098 44 | 39 | + 0.141 03 | - 0.049 89 | - 0.091 15 | + 0.098 14 |
| 40 | + 0.147 95 | - 0.047 35 | - 0.100 59 | + 0.115 35 | 40 | + 0.143 56 | - 0.044 79 | - 0.098 76 | + 0.114 61 |
| 41 | + 0.151 43 | - 0.041 17 | - 0.110 28 | + 0.134 84 | 41 | + 0.146 46 | - 0.038 34 | - 0.108 13 | + 0.133 55 |
| 42 | + 0.155 43 | - 0.033 21 | - 0.122 23 | + 0.157 60 | 42 | + 0.149 78 | - 0.030 10 | - 0.119 68 | + 0.155 62 |
| 43 | + 0.160 00 | - 0.022 94 | - 0.137 06 | + 0.184 57 | 43 | + 0.153 57 | - 0.019 53 | - 0.134 03 | + 0.181 71 |
| 44 | + 0.165 26 | - 0.009 60 | - 0.155 66 | + 0.217 00 | 44 | + 0.157 89 | - 0.005 90 | - 0.151 99 | + 0.213 01 |
| 45 | + 0.171 35 | + 0.007 85 | - 0.179 20 | + 0.256 65 | 45 | + 0.162 86 | + 0.011 84 | - 0.174 71 | + 0.251 18 |
| 46 | + 0.178 54 | + 0.030 87 | - 0.209 41 | + 0.305 97 | 46 | + 0.168 67 | + 0.035 14 | - 0.203 81 | + 0.298 54 |
| 47 | + 0.187 24 | + 0.061 51 | - 0.248 75 | + 0.368 55 | 47 | + 0.175 61 | + 0.066 01 | - 0.241 63 | + 0.358 46 |
| 48 | + 0.198 20 | + 0.102 69 | - 0.300 91 | + 0.449 99 | 48 | + 0.184 28 | + 0.107 35 | - 0.291 64 | + 0.435 90 |
| 49 | + 0.212 80 | + 0.158 66 | - 0.371 45 | + 0.557 51 | 49 | + 0.195 77 | + 0.163 31 | - 0.359 07 | + 0.538 46 |
| 50 | + 0.233 70 | + 0.235 44 | - 0.469 14 | + 0.704 84 | 50 | + 0.212 25 | + 0.239 85 | - 0.452 11 | + 0.678 05 |
| 51 | + 0.266 43 | + 0.341 67 | - 0.608 10 | + 0.912 63 | 51 | + 0.238 32 | + 0.345 49 | - 0.583 82 | + 0.874 09 |
| 52 | + 0.322 91 | + 0.489 03 | - 0.811 95 | + 1.216 44 | 52 | + 0.284 04 | + 0.491 88 | - 0.775 91 | + 1.159 30 |
| 53 | + 0.430 39 | + 0.691 21 | - 1.121 59 | + 1.678 67 | 53 | + 0.372 52 | + 0.693 04 | - 1.065 56 | + 1.590 84 |
| 54 | + 0.654 64 | + 0.955 89 | - 1.610 52 | + 2.412 20 | 54 | + 0.559 82 | + 0.958 81 | - 1.518 64 | + 2.271 42 |
| 55 | + 1.163 22 | + 1.251 17 | - 2.414 40 | + 3.621 88 | 55 | + 0.988 62 | + 1.266 17 | - 2.254 78 | + 3.385 75 |
| 56 | + 2.309 22 | + 1.385 11 | - 3.784 32 | + 5.653 79 | 56 | + 2.034 82 | + 1.456 00 | - 3.490 84 | + 5.251 63 |
| 57 | + 5.511 93 | + 0.638 08 | - 6.150 01 | + 8.900 00 | 57 | + 4.672 67 | + 0.916 43 | - 5.589 09 | + 8.243 78 |
| 58 | + 12.932 86 | - 2.923 59 | - 10.009 26 | + 12.777 21 | 58 | + 11.007 05 | - 2.044 99 | - 8.062 05 | + 11.988 39 |
| 59 | + 26.185 67 | - 11.259 17 | - 14.926 49 | + 12.461 23 | 59 | + 22.761 17 | - 9.475 57 | - 13.285 60 | + 12.554 18 |

TABLE VII.—Continued.

VALUES OF A, B, C, AND D FOR THE ACTION OF VENUS ON THE MOON.

| System 2. | | | | | System 3. | | | | |
|-----------|-------------|------------|-------------|-------------|-----------|-------------|------------|-------------|-------------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +29.624 12 | -15.178 31 | -14.445 82 | + 3.083 50 | 0 | +28.095 38 | -14.200 70 | -13.804 59 | + 3.723 68 |
| 1 | +26.178 17 | -12.858 22 | -13.319 98 | - 7.553 34 | 1 | +25.108 12 | -12.240 65 | -12.867 46 | - 6.979 90 |
| 2 | +15.058 97 | - 5.374 64 | - 9.684 31 | -11.068 21 | 2 | +14.804 22 | - 5.334 68 | - 9.469 55 | -10.470 31 |
| 3 | + 7.082 50 | - 0.827 44 | - 6.255 07 | - 8.775 53 | 3 | + 7.142 71 | - 0.971 49 | - 6.171 21 | - 8.464 11 |
| 4 | + 3.272 10 | + 0.673 17 | - 3.945 29 | - 5.880 03 | 4 | + 3.368 04 | + 0.545 38 | - 3.913 41 | - 5.747 32 |
| 5 | + 1.637 83 | + 0.905 32 | - 2.543 15 | - 3.842 60 | 5 | + 1.709 07 | + 0.821 00 | - 2.530 07 | - 3.786 67 |
| 6 | + 0.926 81 | + 0.774 63 | - 1.701 45 | - 2.571 56 | 6 | + 0.973 32 | + 0.721 94 | - 1.695 25 | - 2.546 14 |
| 7 | + 0.597 76 | + 0.586 40 | - 1.184 10 | - 1.785 90 | 7 | + 0.627 53 | + 0.553 13 | - 1.180 66 | - 1.772 84 |
| 8 | + 0.432 83 | + 0.422 37 | - 0.855 20 | - 1.287 47 | 8 | + 0.452 10 | + 0.400 75 | - 0.852 85 | - 1.279 74 |
| 9 | + 0.342 73 | + 0.295 72 | - 0.638 46 | - 0.959 70 | 9 | + 0.355 45 | + 0.281 22 | - 0.636 65 | - 0.954 45 |
| 10 | + 0.289 09 | + 0.201 73 | - 0.490 82 | - 0.736 06 | 10 | + 0.297 60 | + 0.191 71 | - 0.489 33 | - 0.732 10 |
| 11 | + 0.254 43 | + 0.132 76 | - 0.387 20 | - 0.578 14 | 11 | + 0.260 20 | + 0.125 69 | - 0.385 89 | - 0.574 91 |
| 12 | + 0.230 36 | + 0.082 14 | - 0.312 52 | - 0.463 12 | 12 | + 0.234 28 | + 0.077 06 | - 0.311 33 | - 0.460 36 |
| 13 | + 0.212 60 | + 0.044 82 | - 0.257 41 | - 0.377 00 | 13 | + 0.215 22 | + 0.041 10 | - 0.256 34 | - 0.374 58 |
| 14 | + 0.198 84 | + 0.017 09 | - 0.215 94 | - 0.310 93 | 14 | + 0.200 55 | + 0.014 37 | - 0.214 94 | - 0.308 76 |
| 15 | + 0.187 78 | - 0.003 64 | - 0.184 16 | - 0.259 12 | 15 | + 0.188 83 | - 0.005 63 | - 0.183 21 | - 0.257 16 |
| 16 | + 0.178 66 | - 0.019 25 | - 0.159 42 | - 0.217 69 | 16 | + 0.179 21 | - 0.020 68 | - 0.158 52 | - 0.215 91 |
| 17 | + 0.170 99 | - 0.031 07 | - 0.139 91 | - 0.183 97 | 17 | + 0.171 14 | - 0.032 08 | - 0.139 06 | - 0.182 35 |
| 18 | + 0.164 44 | - 0.040 06 | - 0.124 37 | - 0.156 06 | 18 | + 0.164 29 | - 0.040 74 | - 0.123 55 | - 0.154 59 |
| 19 | + 0.158 80 | - 0.046 93 | - 0.111 87 | - 0.132 62 | 19 | + 0.158 41 | - 0.047 33 | - 0.111 08 | - 0.131 28 |
| 20 | + 0.153 92 | - 0.052 17 | - 0.101 74 | - 0.112 64 | 20 | + 0.153 33 | - 0.052 36 | - 0.100 98 | - 0.111 43 |
| 21 | + 0.149 68 | - 0.056 17 | - 0.093 50 | - 0.095 37 | 21 | + 0.148 94 | - 0.056 18 | - 0.092 76 | - 0.094 27 |
| 22 | + 0.146 00 | - 0.059 21 | - 0.086 79 | - 0.080 24 | 22 | + 0.145 14 | - 0.059 07 | - 0.086 06 | - 0.079 25 |
| 23 | + 0.142 82 | - 0.061 50 | - 0.081 32 | - 0.066 80 | 23 | + 0.141 84 | - 0.061 24 | - 0.080 60 | - 0.065 93 |
| 24 | + 0.140 09 | - 0.063 20 | - 0.076 89 | - 0.054 70 | 24 | + 0.139 01 | - 0.062 82 | - 0.076 17 | - 0.053 94 |
| 25 | + 0.137 75 | - 0.064 41 | - 0.073 34 | - 0.043 66 | 25 | + 0.136 59 | - 0.063 95 | - 0.072 63 | - 0.043 00 |
| 26 | + 0.135 79 | - 0.065 24 | - 0.070 55 | - 0.033 45 | 26 | + 0.134 54 | - 0.064 70 | - 0.069 85 | - 0.032 89 |
| 27 | + 0.134 17 | - 0.065 74 | - 0.068 44 | - 0.023 86 | 27 | + 0.132 86 | - 0.065 13 | - 0.067 73 | - 0.023 41 |
| 28 | + 0.132 88 | - 0.065 95 | - 0.066 92 | - 0.014 73 | 28 | + 0.131 50 | - 0.065 29 | - 0.066 22 | - 0.014 39 |
| 29 | + 0.131 89 | - 0.065 92 | - 0.065 98 | - 0.005 91 | 29 | + 0.130 46 | - 0.065 21 | - 0.065 26 | - 0.005 68 |
| 30 | + 0.131 21 | - 0.065 64 | - 0.065 56 | + 0.002 75 | 30 | + 0.129 72 | - 0.064 89 | - 0.064 83 | - 0.002 87 |
| 31 | + 0.130 81 | - 0.065 13 | - 0.065 67 | + 0.011 37 | 31 | + 0.129 27 | - 0.064 34 | - 0.064 92 | + 0.011 38 |
| 32 | + 0.130 68 | - 0.064 38 | - 0.066 31 | + 0.020 09 | 32 | + 0.129 10 | - 0.063 57 | - 0.065 54 | + 0.019 98 |
| 33 | + 0.130 84 | - 0.063 36 | - 0.067 49 | + 0.029 05 | 33 | + 0.129 21 | - 0.062 53 | - 0.066 69 | + 0.028 80 |
| 34 | + 0.131 28 | - 0.062 03 | - 0.069 25 | + 0.038 38 | 34 | + 0.129 60 | - 0.061 19 | - 0.068 42 | + 0.038 00 |
| 35 | + 0.131 99 | - 0.060 35 | - 0.071 65 | + 0.048 25 | 35 | + 0.130 28 | - 0.059 50 | - 0.070 77 | + 0.047 71 |
| 36 | + 0.132 99 | - 0.058 23 | - 0.074 76 | + 0.058 83 | 36 | + 0.131 23 | - 0.057 40 | - 0.073 84 | + 0.058 14 |
| 37 | + 0.134 28 | - 0.055 58 | - 0.078 69 | + 0.070 35 | 37 | + 0.132 48 | - 0.054 78 | - 0.077 71 | + 0.079 47 |
| 38 | + 0.135 86 | - 0.052 28 | - 0.083 59 | + 0.083 44 | 38 | + 0.134 04 | - 0.051 51 | - 0.082 52 | + 0.081 97 |
| 39 | + 0.137 75 | - 0.048 15 | - 0.089 62 | + 0.097 23 | 39 | + 0.135 90 | - 0.047 44 | - 0.088 46 | + 0.095 94 |
| 40 | + 0.139 98 | - 0.042 95 | - 0.097 02 | + 0.113 30 | 40 | + 0.138 10 | - 0.042 35 | - 0.095 76 | + 0.111 77 |
| 41 | + 0.142 55 | - 0.036 42 | - 0.106 13 | + 0.131 75 | 41 | + 0.140 66 | - 0.035 93 | - 0.104 73 | + 0.129 93 |
| 42 | + 0.145 50 | - 0.028 12 | - 0.117 37 | + 0.153 23 | 42 | + 0.143 60 | - 0.027 81 | - 0.115 80 | + 0.151 08 |
| 43 | + 0.148 85 | - 0.017 55 | - 0.131 31 | + 0.178 57 | 43 | + 0.146 68 | - 0.017 46 | - 0.129 53 | + 0.176 04 |
| 44 | + 0.152 69 | - 0.003 95 | - 0.148 75 | + 0.208 95 | 44 | + 0.150 85 | - 0.004 19 | - 0.146 68 | + 0.205 95 |
| 45 | + 0.157 09 | + 0.013 68 | - 0.170 77 | + 0.245 92 | 45 | + 0.155 33 | + 0.013 00 | - 0.168 33 | + 0.242 36 |
| 46 | + 0.162 22 | + 0.036 71 | - 0.198 94 | + 0.291 73 | 46 | + 0.160 59 | + 0.035 42 | - 0.196 01 | + 0.287 47 |
| 47 | + 0.168 34 | + 0.067 12 | - 0.235 47 | + 0.349 57 | 47 | + 0.166 02 | + 0.064 96 | - 0.231 89 | + 0.344 43 |
| 48 | + 0.175 98 | + 0.107 68 | - 0.283 65 | + 0.424 17 | 48 | + 0.174 89 | + 0.104 27 | - 0.279 15 | + 0.417 85 |
| 49 | + 0.186 10 | + 0.162 34 | - 0.348 43 | + 0.522 71 | 49 | + 0.185 54 | + 0.157 09 | - 0.342 64 | + 0.514 83 |
| 50 | + 0.200 72 | + 0.236 76 | - 0.437 47 | + 0.656 44 | 50 | + 0.201 00 | + 0.228 74 | - 0.429 76 | + 0.646 33 |
| 51 | + 0.224 03 | + 0.338 93 | - 0.562 96 | + 0.843 60 | 51 | + 0.225 68 | + 0.326 64 | - 0.552 32 | + 0.830 17 |
| 52 | + 0.265 29 | + 0.479 66 | - 0.744 95 | + 1.114 72 | 52 | + 0.269 11 | + 0.460 54 | - 0.729 66 | + 1.096 02 |
| 53 | + 0.345 71 | + 0.671 72 | - 1.017 42 | + 1.522 77 | 53 | + 0.353 01 | + 0.641 40 | - 0.994 42 | + 1.495 08 |
| 54 | + 0.516 42 | + 0.923 41 | - 1.439 82 | + 2.161 97 | 54 | + 0.529 02 | + 0.874 36 | - 1.403 38 | + 2.117 62 |
| 55 | + 0.906 36 | + 1.211 94 | - 2.118 20 | + 3.200 54 | 55 | + 0.925 56 | + 1.131 69 | - 2.057 25 | + 3.122 67 |
| 56 | + 1.850 77 | + 1.390 39 | - 3.241 16 | + 4.919 24 | 56 | + 1.870 94 | + 1.262 21 | - 3.133 16 | + 4.769 08 |
| 57 | + 4.204 51 | + 0.910 34 | - 5.114 84 | + 7.648 85 | 57 | + 4.183 37 | + 0.732 85 | - 4.916 23 | + 7.341 83 |
| 58 | + 9.792 93 | - 1.714 51 | - 8.078 43 | + 11.072 42 | 58 | + 9.552 47 | - 1.834 00 | - 7.718 48 | + 10.479 49 |
| 59 | + 20.207 75 | - 8.331 97 | - 11.875 75 | + 11.864 03 | 59 | + 19.331 99 | - 8.023 85 | - 11.308 13 | + 11.063 99 |

TABLE VII.—Continued.

VALUES OF A, B, C, AND D FOR THE ACTION OF VENUS ON THE MOON.

| System 4. | | | | | System 5. | | | | |
|-----------|-------------|------------|-------------|-------------|-----------|-------------|------------|-------------|-------------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +27.753 75 | -13.040 94 | -13.812 81 | + 2.712 93 | 0 | +27.639 90 | -13.806 76 | -13.833 14 | + 1.162 19 |
| 1 | +24.108 07 | -11.431 47 | -12.676 62 | - 7.271 93 | 1 | +22.709 15 | -10.437 90 | -12.271 23 | - 8.008 99 |
| 2 | +14.090 02 | - 4.811 77 | - 9.228 26 | -10.185 94 | 2 | +12.869 67 | - 4.118 27 | - 8.751 42 | -10.017 52 |
| 3 | + 6.826 96 | - 0.838 85 | - 5.983 13 | - 8.143 97 | 3 | + 6.173 36 | - 0.530 43 | - 5.642 95 | - 7.784 12 |
| 4 | + 3.245 71 | + 0.550 49 | - 3.799 20 | - 5.536 29 | 4 | + 2.934 11 | + 0.648 51 | - 3.582 61 | - 5.291 65 |
| 5 | + 1.659 31 | + 0.798 41 | - 2.457 70 | - 3.661 70 | 5 | + 1.504 82 | + 0.824 85 | - 2.329 66 | - 3.485 48 |
| 6 | + 0.949 72 | + 0.700 16 | - 1.649 89 | - 2.471 69 | 6 | + 0.865 47 | + 0.706 39 | - 1.571 85 | - 2.362 90 |
| 7 | + 0.613 90 | + 0.537 34 | - 1.151 26 | - 1.726 69 | 7 | + 0.562 89 | + 0.539 22 | - 1.102 12 | - 1.658 68 |
| 8 | + 0.442 70 | + 0.390 37 | - 0.833 07 | - 1.249 77 | 8 | + 0.408 83 | + 0.392 14 | - 0.800 98 | - 1.205 16 |
| 9 | + 0.348 10 | + 0.274 76 | - 0.622 86 | - 0.934 13 | 9 | + 0.323 90 | + 0.277 25 | - 0.601 14 | - 0.904 24 |
| 10 | + 0.291 44 | + 0.187 92 | - 0.479 37 | - 0.717 80 | 10 | + 0.273 16 | + 0.191 03 | - 0.464 18 | - 0.697 23 |
| 11 | + 0.254 83 | + 0.123 66 | - 0.378 48 | - 0.564 54 | 11 | + 0.240 42 | + 0.127 12 | - 0.367 55 | - 0.550 08 |
| 12 | + 0.229 48 | + 0.076 19 | - 0.305 68 | - 0.452 65 | 12 | + 0.217 78 | + 0.079 80 | - 0.297 59 | - 0.442 33 |
| 13 | + 0.210 89 | + 0.041 01 | - 0.251 91 | - 0.368 74 | 13 | + 0.201 16 | + 0.044 61 | - 0.245 78 | - 0.361 30 |
| 14 | + 0.196 60 | + 0.014 79 | - 0.211 39 | - 0.304 29 | 14 | + 0.188 36 | + 0.018 28 | - 0.206 64 | - 0.298 91 |
| 15 | + 0.185 20 | - 0.004 89 | - 0.180 31 | - 0.253 70 | 15 | + 0.178 13 | - 0.001 56 | - 0.176 56 | - 0.249 82 |
| 16 | + 0.175 85 | - 0.019 74 | - 0.156 12 | - 0.213 22 | 16 | + 0.169 73 | - 0.016 61 | - 0.153 10 | - 0.210 47 |
| 17 | + 0.168 03 | - 0.031 01 | - 0.137 03 | - 0.180 25 | 17 | + 0.162 67 | - 0.028 11 | - 0.134 57 | - 0.178 36 |
| 18 | + 0.161 41 | - 0.039 59 | - 0.121 80 | - 0.152 97 | 18 | + 0.156 68 | - 0.036 92 | - 0.119 77 | - 0.151 73 |
| 19 | + 0.155 71 | - 0.046 15 | - 0.109 56 | - 0.130 05 | 19 | + 0.151 53 | - 0.043 69 | - 0.107 85 | - 0.129 33 |
| 20 | + 0.150 82 | - 0.051 17 | - 0.099 64 | - 0.110 51 | 20 | + 0.147 10 | - 0.048 92 | - 0.098 19 | - 0.110 20 |
| 21 | + 0.146 57 | - 0.055 01 | - 0.091 56 | - 0.093 62 | 21 | + 0.143 28 | - 0.052 95 | - 0.090 31 | - 0.093 64 |
| 22 | + 0.142 90 | - 0.057 92 | - 0.084 98 | - 0.078 83 | 22 | + 0.139 97 | - 0.056 07 | - 0.083 90 | - 0.079 12 |
| 23 | + 0.139 75 | - 0.060 12 | - 0.079 62 | - 0.065 70 | 23 | + 0.137 13 | - 0.058 47 | - 0.078 68 | - 0.065 21 |
| 24 | + 0.137 03 | - 0.061 75 | - 0.075 28 | - 0.053 88 | 24 | + 0.134 73 | - 0.060 28 | - 0.074 44 | - 0.054 57 |
| 25 | + 0.134 73 | - 0.062 93 | - 0.071 80 | - 0.043 10 | 25 | + 0.132 70 | - 0.061 64 | - 0.071 06 | - 0.043 94 |
| 26 | + 0.132 80 | - 0.063 74 | - 0.069 07 | - 0.033 13 | 26 | + 0.131 03 | - 0.062 62 | - 0.068 42 | - 0.034 99 |
| 27 | + 0.131 22 | - 0.064 23 | - 0.067 00 | - 0.023 77 | 27 | + 0.129 70 | - 0.063 28 | - 0.066 41 | - 0.024 84 |
| 28 | + 0.129 97 | - 0.064 45 | - 0.065 51 | - 0.014 86 | 28 | + 0.128 69 | - 0.063 60 | - 0.065 00 | - 0.016 02 |
| 29 | + 0.129 04 | - 0.064 44 | - 0.064 59 | - 0.006 25 | 29 | + 0.127 98 | - 0.063 85 | - 0.064 13 | - 0.007 48 |
| 30 | + 0.128 40 | - 0.064 21 | - 0.064 19 | + 0.002 19 | 30 | + 0.127 58 | - 0.063 79 | - 0.063 79 | + 0.000 92 |
| 31 | + 0.128 06 | - 0.063 75 | - 0.064 30 | + 0.010 61 | 31 | + 0.127 47 | - 0.063 51 | - 0.063 96 | + 0.009 30 |
| 32 | + 0.127 99 | - 0.063 06 | - 0. 64 94 | + 0.019 12 | 32 | + 0.127 64 | - 0.063 00 | - 0.064 65 | + 0.017 79 |
| 33 | + 0.128 22 | - 0.062 12 | - 0.066 11 | + 0.027 87 | 33 | + 0.128 12 | - 0.062 25 | - 0.065 87 | + 0.026 52 |
| 34 | + 0.128 75 | - 0.060 89 | - 0.067 84 | + 0.036 98 | 34 | + 0.128 90 | - 0.061 22 | - 0.067 68 | + 0.035 65 |
| 35 | + 0.129 55 | - 0.059 33 | - 0.070 22 | + 0.046 63 | 35 | + 0.129 98 | - 0.059 87 | - 0.070 11 | + 0.045 33 |
| 36 | + 0.130 66 | - 0.057 36 | - 0.073 29 | + 0.056 99 | 36 | + 0.131 39 | - 0.058 12 | - 0.073 26 | + 0.055 75 |
| 37 | + 0.132 07 | - 0.054 90 | - 0.077 18 | + 0.068 27 | 37 | + 0.133 13 | - 0.055 89 | - 0.077 23 | + 0.067 11 |
| 38 | + 0.133 81 | - 0.051 82 | - 0.082 00 | + 0.080 73 | 38 | + 0.135 23 | - 0.053 05 | - 0.082 17 | + 0.079 68 |
| 39 | + 0.135 90 | - 0.047 94 | - 0.087 95 | + 0.094 66 | 39 | + 0.137 72 | - 0.049 45 | - 0.088 25 | + 0.093 78 |
| 40 | + 0.138 34 | - 0.043 08 | - 0.095 27 | + 0.110 47 | 40 | + 0.140 62 | - 0.044 89 | - 0.095 73 | + 0.109 81 |
| 41 | + 0.141 20 | - 0.036 93 | - 0.104 26 | + 0.128 64 | 41 | + 0.144 00 | - 0.039 07 | - 0.104 93 | + 0.128 28 |
| 42 | + 0.144 49 | - 0.029 13 | - 0.115 36 | + 0.149 82 | 42 | + 0.147 93 | - 0.031 63 | - 0.116 28 | + 0.149 86 |
| 43 | + 0.148 29 | - 0.019 17 | - 0.129 14 | + 0.174 86 | 43 | + 0.152 47 | - 0.022 08 | - 0.130 40 | + 0.175 44 |
| 44 | + 0.152 71 | - 0.006 34 | - 0.146 36 | + 0.204 92 | 44 | + 0.157 79 | - 0.009 72 | - 0.148 08 | + 0.206 20 |
| 45 | + 0.157 85 | + 0.010 28 | - 0.168 13 | + 0.241 57 | 45 | + 0.164 07 | + 0.006 38 | - 0.170 44 | + 0.243 82 |
| 46 | + 0.163 99 | + 0.032 00 | - 0.195 07 | + 0.287 04 | 46 | + 0.171 62 | + 0.027 48 | - 0.199 11 | + 0.290 63 |
| 47 | + 0.171 48 | + 0.060 63 | - 0.232 09 | + 0.344 55 | 47 | + 0.180 98 | + 0.055 39 | - 0.236 37 | + 0.349 98 |
| 48 | + 0.181 02 | + 0.098 73 | - 0.279 74 | + 0.418 83 | 48 | + 0.193 04 | + 0.092 61 | - 0.285 64 | + 0.426 86 |
| 49 | + 0.193 91 | + 0.149 90 | - 0.343 80 | + 0.517 08 | 49 | + 0.209 45 | + 0.142 64 | - 0.352 07 | + 0.528 85 |
| 50 | + 0.212 65 | + 0.219 19 | - 0.431 84 | + 0.650 55 | 50 | + 0.233 30 | + 0.210 35 | - 0.443 66 | + 0.667 81 |
| 51 | + 0.242 36 | + 0.313 54 | - 0.555 90 | + 0.837 40 | 51 | + 0.270 84 | + 0.302 33 | - 0.573 16 | + 0.862 91 |
| 52 | + 0.293 93 | + 0.441 78 | - 0.735 71 | + 1.107 89 | 52 | + 0.335 07 | + 0.426 52 | - 0.761 61 | + 1.146 11 |
| 53 | + 0.391 71 | + 0.612 99 | - 1.004 72 | + 1.514 05 | 53 | + 0.454 69 | + 0.590 01 | - 1.044 70 | + 1.572 14 |
| 54 | + 0.592 84 | + 0.828 29 | - 1.421 12 | + 2.147 02 | 54 | + 0.696 05 | + 0.788 84 | - 1.484 88 | + 2.236 29 |
| 55 | + 1.037 24 | + 1.051 11 | - 2.088 36 | + 3.165 03 | 55 | + 1.219 39 | + 0.973 68 | - 2.193 08 | + 3.301 12 |
| 56 | + 2.076 20 | + 1.112 03 | - 3.188 23 | + 4.817 35 | 56 | + 2.419 26 | + 0.943 90 | - 3.363 18 | + 5.010 76 |
| 57 | + 4.561 11 | + 0.450 28 | - 5.011 40 | + 7.344 32 | 57 | + 5.219 73 | + 0.077 57 | - 5.297 30 | + 7.547 59 |
| 58 | + 10.154 89 | - 2.290 72 | - 7.864 16 | + 10.250 29 | 58 | + 11.281 01 | - 3.005 64 | - 8.275 35 | + 10.190 86 |
| 59 | + 19.856 15 | - 8.398 13 | - 11.458 03 | + 10.295 66 | 59 | + 21.042 69 | - 9.193 81 | - 11.848 89 | + 9.390 27 |

TABLE VII.—Continued.

VALUES OF A, B, C, AND D FOR THE ACTION OF VENUS ON THE MOON.

| System 6. | | | | | System 7. | | | | |
|-----------|-------------|-------------|-------------|-------------|-----------|-------------|-------------|-------------|-------------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +27.168 05 | -13.660 15 | -13.507 87 | - 0.614 53 | 0 | +26.709 86 | -13.595 11 | -13.114 76 | - 2.251 50 |
| 1 | +20.933 58 | - 9.364 52 | -11.569 06 | - 8.339 67 | 1 | +19.448 82 | - 8.466 86 | -10.981 95 | - 9.682 40 |
| 2 | +11.413 64 | - 3.292 23 | - 8.121 39 | - 9.888 68 | 2 | +10.203 37 | - 2.547 15 | - 7.656 24 | - 9.022 08 |
| 3 | + 5.381 20 | - 0.147 12 | - 5.234 09 | - 7.440 99 | 3 | + 4.702 14 | + 0.247 41 | - 4.949 55 | - 7.249 30 |
| 4 | + 2.541 06 | + 0.802 84 | - 3.343 88 | - 4.990 86 | 4 | + 2.189 26 | + 0.993 76 | - 3.183 00 | - 4.817 24 |
| 5 | + 1.301 93 | + 0.889 85 | - 2.191 79 | - 3.310 41 | 5 | + 1.112 88 | + 0.987 87 | - 2.100 76 | - 3.191 27 |
| 6 | + 0.751 59 | + 0.738 57 | - 1.490 15 | - 2.252 64 | 6 | + 0.642 27 | + 0.794 77 | - 1.437 02 | - 2.175 89 |
| 7 | + 0.493 04 | + 0.558 84 | - 1.051 87 | - 1.588 25 | 7 | + 0.424 78 | + 0.594 79 | - 1.019 58 | - 1.539 05 |
| 8 | + 0.362 49 | + 0.406 35 | - 0.768 85 | - 1.159 95 | 8 | + 0.316 91 | + 0.431 49 | - 0.748 40 | - 1.128 06 |
| 9 | + 0.291 15 | + 0.288 68 | - 0.579 82 | - 0.874 26 | 9 | + 0.258 97 | + 0.307 39 | - 0.566 37 | - 0.853 30 |
| 10 | + 0.248 83 | + 0.200 73 | - 0.449 54 | - 0.676 95 | 10 | + 0.225 10 | + 0.215 27 | - 0.440 39 | - 0.663 03 |
| 11 | + 0.221 64 | + 0.135 56 | - 0.357 19 | - 0.536 17 | 11 | + 0.203 54 | + 0.147 21 | - 0.350 75 | - 0.526 89 |
| 12 | + 0.202 85 | + 0.087 21 | - 0.290 06 | - 0.432 71 | 12 | + 0.188 67 | + 0.096 73 | - 0.285 40 | - 0.426 57 |
| 13 | + 0.189 02 | + 0.051 15 | - 0.240 17 | - 0.354 65 | 13 | + 0.177 68 | + 0.059 04 | - 0.236 72 | - 0.350 68 |
| 14 | + 0.178 33 | + 0.024 06 | - 0.202 37 | - 0.249 35 | 14 | + 0.169 10 | + 0.030 66 | - 0.199 77 | - 0.291 91 |
| 15 | + 0.169 72 | + 0.003 54 | - 0.173 25 | - 0.246 79 | 15 | + 0.162 13 | + 0.009 12 | - 0.171 25 | - 0.245 43 |
| 16 | + 0.162 59 | - 0.012 10 | - 0.150 49 | - 0.208 55 | 16 | + 0.156 30 | - 0.007 38 | - 0.148 93 | - 0.207 99 |
| 17 | + 0.156 58 | - 0.024 12 | - 0.132 48 | - 0.177 28 | 17 | + 0.151 34 | - 0.020 10 | - 0.131 25 | - 0.177 29 |
| 18 | + 0.151 46 | - 0.033 39 | - 0.118 07 | - 0.151 29 | 18 | + 0.147 08 | - 0.029 98 | - 0.117 09 | - 0.151 73 |
| 19 | + 0.147 05 | - 0.040 59 | - 0.106 46 | - 0.129 37 | 19 | + 0.143 38 | - 0.037 71 | - 0.105 68 | - 0.130 12 |
| 20 | + 0.143 24 | - 0.046 21 | - 0.097 03 | - 0.110 61 | 20 | + 0.140 19 | - 0.043 78 | - 0.096 42 | - 0.111 60 |
| 21 | + 0.139 95 | - 0.050 60 | - 0.089 36 | - 0.094 35 | 21 | + 0.137 45 | - 0.048 56 | - 0.088 87 | - 0.095 51 |
| 22 | + 0.137 13 | - 0.054 04 | - 0.083 10 | - 0.080 05 | 22 | + 0.135 09 | - 0.052 36 | - 0.082 73 | - 0.081 34 |
| 23 | + 0.134 72 | - 0.056 72 | - 0.078 00 | - 0.067 31 | 23 | + 0.133 11 | - 0.055 37 | - 0.077 73 | - 0.068 68 |
| 24 | + 0.132 70 | - 0.058 81 | - 0.073 88 | - 0.055 81 | 24 | + 0.131 47 | - 0.057 75 | - 0.073 71 | - 0.057 24 |
| 25 | + 0.131 04 | - 0.060 43 | - 0.070 60 | - 0.045 28 | 25 | + 0.130 15 | - 0.059 64 | - 0.070 51 | - 0.046 74 |
| 26 | + 0.129 70 | - 0.061 66 | - 0.068 04 | - 0.035 51 | 26 | + 0.129 14 | - 0.061 13 | - 0.068 03 | - 0.036 98 |
| 27 | + 0.128 69 | - 0.062 57 | - 0.066 12 | - 0.026 31 | 27 | + 0.128 44 | - 0.062 27 | - 0.065 19 | - 0.027 77 |
| 28 | + 0.127 99 | - 0.063 20 | - 0.064 78 | - 0.017 52 | 28 | + 0.128 04 | - 0.063 12 | - 0.064 93 | - 0.018 95 |
| 29 | + 0.127 58 | - 0.063 59 | - 0.064 00 | - 0.008 99 | 29 | + 0.127 93 | - 0.063 72 | - 0.064 21 | - 0.010 37 |
| 30 | + 0.127 47 | - 0.063 75 | - 0.063 73 | - 0.000 59 | 30 | + 0.128 11 | - 0.064 08 | - 0.064 02 | - 0.001 91 |
| 31 | + 0.127 66 | - 0.063 68 | - 0.063 97 | + 0.007 82 | 31 | + 0.128 53 | - 0.064 23 | - 0.064 36 | + 0.006 58 |
| 32 | + 0.128 14 | - 0.063 40 | - 0.064 75 | + 0.016 35 | 32 | + 0.129 37 | - 0.064 14 | - 0.065 23 | + 0.015 22 |
| 33 | + 0.128 93 | - 0.062 87 | - 0.066 06 | + 0.025 16 | 33 | + 0.130 46 | - 0.063 82 | - 0.066 66 | + 0.024 15 |
| 34 | + 0.130 03 | - 0.062 07 | - 0.067 96 | + 0.034 39 | 34 | + 0.131 88 | - 0.063 20 | - 0.068 67 | + 0.033 52 |
| 35 | + 0.131 46 | - 0.060 95 | - 0.070 52 | + 0.044 19 | 35 | + 0.133 65 | - 0.062 28 | - 0.071 36 | + 0.043 50 |
| 36 | + 0.133 25 | - 0.059 43 | - 0.073 80 | + 0.054 76 | 36 | + 0.135 77 | - 0.060 97 | - 0.074 81 | + 0.054 29 |
| 37 | + 0.135 38 | - 0.057 46 | - 0.077 93 | + 0.066 33 | 37 | + 0.138 31 | - 0.059 19 | - 0.079 12 | + 0.066 11 |
| 38 | + 0.137 94 | - 0.054 88 | - 0.083 05 | + 0.079 15 | 38 | + 0.141 28 | - 0.056 83 | - 0.084 45 | + 0.079 25 |
| 39 | + 0.140 92 | - 0.051 56 | - 0.089 35 | + 0.093 57 | 39 | + 0.144 74 | - 0.053 72 | - 0.091 01 | + 0.094 04 |
| 40 | + 0.144 39 | - 0.047 29 | - 0.097 11 | + 0.110 00 | 40 | + 0.148 74 | - 0.049 66 | - 0.099 08 | + 0.110 93 |
| 41 | + 0.148 43 | - 0.041 77 | - 0.106 65 | + 0.128 98 | 41 | + 0.153 39 | - 0.044 38 | - 0.109 00 | + 0.130 48 |
| 42 | + 0.153 10 | - 0.034 67 | - 0.118 44 | + 0.151 20 | 42 | + 0.158 77 | - 0.037 50 | - 0.121 27 | + 0.153 42 |
| 43 | + 0.158 55 | - 0.025 46 | - 0.133 11 | + 0.177 61 | 43 | + 0.165 05 | - 0.028 53 | - 0.136 53 | + 0.180 72 |
| 44 | + 0.164 95 | - 0.013 47 | - 0.151 49 | + 0.209 47 | 44 | + 0.172 46 | - 0.016 77 | - 0.155 67 | + 0.213 73 |
| 45 | + 0.172 57 | + 0.002 22 | - 0.174 80 | + 0.248 52 | 45 | + 0.181 29 | - 0.001 33 | - 0.179 97 | + 0.254 26 |
| 46 | + 0.181 82 | + 0.022 90 | - 0.204 72 | + 0.297 23 | 46 | + 0.192 06 | + 0.019 11 | - 0.211 17 | + 0.304 93 |
| 47 | + 0.193 36 | + 0.050 33 | - 0.243 70 | + 0.359 18 | 47 | + 0.205 57 | + 0.046 31 | - 0.251 88 | + 0.369 51 |
| 48 | + 0.208 36 | + 0.087 00 | - 0.295 37 | + 0.439 67 | 48 | + 0.223 17 | + 0.082 74 | - 0.305 90 | + 0.453 58 |
| 49 | + 0.228 84 | + 0.136 37 | - 0.365 20 | + 0.546 76 | 49 | + 0.247 21 | + 0.131 82 | - 0.379 03 | + 0.565 69 |
| 50 | + 0.258 60 | + 0.203 17 | - 0.461 77 | + 0.693 12 | 50 | + 0.282 11 | + 0.198 18 | - 0.480 29 | + 0.719 23 |
| 51 | + 0.305 13 | + 0.293 60 | - 0.598 74 | + 0.899 21 | 51 | + 0.336 42 | + 0.287 73 | - 0.624 15 | + 0.935 91 |
| 52 | + 0.383 93 | + 0.414 79 | - 0.798 70 | + 1.199 13 | 52 | + 0.427 73 | + 0.406 76 | - 0.834 50 | + 1.251 84 |
| 53 | + 0.528 66 | + 0.571 44 | - 1.100 11 | + 1.651 13 | 53 | + 0.594 08 | + 0.557 85 | - 1.151 93 | + 1.728 56 |
| 54 | + 0.816 50 | + 0.753 57 | - 1.570 07 | + 2.355 73 | 54 | + 0.921 98 | + 0.725 14 | - 1.647 13 | + 2.471 57 |
| 55 | + 1.431 37 | + 0.895 83 | - 2.327 19 | + 3.480 82 | 55 | + 1.616 38 | + 0.827 45 | - 2.443 83 | + 3.653 74 |
| 56 | + 2.817 66 | + 0.757 50 | - 3.575 16 | + 5.262 94 | 56 | + 3.166 15 | + 0.584 08 | - 3.750 22 | + 5.503 98 |
| 57 | + 5.977 20 | - 0.362 00 | - 5.615 20 | + 7.807 13 | 57 | + 6.641 59 | - 0.784 55 | - 5.857 04 | + 8.051 79 |
| 58 | + 12.528 32 | - 3.866 93 | - 8.661 40 | + 10.107 54 | 58 | + 13.612 05 | - 4.704 84 | - 8.907 20 | + 10.018 16 |
| 59 | + 22.187 74 | - 10.133 34 | - 12.054 39 | + 8.285 33 | 59 | + 23.132 00 | - 11.051 60 | - 12.080 40 | + 7.240 47 |

TABLE VII.—Continued.

VALUES OF A, B, C, AND D FOR THE ACTION OF VENUS ON THE MOON.

| System 8. | | | | | System 9. | | | | |
|-----------|------------|------------|------------|------------|-----------|------------|------------|------------|------------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +27.214 80 | -13.938 26 | -13.276 55 | - 3.500 11 | 0 | +29.406 78 | -14.968 87 | -14.437 91 | - 4.127 09 |
| 1 | +19.039 87 | - 8.020 33 | -11.019 53 | -10.665 09 | 1 | +20.202 62 | - 8.251 18 | -11.951 44 | -11.843 65 |
| 2 | + 9.631 65 | - 1.990 26 | - 7.641 36 | -10.302 17 | 2 | + 9.902 42 | - 1.721 59 | - 8.180 82 | -11.106 40 |
| 3 | + 4.310 63 | + 0.617 44 | - 4.928 09 | - 7.329 55 | 3 | + 4.288 72 | - 0.911 18 | - 5.199 88 | - 7.719 82 |
| 4 | + 1.960 54 | + 1.206 21 | - 3.166 75 | - 4.809 35 | 4 | + 1.894 56 | + 1.406 55 | - 3.301 10 | - 4.984 16 |
| 5 | + 0.980 06 | + 1.109 85 | - 2.089 90 | - 3.167 93 | 5 | + 0.925 98 | + 1.232 53 | - 2.158 52 | - 3.248 67 |
| 6 | + 0.561 76 | + 0.868 13 | - 1.429 89 | - 2.155 37 | 6 | + 0.524 26 | + 0.942 42 | - 1.466 67 | - 2.195 56 |
| 7 | + 0.373 31 | + 0.641 49 | - 1.014 79 | - 1.524 13 | 7 | + 0.348 15 | + 0.687 36 | - 1.035 53 | - 1.546 04 |
| 8 | + 0.282 29 | + 0.462 81 | - 0.745 09 | - 1.117 93 | 8 | + 0.265 37 | + 0.491 96 | - 0.757 34 | - 1.131 04 |
| 9 | + 0.234 65 | + 0.329 36 | - 0.564 01 | - 0.846 69 | 9 | + 0.223 12 | + 0.348 43 | - 0.571 56 | - 0.855 24 |
| 10 | + 0.207 40 | + 0.231 26 | - 0.438 66 | - 0.658 89 | 10 | + 0.199 44 | + 0.244 06 | - 0.443 51 | - 0.664 92 |
| 11 | + 0.190 28 | + 0.159 18 | - 0.349 46 | - 0.524 46 | 11 | + 0.184 74 | + 0.167 97 | - 0.352 70 | - 0.528 99 |
| 12 | + 0.178 51 | + 0.105 91 | - 0.284 42 | - 0.425 32 | 12 | + 0.174 64 | + 0.112 05 | - 0.286 67 | - 0.428 89 |
| 13 | + 0.169 76 | + 0.066 21 | - 0.235 97 | - 0.350 25 | 13 | + 0.167 08 | + 0.070 53 | - 0.237 61 | - 0.353 18 |
| 14 | + 0.162 85 | + 0.036 33 | - 0.199 20 | - 0.292 05 | 14 | + 0.161 05 | + 0.039 40 | - 0.200 43 | - 0.294 52 |
| 15 | + 0.157 17 | + 0.013 65 | - 0.170 81 | - 0.245 98 | 15 | + 0.155 99 | + 0.015 80 | - 0.171 81 | - 0.248 10 |
| 16 | + 0.152 34 | - 0.003 74 | - 0.148 61 | - 0.208 80 | 16 | + 0.151 67 | - 0.002 23 | - 0.149 43 | - 0.210 65 |
| 17 | + 0.148 19 | - 0.017 17 | - 0.131 02 | - 0.178 30 | 17 | + 0.147 90 | - 0.016 16 | - 0.131 73 | - 0.179 93 |
| 18 | + 0.144 58 | - 0.027 63 | - 0.116 96 | - 0.152 86 | 18 | + 0.144 58 | - 0.027 01 | - 0.117 60 | - 0.154 30 |
| 19 | + 0.141 43 | - 0.035 83 | - 0.105 61 | - 0.131 33 | 19 | + 0.141 69 | - 0.035 49 | - 0.106 22 | - 0.132 62 |
| 20 | + 0.138 71 | - 0.042 29 | - 0.096 41 | - 0.112 85 | 20 | + 0.139 16 | - 0.042 17 | - 0.097 01 | - 0.114 00 |
| 21 | + 0.136 36 | - 0.047 43 | - 0.088 94 | - 0.096 78 | 21 | + 0.136 98 | - 0.047 47 | - 0.089 52 | - 0.097 79 |
| 22 | + 0.134 36 | - 0.051 51 | - 0.082 85 | - 0.082 60 | 22 | + 0.135 12 | - 0.051 70 | - 0.083 43 | - 0.083 50 |
| 23 | + 0.132 68 | - 0.054 78 | - 0.077 92 | - 0.069 93 | 23 | + 0.133 57 | - 0.055 08 | - 0.078 59 | - 0.070 72 |
| 24 | + 0.131 33 | - 0.057 38 | - 0.073 94 | - 0.058 46 | 24 | + 0.132 33 | - 0.057 79 | - 0.074 54 | - 0.059 14 |
| 25 | + 0.130 27 | - 0.059 48 | - 0.070 80 | - 0.047 91 | 25 | + 0.131 37 | - 0.059 96 | - 0.071 41 | - 0.048 50 |
| 26 | + 0.129 51 | - 0.061 14 | - 0.068 37 | - 0.038 10 | 26 | + 0.130 70 | - 0.061 69 | - 0.069 01 | - 0.038 58 |
| 27 | + 0.129 04 | - 0.062 45 | - 0.066 59 | - 0.028 82 | 27 | + 0.130 31 | - 0.063 05 | - 0.067 25 | - 0.029 21 |
| 28 | + 0.128 85 | - 0.063 46 | - 0.065 39 | - 0.019 93 | 28 | + 0.130 20 | - 0.064 12 | - 0.066 08 | - 0.020 21 |
| 29 | + 0.128 94 | - 0.064 21 | - 0.064 75 | - 0.011 27 | 29 | + 0.130 37 | - 0.064 90 | - 0.065 46 | - 0.011 45 |
| 30 | + 0.129 33 | - 0.064 71 | - 0.064 63 | - 0.002 71 | 30 | + 0.130 83 | - 0.065 44 | - 0.065 38 | - 0.002 79 |
| 31 | + 0.130 02 | - 0.064 98 | - 0.065 04 | + 0.005 89 | 31 | + 0.131 59 | - 0.065 74 | - 0.065 83 | + 0.005 91 |
| 32 | + 0.131 01 | - 0.065 02 | - 0.065 99 | + 0.014 65 | 32 | + 0.132 63 | - 0.065 82 | - 0.066 83 | + 0.014 78 |
| 33 | + 0.132 32 | - 0.064 82 | - 0.067 51 | + 0.023 72 | 33 | + 0.134 01 | - 0.065 63 | - 0.068 39 | + 0.023 97 |
| 34 | + 0.133 97 | - 0.064 32 | - 0.069 63 | + 0.033 25 | 34 | + 0.135 71 | - 0.065 15 | - 0.070 57 | + 0.033 62 |
| 35 | + 0.135 96 | - 0.063 52 | - 0.072 44 | + 0.043 41 | 35 | + 0.137 77 | - 0.064 35 | - 0.073 43 | + 0.043 92 |
| 36 | + 0.138 34 | - 0.062 33 | - 0.076 02 | + 0.054 41 | 36 | + 0.140 22 | - 0.063 15 | - 0.077 06 | + 0.055 06 |
| 37 | + 0.141 13 | - 0.060 66 | - 0.080 48 | + 0.066 47 | 37 | + 0.143 08 | - 0.061 47 | - 0.081 59 | + 0.067 28 |
| 38 | + 0.144 40 | - 0.058 40 | - 0.085 99 | + 0.079 89 | 38 | + 0.146 40 | - 0.059 20 | - 0.087 18 | + 0.080 87 |
| 39 | + 0.148 16 | - 0.055 41 | - 0.092 77 | + 0.095 01 | 39 | + 0.150 22 | - 0.056 18 | - 0.094 05 | + 0.096 19 |
| 40 | + 0.152 52 | - 0.051 45 | - 0.101 08 | + 0.112 29 | 40 | + 0.154 64 | - 0.052 18 | - 0.102 46 | + 0.113 69 |
| 41 | + 0.157 56 | - 0.046 26 | - 0.111 29 | + 0.132 31 | 41 | + 0.159 73 | - 0.046 94 | - 0.112 79 | + 0.133 96 |
| 42 | + 0.163 40 | - 0.039 47 | - 0.123 92 | + 0.155 82 | 42 | + 0.165 61 | - 0.040 07 | - 0.125 54 | + 0.157 76 |
| 43 | + 0.170 20 | - 0.030 58 | - 0.139 61 | + 0.183 84 | 43 | + 0.172 45 | - 0.031 06 | - 0.141 39 | + 0.186 11 |
| 44 | + 0.178 22 | - 0.018 89 | - 0.159 31 | + 0.217 72 | 44 | + 0.180 48 | - 0.019 21 | - 0.161 26 | + 0.220 39 |
| 45 | + 0.187 79 | - 0.003 48 | - 0.184 30 | + 0.259 39 | 45 | + 0.190 04 | - 0.003 58 | - 0.186 46 | + 0.262 54 |
| 46 | + 0.199 46 | + 0.016 95 | - 0.216 40 | + 0.311 52 | 46 | + 0.201 66 | + 0.017 16 | - 0.218 84 | + 0.315 27 |
| 47 | + 0.214 10 | + 0.044 19 | - 0.258 28 | + 0.378 02 | 47 | + 0.216 18 | + 0.044 88 | - 0.261 04 | + 0.382 55 |
| 48 | + 0.233 13 | + 0.080 75 | - 0.313 87 | + 0.464 69 | 48 | + 0.234 99 | + 0.082 10 | - 0.317 09 | + 0.470 25 |
| 49 | + 0.259 12 | + 0.130 04 | - 0.389 15 | + 0.580 41 | 49 | + 0.260 56 | + 0.132 43 | - 0.392 99 | + 0.587 39 |
| 50 | + 0.296 74 | + 0.196 72 | - 0.493 44 | + 0.739 12 | 50 | + 0.297 46 | + 0.200 73 | - 0.498 20 | + 0.748 16 |
| 51 | + 0.355 09 | + 0.286 62 | - 0.641 69 | + 0.963 40 | 51 | + 0.354 63 | + 0.293 26 | - 0.647 89 | + 0.975 66 |
| 52 | + 0.452 86 | + 0.405 76 | - 0.858 63 | + 1.200 97 | 52 | + 0.450 50 | + 0.416 79 | - 0.867 29 | + 1.308 62 |
| 53 | + 0.630 50 | + 0.555 78 | - 1.186 20 | + 1.786 19 | 53 | + 0.625 31 | + 0.574 26 | - 1.199 57 | + 1.813 71 |
| 54 | + 0.980 18 | + 0.717 66 | - 1.697 83 | + 2.559 44 | 54 | + 0.971 84 | + 0.748 81 | - 1.720 64 | + 2.666 76 |
| 55 | + 1.720 92 | + 0.800 56 | - 2.521 46 | + 3.791 24 | 55 | + 1.713 05 | + 0.851 55 | - 2.565 51 | + 3.881 50 |
| 56 | + 3.376 87 | + 0.495 10 | - 3.871 98 | + 5.716 19 | 56 | + 3.399 86 | + 0.566 78 | - 3.666 64 | + 5.903 18 |
| 57 | + 7.094 11 | - 1.048 90 | - 6.045 21 | + 8.332 90 | 57 | + 7.271 80 | - 1.008 83 | - 6.262 95 | + 8.721 65 |
| 58 | +14.504 38 | - 5.336 43 | - 9.167 95 | +10.174 19 | 58 | +15.228 32 | - 5.570 39 | - 9.657 91 | +10.830 84 |
| 59 | +24.307 55 | -11.957 39 | -12.350 17 | + 6.726 53 | 59 | +26.106 78 | -12.841 66 | -13.265 09 | + 7.187 45 |

TABLE VII.—*Concluded.*

VALUES OF A, B, C, AND D FOR THE ACTION OF VENUS ON THE MOON.

| System 10. | | | | | System 11. | | | | |
|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +32.969 68 | -16.569 97 | -16.399 71 | - 3.668 44 | 0 | +35.831 31 | -17.896 16 | -17.935 12 | - 1.712 41 |
| 1 | +22.878 40 | - 9.208 85 | -13.579 54 | -12.862 57 | 1 | +25.980 88 | -10.969 56 | -15.011 32 | -12.871 70 |
| 2 | +11.019 61 | - 1.808 25 | - 9.121 36 | -12.148 82 | 2 | +12.649 60 | - 2.655 75 | - 9.993 85 | -12.897 08 |
| 3 | + 4.649 91 | - 1.018 42 | - 5.668 34 | - 8.326 79 | 3 | + 5.312 22 | - 0.803 15 | - 6.115 36 | - 8.902 19 |
| 4 | + 2.004 91 | + 1.525 68 | - 3.530 58 | - 5.294 55 | 4 | + 2.274 38 | + 1.480 38 | - 3.754 76 | - 5.628 18 |
| 5 | + 0.061 50 | + 1.313 85 | - 2.275 35 | - 3.408 98 | 5 | + 1.084 48 | + 1.308 02 | - 2.392 50 | - 3.595 21 |
| 6 | + 0.537 67 | + 0.991 88 | - 1.529 55 | - 2.283 06 | 6 | + 0.602 79 | + 0.991 77 | - 1.594 55 | - 2.390 23 |
| 7 | + 0.354 96 | + 0.716 40 | - 1.071 36 | - 1.596 99 | 7 | + 0.394 57 | + 0.715 16 | - 1.109 73 | - 1.661 64 |
| 8 | + 0.270 14 | + 0.508 75 | - 0.778 90 | - 1.162 57 | 8 | + 0.297 06 | + 0.505 83 | - 0.802 90 | - 1.203 41 |
| 9 | + 0.227 24 | + 0.357 97 | - 0.585 20 | - 0.875 82 | 9 | + 0.247 04 | + 0.353 97 | - 0.601 02 | - 0.902 67 |
| 10 | + 0.203 27 | + 0.249 27 | - 0.452 55 | - 0.678 94 | 10 | + 0.218 68 | + 0.244 78 | - 0.463 47 | - 0.697 18 |
| 11 | + 0.188 39 | + 0.170 58 | - 0.358 96 | - 0.538 89 | 11 | + 0.200 85 | + 0.165 98 | - 0.366 83 | - 0.551 59 |
| 12 | + 0.178 13 | + 0.113 07 | - 0.291 19 | - 0.436 09 | 12 | + 0.188 48 | + 0.108 59 | - 0.297 07 | - 0.445 09 |
| 13 | + 0.170 40 | + 0.070 59 | - 0.241 00 | - 0.358 52 | 13 | + 0.179 19 | + 0.066 36 | - 0.245 53 | - 0.364 97 |
| 14 | + 0.164 20 | + 0.038 87 | - 0.203 07 | - 0.298 55 | 14 | + 0.171 75 | + 0.034 92 | - 0.206 68 | - 0.303 18 |
| 15 | + 0.159 00 | + 0.014 93 | - 0.173 92 | - 0.251 17 | 15 | + 0.165 57 | + 0.011 29 | - 0.176 86 | - 0.254 49 |
| 16 | + 0.154 52 | - 0.003 31 | - 0.151 19 | - 0.213 01 | 16 | + 0.160 28 | - 0.006 65 | - 0.153 64 | - 0.215 35 |
| 17 | + 0.150 59 | - 0.017 36 | - 0.133 25 | - 0.181 73 | 17 | + 0.155 70 | - 0.020 38 | - 0.135 31 | - 0.183 33 |
| 18 | + 0.147 15 | - 0.028 23 | - 0.118 92 | - 0.155 68 | 18 | + 0.151 69 | - 0.030 98 | - 0.120 70 | - 0.156 70 |
| 19 | + 0.144 13 | - 0.036 72 | - 0.107 39 | - 0.133 65 | 19 | + 0.148 17 | - 0.039 22 | - 0.108 96 | - 0.134 21 |
| 20 | + 0.141 48 | - 0.043 40 | - 0.098 08 | - 0.114 75 | 20 | + 0.145 09 | - 0.045 66 | - 0.099 45 | - 0.114 95 |
| 21 | + 0.139 19 | - 0.048 67 | - 0.090 50 | - 0.098 31 | 21 | + 0.142 43 | - 0.050 70 | - 0.091 72 | - 0.098 23 |
| 22 | + 0.137 22 | - 0.052 86 | - 0.084 36 | - 0.083 81 | 22 | + 0.140 12 | - 0.054 68 | - 0.085 45 | - 0.083 50 |
| 23 | + 0.135 57 | - 0.056 20 | - 0.079 38 | - 0.070 86 | 23 | + 0.138 16 | - 0.057 81 | - 0.080 36 | - 0.070 35 |
| 24 | + 0.134 22 | - 0.058 85 | - 0.075 38 | - 0.059 13 | 24 | + 0.136 53 | - 0.060 27 | - 0.076 26 | - 0.058 46 |
| 25 | + 0.133 17 | - 0.060 96 | - 0.072 22 | - 0.048 36 | 25 | + 0.135 22 | - 0.052 20 | - 0.073 01 | - 0.047 55 |
| 26 | + 0.132 41 | - 0.062 63 | - 0.069 79 | - 0.038 32 | 26 | + 0.134 20 | - 0.053 70 | - 0.070 50 | - 0.037 41 |
| 27 | + 0.131 93 | - 0.063 93 | - 0.068 01 | - 0.028 84 | 27 | + 0.133 48 | - 0.064 83 | - 0.068 64 | - 0.027 83 |
| 28 | + 0.131 73 | - 0.064 92 | - 0.066 81 | - 0.019 75 | 28 | + 0.133 05 | - 0.065 65 | - 0.067 38 | - 0.018 66 |
| 29 | + 0.131 82 | - 0.065 63 | - 0.066 18 | - 0.010 90 | 29 | + 0.132 89 | - 0.066 20 | - 0.066 68 | - 0.009 75 |
| 30 | + 0.132 18 | - 0.066 10 | - 0.066 08 | - 0.002 15 | 30 | + 0.133 02 | - 0.066 51 | - 0.066 51 | - 0.000 96 |
| 31 | + 0.132 84 | - 0.066 32 | - 0.066 51 | + 0.006 62 | 31 | + 0.133 44 | - 0.066 56 | - 0.066 87 | + 0.007 85 |
| 32 | + 0.133 79 | - 0.066 31 | - 0.067 49 | + 0.015 57 | 32 | + 0.134 15 | - 0.066 37 | - 0.067 77 | + 0.016 82 |
| 33 | + 0.135 06 | - 0.066 03 | - 0.069 03 | + 0.024 82 | 33 | + 0.135 15 | - 0.065 91 | - 0.069 23 | + 0.026 08 |
| 34 | + 0.136 64 | - 0.065 45 | - 0.071 18 | + 0.034 54 | 34 | + 0.136 40 | - 0.065 16 | - 0.071 30 | + 0.035 78 |
| 35 | + 0.138 57 | - 0.064 54 | - 0.074 02 | + 0.044 89 | 35 | + 0.138 10 | - 0.064 05 | - 0.074 04 | + 0.046 11 |
| 36 | + 0.140 86 | - 0.063 24 | - 0.077 63 | + 0.056 08 | 36 | + 0.140 07 | - 0.062 54 | - 0.077 55 | + 0.057 24 |
| 37 | + 0.143 55 | - 0.061 43 | - 0.082 13 | + 0.068 34 | 37 | + 0.142 42 | - 0.060 50 | - 0.081 92 | + 0.069 42 |
| 38 | + 0.146 68 | - 0.059 01 | - 0.087 67 | + 0.081 96 | 38 | + 0.145 15 | - 0.057 84 | - 0.087 32 | + 0.082 93 |
| 39 | + 0.150 29 | - 0.055 81 | - 0.094 47 | + 0.097 30 | 39 | + 0.148 32 | - 0.054 37 | - 0.093 95 | + 0.098 11 |
| 40 | + 0.154 44 | - 0.051 63 | - 0.102 80 | + 0.114 80 | 40 | + 0.151 96 | - 0.049 87 | - 0.102 09 | + 0.115 40 |
| 41 | + 0.159 20 | - 0.046 17 | - 0.113 05 | + 0.135 04 | 41 | + 0.156 14 | - 0.044 06 | - 0.112 08 | + 0.135 36 |
| 42 | + 0.164 70 | - 0.039 03 | - 0.125 68 | + 0.158 78 | 42 | + 0.160 93 | - 0.039 52 | - 0.124 42 | + 0.158 73 |
| 43 | + 0.171 06 | - 0.029 69 | - 0.141 37 | + 0.187 03 | 43 | + 0.166 46 | - 0.026 71 | - 0.139 73 | + 0.186 47 |
| 44 | + 0.178 50 | - 0.017 45 | - 0.161 05 | + 0.221 16 | 44 | + 0.172 85 | - 0.013 91 | - 0.158 94 | + 0.219 93 |
| 45 | + 0.187 29 | - 0.001 31 | - 0.185 99 | + 0.263 06 | 45 | + 0.180 36 | + 0.002 93 | - 0.183 28 | + 0.260 93 |
| 46 | + 0.197 90 | + 0.020 12 | - 0.218 01 | + 0.315 43 | 46 | + 0.189 32 | + 0.025 21 | - 0.214 53 | + 0.312 08 |
| 47 | + 0.211 05 | + 0.048 73 | - 0.259 78 | + 0.382 19 | 47 | + 0.200 31 | + 0.054 97 | - 0.255 27 | + 0.377 15 |
| 48 | + 0.227 98 | + 0.087 26 | - 0.315 23 | + 0.469 15 | 48 | + 0.214 31 | + 0.095 04 | - 0.309 35 | + 0.461 76 |
| 49 | + 0.250 86 | + 0.139 52 | - 0.390 37 | + 0.585 26 | 49 | + 0.233 09 | + 0.149 53 | - 0.382 62 | + 0.574 53 |
| 50 | + 0.283 78 | + 0.210 84 | - 0.494 61 | + 0.744 61 | 50 | + 0.260 04 | + 0.224 24 | - 0.484 27 | + 0.729 10 |
| 51 | + 0.334 81 | + 0.308 36 | - 0.643 17 | + 0.970 29 | 51 | + 0.301 96 | + 0.327 27 | - 0.629 23 | + 0.947 79 |
| 52 | + 0.420 84 | + 0.440 62 | - 0.861 46 | + 1.301 21 | 52 | + 0.373 30 | + 0.469 14 | - 0.842 44 | + 1.268 49 |
| 53 | + 0.579 24 | + 0.614 18 | - 1.193 43 | + 1.805 20 | 53 | + 0.506 61 | + 0.660 75 | - 1.167 37 | + 1.757 69 |
| 54 | + 0.897 75 | + 0.819 82 | - 1.717 55 | + 2.602 39 | 54 | + 0.779 60 | + 0.902 68 | - 1.682 27 | + 2.535 09 |
| 55 | + 1.592 91 | + 0.983 93 | - 2.576 84 | + 3.901 43 | 55 | + 1.388 11 | + 1.144 02 | - 2.532 13 | + 3.815 21 |
| 56 | + 3.213 60 | + 0.814 77 | - 4.028 36 | + 6.015 62 | 56 | + 2.843 29 | + 1.141 94 | - 3.985 24 | + 5.946 55 |
| 57 | + 7.077 92 | - 0.596 54 | - 6.481 38 | + 9.125 85 | 57 | + 6.437 87 | + 0.057 82 | - 6.495 70 | + 9.252 71 |
| 58 | +15.483 72 | - 5.189 93 | -10.293 80 | +11.995 97 | 58 | +14.717 82 | - 4.162 63 | -10.555 20 | +12.780 88 |
| 59 | +28.021 10 | -13.352 48 | -14.668 60 | + 8.801 20 | 59 | +28.397 74 | -12.848 84 | -15.548 89 | +10.996 73 |

TABLE VIII.

DEVELOPMENT OF A, B, C, AND D FOR VENUS IN PERIODIC SERIES.

| Coeff. of V, g' | A | | B | | C | | D | |
|----------------------|---------|---------|---------|---------|---------|---------|---------|---------|
| | cos | sin | cos | sin | cos | sin | cos | sin |
| 0 0 | +2.1947 | 0.0000 | -0.5886 | 0.0000 | -1.6061 | 0.0000 | -0.0005 | 0.0000 |
| 0+ 1 | +0.1742 | -0.0428 | -0.0314 | +0.0085 | -0.1428 | +0.0343 | +0.0080 | +0.0774 |
| 0+ 2 | +0.0523 | -0.0556 | -0.0086 | +0.0084 | -0.0438 | +0.0471 | +0.0124 | +0.0131 |
| 0+ 3 | +0.0046 | -0.0075 | -0.0008 | +0.0012 | -0.0038 | +0.0063 | +0.0022 | +0.0016 |
| 0+ 4 | +0.0001 | -0.0015 | 0.0000 | 0.0000 | -0.0001 | +0.0012 | +0.0004 | 0.0000 |
| 0+ 5 | -0.0001 | -0.0002 | 0.0000 | +0.0002 | 0.0000 | +0.0002 | 0.0000 | 0.0000 |
| 0+ 6 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1- 7 | 0.0000 | 0.0000 | -0.0001 | +0.0001 | 0.0000 | 0.0000 | +0.0001 | 0.0000 |
| 1- 6 | -0.0004 | +0.0003 | -0.0003 | 0.0000 | +0.0001 | -0.0003 | 0.0000 | -0.0001 |
| 1- 5 | +0.0004 | +0.0014 | -0.0002 | -0.0005 | -0.0001 | -0.0010 | +0.0005 | -0.0005 |
| 1- 4 | +0.0049 | +0.0084 | -0.0013 | -0.0017 | -0.0038 | -0.0068 | +0.0031 | -0.0021 |
| 1- 3 | +0.0546 | +0.0552 | -0.0127 | -0.0115 | -0.0423 | -0.0441 | +0.0182 | -0.0199 |
| 1- 2 | +0.2534 | +0.0552 | -0.0820 | -0.0156 | -0.1708 | -0.0393 | +0.0201 | -0.1214 |
| 1- 1 | +4.0006 | -0.0006 | -1.1590 | +0.0004 | -2.8416 | 0.0000 | -0.0015 | -1.1602 |
| 1+ 0 | +0.0924 | -0.0288 | +0.0118 | +0.0030 | -0.1036 | +0.0255 | -0.0010 | +0.0525 |
| 1+ 1 | +0.0501 | -0.0549 | -0.0058 | +0.0060 | -0.0445 | +0.0490 | +0.0063 | +0.0068 |
| 1+ 2 | +0.0038 | -0.0064 | -0.0002 | +0.0008 | -0.0030 | +0.0059 | +0.0013 | +0.0009 |
| 1+ 3 | 0.0000 | -0.0014 | 0.0000 | +0.0005 | 0.0000 | +0.0013 | +0.0004 | +0.0001 |
| 1+ 4 | -0.0001 | -0.0002 | 0.0000 | 0.0000 | +0.0002 | +0.0004 | -0.0002 | 0.0000 |
| 1+ 5 | 0.0000 | 0.0000 | -0.0001 | +0.0001 | 0.0000 | 0.0000 | +0.0001 | 0.0000 |
| 2- 8 | 0.0000 | 0.0000 | -0.0001 | -0.0001 | +0.0001 | 0.0000 | +0.0001 | 0.0000 |
| 2- 7 | 0.0000 | +0.0004 | -0.0002 | -0.0001 | +0.0001 | -0.0006 | +0.0002 | 0.0000 |
| 2- 6 | +0.0004 | +0.0015 | 0.0000 | -0.0005 | -0.0002 | -0.0011 | +0.0002 | -0.0001 |
| 2- 5 | +0.0054 | +0.0092 | -0.0016 | -0.0025 | -0.0036 | -0.0065 | +0.0037 | -0.0027 |
| 2- 4 | +0.0567 | +0.0542 | -0.0174 | -0.0144 | -0.0398 | -0.0398 | +0.0223 | -0.0252 |
| 2- 3 | +0.3093 | +0.0648 | -0.1281 | -0.0245 | -0.1826 | -0.0402 | +0.0315 | -0.1729 |
| 2- 2 | +3.7105 | -0.0014 | -1.3562 | +0.0011 | -2.3535 | 0.0000 | -0.0018 | -1.6716 |
| 2- 1 | +0.0402 | -0.0173 | +0.0321 | +0.0010 | -0.0730 | +0.0162 | -0.0016 | +0.0516 |
| 2+ 0 | +0.0483 | -0.0536 | -0.0049 | +0.0052 | -0.0430 | +0.0486 | +0.0001 | +0.0012 |
| 2+ 1 | +0.0032 | -0.0054 | -0.0003 | +0.0003 | -0.0028 | +0.0048 | +0.0008 | +0.0007 |
| 2+ 2 | +0.0001 | -0.0010 | 0.0000 | +0.0002 | 0.0000 | +0.0011 | +0.0001 | 0.0000 |
| 2+ 3 | -0.0002 | -0.0002 | -0.0003 | -0.0001 | +0.0003 | -0.0002 | +0.0002 | 0.0000 |
| 2+ 4 | 0.0000 | 0.0000 | -0.0001 | -0.0001 | +0.0001 | 0.0000 | +0.0001 | 0.0000 |
| 3- 9 | -0.0001 | +0.0001 | -0.0001 | 0.0000 | +0.0001 | 0.0000 | +0.0001 | +0.0001 |
| 3- 8 | 0.0000 | +0.0006 | 0.0000 | -0.0003 | +0.0001 | -0.0003 | +0.0001 | 0.0000 |
| 3- 7 | +0.0004 | +0.0020 | +0.0001 | -0.0007 | -0.0003 | -0.0011 | +0.0007 | -0.0002 |
| 3- 6 | +0.0062 | +0.0093 | -0.0020 | -0.0032 | -0.0041 | -0.0064 | +0.0046 | -0.0033 |
| 3- 5 | +0.0586 | +0.0524 | -0.0217 | -0.0168 | -0.0366 | -0.0354 | +0.0252 | -0.0305 |
| 3- 4 | +0.3454 | +0.0705 | -0.1657 | -0.0317 | -0.1789 | -0.0387 | +0.0408 | -0.2154 |
| 3- 3 | +3.3553 | -0.0017 | -1.4697 | +0.0012 | -1.8858 | +0.0003 | -0.0014 | -1.8630 |
| 3- 2 | +0.0042 | -0.0079 | +0.0456 | -0.0014 | -0.0490 | +0.0094 | +0.0008 | +0.0547 |
| 3- 1 | +0.0454 | -0.0516 | -0.0044 | +0.0049 | -0.0410 | +0.0463 | -0.0056 | -0.0043 |
| 3- 0 | +0.0030 | -0.0045 | -0.0002 | 0.0000 | -0.0030 | +0.0044 | 0.0000 | +0.0003 |
| 3- 1 | -0.0003 | -0.0010 | +0.0004 | +0.0002 | +0.0001 | +0.0011 | +0.0002 | 0.0000 |
| 3- 2 | -0.0004 | 0.0000 | -0.0002 | -0.0001 | +0.0002 | -0.0002 | 0.0000 | +0.0001 |
| 3- 3 | -0.0001 | +0.0001 | -0.0001 | 0.0000 | +0.0001 | 0.0000 | +0.0001 | +0.0001 |
| 4- 10 | -0.0001 | +0.0002 | +0.0001 | +0.0001 | +0.0002 | 0.0000 | +0.0001 | 0.0000 |
| 4- 9 | -0.0001 | +0.0004 | +0.0003 | +0.0001 | 0.0000 | -0.0002 | 0.0000 | -0.0002 |
| 4- 8 | +0.0003 | +0.0018 | 0.0000 | -0.0008 | -0.0001 | -0.0014 | +0.0013 | -0.0003 |
| 4- 7 | +0.0064 | +0.0096 | -0.0025 | -0.0036 | -0.0038 | -0.0060 | +0.0052 | -0.0036 |
| 4- 6 | +0.0584 | +0.0498 | -0.0252 | -0.0190 | -0.0332 | -0.0308 | +0.0267 | -0.0344 |
| 4- 5 | +0.3605 | +0.0726 | -0.1938 | -0.0370 | -0.1671 | -0.0355 | +0.0468 | -0.2442 |
| 4- 4 | +2.9597 | -0.0013 | -1.4783 | +0.0012 | -1.4817 | +0.0002 | -0.0014 | -1.8566 |
| 4- 3 | -0.0206 | -0.0005 | +0.0526 | -0.0043 | -0.0330 | +0.0045 | +0.0037 | +0.0580 |
| 4- 2 | +0.0424 | -0.0483 | -0.0058 | +0.0059 | -0.0369 | +0.0420 | -0.0090 | -0.0075 |
| 4- 1 | +0.0023 | -0.0034 | 0.0000 | -0.0001 | -0.0025 | +0.0034 | 0.0000 | +0.0003 |

TABLE VIII.—*Concluded.*

DEVELOPMENT OF A, B, C, AND D FOR VENUS IN PERIODIC SERIES.

| Coeff. of v, g' | A | | B | | C | | D | |
|----------------------|---------|---------|---------|---------|---------|---------|---------|---------|
| | cos | sin | cos | sin | cos | sin | cos | sin |
| 4+ 0 | -0.0002 | -0.0010 | +0.0001 | +0.0001 | +0.0002 | +0.0013 | -0.0002 | -0.0003 |
| 4+ 1 | 0.0000 | +0.0002 | -0.0001 | -0.0001 | 0.0000 | +0.0003 | -0.0001 | 0.0000 |
| 4+ 2 | +0.0001 | +0.0002 | -0.0001 | +0.0001 | +0.0004 | 0.0000 | +0.0001 | 0.0000 |
| 5-11 | 0.0000 | 0.0000 | -0.0001 | 0.0000 | +0.0001 | -0.0001 | 0.0000 | -0.0001 |
| 5-10 | -0.0004 | 0.0000 | -0.0001 | -0.0004 | +0.0002 | +0.0001 | +0.0002 | 0.0000 |
| 5- 9 | +0.0004 | +0.0018 | -0.0001 | -0.0008 | 0.0000 | -0.0011 | +0.0011 | -0.0003 |
| 5- 8 | +0.0063 | +0.0095 | -0.0028 | -0.0036 | -0.0037 | -0.0056 | +0.0057 | -0.0040 |
| 5- 7 | +0.0579 | +0.0465 | -0.0284 | -0.0200 | -0.0298 | -0.0268 | +0.0276 | -0.0374 |
| 5- 6 | +0.3602 | +0.0712 | -0.2094 | -0.0400 | -0.1501 | -0.0313 | +0.0497 | -0.2587 |
| 5- 5 | +2.5539 | -0.0014 | -1.4070 | +0.0012 | -1.1467 | +0.0002 | -0.0015 | -1.7422 |
| 5- 4 | -0.0350 | +0.0047 | +0.0564 | -0.0068 | -0.0205 | +0.0016 | +0.0067 | +0.0598 |
| 5- 3 | +0.0389 | -0.0445 | -0.0064 | +0.0069 | -0.0328 | +0.0375 | -0.0122 | -0.0108 |
| 5- 2 | +0.0018 | -0.0028 | +0.0001 | +0.0001 | -0.0018 | +0.0029 | +0.0002 | +0.0002 |
| 5- 1 | +0.0004 | -0.0011 | 0.0000 | +0.0002 | +0.0002 | +0.0012 | -0.0002 | 0.0000 |
| 5+ 0 | -0.0001 | +0.0002 | -0.0002 | +0.0002 | -0.0001 | +0.0001 | +0.0002 | 0.0000 |
| 5+ 1 | 0.0000 | 0.0000 | -0.0001 | 0.0000 | +0.0001 | -0.0001 | 0.0000 | -0.0001 |
| 6-12 | -0.0001 | 0.0000 | 0.0000 | 0.0000 | +0.0002 | 0.0000 | +0.0001 | -0.0002 |
| 6-11 | -0.0001 | +0.0003 | +0.0002 | 0.0000 | +0.0004 | +0.0001 | +0.0002 | 0.0000 |
| 6-10 | +0.0003 | +0.0018 | -0.0002 | -0.0008 | -0.0005 | -0.0009 | +0.0012 | -0.0005 |
| 6- 9 | +0.0061 | +0.0091 | -0.0035 | -0.0038 | -0.0033 | -0.0050 | +0.0060 | -0.0040 |
| 6- 8 | +0.0557 | +0.0428 | -0.0295 | -0.0203 | -0.0264 | -0.0225 | +0.0274 | -0.0380 |
| 6- 7 | +0.3455 | +0.0684 | -0.2150 | -0.0414 | -0.1312 | -0.0274 | +0.0500 | -0.2590 |
| 6- 6 | +2.1645 | -0.0007 | -1.2859 | +0.0009 | -0.8788 | -0.0001 | -0.0009 | -1.5648 |
| 6- 5 | -0.0436 | +0.0086 | +0.0558 | -0.0084 | -0.0128 | +0.0002 | +0.0086 | +0.0588 |
| 6- 4 | +0.0356 | -0.0403 | -0.0075 | +0.0078 | -0.0282 | +0.0321 | -0.0139 | -0.0120 |
| 6- 3 | +0.0016 | -0.0022 | 0.0000 | -0.0001 | -0.0018 | +0.0021 | +0.0002 | -0.0001 |
| 6- 2 | 0.0000 | -0.0009 | +0.0002 | +0.0002 | -0.0005 | +0.0009 | 0.0000 | +0.0005 |
| 6- 1 | -0.0001 | +0.0002 | -0.0002 | +0.0001 | -0.0001 | +0.0001 | -0.0002 | -0.0006 |
| 6+ 0 | -0.0001 | 0.0000 | 0.0000 | 0.0000 | -0.0002 | 0.0000 | -0.0001 | -0.0002 |
| 7-13 | -0.0001 | 0.0000 | 0.0000 | -0.0001 | -0.0001 | 0.0000 | -0.0002 | 0.0000 |
| 7-12 | 0.0000 | +0.0005 | +0.0003 | -0.0001 | -0.0001 | -0.0001 | +0.0004 | +0.0002 |
| 7-11 | +0.0006 | +0.0017 | +0.0001 | -0.0009 | -0.0002 | -0.0009 | +0.0007 | -0.0001 |
| 7-10 | +0.0064 | +0.0088 | -0.0033 | -0.0042 | -0.0030 | -0.0046 | +0.0058 | -0.0043 |
| 7- 9 | +0.0532 | +0.0392 | -0.0305 | -0.0200 | -0.0223 | -0.0184 | +0.0260 | -0.0386 |
| 7- 8 | +0.3227 | +0.0632 | -0.2112 | -0.0407 | -0.1116 | -0.0226 | +0.0486 | -0.2508 |
| 7- 7 | +1.8074 | -0.0006 | -1.1384 | +0.0008 | -0.6689 | -0.0002 | -0.0009 | -1.3643 |
| 7- 6 | -0.0458 | +0.0106 | -0.0547 | -0.0102 | -0.0074 | -0.0009 | +0.0105 | +0.0567 |
| 7- 5 | +0.0315 | -0.0359 | -0.0074 | +0.0082 | -0.0240 | +0.0274 | -0.0148 | -0.0129 |
| 7- 4 | +0.0012 | -0.0015 | +0.0001 | -0.0004 | -0.0012 | +0.0016 | +0.0002 | +0.0002 |
| 7- 3 | 0.0000 | -0.0011 | +0.0003 | +0.0003 | 0.0000 | +0.0008 | -0.0005 | +0.0002 |
| 7- 2 | -0.0001 | -0.0002 | -0.0001 | +0.0002 | 0.0000 | +0.0001 | -0.0001 | 0.0000 |
| 7- 1 | -0.0001 | 0.0000 | 0.0000 | -0.0002 | -0.0001 | 0.0000 | -0.0002 | 0.0000 |
| 8-14 | -0.0001 | 0.0000 | 0.0000 | -0.0001 | 0.0000 | -0.0002 | +0.0001 | 0.0000 |
| 8-13 | -0.0002 | +0.0002 | +0.0002 | -0.0002 | 0.0000 | -0.0001 | +0.0002 | -0.0003 |
| 8-12 | +0.0002 | +0.0014 | -0.0002 | -0.0008 | -0.0002 | -0.0010 | +0.0013 | -0.0006 |
| 8-11 | +0.0058 | +0.0080 | -0.0034 | -0.0044 | -0.0027 | -0.0037 | +0.0050 | -0.0341 |
| 8-10 | +0.0496 | +0.0351 | -0.0306 | -0.0190 | -0.0193 | -0.0155 | +0.0250 | -0.0374 |
| 8- 9 | +0.2941 | +0.0577 | -0.1996 | -0.0385 | -0.0942 | -0.0192 | +0.0459 | -0.2335 |
| 8- 8 | +1.4892 | -0.0001 | -0.9842 | +0.0003 | -0.5050 | -0.0001 | -0.0006 | -1.1634 |
| 8- 7 | -0.0461 | +0.0118 | +0.0500 | -0.0104 | -0.0048 | -0.0012 | +0.0115 | +0.0508 |
| 8- 6 | +0.0278 | -0.0316 | -0.0081 | +0.0085 | -0.0198 | +0.0228 | -0.0144 | -0.0122 |
| 8- 5 | +0.0010 | -0.0010 | +0.0001 | -0.0004 | -0.0012 | +0.0012 | -0.0005 | 0.0000 |
| 8- 4 | -0.0001 | -0.0009 | 0.0000 | -0.0001 | -0.0002 | +0.0009 | +0.0001 | +0.0002 |
| 8- 3 | +0.0002 | 0.0000 | 0.0000 | -0.0002 | -0.0001 | +0.0002 | -0.0001 | +0.0005 |
| 8- 2 | -0.0001 | 0.0000 | 0.0000 | -0.0001 | 0.0000 | -0.0002 | +0.0001 | 0.0000 |

TABLE IX.

COMPUTATION OF THE COEFFICIENTS FOR THE HANSENIAN VENUS-TERM OF LONG PERIOD.

| System. | A_0'' | $A_{e,1}$ | $A_{e,2}$ | $A_{s,1}$ | $A_{s,2}$ |
|---------|----------|-----------|-----------|-----------|-----------|
| 0 | +33.3948 | -48.0672 | -15.2486 | + 1.6810 | + 1.6959 |
| 1 | +30.4226 | -44.3154 | -14.3087 | + 5.2845 | + 5.6929 |
| 2 | +27.3802 | -40.4460 | -13.3384 | + 6.9388 | + 7.7952 |
| 3 | +25.7695 | -38.3437 | -12.7915 | + 6.7824 | + 7.8308 |
| 4 | +25.3715 | -37.7570 | -12.6090 | + 5.0267 | + 5.8930 |
| 5 | +25.2326 | -37.5000 | -12.5055 | + 1.9933 | + 2.3924 |
| 6 | +24.7525 | -36.8595 | -12.3300 | - 1.4599 | - 1.6609 |
| 7 | +24.2976 | -36.3246 | -12.2190 | - 4.3516 | - 5.1130 |
| 8 | +24.8273 | -37.1237 | -12.4835 | - 6.2219 | - 7.2996 |
| 9 | +27.0732 | -40.1587 | -13.3322 | - 6.9149 | - 7.9252 |
| 10 | +30.7124 | -44.8051 | -14.5505 | - 5.9534 | - 6.5819 |
| 11 | +33.6483 | -48.4814 | -15.4035 | - 2.7899 | - 3.0391 |
| | B_0'' | $B_{e,1}$ | $B_{e,2}$ | $B_{s,1}$ | $B_{s,2}$ |
| 0 | -19.9136 | +27.3868 | + 7.9770 | - 1.3391 | - 1.2601 |
| 1 | -18.5130 | +25.9046 | + 7.7012 | - 4.0210 | - 4.0255 |
| 2 | -16.9031 | +24.1227 | + 7.4055 | - 5.0839 | - 5.2866 |
| 3 | -15.8666 | +22.8730 | + 7.2028 | - 4.7701 | - 5.0902 |
| 4 | -15.4249 | +22.2499 | + 7.0232 | - 3.4567 | - 3.7608 |
| 5 | -15.2448 | +21.9597 | + 6.9235 | - 1.4491 | - 1.6516 |
| 6 | -15.0836 | +21.7873 | + 6.9008 | + 0.8330 | + 0.8101 |
| 7 | -15.0404 | +21.8370 | + 6.9098 | + 2.9218 | + 3.1445 |
| 8 | -15.4663 | +22.4592 | + 7.1627 | + 4.4869 | + 4.9005 |
| 9 | -16.6559 | +23.9194 | + 7.4839 | + 5.2206 | + 5.6178 |
| 10 | -18.4509 | +25.9344 | + 7.8260 | + 4.5771 | + 4.7687 |
| 11 | -19.9292 | +27.4474 | + 8.0139 | + 2.1201 | + 2.1782 |
| | C_0'' | $C_{e,1}$ | $C_{e,2}$ | $C_{s,1}$ | $C_{s,2}$ |
| 0 | -13.4811 | +20.6804 | + 7.2716 | - 0.3420 | - 0.4358 |
| 1 | -11.9096 | +18.4107 | + 6.5475 | - 1.2636 | - 1.6673 |
| 2 | -10.4771 | +16.3233 | + 5.8729 | - 1.8550 | - 2.0586 |
| 3 | - 9.9030 | +15.4707 | + 5.5887 | - 2.0122 | - 2.7407 |
| 4 | - 9.9466 | +15.5072 | + 5.5856 | - 1.5700 | - 2.1323 |
| 5 | - 9.9878 | +15.5402 | + 5.5820 | - 0.5442 | - 0.7409 |
| 6 | - 9.6689 | +15.0722 | + 5.4291 | + 0.6270 | + 0.8508 |
| 7 | - 9.2573 | +14.4877 | + 5.2492 | + 1.4299 | + 1.9685 |
| 8 | - 9.3611 | +14.6645 | + 5.3207 | + 1.7351 | + 2.3991 |
| 9 | -10.4173 | +16.2394 | + 5.8483 | + 1.6943 | + 2.3074 |
| 10 | -12.2555 | +18.9306 | + 6.7244 | + 1.3762 | + 1.8132 |
| 11 | -13.7191 | +21.0340 | + 7.3897 | + 0.6699 | + 0.8668 |
| | D_0'' | $D_{e,1}$ | $D_{e,2}$ | $D_{s,1}$ | $D_{s,2}$ |
| 0 | + 1.1897 | - 1.3484 | - 0.2485 | -29.8546 | -38.9716 |
| 1 | + 3.5868 | - 4.2373 | - 0.8724 | -27.5111 | -36.6653 |
| 2 | + 4.5580 | - 5.5349 | - 1.2117 | -24.9093 | -34.0089 |
| 3 | + 4.3152 | - 5.3345 | - 1.2153 | -23.3292 | -32.2553 |
| 4 | + 3.1531 | - 3.9457 | - 0.9269 | -22.7393 | -31.4609 |
| 5 | + 1.3233 | - 1.7080 | - 0.4334 | -22.5117 | -31.0906 |
| 6 | - 0.7706 | + 0.8979 | + 0.1689 | -22.2069 | -30.7822 |
| 7 | - 2.6659 | + 3.3202 | + 0.7653 | -22.0282 | -30.7403 |
| 8 | - 4.0554 | + 5.1025 | + 1.2108 | -22.6267 | -31.5788 |
| 9 | - 4.6896 | + 5.8349 | + 1.3576 | -24.5324 | -33.7503 |
| 10 | - 4.1057 | + 4.9831 | + 1.1038 | -27.4981 | -36.8202 |
| 11 | - 1.9060 | + 2.2816 | + 0.4940 | -29.9252 | -39.1222 |

TABLE X.

COEFFICIENTS OF $\cos 18L$ AND $\sin 18L$ FOR A, B, C, AND D IN EACH OF
12 SYSTEMS ($L = v - g'$).

| System. | $30A_c$ | $30A_s$ | $30B_c$ | $30B_s$ | $30C_c$ | $30C_s$ | $30D_c$ | $30D_s$ |
|-----------|---------|---------|---------|---------|---------|---------|---------|---------|
| 0 | +6.2049 | +0.6020 | -4.9971 | -0.5329 | -1.2077 | -0.0692 | +0.5720 | -5.4864 |
| 1 | +5.1524 | +1.6797 | -4.2291 | -1.4580 | -0.9233 | -0.2217 | +1.5716 | -4.6133 |
| 2 | +4.0908 | +2.0174 | -3.4091 | -1.7277 | -0.6816 | -0.2896 | +1.8673 | -3.7002 |
| 3 | +3.5721 | +1.8476 | -2.9712 | -1.5447 | -0.6009 | -0.3028 | +1.6835 | -3.2281 |
| 4 | +3.5031 | +1.3168 | -2.8674 | -1.0770 | -0.6358 | -0.2398 | +1.1840 | -3.1341 |
| 5 | +3.5273 | +0.4896 | -2.8577 | -0.4074 | -0.6697 | -0.0821 | +0.4448 | -3.1352 |
| 6 | +3.3871 | -0.4122 | -2.7680 | +0.3160 | -0.6191 | +0.0962 | -0.3565 | -3.0267 |
| 7 | +3.1874 | -1.1332 | -2.6537 | +0.9305 | -0.5337 | +0.2028 | -1.0208 | -2.8813 |
| 8 | +3.2562 | -1.6267 | -2.7313 | +1.3868 | -0.5250 | +0.2401 | -1.2091 | -2.9577 |
| 9 | +3.8775 | -1.9181 | -3.2097 | +1.6630 | -0.6677 | +0.2552 | -1.7883 | -3.4938 |
| 10 | +5.0768 | -1.7932 | -4.1114 | +1.5501 | -0.9055 | +0.2431 | -1.6730 | -4.5098 |
| 11 | +6.2050 | -0.8671 | -4.9641 | +0.7360 | -1.2409 | +0.1311 | -0.8012 | -5.4650 |
| a_0 | +4.2534 | +0.0169 | -3.4808 | -0.0138 | -0.7726 | -0.0031 | +0.0154 | -3.8026 |
| a_1 | +1.3404 | +0.4237 | -1.0631 | -0.3618 | -0.2773 | -0.0620 | +0.3915 | -1.1728 |
| β_1 | -0.2170 | +1.9499 | +0.1657 | -1.6577 | +0.0512 | -0.2923 | +1.7968 | +0.1855 |
| a_2 | +0.5358 | +0.0646 | -0.3961 | -0.0834 | -0.1397 | +0.0188 | +0.0796 | -0.4480 |
| β_2 | -0.3789 | +0.2585 | +0.2565 | -0.2410 | +0.1224 | -0.0174 | +0.2547 | +0.3019 |
| a_3 | +0.0682 | +0.0800 | -0.0512 | -0.0602 | -0.0170 | -0.0197 | +0.0698 | -0.0569 |
| β_3 | -0.0679 | +0.0673 | +0.0488 | -0.0540 | +0.0192 | -0.0133 | +0.0611 | +0.0554 |

The coefficients A_c , A_s , etc., have a separate value for each of the 12 systems. These special values are developed in a periodic series proceeding according to the sines and cosines of multiples of g' , in the form (a) §36 with results shown in the last seven lines above. The final development is then shown below in the form (b).

TABLE XI.

COMPUTATION OF A- AND K-COEFFICIENTS FOR THE HANSENIAN INEQUALITY OF
LONG PERIOD.

| Arg. | $30A_c$ | $30A_s$ | $30B_c$ | $30B_s$ | $30C_c$ | $30C_s$ | $30D_c$ | $30D_s$ |
|----------|---------|---------|------------|------------|------------|------------|------------|------------|
| 18v-18g' | +4.2534 | +0.0169 | -3.4808 | -0.0138 | -0.7726 | -0.0031 | +0.0154 | -3.8026 |
| 18v-17g' | -0.3048 | +0.1034 | +0.2973 | -0.0981 | +0.0075 | -0.0054 | +0.1030 | +0.3120 |
| 18v-16g' | +0.1387 | -0.1572 | -0.0775 | +0.0865 | -0.0611 | +0.0706 | -0.1111 | -0.0966 |
| 18v-15g' | +0.0005 | +0.0061 | +0.0014 | -0.0057 | -0.0019 | -0.0003 | +0.0072 | +0.0021 |
| Arg. | $30K_c$ | $30K_s$ | 10^3MK_c | 10^3MK_s | 10^3MC_c | 10^3MC_s | 10^3MD_c | 10^3MD_s |
| 18v-18g' | +3.8671 | +0.0104 | +0.5469 | +0.0015 | -0.1093 | -0.0004 | +0.0022 | -0.5376 |
| 18v-17g' | -0.3010 | +0.1008 | -0.0426 | +0.0142 | +0.0011 | -0.0008 | +0.0146 | +0.0441 |
| 18v-16g' | +0.1081 | -0.1218 | +0.01528 | -0.01723 | -0.00864 | +0.00998 | -0.01571 | -0.01366 |
| 18v-15g' | -0.0004 | +0.0059 | -0.00006 | +0.00083 | -0.00027 | -0.00004 | +0.00102 | +0.00030 |

§ 37. *Coefficients E and F for Venus.* Some preliminary computations render it doubtful whether the planetary coefficients *E* and *F* would lead to sensible inequalities in any case. But, in order to leave no doubt, they are computed for six of the twelve systems and thirty alternate values of the index for Venus. The separate numerical results are shown in Table XII. The general development will be, so far as it seemed useful to use it, found in Part IV.

TABLE XII.

SPECIAL VALUES OF E AND F FOR THE ACTION OF VENUS ON THE MOON.

| Coefficient E. | | | | | | | Coefficient F. | | | | | | |
|----------------|----------|----------|----------|----------|----------|-----------|----------------|----------|----------|----------|----------|----------|-----------|
| <i>i</i> | System 0 | System 2 | System 4 | System 6 | System 8 | System 10 | <i>i</i> | System 0 | System 2 | System 4 | System 6 | System 8 | System 10 |
| 0 | +3.528 | +6.997 | +3.567 | -2.569 | -6.300 | -4.684 | 0 | +0.071 | +0.617 | +0.231 | +0.039 | +0.532 | +0.345 |
| 1 | +2.216 | +3.683 | +1.277 | -1.664 | -2.541 | -1.248 | 1 | -1.154 | -1.613 | -0.556 | +0.836 | +1.484 | +0.750 |
| 2 | +0.643 | +0.872 | +0.160 | -0.545 | -0.620 | -0.150 | 2 | -0.571 | +0.701 | -0.126 | +0.459 | +0.574 | +0.144 |
| 3 | +0.218 | +0.233 | -0.006 | -0.198 | -0.179 | 0.000 | 3 | -0.229 | -0.226 | -0.005 | +0.198 | +0.192 | 0.000 |
| 4 | +0.094 | +0.078 | -0.024 | -0.089 | -0.064 | +0.019 | 4 | -0.100 | -0.077 | +0.023 | +0.090 | +0.069 | -0.021 |
| 5 | +0.049 | +0.030 | -0.022 | -0.046 | -0.026 | +0.013 | 5 | -0.048 | -0.028 | +0.020 | +0.045 | +0.026 | -0.019 |
| 6 | +0.028 | +0.012 | -0.018 | -0.027 | -0.024 | +0.015 | 6 | -0.025 | -0.010 | +0.015 | +0.024 | +0.010 | -0.014 |
| 7 | +0.017 | +0.004 | -0.014 | -0.017 | -0.004 | +0.013 | 7 | -0.014 | +0.003 | +0.011 | +0.013 | +0.003 | -0.010 |
| 8 | +0.011 | 0.000 | -0.012 | -0.011 | 0.000 | +0.011 | 8 | -0.007 | 0.000 | +0.007 | +0.007 | 0.000 | -0.007 |
| 9 | +0.007 | -0.002 | -0.009 | -0.007 | +0.002 | +0.009 | 9 | -0.004 | +0.001 | +0.005 | +0.004 | -0.001 | -0.005 |
| 10 | +0.004 | -0.003 | -0.008 | -0.004 | +0.003 | +0.008 | 10 | -0.002 | +0.002 | +0.003 | +0.002 | -0.001 | -0.004 |
| 11 | +0.003 | -0.004 | -0.007 | -0.003 | +0.004 | +0.006 | 11 | -0.001 | +0.001 | +0.002 | +0.001 | -0.001 | -0.002 |
| 12 | +0.001 | -0.004 | -0.005 | -0.001 | +0.004 | +0.005 | 12 | 0.000 | +0.001 | +0.001 | 0.000 | -0.001 | -0.002 |
| 13 | 0.000 | -0.005 | -0.005 | 0.000 | +0.004 | +0.004 | 13 | 0.000 | +0.001 | +0.001 | 0.000 | -0.001 | -0.001 |
| 14 | -0.001 | -0.005 | -0.004 | +0.001 | +0.005 | +0.004 | 14 | 0.000 | 0.000 | 0.000 | 0.000 | -0.001 | 0.000 |
| 15 | -0.002 | -0.005 | -0.003 | +0.002 | +0.005 | +0.003 | 15 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 16 | -0.003 | -0.005 | -0.002 | +0.003 | +0.005 | +0.002 | 16 | 0.000 | -0.001 | 0.000 | 0.000 | 0.000 | 0.000 |
| 17 | -0.004 | -0.005 | -0.001 | +0.004 | +0.005 | +0.001 | 17 | -0.001 | -0.001 | 0.000 | +0.001 | +0.001 | 0.000 |
| 18 | -0.005 | -0.005 | 0.000 | +0.005 | +0.005 | 0.000 | 18 | -0.001 | -0.001 | 0.000 | +0.001 | +0.001 | 0.000 |
| 19 | -0.006 | -0.005 | +0.001 | +0.006 | +0.005 | -0.002 | 19 | -0.002 | -0.002 | 0.000 | +0.002 | +0.002 | -0.001 |
| 20 | -0.008 | -0.004 | +0.003 | +0.007 | +0.005 | -0.003 | 20 | -0.004 | -0.002 | +0.001 | +0.003 | +0.002 | -0.002 |
| 21 | -0.010 | -0.004 | +0.005 | +0.009 | +0.004 | -0.006 | 21 | -0.006 | -0.002 | +0.003 | +0.005 | +0.002 | -0.003 |
| 22 | -0.012 | -0.003 | +0.009 | +0.012 | +0.002 | -0.010 | 22 | -0.008 | -0.001 | +0.006 | +0.008 | +0.002 | -0.007 |
| 23 | -0.016 | 0.000 | +0.014 | +0.015 | 0.000 | -0.017 | 23 | -0.012 | 0.000 | +0.011 | +0.012 | 0.000 | -0.012 |
| 24 | -0.021 | +0.005 | +0.024 | +0.020 | -0.007 | -0.029 | 24 | -0.019 | +0.005 | +0.022 | +0.017 | -0.006 | -0.025 |
| 25 | -0.028 | +0.018 | +0.043 | +0.027 | -0.023 | -0.053 | 25 | -0.028 | +0.018 | +0.043 | +0.026 | -0.021 | -0.050 |
| 26 | -0.039 | +0.050 | +0.084 | +0.037 | -0.065 | -0.108 | 26 | -0.042 | +0.055 | +0.090 | +0.038 | -0.064 | -0.109 |
| 27 | -0.050 | +0.152 | +0.194 | +0.045 | -0.208 | -0.264 | 27 | -0.053 | +0.167 | +0.205 | +0.044 | -0.198 | -0.260 |
| 28 | 0.000 | +0.569 | +0.561 | -0.017 | -0.799 | -0.819 | 28 | 0.000 | +0.543 | +0.507 | -0.014 | -0.623 | -0.672 |
| 29 | +0.730 | +2.564 | +1.885 | -0.681 | -3.325 | -2.919 | 29 | +0.406 | +1.557 | +1.061 | -0.325 | -1.402 | -1.331 |

B. ACTION OF MARS.

§ 38. For Mars the coefficients *A*, *B*, *C*, and *D* were developed much in the same way as for Venus. But, owing to the supposed absence of terms having a high multiple of the mean longitude of Mars, it was considered sufficient to divide the mean orbit of Mars into 24 parts for the special computations of the *A*-coefficients. The adopted number of systems was 12, as in the case of Venus.

The following statements, with the diagram, will make clear the method of carrying out the computation. In system 0 the Earth remains at rest at its perihelion

and is, therefore, in longitude approximately $\pi_0' = 99^\circ.5$. Mars starting from this same mean longitude, π_0' , takes the twenty-four consecutive mean longitudes π_0' , $\pi_0' + 15^\circ$, $\pi_0' + 30^\circ$, etc., to $\pi_0' + 345^\circ$. These twenty-four positions are designated by the twenty-four indices 0, 1, 2, 3, . . . 23.

In system 1 the Earth is in mean anomaly 30° . Then, as before, Mars takes the successive mean longitudes $\pi_0' + 30^\circ$, $\pi_0' + 45^\circ$, . . . up to $\pi_0' + 15^\circ$.

The same plan is carried through; the constant mean anomaly of the Earth in the i th system being $i \times 30^\circ$, while Mars, starting with the same mean longitude, goes through its twenty-four consecutive mean positions, the indices which express the mean longitude of Mars always starting with the value 0 when Mars is in mean conjunction with the Earth.

As in the case of Venus, the elements were taken with their values for 1800, in order to correspond to the mean of the period during which the longitude of the Moon has been observed. The numbers and data for computing the longitude of Mars are, then, as follows:

- π_0' ; long. of \oplus 's perihelion for 1800; $99^\circ 30' 7''.6$
- π_4 ; " " Mars' " " " ; $332^\circ 22' 42''.9$
- $\pi_0' - \pi_4$; initial mean anom. of Mars for 1800; $127^\circ 7' 24''.7$

Initial mean anomaly of Mars in system j

$$g_1 = 127^\circ 7' 24''.7 + 30^\circ \times j$$

For system j and index i

$$g_i = 127^\circ 7' 24''.7 + 30^\circ \times j + 15^\circ \times i$$

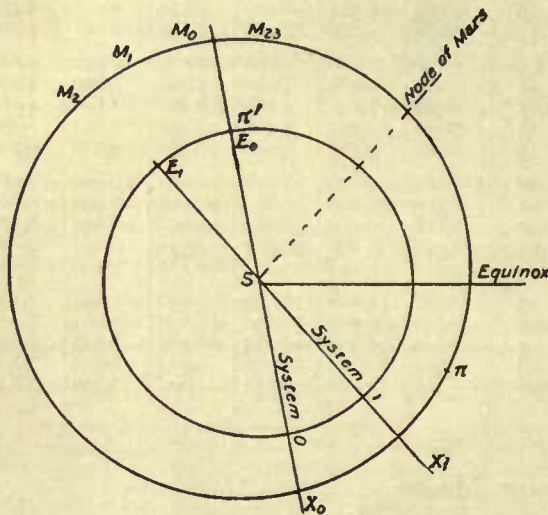
From the numbers found in *Tables of Mars*, page 397, it is found that to this initial mean anomaly corresponds

$$\text{Fund. Arg. } N = 243^d.0948$$

and that the increment of N for 15° of mean anomaly is

$$\Delta N = 28^d.62482$$

For the numbers arising from the inclination of the orbit of Mars we have:



Arrangement of Coördinate Axes in Systems 0, 1, etc., for Mars.

Long. of node, 1800; . $\theta = 48^\circ 0' 52''.5$

Node from \oplus 's perihelion; $308^\circ 30' 44''.9$

Inclination, 1800; $I = 1^\circ 51' 3''.6$

The results of the main steps in the computation of the coördinates of Mars are shown in the following table. The first column corresponds to the indices of system *o*. In the *j*th system they are diminished by 27.

The second column shows the value of *N* actually used in entering the tables. The discrepancy of two units in the fourth place results from using two computations of *N*. Column *f* gives the mean anomaly as taken from the tables, reduced by the secular variation to 1800. Column *u* is formed by adding to *f* the distance from the node to the perihelion of Mars and applying the reduction to the ecliptic. This reduction was applied in order to use for *x* and *y* simple formulæ for the ecliptic longitude. Actually, through a misapprehension, the rectangular coördinates were computed on the supposition that *u* was counted along the orbit, as in the case of Venus. There is therefore an error in the last figures of the coördinates, the amount of which can readily be determined, but which has been deemed too small to need correction for the present problem.

TABLE XIII.

COMPUTATION OF HELIOCENTRIC COÖRDINATES OF MARS.

| <i>i</i> | <i>N</i> | <i>f</i> | <i>u</i> | log. <i>r</i> | <i>x</i> | <i>y</i> | <i>z</i> |
|----------|----------|------------------------------------|-----------|---------------|-----------|-----------|-----------|
| 0 | 243.0946 | 135 ^o 3 17 ["] | 59 24 20 | 0.208 749 | -1.601 16 | -0.222 32 | +0.044 97 |
| 1 | 271.7194 | 148 7 1 | 72 28 19 | 0.214 918 | -1.530 86 | -0.586 91 | +0.050 53 |
| 2 | 300.3442 | 160 52 11 | 85 13 52 | 0.219 143 | -1.376 61 | -0.919 51 | +0.053 32 |
| 3 | 328.9690 | 173 26 7 | 97 48 12 | 0.221 310 | -1.149 04 | -1.203 24 | +0.053 27 |
| 4 | 357.5939 | 185 56 13 | 110 18 38 | 0.221 364 | -0.861 21 | -1.423 86 | +0.050 43 |
| 5 | 386.2187 | 198 29 47 | 122 52 26 | 0.219 303 | -0.528 30 | -1.569 81 | +0.044 95 |
| 6 | 414.8435 | 211 14 12 | 135 36 56 | 0.215 179 | -0.167 45 | -1.632 28 | +0.037 08 |
| 7 | 443.4683 | 224 16 54 | 148 39 31 | 0.209 102 | +0.202 38 | -1.605 53 | +0.027 19 |
| 8 | 472.0932 | 237 45 02 | 162 7 24 | 0.201 264 | +0.560 38 | -1.487 37 | +0.015 76 |
| 9 | 500.7180 | 251 45 55 | 176 7 52 | 0.191 962 | +0.884 48 | -1.279 95 | +0.003 39 |
| 10 | 529.3428 | 266 25 53 | 190 47 23 | 0.181 634 | +1.151 73 | -0.990 76 | -0.009 19 |
| 11 | 557.9676 | 281 49 50 | 206 10 58 | 0.170 884 | +1.339 64 | -0.633 72 | -0.021 13 |
| 12 | 586.5924 | 298 0 12 | 222 21 9 | 0.160 502 | +1.428 36 | -0.230 06 | -0.031 49 |
| 13 | 615.2172 | 314 55 23 | 239 16 26 | 0.151 419 | +1.403 60 | +0.191 54 | -0.039 35 |
| 14 | 643.8421 | 332 28 46 | 256 50 12 | 0.144 609 | +1.260 23 | +0.596 86 | -0.043 88 |
| 15 | 672.4669 | 350 28 12 | 274 50 11 | 0.140 910 | +1.005 34 | +0.949 09 | -0.044 52 |
| 16 | 14.0961 | 8 37 13 | 292 59 42 | 0.140 817 | +0.659 23 | +1.215 07 | -0.041 12 |
| 17 | 42.7209 | 26 37 36 | 311 00 19 | 0.144 343 | +0.253 23 | +1.370 65 | -0.033 99 |
| 18 | 71.3457 | 44 12 35 | 328 35 12 | 0.151 014 | -0.175 28 | +1.404 75 | -0.023 84 |
| 19 | 99.9705 | 61 9 53 | 345 32 8 | 0.160 006 | -0.589 17 | +1.319 88 | -0.011 66 |
| 20 | 128.5954 | 77 22 34 | 1 44 20 | 0.170 346 | -0.956 46 | +1.129 79 | +0.001 45 |
| 21 | 157.2202 | 92 48 50 | 17 10 10 | 0.181 098 | -1.253 06 | +0.855 63 | +0.014 47 |
| 22 | 185.8450 | 107 30 54 | 31 51 56 | 0.191 465 | -1.403 47 | +0.522 13 | +0.026 50 |
| 23 | 214.4698 | 121 33 36 | 45 54 32 | 0.200 829 | -1.579 94 | +0.154 73 | +0.036 84 |

TABLE XIV.

G-COÖRDINATES OF MARS REDUCED TO THE DIFFERENT SYSTEMS.

| | System 0. | | System 1. | | System 2. | | System 3. | |
|----|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> |
| 0 | -0.617 95 | -0.222 32 | -0.666 54 | -0.091 17 | -0.672 31 | +0.063 05 | -0.632 56 | +0.201 03 |
| 1 | -0.547 65 | -0.586 91 | -0.611 33 | -0.450 67 | -0.632 25 | -0.298 23 | -0.605 81 | -0.168 80 |
| 2 | -0.393 40 | -0.919 51 | -0.472 37 | -0.785 65 | -0.505 93 | -0.641 98 | -0.487 65 | -0.526 80 |
| 3 | -0.165 83 | -1.203 24 | -0.257 03 | -1.078 49 | -0.297 85 | -0.948 87 | -0.280 23 | -0.850 90 |
| 4 | +0.122 00 | -1.423 86 | +0.024 24 | -1.313 03 | -0.016 52 | -1.199 84 | +0.008 96 | -1.118 15 |
| 5 | +0.454 91 | -1.569 81 | +0.357 89 | -1.474 77 | +0.325 16 | -1.376 81 | +0.366 00 | -1.306 06 |
| 6 | +0.815 76 | -1.632 28 | +0.727 02 | -1.351 44 | +0.709 23 | -1.463 66 | +0.769 66 | -1.394 78 |
| 7 | +1.185 59 | -1.605 53 | +1.111 41 | -1.533 86 | +1.112 39 | -1.447 88 | +1.191 26 | -1.370 02 |
| 8 | +1.543 59 | -1.487 37 | +1.487 44 | -1.417 03 | +1.506 33 | -1.322 88 | +1.596 58 | -1.226 65 |
| 9 | +1.867 69 | -1.279 95 | +1.828 70 | -1.201 79 | +1.859 07 | -1.090 63 | +1.948 81 | -0.971 76 |
| 10 | +2.134 94 | -0.990 76 | +2.107 36 | -0.896 57 | +2.138 39 | -0.763 82 | +2.214 79 | -0.625 65 |
| 11 | +2.322 85 | -0.633 72 | +2.296 71 | -0.519 07 | +2.316 00 | -0.366 96 | +2.370 37 | -0.219 65 |
| 12 | +2.411 57 | -0.230 06 | +2.375 22 | -0.096 37 | +2.373 28 | +0.065 77 | +2.404 47 | +0.208 86 |
| 13 | +2.386 81 | +0.191 54 | +2.330 58 | +0.336 12 | +2.305 02 | +0.495 16 | +2.319 60 | +0.622 75 |
| 14 | +2.243 44 | +0.596 86 | +2.163 83 | +0.739 52 | +2.120 30 | +0.883 32 | +2.129 51 | +0.990 04 |
| 15 | +1.988 55 | +0.949 09 | +1.890 02 | +1.077 26 | +1.839 87 | +1.199 33 | +1.855 35 | +1.286 64 |
| 16 | +1.642 44 | +1.215 07 | +1.535 96 | +1.321 04 | +1.491 59 | +1.422 36 | +1.521 85 | +1.497 05 |
| 17 | +1.236 44 | +1.370 65 | +1.135 09 | +1.454 49 | +1.105 86 | +1.542 15 | +1.154 45 | +1.613 52 |
| 18 | +0.807 93 | +1.404 75 | +0.721 96 | +1.473 51 | +0.711 84 | +1.557 61 | +0.777 40 | +1.634 74 |
| 19 | +0.394 04 | +1.319 88 | +0.328 01 | +1.384 38 | +0.335 42 | +1.474 78 | +0.412 81 | +1.564 44 |
| 20 | +0.026 75 | +1.129 79 | -0.020 95 | +1.200 76 | -0.001 73 | +1.304 64 | +0.080 21 | +1.410 19 |
| 21 | -0.269 85 | +0.855 63 | -0.305 52 | +0.940 82 | -0.282 32 | +1.061 47 | -0.203 52 | +1.182 62 |
| 22 | -0.480 26 | +0.522 13 | -0.512 42 | +0.624 89 | -0.493 23 | +0.761 58 | -0.424 14 | +0.894 79 |
| 23 | -0.596 73 | +0.154 73 | -0.633 83 | +0.274 00 | -0.625 17 | +0.422 63 | -0.570 09 | +0.561 88 |
| | System 4. | | System 5. | | System 6. | | System 7. | |
| 0 | -0.560 10 | +0.287 39 | -0.478 34 | +0.298 89 | -0.411 57 | +0.230 06 | -0.375 36 | +0.096 49 |
| 1 | -0.542 52 | -0.097 00 | -0.462 56 | -0.104 27 | -0.386 81 | -0.191 54 | -0.330 72 | -0.336 00 |
| 2 | -0.425 69 | -0.473 03 | -0.337 56 | -0.498 21 | -0.243 44 | -0.596 86 | -0.163 97 | -0.739 40 |
| 3 | -0.210 45 | -0.814 29 | -0.105 31 | -0.850 95 | +0.011 45 | -0.949 09 | +0.109 84 | -1.077 14 |
| 4 | +0.094 77 | -1.092 95 | +0.221 50 | -1.130 27 | +0.357 56 | -1.215 07 | +0.463 90 | -1.320 92 |
| 5 | +0.472 27 | -1.282 30 | +0.618 36 | -1.307 88 | +0.763 56 | -1.370 65 | +0.864 77 | -1.454 37 |
| 6 | +0.894 97 | -1.360 81 | +1.051 09 | -1.365 16 | +1.192 07 | -1.404 75 | +1.277 90 | -1.473 39 |
| 7 | +1.327 46 | -1.316 17 | +1.480 48 | -1.296 90 | +1.605 96 | -1.319 88 | +1.671 85 | -1.384 26 |
| 8 | +1.730 86 | -1.149 42 | +1.868 64 | -1.112 18 | +1.973 25 | -1.129 79 | +2.020 81 | -1.200 64 |
| 9 | +2.068 60 | -0.875 61 | +2.184 65 | -0.831 75 | +2.269 85 | -0.855 63 | +2.305 38 | -0.940 70 |
| 10 | +2.312 38 | -0.521 55 | +2.407 68 | -0.483 47 | +2.480 26 | -0.522 13 | +2.512 28 | -0.624 77 |
| 11 | +2.445 83 | -0.120 68 | +2.527 47 | -0.097 74 | +2.596 73 | -0.154 73 | +2.633 69 | -0.273 88 |
| 12 | +2.464 85 | +0.292 45 | +2.542 93 | +0.296 28 | +2.617 95 | +0.222 32 | +2.666 40 | +0.091 29 |
| 13 | +2.375 72 | +0.686 40 | +2.460 10 | +0.672 70 | +2.547 65 | +0.586 91 | +2.611 19 | +0.450 79 |
| 14 | +2.192 10 | +1.035 36 | +2.289 96 | +1.009 85 | +2.393 40 | +0.919 51 | +2.472 23 | +0.785 77 |
| 15 | +1.932 16 | +1.319 93 | +2.046 79 | +1.290 44 | +2.165 83 | +1.203 24 | +2.256 69 | +1.078 61 |
| 16 | +1.616 23 | +1.526 83 | +1.746 90 | +1.501 35 | +1.878 00 | +1.423 86 | +1.975 62 | +1.313 15 |
| 17 | +1.265 34 | +1.648 24 | +1.407 95 | +1.633 29 | +1.545 09 | +1.569 81 | +1.641 97 | +1.474 89 |
| 18 | +0.900 17 | +1.680 95 | +1.048 37 | +1.680 43 | +1.184 24 | +1.632 28 | +1.272 84 | +1.551 56 |
| 19 | +0.540 67 | +1.625 74 | +0.687 09 | +1.640 37 | +0.814 41 | +1.605 53 | +0.888 45 | +1.533 98 |
| 20 | +0.205 69 | +1.486 78 | +0.343 34 | +1.514 05 | +0.456 41 | +1.487 37 | +0.512 42 | +1.417 15 |
| 21 | -0.087 15 | +1.271 44 | +0.036 45 | +1.305 97 | +0.132 31 | +1.279 95 | +0.171 16 | +1.201 91 |
| 22 | -0.321 69 | +0.990 17 | -0.214 52 | +1.024 64 | -0.134 94 | +0.990 76 | -0.107 50 | +0.896 69 |
| 23 | -0.483 43 | +0.656 52 | -0.391 49 | +0.682 96 | -0.322 85 | +0.633 72 | -0.296 85 | +0.519 19 |

TABLE XIV.—*Concluded.*

G-COÖRDINATES OF MARS REDUCED TO THE DIFFERENT SYSTEMS.

| | System 8. | | System 9. | | System 10. | | System 11. | |
|----|-----------|-----------|-----------|-----------|------------|-----------|------------|-----------|
| | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> | <i>X</i> | <i>Y</i> |
| 0 | -0.373 70 | -0.065 64 | -0.405 03 | -0.208 86 | -0.465 27 | -0.292 58 | -0.543 07 | -0.296 40 |
| 1 | -0.305 44 | -0.495 03 | -0.320 16 | -0.622 75 | -0.376 14 | -0.686 53 | -0.460 24 | -0.672 82 |
| 2 | -0.120 72 | -0.883 19 | -0.130 07 | -0.990 04 | -0.192 52 | -1.035 49 | -0.290 10 | -1.009 97 |
| 3 | +0.159 71 | -1.199 20 | +0.144 09 | -1.286 64 | +0.067 42 | -1.320 06 | -0.046 93 | -1.290 56 |
| 4 | +0.507 99 | -1.422 23 | +0.477 59 | -1.497 05 | +0.383 35 | -1.526 96 | +0.252 96 | -1.501 47 |
| 5 | +0.893 72 | -1.542 02 | +0.844 99 | -1.613 52 | +0.734 24 | -1.648 37 | +0.591 91 | -1.633 41 |
| 6 | +1.287 74 | -1.557 48 | +1.222 04 | -1.634 74 | +1.099 41 | -1.681 08 | +0.951 49 | -1.680 55 |
| 7 | +1.664 16 | -1.474 65 | +1.586 63 | -1.564 44 | +1.458 91 | -1.625 87 | +1.312 77 | -1.640 49 |
| 8 | +2.001 31 | -1.304 51 | +1.919 23 | -1.410 19 | +1.793 89 | -1.486 91 | +1.656 52 | -1.514 17 |
| 9 | +2.281 90 | -1.061 34 | +2.202 96 | -1.182 62 | +2.086 73 | -1.271 57 | +1.963 41 | -1.306 09 |
| 10 | +2.492 81 | -0.761 45 | +2.423 58 | -0.894 79 | +2.321 27 | -0.990 30 | +2.214 38 | -1.024 76 |
| 11 | +2.624 75 | -0.422 50 | +2.569 53 | -0.561 88 | +2.483 01 | -0.656 65 | +2.391 35 | -0.683 08 |
| 12 | +2.671 89 | -0.062 92 | +2.632 00 | -0.201 03 | +2.559 68 | -0.287 52 | +2.478 20 | -0.299 01 |
| 13 | +2.631 83 | +0.298 36 | +2.605 25 | +0.168 80 | +2.542 10 | +0.096 87 | +2.462 42 | +0.104 15 |
| 14 | +2.505 51 | +0.642 11 | +2.487 09 | +0.526 80 | +2.425 27 | +0.472 90 | +2.337 42 | +0.498 09 |
| 15 | +2.297 43 | +0.949 00 | +2.279 67 | +0.850 90 | +2.210 03 | +0.814 16 | +2.105 17 | +0.850 83 |
| 16 | +2.016 10 | +1.199 97 | +1.990 48 | +1.118 15 | +1.904 81 | +1.092 82 | +1.778 36 | +1.130 15 |
| 17 | +1.674 42 | +1.376 94 | +1.633 44 | +1.306 06 | +1.527 31 | +1.282 17 | +1.381 50 | +1.307 76 |
| 18 | +1.290 35 | +1.463 79 | +1.229 78 | +1.394 78 | +1.104 61 | +1.360 68 | +0.948 77 | +1.305 04 |
| 19 | +0.887 19 | +1.448 01 | +0.808 18 | +1.370 02 | +0.672 12 | +1.316 04 | +0.519 38 | +1.296 78 |
| 20 | +0.493 25 | +1.323 01 | +0.402 86 | +1.226 65 | +0.268 72 | +1.149 29 | +0.131 22 | +1.112 06 |
| 21 | +0.140 51 | +1.090 76 | +0.050 63 | +0.971 76 | -0.069 02 | +0.875 48 | -0.184 79 | +0.831 63 |
| 22 | -0.138 81 | +0.763 95 | -0.215 35 | +0.625 65 | -0.312 80 | +0.521 42 | -0.407 82 | +0.483 35 |
| 23 | -0.316 42 | +0.367 09 | -0.370 93 | +0.219 65 | -0.446 25 | +0.120 55 | -0.527 61 | +0.097 62 |

TABLE XV.

SPECIAL VALUES OF A, B, C, AND D FOR MARS.

| System 0. | | | | System 1. | | | | | |
|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +1.920 41 | -0.768 57 | -1.151 95 | +1.111 16 | 0 | +2.088 60 | -1.024 97 | -1.064 03 | +0.433 99 |
| 1 | +0.250 33 | +0.382 65 | -0.633 03 | +0.954 82 | 1 | +0.705 52 | +0.038 62 | -0.744 19 | +1.076 90 |
| 2 | -0.178 22 | +0.507 19 | -0.328 97 | +0.358 95 | 2 | -0.088 66 | +0.515 53 | -0.426 83 | +0.568 93 |
| 3 | -0.175 15 | +0.359 60 | -0.184 43 | +0.075 13 | 3 | -0.204 72 | +0.447 51 | -0.242 79 | +0.164 80 |
| 4 | -0.111 50 | +0.225 06 | -0.113 56 | -0.029 05 | 4 | -0.146 86 | +0.293 51 | -0.146 66 | -0.008 13 |
| 5 | -0.058 53 | +0.134 50 | -0.076 06 | -0.061 07 | 5 | -0.079 42 | +0.174 65 | -0.095 23 | -0.065 51 |
| 6 | -0.021 97 | +0.076 72 | -0.054 76 | -0.065 74 | 6 | -0.030 47 | +0.096 73 | -0.066 25 | -0.076 39 |
| 7 | +0.002 45 | +0.039 44 | -0.041 89 | -0.060 08 | 7 | +0.001 61 | +0.047 44 | -0.049 04 | -0.059 91 |
| 8 | +0.018 80 | +0.015 03 | -0.033 83 | -0.050 72 | 8 | +0.022 02 | +0.016 43 | -0.038 44 | -0.057 60 |
| 9 | +0.029 90 | -0.001 19 | -0.028 72 | -0.040 17 | 9 | +0.034 83 | -0.003 03 | -0.031 80 | -0.043 79 |
| 10 | +0.037 54 | -0.011 98 | -0.025 57 | -0.029 29 | 10 | +0.042 73 | -0.014 99 | -0.027 72 | -0.029 98 |
| 11 | +0.042 79 | -0.018 92 | -0.023 87 | -0.018 19 | 11 | +0.047 31 | -0.021 81 | -0.025 51 | -0.016 46 |
| 12 | +0.046 23 | -0.022 81 | -0.023 43 | -0.006 65 | 12 | +0.049 46 | -0.024 68 | -0.024 77 | -0.003 01 |
| 13 | +0.048 05 | -0.023 80 | -0.024 25 | +0.005 80 | 13 | +0.049 46 | -0.023 96 | -0.025 49 | +0.010 81 |
| 14 | +0.047 95 | -0.021 35 | -0.026 60 | +0.019 84 | 14 | +0.046 97 | -0.019 12 | -0.027 83 | +0.025 58 |
| 15 | +0.044 92 | -0.013 81 | -0.031 10 | +0.036 30 | 15 | +0.040 91 | -0.008 56 | -0.032 35 | +0.041 77 |
| 16 | +0.036 65 | +0.002 37 | -0.039 01 | +0.056 01 | 16 | +0.029 03 | +0.011 04 | -0.040 06 | +0.059 44 |
| 17 | +0.018 30 | +0.034 61 | -0.052 92 | +0.079 09 | 17 | +0.007 19 | +0.045 88 | -0.053 06 | +0.077 22 |
| 18 | -0.019 93 | +0.098 16 | -0.078 25 | +0.101 49 | 18 | -0.031 63 | +0.107 09 | -0.075 45 | +0.089 44 |
| 19 | -0.096 22 | +0.223 72 | -0.127 50 | +0.104 86 | 19 | -0.097 28 | +0.212 99 | -0.115 69 | +0.077 88 |
| 20 | -0.230 56 | +0.461 52 | -0.230 95 | +0.016 40 | 20 | -0.192 14 | +0.384 18 | -0.192 04 | -0.010 06 |
| 21 | -0.336 21 | +0.797 25 | -0.461 05 | -0.396 96 | 21 | -0.245 44 | +0.587 62 | -0.342 21 | -0.302 42 |
| 22 | +0.347 58 | +0.580 43 | -0.927 87 | -1.390 90 | 22 | +0.127 35 | +0.495 62 | -0.622 90 | -0.922 00 |
| 23 | +2.549 00 | -1.148 74 | -1.400 16 | -1.027 90 | 23 | +1.520 82 | -0.532 46 | -0.988 31 | -1.091 63 |

TABLE XV.—Continued.

SPECIAL VALUES OF A, B, C, AND D FOR MARS.

| System 2. | | | | | System 3. | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +2.101 41 | -1.045 67 | -1.055 73 | -0.297 76 | 0 | +1.947 47 | -0.823 38 | -1.124 08 | -0.979 52 |
| 1 | +1.400 17 | -0.442 44 | -0.957 75 | +1.117 88 | 1 | +2.376 80 | -1.048 03 | -1.328 82 | +1.034 57 |
| 2 | +0.089 45 | +0.515 34 | -0.604 76 | +0.885 66 | 2 | +0.345 55 | +0.553 68 | -0.899 15 | +1.346 03 |
| 3 | -0.247 49 | +0.585 27 | -0.337 75 | +0.289 97 | 3 | -0.327 52 | +0.791 16 | -0.463 59 | +0.413 24 |
| 4 | -0.192 78 | +0.385 57 | -0.192 79 | +0.007 96 | 4 | -0.238 32 | +0.476 68 | -0.238 32 | -0.005 73 |
| 5 | -0.099 08 | +0.216 83 | -0.117 74 | -0.079 02 | 5 | -0.104 37 | +0.237 83 | -0.133 43 | -0.104 06 |
| 6 | -0.033 27 | +0.110 73 | -0.077 45 | -0.091 19 | 6 | -0.024 71 | +0.107 04 | -0.032 30 | -0.104 54 |
| 7 | +0.006 21 | +0.048 52 | -0.054 73 | -0.079 34 | 7 | +0.016 21 | +0.039 39 | -0.055 58 | -0.082 65 |
| 8 | +0.028 67 | +0.012 65 | -0.041 33 | -0.001 50 | 8 | +0.036 14 | +0.004 61 | -0.040 75 | -0.059 12 |
| 9 | +0.040 97 | -0.007 72 | -0.033 24 | -0.043 55 | 9 | +0.045 21 | -0.013 00 | -0.032 22 | -0.038 63 |
| 10 | +0.047 22 | -0.018 80 | -0.028 43 | -0.027 03 | 10 | +0.048 58 | -0.021 27 | -0.027 30 | -0.021 44 |
| 11 | +0.049 75 | -0.023 94 | -0.025 81 | -0.011 98 | 11 | +0.048 76 | -0.024 07 | -0.024 68 | -0.005 81 |
| 12 | +0.049 71 | -0.024 83 | -0.024 87 | +0.002 07 | 12 | +0.046 87 | -0.023 18 | -0.023 70 | +0.006 13 |
| 13 | +0.047 48 | -0.022 06 | -0.025 41 | +0.015 66 | 13 | +0.043 26 | -0.019 21 | -0.024 06 | +0.018 07 |
| 14 | +0.042 80 | -0.015 30 | -0.027 49 | +0.029 29 | 14 | +0.037 75 | -0.012 02 | -0.025 74 | +0.029 52 |
| 15 | +0.034 78 | -0.003 32 | -0.031 46 | +0.043 18 | 15 | +0.029 70 | -0.000 75 | -0.028 96 | +0.040 68 |
| 16 | +0.021 75 | +0.016 33 | -0.038 07 | +0.057 04 | 16 | +0.017 96 | +0.016 27 | -0.034 24 | +0.051 37 |
| 17 | +0.000 92 | +0.047 85 | -0.048 76 | +0.069 29 | 17 | +0.000 66 | +0.041 96 | -0.042 62 | +0.060 55 |
| 18 | -0.031 96 | +0.098 26 | -0.066 29 | +0.075 22 | 18 | -0.025 10 | +0.081 14 | -0.056 05 | +0.065 29 |
| 19 | -0.082 07 | +0.178 16 | -0.096 09 | +0.062 41 | 19 | -0.063 25 | +0.141 60 | +0.078 35 | +0.058 10 |
| 20 | -0.149 84 | +0.299 14 | -0.149 31 | -0.000 60 | 20 | -0.116 89 | +0.234 43 | -0.117 53 | +0.020 05 |
| 21 | -0.201 17 | +0.450 32 | -0.249 17 | -0.186 47 | 21 | -0.175 77 | +0.366 96 | -0.191 20 | -0.096 25 |
| 22 | -0.051 76 | +0.491 04 | -0.439 33 | -0.605 51 | 22 | -0.154 23 | +0.493 56 | -0.339 31 | -0.396 04 |
| 23 | +0.807 50 | -0.049 04 | -0.758 48 | -1.066 38 | 23 | +0.334 45 | +0.366 39 | -0.640 81 | -0.967 23 |
| System 4. | | | | | System 5. | | | | |
| 0 | +1.832 10 | -0.500 77 | -1.331 96 | -1.624 80 | 0 | +2.148 15 | -0.293 03 | -1.855 19 | -2.502 41 |
| 1 | +3.797 02 | -1.806 10 | -1.990 90 | +1.034 88 | 1 | +5.764 33 | -2.665 97 | -3.098 75 | +2.002 10 |
| 2 | +0.442 09 | +0.849 47 | -1.292 02 | +1.927 87 | 2 | -0.089 37 | +1.600 16 | -1.510 72 | +2.116 20 |
| 3 | -0.454 66 | +1.013 21 | -0.558 66 | +0.406 52 | 3 | -0.503 27 | +1.027 00 | -0.523 75 | +0.192 32 |
| 4 | -0.246 47 | +0.497 94 | -0.251 49 | -0.065 04 | 4 | -0.193 56 | +0.410 28 | -0.216 73 | -0.123 06 |
| 5 | -0.083 76 | +0.213 91 | -0.130 15 | -0.126 83 | 5 | -0.049 74 | +0.159 37 | -0.109 63 | -0.127 33 |
| 6 | -0.007 31 | +0.084 19 | -0.076 89 | -0.106 05 | 6 | +0.007 54 | +0.057 46 | -0.065 01 | -0.094 38 |
| 7 | +0.026 10 | +0.024 79 | -0.050 89 | -0.076 42 | 7 | +0.030 46 | +0.013 21 | -0.043 66 | -0.064 96 |
| 8 | +0.040 16 | -0.003 05 | -0.037 10 | -0.051 33 | 8 | +0.039 37 | -0.005 98 | -0.032 40 | -0.042 72 |
| 9 | +0.045 38 | -0.016 00 | -0.029 38 | -0.031 65 | 9 | +0.042 28 | -0.016 18 | -0.025 09 | -0.026 03 |
| 10 | +0.046 40 | -0.021 39 | -0.025 01 | -0.016 11 | 10 | +0.042 40 | -0.019 89 | -0.022 51 | -0.013 03 |
| 11 | +0.045 24 | -0.022 53 | -0.022 70 | -0.003 35 | 11 | +0.041 09 | -0.020 51 | -0.020 60 | -0.002 39 |
| 12 | +0.042 68 | -0.020 89 | -0.021 80 | +0.007 65 | 12 | +0.038 92 | -0.019 06 | -0.019 85 | +0.006 85 |
| 13 | +0.038 98 | -0.016 95 | -0.022 04 | +0.017 63 | 13 | +0.035 97 | -0.015 89 | -0.020 07 | +0.015 33 |
| 14 | +0.033 97 | -0.010 59 | -0.023 38 | +0.027 09 | 14 | +0.032 11 | -0.010 87 | -0.021 23 | +0.023 53 |
| 15 | +0.027 18 | -0.001 19 | -0.025 99 | +0.035 51 | 15 | +0.026 95 | -0.003 45 | -0.023 48 | +0.031 81 |
| 16 | +0.017 72 | +0.012 55 | -0.030 27 | +0.045 37 | 16 | +0.019 75 | +0.007 46 | -0.027 21 | +0.040 39 |
| 17 | +0.004 14 | +0.032 90 | -0.037 05 | +0.053 75 | 17 | +0.009 24 | +0.023 92 | -0.033 15 | +0.049 24 |
| 18 | -0.015 94 | +0.063 85 | -0.047 91 | +0.059 91 | 18 | -0.006 86 | +0.049 63 | -0.042 78 | +0.057 70 |
| 19 | -0.046 43 | +0.112 41 | -0.065 99 | +0.059 39 | 19 | -0.032 71 | +0.091 80 | -0.059 09 | +0.063 25 |
| 20 | -0.092 87 | +0.190 96 | -0.098 08 | +0.040 04 | 20 | -0.075 96 | +0.164 81 | -0.088 86 | +0.057 56 |
| 21 | -0.158 48 | +0.318 61 | -0.160 13 | -0.032 86 | 21 | -0.149 03 | +0.298 19 | -0.149 19 | +0.012 49 |
| 22 | -0.357 45 | +1.200 62 | -0.843 21 | -1.004 68 | 22 | -0.253 88 | +0.544 16 | -0.290 26 | -0.174 74 |
| 23 | +0.032 96 | +0.579 17 | -0.612 03 | -0.878 68 | 23 | -0.176 33 | +0.859 51 | -0.683 21 | -0.884 34 |

TABLE XV.—Continued.

SPECIAL VALUES OF A, B, C, AND D FOR MARS.

| System 6. | | | | | System 7. | | | | |
|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +4.029 84 | -0.912 73 | -3.116 74 | -4.018 27 | 0 | +9.990 63 | -4.586 21 | -5.404 24 | -4.012 20 |
| 1 | +5.687 73 | -1.695 28 | -3.992 42 | +4.843 56 | 1 | +1.453 90 | +1.601 76 | -3.055 56 | +4.666 10 |
| 2 | -0.709 53 | +1.028 11 | -1.218 70 | +1.290 50 | 2 | -0.656 79 | +1.413 86 | -0.757 15 | +0.482 93 |
| 3 | -0.388 33 | +0.774 20 | -0.385 94 | -0.014 03 | 3 | -0.254 14 | +0.515 57 | -0.261 46 | -0.079 32 |
| 4 | -0.124 66 | +0.287 92 | -0.163 25 | -0.132 92 | 4 | -0.081 45 | +0.202 75 | -0.121 32 | -0.113 85 |
| 5 | -0.024 99 | +0.111 12 | -0.086 12 | -0.109 95 | 5 | -0.014 79 | +0.083 51 | -0.068 73 | -0.090 63 |
| 6 | +0.013 63 | +0.039 63 | -0.053 26 | -0.078 85 | 6 | +0.012 94 | +0.032 00 | -0.044 93 | -0.066 72 |
| 7 | +0.029 34 | +0.007 77 | -0.037 10 | -0.054 60 | 7 | +0.025 42 | +0.007 18 | -0.032 59 | -0.048 03 |
| 8 | +0.035 71 | -0.007 35 | -0.028 35 | -0.036 68 | 8 | +0.031 23 | -0.005 58 | -0.025 65 | -0.033 80 |
| 9 | +0.037 98 | -0.014 63 | -0.023 35 | -0.023 12 | 9 | +0.033 91 | -0.012 35 | -0.021 58 | -0.022 65 |
| 10 | +0.038 32 | -0.017 86 | -0.020 46 | -0.012 38 | 10 | +0.035 04 | -0.015 85 | -0.019 18 | -0.013 49 |
| 11 | +0.037 65 | -0.018 73 | -0.018 92 | -0.003 37 | 11 | +0.035 30 | -0.017 36 | -0.017 92 | -0.005 54 |
| 12 | +0.036 33 | -0.017 98 | -0.018 35 | +0.004 65 | 12 | +0.035 00 | -0.017 48 | -0.017 52 | +0.001 80 |
| 13 | +0.034 45 | -0.015 82 | -0.018 62 | +0.012 23 | 13 | +0.034 24 | -0.016 35 | -0.017 88 | +0.009 00 |
| 14 | +0.031 88 | -0.012 14 | -0.019 73 | +0.019 84 | 14 | +0.032 90 | -0.013 83 | -0.019 06 | +0.016 52 |
| 15 | +0.028 28 | -0.006 41 | -0.021 87 | +0.027 88 | 15 | +0.030 68 | -0.009 42 | -0.021 27 | +0.024 84 |
| 16 | +0.023 00 | +0.002 40 | -0.025 42 | +0.036 73 | 16 | +0.026 96 | -0.002 02 | -0.024 94 | +0.034 51 |
| 17 | +0.014 84 | +0.016 27 | -0.031 11 | +0.046 70 | 17 | +0.020 46 | +0.010 52 | -0.030 99 | +0.046 22 |
| 18 | +0.001 39 | +0.039 19 | -0.040 59 | +0.057 91 | 18 | +0.008 52 | +0.032 70 | -0.041 23 | +0.060 66 |
| 19 | -0.022 05 | +0.079 14 | -0.057 07 | +0.069 11 | 19 | +0.008 53 | +0.032 71 | -0.041 24 | +0.060 67 |
| 20 | -0.065 65 | +0.154 13 | -0.088 47 | +0.074 45 | 20 | -0.063 61 | +0.160 98 | -0.097 38 | +0.093 42 |
| 21 | -0.154 98 | +0.315 09 | -0.160 14 | +0.049 51 | 21 | -0.175 09 | +0.361 07 | -0.186 02 | +0.077 93 |
| 22 | -0.315 17 | +0.648 46 | -0.333 30 | -0.133 72 | 22 | -0.432 50 | +0.882 46 | -0.450 02 | -0.159 94 |
| 23 | -0.353 82 | +1.276 69 | -0.922 91 | -1.121 87 | 23 | -0.408 83 | +1.937 10 | -1.528 17 | -1.992 73 |
| System 8. | | | | | System 9. | | | | |
| 0 | +11.253 07 | -5.464 71 | -5.788 03 | +3.030 00 | 0 | +4.782 03 | -1.303 27 | -3.478 85 | +4.274 64 |
| 1 | -0.295 87 | +1.903 85 | -1.667 47 | +2.251 42 | 1 | -0.362 00 | +1.331 70 | -0.969 66 | +1.183 54 |
| 2 | -0.444 25 | +0.913 37 | -0.469 09 | +0.189 10 | 2 | +0.317 73 | +0.652 46 | -0.334 77 | +0.129 70 |
| 3 | -0.178 40 | +0.366 62 | -0.188 19 | +0.073 90 | 3 | -0.147 87 | +0.301 39 | -0.153 52 | -0.050 95 |
| 4 | -0.063 93 | +0.160 71 | -0.096 78 | -0.091 97 | 4 | -0.062 08 | +0.147 89 | -0.085 80 | -0.074 57 |
| 5 | -0.014 47 | +0.073 33 | -0.058 87 | -0.076 63 | 5 | -0.019 55 | +0.074 61 | -0.055 06 | -0.067 95 |
| 6 | +0.008 79 | +0.031 56 | -0.040 36 | -0.059 48 | 6 | +0.002 94 | +0.036 19 | -0.039 12 | -0.056 34 |
| 7 | +0.020 61 | +0.009 67 | -0.030 29 | -0.045 12 | 7 | +0.015 67 | +0.014 40 | -0.030 06 | -0.045 14 |
| 8 | +0.027 00 | -0.002 58 | -0.024 40 | -0.033 52 | 8 | +0.023 35 | +0.001 26 | -0.024 62 | -0.035 28 |
| 9 | +0.030 62 | -0.009 76 | -0.020 87 | -0.023 97 | 9 | +0.028 30 | -0.007 01 | -0.021 28 | -0.026 63 |
| 10 | +0.032 79 | -0.014 00 | -0.018 79 | -0.015 76 | 10 | +0.031 67 | -0.012 37 | -0.019 30 | -0.018 82 |
| 11 | +0.034 09 | -0.016 39 | -0.017 71 | -0.008 34 | 11 | +0.034 10 | -0.015 80 | -0.018 29 | -0.011 46 |
| 12 | +0.034 85 | -0.017 42 | -0.017 43 | -0.001 23 | 12 | +0.035 91 | -0.017 80 | -0.018 11 | -0.004 13 |
| 13 | +0.035 17 | -0.017 25 | -0.017 91 | +0.006 02 | 13 | +0.037 22 | -0.018 50 | -0.018 72 | +0.003 63 |
| 14 | +0.034 95 | -0.015 70 | -0.019 25 | +0.013 89 | 14 | +0.037 96 | -0.017 67 | -0.020 28 | +0.012 31 |
| 15 | +0.033 90 | -0.012 21 | -0.021 69 | +0.022 97 | 15 | +0.037 78 | -0.014 65 | -0.023 14 | +0.022 74 |
| 16 | +0.031 36 | -0.005 56 | -0.025 81 | +0.034 03 | 16 | +0.035 87 | -0.007 85 | -0.028 01 | +0.035 88 |
| 17 | +0.026 84 | +0.006 88 | -0.032 72 | +0.048 15 | 17 | +0.030 24 | +0.006 33 | -0.036 58 | +0.053 56 |
| 18 | +0.013 99 | +0.030 88 | -0.044 86 | +0.066 76 | 18 | +0.016 16 | +0.035 63 | -0.051 78 | +0.077 10 |
| 19 | -0.012 33 | +0.080 37 | -0.068 02 | +0.090 94 | 19 | -0.018 70 | +0.101 31 | -0.082 60 | +0.108 59 |
| 20 | -0.075 03 | +0.193 18 | -0.118 15 | +0.116 14 | 20 | -0.109 51 | +0.263 59 | -0.154 08 | +0.137 35 |
| 21 | -0.237 87 | +0.486 97 | -0.249 14 | +0.094 95 | 21 | -0.357 72 | +0.716 16 | -0.358 39 | +0.056 10 |
| 22 | -0.640 95 | +1.342 80 | -0.701 91 | -0.372 76 | 22 | -0.781 89 | +1.912 71 | -1.130 82 | -1.052 12 |
| 23 | +0.775 27 | +2.043 47 | -2.818 93 | -4.253 90 | 23 | +4.977 43 | -9.931 51 | -4.045 98 | -5.388 50 |

C. ACTION OF JUPITER.

§ 39. The action of Jupiter being computed on the same general method as Venus and Mars, but being much simpler, no detailed explanation seems necessary. Six systems, which suffice to carry the coefficients to terms of the third order in the eccentricities, were deemed enough.

The principal numbers used or derived are shown in the following tables. The fundamental data in the first table were derived from Hill's *Tables of Jupiter*.

TABLE XVII.
ECLIPTIC COÖRDINATES OF JUPITER FOR THE 12 POINTS OF DIVISION.

| <i>i</i> | Arg. <i>l</i> . | <i>f</i> + Red. to Ecliptic (Table 37). | log. <i>r</i> (Table 60). | <i>l</i> | <i>l</i> - π , | <i>x</i> | <i>y</i> | <i>z</i> |
|----------|-----------------|---|---------------------------|-----------|--------------------|----------|----------|----------|
| 0 | 1062.6047 | 93° 49' 10" | 0.716 624 | 105 1 44 | 185 31 36 | -5.1832 | -0.5015 | +0.0137 |
| 1 | 1423.6537 | 123 0 50 | 0.726 798 | 134 13 23 | 214 43 16 | -4.3816 | -3.0364 | +0.0714 |
| 2 | 1784.7027 | 151 3 0 | 0.733 962 | 162 15 33 | 242 45 26 | -2.4808 | -4.8184 | +0.1114 |
| 3 | 2145.7517 | 178 26 55 | 0.736 696 | 189 39 28 | 270 9 21 | +0.0148 | -5.4537 | +0.1248 |
| 4 | 2506.8007 | 205 48 41 | 0.734 514 | 217 1 15 | 297 31 7 | +2.5072 | -4.8125 | +0.1091 |
| 5 | 2867.8497 | 233 44 42 | 0.727 800 | 244 57 16 | 325 27 8 | +4.4010 | -3.0300 | +0.0675 |
| 6 | 3228.8987 | 262 47 7 | 0.717 865 | 273 59 41 | 354 29 33 | +5.1982 | -0.5012 | +0.0092 |
| 7 | 3589.9477 | 293 16 53 | 0.707 018 | 304 29 26 | 24 59 19 | +4.6167 | +2.1517 | -0.0512 |
| 8 | 3950.9967 | 325 13 29 | 0.698 343 | 336 26 2 | 56 55 55 | +2.7242 | +4.1841 | -0.0969 |
| 9 | 4312.0457 | 358 7 4 | 0.694 769 | 9 19 38 | 89 49 30 | +0.0151 | +4.9518 | -0.1134 |
| 10 | 340.5067 | 31 3 59 | 0.697 634 | 42 16 32 | 122 46 24 | -2.6983 | +4.1912 | -0.0948 |
| 11 | 701.5557 | 63 9 2 | 0.705 860 | 74 21 36 | 154 51 28 | -4.5987 | +2.1583 | -0.0474 |

TABLE XVIII.

JUPITER; DIRECT ACTION; SPECIAL VALUES OF THE A-COEFFICIENTS FOR 6 SYSTEMS.

| System 0. | | | | | System 1. | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +0.008 62 | -0.004 22 | -0.004 40 | +0.001 56 | 0 | +0.007 65 | -0.003 80 | -0.003 83 | +0.000 60 |
| 1 | +0.002 35 | -0.001 17 | -0.003 52 | +0.005 25 | 1 | +0.003 28 | +0.000 13 | -0.003 40 | +0.004 86 |
| 2 | -0.001 91 | +0.004 50 | -0.002 59 | +0.002 20 | 2 | -0.001 51 | +0.004 27 | -0.002 76 | +0.002 97 |
| 3 | -0.001 76 | +0.003 72 | -0.001 95 | -0.001 04 | 3 | -0.002 13 | +0.004 33 | -0.002 20 | -0.000 70 |
| 4 | +0.000 05 | +0.001 53 | -0.001 58 | -0.002 26 | 4 | -0.000 13 | +0.001 95 | -0.001 82 | -0.002 52 |
| 5 | +0.001 81 | -0.000 39 | -0.001 41 | -0.001 81 | 5 | +0.002 06 | -0.000 46 | -0.001 61 | -0.002 06 |
| 6 | +0.002 77 | -0.001 37 | -0.001 40 | -0.000 34 | 6 | +0.003 11 | -0.001 55 | -0.001 56 | -0.000 19 |
| 7 | +0.002 49 | -0.000 95 | -0.001 54 | +0.001 55 | 7 | +0.002 43 | -0.000 76 | -0.001 67 | +0.001 93 |
| 8 | +0.000 61 | +0.001 30 | -0.001 91 | +0.002 84 | 8 | +0.000 10 | +0.001 87 | -0.001 97 | +0.002 31 |
| 9 | -0.002 28 | +0.004 86 | -0.002 58 | +0.001 50 | 9 | -0.002 39 | +0.004 87 | -0.002 48 | +0.000 31 |
| 10 | -0.002 04 | +0.005 63 | -0.003 58 | -0.003 77 | 10 | -0.001 40 | +0.004 56 | -0.003 15 | -0.003 68 |
| 11 | +0.005 41 | -0.000 95 | -0.004 46 | -0.005 89 | 11 | +0.004 49 | -0.000 75 | -0.003 73 | -0.004 95 |
| System 2. | | | | | System 3. | | | | |
| 0 | +0.007 67 | -0.003 81 | -0.003 85 | -0.000 69 | 0 | +0.008 73 | -0.004 27 | -0.004 46 | -0.001 58 |
| 1 | +0.004 63 | -0.000 83 | -0.003 81 | +0.005 02 | 1 | +0.005 47 | -0.000 95 | -0.004 51 | +0.005 97 |
| 2 | -0.001 42 | +0.004 67 | -0.003 25 | +0.003 80 | 2 | -0.002 06 | +0.005 67 | -0.003 60 | +0.003 79 |
| 3 | -0.002 45 | +0.005 00 | -0.002 55 | -0.000 84 | 3 | -0.002 28 | +0.004 86 | -0.002 58 | -0.001 50 |
| 4 | +0.000 12 | +0.001 88 | -0.002 00 | -0.002 87 | 4 | +0.000 61 | +0.001 29 | -0.001 90 | -0.002 32 |
| 5 | +0.002 46 | -0.000 78 | -0.001 68 | -0.001 92 | 5 | +0.002 47 | -0.000 94 | -0.001 53 | -0.001 54 |
| 6 | +0.003 09 | -0.001 54 | -0.001 55 | +0.000 21 | 6 | +0.002 74 | -0.001 36 | -0.001 39 | +0.000 33 |
| 7 | +0.002 01 | -0.000 43 | -0.001 58 | +0.002 04 | 7 | +0.001 79 | -0.000 39 | -0.001 40 | +0.001 80 |
| 8 | -0.000 15 | +0.001 92 | -0.001 76 | +0.002 46 | 8 | +0.000 06 | +0.001 52 | -0.001 58 | +0.002 25 |
| 9 | -0.002 08 | +0.004 23 | -0.002 15 | +0.000 68 | 9 | -0.001 76 | +0.003 71 | -0.001 95 | +0.001 04 |
| 10 | -0.001 49 | +0.004 19 | -0.002 70 | -0.002 90 | 10 | -0.001 92 | +0.004 52 | -0.002 60 | -0.002 21 |
| 11 | +0.003 18 | +0.000 19 | -0.003 36 | -0.004 82 | 11 | +0.002 36 | +0.001 19 | -0.003 55 | -0.005 30 |

TABLE XVIII.—*Concluded.*

JUPITER; DIRECT ACTION; SPECIAL VALUES OF THE A-COEFFICIENTS FOR 6 SYSTEMS.

| System 4. | | | | | System 5. | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>i</i> | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> |
| 0 | +0.010 47 | -0.005 21 | -0.005 26 | -0.000 94 | 0 | +0.010 36 | -0.005 15 | -0.005 21 | +0.001 06 |
| 1 | +0.004 29 | +0.000 44 | -0.004 73 | +0.006 84 | 1 | +0.002 55 | +0.001 57 | -0.004 12 | +0.006 16 |
| 2 | -0.002 58 | +0.005 91 | -0.003 33 | +0.002 64 | 2 | -0.002 34 | +0.005 16 | -0.002 82 | +0.001 95 |
| 3 | -0.001 75 | +0.004 00 | -0.002 25 | -0.001 77 | 3 | -0.001 58 | +0.003 55 | -0.001 97 | -0.001 48 |
| 4 | +0.000 68 | +0.000 96 | -0.001 65 | -0.002 46 | 4 | +0.000 41 | +0.001 11 | -0.001 51 | -0.002 24 |
| 5 | +0.002 16 | -0.000 80 | -0.001 35 | -0.001 39 | 5 | +0.001 88 | -0.000 57 | -0.001 30 | -0.001 52 |
| 6 | +0.002 51 | -0.001 25 | -0.001 25 | +0.000 14 | 6 | +0.002 51 | -0.001 25 | -0.001 26 | -0.000 16 |
| 7 | +0.001 90 | -0.000 59 | -0.001 31 | +0.001 52 | 7 | +0.002 20 | -0.000 83 | -0.001 37 | +0.001 39 |
| 8 | +0.000 43 | +0.001 11 | -0.001 54 | +0.002 28 | 8 | +0.000 72 | +0.000 96 | -0.001 68 | +0.002 52 |
| 9 | -0.001 61 | +0.003 62 | -0.002 02 | +0.001 52 | 9 | -0.001 79 | +0.004 10 | -0.002 31 | +0.001 82 |
| 10 | -0.002 41 | +0.005 30 | -0.002 90 | -0.002 01 | 10 | -0.002 64 | +0.006 06 | -0.003 42 | -0.002 72 |
| 11 | +0.002 68 | +0.001 55 | -0.004 23 | -0.006 32 | 11 | +0.004 44 | +0.000 36 | -0.004 80 | -0.006 91 |

TABLE XIX.

JUPITER; DIRECT ACTION; DEVELOPMENT OF THE A-COEFFICIENTS.

| Arg. | 10 ⁶ <i>A</i> | | 10 ⁶ <i>B</i> | | 10 ⁶ <i>C</i> | | 10 ⁶ <i>D</i> | | |
|------|--------------------------|-------|--------------------------|-------|--------------------------|-------|--------------------------|------|-------|
| | LJ, <i>g</i> ' | cos | sin | cos | sin | cos | sin | cos | sin |
| 0 0 | | +1347 | 0 | +1237 | 0 | -2583 | 0 | - 1 | 0 |
| 0 1 | | - 4 | - 58 | - 1 | - 19 | + 4 | + 76 | - 18 | + 3 |
| 1-2 | | - 7 | - 77 | + 17 | + 86 | - 12 | - 10 | + 82 | - 13 |
| 1-1 | | +1112 | 0 | + 358 | 0 | -1470 | 0 | 0 | + 539 |
| 1 0 | | - 11 | -211 | - 16 | -184 | + 28 | +395 | 0 | + 2 |
| 1+1 | | - 3 | 0 | - 1 | + 2 | + 5 | 0 | 0 | + 1 |
| 2-3 | | - 3 | - 82 | + 8 | + 82 | - 4 | - 1 | + 83 | - 5 |
| 2-2 | | +3878 | + 2 | -3526 | - 5 | - 355 | + 2 | - 3 | +3699 |
| 2-1 | | - 7 | -165 | - 5 | - 53 | + 12 | +217 | + 53 | - 2 |
| 2 0 | | - 16 | + 2 | - 15 | + 3 | + 30 | - 5 | + 1 | - 11 |
| | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3-4 | | + 13 | - 40 | - 12 | + 40 | - 3 | 0 | + 42 | + 12 |
| 3-3 | | +1779 | + 1 | -1700 | - 3 | - 79 | + 1 | - 2 | +1737 |
| 3-2 | | - 28 | -672 | + 24 | +595 | + 5 | + 77 | +633 | - 25 |
| 3-1 | | - 18 | + 3 | - 6 | + 1 | + 24 | - 4 | 0 | - 6 |
| 4-5 | | + 10 | - 10 | - 8 | + 10 | 0 | + 1 | + 21 | + 9 |
| 4-4 | | + 587 | - 3 | - 570 | + 1 | - 18 | + 1 | + 2 | + 575 |
| 4-3 | | - 18 | -434 | + 16 | +412 | + 2 | + 22 | +423 | - 17 |
| 4-2 | | - 80 | + 7 | + 70 | - 6 | + 11 | 0 | - 6 | - 76 |
| 5-6 | | + 2 | + 16 | - 3 | - 14 | + 1 | - 1 | + 26 | + 6 |
| 5-5 | | + 176 | - 2 | - 172 | + 2 | - 3 | 0 | + 3 | + 154 |
| 5-4 | | - 8 | -185 | + 7 | +180 | 0 | + 5 | +184 | - 8 |
| 5-3 | | - 66 | + 6 | + 64 | - 6 | + 4 | - 1 | - 6 | - 67 |

D. ACTION OF SATURN AND MERCURY.

§ 40. The inequalities due to the direct action of Saturn are so minute that an approximate development will suffice. I have therefore used the development of Δ^{-3} and Δ^{-5} by spherical harmonics. We put a_1 for the mean distance of Saturn, L , as usual, for the difference of mean heliocentric longitudes of the planet and Earth ($L = s - g'$), and α for the ratio of the mean distances. With this notation the developments to α^4 are

$$\begin{aligned} \frac{a_1^3}{\Delta^3} &= 1 + \frac{9}{4}\alpha^2 + \frac{225}{64}\alpha^4 + \dots + (3 + \frac{45}{8}\alpha^2 + \dots)\alpha \cos L \\ &\quad + (\frac{15}{4} + \frac{105}{16}\alpha^2)\alpha^2 \cos 2L + \frac{35}{8}\alpha^3 \cos 3L + \frac{315}{64}\alpha^4 \cos 4L \\ \frac{a_1^5}{\Delta^5} &= 1 + \frac{25}{4}\alpha^2 + \frac{1225}{64}\alpha^4 + \dots + (5 + \frac{175}{8}\alpha^2 + \dots)\alpha \cos L \\ &\quad + (\frac{35}{4} + \frac{525}{16}\alpha^2 \dots)\alpha^2 \cos 2L + \frac{105}{8}\alpha^3 \cos 3L + \frac{1155}{64}\alpha^4 \cos 4L \end{aligned}$$

This development is valid when the eccentricities are taken account of, provided we use the true radii vectores and true longitudes instead of the mean ones. But this is unnecessary in the present case. For Saturn we have

$$\alpha = 0.1070$$

Reducing to numbers this gives

$$\begin{aligned} \frac{a_1^3}{\Delta^3} &= 1.0262 + 0.328 \cos L + 0.044 \cos 2L + 0.005 \cos 3L \dots \\ \frac{a_1^5}{\Delta^5} &= 1.0741 + 0.557 \cos L + 0.110 \cos 2L + .016 \cos 3L + \dots \end{aligned}$$

For the geocentric coördinates X, Y, Z , of Saturn we have

$$X = a' - a_1 \cos L = a_1(\alpha - \cos L) \quad Y = -a_1 \sin L \quad Z = 0$$

Then

$$2K = \frac{a'^3}{\Delta^5}(X^2 - Y^2) = \alpha^3 \frac{a_1^5}{\Delta^5}(\alpha^2 - 2\alpha \cos L + \cos 2L)$$

$$C_1 = a'^3 C = -\frac{\alpha^3}{3} \frac{a_1^3}{\Delta^3}$$

$$D_1 = a'^3 D = \alpha^3 \frac{a_1^5}{\Delta^5} (\frac{1}{2} \sin 2L - \alpha \sin L)$$

Reducing to numbers, and performing the necessary multiplications we find

$$10^3 K = +.0027 + .031 \cos L + .620 \cos 2L$$

$$10^3 C_1 = -.419 - .135 \cos L - .018 \cos 2L$$

$$10^3 D_1 = -.029 \sin L + .607 \sin 2L$$

Then, the principal terms are

$$\begin{aligned} 10^3 MK &= + .0013 + .015 \cos L + .307 \cos 2L \\ 10^3 MC_1 &= - .208 - .067 \cos L - .009 \cos 2L \\ 10^3 MD_1 &= \dots\dots\dots - .014 \sin L + .302 \sin 2L \end{aligned}$$

§ 41. The mass of Mercury is so minute that its action upon Venus, the only planet whose motion it can sensibly affect, has never been determined with certainty. There is every reason to believe that the uncertain determinations of the mass which have been made were too great by 2 or 3 times their entire amount. From Hill's estimate, based on the volume and probable density of the planet, it is very probable that the mass is less than $1 \div 10\,000\,000$ that of the Sun. From the results of § 30 it is inferred that its secular effect on the motion of the lunar elements is proportionally yet smaller than its mass.

The only periodic inequalities that could become sensible are those of comparatively long period. Their probable limiting values are considered in *Action*, p. 273, from which it appears that the largest inequality is that depending on the argument

$$l + \pi + 3M' + g'$$

and that the limiting value of the coefficient was estimated at $0''.1$. For another argument the limiting value was $0''.04$. These estimates rest on a mass double of what may now be considered the most probable value. For these reasons it was intended to leave the action of Mercury entirely out of consideration in the present investigation. But, for the sake of completeness, and to leave open as few questions as possible, it was at length decided to compute the action in the same way as that of Venus. Twelve systems and twelve indices were used. With 144 special values, it is easy to compute not only the secular, but the principal periodic terms. Among the results are the following constant terms and terms depending on the above argument, the form being

$$A = A_0 + A_c \cos(3M' + g') + A_s \sin(3M' + g')$$

| | | |
|------------------|------------------|------------------|
| $A_0 = + 0.867$ | $A_c = - .00059$ | $A_s = 0$ |
| $B_0 = - 0.381$ | $B_c = + .00035$ | $B_s = + .00008$ |
| $C_0 = - 0.486$ | $C_c = + .00026$ | $C_s = - .00006$ |
| $D_0 = + 0.0022$ | $D_c = + .0005$ | $D_s = - .0023$ |
| $K_0 = + 0.624$ | $K_c = - .00047$ | $K_s = - .00004$ |

§ 42. *K-coefficients.* From the preceding developments of *A*, *B*, *C*, and *D* for the four disturbing planets the coefficients $K = \frac{1}{2} (A - B)$ are formed, and *K*, *C*₁, and *D*₁ are multiplied by *M*.

This special set of coefficients, containing the factor *M*, are designated as *K*-coefficients. Their values are tabulated for Venus, Mars, and Jupiter as follows.

The values for Saturn are found at the end of § 40 preceding.

D. ACTION OF SATURN AND MERCURY.

§ 40. The inequalities due to the direct action of Saturn are so minute that an approximate development will suffice. I have therefore used the development of Δ^{-3} and Δ^{-5} by spherical harmonics. We put a_1 for the mean distance of Saturn, L , as usual, for the difference of mean heliocentric longitudes of the planet and Earth ($L = s - g'$), and α for the ratio of the mean distances. With this notation the developments to α^4 are

$$\begin{aligned} \frac{a_1^3}{\Delta^3} &= 1 + \frac{9}{4}\alpha^2 + \frac{225}{64}\alpha^4 + \dots + (3 + \frac{45}{8}\alpha^2 + \dots)\alpha \cos L \\ &\quad + (\frac{15}{4} + \frac{105}{16}\alpha^2)\alpha^2 \cos 2L + \frac{35}{8}\alpha^3 \cos 3L + \frac{315}{64}\alpha^4 \cos 4L \\ \frac{a_1^5}{\Delta^5} &= 1 + \frac{25}{4}\alpha^2 + \frac{1225}{64}\alpha^4 + \dots + (5 + \frac{175}{8}\alpha^2 + \dots)\alpha \cos L \\ &\quad + (\frac{35}{4} + \frac{525}{16}\alpha^2 \dots)\alpha^2 \cos 2L + \frac{105}{8}\alpha^3 \cos 3L + \frac{1155}{64}\alpha^4 \cos 4L \end{aligned}$$

This development is valid when the eccentricities are taken account of, provided we use the true radii vectores and true longitudes instead of the mean ones. But this is unnecessary in the present case. For Saturn we have

$$\alpha = 0.1070$$

Reducing to numbers this gives

$$\frac{a_1^3}{\Delta^3} = 1.0262 + 0.328 \cos L + 0.044 \cos 2L + 0.005 \cos 3L \dots$$

$$\frac{a_1^5}{\Delta^5} = 1.0741 + 0.557 \cos L + 0.110 \cos 2L + .016 \cos 3L + \dots$$

For the geocentric coördinates X, Y, Z , of Saturn we have

$$X = a' - a_1 \cos L = a_1(\alpha - \cos L) \quad Y = -a_1 \sin L \quad Z = 0$$

Then

$$2K = \frac{a'^3}{\Delta^3}(X^2 - Y^2) = \alpha^3 \frac{a_1^5}{\Delta^5}(\alpha^2 - 2\alpha \cos L + \cos 2L)$$

$$C_1 = a'^3 C = -\frac{\alpha^3}{3} \frac{a_1^3}{\Delta^3}$$

$$D_1 = a'^3 D = \alpha^3 \frac{a_1^5}{\Delta^5} (\frac{1}{2} \sin 2L - \alpha \sin L)$$

Reducing to numbers, and performing the necessary multiplications we find

$$10^3 K = +.0027 + .031 \cos L + .620 \cos 2L$$

$$10^3 C_1 = -.419 - .135 \cos L - .018 \cos 2L$$

$$10^3 D_1 = -.029 \sin L + .607 \sin 2L$$

Then, the principal terms are

$$\begin{aligned} 10^3MK &= + .0013 + .015 \cos L + .307 \cos 2L \\ 10^3MC_1 &= - .208 - .067 \cos L - .009 \cos 2L \\ 10^3MD_1 &= \dots \dots - .014 \sin L + .302 \sin 2L \end{aligned}$$

§ 41. The mass of Mercury is so minute that its action upon Venus, the only planet whose motion it can sensibly affect, has never been determined with certainty. There is every reason to believe that the uncertain determinations of the mass which have been made were too great by 2 or 3 times their entire amount. From Hill's estimate, based on the volume and probable density of the planet, it is very probable that the mass is less than $1 \div 10\,000\,000$ that of the Sun. From the results of § 30 it is inferred that its secular effect on the motion of the lunar elements is proportionally yet smaller than its mass.

The only periodic inequalities that could become sensible are those of comparatively long period. Their probable limiting values are considered in *Action*, p. 273, from which it appears that the largest inequality is that depending on the argument

$$l + \pi + 3M' + g'$$

and that the limiting value of the coefficient was estimated at $0''.1$. For another argument the limiting value was $0''.04$. These estimates rest on a mass double of what may now be considered the most probable value. For these reasons it was intended to leave the action of Mercury entirely out of consideration in the present investigation. But, for the sake of completeness, and to leave open as few questions as possible, it was at length decided to compute the action in the same way as that of Venus. Twelve systems and twelve indices were used. With 144 special values, it is easy to compute not only the secular, but the principal periodic terms. Among the results are the following constant terms and terms depending on the above argument, the form being

$$A = A_0 + A_c \cos(3M' + g') + A_s \sin(3M' + g')$$

| | | |
|------------------|------------------|------------------|
| $A_0 = + 0.867$ | $A_c = - .00059$ | $A_s = 0$ |
| $B_0 = - 0.381$ | $B_c = + .00035$ | $B_s = + .00008$ |
| $C_0 = - 0.486$ | $C_c = + .00026$ | $C_s = - .00006$ |
| $D_0 = + 0.0022$ | $D_c = + .0005$ | $D_s = - .0023$ |
| $K_0 = + 0.624$ | $K_c = - .00047$ | $K_s = - .00004$ |

§ 42. *K-coefficients.* From the preceding developments of *A*, *B*, *C*, and *D* for the four disturbing planets the coefficients $K = \frac{1}{2} (A - B)$ are formed, and *K*, *C*₁, and *D*₁ are multiplied by *M*.

This special set of coefficients, containing the factor *M*, are designated as *K*-coefficients. Their values are tabulated for Venus, Mars, and Jupiter as follows.

The values for Saturn are found at the end of § 40 preceding.

ACTION OF THE PLANETS ON THE MOON.

TABLE XX.

K-COEFFICIENTS FOR DIRECT ACTION OF VENUS.

| v, g' | $10^3 MK_c$ | $10^3 MK_s$ | $\frac{1}{2}10^3 MC_c$ | $\frac{1}{2}10^3 MC_s$ | $10^3 MD_c$ | $10^3 MD_s$ |
|---------|-------------|-------------|------------------------|------------------------|-------------|-------------|
| 0, 0 | + 5.903 | 0.00 | -3.406 | 0.000 | 0.000 | 0.000 |
| 0, 1 | + 0.44 | -0.11 | -0.30 | +0.07 | +0.03 | +0.33 |
| 0, 2 | + 0.13 | -0.14 | -0.09 | +0.10 | +0.05 | +0.06 |
| 1, -2 | + 0.71 | +0.15 | -0.36 | -0.08 | +0.08 | -0.52 |
| 1, -1 | +10.95 | 0.00 | -6.03 | 0.00 | -0.01 | -4.92 |
| 1, 0 | + 0.17 | -0.07 | -0.22 | +0.05 | 0.00 | +0.22 |
| 2, -4 | + 0.16 | +0.14 | -0.08 | -0.08 | +0.09 | -0.11 |
| 2, -3 | + 0.93 | +0.19 | -0.39 | -0.08 | +0.13 | -0.73 |
| 2, -2 | +10.75 | 0.00 | -4.99 | 0.00 | -0.01 | -7.09 |
| 2, -1 | + 0.02 | -0.04 | -0.16 | +0.03 | -0.01 | +0.22 |
| 3, -6 | + 0.02 | +0.03 | -0.01 | -0.01 | +0.02 | -0.01 |
| 3, -5 | + 0.170 | +0.147 | -0.078 | -0.075 | +0.11 | -0.13 |
| 3, -4 | + 1.08 | +0.22 | -0.38 | -0.08 | +0.17 | -0.91 |
| 3, -3 | +10.24 | 0.00 | -4.00 | 0.00 | -0.01 | -7.91 |
| 4, -6 | + 0.18 | +0.15 | -0.07 | -0.07 | +0.11 | -0.15 |
| 4, -5 | + 1.17 | +0.24 | -0.36 | -0.08 | +0.20 | -1.04 |
| 4, -4 | + 9.42 | 0.00 | -3.14 | 0.00 | -0.01 | -7.89 |
| 5, -8 | + 0.019 | +0.028 | -0.007 | -0.012 | +0.024 | -0.017 |
| 5, -7 | + 0.19 | +0.14 | -0.06 | -0.06 | +0.12 | -0.16 |
| 5, -6 | + 1.21 | +0.24 | -0.32 | -0.07 | +0.21 | -1.05 |
| 5, -5 | + 8.40 | 0.00 | -2.43 | 0.00 | -0.01 | -7.39 |
| 6, -7 | + 1.19 | +0.24 | -0.28 | -0.06 | +0.21 | -0.11 |
| 6, -6 | + 7.32 | 0.00 | -1.86 | 0.00 | 0.00 | -6.64 |

TABLE XXI.

K-COEFFICIENTS FOR DIRECT ACTION OF MARS.

| M, g' | $10^3 MK_c$ | $10^3 MK_s$ | $\frac{1}{2}10^3 MC_c$ | $\frac{1}{2}10^3 MC_s$ | $10^3 MD_c$ | $10^3 MD_s$ |
|---------|-------------|-------------|------------------------|------------------------|-------------|-------------|
| 0, 0 | + 0.0465 | 0.000 | -0.1006 | 0.000 | 0.000 | 0.000 |
| 0, 1 | - 0.020 | -0.024 | +0.028 | +0.029 | -0.008 | +0.010 |
| 1, -2 | - 0.012 | +0.014 | +0.017 | -0.018 | -0.008 | -0.012 |
| 1, -1 | + 0.110 | +0.001 | -0.169 | 0.000 | 0.000 | +0.054 |
| 1, 0 | - 0.025 | -0.029 | +0.042 | +0.045 | 0.000 | 0.000 |
| 2, -3 | - 0.002 | 0.000 | +0.009 | -0.010 | +0.006 | -0.002 |
| 2, -2 | + 0.194 | +0.002 | -0.129 | +0.001 | 0.000 | +0.165 |
| 2, -1 | - 0.035 | -0.039 | +0.049 | +0.053 | +0.013 | -0.014 |
| 2, 0 | 0.000 | +0.011 | +0.003 | -0.016 | +0.002 | -0.002 |
| 3, -3 | + 0.233 | +0.004 | -0.093 | +0.001 | -0.002 | +0.217 |
| 3, -2 | - 0.064 | -0.070 | +0.049 | +0.053 | +0.050 | -0.048 |
| 4, -4 | + 0.229 | +0.004 | -0.064 | +0.001 | -0.003 | +0.221 |
| 4, -3 | - 0.094 | -0.103 | +0.044 | +0.049 | +0.090 | -0.083 |
| 4, -2 | - 0.002 | +0.030 | +0.003 | -0.028 | -0.019 | -0.003 |
| 5, -4 | - 0.115 | -0.126 | +0.037 | +0.042 | +0.119 | -0.107 |
| 5, -3 | - 0.005 | +0.051 | +0.003 | -0.030 | -0.042 | -0.004 |
| 5, -2 | + 0.009 | -0.004 | -0.006 | +0.005 | +0.003 | +0.007 |
| 6, -5 | - 0.122 | -0.134 | +0.030 | +0.034 | +0.131 | -0.117 |
| 6, -4 | - 0.009 | +0.074 | +0.002 | -0.029 | -0.068 | -0.007 |
| 6, -3 | + 0.015 | -0.009 | -0.007 | +0.006 | +0.008 | +0.011 |

TABLE XXII.

K-COEFFICIENTS FOR DIRECT ACTION OF JUPITER.

| J, g' | $10^3 K_e$ | $10^3 K_s$ | $\frac{1}{2} 10^3 MC_e$ | $\frac{1}{2} 10^3 MC_s$ | $10^3 MD_e$ | $10^3 MD_s$ |
|---------|------------|------------|-------------------------|-------------------------|-------------|-------------|
| 0, 0 | + 0.091 | 0.000 | -2.135 | 0.000 | 0.000 | 0.000 |
| 0, 1 | - 0.002 | -0.032 | +0.003 | +0.063 | -0.030 | +0.005 |
| 1, -2 | - 0.020 | -0.135 | -0.010 | -0.008 | +0.135 | -0.021 |
| 1, -1 | + 0.623 | 0.000 | -1.215 | 0.000 | 0.000 | +0.593 |
| 1, 0 | + 0.004 | -0.022 | +0.023 | +0.326 | 0.000 | +0.003 |
| 1, +1 | - 0.002 | -0.001 | +0.004 | 0.000 | 0.000 | +0.002 |
| 2, -3 | - 0.009 | -0.135 | -0.003 | -0.001 | +0.137 | -0.008 |
| 2, -2 | + 6.119 | +0.006 | -0.293 | +0.001 | -0.005 | +6.114 |
| 2, -1 | - 0.001 | -0.093 | +0.010 | +0.179 | +0.087 | -0.003 |
| 2, 0 | - 0.001 | -0.001 | +0.025 | -0.004 | +0.001 | -0.018 |
| 3, -3 | + 2.875 | +0.003 | -0.065 | +0.001 | -0.003 | +2.875 |
| 3, -2 | - 0.043 | -1.048 | +0.004 | +0.064 | +1.046 | -0.041 |

CHAPTER V.

PLANETARY COEFFICIENTS FOR THE INDIRECT ACTION.

§ 43. Our next step is to form the coefficients $G, J,$ and $I,$ which are the planetary coefficients for the indirect action, and correspond to $K, \frac{1}{2}C,$ and $D.$ These we have found to be linear functions of the perturbations in the motion of the Earth around the Sun produced by the action of all the planets. From the way in which they are formed it will be seen that they should include all deviations in the motion of the Sun from the actual formulæ adopted for the expression of Ω as used in determining the action of the Sun itself. It would therefore be necessary, in strictness, to include the effect of any corrections that may be necessary to the elements of the Sun's motion employed by Delaunay. But as the eccentricity of the Earth's orbit enters as a symbolic quantity into the theories of both Delaunay and Brown, it will not be necessary to apply any correction on this account. The same remark applies to the position of the Earth's perihelion. But as the solar elements are assumed to be constant in the first integration it is necessary to take into account the effects of their secular variations, as well as of the periodic inequalities.

Moreover, in developing the action of the Sun upon the Moon for the first integration, it is assumed that the mean distance of the Earth's orbit is strictly connected with its mean motion by the fundamental relation

$$a^3 n^2 = m' + \mu$$

It is therefore necessary to include in $\delta\rho'$ the constant correction arising from the action of the planets.

We may conveniently classify the various terms of $\delta v'$ and $\delta\rho'$ which are to be used in the expressions (60) as follows:

1. The terms arising from the secular variation of the eccentricity of the Earth's orbit.
2. Constant and periodic terms independent of the mean longitude of the disturbing planet.
3. Periodic terms containing that mean longitude.

§ 44. *Secular terms arising from the variation of the eccentricity of the Earth's orbit.*

The action of the Sun upon the Moon being a function of the eccentricity of the Earth's orbit it follows that the indirect action will vary with that element. The variation may be taken account of by assigning to $\delta v'$ and $\delta\rho'$ the increments of the

Earth's polar coördinates due to the variation of the eccentricity. It is not necessary to take into account the variation of the solar perigee, because this element is retained in its general form in the final expressions of all the perturbations.

To find the required values of $\delta v'$ and $\delta \rho'$ we differentiate the expressions for v' and ρ' in terms of the eccentricity, thus obtaining

$$\begin{aligned} \frac{\partial v'}{\partial e'} &= (2 - \frac{3}{4}e'^2) \sin g' + (\frac{5}{2}e' - \frac{11}{6}e'^3) \sin 2g' + \frac{1}{4}e'^2 \sin 3g' + \frac{1}{24}e'^3 \sin 4g' \\ \frac{\partial \rho'}{\partial e'} &= \frac{1}{2}e' + \frac{1}{8}e'^3 - (1 - \frac{3}{8}e'^2) \cos g' - (\frac{3}{2}e' - \frac{11}{6}e'^3) \cos 2g' - \frac{1}{8}e'^2 \cos 3g' - \frac{7}{24}e'^3 \cos 4g' \end{aligned} \quad (84)$$

Putting $\Delta e'$ for the increment of e' due to secular variation, the values of $\delta v'$ and $\delta \rho'$ to quantities of the first order are found by multiplying these derivatives by $\Delta e'$. To determine what terms of higher order are necessary we remark that for an interval of 1000 years before or after 1900 we have

$$\Delta e' = \pm .000418 = \pm 86''.0$$

whence

$$(\Delta e')^2 = 0''.035$$

This quantity is so small that the powers of $\Delta e'$ above the first order may be dropped. But $\Delta e'$ will contain terms in T^2 which it will be well to include for the sake of approximation to rigor in the theory.

Substituting in the values of the differential coefficients just found the numerical value of e' for 1850,

$$e' = .0167711$$

we shall have

$$\begin{aligned} \frac{\partial v'}{\partial e'} &= 1.99979 \sin g' + .04192 \sin 2g' + .00091 \sin 3g' + .00002 \sin 4g' \\ \frac{\partial \rho'}{\partial e'} &= .00839 - .99968 \cos g' - .02515 \cos 2g' - .00060 \cos 3g' - .00001 \cos 4g' \end{aligned} \quad (85)$$

The value of $\Delta e'$ by which these expressions are to be multiplied is that used in the author's *Tables of the Sun*:

$$\Delta e' = -8''.595T - 0''.0260T^2$$

T being counted in centuries from 1850.

The corresponding portions of G , J , and I are found by substituting for $\delta v'$ and $\delta \rho'$ in the expressions (60) the quantities

$$\delta v' = \frac{\partial v'}{\partial e'} \Delta e' \quad \delta \rho' = \frac{\partial \rho'}{\partial e'} \Delta e'$$

If we suppose that G , J , and I are expressed in the form

$$G = G_0 + G_1 \Delta e'$$

with similar forms for J and I , we find by developing to e'^2

$$G_1 = + \frac{1}{4} e' - \left(\frac{9}{4} - \frac{5}{3} \frac{9}{2} e'^2 \right) \cos g' - \frac{5}{4} e' \cos 2g' - \frac{1}{3} \frac{9}{2} e'^2 \cos 3g'$$

$$J_1 = - \frac{3}{4} e' - \left(\frac{3}{4} + \frac{8}{3} \frac{1}{2} e'^2 \right) \cos g' - \frac{3}{4} e' \cos 2g' - \frac{1}{3} \frac{5}{2} e'^2 \cos 3g'$$

$$I_1 = (3 - \frac{3}{16} e'^2) \sin g' + \frac{5}{4} e' \sin 2g' + \frac{5}{16} \frac{3}{2} e'^2 \sin 3g'$$

The following numerical values have not been formed from these, but by multiplying the numerical values of the factors given in (60) and (85), which are derived from developments to e'^3 .

$$\begin{aligned} G_1 &= + .06238 - 2.24517 \cos g' - .21296 \cos 2g' - .01115 \cos 3g' \\ J_1 &= - .01257 - 0.75039 \cos g' - .03771 \cos 2g' - .00140 \cos 3g' \\ I_1 &= + 2.96280 \sin g' + .21366 \sin 2g' + .04342 \sin 3g' \end{aligned} \tag{86}$$

§ 45. *Terms independent of the mean longitude of the disturbing planet.* These terms arise from the terms of $\delta v'$ and $\delta \rho'$ which are either constants, or functions of g' alone. In the case of the longitude the eccentricity and perihelion of the Earth's orbit are so adjusted that both the constant terms and those dependent on Arg. g' shall vanish, leaving the only terms of $\delta v'$ to be considered those depending on Arg. $2g'$ etc. Both these terms themselves and the factors by which they are subsequently multiplied to form G , J , and I are so minute that the results are assumed to be insensible; we have, therefore, only to consider the terms of $\delta \rho'$ which remain after the adjustment of the eccentricity and perihelion just mentioned. These might be derived from the numbers in *Tables of the Sun*; but the author finds that the results have not been carried out with the precision desirable in the present problem. He has, therefore, computed these terms independently from theory, using the method of variation of elements, and carrying the results to terms of the second order in the eccentricities and mutual inclination. The general formulæ are as follows.* The accented quantities refer to the outer planet.

Action of an outer on an inner planet.

$$\delta \rho = m' \alpha \{ \rho_0 + \rho_1 \cos \Pi + (\rho_{0,e} + \rho_{1,e} \cos \Pi) \cos g + \rho_{1,s} \sin \Pi \sin g \}$$

where

$$\Pi = \pi - \pi'$$

$$\rho_0 = - \frac{1}{6} D A_0 + \frac{e^2}{48} (3D - 8D^2 - 2D^3) A_0 - \frac{e'^2}{24} (D^2 + D^3) A_0 \quad \rho_1 = \frac{ee'}{24} (-7D + 5D^2 + 2D^3) A_1$$

$$\rho_{0,e} = \frac{e}{8} (3D + 2D^2) A_0 \quad \rho_{1,e} = \frac{e'}{4} (1 - D^2) A_1 \quad \rho_{1,s} = - \frac{e'}{4} (1 - D^2) A_1$$

* The derivation has appeared in the *Astronomical Journal*, vol. xxv.

Action of an inner on an outer planet.

where $\delta\rho' = m\{\rho_0' + \rho_1' \cos \Pi' + (\rho_{0,c}' + \rho_{1,c}' \cos \Pi') \cos g' + \rho_{1,s}' \sin \Pi' \sin g'\}$

$$\Pi' = \pi' - \pi$$

$$\rho_0' = \frac{1}{6}(1 + D)A_0 - \frac{e'^2}{48}(9 + 13D + 2D^2 - 2D^3)A_0 + \frac{e^2}{24}(D + 2D^2 + D^3)A_0$$

$$\rho_1' = \frac{ee'}{24}(10 + 11D - D^2 - 2D^3)A_1 \quad \rho_{0,c}' = \frac{e'}{8}(-1 + D + 2D^2)A_0$$

$$\rho_{1,c}' = -\frac{e}{4}(2D + D^2)A_1 \quad \rho_{1,s}' = \frac{e}{4}(2D + D^2)A_1$$

The two actions are mutually interchanged by replacing D by $-(1 + D)$ in either. They were, however, developed independently in order that this relation might serve as a test of the accuracy of both.

The coefficients A_0 and A_1 are functions of the mutual inclination of the orbits ($\sigma = \sin \frac{1}{2}I$) and of the coefficients $b_i^{(i)}$ defined by the development

$$(1 - 2\alpha \cos L + \alpha^2)^s = \frac{1}{2} \sum b_i^{(i)} \cos iL$$

$$A_0 = b_{\frac{1}{2}}^{(0)} - \sigma\alpha^2 b_{\frac{1}{2}}^{(1)} \quad A_1 = b_{\frac{1}{2}}^{(1)} - \frac{1}{2}\sigma\alpha^2(b_{\frac{1}{2}}^{(0)} + b_{\frac{1}{2}}^{(2)})$$

D^n means the n th derivative as to $\log a$, or the symbolic value of $[a(\partial/\partial a)]^n$. If it be desired to use the usual successive derivatives as to a itself, we may do so by the substitutions

$$D = \alpha D_\alpha \quad D^2 = \alpha D_\alpha + \alpha^2 D_\alpha^2 \quad D^3 = \alpha D_\alpha + 3\alpha^2 D_\alpha^2 + \alpha^3 D_\alpha^3$$

From the numerical values of the coefficients A_0 , A_1 , and their D 's we have the following results:

| | | |
|-----------------|-------------------------------|------------------------------|
| Action of Venus | $10^9 \delta\rho' = + 1443.0$ | + $31 \cos g' - 17 \sin g'$ |
| Mars | - $30.$ | + $11 \cos g' - 8 \sin g'$ |
| Jupiter | - 1183.1 | + $90 \cos g' + 50 \sin g'$ |
| Saturn | - 55.4 | |
| Uranus | - 1.0 | |
| Total | + 173.5 | + $132 \cos g' + 25 \sin g'$ |

Additional to these we have, for Mercury, with mass = 10^{-7}

$$10^9 \delta\rho' = + 38.0 - 7 \cos g' + 3 \sin g'$$

which I treat separately.

From these (60) gives the following coefficients for $G, J,$ and $I,$ these quantities being expressed in the form

$$G = G_0 + G_c \cos g' + G_s \sin g'$$

| Action of | $10^9 G_0$ | $10^9 G_c$ | $10^9 G_s$ | $10^9 J_0$ | $10^9 J_c$ | $10^9 J_s$ | $10^9 I_0$ | $10^9 I_c$ | $10^9 I_s$ |
|-----------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Venus | +3246.8 | +233.3 | - 38.2 | +1083.3 | + 77.8 | -12.8 | +1.3 | | -217.7 |
| Mars | - 66.8 | + 21.4 | - 18.0 | - 22.3 | + 7.2 | - 6.0 | + .6 | | + 4.5 |
| Jupiter | -2655.0 | + 68.8 | +112.3 | - 886.0 | + 22.8 | +37.5 | -3.7 | -.1 | +178.2 |
| Saturn | - 124.6 | - 6.3 | 0 | - 41.6 | - 2.1 | 0 | 0 | | + 8.4 |
| Uranus | - 2.2 | - .1 | 0 | - .8 | 0 | 0 | 0 | | + .2 |
| Total | + 397.6 | +316.8 | + 56.1 | + 132.7 | +105.5 | +18.7 | -1.9 | -.1 | - 26.6 |
| Mercury | 85.1 | - 11.4 | + 6.7 | + 28.4 | - 3.9 | + 2.2 | -0.2 | 0 | - 5.7 |

(87)

The totals here given are not formed by addition, but by an independent computation of the entire amount. Hence small discrepancies between the totals and the sums.

§ 46. *Periodic perturbations of the point G, containing the mean longitude of the disturbed planet.*

These are taken from *Astronomical Papers*, Vol. III, Part V, where they are found:

- For Venus, on pp. 486-488
- For Mars, " " 527-530
- For Jupiter, " " 550-551

The perturbations by Venus are diminished by the factor .015 for reduction to the adopted value of the mass.

The expressions thus found are shown in tabular form below. In the original the constituents of the arguments were the mean anomalies alone, but, in the present work, the longitudes of the disturbing planets are reckoned from the Earth's perihelion. In order that the arguments for the direct and indirect inequalities may coincide, these perturbations have been transformed so that the planet's mean longitude shall be reckoned from the Earth's perihelion. The following are the numbers used:

| | | |
|---------|-----------------------|----------------|
| | | $\pi_4 - \pi'$ |
| Earth | $\pi = 100^\circ 21'$ | $0^\circ 0'$ |
| Venus | 129 27 | 29 6 |
| Mars | 333 18 | 232 57 |
| Jupiter | 11 56 | 271 35 |

Then, if any pair of terms in $\delta v'$ or $\delta \rho'$ be represented by

$$v_c \cos (ig_4 + i'g') + v_s \sin (ig_4 + i'g')$$

we have to compute

$$b_c = v_c \cos i(\pi_4 - \pi') - v_s \sin i(\pi_4 - \pi')$$

$$b_s = v_c \sin i(\pi_4 - \pi') + v_s \cos i(\pi_4 - \pi')$$

to transform them into

$$b_c \cos(il_4 + i'g') + b_s \sin(il_4 + i'g')$$

l_4 being the mean longitude of the planet from π' , designated by v, m, j, and s in the cases of the individual planets.

The original and transformed values of $\delta v'$ and $\delta \rho'$ are shown in Tables XXIII to XXVI.

The subsequent steps are shown in Tables XXVII-XXXIV in the following order:

The values of $G, J,$ and I given in Tables XXVII-XXX are formed from the expressions of $\delta v'$ and $\delta \rho'$ in terms of g_4 by the formulæ (60). These are then subjected to the transformation of §46 and multiplied by the constant coefficient $10^3 m^2 = 5.595$. The factor 10^3 is introduced in order to have the most convenient unit in subsequent computation. As a check upon the work the values of $J, G,$ and I were also computed using the transformed expressions for $\delta v'$ and $\delta \rho'$, and the results compared with the others. It has not been deemed necessary to set forth the steps of this simple duplicate computation.

TABLE XXIII.

ACTION OF VENUS ON THE EARTH.

| Arg. $g_4 \ g'$ | $\delta v'$ | | $\delta \rho'$ | | Arg. V, g' | $\delta v'$ | | $\delta \rho'$ | |
|--------------------|-------------|--------|----------------|-----------|-----------------|-------------|--------|----------------|-----------|
| | cos | sin | cos | sin | | cos | sin | cos | sin |
| -1, 0 | +0.03 | -0.01 | -0.041 | -0.018 | -1, 0 | 0.00 | -0.07 | -0.045 | +0.004 |
| -1, 1 | +2.35 | -4.23 | -0.980 | -0.544 | -1, 1 | -0.01 | -4.84 | -1.121 | +0.001 |
| -1, 2 | -0.06 | -0.03 | +0.032 | -0.006 | -1, 2 | -0.06 | 0.00 | +0.025 | -0.021 |
| -2, 1 | -0.10 | +0.06 | +0.041 | +0.065 | -2, 1 | 0.00 | +0.11 | +0.077 | -0.001 |
| -2, 1 | -4.70 | +2.90 | +1.709 | +2.765 | -2, 2 | -0.02 | +5.52 | +3.251 | +0.004 |
| -2, 3 | +1.80 | -1.74 | -0.282 | -0.300 | -2, 3 | -0.53 | -2.45 | -0.404 | +0.082 |
| -2, 4 | +0.03 | -0.03 | +0.018 | +0.016 | -2, 4 | -0.01 | -0.05 | +0.023 | -0.007 |
| -3, 3 | -0.67 | +0.03 | +0.020 | +0.496 | -3, 3 | 0.00 | +0.67 | +0.497 | +0.003 |
| -3, 4 | +1.51 | -0.40 | -0.181 | -0.689 | -3, 4 | -0.33 | -1.53 | -0.697 | +0.149 |
| -3, 5 | +0.76 | -0.68 | +0.059 | +0.069 | -3, 5 | -0.64 | -0.79 | +0.072 | -0.056 |
| -3, 6 | +0.01 | -0.01 | +0.006 | +0.006 | -3, 6 | -0.01 | -0.01 | +0.006 | -0.006 |
| -4, 4 | -0.19 | -0.09 | -0.079 | +0.160 | -4, 4 | 0.00 | +0.21 | +0.178 | 0.000 |
| -4, 5 | -0.14 | -0.04 | -0.024 | +0.089 | -4, 5 | +0.02 | +0.15 | +0.091 | -0.018 |
| -4, 6 | +0.15 | -0.04 | -0.012 | -0.047 | -4, 6 | -0.11 | -0.11 | -0.034 | +0.030 |
| -5, 6 | -0.03 | -0.02 | -0.018 | +0.020 | -5, 6 | +0.01 | +0.04 | +0.026 | -0.006 |
| -5, 7 | -0.12 | -0.03 | -0.018 | +0.065 | -5, 7 | +0.08 | +0.09 | +0.052 | -0.044 |
| -5, 8 | +0.154 | -0.001 | 0.000 | -0.013 | -5, 8 | -0.128 | -0.086 | -0.007 | +0.011 |
| -8, 11 | 0.000 | -0.002 | -0.001 | 0.000 | -8, 11 | +0.002 | +0.001 | +0.001 | -0.001 |
| -8, 12 | -0.008 | -0.041 | -0.020 5 | +0.003 9 | -8, 12 | +0.038 | +0.019 | +0.009 3 | -0.018 7 |
| -8, 13 | +1.268 | +1.416 | +0.004 23 | -0.003 66 | -8, 13 | -1.895 | +0.153 | +0.000 36 | +0.005 58 |
| -8, 14 | +0.021 | +0.024 | +0.010 6 | +0.004 3 | -8, 14 | -0.032 | +0.002 | -0.009 8 | +0.005 8 |

TABLE XXIV.
ACTION OF MARS ON THE EARTH.

| Arg. | | $\delta v'$ | | $\delta \rho'$ | | Arg. | | $\delta v'$ | | $\delta \rho'$ | |
|-------|------|-------------|--------|----------------|--------|---------|--------|-------------|--------|----------------|--|
| g_4 | g' | cos | sin | cos | sin | M, g' | cos | sin | cos | sin | |
| 1, | -1 | " | " | " | " | 1, | " | " | " | " | |
| 1, | 0 | -0.216 | -0.167 | -0.043 | +0.056 | 1, | -0.003 | +0.273 | +0.071 | 0.000 | |
| 2, | -3 | -0.008 | -0.047 | +0.013 | -0.003 | 1, | -0.033 | +0.034 | -0.010 | -0.008 | |
| 2, | -2 | +0.040 | -0.010 | -0.006 | -0.024 | 2, | -0.001 | +0.041 | +0.025 | +0.001 | |
| 2, | -1 | +1.963 | -0.567 | -0.272 | -0.937 | 2, | +0.007 | +2.043 | +0.977 | -0.005 | |
| 2, | 0 | -1.659 | -0.617 | +0.030 | -0.065 | 2, | +1.048 | -1.427 | +0.054 | +0.047 | |
| 3, | -3 | -0.024 | +0.015 | -0.008 | -0.012 | 2, | -0.007 | -0.027 | +0.014 | -0.005 | |
| 3, | -2 | +0.053 | -0.118 | -0.073 | -0.032 | 3, | +0.006 | -0.129 | -0.080 | -0.004 | |
| 3, | -1 | +0.396 | -0.153 | -0.037 | -0.096 | 3, | +0.314 | -0.286 | -0.070 | -0.077 | |
| 4, | -4 | +0.001 | +0.032 | +0.022 | -0.008 | 4, | +0.008 | -0.033 | -0.023 | -0.005 | |
| 4, | -3 | -0.131 | +0.483 | +0.219 | +0.059 | 4, | +0.366 | -0.342 | -0.155 | -0.165 | |
| 4, | -2 | +0.526 | -0.256 | +0.021 | +0.045 | 4, | -0.582 | -0.059 | +0.006 | -0.049 | |
| 5, | -4 | +0.049 | +0.069 | +0.041 | -0.029 | 5, | -0.064 | +0.055 | +0.033 | +0.038 | |
| 5, | -3 | -0.038 | +0.200 | +0.041 | +0.008 | 5, | -0.202 | -0.020 | -0.004 | +0.042 | |
| 6, | -5 | -0.020 | -0.002 | -0.001 | +0.014 | 6, | -0.016 | +0.012 | +0.008 | +0.011 | |
| 6, | -4 | -0.104 | -0.113 | -0.048 | +0.045 | 6, | -0.153 | -0.014 | -0.006 | +0.065 | |
| 6, | -3 | -0.011 | +0.100 | -0.013 | -0.002 | 6, | +0.059 | +0.081 | -0.011 | +0.008 | |
| 15, | -9 | +0.018 | -0.023 | -0.008 | -0.007 | 15, | -0.027 | -0.011 | -0.005 | +0.010 | |
| 15, | -8 | +0.201 | -0.030 | 0.000 | -0.003 | 15, | -0.083 | -0.184 | -0.003 | +0.001 | |

TABLE XXV.
ACTION OF JUPITER ON THE EARTH.

| Arg. | | $\delta v'$ | | $\delta \rho'$ | | Arg. | | $\delta v'$ | | $\delta \rho'$ | |
|-------|------|-------------|--------|----------------|--------|---------|--------|-------------|--------|----------------|--|
| g_4 | g' | cos | sin | cos | sin | J, g' | cos | sin | cos | sin | |
| 1, | -3 | " | " | " | " | 1, | " | " | " | " | |
| 1, | -2 | -0.003 | -0.001 | -0.001 | +0.002 | 1, | -0.001 | +0.003 | +0.002 | +0.001 | |
| 1, | -1 | -0.155 | -0.052 | -0.037 | +0.092 | 1, | -0.056 | +0.154 | +0.091 | +0.040 | |
| 1, | 0 | -7.208 | +0.059 | +0.026 | +3.356 | 1, | -0.140 | +7.207 | +3.356 | +0.067 | |
| 1, | +1 | -0.307 | -2.582 | +0.108 | -0.042 | 1, | -2.589 | +0.236 | -0.039 | -0.109 | |
| 2, | -3 | +0.008 | -0.073 | +0.037 | +0.004 | 1, | -0.073 | -0.010 | +0.005 | -0.037 | |
| 2, | -2 | +0.011 | +0.068 | +0.049 | -0.008 | 2, | -0.008 | -0.069 | -0.049 | +0.005 | |
| 2, | -1 | +0.136 | +2.728 | +1.910 | -0.097 | 2, | +0.014 | -2.731 | -1.912 | -0.008 | |
| 2, | 0 | -0.537 | +1.518 | +0.654 | +0.231 | 2, | +0.619 | -1.486 | -0.640 | -0.267 | |
| 3, | -4 | -0.022 | -0.070 | 0.000 | -0.004 | 2, | +0.018 | +0.071 | 0.000 | +0.004 | |
| 3, | -3 | -0.005 | +0.002 | +0.001 | +0.004 | 3, | -0.002 | -0.005 | -0.004 | +0.001 | |
| 3, | -2 | -0.162 | +0.027 | +0.021 | +0.132 | 3, | -0.014 | -0.164 | -0.134 | +0.010 | |
| 3, | -1 | +0.071 | +0.551 | +0.378 | -0.049 | 3, | -0.555 | +0.025 | +0.018 | +0.381 | |
| 3, | 0 | -0.031 | +0.208 | +0.082 | +0.012 | 3, | -0.205 | -0.048 | -0.019 | +0.081 | |

TABLE XXVI.

ACTION OF SATURN ON THE EARTH.

| Arg. | | $\delta v'$ | | $10^9 \delta \rho'$ | | Arg. | | $\delta v'$ | | $\delta \rho'$ | |
|-------|------|-------------|--------|---------------------|------|------|------|-------------|--------|----------------|--------|
| g_4 | g' | cos | sin | cos | sin | $s,$ | g' | cos | sin | cos | sin |
| 1, | -1 | " | " | +972 | +182 | 1, | -1 | " | " | +0.204 | +0.001 |
| 1, | 0 | -0.077 | +0.412 | +18 | -2 | 1, | 0 | -0.003 | +0.419 | +0.004 | -0.001 |
| 2, | -2 | -0.003 | -0.320 | -350 | -132 | 2, | -2 | -0.060 | -0.314 | -0.077 | 0.000 |
| 2, | -1 | +0.038 | -0.101 | -236 | -101 | 2, | -1 | -0.001 | -0.108 | -0.053 | -0.002 |
| | | +0.045 | -0.103 | | | | | +0.006 | -0.113 | | |

TABLE XXVII.

PLANETARY COEFFICIENTS FOR THE INDIRECT ACTION OF VENUS.

| Arg. | | G | | J | | I | |
|-------|------|---------|---------|-----------|-----------|--------|--------|
| g_4 | g' | sin | cos | sin | cos | sin | cos |
| -1, | 0 | " | " | " | " | " | " |
| -1, | 1 | -0.190 | -0.359 | -0.024 | -0.049 | -0.33 | +0.175 |
| -1, | 2 | -1.220 | -2.203 | -0.408 | -0.735 | -6.34 | +3.52 |
| -2, | 1 | +0.074 | +0.229 | -0.014 | +0.005 | -0.125 | -0.04 |
| -2, | 2 | +0.533 | +0.330 | +0.101 | +0.062 | +0.32 | -0.53 |
| -2, | 3 | +6.113 | +3.737 | +2.069 | +1.278 | +4.26 | -6.96 |
| -2, | 4 | -0.755 | -0.683 | -0.173 | -0.180 | -2.63 | +2.73 |
| -3, | 3 | +0.108 | +0.110 | +0.007 | +0.009 | -0.10 | +0.09 |
| -3, | 4 | +1.001 | +0.014 | +0.359 | +0.012 | +0.016 | -0.895 |
| -3, | 5 | -1.590 | -0.439 | -0.507 | -0.133 | -0.62 | +2.30 |
| -3, | 6 | +0.191 | +0.143 | +0.039 | +0.041 | -1.02 | +1.145 |
| -4, | 4 | +0.056 | +0.051 | +0.005 | +0.005 | -0.045 | +0.05 |
| -4, | 5 | +0.372 | -0.181 | +0.122 | -0.059 | -0.13 | -0.30 |
| -4, | 6 | +0.190 | -0.057 | +0.069 | -0.019 | -0.06 | -0.20 |
| -5, | 6 | -0.099 | -0.026 | -0.030 | -0.009 | -0.06 | +0.23 |
| -5, | 7 | +0.061 | -0.042 | +0.011 | -0.013 | -0.03 | -0.055 |
| -5, | 8 | +0.136 | -0.040 | +0.049 | -0.013 | -0.04 | -0.17 |
| -8, | 12 | -0.031 | 0.000 | -0.009 | 0.000 | 0.000 | +0.231 |
| -8, | 13 | +0.0550 | +0.025 | +0.002 90 | -0.015 | -0.007 | +0.036 |
| -8, | 14 | -0.0093 | +0.0122 | -0.002 60 | +0.002 98 | +2.126 | +1.903 |
| | | +0.073 | -0.047 | +0.003 | +0.008 | +0.093 | +0.079 |

TABLE XXVIII.

PLANETARY COEFFICIENT FOR THE INDIRECT ACTION OF MARS.

| Arg. | <i>G</i> | | <i>J</i> | | <i>I</i> | |
|----------------------------------|----------|--------|----------|--------|----------|--------|
| <i>g</i> ₄ <i>g</i> ' | sin | cos | sin | cos | sin | cos |
| 1, -1 | +0.126 | -0.098 | +0.042 | -0.033 | -0.251 | -0.324 |
| 1, 0 | +0.015 | +0.035 | -0.001 | +0.009 | -0.073 | -0.016 |
| 2, -3 | -0.209 | -0.057 | -0.036 | -0.009 | -0.058 | +0.208 |
| 2, -2 | -2.026 | -0.641 | -0.704 | -0.203 | -0.871 | +2.884 |
| 2, -1 | -0.100 | +0.082 | -0.067 | +0.017 | -0.924 | -2.485 |
| 2, 0 | -0.113 | +0.015 | -0.010 | -0.005 | -0.003 | -0.010 |
| 3, -3 | -0.097 | -0.174 | -0.026 | -0.056 | -0.186 | +0.101 |
| 3, -2 | -0.215 | -0.081 | -0.072 | -0.029 | -0.227 | +0.594 |
| 4, -4 | -0.009 | +0.085 | -0.005 | +0.020 | +0.083 | +0.008 |
| 4, -3 | +0.111 | +0.480 | +0.045 | +0.164 | +0.714 | -0.180 |
| 4, -2 | +0.097 | +0.035 | +0.035 | +0.020 | -0.383 | +0.788 |
| 5, -4 | -0.063 | +0.104 | -0.022 | +0.032 | +0.114 | +0.071 |
| 5, -3 | +0.018 | +0.091 | +0.006 | +0.032 | +0.299 | -0.057 |
| 6, -5 | +0.039 | -0.011 | +0.012 | -0.002 | -0.011 | -0.037 |
| 6, -4 | +0.102 | -0.104 | +0.034 | -0.036 | -0.166 | -0.156 |
| 6, -3 | -0.006 | -0.026 | -0.001 | -0.011 | +0.150 | -0.017 |
| 15, -9 | -0.026 | -0.020 | -0.005 | -0.006 | -0.036 | +0.035 |
| 15, -8 | -0.006 | +0.001 | -0.003 | 0.000 | -0.046 | +0.301 |

TABLE XXIX.

PLANETARY COEFFICIENTS FOR THE INDIRECT ACTION OF JUPITER.

| Arg. | <i>G</i> | | <i>J</i> | | <i>I</i> | |
|----------------------------------|----------|--------|----------|--------|----------|--------|
| <i>g</i> ₄ <i>g</i> ' | cos | sin | cos | sin | cos | sin |
| 1, -3 | -0.007 | +0.039 | -0.002 | +0.006 | -0.039 | -0.006 |
| 1, -2 | -0.084 | +0.759 | -0.028 | +0.132 | -0.757 | -0.079 |
| 1, -1 | -0.064 | +7.554 | +0.020 | +2.518 | -10.813 | 0.000 |
| 1, 0 | +0.238 | -0.266 | +0.082 | +0.032 | -0.479 | -3.870 |
| 1, +1 | +0.218 | -0.012 | +0.029 | +0.004 | -0.007 | -0.214 |
| 2, -3 | +0.360 | -0.030 | +0.073 | -0.008 | +0.026 | +0.352 |
| 2, -2 | +4.407 | -0.177 | +1.447 | -0.069 | +0.167 | +4.194 |
| 2, -1 | +1.437 | +0.522 | +0.527 | +0.171 | -0.808 | +2.231 |
| 2, 0 | -0.039 | -0.023 | +0.013 | +0.001 | -0.036 | -0.097 |
| 3, -4 | +0.006 | +0.024 | +0.001 | +0.005 | -0.023 | +0.008 |
| 3, -3 | +0.096 | +0.290 | +0.023 | +0.098 | -0.236 | +0.090 |
| 3, -2 | +0.865 | -0.109 | +0.286 | -0.035 | +0.109 | +0.839 |
| 3, -1 | +0.177 | +0.028 | +0.069 | +0.008 | -0.047 | +0.304 |

TABLE XXX.

PLANETARY COEFFICIENTS FOR THE INDIRECT ACTION OF SATURN.

| Arg. | <i>G</i> | | <i>J</i> | | <i>I</i> | |
|-----------------------------|----------|--------|----------|--------|----------|--------|
| <i>i, j</i> <i>S, g'</i> | cos | sin | cos | sin | cos | sin |
| 1, -1 | +0.443 | +0.005 | +0.153 | +0.001 | -0.006 | +0.616 |
| 1, 0 | -0.001 | -0.002 | +0.007 | -0.001 | -0.090 | -0.471 |
| 2, -2 | -0.182 | 0.000 | -0.059 | 0.000 | +0.001 | -0.171 |
| 2, -1 | -0.118 | -0.004 | -0.041 | -0.002 | +0.009 | -0.167 |

TABLE XXXI.

G-COEFFICIENTS FOR VENUS.

| Arg. | $10^3 m^2 G$ | | $10^3 m^2 J$ | | $10^3 m^2 I$ | |
|--------------|--------------|---------|--------------|-----------|--------------|---------|
| <i>V, g'</i> | cos | sin | cos | sin | cos | sin |
| -1, 0 | - 2.272 | +0.048 | - 0.304 | +0.016 | - 0.042 | - 2.089 |
| -1, 1 | -14.09 | +0.031 | - 4.703 | +0.005 | - 0.043 | -40.572 |
| -1, 2 | + 1.320 | -0.261 | - 0.014 | -0.082 | - 0.530 | - 0.502 |
| -2, 1 | + 3.508 | +0.002 | + 0.663 | +0.003 | - 0.071 | + 3.510 |
| -2, 2 | +40.100 | +0.253 | +13.764 | +0.121 | - 0.263 | +45.655 |
| -2, 3 | - 5.607 | +1.024 | - 1.354 | +0.346 | - 4.457 | -20.735 |
| -2, 4 | + 0.838 | -0.205 | + 0.060 | -0.022 | - 0.209 | - 0.723 |
| -3, 3 | + 5.602 | +1.186 | + 2.010 | +0.028 | - 0.146 | + 5.006 |
| -3, 4 | - 9.004 | +2.036 | - 2.869 | +0.609 | - 2.855 | -13.017 |
| -3, 5 | + 1.106 | -0.749 | + 0.229 | -0.219 | - 5.400 | - 6.668 |
| -3, 6 | + 0.326 | -0.270 | + 0.029 | -0.027 | - 0.239 | - 0.292 |
| -4, 4 | + 2.314 | -0.018 | + 0.759 | -0.008 | + 0.095 | + 1.827 |
| -4, 5 | + 1.094 | -0.180 | + 0.393 | -0.077 | + 0.197 | + 1.152 |
| -4, 6 | - 0.431 | +0.378 | - 0.128 | +0.121 | - 0.873 | - 1.003 |
| -5, 6 | + 0.389 | -0.148 | + 0.095 | -0.010 | + 0.159 | + 0.312 |
| -5, 7 | + 0.616 | -0.500 | + 0.215 | -0.185 | + 0.657 | + 0.723 |
| -5, 8 | - 0.098 | +0.143 | - 0.029 | +0.042 | - 1.065 | - 0.732 |
| -8, 11 | + 0.016 | -0.011 | + 0.005 | -0.006 | - 0.788 | + 1.039 |
| -8, 12 | + 0.1611 | +0.2994 | + 0.039 | -0.077 7 | - 0.091 | + 0.184 |
| -8, 13 | + 0.0045 | +0.0661 | + 0.001 45 | +0.022 05 | -15.912 | + 1.289 |
| -8, 14 | - 0.166 | -0.4588 | - 0.040 | +0.024 6 | - 0.681 | + 0.037 |

TABLE XXXII.
G-COEFFICIENTS FOR MARS.

| Arg. | $10^3 m^2 G$ | | $10^3 m^2 J$ | | $10^3 m^2 I$ | |
|---------|--------------|---------|--------------|---------|--------------|----------|
| M, g' | cos | sin | cos | sin | cos | sin |
| 1, -1 | + 0.893 | + 0.012 | + 0.300 | + 0.006 | - 0.065 | + 2.293 |
| 1, 0 | - 0.185 | - 0.105 | - 0.035 | - 0.036 | - 0.272 | + 0.318 |
| 2, -3 | + 1.211 | + 0.013 | + 0.207 | + 0.007 | - 0.006 | + 1.208 |
| 2, -2 | + 12.777 | - 0.089 | + 4.100 | - 0.014 | + 0.073 | + 17.531 |
| 2, -1 | + 0.413 | + 0.595 | + 0.335 | + 0.194 | + 1.161 | + 14.821 |
| 2, 0 | - 0.309 | 0.000 | + 0.062 | - 0.012 | - 0.019 | + 0.129 |
| 3, -3 | - 1.205 | - 0.155 | - 0.344 | - 0.022 | + 0.151 | - 1.175 |
| 3, -2 | - 0.857 | - 0.958 | - 0.296 | - 0.318 | + 2.641 | - 2.384 |
| 4, -4 | - 0.431 | - 0.208 | - 0.109 | - 0.035 | + 0.207 | - 0.418 |
| 4, -3 | - 1.956 | - 1.943 | - 0.638 | - 0.695 | + 2.961 | - 2.864 |
| 4, -2 | + 0.119 | - 0.565 | + 0.009 | - 0.224 | - 4.877 | - 0.502 |
| 5, -4 | + 0.404 | + 0.548 | + 0.139 | + 0.167 | - 0.600 | + 0.452 |
| 5, -3 | - 0.054 | + 0.516 | - 0.018 | + 0.181 | - 1.695 | - 0.166 |
| 6, -4 | - 0.047 | + 0.815 | - 0.021 | + 0.276 | - 1.271 | - 0.100 |
| 6, -3 | - 0.130 | + 0.073 | - 0.050 | + 0.038 | + 0.495 | + 0.685 |
| 15, -9 | - 0.109 | + 0.147 | - 0.018 | + 0.041 | - 0.246 | - 0.135 |
| 15, -8 | - 0.035 | + 0.003 | - 0.016 | + 0.005 | - 0.704 | - 1.551 |

TABLE XXXIII.
G-COEFFICIENTS FOR JUPITER.

| Arg. | $10^3 m^2 G$ | | $10^3 m^2 J$ | | $10^3 m^2 I$ | |
|---------|--------------|---------|--------------|---------|--------------|----------|
| J, g' | cos | sin | cos | sin | cos | sin |
| 1, -3 | + 0.218 | + 0.039 | + 0.022 | + 0.011 | - 0.039 | + 0.217 |
| 1, -2 | + 4.240 | + 0.594 | + 0.738 | + 0.173 | - 0.553 | + 4.241 |
| 1, -1 | + 42.237 | + 1.534 | + 14.088 | + 0.274 | - 1.672 | + 60.471 |
| 1, 0 | - 1.459 | - 1.376 | + 0.196 | - 0.458 | - 21.709 | + 2.097 |
| 1, +1 | - 0.040 | - 1.225 | + 0.017 | - 0.168 | - 1.203 | + 0.006 |
| 2, -3 | - 2.012 | + 0.050 | - 0.408 | + 0.022 | - 0.061 | - 1.991 |
| 2, -2 | - 24.668 | - 0.358 | - 8.096 | - 0.061 | + 0.363 | - 23.488 |
| 2, -1 | - 7.872 | - 3.363 | - 2.887 | - 1.119 | + 5.192 | - 12.225 |
| 2, 0 | + 0.218 | + 0.140 | - 0.067 | - 0.011 | + 0.173 | + 0.542 |
| 3, -4 | - 0.140 | + 0.017 | - 0.034 | + 0.006 | - 0.017 | - 0.129 |
| 3, -3 | - 1.677 | + 0.403 | - 0.559 | + 0.078 | - 0.397 | - 1.365 |
| 3, -1 | + 0.212 | + 4.874 | + 0.061 | + 1.611 | - 4.733 | + 0.212 |
| 3, -1 | - 0.240 | + 0.984 | - 0.078 | + 0.380 | - 1.672 | - 0.402 |

TABLE XXXIV.
G-COEFFICIENTS FOR SATURN.

| Arg. | $10^3 m^2 G$ | | $10^3 m^2 J$ | | $10^3 m^2 I$ | |
|---------|--------------|--------|--------------|--------|--------------|--------|
| S, g' | cos | sin | cos | sin | cos | sin |
| 1, -1 | + 2.48 | + 0.03 | + 0.86 | + 0.01 | - 0.03 | + 3.45 |
| 1, 0 | + 0.01 | - 0.01 | + 0.03 | + 0.01 | - 0.50 | + 2.64 |
| 2, -2 | - 1.02 | 0.00 | - 0.33 | 0.00 | 0.00 | - 0.96 |
| 2, -1 | - 0.66 | - 0.02 | - 0.23 | - 0.01 | + 0.05 | - 0.94 |

PART III.

FUNCTIONS OF THE COÖRDINATES
OF THE MOON.

CHAPTER VI.

FORMATION OF THE LUNAR COEFFICIENTS.

§ 47. In attacking the problem before us it has been assumed that we have expressions of the Moon's coördinates relative to the centre of the Earth as functions of the six arbitrary constants introduced through integrating the differential equations in these coördinates. Moreover, the constants in question enter the expressions for the disturbing function R only through these coördinates. It follows from the general expression of R that if c represents any one of the six lunar elements, the partial derivatives of the disturbing function may be derived from the form

$$\frac{\partial R_2}{\partial c} = A \frac{\partial x^2}{\partial c} + B \frac{\partial y^2}{\partial c} + C \frac{\partial z^2}{\partial c} + 2D \frac{\partial xy}{\partial c} + \dots \quad (1)$$

It is therefore necessary to have such expressions for the squares and products of the coördinates of the Moon that each of the required derivatives can be found as easily as may be.

When the present work was commenced it was intended to make use of the developments of the powers and products x^2, y^2 , etc., as derived from Delaunay's theory, and found in *Action*, pp. 154-172 and 213-224, where the processes by which these quantities may be expressed are fully set forth. But, before the work was put into final shape, Brown's work on the Lunar Theory was completed and published so far as the action of the Sun was concerned; and it therefore became a question whether to use Brown's expressions instead of those of Delaunay, or to go on with the latter. Each course was found to have its drawbacks. The former developments from Delaunay's theory being intended mainly to make an exhaustive search for possible terms hitherto unknown in the Moon's motion, were not completed beyond the third order, though the constant term was carried to the sixth order. To speak more exactly, the development was carried to such a point that the square of each coefficient would be correct to the sixth order.

It was found, however, that the use of Brown's more rigorous theory would be quite convenient except in a single point. In this theory the coördinates are explicit functions of all the lunar elements except the Moon's distance, which enters into m , and of which Brown used only the numerical value in his developments. Brown has shown how it is possible from the data and methods of his theory to form the complete derivatives as to this element without using an analytic development in powers of m . But as the application of this method would require a longer and more laborious study of the subject than the author was prepared to enter upon, it was decided to use the Delaunay developments for obtaining the derivatives as to

log a . The outcome of these considerations has been that, for the sake of trial and comparison, both Delaunay's and Brown's developments have been to a large extent independently used, and the results compared with a view of facilitating an estimate of the errors to which the analytic development is subject.

§ 48. *Reduction of coördinates to the radius vector of the Mean Sun as X -axis.*

In the developments in *Action* the Sun's perihelion was taken as the origin from which longitudes were measured. When the present work was undertaken, it being found that the development of the A -coefficients would be most easily effected by taking the direction of the mean Sun as the axis of X , the same origin had to be taken for the lunar coördinates. This has been done throughout the work; and it must be understood in the subsequent developments that x and y are referred to the radius vector of the mean Sun as axis of X except in terms arising from the motion of the ecliptic.

In the use of either theory we take, as the initial data of the problem, the rectangular coördinates of the Moon referred to the mean Moon as the axis of X , which coördinates we represent by x_1 and y_1 . These coördinates are those which Brown's theory gives in the first instance, and they are also those which I have developed in powers of m , etc., from Delaunay's theory in *Action*, pp. 167 and 169. The notation of arguments from the latter paper is:

- g , the Moon's mean anomaly; g' , the Sun's mean anomaly;
- λ , the mean elongation of the Moon from the Moon's ascending node, equivalent to Delaunay's F , or the mean argument of latitude;
- λ' , the same for the mean Sun;
- θ , the longitude of the Moon's node;
- $l = g + \pi + \theta$, the Moon's mean longitude; $l' = g' + \lambda' + \theta$, the Sun's mean longitude;
- $D = l - l' = \lambda - \lambda'$, as in Delaunay, the mean Moon's departure from the mean Sun.

Putting δv for the excess of the true longitude over l , we then have

$$\begin{aligned} x_1 &= r \cos \beta \cos \delta v = a \Sigma k \cos N \\ y_1 &= r \cos \beta \sin \delta v = a \Sigma k' \sin N \\ z &= r \sin \beta = a \Sigma c \sin N' \end{aligned} \tag{2}$$

where k , k' , and c of dimensions 0 are developed in powers of e , e' , y , and m .

The general form of the arguments N and N' is

$$N \text{ or } N' = ig + i'g' + j\lambda + j'\lambda' \tag{3}$$

where $g = l - \pi$, $g' = l' - \pi'$, $\lambda = l - \theta$, $\lambda' = l' - \theta$.

The equations for transforming x_1 and y_1 into x and y are

$$x = x_1 \cos D - y_1 \sin D \quad y = x_1 \sin D + y_1 \cos D \tag{4}$$

If we put

$$h = \frac{1}{2}(k + k') \quad h' = \frac{1}{2}(k - k')$$

the substitution of the development will give

$$\begin{aligned} \frac{x}{a} &= \Sigma h \cos (D + N) + \Sigma h' \cos (D - N) \equiv \xi \\ \frac{y}{a} &= \Sigma h \sin (D + N) + \Sigma h' \sin (D - N) \equiv \eta \end{aligned} \tag{5}$$

§ 49. There are now two ways of proceeding in order to form the squares and products. We may either form the last expressions for x and y and square them, or we may form the squares and products of x_1 and y_1 , and transform them from the mean Sun to the mean Moon. Following the latter method we have

$$\begin{aligned} x^2 &= \frac{1}{2}(x_1^2 + y_1^2) + \frac{1}{2}(x_1^2 - y_1^2) \cos 2D - x_1 y_1 \sin 2D \\ y^2 &= \frac{1}{2}(x_1^2 + y_1^2) - \frac{1}{2}(x_1^2 - y_1^2) \cos 2D + x_1 y_1 \sin 2D \\ x^2 - y^2 &= (x_1^2 - y_1^2) \cos 2D - 2x_1 y_1 \sin 2D \\ 2xy &= 2x_1 y_1 \cos 2D + (x_1^2 - y_1^2) \sin 2D \end{aligned} \tag{6}$$

The three functions required in the work being

$$(x^2 - y^2), \quad r^2 - 3z^2 \quad \text{and} \quad 2xy$$

we see from the preceding equations that the first and third can be formed at once from the corresponding functions of x_1^2 and y_1^2 by a transformation through the angle $2D$. If we have, for any argument N ,

$$x_1^2 - y_1^2 = h_1 \cos N \quad 2x_1 y_1 = h_2 \sin N \tag{7}$$

the corresponding terms referred to the mean Sun are

$$\begin{aligned} x^2 - y^2 &= \frac{1}{2}(h_1 + h_2) \cos (2D + N) + \frac{1}{2}(h_1 - h_2) \cos (2D - N) \\ 2xy &= \frac{1}{2}(h_1 + h_2) \sin (2D + N) + \frac{1}{2}(h_1 - h_2) \sin (2D - N) \end{aligned} \tag{8}$$

There are some cases in which a reference to a fixed axis is convenient. Let us put,

$$x_0, y_0, \text{ coördinates referred to any fixed axis.}$$

So long as this axis is unrestricted the coefficients for x_0 and y_0 will be equal, as is seen from (5). Hence, if we write for any term of x_0 and of y_0 depending on any argument N

$$x_0 = h_0 \cos N \quad y_0 = h_0 \sin N \tag{9}$$

this term will be transformed into the corresponding term of x and of y , and *vice versa*, by means of the equations

$$\begin{aligned}
 x &= x_0 \cos l' + y_0 \sin l' & y &= y_0 \cos l' - x_0 \sin l' \\
 \text{or} & & & \\
 x_0 &= x \cos l' - y \sin l' & y_0 &= y \cos l' + x \sin l'
 \end{aligned} \tag{10}$$

The special term (9) will, therefore, transform into the terms of x and of y

$$x = h_0 \cos (N - l') \quad y = h_0 \sin (N - l') \tag{11}$$

For the special functions required in the lunar theory we shall have the following transformations of the same form as (6)

$$x^2 - y^2 = (x_0^2 - y_0^2) \cos 2l' + 2x_0y_0 \sin 2l' \tag{12}$$

$$2xy = 2x_0y_0 \cos 2l' - (x_0^2 - y_0^2) \sin 2l'$$

$$x_0^2 - y_0^2 = (x^2 - y^2) \cos 2l' - 2xy \sin 2l' \tag{13}$$

$$2x_0y_0 = 2xy \cos 2l' + (x^2 - y^2) \sin 2l'$$

The transformation of any one term may be made by the equations (6) by writing $+ 2l'$ or $- 2l'$ for $2D$.

If, as in most of the present work, the solar perigee is taken as the fundamental fixed X -axis, we write g' instead of l' in these equations.

An important remark to be made on these transformations of terms from one axis to the other is that the equality of coefficients expressed in the equations (9) and (11) is true only when the fixed axis of X is unrestricted. If, as will sometimes be more convenient, we take the direction of the solar perigee for this axis, some values of argument N in (9) will be equal with opposite signs. By combining the terms depending on these arguments the equality in question will cease to hold. If, however, the Sun's eccentricity is dropped, the general equations will remain valid for the Sun's perigee also.

It thus happens that, in the developments given in *Action*, pages 213-215, the coördinates are quite general, while the expressions for their squares and products given on pp. 217-223 are not general, because the solar perigee is here taken as the fundamental axis.

§ 50. Recalling that throughout the work we use the symbol D to represent the logarithmic derivative as to a of any function, a serious question is that of determining the value of this derivative with the necessary precision in each special class of terms. In actually performing the work so many tentative combinations have been made, as better and better methods were found, that it is difficult to present any one process as the definitive one. The following method was at length seen to be the best under the circumstances I have described. Let

$$u = a^i \phi(m)$$

be any function of the coördinates of which D is to be formed. Practically i will

be equal to 1 or 2 according as the expression we are dealing with is of the first or second degree in the rectangular coördinates. If we can compute the value of $D\phi(m)$ with sufficient precision the complete value of Du will be

$$Du = ia^i\phi(m) + a^iD\phi(m) \tag{14}$$

If it is developed in powers of m , $\phi(m) = \alpha_0 + \alpha_1m + \alpha_2m^2 + \dots$ and we shall have

$$D\phi(m) = \frac{2}{3}\alpha_1m + 3\alpha_2m^2 + \dots$$

the coefficient of each term being $\frac{3}{2}$ of the exponent of m . (v. § 12, Eq. 23.)

If we have the numerically accurate value of any $\phi(m)$ from Brown's theory and an approximate one from the analytic development, the comparison of the two will furnish a rude index to the probable value of the omitted powers of m in the development. It follows that the nearest approximation to the value of Du will be obtained by using in the first term of the second member of (14) the numerical value of $a^i\phi(m) = u$, the analytic development being used only for the second term. Moreover, having an approximate estimate of the value of the omitted terms of the analytic development of the second member of (14), we may use it to correct the last term of this member. I conceive that no lack of theoretical rigor pertaining to this process will lead to an error of the slightest importance in the present work.

§ 51. *Formation of the D's from Delaunay's Theory.*

In the final formation of the D -derivatives I have extended the developments given in *Action*, by the aid of Delaunay's results, as follows. Delaunay expresses the reciprocal of the Moon's radius vector in a form which we may write

$$\frac{a}{r} = 1 + \pi_1$$

where π_1 is put for the sum of an infinite series of terms, each developed in powers of m , as well as of e , e' , and γ . This quantity π_1 is related to the Moon's parallax π by the equation

$$\sin \pi = \frac{a_1}{a} (1 + \pi_1)$$

a_1 being the Earth's equatorial radius.

It is to be remarked that Delaunay's expression for the parallax was only carried to terms of the fifth order, so that it does not suffice for all theoretical purposes. It is indeed fairly probable that it would suffice for the object now in view. In order, however, to lessen the danger of any insufficiency in this respect I have, in forming the value of π_1 , compared each coefficient in the expression of Delaunay's parallax found in my transformation of Hansen's lunar theory with the more accurate value derived from Hansen's or Brown's expression. We may conceive that the correction necessary to reduce Delaunay's coefficient to Hansen's value is of the form

$$\delta\pi_1 = \alpha_i m^i + \alpha_{i+1} m^{i+1} + \dots$$

in which i is the power of m next above the highest to which Delaunay has carried his coefficient. From what we have already shown it follows that the corresponding correction to $D\pi_1$ is

$$\frac{3}{2}i\alpha_1 m^i + \frac{3}{2}(i+1)\alpha_{i+1} m^{i+1} \quad (15)$$

an approximate value of which is

$$\frac{3}{2}i\delta\pi_1$$

In order to make this correction rigorously exact we should know the values of the coefficients of the omitted powers of i . This being unknown, the minute correction is to a certain extent a matter of estimation. I do not conceive, however, that the uncertainty is at all important in the present investigation.

We have next to consider the D -derivatives of the three functions

$$\rho^2 - 3\zeta^2; \quad \xi_1^2 - \eta_1^2; \quad \text{and} \quad 2\xi_1\eta_1$$

Starting with the equations (2) the values of δv and β , developed in powers of m , are given at the end of Delaunay's *Theorie*, Vol. II. The values of $D\delta v$ are formed from these with great facility by means of the form (23) of § 12, because Delaunay gives the numerical value of each part of every term of the longitude.

The steps of the subsequent process consist in simple trigonometric multiplications, and are presented in tabular form on the following pages. The fundamental quantities are

$$\pi_1 = \frac{a}{r} - 1, \quad \delta v, \quad \beta \quad \text{and} \quad D\frac{a}{r}, \quad D\delta v, \quad D\beta$$

which are formed from Delaunay's numbers in the way just shown.

The following functions are then formed by trigonometric multiplication

$$\rho = 1 - \pi_1 + \pi_1^2 - \pi_1^3 + \dots \quad \rho^2 = 1 - 2\pi_1 + 3\pi_1^2 - 4\pi_1^3 + \dots \quad \rho^3 = 1 - 3\pi_1 + 6\pi_1^2 - 10\pi_1^3 + \dots$$

In the final work, however, ρ has been formed from Brown's theory. Then

$$\begin{aligned} \rho^2 &= \xi^2 + \eta^2 + \zeta^2 \\ \sin \beta &= \beta - \frac{1}{6}\beta^3 & \cos \beta &= 1 - \frac{1}{2}\beta^2 + \frac{1}{24}\beta^4 & \cos^2 \beta &= 1 - \sin^2 \beta \\ \sin \delta v &= \delta v - \frac{1}{6}\delta v^3 & \cos \delta v &= 1 - \frac{1}{2}\delta v^2 \\ \xi_1^2 - \eta_1^2 &= \rho^2 \cos^2 \beta (1 - 2 \sin^2 \delta v) & \xi_1 \eta_1 &= \rho^2 \cos^2 \beta \cos \delta v \sin \delta v \\ \zeta &= \rho \sin \beta & \zeta^2 &= \rho^2 \sin^2 \beta & D \cdot \rho^2 &= -2\rho^3 D\pi_1 \\ D \sin \beta &= \cos \beta D\beta & D \sin^2 \beta &= 2 \sin \beta D \sin \beta & D\rho^2 \cos^2 \beta &= \cos^2 \beta D\rho^2 + \rho^2 D \cos^2 \beta \quad (16) \\ D \sin^2 \delta v &= 2 \sin \delta v D \sin \delta v = 2 \sin \delta v \cos \delta v D\delta v \\ D(\xi_1^2 - \eta_1^2) &= (1 - 2 \sin^2 \delta v) D\rho^2 \cos^2 \beta - 2\rho^2 \cos^2 \beta D \sin^2 \delta v \\ D \cdot \xi_1 \eta_1 &= \sin \delta v \cos \delta v D\rho^2 \cos^2 \beta + \rho^2 \cos^2 \beta (1 - 2 \sin^2 \delta v) D\delta v \\ D \cdot \zeta^2 &= \rho^2 D \sin^2 \beta + \sin^2 \beta D \cdot \rho^2 \end{aligned}$$

The same method might be used to form the derivatives as to the e and γ , but this has been deemed unnecessary, as they can be formed with entire precision from Brown's Theory, and probably with all necessary precision from the developments found in *Action* with some extensions in special cases. As a matter of fact they have been formed by both methods.

§ 52. *Derivatives from Brown's theory.* To form the partial derivatives as to Delaunay's e and γ from Brown's expressions it is to be noted that Brown uses instead of e and γ two constants e and k which, omitting unimportant terms, are expressed thus in terms of the Delaunay elements:

$$e = (2.000543 + .049e'^2)e - .3668e^3 - 2.012e\gamma^2$$

$$k = (1.000128 - .0004e'^2)\gamma - .496\gamma^3 - 0.499e^2\gamma$$

A distinction is to be made between the a of the present work, defined by the condition $a^3n^2 = \mu$, and Brown's a , used in his work. Brown's e is defined as the coefficient of $\sin g$ in the development of y_1/a , or, using the notation of the present paper, in the development of

$$\frac{a}{a} \cdot \frac{r}{a} \cos \beta \sin \delta v = \frac{a}{a} \eta$$

This will enable us to make a comparison of the preceding value of e with that to be derived from the analytic development in *Action*, p. 168, from which we find

$$\frac{a}{a} e = (2 - \frac{1}{3}m^2 + \frac{75}{128}m^3 + \frac{33353}{4608}m^4 + \frac{23}{8}m^2e'^2)e - (\frac{3}{8} + \frac{1}{4}\gamma^2 - \frac{97}{128}m^2)e^3 - (2 + \frac{125}{8}m^2)e\gamma^2$$

Brown's $2k$ is the coefficient of $\sin \lambda$, λ being the mean argument of latitude, in the development of $r/a \sin \beta$, found on p. 159 of *Action*. From the coefficient as developed in *Action* we find

$$\frac{a}{a} k = (1 - \frac{1}{6}m^2 + \frac{3}{16}m^3 + \frac{1031}{876}m^4 - \frac{1}{4}m^2e'^2)\gamma - (\frac{1}{2} + \frac{25}{8}m^2)e^2\gamma - (\frac{1}{2} + \frac{11}{16}m^2)\gamma^3$$

Brown also gives

$$\frac{a}{a} = .999093; \quad \frac{a}{a} = 1.000908$$

The two results are as follows, B indicating those from Brown's formulæ, A those from the analytic development.

$$B; e = 2.000557e - .367e^3 - 2.012e\gamma^2 \quad B; k = 1.000128\gamma - .499e^2\gamma - .496\gamma^3$$

$$A; e = 2.000426e - .371e^3 - 2.004e\gamma^2 \quad A; k = 1.000108\gamma - .501e^2\gamma - .500\gamma^3$$

The difference, arising from the dropping of higher powers of m in the analytic development, is too small to affect the solution of our present problem.

To find the partial derivatives of any function u of e and k with respect to e and γ we have from the preceding expressions

$$\frac{\partial u}{\partial e} = \frac{\partial u}{\partial e} \frac{\partial e}{\partial e} + \frac{\partial u}{\partial k} \frac{\partial k}{\partial e} = 1.9932 \frac{\partial u}{\partial e} - .0099 \frac{\partial u}{\partial k} \quad (17)$$

$$\frac{\partial u}{\partial \gamma} = \frac{\partial u}{\partial e} \frac{\partial e}{\partial \gamma} + \frac{\partial u}{\partial k} \frac{\partial k}{\partial \gamma} = 0.9956 \frac{\partial u}{\partial k} - .0025 \frac{\partial u}{\partial e}$$

These equations enable us to find the derivatives as to e and γ from Brown's as to e and k .

§ 53. *Tables of the functions and derivatives of the Moon's coördinates.*

The numerical processes by which the required functions of the coördinates were developed may be followed and tested by the aid of the following tables. The notation of the arguments, expressed by the indices in the first column, has been defined in § 48.

Owing to the circumstances mentioned in § 46, and to the widely different degree of precision required in the coefficients of different arguments, the numbers of these tables are not always consistently continuous. The terms of many, perhaps more than half the arguments, lead to no sensible inequalities; with these pains were not always taken to reach a higher degree of precision than was required to show the order of magnitude of the results. In the preliminary steps of the investigation it was deemed sufficient to carry the expressions for the Moon's coördinates to the 5th place of decimals, and those for the derivatives to the 3d or 4th place. But when the inequalities of the elements themselves were reached by integration, it was found that this degree of precision, while more than sufficient for the periodic terms in general, was not sufficient either in the terms related to the evection, or in those determining the secular variations and accelerations of l , π , and θ . A number of successive revisions was found to be necessary, in which the coefficients depending on the argument g' were carried to the 7th place of decimals. As the last place was always more or less doubtful only the sixth place has been included in the printing.

It may also be remarked that in commencing the tables it was supposed that the analytic development in *Action* would suffice for the work. This expectation proving ill-founded, the developments of the Moon's coördinates given by Delaunay, then those by Hansen, and finally those by Brown were successively used in the case of those terms in which greater precision was needed. Finally the D -derivatives were, in their important terms, recomputed by formulæ proposed by Dr. Ross, which were much briefer than those already given in (16) of § 51.

The want of homogeneity thus arising in the tables could be cured by a fresh development from the fundamental data of Brown and Delaunay, but I do not think any important change would thus result in the expressions for the inequalities of the Moon's elements found in Part IV.

TABLE XXXV.

FUNCTIONS OF THE LATITUDE AND THEIR DERIVATIVES.

| Arg. | β | $D\beta$ | $\sin \beta$ | $D \sin \beta$ | $\zeta = \rho \sin \beta$ | $D\zeta$ | $\partial\zeta/\partial e$ | $\partial\zeta/\partial \gamma$ |
|--------------------------|-----------|-----------|--------------|----------------|---------------------------|-----------|----------------------------|---------------------------------|
| $g' g' \lambda \lambda'$ | sin | sin | sin | sin | sin | sin | sin | sin |
| -2 0 1 0 | -.000 154 | +.000 09 | -.000 154 | +.000 90 | -.000 088 | +.000 08 | -.004 9 | -0.003 0 |
| -1 0 1 0 | -.004 842 | +.000 32 | -.004 840 | +.000 32 | -.007 240 | +.000 44 | -.130 4 | -0.161 5 |
| 0 0 1 0 | +.089 503 | .000 00 | +.089 413 | .000 00 | +.089 474 | -.000 18 | -.004 9 | +1.998 |
| 1 0 1 0 | +.004 898 | -.000 05 | +.004 896 | -.000 05 | +.002 466 | +.000 03 | +.045 4 | +0.055 |
| 2 0 1 0 | +.000 301 | -.000 01 | +.000 301 | -.000 01 | +.000 101 | -.000 01 | | +0.002 3 |
| 0 -1 1 0 | +.000 023 | -.000 038 | +.000 023 | -.000 038 | +.000 029 | -.000 017 | +.000 052 | +0.000 642 |
| 1 -1 1 0 | | | | | +.000 017 | | +.000 32 | +0.000 39 |
| -1 -1 1 0 | | | | | -.000 042 | | -.000 76 | -0.000 94 |
| 0 1 1 0 | -.000 032 | +.000 013 | -.000 030 | +.000 013 | -.000 024 | +.000 031 | -.000 079 | -0.000 535 |
| 0 0 3 0 | -.000 030 | +.000 01 | -.000 030 | +.000 | | | | |
| -1 0 3 -2 | +.000 968 | +.002 02 | +.000 968 | +.002 01 | +.000 545 | +.001 24 | +.009 7 | +0.012 2 |
| -1 -1 3 -2 | | | | | +.000 026 | | +.000 47 | |
| 0 0 3 -2 | +.000 568 | +.001 80 | +.000 568 | +.001 80 | +.000 177 | +.000 58 | | +0.004 1 |
| -1 -1 1 -2 | | | | | +.000 051 | | -.000 94 | -0.001 16 |
| 0 -1 1 -2 | +.000 144 | +.000 30 | +.000 144 | +.000 30 | +.000 165 | +.000 18 | | +0.003 2 |
| -1 0 1 -2 | +.000 808 | +.001 75 | +.000 808 | +.001 74 | +.001 179 | +.002 44 | +.021 1 | +0.026 1 |
| 0 0 1 -2 | +.003 022 | +.005 42 | +.003 020 | +.005 40 | +.003 308 | +.006 47 | -.000 7 | +0.073 9 |
| 1 0 1 -2 | +.000 161 | +.000 28 | +.000 161 | +.000 28 | +.000 080 | +.000 12 | | +0.001 7 |
| 0 1 1 -2 | -.000 060 | -.000 12 | -.000 060 | -.000 12 | -.000 061 | +.000 18 | | -0.001 4 |

TABLE XXXVI.

FUNCTIONS OF THE RADIUS VECTOR AND LATITUDE.

| Arg. | $D\pi_1$ | $\rho^2 = r^2/a^2$ | ζ^2 | $\rho^2 \cos^2 \beta$ | $D. \rho^2$ | $D. \zeta^2$ | $D. \rho^2 \cos^2 \beta$ |
|--------------------------|-----------|--------------------|-----------|-----------------------|-------------|--------------|--------------------------|
| $g' g' \lambda \lambda'$ | cos | cos | cos | cos | cos | cos | cos |
| 0 0 0 0 | +.002 638 | +1.002 866 | +.004 038 | +.998 828 | -.004 43 | +.000 01 | -.004 44 |
| 1 0 0 0 | -.001 40 | -0.108 58 | -.000 42 | -.108 17 | +.004 80 | +.000 06 | +.004 74 |
| 2 0 0 0 | -.000 16 | -0.001 52 | -.000 02 | -.001 51 | +.000 08 | +.000 01 | +.000 08 |
| -1 1 0 0 | +.000 917 | -0.000 70 | -.000 00 | -.000 70 | -.001 77 | .000 00 | -.001 76 |
| 0 1 0 0 | -.000 267 | +0.000 266 | +.000 001 | +.000 266 | +.000 713 | +.000 001 | +.000 712 |
| 1 1 0 0 | -.000 037 | +.000 54 | .000 00 | +.000 54 | +.001 27 | .000 00 | +.001 26 |
| -1 0 2 0 | +.000 10 | +0.000 32 | +.000 65 | -.000 33 | -.000 19 | -.000 03 | -.000 15 |
| 0 0 2 0 | +.000 06 | -0.000 02 | -.003 98 | +.003 97 | -.000 10 | +.000 02 | -.000 12 |
| 1 0 2 0 | +.000 00 | +0.000 00 | -.000 22 | +.000 22 | .000 00 | .000 00 | +.000 01 |
| -2 0 2 -2 | -.000 32 | +.000 83 | .000 00 | +.001 82 | +.003 80 | +.000 02 | +.003 77 |
| -1 0 2 -2 | +.019 66 | -0.018 91 | -.000 03 | -.018 88 | -.035 22 | -.000 06 | -.035 15 |
| 0 0 2 -2 | +.026 43 | -0.014 86 | -.000 29 | -.014 57 | -.049 46 | -.000 54 | -.048 92 |
| 1 0 2 -2 | +.002 91 | -0.000 48 | -.000 02 | -.000 46 | -.001 54 | -.000 03 | -.001 50 |
| 2 0 2 -2 | +.000 27 | -0.000 04 | .000 00 | -.000 04 | -.000 07 | .000 00 | -.000 07 |
| -1 1 2 -2 | +.000 216 | +0.000 06 | .000 00 | +.000 06 | -.000 48 | .000 00 | -.000 47 |
| 0 1 2 -2 | -.000 441 | +0.000 144 | +.000 005 | +.000 139 | +.000 84 | -.000 016 | +.000 856 |
| 1 1 2 -2 | -.000 058 | .000 00 | .000 00 | .000 00 | +.000 01 | .000 00 | +.000 01 |
| -1 -1 2 -2 | +.000 844 | -0.000 80 | .000 00 | -.000 80 | -.001 40 | .000 00 | -.001 40 |
| 0 -1 2 -2 | +.002 027 | -0.001 043 | -.000 015 | -.001 028 | -.003 86 | -.000 02 | -.003 84 |
| 1 -1 2 -2 | +.000 260 | .000 00 | .000 00 | .000 00 | -.000 15 | .000 00 | -.000 15 |
| -1 0 0 2 | -.000 02 | -0.000 05 | -.000 02 | -.000 03 | -.000 02 | -.000 04 | +.000 01 |
| 0 0 0 2 | -.000 08 | +0.000 5 | +.000 287 | -.000 23 | +.000 16 | +.000 56 | -.000 40 |
| 1 0 0 2 | -.000 04 | +0.000 6 | +.000 11 | -.000 05 | -.000 07 | +.000 23 | -.000 30 |
| 0 2 0 0 | -.000 018 | | | | +.000 036 | | +.000 036 |
| 0 -2 2 -2 | +.000 106 | | | | -.000 212 | | -.000 212 |
| 0 2 2 -2 | -.000 004 | | | | +.000 008 | | +.000 008 |

TABLE XXXVII.

FUNCTIONS OF THE LONGITUDE AND THEIR DERIVATIVES.

| Arg. | $\sin \delta v$ | $\cos \delta v$ | $\frac{1}{2} \sin 2\delta v$, | $\sin^2 \delta v$ | $D \cdot \sin^2 \delta v$ | $D\delta v$ | $\frac{1}{2} D \sin 2\delta v$ |
|-------------------------------|-----------------|-----------------|--------------------------------|-------------------|---------------------------|-------------|--------------------------------|
| $g \ g' \ \lambda \ \lambda'$ | sin | cos | sin | cos | cos | sin | sin |
| 0 0 0 0 | | +096 83 | | +006 33 | +001 483 | | |
| 1 0 0 0 | +109 58 | -000 35 | +109 03 | +000 70 | +001 55 | .000 000 | -000 320 |
| 2 0 0 0 | +003 71 | +003 00 | +003 65 | -005 97 | +000 20 | -000 138 | -000 314 |
| -1 1 0 0 | -000 72 | +000 17 | -000 71 | +000 33 | -000 19 | -002 052 | -002 008 |
| 0 1 0 0 | -003 233 | -000 02 | -003 20 | +000 04 | +000 249 | -002 8437 | -002 7902 |
| 1 1 0 0 | -000 53 | -000 18 | -000 53 | +000 36 | +000 36 | -001 199 | -001 200 |
| -1 0 2 0 | -000 19 | +000 11 | -000 19 | -000 22 | +000 03 | +000 215 | +000 212 |
| 0 0 2 0 | -001 99 | -000 01 | -001 97 | +000 02 | -000 01 | +000 091 | +000 090 |
| 1 0 2 0 | -000 22 | -000 11 | -000 22 | +000 22 | -000 01 | | |
| -2 0 2 -2 | +001 03 | -001 25 | +001 07 | +002 49 | +005 31 | +002 545 | +002 705 |
| -1 0 2 -2 | +022 17 | -000 58 | +022 03 | +001 16 | +003 77 | +047 405 | +046 777 |
| 0 0 2 -2 | +011 45 | +001 17 | +011 35 | -002 34 | -004 83 | +037 838 | +037 341 |
| 1 0 2 -2 | +000 96 | +000 67 | +000 98 | -001 34 | -004 27 | +003 056 | +003 273 |
| 2 0 2 -2 | +000 09 | +000 07 | +000 15 | -000 15 | -000 48 | +000 228 | +000 469 |
| -1 1 2 -2 | -000 14 | -000 03 | -000 14 | +000 07 | +000 20 | +000 482 | +000 490 |
| 0 1 2 -2 | -000 12 | -000 03 | -000 12 | +000 06 | +000 148 | -000 3608 | -000 3662 |
| 1 1 2 -2 | -000 02 | | -000 02 | +000 01 | +000 08 | -000 055 | -000 075 |
| -1 -1 2 -2 | +001 00 | -000 01 | +000 99 | +000 02 | +000 07 | +002 274 | +002 223 |
| 0 -1 2 -2 | +000 80 | +000 07 | +000 80 | -000 16 | -000 451 | +002 9357 | +002 9079 |
| 1 -1 2 -2 | +000 07 | +000 05 | +000 08 | -000 10 | -000 39 | +000 271 | +000 305 |
| -1 0 0 2 | | +000 02 | | -000 03 | -000 02 | | |
| 0 0 0 2 | -000 27 | +000 01 | -000 27 | -000 02 | -000 08 | -000 294 | -000 300 |
| 1 0 0 2 | | +000 01 | | -000 02 | -000 07 | | +000 008 |
| 0 2 0 0 | -000 036 | | -000 036 | | | -000 008 | |
| 0 -2 2 -2 | +000 039 | | +000 039 | | | +000 156 | |

TABLE XXXVIII.

COÖRDINATES REFERRED TO MEAN MOON AND THEIR DERIVATIVES.

| Arg. | ξ_1 Brown. | $D\xi_1$ Anal. | $\partial\xi_1/\partial e$ Brown. | $\partial\xi_1/\partial \gamma$ Brown. | η_1 Brown. | $D\eta_1$ Anal. | $\partial\eta_1/\partial e$ Brown. | $\partial\eta_1/\partial \gamma$ Brown. |
|-------------------------------|-------------------|-------------------|--------------------------------------|---|--------------------|--------------------|---------------------------------------|--|
| $g \ g' \ \lambda \ \lambda'$ | cos | cos | cos | cos | sin | sin | sin | sin |
| 0 0 0 0 | +095 47 | -003 02 | -058 4 | -089 4 | | | | |
| 1 0 0 0 | -054 49 | +001 27 | -095 5 | +004 6 | +109 44 | -000 17 | +1991 4 | |
| 2 0 0 0 | +001 51 | +000 01 | +055 03 | +000 1 | +000 74 | +000 01 | +026 7 | |
| -1 1 0 0 | -000 174 | +000 04 | -003 17 | | -000 643 | -000 38 | -0011 71 | |
| 0 1 0 0 | +000 1034 | +000 33 | -000 346 | -000 063 | -003 2283 | -003 12 | -0002 508 | +001 511 |
| 1 1 0 0 | +000 095 | -000 04 | +001 74 | | -000 440 | -000 38 | -0007 96 | |
| -1 0 2 0 | +000 04 | .000 00 | +000 8 | +001 8 | -000 25 | .000 00 | -0004 4 | -010 9 |
| 0 0 2 0 | +001 99 | +000 01 | | +009 8 | -001 99 | +000 10 | | -097 8 |
| 1 0 2 0 | +000 05 | .000 00 | +001 0 | +002 5 | -000 05 | .000 00 | -0001 0 | -002 5 |
| -2 0 2 -2 | -000 593 | -000 63 | -021 56 | +002 6 | +000 967 | +000 95 | +0035 13 | |
| -1 0 2 -2 | -010 16 | -019 31 | -184 4 | +001 9 | +022 24 | +044 88 | +0403 7 | -004 7 |
| 0 0 2 -2 | -006 36 | -022 85 | +023 7 | +006 8 | +010 32 | +035 21 | +010 6 | -007 7 |
| 1 0 2 -2 | +000 18 | +000 29 | +004 8 | | +000 20 | +000 40 | +0004 8 | |
| 2 0 2 -2 | +000 02 | | | | +000 02 | | | |
| -1 1 2 -2 | +000 028 | +000 19 | +000 52 | | -000 118 | -000 39 | -0002 15 | |
| 0 1 2 -2 | +000 0478 | +000 20 | -000 262 | -000 118 | -000 0942 | -000 31 | -0000 169 | +000 132 |
| 1 1 2 -2 | -000 002 | | -000 04 | | -000 003 | | -0000 04 | |
| -1 -1 2 -2 | -000 400 | -000 44 | -007 28 | | +000 993 | +000 90 | +0018 04 | |
| 0 -1 2 -2 | -000 4506 | -001 55 | +001 256 | +000 337 | +000 7327 | +002 25 | +0000 594 | -000 406 |
| 1 -1 2 -2 | +000 013 | | +000 24 | | +000 014 | | +0000 26 | |
| 0 0 0 2 | -000 10 | -000 17 | | -004 5 | +000 27 | +000 08 | | +012 2 |

TABLE XXXIX.

FUNCTIONS OF COÖRDINATES REFERRED TO MEAN MOON.

| Arg. | | | | ξ_1^2 Brown. | η_1^2 Brown. | $\xi_1^2 - \eta_1^2$ Brown. | $2\xi_1\eta_1$ Brown. | $D(\xi_1^2 - \eta_1^2)$ Delaunay. | $2D(\xi_1\eta_1)$ Delaunay. |
|----------|-----------|-----------|------------|---------------------|----------------------|--------------------------------|--------------------------|--------------------------------------|--------------------------------|
| <i>g</i> | <i>g'</i> | λ | λ' | cos | cos | cos | sin | cos | sin |
| 0 | 0 | 0 | 0 | +0.992 529 | +0.006 299 | +0.986 230 | | -0.007 345 | |
| 1 | 0 | 0 | 0 | -.108 50 | +0.000 33 | -.108 83 | +0.217 74 | +0.001 95 | -.000 70 |
| 2 | 0 | 0 | 0 | +0.004 504 | -.005 989 | +0.010 493 | -.004 501 | -.000 18 | +0.000 12 |
| -1 | 1 | 0 | 0 | -.000 35 | -.000 35 | .000 000 | -.001 10 | -.001 36 | -.003 84 |
| 0 | 1 | 0 | 0 | +0.000 217 | +0.000 049 | +0.000 168 | -.006 386 | +0.000 198 | -.005 552 |
| 1 | 1 | 0 | 0 | +0.000 19 | +0.000 35 | -.000 16 | -.000 70 | +0.000 54 | -.002 10 |
| -1 | 0 | 2 | 0 | -.000 11 | -.000 22 | +0.000 11 | -.000 12 | -.000 21 | +0.000 41 |
| 0 | 0 | 2 | 0 | +0.003 97 | .000 00 | +0.003 97 | -.003 95 | -.000 11 | +0.000 16 |
| 1 | 0 | 2 | 0 | .000 000 | +0.000 22 | -.000 22 | +0.000 22 | +0.000 03 | -.000 03 |
| -2 | 0 | 2 | -2 | -.000 637 | +0.002 444 | -.003 081 | +0.001 843 | -.006 70 | +0.004 32 |
| -1 | 0 | 2 | -2 | -.019 90 | +0.001 02 | -.020 92 | +0.044 34 | -.042 09 | +0.004 72 |
| 0 | 0 | 2 | -2 | -.012 13 | -.002 44 | -.009 69 | +0.018 19 | -.038 63 | +0.065 56 |
| 1 | 0 | 2 | -2 | +0.000 69 | -.001 15 | +0.001 84 | -.000 82 | +0.006 32 | -.003 03 |
| 2 | 0 | 2 | -2 | -.000 02 | -.000 02 | .000 00 | +0.000 04 | +0.000 12 | +0.000 19 |
| -1 | 1 | 2 | -2 | +0.000 06 | | +0.000 06 | -.000 24 | -.000 91 | +0.001 12 |
| 0 | 1 | 2 | -2 | +0.000 092 | +0.000 056 | +0.000 036 | -.000 154 | +0.000 587 | -.000 553 |
| 1 | 1 | 2 | -2 | .000 00 | .000 000 | -.000 00 | .000 00 | -.000 12 | +0.000 07 |
| -1 | -1 | 2 | -2 | -.000 80 | .000 000 | -.000 80 | +0.001 97 | -.001 50 | +0.004 41 |
| 0 | -1 | 2 | -2 | -.000 875 | -.000 154 | -.000 721 | +0.001 336 | -.002 889 | +0.005 097 |
| 1 | -1 | 2 | -2 | .000 00 | | .000 00 | .000 00 | +0.000 55 | -.000 26 |
| 1 | 0 | 0 | 2 | -.000 05 | .000 00 | -.000 05 | -.000 05 | -.000 14 | -.000 11 |
| 0 | 0 | 0 | 2 | -.000 21 | -.000 02 | -.000 19 | -.000 56 | -.000 24 | -.000 60 |
| -1 | 0 | 0 | 2 | .000 00 | -.000 03 | +0.000 03 | .000 00 | +0.000 06 | +0.000 08 |
| -2 | 0 | 4 | -4 | +0.000 187 | -.000 253 | +0.000 440 | -.000 175 | -.000 11 | -.001 02 |
| -1 | 0 | 4 | -4 | +0.000 06 | -.000 23 | +0.000 29 | -.000 16 | +0.002 64 | -.000 51 |
| 0 | 0 | 4 | -4 | +0.000 02 | -.000 06 | +0.000 08 | -.000 06 | +0.000 74 | +0.000 04 |

| Arg. | | | | $\frac{\partial \cdot \xi_1^2}{\partial e}$ | $\frac{\partial \cdot \eta_1^2}{\partial e}$ | $\frac{2\partial \cdot \xi_1\eta_1}{\partial e}$ | $\frac{\partial \cdot \xi_1^2}{\partial \gamma}$ | $\frac{\partial \cdot \eta_1^2}{\partial \gamma}$ | $\frac{2\partial \cdot \xi_1\eta_1}{\partial \gamma}$ | $\frac{\partial \cdot \zeta^2}{\partial e}$ | $\frac{\partial \cdot \zeta^2}{\partial \gamma}$ |
|----------|-----------|-----------|------------|---|--|--|--|---|---|---|--|
| <i>g</i> | <i>g'</i> | λ | λ' | cos | cos | sin | cos | cos | sin | cos | cos |
| 0 | 0 | 0 | 0 | -0.058 598 | +0.227 700 | | -.178 059 | -.000 281 | | -.000 695 | +0.179 588 |
| 1 | 0 | 0 | 0 | -1.978 4 | +0.008 4 | +3.940 0 | +0.011 7 | | -.024 7 | -.007 6 | -.019 2 |
| 2 | 0 | 0 | 0 | +0.163 69 | -.217 35 | -.164 64 | +0.000 6 | | | | |
| -1 | 1 | 0 | 0 | -.006 4 | | -.023 5 | | | | | |
| 0 | 1 | 0 | 0 | -.000 419 | +0.001 537 | -.000 478 | -.000 067 | -.000 014 | +0.001 786 | +0.000 004 | +0.000 040 |
| 1 | 1 | 0 | 0 | +0.001 8 | | -.015 9 | | | | | |
| -1 | 0 | 2 | 0 | | -.003 9 | -.002 0 | | +0.010 7 | -.005 4 | +0.011 5 | +0.029 0 |
| 0 | 0 | 2 | 0 | | | | +0.195 6 | | -.194 8 | +0.001 8 | -.178 1 |
| 1 | 0 | 2 | 0 | | +0.003 9 | +0.005 8 | | -.010 7 | +0.016 1 | -.003 9 | -.009 8 |
| -2 | 0 | 2 | -2 | -.023 02 | +0.088 81 | +0.026 3 | | | | | |
| -1 | 0 | 2 | -2 | -.360 0 | +0.017 7 | +0.796 9 | +0.005 3 | | -.013 7 | | |
| 0 | 0 | 2 | -2 | +0.067 295 | -.087 766 | -.066 474 | +0.014 604 | +0.000 597 | -.016 720 | +0.000 1 | -.013 2 |
| 1 | 0 | 2 | -2 | +0.014 3 | -.021 7 | -.008 7 | | | | | |
| 0 | 1 | 2 | -2 | -.000 620 | +0.000 877 | +0.000 230 | -.000 121 | -.000 044 | +0.000 106 | | |
| -1 | -1 | 2 | -2 | -.014 7 | | -.036 2 | | | | | |
| 0 | -1 | 2 | -2 | +0.003 395 | -.004 482 | -.002 870 | +0.000 375 | +0.000 049 | +0.000 432 | | |
| 0 | 0 | 0 | 2 | | | | -.009 0 | | -.024 4 | | +0.013 2 |

TABLE XL.

FUNCTIONS OF COÖRDINATES REFERRED TO MEAN SUN.

| Arg. | | | | $\xi^2 - \gamma^2$ | $\rho^2 - 3\zeta^2$ | $2\xi\eta$ | $D(\xi^2 - \gamma^2)$ | $D(\rho^2 - 3\zeta^2)$ | $2D\xi\eta$ |
|----------|-----------|-----------|------------|--------------------|---------------------|------------|-----------------------|------------------------|-------------|
| <i>g</i> | <i>g'</i> | λ | λ' | cos | cos | sin | cos | cos | sin |
| 0 | 0 | 0 | 0 | -.013 96 | +.990 74 | | -.052 095 | -.004 447 | |
| 1 | 0 | 0 | 0 | -.031 26 | -.108 60 | -.033 92 | -.003 73 | +.004 62 | -.073 08 |
| 2 | 0 | 0 | 0 | -.002 50 | +.000 96 | -.002 43 | -.005 55 | +.000 07 | -.005 47 |
| -1 | 1 | 0 | 0 | +.000 13 | -.000 71 | -.000 08 | -.000 58 | -.001 76 | +.001 37 |
| 0 | 1 | 0 | 0 | -.000 933 | +.000 264 | -.001 123 | -.003 423 | +.000 710 | -.004 563 |
| 1 | 1 | 0 | 0 | -.001 35 | +.000 55 | -.001 34 | -.003 04 | +.001 26 | -.002 89 |
| -1 | 0 | 2 | 0 | -.000 04 | -.000 32 | +.000 10 | -.000 01 | -.000 09 | -.000 01 |
| 0 | 0 | 2 | 0 | -.000 38 | +.011 96 | -.000 38 | -.000 42 | -.000 15 | -.000 42 |
| 1 | 0 | 2 | 0 | -.000 02 | +.000 66 | -.000 02 | -.000 12 | +.000 01 | -.000 12 |
| -2 | 0 | 2 | -2 | +.007 809 | +.001 807 | +.007 185 | +.000 30 | +.003 73 | -.000 60 |
| -1 | 0 | 2 | -2 | -.163 02 | -.018 60 | -.163 54 | +.002 91 | -.035 03 | -.000 25 |
| 0 | 0 | 2 | -2 | +.986 19 | -.013 99 | +.986 11 | -.007 00 | -.047 84 | -.007 70 |
| 1 | 0 | 2 | -2 | +.054 44 | -.000 42 | +.054 44 | +.000 62 | -.001 53 | +.000 62 |
| 2 | 0 | 2 | -2 | +.003 00 | -.000 02 | +.003 00 | -.000 07 | -.000 07 | -.000 03 |
| -1 | 1 | 2 | -2 | -.000 55 | +.000 15 | -.000 56 | -.002 60 | -.000 47 | -.002 60 |
| 0 | 1 | 2 | -2 | -.003 18 | +.000 03 | -.003 17 | -.002 76 | +.000 89 | -.002 76 |
| 1 | 1 | 2 | -2 | -.000 42 | .000 00 | -.000 42 | -.000 77 | +.000 01 | -.000 77 |
| -1 | -1 | 2 | -2 | +.000 27 | -.000 87 | +.000 28 | +.001 33 | -.001 40 | +.001 33 |
| 0 | -1 | 2 | -2 | +.003 22 | -.000 06 | +.003 14 | +.002 89 | -.003 98 | +.002 89 |
| 1 | -1 | 2 | -2 | +.000 54 | .000 00 | +.000 54 | +.001 24 | -.000 15 | +.001 23 |
| 1 | 0 | 0 | 2 | -.000 20 | -.000 32 | +.000 24 | +.000 03 | -.000 76 | -.000 03 |
| 0 | 0 | 0 | 2 | +.003 96 | -.000 84 | -.003 96 | -.000 13 | -.001 52 | +.000 13 |
| 1 | 0 | 0 | -2 | +.000 10 | -.000 04 | +.000 10 | -.000 31 | +.000 08 | -.000 31 |
| 0 | 2 | 0 | 0 | -.000 059 | +.000 005 | -.000 059 | -.000 258 | +.000 036 | -.000 266 |

| Arg. | | | | $\frac{\partial(\xi^2 - \gamma^2)}{\partial e}$ | $\frac{\partial(\rho^2 - 3\zeta^2)}{\partial e}$ | $2 \frac{\partial \xi \eta}{\partial e}$ | $\frac{\partial(\xi^2 - \gamma^2)}{\partial \gamma}$ | $\frac{\partial(\rho^2 - 3\zeta^2)}{\partial \gamma}$ | $2 \frac{\partial \xi \eta}{\partial \gamma}$ |
|----------|-----------|-----------|------------|---|--|--|--|---|---|
| <i>g</i> | <i>g'</i> | λ | λ' | cos | cos | sin | cos | cos | sin |
| 0 | 0 | 0 | 0 | +.0.110 765 | +.0.170 489 | | +.015 359 | -.537 525 | |
| 1 | 0 | 0 | 0 | -.0565 7 | -1.955 1 | -.0608 8 | +.009 4 | +.050 2 | +.009 5 |
| 2 | 0 | 0 | 0 | -.073 3 | -.054 5 | -.069 2 | | | |
| -1 | 1 | 0 | 0 | -.000 0 | -.006 4 | | | | |
| 0 | 1 | 0 | 0 | +.0004 519 | +.001 109 | +.0006 220 | +.000 287 | -.000 161 | +.000 469 |
| 1 | 1 | 0 | 0 | -.025 2 | +.003 6 | -.025 6 | | | |
| -1 | 0 | 2 | 0 | | -.023 0 | | | -.058 0 | |
| 0 | 0 | 2 | 0 | | -.003 6 | | -.017 3 | +.551 6 | -.015 1 |
| 1 | 0 | 2 | 0 | | +.007 8 | | | +.019 6 | |
| -2 | 0 | 2 | -2 | +.0.284 09 | +.0.065 69 | +.0.261 69 | | | |
| -1 | 0 | 2 | -2 | -2.964 1 | -.0.343 1 | -2.964 2 | +.018 2 | +.005 2 | +.018 3 |
| 0 | 0 | 2 | -2 | -.0.286 3 | -.0.021 5 | -.0.286 4 | -.178 2 | +.041 0 | -.178 0 |
| 1 | 0 | 2 | -2 | +.0.976 9 | -.0.007 5 | +.0.976 8 | -.006 6 | | -.006 4 |
| 2 | 0 | 2 | -2 | +.0.109 0 | | +.0.109 0 | | | |
| 1 | 1 | 2 | -2 | -.0006 4 | 0.000 0 | -.0006 0 | | | |
| -1 | -1 | 2 | -2 | +.0009 5 | -.0014 7 | +.0009 6 | | | |
| 1 | -1 | 2 | -2 | +.0008 8 | 0.000 0 | +.0008 4 | | | |
| 0 | 0 | 0 | 2 | | | | +.195 0 | -.035 4 | -.195 2 |

PART IV.
DERIVATION OF RESULTS.

CHAPTER VII.

CONSTANT AND SECULAR TERMS.

We recall the arrangement of the present work. In Part I, the general equations have been formed, the theory outlined, and the methods developed so far as could be done. Nearly all the fundamental quantities were developed as sums of products of two factors, one factor of each pair being a function of the Moon's coördinates, the other a function of the coördinates of the planets. The latter functions are developed in detail in Part II, one chapter of which is devoted to the developments of the coefficients of the direct action, the other to the coefficients of the indirect action. In Part III, Chapter VI, have been developed the numerical functions for the lunar coefficients. These are the same for both actions. The present concluding Part is devoted to the combination of these factors and the derivation and discussion of results.

We may divide the matter of this part into three chapters. In the first chapter we consider the terms not purely periodic. By a purely periodic term is meant one of which the coefficient of the sine or cosine is constant. We may, therefore, define the terms to be first considered as constant and secular, two classes which need not be considered separately.

§ 54. The arguments on which the planetary and lunar factors depend are all distinct except g' , which is common to both. It follows that no constant or secular term in the variations of the elements can arise by the multiplication of factors depending on any other variable argument than g' . In all cases in which another argument than this enters into either factor, the results will be periodic in form, the coefficient, however, having, in the general case, a secular variation. Since no terms of the class in question contain l , π , or θ , they give

$$D\alpha = 0 \quad D\epsilon = 0 \quad D\gamma = 0$$

To form the constant and secular terms we begin by collecting those planetary factors which are either constant or depend on the argument g' . We shall consider the direct and indirect actions separately. The planetary factors for the direct action, as collected from § 42, with some revision of the numbers there found, are shown on the next page.

FACTORS FOR DIRECT ACTION.

Action of Venus.

$$\begin{aligned} 10^3 MK &= + 5'' .9045 + 0'' .44 \cos g' - 0'' .11 \sin g' \\ \frac{1}{2} 10^3 MC &= - 3 .4072 - 0 .30 \cos g' + 0 .07 \sin g' \\ 10^3 MD &= + 0'' .33 \sin g' + 0'' .03 \cos g' \end{aligned}$$

Action of Mars.

$$\begin{aligned} 10^3 MK &= + 0'' .0468 - 0'' .020 \cos g' - 0'' .024 \sin g' \\ \frac{1}{2} 10^3 MC &= - 0 .1006 + 0 .028 \cos g' + 0 .029 \sin g' \\ 10^3 MD &= + 0'' .010 \sin g' - 0'' .008 \cos g' \end{aligned} \quad (18)$$

Action of Jupiter.

$$\begin{aligned} 10^3 MK &= + 0'' .0913 - 0'' .002 \cos g' - 0'' .032 \sin g' \\ \frac{1}{2} 10^3 MC &= - 2 .1348 + 0 .004 \cos g' + 0 .062 \sin g' \\ 10^3 MD &= + 0'' .005 \sin g' - 0'' .030 \cos g' \end{aligned}$$

Action of Saturn.

$$10^3 MK = + 0'' .0013 \quad \frac{1}{2} 10^3 MC = - 0'' .1040 \quad 10^3 MD = 0$$

The corresponding factors for the indirect action have been combined for the five disturbing planets, Venus to Uranus. From the combined values of G , J , and I , reached in § 44, we find, including Uranus, but omitting Mercury:

$$\begin{aligned} 10^3 m^2 G &= + 0'' .459 + 0'' .36 \cos g' + 0'' .06 \sin g' \\ 10^3 m^2 J &= + 0 .153 + 0 .12 \cos g' + 0 .02 \sin g' \\ 10^3 m^2 I &= - 0 .03 \sin g' \end{aligned}$$

§ 55. *Lunar Factors.* If, for brevity, we put F for any one of the three lunar factors, say

$$F = \xi^2 - \eta^2 \quad F' = \rho^2 - 3\xi^2 \quad F'' = 2\xi\eta \quad (19)$$

the terms of the fundamental equations (42) or (57) corresponding to each F will be:

$$\text{in } -D_n l_0; \quad \alpha_1 D' F + e_1 \frac{\partial F}{\partial e} + \gamma_1 \frac{\partial F}{\partial \gamma} \equiv F_1$$

$$\text{in } -D_n \pi_0; \quad \alpha_2 D' F + e_2 \frac{\partial F}{\partial e} + \gamma_2 \frac{\partial F}{\partial \gamma} \equiv F_2$$

$$\text{in } -D_n \theta_0; \quad \alpha_3 D' F + e_3 \frac{\partial F}{\partial e} + \gamma_3 \frac{\partial F}{\partial \gamma} \equiv F_3$$

From the tabular values of the functions of the coördinates and their derivatives in Table XL, p. 112, noting that symbolically, $D' = D + 2$, we have the following values of the terms of these functions which are independent of the lunar arguments

$$\begin{aligned} F &= \xi^2 - \eta^2 = - .013 \ 96 - .000 \ 933 \cos g' - .000 \ 06 \cos 2g' \\ F' &= \rho^2 - 3\xi^2 = .990 \ 74 + .000 \ 264 \cos g' \\ F'' &= 2\xi\eta = - .001 \ 123 \sin g' - .000 \ 06 \sin 2g' \end{aligned}$$

$$\begin{aligned}
 D'F &= D'(\xi^2 - \eta^2) = -.080\ 02 - .005\ 288 \cos g' - .000\ 38 \cos 2g' \\
 D'F' &= D'(\rho^2 - 3\xi^2) = 1.9770 + .001\ 239 \cos g' + .000\ 04 \cos 2g' \\
 D'F'' &= 2D'\xi\eta = -.006\ 809 \sin g' - .000\ 39 \sin 2g' \\
 \frac{\partial F}{\partial e} &= \frac{\partial(\xi^2 - \eta^2)}{\partial e} = +.1108 + .004\ 519 \cos g' \\
 \frac{\partial F'}{\partial e} &= \frac{\partial(\rho^2 - 3\xi^2)}{\partial e} = +.1705 + .001\ 109 \cos g' \\
 \frac{\partial F''}{\partial e} &= \frac{2\partial\xi\eta}{\partial e} = +.006\ 220 \sin g' \\
 \frac{\partial F}{\partial \gamma} &= \frac{\partial(\xi^2 - \eta^2)}{\partial \gamma} = +.0154 + .000\ 287 \cos g' \\
 \frac{\partial F'}{\partial \gamma} &= \frac{2(\rho^2 - 3\xi^2)}{\partial \gamma} = -.5375 - .000\ 161 \cos g' \\
 \frac{\partial F''}{\partial \gamma} &= \frac{2\partial\xi\eta}{\partial \gamma} = +.000\ 469 \sin g'
 \end{aligned}$$

The factors a_i, e_i , etc., are derived in § 14, and found in (26). From the preceding scheme we find by using the preceding values and their derivatives in (20)

$$\begin{aligned}
 F_1 &= -0.1641 - .010\ 92 \cos g' - .000\ 77 \cos 2g' \\
 F_2 &= -2.1194 - .086\ 40 \cos g' + .000\ 01 \cos 2g' \\
 F_3 &= -0.0859 - .001\ 63 \cos g' \\
 F'_1 &= +4.0086 + .002\ 49 \cos g' + .000\ 08 \cos 2g' \\
 F'_2 &= -3.3142 - .021\ 36 \cos g' \\
 F'_3 &= +3.0093 - .000\ 90 \cos g' \\
 F''_1 &= -.013\ 89 \sin g' - .000\ 79 \sin 2g' \\
 F''_2 &= -.118\ 94 \sin g' + .000\ 01 \sin 2g' \\
 F''_3 &= -.002\ 64 \sin g'
 \end{aligned} \tag{20}$$

§ 56. *Secular motions of l, π , and θ .* The function MH , as defined in § 20, may now be written

$$MH = MKF - \frac{1}{2}MC_1F' + MD_1F''$$

and introducing the linear functions of its derivatives which we have just formed we have from (42)

$$\begin{aligned}
 D_n l_0 &= -MKF_1 + \frac{1}{2}MC_1F'_1 - MDF''_1 \\
 D_n \pi_0 &= -MKF_2 + \frac{1}{2}MCF'_2 - MDF''_2 \\
 D_n \theta_0 &= -MKF_3 + \frac{1}{2}MCF'_3 - MDF''_3
 \end{aligned} \tag{21}$$

of all which factors we have just given the numerical values. For the indirect action the second members are

$$m^2GF_i + m^2JF'_i - m^2IF''_i \dots (i = 1, 2, 3) \tag{22}$$

Performing the multiplications we find the following secular motions of l_0 , π_0 , and θ_0 arising from the terms of direct and indirect action under consideration.

| Direct Action of | $10^3 D_n l_0$ | $10^3 D_n \pi_0$ | $10^3 D_n \theta_0$ |
|------------------|----------------|------------------|---------------------|
| Venus | - 12.66 | + 23.846 | - 9.747 |
| Mars | - 0.41 | + 0.433 | - 0.300 |
| Jupiter | - 8.54 | + 7.269 | - 6.416 |
| Saturn | - 0.42 | + 0.346 | - 0.318 |
| Uranus | - 0.01 | + 0.007 | - 0.006 |
| Sum | - 22.04 | + 31.901 | - 16.786 |
| Indirect | + 0.54 | - 1.495 | + 0.422 |
| Total | - 21.50 | + 30.406 | - 16.364 |

Taking the Julian century as unit of time $n = 8400$. The centennial motions arising from the factors here employed are therefore:

$$\text{Centennial motion of } l_0 = -180''.6, \text{ of } \pi_0 = +255.41, \text{ of } \theta_0 = -137.46. \quad (23)$$

From the vanishing of $D_i a$, $D_i e$, and $D_i \gamma$ we have

$$\delta n = \text{const.} \quad \delta \pi_1 = \text{const.} \quad \delta \theta_1 = \text{const.}$$

the constants being functions of the arbitrary constants of integration, determined at the end of this chapter.

§ 57. *Terms arising from the secular variation of the earth's eccentricity.*

Both the direct and indirect actions contain, in rigor, terms of this class. They enter into the direct action because the direct action of the planet on the Moon varies with the variation of the orbit of the earth around the Sun. But the effect of this variation is found to be so slight that it will be left out of consideration in the present work. We therefore begin with the indirect action. The terms of the coefficients G , I , and J , on which the action depends, have been developed in Chapter V, § 44.

Our fundamental quantity for the indirect action is H' of § 25, of which the only terms required are

$$H' = -G(\xi^2 - \eta^2) - J(\rho^2 - 3\zeta^2) + 2I\xi\eta = -GF - JF' + IF'' \quad (24)$$

The terms of G , I , and J required for the present purpose are

$$G = G_1 \Delta e' \quad I = I_1 \Delta e' \quad J = J_1 \Delta e'$$

G_1 , I_1 , and J_1 being found in § 44 and

$$\Delta e' = -8''.595 T - 0''.0260 T^2 = -8''.595 T(1 + .00302 T)$$

The secular terms of these coefficients thus become

$$\begin{aligned} G &= (-0''.5358 + 19''.29 \cos g' + 1''.83 \cos 2g') T(1 + .00302 T) \\ J &= (+0''.1080 + 6''.44 \cos g' + 0''.32 \cos 2g') T(1 + .00302 T) \\ I &= (-25''.45 \sin g' - 1''.84 \sin 2g') T(1 + .00302 T) \end{aligned} \quad (25)$$

Using these values in (56) we find

$$D_n \alpha = D_n e = D_n \gamma = 0$$

If we put G' , J' , and I' for the coefficients of T in (25) we shall have from (20) and (22) the following computation for the secular accelerations from the fundamental equations (57), in which only the non-periodic terms are to be used :

$$\begin{aligned} [l] &= G'F_1 + J'F_1' - I'F_1'' = + 0''.2467 \\ [\pi] &= G'F_2 + J'F_2' - I'F_2'' = - 1.6378 \\ [\theta] &= G'F_3 + J'F_3' - I'F_3'' = + 0.3246 \end{aligned}$$

Then, postponing the terms in T^2

$$D_n l = m^2[l] T \quad D_n \pi = m^2[\pi] T \quad D_n \theta = m^2[\theta] T \quad (26)$$

The terms in T^2 in (25) are only those arising from the term of e' in T^2 . To find the complete values we note that all the terms of $[l]$, $[\pi]$, and $[\theta]$ contain e' as a factor, and may therefore be expressed in the form $e'k$, k being a quantity which, though containing minute terms in e'^2 , may be regarded as a constant. Then

$$D_t[l] = kD_t e' = [l] \frac{D_t e'}{e'} = - .002495[l]$$

and the actual values of $[l]$, $[\pi]$, and $[\theta]$ may be written in the form

$$[l] = [l]_0(1 - .00250 T)(1 + .00302 T) = [l]_0(1 + .00052 T)$$

$[l]_0$, etc., being the values computed above. Multiplying by T we find that the terms of $D_t l$, $D_t \pi$, and $D_t \theta$ in T^2 are found from those in T by multiplying the latter by the factor $+ .00052 T$.

Taking the Julian century as the unit of time, $m^2 n = 46.998$, whence

$$D_t l = + 11''.60 T + 0''.0060 T^2 \quad D_t \pi = - 76''.98 T - 0''.040 T^2 \quad D_t \theta = + 15.25 T + 0.0079 T^2$$

Then by integration

$$\delta l = 5''.80 T^2 + 0''.0020 T^3 \quad \delta \pi = - 38''.49 T^2 - 0''.013 T^3 \quad \delta \theta = 7''.62 T^2 + 0''.0026 T^3 \quad (27)$$

This value of the secular acceleration of the mean longitude is, I believe, markedly smaller than any heretofore found. Delaunay's last result was $6''.11$, which, reduced to the now adopted value of the secular diminution of e' , would become $6''.02$. The necessity of using Delaunay's development of the parallax in forming the D 's of some of the coefficients leads to some uncertainty in the present result. But my rough estimate would lead to the conclusion that the uncertainty should be less than one per cent. of the whole amount. The question of the precision of the value here reached I must leave to other investigators.*

* As this work is going through the press the author notices that Brown's value found in *Monthly Notices Royal Astronomical Society*, vol. LVII, is reduced from $5''.91$ to $5''.81$ when the now adopted $D_t e'$ is used.

§ 58. We have next to consider the secular variations of the periodic terms in general. Taking any set of such terms depending on any argument N

$$\zeta^2 - \eta^2 = 2p \cos N \quad \rho^2 - 3\zeta^2 = 2q \cos N \quad 2\xi\eta = \kappa_4 \sin N$$

we shall have the terms of H' in (24)

$$\begin{aligned} H' &= (1''.072p - 0''.216q) T \cos N + (-38''.6p - 12''.9q) T \cos g' \cos N - 25''.4\kappa_4 T \sin g' \sin N \\ &= (1''.072p - 0''.216q) T \cos N - (19''.3p + 6''.4q + 12''.7\kappa_4) T \cos(N - g') \\ &\quad - (19''.3p + 6''.4q - 12''.7\kappa_4) T \cos(N + g') \end{aligned}$$

Forming the partial derivatives of these terms of H' as to l , π , θ , a , e , and γ , and carrying them into the fundamental equations (64) and (65) by the processes of § § 22 and 23 we shall be led to

$$\begin{aligned} D_{nt} a &= m^2(-1''.072ap + 0''.216aq) T \sin N + m^2(19''.3ap + 6''.4aq + 12''.7a\kappa_4) T \sin(N - g') \\ &\quad + m^2(19''.3ap + 6''.4aq - 12''.7a\kappa_4) T \sin(N + g') \end{aligned} \quad (28)$$

with similar equations for e and γ formed by writing e and g respectively for a . Also, we shall have

$$\begin{aligned} D_{nt} l_0 &= m^2(1''.072L' - 0''.216L'') T \cos N^2 - m^2(19''.3L' + 6''.4L'' + 12''.7L_4) T \cos(N - g') \\ &\quad - m^2(19''.3L' + 6''.4L'' - 12''.7L_4) T \cos(N + g') \end{aligned} \quad (29)$$

with similar equations for $D_{nt} \pi_0$ and $D_{nt} \theta_0$ formed by writing P and R respectively for L

§ 59. The special values of N of most importance in the present connection are

$$N = 0 \quad N = g' \quad N = g$$

on which depend, respectively, the constant term, the annual equation, the equation of the center, and the evection

CASE I; $N = 0$.

The factors for $D_{nt} a$, $D_{nt} e$, and $D_{nt} \gamma$ all vanish. The values of the L -coefficients are found in the first line of Table XLIX, p. 147. The first or purely secular term of (29) has already been computed. The remaining terms give

$$\begin{aligned} D_{nt} l_0 &= m^2 n (38''.6L' + 12''.9L'') T \cos g' \\ D_{nt} \pi_0 &= m^2 n (38''.6P' + 12''.9P'') T \cos g' \\ D_{nt} \theta_0 &= m^2 n (38''.6R' + 12''.9R'') T \cos g' \end{aligned}$$

Substituting the numerical values of L , P , R , and $m^2 n = 47.00$;

$$D_{nt} l_0 = +1062'' T \cos g' \quad D_{nt} \pi_0 = -2961'' T \cos g' \quad D_{nt} \theta_0 = +827'' T \cos g'$$

We cite, for convenient reference, the following indefinite integrals

$$\int t \sin Nt dt = \frac{t}{N^2} \sin Nt - \frac{t}{N} \cos Nt \quad \int t \cos Nt dt = \frac{t}{N^2} \cos Nt + \frac{t}{N} \sin Nt$$

The unit of t in these equations being 100 years, N is the motion of g' in this period, for which we may take 200π , or $N = 628$.

Integration by the above formulæ then gives

$$\begin{aligned} \delta l_0 &= + 1''.69 T \sin g' + 0''.003 \cos g' \\ \delta \pi_0 &= - 4.71 T \sin g' - .008 \cos g' \\ \delta \theta_0 &= + 1.32 T \sin g' + .002 \cos g' \end{aligned} \quad (30)$$

CASE II; $N = g'$; *the annual term.*

Here also the variations of α , e , and γ vanish, so that only those of l_0 , π_0 , and θ_0 are affected. Carrying into the equations (29) the numerical values of the lunar coefficients for the Arg. g' we find, dropping the constant terms, which have been already computed,

$$\begin{aligned} D_l l_0 &= m^2 n T (0''.0061 \cos g' - 0''.082 \cos 2g') = 0''.29 T \cos g' - 3''.80 T \cos 2g' \\ D_\pi \pi_0 &= m^2 n T (0.0485 \cos g' + 0.131 \cos 2g') = 2.28 T \cos g' + 3.44 T \cos 2g' \\ D_\theta \theta_0 &= m^2 n T (0''.0010 \cos g' + 0''.022 \cos 2g') = 0''.47 T \cos g' + 1.03 T \cos 2g' \end{aligned}$$

Then, integrating, and dropping insignificant constant coefficients

$$\begin{aligned} \delta l_0 &= + 0''.00047 T \sin g' - 0''.0036 T \sin 2g' \\ \delta \pi_0 &= + 0.0037 T \sin g' - 0.0028 T \sin 2g' \\ \delta \theta_0 &= + 0.0008 T \sin g' - 0.0016 T \sin 2g' \end{aligned}$$

CASE III; $N = g$.

For this argument I have used the following preliminary values of the lunar coefficients, differing from those of Tables XLVIII and XLIX by amounts here unimportant

| | | |
|-------------------|-------------------|--------------------------|
| $L' = - 0.1197$ | $L'' = - 0.1962$ | $L_4 = - 0.2648$ |
| $P' = + 5.403$ | $P'' = + 18.734$ | $P_4 = + 11.688$ |
| $R' = - 0.0028$ | $R'' = - 0.1431$ | $R_4 = - 0.0560$ |
| $ap = - 0.032 23$ | $aq = - 0.110 49$ | $a\kappa_4 = - 0.069 70$ |
| $ep = - 0.300 45$ | $eq = - 1.033 40$ | $e\kappa_4 = - 0.650 66$ |
| $gp = + 0.000 09$ | $gq = + 0.000 31$ | $g\kappa_4 = + 0.000 10$ |

Carrying these values into the equations (28) and (29) we find, for the terms depending on the argument g alone,

$$\begin{aligned} D_\alpha \alpha &= + 0''.520 T \sin g & D_e e &= + 4''.70 T \sin g \\ D_l l_0 &= + 4''.04 T \cos g & D_\pi \pi_0 &= - 82''.2 T \cos g \end{aligned}$$

For the motion of g , $N = 8329$.

Integration then gives

$$\begin{aligned} \delta \alpha &= - 0''.000 062 T \cos g + (74'' \div 10^{10}) \sin g & \delta e &= - 0''.0056 T \cos g \\ \delta l_0 &= + 0''.000 485 T \sin g & \delta \pi_0 &= - 0''.009 87 T \sin g \end{aligned}$$

We drop the terms with constant coefficients, owing to their minuteness, and find, with $n=8400$;

$$\delta n = -\frac{3}{8}n\delta\alpha = +0''.78 T \cos g$$

Then by integration

$$\delta_n l = \int \delta n dt = +0''.000\ 094 T \sin g$$

This, added to δl_0 , gives for the entire term in δl

$$\delta l = +0''.000\ 578 T \sin g \quad (31)$$

§ 60. In order to determine the complete expressions for the coördinates themselves, the terms computed in the present section, together with those which may be found in a similar way for the other periodic terms, are to be carried into the expression for the Moon's true longitude in terms of the elements. I have not, however, deemed it necessary to do this in the case of the secular variations of the periodic terms, because these can be most readily determined by varying the value of e' in the Delaunay or Brown expressions for the Moon's longitude.

I have, however, computed the preceding variations of some terms owing to the theoretical interest which attaches to the relations implied by the equality of the result of the present method to those of the other method. The two methods correspond to the two methods by which the secular acceleration may be determined. In *Action*, p. 191, it is shown that the secular acceleration of l , π , and θ may be derived from the secular change of e' by determining the corresponding secular changes in α , e , and γ . This theorem has been discussed and extended by Brown in his paper on *Transmitted Motions and Indirect Perturbations*.*

By this method the secular variations in question appear as variations of n , π_1 , and θ_1 , the latter being functions of the variables α , e , and γ . But, in the present theory, α , e , and γ remain constant so far as the secular change of e' is concerned, and the changes are thrown wholly upon l_0 , π_0 , and θ_0 .

There is therefore a seeming contradiction in that the lunar elements α , e , and γ are affected by a secular variation in one theory, while in the other they are practically constant. Referring to Brown's paper for the theory of the subject it will be instructive to show the relation between the two methods.

In what I have, for brevity, called the Delaunay solution of the problem, the Moon's coördinates appear as functions of the lunar elements, introduced as arbitrary constants, and of the Sun's eccentricity, which is regarded as a quantity given in advance. But, when the action of the planets is introduced, the solar element e' , as well as the lunar elements α , e , and γ , become variable. In what I may call method *A* of treating the planetary action, which was that adopted in *Action*, the final values of the coördinates as affected by planetary action are determined by introducing the simultaneous variations of all four elements into the Delaunay

* *Transactions of the American Mathematical Society*, vol. VI, p. 332. See also, *Monthly Notices, Royal Astronomical Society*, vol. LVII.

expressions. But in method *B*, adopted in the present work, the entire variations have been thrown upon the lunar elements, the solar elements being regarded as constant. In the case of the periodic perturbations this course is practically a necessity, owing to the extreme complexity introduced into the formulæ if we suppose the coördinates expressed in terms of the value of e' affected by periodic inequalities. But it is different in the case of the secular motion of e' . Here it is more logical to consider that at any epoch the action of the Sun is computed with the actual eccentricity at that epoch, and so to use method *A*.

Not having done this in the present work, but having regarded the value of e' at the epoch 1850 as a fundamental constant, the values of G , J , and I , though functions of e' , and therefore variable, have appeared in the theory as constants.

In the present investigation the author has not, for want of time, investigated the modifications which would be made in the problem if these coefficients were taken as affected by their secular variations. One reason for refraining from this course was that the determination of the secular acceleration from the equations given in *Action*, page 191, require a much more extended development of the canonical elements in terms of e' than it was practicable to undertake in the present paper. The question is therefore left to others, reference being made to Brown's paper on the variation of given and arbitrary constants.*

A comparison of the secular variation of the coefficient of $\sin g'$ with that found by Delaunay's value of this term will, however, be of interest. With the eccentricity of 1850 the coefficient of this annual term is $-670''$. It contains e' as a factor, the portion arising from higher powers of this element being unimportant in the present case. It follows that the secular variation of the coefficient of $\sin g'$ in δv is

$$-670'' \frac{\delta e'}{e'} = +1''.67 T$$

The term found in (30) for δl is $1''.69 T$. I have not computed δv itself.

The two methods of treating the effect of the motion of the ecliptic are related to each other in the same way as this just discussed. Had the method of the present paper been strictly followed throughout, the coördinates of the Moon would have been referred to a fixed ecliptic, because the ecliptic remains fixed when planetary action is omitted. But it was seen that by a very slight and easily determined change, the coördinates could be referred to the actually moving ecliptic, and and the work was carried on accordingly. In concluding the work, it is a matter of regret to the author that he did not investigate the question whether the Moon's coördinates could not, on the same principle, be expressed in terms of a varying solar eccentricity, *ab initio*, thus simplifying the problem in conception at least. Owing, however, to the theoretical interest attaching to the relation between the two methods, the effect of the motion of the ecliptic might be treated by both methods.

* *L. c.*, vol. IV, p. 333.

§ 61. *Adjustment of the Arbitrary Constants.* The problem before us may be outlined thus. The preliminary solution of the problem of three bodies leads to expression of the Moon's coördinates as functions of six arbitrary constants, through the intermediary of three other functions of these constants l , π , and θ . The solution in terms of the six elements a , e , γ , l , π , θ takes the form:

$$l = l_0 + nt \quad \pi = \pi_0 + \pi_1 t \quad \theta = \theta_0 + \theta_1 t \quad v = l + \phi \quad \rho = 1 + \phi \quad \beta = \phi$$

the functions ϕ being of a form not necessary to specify at present. As already mentioned, n , π_1 , and θ_1 are functions of a (or n), e , and γ . The solution of our problem is now completed by adding to the expressions for the Moon's coördinates $\equiv v$, r , and β , the quantities

$$\delta v = \frac{\partial v}{\partial a} \delta a + \frac{\partial v}{\partial l} \delta l + \frac{\partial v}{\partial e} \delta e + \frac{\partial v}{\partial \pi} \delta \pi + \dots \quad (32)$$

with similar forms for r and β , which we need not write. For our present purpose it will be necessary and sufficient to consider the following terms in v , the true longitude.

$$v = l + 2e \sin(l - \pi)$$

We then have

$$\begin{aligned} \frac{\partial v}{\partial l} &= \frac{\partial v}{\partial l_0} = 1 + 2e \cos g & \frac{\partial v}{\partial \pi} &= -2e \cos g \\ \frac{\partial v}{\partial e} &= 2 \sin g + \frac{\partial v}{\partial \pi} \frac{\partial \pi}{\partial e} & \frac{\partial v}{\partial a} &= \frac{\partial v}{\partial l} \frac{\partial l}{\partial a} + \frac{\partial v}{\partial \pi} \frac{\partial \pi}{\partial a} \end{aligned}$$

Substituting in (32) and omitting unimportant terms

$$\delta v = -\frac{3}{2}nt(1 + 2e \cos g)\delta a - 2e \cos g \delta \pi + (1 + 2e \cos g)\delta l_0 + 2 \sin g \delta e$$

We put

$$\delta \alpha_0, \delta e_0, \delta \pi_0, \delta l_0,$$

the arbitrary constants to be added to the perturbations δa , δe , $\delta \pi$, and δl . We then have the following perturbations depending on the purely lunar arguments

$$\begin{aligned} \delta a &= \delta \alpha_0 - 0''.0016 \sin g & \delta e &= \delta e_0 - 0''.0150 \cos g \\ \delta l &= \delta l_0 - 0''.0212nt + 0''.0059 \sin g & \delta \pi &= \delta \pi_0 + 0''.0315nt - 0''.272 \sin g \end{aligned}$$

Substituting in the derivatives we have the result that the mean sidereal motion of the Moon is

$$nt(1 - 0''.0212 - \frac{3}{2}\delta_0 a)$$

We now determine $\delta_0 a$ by the condition that the mean motion shall be represented by n . Thus

$$\delta_0 a = -0''.0141 \quad \delta_0 n = 0''.0212n = +178'' \quad (33)$$

Also, the coefficient of $\sin g$ in the expression for the longitude becomes

$$2e + 0''.0059 + 2\delta_0 e$$

We now determine $\delta_0 e$ by the condition that the expression for the coefficient shall remain unchanged. This gives

$$\delta_0 e = -0''.003$$

The longitudes, perigee, and node being given by the equations

$$\pi = \pi_0 + \pi_1 t \quad \theta = \theta_0 + \theta_1 t$$

the introduction of the perturbations of the elements will give rise to the increments

$$\delta\pi_1 = \frac{\partial\pi_1}{\partial n} \delta n + \frac{\partial\pi_1}{\partial e} \delta e + \frac{\partial\pi_1}{\partial \gamma} \delta \gamma \quad \delta\theta_1 = \frac{\partial\theta_1}{\partial n} \delta n + \frac{\partial\theta_1}{\partial e} \delta e + \frac{\partial\theta_1}{\partial \gamma} \delta \gamma$$

The effects $\delta_0 e$ and $\delta_0 \gamma$ are inappreciable. Taking only $\delta_0 n$ from (33) we have

$$\delta\pi_1 = -0.014 \ 80 \delta_0 n = -0''.000 \ 314 n \quad \delta\theta_1 = -0.001 \ 01 \delta_0 n = -''.000 \ 021 n$$

Taking the century as the unit, the adjustment gives

$$\delta\pi_1 = -2''.64 \quad \delta\theta_1 = -0''.18 \quad \text{and} \quad \delta\pi = -2''.64 T \quad \delta\theta = -0''.18 T$$

Adding thereto the secular terms of π_0 and θ_0 already found, we have the following results, for the entire secular effect of the action of the planets on π and θ

| | $D\pi$ | $D\theta$ |
|--|------------|------------|
| Direct action of the planets Venus to Uranus | + 267''.97 | - 141''.00 |
| Indirect action of the planets Venus to Uranus | - 12 .56 | + 3 .54 |
| Total action of Mercury ($m = 10^{-1}$) | + 0 .45 | - 0 .21 |
| Adjustment of elements | - 2 .64 | - 0 .18 |
| Sum | + 253 .22 | - 137 .85 |

This motion of the perigee, greater by 5'' than that found by Brown, goes to confirm his conclusion that the gravitation of the Earth does not deviate from Newton's law of the inverse square.

§ 62. As the reason for the last correction may not be quite clear, it may be of interest to state in a general way how it enters into the theory. The action of the planets on the Moon is found on the supposition of what we may call an undisturbed orbit of the Moon, meaning thereby an orbit in which the action of the Sun is completely taken account of, on the supposition that no other extraneous action enters. We thus have a certain mean motion n determined from observations, and a certain undisturbed mean distance, a , determined by the relation $a^3 n^2 = \mu$, which requires a constant Δa of correction to the mean distance computed from the action of the Sun, giving rise to an expression for the constant of the Moon's radius vector $a + \Delta a_1 \equiv a_1$ completely representing the action of the Sun on the supposition of no planetary action.

It is with this mean distance a_1 that the actions of the planets, both direct and indirect, are computed. But, as a matter of fact, the action of the planet modifies the relation between a_1 and n , so that we must change either the mean motion or the mean distance according to what values of the elements we assume. If we take the arbitrary constants so that the mean motion remains unchanged, then the actual mean distance will require a constant correction on account of the action of the planets. If we regard the mean distance as an invariable quantity, then there will be a correction to the mean motion.

It follows by either method that when we compute the motion of the perigee and node under the action of the Sun alone, we must make one or the other of these modifications produced by the action of the planet, and determine the effect upon the motion of π and θ . If we regard the actually observed mean motion as that due to the Sun alone then we must introduce a correction to the mean distance, and determine its effect upon π_1 and θ_1 . But if, which is the more natural method, we regard the mean distance of the Moon as the given actual element, then we must compute that part of the motion of the perigee and node due to the Sun alone with a different n from that given by observation; that is, with a value found by subtracting the planetary effect from the observed value.

We may therefore regard the corrections $-2''.64$ and $-0''.18$ to π_1 and θ_1 as reducing π_1 and θ_1 to their true values under the action of the Sun alone.

§ 63. *Secular Variation of e .* If we require, as we should, that the coefficient of $\sin g$ in the Moon's true longitude should be represented by a function of e then the expression (31) shows that this element will be affected by the secular variation

$$\delta e = +0''.00029T$$

This being less than $0''.01$ in a thousand years, is of no practical importance, though of theoretical interest.

It may also be remarked in the present connection that the existence of this variation, and the approximate algebraic expression for its amount, was first made known by Adams.*

* *Monthly Notices, Royal Astronomical Society*, vol. XIX, p. 207.

CHAPTER VIII.

SPECIAL PERIODIC INEQUALITIES.

§ 64. *Reduction to the moving ecliptic.* Since when the Sun is the disturbing body the plane of the ecliptic remains fixed, the inequalities of the coördinates so far reached are referred to the ecliptic of any date regarded as fixed. The only way in which they are affected by the motion of the ecliptic is through the secular variations of the coördinates of the planet arising from that motion. The effects of these are supposed to be too small to need consideration at present. It is, however, necessary to refer the elements to the moving ecliptic. I have shown in § 4 how this may be done by the simple device of adding to the perturbative function the terms

$$\Delta R = 2z(pD_x x_1 - qD_y y_1) + 2(qy - px)D_z z_1 \quad (33)$$

and then integrating the portions of the differential equations thus arising. In this expression p and q are the coefficients expressing the speed of rotation of the ecliptic around the axes of y and x respectively, and are found by putting

Π , the longitude of the ascending node of the moving on the fixed ecliptic;
 κ , the speed of rotation.

Then

$$p = \kappa \sin \Pi \quad q = \kappa \cos \Pi \quad (34)$$

It is to be noted that κ is here used as the speed of rotation, and not as the actual angle rotated through. It is, therefore, of dimension T^{-1} and the expression for ΔR is of dimensions $L^2 T^{-2}$, which, by introducing the dimensions of mass, become identical with the dimensions of P as hitherto used.

The partial derivatives of ΔR as to the lunar elements are to be taken only as they enter through x , y , and z , so that the D_i of the Moon's coördinates, the latter being called for this purpose x_1 , y_1 , and z_1 , are to be regarded as numerically given quantities.

To form the partial derivatives of x , y , and z we use the developments of these coördinates in terms of the lunar elements already given, substituting in x , y , and z the values of ξ , η , and ζ . But in this part of the work it will be convenient to refer the coördinates x and y to a general fixed X-axis, instead of the mean Sun, as heretofore. When this is done the expressions for the ratios of the coördinates to a take the form

$$\xi = \Sigma k \cos N \quad \eta = \Sigma k \sin N \quad \zeta = \Sigma c \sin N' \quad (35)$$

where N and N' are of the general form

$$N = il + i_1\pi + i_2\theta + j'l' + j_1\pi' \quad N' = i'l + i_1'\pi + i_2'\theta + j'l' + j_1'\pi'$$

the indices satisfying the conditions

$$i + i_1 + i_2 + j + j_1 = 0 \quad i' + i_1' + i_2' + j' + j_1' = 1$$

In forming the D_i 's of these expressions we put n, n' , the *ratios* of the motion of the arguments N or N' to n , that of the Moon. We then have

$$D_x z_1 = -an\Sigma kn \sin N \quad D_y z_1 = an\Sigma kn \cos N \quad D_z z_1 = an\Sigma cn' \cos N'$$

The values (34) of p and q then give

$$pD_x z_1 - qD_y z_1 = -an\kappa\Sigma kn \cos(N - \Pi) \quad (36)$$

$$qy - px = a\kappa\Sigma k \sin(N - \Pi) \quad (37)$$

Our next step is to form the derivatives of z and $qy - px$ as to the lunar elements. The partial derivatives as to z are found from the last equation (35)

$$Dz = a\Sigma D'c \sin N' \quad \frac{\partial z}{\partial e} = a\Sigma \frac{\partial c}{\partial e} \sin N' \quad \frac{\partial z}{\partial \gamma} = a\Sigma \frac{\partial c}{\partial \gamma} \sin N' \quad (38)$$

$$\frac{\partial z}{\partial l} = a\Sigma i'c \cos N' \quad \frac{\partial z}{\partial \pi} = a\Sigma i_1'c \cos N' \quad \frac{\partial z}{\partial \theta} = a\Sigma i_2'c \cos N' \quad (39)$$

By differentiating (37) on the same system we have

$$D(qy - px) = a\kappa\Sigma D'k \sin(N - \Pi) \\ \frac{\partial(qy - px)}{\partial e} = a\kappa\Sigma \frac{\partial k}{\partial e} \sin(N - \Pi) \quad (40)$$

$$\frac{\partial(qy - px)}{\partial \gamma} = a\kappa\Sigma \frac{\partial k}{\partial \gamma} \sin(N - \Pi)$$

$$\frac{\partial(qy - px)}{\partial l} = a\kappa\Sigma i k \cos(N - \Pi)$$

$$\frac{\partial(qy - px)}{\partial \pi} = a\kappa\Sigma i_1 k \cos(N - \Pi) \quad (41)$$

$$\frac{\partial(qy - px)}{\partial \theta} = a\kappa\Sigma i_2 k \cos(N - \Pi)$$

We next have to form the products of (36) by the derivatives (38) and (39) and of $D_z z_1$ by (40) and (41), and form their several sums. We thus find that the

combination of any term of argument N with any term of argument N' gives rise to the following terms in the partial derivatives as to e and l :

$$\frac{\partial \Delta R}{\partial e} = a^2 n \kappa \left\{ n' c \frac{\partial k}{\partial e} - n k \frac{\partial c}{\partial e} \right\} \sin(N + N' - \Pi) + a^2 n \kappa \left\{ n' c \frac{\partial k}{\partial e} + n k \frac{\partial c}{\partial e} \right\} \sin(N - N' - \Pi)$$

$$\frac{\partial \Delta R}{\partial l} = a^2 n \kappa c k \{ i n' - i' n \} \{ \cos(N + N' - \Pi) + \cos(N - N' - \Pi) \} \quad (42)$$

The derivatives as to $\log a$ and γ are formed from the first of these equations by simple substitution. Those as to π and θ are formed from the last equation by writing i_1 and i_2 for i , and i'_1 and i'_2 for i' .

The derivatives thus formed being substituted in the fundamental equations the integration of the latter will give the inequalities of the elements. It will be convenient to use the following formulæ of substitution. We first put, in the combination of any term of argument N with any term of argument N' :

$$k_a = n' c D' k + n k D' c \quad k'_a = n' c D' k - n k D' c$$

$$k_e = n' c \frac{\partial k}{\partial e} + n k \frac{\partial c}{\partial e} \quad k'_e = n' c \frac{\partial k}{\partial e} - n k \frac{\partial c}{\partial e}$$

$$k_\gamma = n' c \frac{\partial k}{\partial \gamma} + n k \frac{\partial c}{\partial \gamma} \quad k'_\gamma = n' c \frac{\partial k}{\partial \gamma} - n k \frac{\partial c}{\partial \gamma} \quad (43)$$

$$k_i = (i n' - i' n) c k \quad k_\pi = (i_1 n' - i'_1 n) c k \quad k_\theta = (i_2 n' - i'_2 n) c k$$

The quantities $k_a, k'_a, \text{etc.}$, will then be the coefficients of the constant factor $a^2 n \kappa$ in the expressions for the derivatives of the elements. Substituting ΔR for P_1 in the differential equations (27), p. 18, the latter will reduce to the form

$$D_t \alpha = (\alpha_1 k_i + \alpha_2 k_\pi + \alpha_3 k_\theta) \kappa \{ \cos(N + N' - \Pi) + \cos(N - N' - \Pi) \}$$

$$D_t e = (e_1 k_i + e_2 k_\pi + e_3 k_\theta) \kappa \{ \cos(N + N' - \Pi) + \cos(N - N' - \Pi) \} \quad (44)$$

$$D_t \gamma = (\gamma_1 k_i + \gamma_2 k_\pi + \gamma_3 k_\theta) \kappa \{ \cos(N + N' - \Pi) + \cos(N - N' - \Pi) \}$$

$$- D_t l_0 = (\alpha_1 k'_a + e_1 k'_e + \gamma_1 k'_\gamma) \kappa \sin(N - N' - \Pi) + (\alpha_1 k_a + e_1 k_e + \gamma_1 k_\gamma) \kappa \sin(N + N' - \Pi)$$

$$- D_t \pi_0 = (\alpha_2 k'_a + e_2 k'_e + \gamma_2 k'_\gamma) \kappa \sin(N - N' - \Pi) + (\alpha_2 k_a + e_2 k_e + \gamma_2 k_\gamma) \kappa \sin(N + N' - \Pi)$$

$$- D_t \theta_0 = (\alpha_3 k'_a + e_3 k'_e + \gamma_3 k'_\gamma) \kappa \sin(N - N' - \Pi) + (\alpha_3 k_a + e_3 k_e + \gamma_3 k_\gamma) \kappa \sin(N + N' - \Pi)$$

By integrating these equations we shall have, in the case of each argument, a divisor which we may call N , equal to the motion of the argument in the unit of time. The quotient $\kappa \div N$ expresses the angular motion of the ecliptic during the time required for the argument to move through the unit radian.

In the above differential equations we substitute for $\alpha_i, e_i, \text{and } \gamma_i$, their numerical values and write, for brevity,

$$C_i = 2.023 k_a - 0.017 k_e - 0.0229 k_\gamma$$

$$C_\pi = -0.0301 k_a - 19.153 k_e - 0.020 k_\gamma \quad (45)$$

$$C_\theta = 0.0075 k_a + 0.0026 k_e - 5.570 k_\gamma$$

with similar expressions for the accented quantities, and

$$\begin{aligned} C_a &= 2.023k_1 - 0.0301k_\pi + 0.0075k_\theta \\ C_e &= -0.0168k_1 - 19.153k_\pi + 0.0026k_\theta \\ C_\gamma &= -0.0229k_1 - 0.0200k_\pi - 5.570k_\theta \end{aligned} \quad (46)$$

We also put for brevity

$$A = N - N' - \Pi \quad A' = N + N' - \Pi$$

The values of N and N' , the coefficients of the time in A and A' respectively take the form

$$N = (n - n')n \quad N' = (n + n')n$$

and the differential variations become

$$\begin{aligned} D_t \alpha &= C_a \kappa (\cos A + \cos A') & - D_t l_0 &= C_l \kappa \sin A + C'_l \kappa \sin A' \\ D_t e &= C_e \kappa (\cos A + \cos A') & - D_t \pi_0 &= C_\pi \kappa \sin A + C'_\pi \kappa \sin A' \\ D_t \gamma &= C_\gamma \kappa (\cos A + \cos A') & - D_t \theta_0 &= C_\theta \kappa \sin A + C'_\theta \kappa \sin A' \end{aligned} \quad (47)$$

We shall then have by integration

$$\begin{aligned} \delta \alpha &= \frac{\kappa}{N} C_a \sin A + \frac{\kappa}{N'} C_a \sin A' & \delta l_0 &= \frac{\kappa}{N} C_l \cos A + \frac{\kappa}{N'} C'_l \cos A' \\ \delta e &= \frac{\kappa}{N} C_e \sin A + \frac{\kappa}{N'} C_e \sin A' & \delta \pi_0 &= \frac{\kappa}{N} C_\pi \cos A + \frac{\kappa}{N'} C'_\pi \cos A' \\ \delta \gamma &= \frac{\kappa}{N} C_\gamma \sin A + \frac{\kappa}{N'} C_\gamma \sin A' & \delta \theta_0 &= \frac{\kappa}{N} C_\theta \cos A + \frac{\kappa}{N'} C'_\theta \cos A' \end{aligned} \quad (48)$$

The largest terms which enter into the theory are shown in Table XLIa, for Arg. N , and Table XLIb for Arg. N' . The coefficients of the principal terms of each have been derived from the numbers given in Part III.

TABLE XLIa.

COEFFICIENTS FOR FORMING $p\alpha - q\gamma$; ARG. N .

| No. | l | π | θ | l' | π' | n | k | $D'k$ | $\partial k / \partial e$ | $\partial k / \partial \gamma$ | nk |
|-----|-----|-------|----------|-------|--------|-----------|---------|---------|---------------------------|--------------------------------|-----------|
| | i | i_1 | i_2 | j_1 | j_2 | | | | | | |
| 1 | 1 | 0 | 0 | 0 | 0 | +1.000 00 | + .9955 | + .9925 | - .0588 | + .9955 | + .995 5 |
| 2 | 2 | -1 | 0 | 0 | 0 | +1.991 55 | + .0275 | + .0275 | + .4980 | .0000 | + .054 7 |
| 3 | 0 | 1 | 0 | 0 | 0 | +0.008 45 | - .0820 | - .0815 | -1.4934 | .0000 | - .000 69 |
| 4 | -1 | 2 | 0 | 0 | 0 | -0.983 1 | + .0004 | + .0004 | + .0142 | .0000 | - .000 4 |
| 5 | 2 | -1 | 0 | -1 | 1 | +1.916 8 | + .0002 | + .0001 | + .0038 | .0000 | + .000 3 |
| 6 | 0 | 1 | 0 | 1 | -1 | +0.083 2 | - .0004 | .0000 | - .0070 | .0000 | .000 0 |
| 7 | -1 | 0 | 2 | 0 | 0 | -1.008 0 | + .0020 | + .0020 | + .0002 | + .0980 | - .002 0 |
| 8 | -1 | 0 | 0 | 2 | 0 | -0.850 4 | - .0083 | - .0081 | + .0052 | + .0072 | + .007 1 |

TABLE XLIb.

COEFFICIENTS FOR ζ ; ARG. N' .

| No. | l i' | π i'_1 | θ i'_2 | l' j'_1 | π' j'_2 | n' | c | $D'c$ | $\partial c/\partial e$ | $\partial c/\partial \gamma$ | $n'c$ |
|-----|-------------|-----------------|--------------------|----------------|------------------|----------|----------|--------|-------------------------|------------------------------|--------|
| 1 | 0 | 1 | -1 | 0 | 0 | 0.012 5 | -.007 2 | -.0068 | -.131 | -0.165 | -.0001 |
| 2 | 1 | 0 | -1 | 0 | 0 | 1.004 02 | +.089 5 | +.0893 | -.0050 | +1.989 | +.0899 |
| 3 | 2 | -1 | -1 | 0 | 0 | 1.995 56 | +.002 47 | +.0025 | +.045 | +0.055 | +.0050 |
| 4 | 1 | 0 | 1 | -2 | 0 | 0.846 4 | +.003 3 | +.0098 | .000 | +0.068 | +.0028 |

It should be added that the coefficients of the smaller terms show only the order of magnitude in each case, and not the precise numerical value. The latter will be required only in the case of terms found to be sensible.

The theorem that all the inequalities have, as a coefficient, the motion of the ecliptic during nearly one-sixth the period of the argument will enable us to limit the combinations of the arguments to be considered.

In the case of any argument $N \pm N'$ containing the Moon's mean longitude, one-sixth the period will never materially exceed 5 days, for which we have

$$\frac{\kappa}{N} = 0''.0064$$

In none of the terms of this class is there a factor C so large as to bring the coefficient up to 0''.05. It follows that all the combinations $N \pm N'$ which contain the Moon's mean longitude may be omitted.

Of the terms which remain none can have a period several times greater than that of the node, for which the ratio $\kappa : N = 1''.5$. It follows that no combinations of arguments giving products of coefficients less than 0.01 need to be computed.

Numbering the arguments N as in the first column of the tables, these two rules will be found to leave the following combinations as the only ones to be considered:

$$\begin{array}{llll} N_1 - N'_2 = \theta & N_2 - N'_3 = \theta & N_3 - N'_1 = \theta & N_7 + N'_2 = \theta \\ N_8 + N'_4 = \theta & N_3 + N'_1 = 2\pi - \theta & N_1 - N'_4 = 2l' - \theta & N_8 + N'_2 = 2l' - \theta \end{array}$$

Using these numbers the computation of the formulæ (43) gives the following values of the coefficients k_a, k_e , etc., for the argument θ .

| Arg. | k_l | k_π | k_θ | k_a | k_e | k_γ |
|--------------|-----------|---------|------------|----------|----------|------------|
| $N_1 - N'_2$ | + .000358 | 0 | + 0.0891 | + 0.1779 | - 0.0102 | + 1.972 |
| $N_2 - N'_3$ | + 1 | 0 | - 1 | + .0002 | + .0050 | + .003 |
| $N_3 - N'_1$ | 0 | 0 | | 0000 | + .0002 | .000 |
| $N_7 + N'_2$ | + 1 | 0 | + .0002 | + .0004 | + 0000 | + .013 |
| $N_8 + N'_4$ | 0 | 0 | - .0002 | 0000 | 0000 | - .001 |
| Sum | + .000359 | 0 | + 0.0889 | + 0.1785 | - 0.0050 | + 1.987 |

It will be remarked that the only accented coefficients are those of the last two lines; and that, as the combined argument $\theta - \Pi$ is the only one included in summation, the accented and unaccented k_a , etc., may all be combined.

For these numbers we derive by (45) and (46)

$$\begin{array}{lll} C_l = + 0.3157 & C_x = + 0.0506 & C_\theta = - 11.067 \\ C_a = + 0.001393 & C_e = + 0.000187 & C_\gamma = - 0.4952 \end{array}$$

We have from the adopted elements of motion of the ecliptic:

$$\kappa = 0''.4714 \quad \Pi = 173^\circ 30' + 0'.59(t - 1850)$$

The following are then the results for the argument θ :

$$\frac{\kappa}{N} = - 1''.396$$

$$\begin{array}{lll} \delta l_0 = - 0''.441 \cos(\theta - \Pi) & \delta \pi_0 = - 0''.01 \cos(\theta - \Pi) & \delta \theta_0 = + 15''.45 \cos(\theta - \Pi) \\ \delta \alpha = - 0''.001945 \sin(\theta - \Pi) & \delta e = 0''.000 & \delta \gamma = + 0''.691 \sin(\theta - \Pi) \end{array} \quad (49)$$

To these expressions for δl_0 , $\delta \pi_0$, and $\delta \theta_0$ are to be added the respective increments

$$\int \delta n dt \quad \int \delta \pi_1 dt \quad \text{and} \quad \int \delta \theta_1 dt$$

arising from substituting the values of $\delta n (= -\frac{3}{2}n\delta\alpha)$, $\delta e (= 0)$, and $\delta \gamma$ in the analytic expressions for n , π_1 , and θ_1 .

The value of $\delta \alpha$ gives the inequality of n

$$\delta n = -\frac{3}{2}n\delta\alpha = 0''.00292n \sin(\theta - \Pi)$$

This adds to the mean longitude the inequality

$$\delta l = - 0''.00292\nu \cos(\theta - \Pi)$$

where ν is the ratio $n:(\theta_1 - D_t\Pi) = - 248.7$.

The complete inequality of the mean longitude thus takes the coefficient $0''.285$.

We have from § 27, (74)

$$\delta \pi_1 = (.022\delta\alpha - .00433\delta\gamma)n$$

The substitution of the preceding values of $\delta \alpha$ and $\delta \gamma$ gives the increments

$$\delta \pi_1 = - .00304 \sin(\theta - \Pi) \quad \text{and} \quad \delta \pi = - 0''.76 \cos(\theta - \Pi)$$

We find, in the same way, the increment

$$\delta \theta = + 0''.11 \cos(\theta - \Pi)$$

The inequalities of l , π , and θ now become

$$\delta l = + 0''.285 \cos(\theta - \Pi) \quad \delta \pi = - 0''.77 \cos(\theta - \Pi) \quad \delta \theta = + 15''.56 \cos(\theta - \Pi) \quad (50)$$

The coefficients of the arguments $2\pi - \theta$ and $2l - \theta$ seem so small that we leave them out of consideration.

§ 65. *Inequalities arising from the coefficients E and F.*

These inequalities have been considered separately on account of their minuteness, and on their depending on arguments different from those of the other inequalities. Some special values of the coefficients *E* and *F* for Venus are given in tabular form in Table XII. In these expressions the axis of *X* passes through the mean Sun, as in the case of the inequalities depending on the mean longitudes. But, on essaying the computation of the principal inequalities arising from *E* and *F*, it was found that a fixed axis of *X* would be more convenient to use. The expressions were therefore transformed so as to refer them to the Sun's perigee as the initial axis. From the form of the expressions the equations of the transformation for *x* and *y* are readily found to be

$$x' = x \cos g' - y \sin g' \qquad y' = x \sin g' + y \cos g'$$

where the accents refer to the fixed solar perigee. It follows that if

$$E = a \cos N + b \sin N \qquad F = a' \cos N + b' \sin N$$

be any pair of the terms *E* and *F* depending on the argument *N*, the corresponding transformed terms, which we represent by *E'* and *F'*, will be

$$\begin{aligned} E' &= \frac{1}{2}(a + b') \cos(N + g') + \frac{1}{2}(a - b') \cos(N - g') \\ &\qquad + \frac{1}{2}(b - a') \sin(N + g') + \frac{1}{2}(b + a') \sin(N - g') \\ F' &= \frac{1}{2}(a' - b) \cos(N + g') + \frac{1}{2}(a' + b) \cos(N - g') \\ &\qquad + \frac{1}{2}(b' + a) \sin(N + g') + \frac{1}{2}(b' - a) \sin(N - g') \end{aligned}$$

The transformed expressions thus arising are shown subsequently in Table XLII.

As a check against any large accidental error in the development of the coefficients, their approximate values, neglecting the small eccentricities of Venus and the Earth, were also computed by analytic development as follows: Taking the mean radius vector of the Earth as the unit of distance, and putting *a* for the corresponding numerical expression for the radius vector of Venus, the Laplace-Gauss form of development will give

$$\Delta^{-5} = \frac{1}{2} \sum b_s^{(4)} \cos iL$$

L being the difference of the heliocentric longitudes of Venus and of the Earth which we represent for the present by *l* and *l'* respectively.

The expressions for the rectangular geocentric coördinates of Venus will then be, when powers of the eccentricities and inclination are dropped in the development

$$X = -\cos l' + a \cos l \qquad Y = -\sin l' + a \sin l \qquad Z = a \sin I \sin(l - \theta_v)$$

where *I* is the inclination of the orbit of Venus, and θ_v the longitude of its node, reckoned from an arbitrary fixed origin. Forming the product of the several factors which form *E* and *F*, noting that the summation changes from positive to

negative, changing and transforming the indices so as to reduce the summation to its simplest form, the values of E and F take the following general form:

$$E = \frac{\sin I}{4} \Sigma \{ (\alpha b_s^{(i+1)} - \alpha^2 b_s^{(i)}) \sin (iL + \theta_v) + (\alpha b_s^{(i+1)} - \alpha^2 b_s^{(i+2)}) \sin (iL - 2l' + \theta_v) \}$$

$$F = \frac{\sin I}{4} \Sigma \{ -(\alpha b_s^{(i+1)} - \alpha^2 b_s^{(i)}) \cos (iL + \theta_v) + (\alpha b_s^{(i+1)} - \alpha^2 b_s^{(i+2)}) \cos (iL - 2l' + \theta_v) \}$$

If we put, for brevity

$$\beta_i = \frac{1}{4} (\alpha b_s^{(i+1)} - \alpha^2 b_s^{(i)}) \sin I \quad \beta'_i = \frac{1}{4} (\alpha b_s^{(i+1)} - \alpha^2 b_s^{(i+2)}) \sin I$$

we shall have

$$E = \Sigma \beta_i \sin (iL + \theta) + \Sigma \beta'_i \sin (iL - 2l' + \theta_v)$$

$$F = -\Sigma \beta_i \cos (iL + \theta_v) + \Sigma \beta'_i \cos (iL - 2l' + \theta_v)$$

The numerical values of the coefficients $b^{(i)}$ may be taken from any one of various publications. In *Astronomical Papers of the American Ephemeris*, Vol. V, Pt. IV, p. 343, are found values of $c_s^{(i)} = \alpha^2 b^{(i)}$ for Venus and the Earth, as follows:

| | | | | |
|---------------------|---------|---------|---------|---------|
| $i = 0$ | 1 | 2 | 3 | 4 |
| $c_s^{(i)} = 44.88$ | 43.64 | 40.61 | 36.52 | 31.99 |

From these we find:

| | | | | |
|--|---------|---------|---------|---------|
| $i = -2$ | -1 | 0 | $+1$ | $+2$ |
| $\frac{1}{4} \alpha b_s^{(i+1)} = 15.10$ | 15.53 | 15.10 | 14.05 | 12.64 |
| $\frac{1}{4} \alpha^2 b_s^{(i)} = 10.15$ | 10.91 | 11.22 | 10.91 | 10.15 |
| $\beta_i \div \sin I = 4.95$ | 4.62 | 3.88 | 3.14 | 2.51 |
| $\beta'_i \div \sin I = 3.88$ | 4.62 | 4.95 | 4.92 | 4.64 |

We thus have the following general expressions for E and F , the axis of X , in the ecliptic, being arbitrary.

We use

$$\sin I = .0592$$

Then

$$\begin{aligned} E = & + .293 \sin (-2L + \theta_v) + .229 \sin (-2L - 2l' + \theta_v) \\ & + .273 \sin (-L + \theta_v) + .273 \sin (-L - 2l' + \theta_v) \\ & + .229 \sin \theta_v \quad + .293 \sin (-2l' + \theta_v) \\ & + .186 \sin (L + \theta_v) \quad + .291 \sin (-L - 2l' + \theta_v) \\ & + .148 \sin (2L + \theta_v) \quad + .274 \sin (2L - 2l' + \theta_v) \\ F = & - .293 \cos (-2L + \theta_v) + .229 \cos (-2L - 2l' + \theta_v) \\ & - .273 \cos (-L + \theta_v) + .273 \cos (-L - 2l' + \theta_v) \\ & - .229 \cos \theta_v \quad + .293 \cos (-2l' + \theta_v) \\ & - .186 \cos (L + \theta_v) \quad + .291 \cos (L - 2l' + \theta_v) \\ & - .148 \cos (2L + \theta_v) \quad + .274 \cos (2L - 2l' + \theta_v) \end{aligned}$$

Measuring θ_v from the solar perigee, in longitude $279^\circ.5$, we have

$$\theta_v = 155^\circ.4 \quad l' = g' + 180^\circ$$

The results both of this computation and of the analytic development are shown in tabular form as follows:

TABLE XLII.
E AND *F* FOR THE ACTION OF VENUS.

| Arg. | | <i>E</i> | | | | Arg. | | <i>F</i> | | | |
|--------------|--|----------|-------|-------|-------|--------------|--|----------|-------|-------|-------|
| <i>L, g'</i> | | cos | | sin | | <i>L, g'</i> | | cos | | sin | |
| | | Num. | Anal. | Num. | Anal. | | | Num. | Anal. | Num. | Anal. |
| 0 0 | | +.088 | +.095 | .000 | .000 | 0 0 | | +.197 | +.208 | .000 | .000 |
| 0 1 | | +.007 | | +.008 | | 0 1 | | +.014 | | -.005 | |
| 0 2 | | +.124 | +.122 | +.259 | +.266 | 0 2 | | -.255 | -.266 | +.116 | +.122 |
| 1 -2 | | +.120 | +.121 | -.252 | -.264 | 1 -2 | | -.252 | -.264 | -.113 | -.121 |
| 1 -1 | | +.012 | | -.006 | | 1 -1 | | +.020 | | +.011 | |
| 1 0 | | +.183 | +.191 | +.078 | +.078 | 1 0 | | +.398 | +.417 | -.034 | -.036 |
| 1 1 | | +.010 | | +.014 | | 1 1 | | +.010 | | -.008 | |
| 1 2 | | +.113 | +.114 | +.237 | +.248 | 1 2 | | -.239 | -.248 | +.104 | +.114 |
| 2 -2 | | +.112 | +.114 | -.236 | -.249 | 2 -2 | | -.236 | -.249 | -.104 | -.114 |
| 2 -1 | | +.010 | | -.002 | | 2 -1 | | +.022 | | -.008 | |
| 2 0 | | +.174 | +.183 | +.129 | +.132 | 2 0 | | +.382 | +.401 | -.058 | -.060 |
| 2 1 | | +.010 | | +.014 | | 2 1 | | +.006 | | -.008 | |
| 2 2 | | +.096 | +.095 | +.198 | +.208 | 2 2 | | -.200 | -.208 | +.087 | +.095 |

The largest terms arising from *E* and *F* are those whose arguments are independent of the mean longitude of the Moon, Sun, and Earth. These arise from the constant terms of *E* and *F*, which are, when referred to the solar perigee

$$E = +.088 \quad F = +.197$$

The computation of the inequalities arising from this pair of terms will be yet further simplified by taking the node of Venus as the axis of *X*. By transforming to this axis we shall have

$$E = .002 \quad F = -.216$$

We may regard this value of *E* as evanescent, thus confining the terms we have to determine to the expression

$$2F\eta\zeta$$

From the expressions for ξ , η , and ζ we find the largest terms of the products and their derivatives to be:

$$2\xi\zeta = -.0895 \sin \theta - .0039 \sin (2l' - \theta) + .0006 \sin (2\pi - \theta)$$

$$2D'\xi\zeta = -.1786 \quad \text{''} \quad -.0135 \quad \text{''} \quad +.0012 \quad \text{''}$$

$$\frac{2\partial\xi\zeta}{\partial e} = -.0137 \quad \text{''} \quad +.0006 \quad \text{''} \quad +.0218 \quad \text{''}$$

$$\frac{2\partial\xi\eta}{\partial \gamma} = -1.988 \quad \text{''} \quad -.089 \quad \text{''} \quad +.014 \quad \text{''}$$

$$\begin{aligned}
 2\eta\zeta &= +.0895 \cos \theta + .0039 \cos (2l' - \theta) - .0006 \cos (2\pi - \theta) \\
 2D'\eta\zeta &= +.1786 \quad \text{“} \quad +.0135 \quad \text{“} \quad - .0012 \quad \text{“} \\
 2\frac{\partial\eta\zeta}{\partial e} &= +.0137 \quad \text{“} \quad - .0006 \quad \text{“} \quad - .0218 \quad \text{“} \\
 2\frac{\partial\eta\zeta}{\partial\gamma} &= +1.988 \quad \text{“} \quad +.089 \quad \text{“} \quad - .014 \quad \text{“}
 \end{aligned}$$

The resulting terms of H , heretofore omitted, are

$$H = 2E\xi\zeta + 2F\eta\zeta$$

Taking the node of Venus as origin, we have, as shown on p. 135, the following terms of E and F

$$E = .285 \sin 2l' \quad F = -.216 + .285 \cos 2l'$$

With these numbers we find for argument θ

$$\begin{aligned}
 H &= -.0182 \cos \theta & D'H &= -.0348 \cos \theta & \frac{\partial H}{\partial e} &= -.0032 \cos \theta \\
 \frac{\partial H}{\partial\gamma} &= -.403 \cos \theta & \frac{\partial H}{\partial l} &= \frac{\partial H}{\partial\pi} = 0 & \frac{\partial H}{\partial\theta} &= +.0182 \sin \theta
 \end{aligned}$$

These derivatives are to be substituted in the fundamental equations (41) and (42), § 21, and each equation integrated. For the latter process the factor of integration is

$$\frac{n}{\theta_1} = -248.8$$

The product of this into M for Venus (§ 17) is $-1''.055$

We thus have the following results:

$$\begin{aligned}
 D_n l_0 &= +.061M \cos \theta & D_n \pi_0 &= -.070M \cos \theta & D_n \theta_0 &= -2.24M \cos \theta \\
 \delta l_0 &= -0''.064 \sin \theta & \delta \pi_0 &= +''.074 \sin \theta & \delta \theta_0 &= +2''.36 \sin \theta \\
 D_n \alpha &= +.000136M \sin \theta & D_n e &= +.000047M \sin \theta & D_n \gamma &= -.1014M \sin \theta \quad (51) \\
 \delta \alpha &= +0''.000144 \cos \theta & \delta e &= +''.000050 \cos \theta & \delta \gamma &= -0''.107 \cos \theta
 \end{aligned}$$

To find the complete inequalities in l , π , and θ we must add the respective quantities

$$\int \delta n dt \quad \int \delta \pi_1 dt, \quad \int \delta \theta_1 dt$$

of which the expressions in terms of δn , δe , and $\delta \gamma$ are formed by § 27, Eq. 74. We thus have, dropping unimportant terms,

$$\begin{aligned}
 \delta n &= -\frac{3}{2}n\delta\alpha = -0''.000216n \cos \theta & \delta \pi_1 &= -0.0148\delta n - 0.0043n\delta\gamma = +0''.00046n \cos \theta \\
 \delta \theta_1 &= +.0038\delta n + .00066n\delta\gamma = -.000071n \cos \theta
 \end{aligned}$$

The completed values of δl , $\delta\pi$, and $\delta\theta$ thus become

$$\begin{aligned} \delta l &= + 0''.054 \sin \theta + \delta l_0 = - 0''.010 \sin \theta \\ \delta\pi &= - 0.115 \sin \theta + \delta\pi_0 = - 0''.041 \sin \theta \\ \delta\theta &= + 0.018 \sin \theta + \delta\theta_0 = + 2''.38 \sin \theta \end{aligned} \tag{52}$$

in all which expressions θ is reckoned from the ascending node of Venus.

The coefficients of the term in $2\pi - \theta$ are, for δy and $\delta\theta$, less than one hundredth those for θ , and the integrating factor ν is less than 0.3 as great. The coefficients in $2l - \theta$ are but a fraction of those in θ , and the integrating divisor is nearly 40 times as great. We therefore conclude that the inequalities depending on these arguments are inappreciable.

§ 66. *Action of Mars and Jupiter.* In Mars the product $M \sin I$ is about .08 that for Venus. I have therefore not computed the terms.

In the case of Jupiter the largest quantities which enter into the constant part of F are

$$\frac{a_1^5}{\Delta^5} = 1.26 \quad YZ = \frac{1}{2} a_1^2 \sin I \quad \sin I = 0.0231$$

Hence

$$a'^3 F = 1.26 \times .0231 \alpha^3 = + .000103$$

The product $10^3 MF$ is, approximately,

$$\text{For Venus} \quad - 0''.92 \quad \text{For Jupiter} \quad + 0''.170$$

The inequalities depending on θ are proportional to this product. We conclude that the inequalities arising from the action of Jupiter may be derived from those of Venus by multiplying the coefficients by $- 0.185$. We thus have, from the action of Jupiter,

$$\delta\theta = - 0''.43 \sin(\theta - \theta_j) \quad \delta\gamma = + 0.020 \cos(\theta - \theta_j) \tag{53}$$

where θ_j is the longitude of the ascending node of Jupiter on the ecliptic. The inequalities of the other elements are unimportant.

§ 67. *Combination of terms depending on the longitude of the Moon's Node.*

The inequalities (49), (50), (51), (52), and (53), all depending on the same argument θ , may now be combined. We shall do this for the two epochs, 1800 and 1900.

The value of Π which I have derived in *Elements and Constants*, p. 186, there called L' , is

$$\Pi = 173^\circ 29'.7 + 54'.4 T \text{ (from 1850)}$$

Taking approximate values of the nodes of Jupiter and Saturn, and this value of Π , we have

$$\begin{array}{ccc} \Pi & 1800 & 1900 \\ & 173^\circ 2' & 173^\circ 57' \end{array}$$

We take the nodes of Venus and Jupiter as constant, using the values for 1850

$$\theta_v = 75^\circ.3 \quad \theta_j = 98^\circ.9$$

Carrying these values into the inequalities of the elements in question and combining them, we find:

$$\begin{aligned} \delta l &= + 0''.029 \sin \theta - 0''.271 \cos \theta \\ \delta \pi &= - 0.10 \sin \theta + 0.80 \cos \theta \\ \delta \theta &= + 2.55 \sin \theta - 17.33 \cos \theta \dots \text{(for 1800)} \\ \delta \theta &= + 2.31 \sin \theta - 17.34 \cos \theta \dots \text{(for 1900)} \\ \delta \gamma &= - 0''.114 \cos \theta - 0.769 \sin \theta \dots \text{(for 1800)} \\ \delta \gamma &= - 0.103 \cos \theta - 0.770 \sin \theta \dots \text{(for 1900)} \end{aligned}$$

§ 68. *Special computation of the Hansenian Venus-term of long period.*

The following are the planetary and lunar arguments whose differences make up the argument

$$18v - 16g' - g$$

of the term in question.

| | Planetary | Lunar |
|-----|--------------|-----------|
| (1) | $18v - 18g'$ | $g - 2g'$ |
| (2) | $18 - 17$ | $g - g'$ |
| (3) | $18 - 16$ | g |
| (4) | $18 - 15$ | $g + g'$ |

The coefficients $h_{a,s'}$, $h_{a,c'}$, etc., are computed by §§ 22 and 23. The planetary coefficients MK , MC , and MD are found in Table X. The lunar coefficients ap , etc., are given in the next chapter, Tables XLVIII and XLIX. For the argument $g - g'$ we change the signs of a , e , g and k , as given for the argument $-g + g'$.

I have not computed the coefficients for the argument $g - 2g'$ believing their effect to be insensible. Their characteristic is $ee'^2 = .000050$, and, in the principal term of η , this is in Brown's theory multiplied by a factor of the order of magnitude .04. The largest planetary coefficient being $0.5 \div 10^3$, the value of h_a will be of the order of magnitude $1'' \div 10^9$, which would result in a term in δl of the order of magnitude $0''.02$. Actually, the computation shows that the combinations (2) and (4) are also much smaller than (3).

We have now all the data for computing the coefficients $h_{a,c'}$, $h_{a,s'}$, etc., from the formulæ of § 22. The results are:

$$\begin{aligned} h_{a,c'} &= -''.5597 \div 10^6 & h_{a,s'} &= +''.4880 \div 10^6 \\ h_{e,c'} &= - .0052 \div 10^3 & h_{e,s'} &= + .0047 \div 10^3 \\ h_{l,c'} &= - .00081 \div 10^3 & h_{l,s'} &= - .00094 \div 10^3 \\ h_{\pi,c'} &= + .084 \div 10^3 & h_{\pi,s'} &= + .095 \div 10^3 \end{aligned}$$

The coefficients for γ and θ are much smaller, and are omitted. The coefficients we have given correspond to the argument

$$N - N_4 = g + 16g' - 18v \equiv A$$

of which the annual motion is

$$N = -4747''.8$$

giving

$$\nu = -3649$$

We therefore have the following inequalities in l_0 , π , and e

$$\delta l_0 = -0''.003 \sin A + 0''.003 \cos A$$

$$\delta \pi = +0.31 \sin A - 0.35 \cos A$$

$$\delta e = -0.019 \sin A - 0.017 \cos A$$

The term of δl_0 is so minute as to be unimportant. For the term in the mean longitude arising from δn we have

$$\log \frac{3}{2} \nu^2 = 7.3005$$

which gives

$$\delta l = -11''.18 \cos A + 9''.75 \sin A = 14''.83 \sin (A - 48^\circ 55'.2)$$

It will be convenient to use the negative of this argument in order that its motion may be positive. We shall therefore write

$$\delta l = 14''.83 \sin (18\nu - 16g' - g + 228^\circ 55'.2)$$

where ν is the mean longitude of Venus measured from the earth's perihelion.

It will be of interest to compare this result with those reached by other investigators. The following are arranged in the order of time. Putting

L , the mean long. of Venus—that of Earth

$$M = 18L + 2g' - g$$

and reducing all results to the mass $1 \div 408,000$ of Venus, there has been found, for the direct action, by

| | |
|-----------------|---|
| Hansen * | $\delta l = 15''.34 \sin (M + 229^\circ.2)$ |
| Delaunay † | $= 16.34 \sin (M + 228.5)$ |
| Newcomb ‡ | $= 14.80 \sin (M + 229.5)$ |
| Radau § | $= 14.14 \sin (M + 229.0)$ |
| Newcomb (above) | $= 14.83 \sin (M + 228.9)$ |

To judge the precision of this value we have to estimate the error to which the development by mechanical quadratures is liable. The circle being divided into 60 parts, any coefficient which we have taken as A_{18} is really the sum of an infinite series of which the first two terms are $A_{18} \pm A_{42}$. We have dropped all the terms after the first. From the progression of the coefficients it would seem that the

* *Tables de la Lune*, p. 9.
 † *Action of Planets*, p. 286.

‡ *Conn. des Temps*, 1862, App., p. 58.
 § *Inégalités Planétaires*, p. 113.

ratio $A_i : A_{i+1}$ is approximately 1 : 1.26, whence the ratio $A_{18} : A_{42}$ would be about 250. The error of the computed term may therefore well be $\pm 0''.06$. It has been only as this work is in press that the author has looked into the possible effect of the slow convergence; and while it seems likely that the error entering through the coefficients K and C will not exceed that just stated, the same may not be true of the coefficient D .

A quantitative estimate of the correction may be made in various ways; but the author is unable to enter upon the subject in the present work.

It is also to be noted that the term as above computed contains the effect, whatever it may be, of the mutual perturbations of Venus and the Earth. A separate computation has been made of the fundamental numbers due to these perturbations, but as the final result of the coefficients amounts to only a fraction of a second, the computation has not been completed. The effect being included in the computed term, a knowledge of its amount is necessary to compare the result with that reached by the ordinary method of development.

The change in the term as computed is too minute to account for the observed variation of long period in the Moon's mean motion. As the period of this variation seems to be nearly the same as that of the inequality under consideration, the question naturally arises whether the effect of the indirect action may be appreciable. This being the most important question in the lunar theory, a computation of the principal part of the indirect term has been made. The result being altogether unimportant, it seems unnecessary to do more than present such a brief statement of the method as will enable the subject to be taken up by another in case the author's conclusion is not well founded. The required perturbations of the Earth by Venus are most easily computed for the case in question by using, instead of the Lagrangian brackets, the corresponding functions of the coördinates. The formulæ necessary for the purpose are found in Moulton's *Celestial Mechanics*, p. 291. The eccentricities have been dropped as unnecessary, and attention was confined to the longitude elements. The terms dependent upon the action of the planet on the Sun are also dropped, being appreciable only in terms depending on small multiples of mean longitude. The development of $\frac{a^3}{\Delta^3}$ used in the computation is that in *Action*, pp. 248-251. The result for the indirect action is

$$\delta l = + 0''.044 \cos A - 0''.036 \sin A.$$

This, being added to the terms already found, gives for the entire term

$$\delta l = 14''.77 \sin (18v - 16g' - g + 228^\circ 54')$$

which is the definitive result of the present investigation.

§ 69. *The Radau terms of long period.* Radau has computed certain additional terms of long period due to the action of Venus, with the following results, the arguments being reduced to those adopted in the present work:

| | |
|---|--------------|
| $\delta v = + 0''.140 \sin (2\pi + g - 20v + 19g' + 171^\circ)$ | Per. = 347.8 |
| + 0 .110 $\sin (g - 26v + 29g' + 62^\circ)$ | 127.2 |
| + 0 .056 $\sin (g - 21v + 21g')$ | 8.35 |
| + 0 .019 $\sin (\pi + g - 23v + 24g' + 295^\circ)$ | 55. |
| + 0 .016 $\sin (\pi + g - 15v + 11g' + 219^\circ)$ | 71. |
| - 0 .012 $\sin (2\pi - g + 24v - 26g' + 159^\circ)$ | 58. |
| + 0 .012 $\sin (g - 23v + 24g' + 14^\circ)$ | 7.6 |
| + 0 .008 $\sin (\pi - \theta + g - 23v + 24g' + 101^\circ)$ | 28.2 |
| + 0 .004 $\sin (2\theta - g + 23v - 24g' + 183^\circ)$ | 42. |
| + 0 .003 $\sin (\pi - g + 21v - 21g' + 288^\circ)$ | 148. |

The first three of these terms are the only ones that need be considered for the practical applications of the lunar theory. The third might also be omitted, but is easily computed in connection with the first.

For all the terms except the second the planetary coefficients A , B , C , and D may be derived with all necessary precision from the special values of these coefficients given in Table VII, by the following process. Putting

$$L = v - g'$$

let the value of the planetary arguments for which we desire the coefficients be

$$N = hL + kg'$$

Recalling that the 720 special values of each coefficient, say A , are arranged in 12 systems of 60 indices each, the special value of N corresponding to the j th system and the index i will be

$$N_{ij} = 6^\circ \times hi + 30^\circ \times kj$$

We may mark each special value of A in the same way. The values of the coefficients A_c and A_s will then be given by the equations

$$360A_c = \sum A_{i,j} \cos N_{i,j}$$

$$360A_s = \sum A_{i,j} \sin N_{i,j}$$

The terms of A for the special argument N will then be

$$A = A_c \cos N + A_s \sin N$$

In most cases the computation may be simplified, as in the usual method of executing periodic developments, by adding together in advance the special values of A which are to be multiplied by the same sine or the same cosine. Another method

may be used in computing these terms by the developments found in *Action*, Chapter III, § 18. Some modification is, however, necessary owing to the circumstance that in that work the rectangular coördinates are reckoned from a fixed axis passing through the earth's perihelion or the solar perigee, while in the present case the axes pass through the mean sun. It is therefore necessary to use the expressions for the geocentric coördinates of Venus referred to this moving axis, a development which may readily be made from the special values already given for the coördinates of Venus and the sun. It is necessary to transform the table so that the arguments shall be the mean anomaly of Venus instead of its mean longitude because the development for Δ^{-5} which are tabulated on p. 25 of *Action* have the mean anomaly of Venus as an argument.

I have applied the method of development from special values to the first term with the following results:

Planetary Coefficients for Arg. $20v - 21g'$.

| | |
|-----------------|-----------------|
| $A_o = +.03562$ | $A_s = +.00694$ |
| $B_o = -.02999$ | $B_s = -.00583$ |
| $C_o = -.00563$ | $C_s = -.00112$ |
| $D_o = +.00634$ | $D_s = -.03254$ |
| $K_o = +.03280$ | $K_s = +.00638$ |
| $C_e = -.00282$ | $C_i = -.00056$ |

The lunar portion of the argument is equivalent $2D - g$, of which the indices in Table XL are $(-1, 0, 2, -2)$. From the numbers in this table we find for the direct action

$$\delta l = 0''.11 \sin (g + 2\pi - 20v + 19g' + 10^\circ)$$

π being measured from the earth's perihelion.

This coefficient is less than that found by Radau ; but the lunar argument is one to which the present method is not well adapted and a redetermination is desirable.

None of the other Radau terms are completely computed in the present work. Such computations as I have made seem to indicate even smaller coefficients than those found by Radau.

CHAPTER IX.

PERIODIC INEQUALITIES IN GENERAL.

§ 70. For convenience we mention the formulæ derived in Part I, giving them the special form adopted in the actual numerical work. We recall that the combination of any lunar argument N with a planetary argument N_4 gives rise to two arguments G , $N+N_4$ and $N-N_4$. For each argument there are two terms in the D_{nt} of each of the elements, one a cosine term; the other a sine term. We represent the coefficients of these terms for the element α by

$$h_{\alpha,c}, h_{\alpha,s}, h_{\alpha,c'}, \text{ and } h_{\alpha,s'}$$

with a similar notation for the remaining elements,

$$e, \gamma, l_0, \pi_0, \text{ and } \theta_0$$

except that the coefficients for the angular elements have the negative sign.

The expressions of these coefficients for the direct action are given *in extenso* in Part I by the equations (46), (47), (48), (50), and (51). For the indirect action the coefficients are given in (64) and (65), but we may use the equations for direct action by making the substitution indicated in § 25 (66), which gives the expressions for the sum of the two actions.

For convenience in computation the coefficients are so used as to give the result in terms of $0''.001$ as the unit. The numerical values of the planetary coefficients practically used for the purely periodic inequalities are these

$$K'_c = 10^3(MK_c - m^2G_c) \quad C'_c = 10^3(\frac{1}{2}MC_c + m^2J_c) \quad D'_c = 10^3(MD_c + m^2I_c)$$

with corresponding values of K'_s , C'_s , and D'_s .

Since each combination of a lunar with a planetary argument gives rise to two combined arguments, one equal to their sum the other equal to their difference, the coefficients relating to the latter are distinguished by accents.

The numerical values of the planetary coefficients, as derived from the numbers of Part II, and just defined, are shown in the following tables.

Values of the Planetary K'-Coefficients, Combining Direct and Indirect Action.

TABLE XLIII.

ACTION OF VENUS.

| Arg. v, g' | K'_c | C'_c | D'_c | K'_d | C'_d | D'_d |
|---------------|----------|---------|---------|---------|--------|--------|
| 1 - 2 | - 0.61 | - 0.37 | - 0.02 | - 0.11 | .00 | - 0.46 |
| 1 - 1 | +25.04 | -10.73 | +35.66 | +0.03 | -0.01 | - 0.05 |
| 1 - 0 | + 2.44 | - 0.52 | + 2.31 | -0.02 | +0.03 | - 0.04 |
| 2 - 4 | - 0.68 | - 0.02 | + 0.61 | -0.06 | -0.06 | - 0.12 |
| 2 - 3 | + 6.53 | - 1.74 | +20.01 | +1.21 | -0.47 | - 4.33 |
| 2 - 2 | -29.33 | + 8.77 | -52.76 | +0.25 | -0.12 | - 0.27 |
| 2 - 1 | - 3.49 | + 0.50 | - 3.29 | -0.02 | +0.03 | - 0.08 |
| 3 - 6 | - 0.31 | + 0.02 | + 0.28 | -0.24 | +0.02 | - 0.22 |
| 3 - 5 | - 0.94 | + 0.15 | + 6.54 | -0.61 | +0.15 | - 5.29 |
| 3 - 4 | +10.08 | - 3.25 | +12.11 | +2.25 | -0.69 | - 2.69 |
| 3 - 3 | + 4.64 | - 1.99 | -12.92 | +0.19 | -0.03 | - 0.16 |
| 4 - 6 | + 0.61 | - 0.20 | + 0.85 | +0.53 | -0.19 | - 0.76 |
| 4 - 5 | + 0.68 | + 0.03 | - 2.19 | +0.05 | .00 | + 0.40 |
| 4 - 4 | + 7.11 | - 2.38 | - 9.72 | -0.02 | +0.01 | + 0.08 |
| 5 - 8 | + 0.12 | - 0.04 | + 0.71 | +0.17 | -0.05 | - 1.04 |
| 5 - 7 | - 0.43 | + 0.16 | - 0.88 | -0.36 | +0.12 | + 0.78 |
| 5 - 6 | + 0.82 | - 0.23 | - 1.36 | +0.09 | -0.06 | + 0.37 |
| 5 - 5 | + 8.40 | - 2.43 | - 7.39 | | | |
| 6 - 9 | + 0.02 | - 0.01 | - 0.02 | +0.03 | -0.01 | + 0.03 |
| 6 - 8 | + 0.18 | - 0.06 | - 0.16 | +0.14 | -0.05 | + 0.12 |
| 6 - 7 | + 1.19 | - 0.28 | - 0.11 | +0.24 | -0.06 | + 0.21 |
| 6 - 6 | + 7.32 | - 1.86 | - 6.64 | 0.00 | .00 | 0.00 |
| 7 - 9 | + 0.18 | - 0.05 | - 0.16 | +0.12 | -0.04 | + 0.11 |
| 7 - 8 | + 1.13 | - 0.24 | - 0.11 | +0.22 | -0.05 | + 0.21 |
| 7 - 7 | + 6.25 | - 1.42 | - 5.79 | 0.00 | .00 | 0.00 |
| 8 -13 | - 0.0045 | + 0.003 | - 1.289 | +0.0661 | -0.022 | -15.92 |

NOTE.— The units in these tables are 0".001.

TABLE XLIV.
ACTION OF MARS.

| Arg. M, g' | K'_c | C'_c | D'_c | K'_s | C'_s | D'_s |
|-----------------|--------|--------|--------|--------|--------|--------|
| 1 -1 | -0.78 | +0.13 | +2.34 | -0.01 | +0.01 | -0.05 |
| 1 0 | +0.18 | -0.31 | +0.32 | +0.08 | +0.01 | -0.27 |
| 2 -2 | -11.70 | +3.97 | +17.04 | +0.34 | -0.01 | +0.26 |
| 2 -1 | -0.45 | +0.38 | -11.98 | -0.63 | +0.24 | +8.80 |
| 3 -3 | +1.38 | -0.43 | -0.95 | +0.16 | -0.02 | +0.15 |
| 3 -2 | +0.81 | -0.25 | -2.44 | +0.89 | -0.27 | +2.69 |
| 4 -4 | +0.66 | -0.17 | -0.20 | +0.22 | -0.04 | +0.21 |
| 4 -3 | +1.86 | -0.60 | -2.94 | +1.84 | -0.64 | +3.05 |
| 4 -2 | -0.12 | +0.01 | -0.50 | +0.59 | -0.25 | -4.90 |
| 5 -4 | -0.52 | +0.18 | +0.34 | -0.68 | +0.21 | -0.48 |
| 5 -3 | +0.04 | -0.02 | -0.19 | -0.47 | +0.15 | -1.73 |
| 6 -5 | -0.22 | +0.07 | -0.03 | -0.33 | +0.09 | -0.06 |
| 6 -4 | +0.04 | -0.02 | +0.11 | -0.74 | +0.25 | -1.34 |
| 6 -3 | +0.15 | -0.05 | +0.69 | -0.08 | +0.05 | +0.50 |
| 15 -9 | +0.11 | -0.02 | -0.13 | -0.15 | +0.04 | -0.25 |
| 15 -8 | +0.04 | -0.02 | -1.55 | 0.00 | +0.01 | -0.70 |

TABLE XLV.
ACTION OF JUPITER.

| Arg. J, g' | K'_c | C'_c | D'_c | K'_s | C'_s | D'_s |
|-----------------|--------|--------|--------|--------|--------|--------|
| +1 -2 | -4.25 | +0.72 | +4.20 | -0.72 | +0.19 | -0.43 |
| +1 -1 | -41.87 | +12.87 | +61.07 | -1.53 | +0.28 | -1.67 |
| +1 0 | +1.45 | +0.21 | +2.08 | +1.35 | -0.12 | -21.72 |
| +2 -3 | +2.01 | -0.41 | -1.98 | -0.20 | +0.02 | +0.10 |
| +2 -2 | +30.81 | -8.39 | -17.37 | +0.38 | -0.06 | +0.35 |
| +2 -1 | +7.86 | -2.88 | -12.22 | +3.26 | -0.94 | +5.29 |
| +2 0 | -0.21 | -0.04 | +0.53 | -0.14 | -0.01 | +0.17 |
| +3 -3 | +4.53 | -0.63 | -10.71 | -0.40 | +0.08 | -0.39 |
| +3 -2 | -0.15 | +0.06 | +0.18 | -5.93 | +1.67 | -3.69 |
| +3 -1 | +0.24 | -0.08 | -0.40 | -0.97 | +0.38 | -1.67 |

TABLE XLVI.
ACTION OF SATURN.

| Arg. S, g' | K'_c | C'_c | D'_c | K'_s | C'_s | D'_s |
|-----------------|--------|--------|--------|--------|--------|--------|
| 1 -1 | -2.46 | +0.83 | +3.48 | -0.03 | +0.01 | -0.03 |
| 1 0 | +0.01 | +0.03 | -2.64 | +0.01 | -0.01 | -0.50 |
| 2 -2 | +1.33 | -0.33 | -1.57 | 0.00 | 0.00 | 0.00 |
| 2 -1 | +0.66 | -0.23 | -0.94 | +0.02 | -0.01 | +0.05 |

§ 71. The lunar coefficients fall into two classes, one determining the elements α , e , and γ and called, for brevity, the a-coefficients; the other determining l , π , and θ , and called the L -coefficients. Those of the first class are computed by the formulæ of § 20 and § 22; those of the second class by the formulæ of § 23, Eq. (50). In the computation we write k for k_4 .

The a-coefficients are the nine products of the factors a , e , and g defined in § 22, Eq. 43, into p , q , and k .

From § 22, (46) to (48), it will be seen that by using the planetary factors in the form just given and taking the a-coefficients

$$ap, aq, \frac{1}{2}ak, \text{ etc.}$$

the coefficients of the terms of $D_{ni}(\alpha, e, \text{ and } \gamma)$ will each be the sum of three products of two factors each. But the quantities we actually compute are the values of $2\delta e$ and $2\delta\gamma$. We therefore double the coefficients for δe and $\delta\gamma$, using

$$2ep, 2eq, ek; 2gp, 2gq \text{ and } gk$$

We have also multiplied the inequalities of π and θ by the factors $2e$ and 2γ , required to reduce them to inequalities of the actual longitude and latitude. To do this we take for the nine L -coefficients

$$L', L'', \frac{1}{2}L_4; 2eP', 2eP'', eP_4; 2\gamma R', 2\gamma R'', \gamma R_4$$

Each of the coefficients to form a term of $D_{ni}l_0$, $2eD_{ni}\pi_0$ or $2\gamma D_{ni}\theta_0$ will then be the sum of three products formed by taking one factor from one of the Tables XLIII to XLVI, and the other from Table XLIX, the product $D'L_4$ being divided by 2.

TABLE XLVII.

DATA FOR a-COEFFICIENTS.

| Arg. $g \ g' \ \lambda \ \lambda'$ | Arg. | $i \ i' \ i''$ | a | e | g |
|---------------------------------------|--------------|----------------|---------|----------|----------|
| 0 0 0 0 | 0 | 0 0 0 | 0.0000 | 00.0000 | 00.0000 |
| 0 1 0 0 | g' | 0 0 0 | 0.0000 | 00.0000 | 00.0000 |
| 1 -1 0 0 | $g-g'$ | 1 -1 0 | +2.0529 | +19.137 | -00.0029 |
| 1 0 0 0 | g | 1 -1 0 | +2.0529 | +19.137 | -00.0029 |
| 1 1 0 0 | $g+g'$ | 1 -1 0 | +2.0529 | +19.137 | -00.0029 |
| 2 0 0 0 | $2g$ | 2 -2 0 | +4.106 | +38.274 | -00.0058 |
| -2 -0 2 -2 | $2D-2g$ | 0 2 0 | -0.6002 | -38.307 | -00.0400 |
| -1 0 2 -2 | $2D-g$ | 1 1 0 | +1.9927 | -19.170 | -00.0429 |
| 0 0 2 -2 | $2D$ | 2 0 0 | +4.0456 | -00.0336 | -00.0458 |
| 1 0 2 -2 | $2D+g$ | 3 -1 0 | +6.098 | +19.103 | -00.0487 |
| 0 -1 2 -2 | $2D-g'$ | 2 0 0 | +4.046 | -00.0336 | -00.0458 |
| 0 1 2 -2 | $2D+g'$ | 2 0 0 | +4.046 | -00.0336 | -00.0458 |
| -1 0 2 0 | $2\lambda-g$ | 1 1 -2 | +1.978 | -19.175 | +11.0971 |
| 0 0 2 0 | 2λ | 2 0 -2 | +4.0306 | -00.0388 | +11.0942 |
| 1 0 2 0 | $2\lambda+g$ | 3 -1 -2 | +6.083 | +19.098 | +11.0913 |
| 0 0 0 2 | $2\lambda'$ | 0 0 -2 | +0.015 | - 0.005 | +11.140 |

TABLE XLVIII.
LUNAR a-COEFFICIENTS FOR a , e , AND γ .

| Arguments. | | ap | aq | $\frac{1}{2}ak$ | ep | eq | $\frac{1}{2}ek$ | gp | gq | $\frac{1}{2}gk$ |
|----------------------------|----------------------|----------------------|---------------------|----------------------|---------------------|---------------------|---------------------|----------|-----------------|-----------------|
| g, g', λ, λ' | l, π, θ, g' | | | | | | | | | |
| 0 0 0 0 | 0 0 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 0 0 0 | +1 -1 0 0 | -0.032 09 | -.111 47 | -0.034 81 | -0.299 1 | -1.039 1 | -0.324 6 | +.000 05 | +.000 16 | +.000 05 |
| 2 0 0 0 | +2 -2 0 0 | -0.005 13 | +.001 97 | -0.004 99 | -0.047 84 | +0.018 37 | -0.046 50 | +.000 01 | 0 | +.000 01 |
| -1 1 0 0 | -1 +1 0 +1 | +0.000 13 | -.000 73 | +0.000 08 | +0.001 24 | -0.006 79 | +0.000 77 | 0 | 0 | 0 |
| 1 1 0 0 | +1 -1 0 +1 | -0.001 39 | +.000 56 | -0.001 38 | -0.012 92 | +0.005 26 | -0.012 82 | 0 | 0 | 0 |
| -1 0 2 0 | +1 +1 -2 0 | -0.000 04 | -.000 32 | +0.000 10 | +0.000 38 | +0.003 17 | -0.000 96 | -.000 22 | -.001 78 | +.000 56 |
| 0 0 2 0 | +2 0 -2 0 | -0.000 77 | +.024 10 | -0.000 77 | +0.000 01 | -0.000 23 | +0.000 01 | -.002 11 | +.066 34 | -.002 11 |
| 1 0 2 0 | +3 -1 -2 0 | -0.000 06 | +.001 99 | -0.000 06 | -0.000 19 | +0.006 30 | -0.000 19 | -.000 11 | +.003 66 | -.000 11 |
| -2 0 2 -2 | 0 +2 0 -2 | -0.000 235 | -.000 054 | -0.000 216 | -0.149 20 | -0.034 28 | -0.137 90 | -.000 16 | -.000 04 | -.000 14 |
| -1 0 2 -2 | +1 +1 0 -2 | -0.162 43 | -.018 53 | -0.162 95 | +1.562 6 | +0.178 3 | +1.567 5 | +.003 50 | +.000 40 | +.003 51 |
| 0 0 2 -2 | +2 0 0 -2 | +1.994 9 | -.028 26 | +1.994 70 | -0.016 56 | +0.000 23 | -0.016 56 | -.022 58 | +.000 32 | -.022 58 |
| 1 0 2 -2 | +3 +1 0 -2 | +0.166 0 | -.001 28 | +0.166 0 | +0.519 98 | -0.004 01 | +0.519 98 | -.001 32 | +.000 01 | -.001 32 |
| 0 1 2 -2 | +2 0 0 -1 | -0.006 43 | +.000 06 | -0.006 41 | +0.000 05 | $35 \div 10^8$ | +0.000 05 | +.000 07 | $687 \div 10^8$ | +.000 07 |
| 0 -1 2 -2 | 2 0 0 -3 | +0.006 51 | -.000 12 | +0.006 35 | -0.000 05 | $708 \div 10^8$ | -0.000 05 | -.000 07 | $137 \div 10^8$ | -.000 07 |
| 0 0 0 2 | 0 0 -2 +2 | +297+10 ⁷ | -63+10 ⁷ | -297+10 ⁷ | -99+10 ⁷ | +21+10 ⁷ | +99+10 ⁷ | +.022 36 | -.004 68 | -.022 06 |

TABLE XLIX.
LUNAR L-COEFFICIENTS FOR l , π , AND θ .

| Arguments. | | L' | L'' | L_4 | $2eP'$ | $2eP''$ | eP_4 | $2\gamma R'$ | $2\gamma R''$ | γR_4 |
|----------------------------|----------------------|------------|------------|------------|------------|------------|------------|--------------|---------------|--------------|
| g, g', λ, λ' | l, π, θ, g' | | | | | | | | | |
| 0 0 0 0 | 0 0 0 0 | -0.082 04 | +2.004 31 | | -0.116 35 | -0.181 96 | | -0.003 85 | +.135 12 | |
| 1 0 0 0 | +1 -1 0 0 | -0.123 05 | -0.199 14 | -0.275 07 | +0.595 03 | +2.056 09 | +0.640 4 | -.002 46 | -.012 85 | -.002 50 |
| 2 0 0 0 | +2 -2 0 0 | -0.010 05 | +0.002 48 | -0.019 74 | +0.077 07 | +0.057 30 | +0.072 8 | -.000 01 | | -.000 04 |
| -1 1 0 0 | -1 +1 0 4 | -0.000 32 | -0.003 16 | +0.002 44 | 0 | +0.006 73 | | | | |
| 0 1 0 0 | 0 0 0 +1 | -0.005 454 | +0.001 241 | -0.014 128 | -0.004 743 | -0.001 172 | -0.006 53 | -.000 073 | +.000 041 | -.000 12 |
| 1 1 0 0 | +1 -1 0 +1 | -0.005 59 | +0.002 42 | -0.010 86 | +0.026 51 | -0.000 39 | +0.027 0 | | | |
| -1 0 2 0 | +1 +1 -2 0 | -0.000 09 | +0.000 11 | +0.000 38 | | +0.024 25 | | | +.014 50 | |
| 0 0 2 0 | +2 0 -2 0 | -0.000 99 | +0.017 75 | -0.002 03 | +0.000 02 | +0.003 15 | +0.000 02 | +.004 33 | -.137 90 | +.003 78 |
| 1 0 2 0 | +3 -1 -2 0 | -0.000 16 | +0.001 05 | -0.000 32 | | -0.008 24 | | | -.004 90 | |
| -2 0 2 -2 | 0 +2 +0 -2 | +0.013 67 | +0.006 84 | +0.023 51 | -0.298 75 | -0.069 08 | -0.275 19 | +.000 04 | +.000 01 | +.000 04 |
| -1 0 2 -2 | +1 +1 0 -2 | -0.302 23 | -0.070 22 | -0.612 74 | +3.117 20 | +0.360 88 | +3.117 4 | -.005 00 | -.001 36 | -.005 03 |
| 0 0 2 -2 | +2 0 0 -2 | +1.992 22 | -0.076 97 | +3.984 14 | +0.298 00 | +0.022 69 | +0.298 1 | +.045 17 | -.010 28 | +.045 14 |
| 1 0 2 -2 | +3 -1 0 -2 | +0.102 62 | -0.002 34 | +0.205 24 | -1.027 38 | +0.007 90 | -1.027 3 | +.001 80 | | +.001 75 |
| 2 0 2 -2 | +4 -1 0 -2 | +0.005 12 | -0.000 11 | +0.010 24 | -0.114 62 | | -0.114 6 | +.000 01 | | +.000 01 |
| -1 1 2 -2 | +1 +1 0 -1 | -0.003 614 | -0.000 172 | -0.007 273 | +0.015 989 | | +0.015 785 | -.000 003 | | -.000 002 |
| 0 1 2 -2 | +2 0 0 -1 | -0.009 22 | +0.000 94 | -0.018 40 | +0.000 02 | | | | | |
| 1 1 2 -2 | +3 -1 0 -1 | -0.001 58 | +0.000 01 | -0.003 16 | +0.006 73 | | +0.006 3 | | | |
| -1 -1 2 -2 | +1 +1 0 -3 | +0.001 810 | -0.003 176 | +0.003 661 | -0.009 992 | +0.015 462 | -0.010 1 | +.000 002 | -.000 003 | +.000 001 |
| 0 -1 2 -2 | 2 0 0 -3 | +0.009 43 | -0.004 14 | +0.018 66 | -0.000 02 | +0.000 01 | -0.000 02 | | | |
| 1 -1 2 -2 | 3 -1 0 -3 | +0.002 27 | -0.000 15 | +0.004 54 | -0.008 927 | -0.004 64 | -0.008 8 | | | |
| -1 0 0 2 | -1 +1 -2 +2 | -0.000 11 | -0.000 07 | -0.000 22 | | | | | | |
| 0 0 0 2 | 0 0 -2 +2 | +0.005 65 | -0.001 69 | -0.011 29 | -0.000 23 | +0.000 04 | +0.000 22 | -.048 75 | +.008 85 | +.048 80 |
| 1 0 0 -2 | +1 -1 -2 +2 | -0.000 37 | -0.000 95 | +0.000 90 | | | | | | |
| -2 -1 2 -2 | | -0.000 019 | +0.000 130 | -0.000 207 | +0.000 915 | -0.002 766 | +0.002 976 | 0 | 0 | 0 |
| -2 1 2 -2 | | +0.000 101 | -0.000 006 | +0.000 224 | -0.002 797 | -0.000 042 | -0.002 966 | 0 | 0 | 0 |

§ 72. From these two tables the four coefficients for each element are formed by the following computation, an adaptation of (46) to (51)

The inequalities of e have received the factor 2, and those of π the factor $2e$ in order to transform them into the principal terms of the true longitude without further multiplication.

Two other points which may be recalled are these: (1) We use k instead of κ_4 in the formulæ; (2) it is to be recalled that C'_c and C'_s contain only $\frac{1}{2}C$, as that symbol is used in Part I.

Element α

$$\begin{aligned} a_1 &= K'_s'ap - C'_s'ag & a_2 &= -K'_c'ap + C'_c'ag \\ h_{\alpha,c} &= \frac{1}{2}D'_c'ak + a_1 & h_{\alpha,c}' &= \frac{1}{2}D'_c'ak - a_1 \\ h_{\alpha,s} &= a_2 + \frac{1}{2}D'_s'ak & h_{\alpha,s}' &= a_2 - \frac{1}{2}D'_s'ak \end{aligned}$$

Element e

$$\begin{aligned} e_1 &= 2K'_s'ep - 2C'_s'eq & e_2 &= -2K'_c'ep + 2C'_c'eq \\ 2h_{e,c} &= D'_c'ek + e_1 & 2h_{e,c}' &= D'_c'ek - e_1 \\ 2h_{e,s} &= e_2 + D'_s'ek & 2h_{e,s}' &= e_2 - D'_s'ek \end{aligned}$$

Element γ

$$\begin{aligned} \gamma_1 &= 2K'_s'gp - 2C'_s'gq & \gamma_2 &= -2K'_c'gp + 2C'_c'gq \\ 2h_{\gamma,c} &= D'_c'gk + \gamma_1 & 2h_{\gamma,c}' &= D'_c'gk - \gamma_1 \\ 2h_{\gamma,s} &= \gamma_2 + D'_s'gk & 2h_{\gamma,s}' &= \gamma_2 - D'_s'gk \end{aligned}$$

Element l_0

$$\begin{aligned} \lambda_1 &= K'_c'L' - C'_c'L'' & \lambda_2 &= K'_s'L' - C'_s'L'' \\ h_{l,c} &= \lambda_1 - \frac{1}{2}D'_s'L_4 & h_{l,c}' &= \lambda_1 + \frac{1}{2}D'_s'L_4 \\ h_{l,s} &= \frac{1}{2}D'_c'L_4 + \lambda_2 & h_{l,s}' &= \frac{1}{2}D'_c'L_4 - \lambda_2 \end{aligned}$$

Element π_0

$$\begin{aligned} \pi_1 &= 2K'_c'eP' - 2C'_c'eP'' & \pi_2 &= 2K'_s'eP' - 2C'_s'eP'' \\ 2eh_{\pi,c} &= \pi_1 - D'_s'eP_4 & 2eh_{\pi,c}' &= \pi_1 + D'_s'eP_4 \\ 2eh_{\pi,s} &= D'_c'eP_4 + \pi_2 & 2eh_{\pi,s}' &= D'_c'eP_4 - \pi_2 \end{aligned}$$

Element θ_0

$$\begin{aligned} \theta_1 &= 2K'_c'\gamma R' - 2C'_c'\gamma R'' & \theta_2 &= 2K'_s'\gamma R' - 2C'_s'\gamma R'' \\ 2\gamma h_{\theta,c} &= \theta_1 - D'_s'\gamma R_4 & 2\gamma h_{\theta,c}' &= \theta_1 + D'_s'\gamma R_4 \\ 2\gamma h_{\theta,s} &= D'_c'\gamma R_4 + \theta_2 & 2\gamma h_{\theta,s}' &= D'_c'\gamma R_4 - \theta_2 \end{aligned}$$

In the exceptional cases when one of the constituent factors of either class, planetary or lunar, is a constant, there will be a merging of the accented and unaccented arguments and terms.

For the case $N = 0$, a , e and g all vanish, and we have

$$D_{nt}\alpha = D_{nt}e = D_{nt}\gamma = 0 \quad k = 0$$

while (49) of § 23 may be written

$$-D_{nt}I_0 = (2K'_0L'_0 - 2C'_0L''_0) \cos N_4 + (2K'_sL'_0 - 2C'_sL''_0) \sin N_4$$

We have, therefore, in this case, only to double the values of the L -coefficients for argument 0 .

In the combination of a constant planetary factor ($N_4 = 0$) with a periodic lunar factor we may use, instead of (46)

$$h_{a,s} = -2K'_0ap + 2C'_0aq$$

Then

$$\delta\alpha = -\nu h_{a,s} \cos N$$

with similar equations for e and γ , formed by writing e and g for a . We also have, instead of (51)

$$h_{l,c} = 2K'_0L' - 2C'_0L''$$

Then

$$\delta I_0 = -\nu h_{l,c} \sin N$$

with similar equations for π and θ .

As neither D nor I has a constant term, there are only cosine-terms of this class in α , e , and γ , and only sine-terms in l , π , and θ .

From these coefficients for the D_{nt} of the elements we have those for the elements themselves by multiplication by the integrating factor ν . The motion of the lunar argument is

$$in + i'\pi_1 + i''\theta_1 + jn' \equiv N$$

and that of the planetary argument

$$k'n' + kn_4 \equiv N_4$$

We compute

$$\nu = \frac{n}{N + N_4} = \frac{1}{n + n_4}$$

$$\nu' = \frac{n}{N - N_4} = \frac{1}{n - n_4}$$

Then the coefficients which we compute are

$$\begin{array}{llll} \alpha_s = \nu h_{a,c} & \alpha_c = -\nu h_{a,s} & \alpha'_s = \nu' h_{a,c}' & \alpha'_c = -\nu' h_{a,s}' \\ 2e_s = 2\nu h_{e,c} & 2e_c = -2\nu h_{e,s} & 2e'_s = 2\nu' h_{e,c}' & 2e'_c = -2\nu' h_{e,s}' \\ 2\gamma_s = 2\nu h_{\gamma,c} & 2\gamma_c = -2\nu h_{\gamma,s} & 2\gamma'_s = 2\nu' h_{\gamma,c}' & 2\gamma'_c = -2\nu' h_{\gamma,s}' \\ l_s = \frac{3}{2}\nu^2 h_{a,s} - \nu h_{l,c} = \nu(\frac{3}{2}\nu h_{a,s} - h_{l,c}) & & & \\ l_c = \frac{3}{2}\nu^2 h_{a,c} + \nu h_{l,s} = \nu(\frac{3}{2}\nu h_{a,c} + h_{l,s}) & & & \\ 2e\pi_s = -\nu \times 2eh_{\pi,c} & & & \\ 2e\pi_c = +\nu \times 2eh_{\pi,s} & & & \end{array}$$

with similar forms for θ when required,

The inequalities of the elements are then

$$\begin{aligned} \delta l &= l_c \cos(N + N_4) + l_s \sin(N + N_4) + l'_c \cos(N - N_4) + l'_s \sin(N - N_4) \\ \delta \pi &= \pi_c \quad \quad \quad + \pi_s \quad \quad \quad + \pi'_c \quad \quad \quad + \pi'_s \quad \quad \quad \\ \delta \theta &= e_c \quad \quad \quad + e_s \quad \quad \quad + e'_c \quad \quad \quad + e'_s \quad \quad \quad \end{aligned}$$

A similar computation was made for γ and θ ; but the results were unimportant in all but one of the arguments.

§ 73. The motions of the arguments from which the integrating factors ν or ν' are to be computed are the following. The sidereal motion for a Julian year is given in revolutions for the lunar, and in seconds for the planetary arguments. Then follows the ratio of each to the mean motion of the Moon.

Motions of Arguments.

| | Mot. in 365 ^d .25 | n |
|------------------------|------------------------------|--------------|
| $g; g_1 =$ | 13 ^r .255 523 | 0.991 5452 |
| $l; n =$ | 13 .368 513 | 1. |
| $\pi; \pi_1 =$ | 0 .112 990 | 0.008 4518 |
| $\theta; \theta_1 = -$ | 0 .053 765 | - 0.004 0218 |
| Venus | 2106 641 ^{''} .38 | 0.121 5913 |
| Earth | 1295 977 .43 | 0.074 8013 |
| Mars | 689 050 .9 | 0.039 7707 |
| Jupiter | 109 256 .6 | 0.006 3061 |
| Saturn | 43 996 .2 | 0.002 5394 |

The elemental inequalities computed from these formulæ are shown in tabular form on the following pages. On making the computation it was found that the coefficients for a were so minute that no terms in the parallax would need to be considered, and only in some exceptional cases, generally terms of long period, did the inequality of γ affect the longitude. The coefficients for these elements are therefore omitted in the tables of longitude elements. The given coefficients are those for the mean longitude, δl , $2\delta e$, $e\delta\pi$. It must be remembered that the accented e' and π' do not refer to solar elements, but designate only the coefficients depending upon the differences between the lunar and the planetary arguments, while the unaccented coefficients depend upon their sum.

It was also found that the inequalities of γ and θ were insensible in nearly all cases. The few terms of these elements found to be sensible are therefore given separately.

§ 74. *Terms with purely Lunar Arguments.* We here make a single computation for the combined action of all the planets. To include the effect of the indirect action, we have only to modify the values of MK , etc., as indicated in (66).

Then, from the values of the constant term already given for the four principal disturbing planets in § 54 we find

$$\begin{aligned} 10^3 \Sigma MK_0 &= + 6''.070 & 10^3 \Sigma MC_0 &= - 5''.76 \\ - 10^3 m^2 G_0 &= - 0.459 & 10^3 m^2 J_0 &= + 0.153 \\ 10^3 K_0' &= + 5.611 & 10^3 C_0' &= - 2.727 \end{aligned}$$

For the terms in question we now have, for each lunar argument

$$h_{\alpha, s} = - 11''.22ap - 5''.45aq$$

$$h_{e, s} = - 11''.22ep - 5''.45eq$$

and

$$h_{l, c} = + 11''.22L' + 5''.45L''$$

$$h_{\pi, c} = + 11''.22P' + 5''.45P''$$

the terms in γ and θ being omitted as unimportant.

The inequalities of l_0 , e , and π may now be computed as in §§ 26 and 27. The most condensed formulæ of computation are

$$\begin{aligned} 10^3 l_s &= - \nu^2(16''.8ap + 8''.2aq) - \nu(11''.2L' + 5.4L'') \\ 10^3 e\pi_s &= - \nu(11''.2eP' + 5.4eP'') \\ 10^3 e_c &= + \nu(11''.2ep + 5.4eq) \end{aligned}$$

The elemental inequalities then are

$$\delta l = l_s \sin N \quad e\delta\pi = e\pi_s \sin N \quad \delta e = e_c \cos N$$

The results of this computation for the only terms which I have found to give any appreciable result are, in units of $0''.001$;

| Arg. | $10^3 l_s$ | $10^3 e_c$ | $10^3 e\pi_s$ |
|-------------|------------|------------|---------------|
| g | 3.8 | - 9.0 | - 9.0 |
| $2D - 2g$ | + 1.5 | + 14.0 | - 13.6 |
| $2D - 2g$ | + 8.2 | + 21.6 | - 21.5 |
| $2D$ | - 22.0 | - 0.1 | - 0.9 |
| $2\lambda'$ | + 0.4 | + 2.0 | + 2.0 |

The only corrections of the true longitude to be considered are the following to the evection and variation.

$$\delta v = + 0''.036 \sin(2D - g) + 0''.021 \sin 2D.$$

§ 75. *Elemental Inequalities.* The miscellaneous inequalities of the mean longitude, the eccentricity and the perigee, as given by the preceding formulæ and data, are tabulated in the following pages.

It may be repeated that the mean longitudes, v , m , j , and s , are measured from the solar perigee.

Periodic Elemental Inequalities in Units of 0."001.

TERMS INDEPENDENT OF THE LUNAR ARGUMENTS. ($N=0$.)

| Action of Venus. | | | | | | Action of Mars. | | | | | |
|------------------|---------|-------|-------|-----------|-----------|-----------------|---------|-------|-------|-----------|-----------|
| Arg. | ν | l_s | l_c | $2e\pi_s$ | $2e\pi_c$ | Arg. | ν | l_s | l_c | $2e\pi_s$ | $2e\pi_c$ |
| v | + 8.22 | - 14 | - 1 | + 6 | 0 | M | + 25.1 | - 30 | - 1 | + 4 | - 0 |
| v-g' | + 21.37 | -831 | + 1 | +208 | 0 | M-g' | - 28.6 | - 11 | + 1 | + 7 | 0 |
| v-2g' | - 35.70 | + 56 | - 1 | 0 | - 1 | 2M-g' | +211.0 | +308 | -181 | -48 | +49 |
| 2v-2g' | + 10.69 | +324 | + 5 | -107 | - 1 | 2M-2g' | - 14.27 | -200 | 0 | +60 | 0 |
| 2v-3g' | + 53.25 | -314 | + 90 | +114 | -24 | 3M-2g' | - 33.0 | + 29 | - 31 | - 9 | +10 |
| 2v-4g' | - 17.85 | + 3 | - 4 | + 3 | 0 | 3M-3g' | - 9.5 | + 14 | 0 | - 4 | 0 |
| 3v-3g' | + 7.12 | - 51 | + 1 | + 13 | 0 | 4M-2g' | +105.5 | + 2 | + 95 | - 3 | -24 |
| 3v-4g' | + 15.25 | -173 | + 36 | + 54 | -12 | 4M-3g' | - 15.3 | + 32 | - 35 | -10 | +10 |
| 3v-5g' | -108.3 | - 48 | + 54 | + 30 | -21 | 5M-3g' | - 39.1 | + 23 | - 20 | - 1 | - 6 |
| 5v-8g' | +105 | - 15 | + 18 | + 4 | - 6 | 15M-8g' | -540.5 | + 39 | + 22 | - 9 | - 2 |
| 8v-13g' | +319.4 | + 16 | +246 | - 5 | -74 | | | | | | |

| Action of Saturn. | | | | | | Action of Jupiter. | | | | | |
|-------------------|--------|-------|-------|-----------|-----------|--------------------|--------|-------|-------|-----------|-----------|
| Arg. | ν | l_s | l_c | $2e\pi_s$ | $2e\pi_c$ | Arg. | ν | l_s | l_c | $2e\pi_s$ | $2e\pi_c$ |
| s | + 39.4 | + 48 | + 16 | - 4 | 0 | J | +158.6 | +171 | + 41 | + 41 | -57 |
| s-g' | - 13.8 | - 40 | 0 | + 11 | 0 | J-g' | - 14.6 | -652 | + 13 | +210 | - 7 |
| 2s-g' | - 14.3 | + 11 | - 1 | - 3 | 0 | J-2g' | - 7.0 | - 15 | + 4 | + 9 | - 2 |
| 2s-2g' | - 6.9 | + 8 | 0 | - 3 | 0 | 2J-g' | - 16.1 | +165 | - 52 | - 46 | -18 |
| | | | | | | 2J-2g' | - 7.30 | +208 | - 1 | - 74 | - 1 |
| | | | | | | 2J-3g' | - 4.7 | + 6 | 0 | - 3 | 0 |
| | | | | | | 3J-g' | - 17.9 | + 5 | - 24 | - 2 | - 6 |
| | | | | | | 3J-2g' | - 7.6 | - 2 | + 42 | + 1 | -15 |
| | | | | | | 3J-3g' | - 4.9 | + 9 | + 1 | - 6 | + 1 |

LUNAR ARGUMENT $N=g$.

| Planetary Argument. | ν | ν' | l_s | l_c | l'_s | l'_c | $2e_s$ | $2e_c$ | $2e'_s$ | $2e'_c$ | $2e\pi_s$ | $2e\pi_c$ | $2e\pi'_s$ | $2e\pi'_c$ |
|---------------------|---------|---------|-------|-------|--------|--------|--------|--------|---------|---------|-----------|-----------|------------|------------|
| v-g' | +0.9631 | +1.0585 | + 1 | -0 | +16 | 0 | 0 | -13 | 0 | -63 | -13 | 0 | -63 | 0 |
| 2v-3g' | +0.9898 | +1.0281 | - 4 | +1 | + 6 | + 1 | + 1 | + 5 | + 5 | -22 | + 5 | - 1 | -22 | - 5 |
| 2v-2g' | +0.9216 | +1.1137 | - 1 | 0 | -22 | 0 | 0 | + 1 | 0 | +77 | + 1 | 0 | +77 | 0 |
| 3v-5g' | +1.0180 | +0.9993 | + 1 | +1 | + 1 | + 1 | + 3 | + 5 | + 3 | - 3 | + 5 | - 3 | - 3 | - 3 |
| 3v-4g' | +0.9460 | +1.0800 | 0 | 0 | + 4 | 0 | 0 | - 5 | + 4 | -23 | - 5 | 0 | -23 | - 4 |
| 3v-3g' | +0.8814 | +1.1750 | + 3 | 0 | - 1 | 0 | 0 | -13 | 0 | + 1 | -13 | 0 | + 1 | 0 |
| 2M-2g' | +1.0853 | +0.9420 | - 6 | 0 | + 1 | 0 | 0 | +29 | 0 | + 5 | +29 | 0 | + 5 | 0 |
| 2M-g' | +1.0038 | +1.0134 | + 2 | 0 | - 2 | - 7 | - 6 | + 9 | - 1 | 0 | + 7 | + 5 | + 9 | + 5 |
| J-g' | +1.0834 | +0.9434 | - 23 | 0 | 0 | 0 | + 2 | +98 | - 1 | +10 | +97 | - 2 | +11 | 0 |
| J | +1.0022 | +1.0150 | 0 | +5 | 0 | +13 | + 5 | 0 | +15 | - 2 | 0 | -13 | - 2 | -15 |
| 2J-2g' | +1.1703 | +0.8861 | +150 | 0 | +40 | 0 | 0 | -54 | 0 | -21 | -54 | 0 | -21 | 0 |
| 2J-g' | +1.0761 | +0.9490 | + 40 | -1 | 00 | - 8 | - 8 | -21 | + 1 | - 3 | -21 | + 8 | - 3 | - 1 |

LUNAR ARGUMENT $N = 2D - 2g = 2\pi - 2g'$ (EVECTION-TERMS).

| Planetary Argument. | ν | ν' | l_s | l_c | l'_s | l'_c | $2e_s$ | $2e_c$ | $2e'_s$ | $2e'_c$ | $2e\pi_s$ | $2e\pi_c$ | $2e\pi'_s$ | $2e\pi'_c$ |
|---------------------|----------|-----------|-------|-------|--------|--------|--------|--------|---------|---------|-----------|-----------|------------|------------|
| $v-g'$ | - 11.64 | - 5.572 | - 1 | 0 | + 6 | 0 | 0 | - 19 | 0 | + 101 | + 18 | 0 | - 101 | 0 |
| $2v-3g'$ | - 8.779 | - 6.602 | - 2 | 0 | + 3 | + 1 | - 7 | - 30 | - 11 | + 50 | + 30 | - 8 | - 51 | - 11 |
| $2v-2g'$ | - 25.57 | - 4.419 | + 9 | 0 | - 6 | 0 | 0 | + 134 | - 1 | - 106 | - 130 | 0 | + 107 | - 1 |
| $3v-5g'$ | - 7.046 | - 8.100 | - 1 | + 1 | + 1 | + 1 | - 12 | - 15 | - 10 | + 12 | + 15 | - 12 | - 13 | - 11 |
| $3v-4g'$ | - 14.90 | - 5.045 | 0 | 0 | + 2 | 0 | 0 | - 1 | - 7 | + 33 | 0 | - 1 | - 33 | - 7 |
| $3v-3g'$ | + 129.9 | - 3.66 | + 72 | 0 | 0 | 0 | - 2 | - 661 | 0 | - 7 | + 659 | - 2 | + 7 | 0 |
| $6v-8g'$ | - 625.0 | - 3.79 | + 50 | - 37 | 0 | 0 | + 49 | + 64 | 0 | 0 | - 64 | + 49 | 0 | 0 |
| $5v-8g'$ | + 737.7 | - 3.43 | 0 | 0 | 0 | 0 | - 5 | - 24 | 0 | 0 | + 24 | - 5 | 0 | 0 |
| $m-g'$ | - 5.962 | - 10.24 | 0 | 0 | 0 | 0 | 0 | - 5 | 0 | + 4 | + 5 | 0 | - 4 | 0 |
| $2m-2g'$ | - 4.932 | - 15.96 | - 2 | 0 | + 1 | 0 | + 1 | - 42 | 0 | + 15 | + 42 | 0 | - 15 | 0 |
| $2m-g'$ | - 7.815 | - 7.276 | + 1 | - 2 | - 5 | - 2 | + 17 | + 25 | + 19 | - 25 | - 25 | + 17 | + 25 | + 19 |
| $3m-3g'$ | - 4.205 | - 36.23 | 0 | 0 | 0 | 0 | 0 | + 3 | 0 | + 6 | - 3 | 0 | - 6 | 0 |
| $3m-2g'$ | - 6.135 | - 9.766 | 0 | 0 | 0 | 0 | + 6 | + 6 | + 4 | - 4 | - 6 | + 6 | + 4 | + 5 |
| $4m-3g'$ | - 5.050 | - 14.84 | 0 | 0 | 0 | 0 | + 7 | + 7 | + 4 | - 3 | - 7 | + 7 | + 4 | + 5 |
| $4m-2g'$ | - 8.116 | - 7.034 | 0 | 0 | 0 | 0 | + 9 | + 1 | - 11 | - 1 | - 1 | - 10 | + 1 | - 11 |
| $15m-8g'$ | - 7.429 | - 7.645 | 0 | 0 | 0 | 0 | - 1 | + 3 | - 1 | - 3 | - 1 | - 29 | 0 | 0 |
| $6m-5g'$ | - 3.73 | + 370.4 | 0 | 0 | - 1 | - 8 | - 1 | 0 | - 22 | + 29 | + 0 | - 1 | - 29 | - 23 |
| $J-2g'$ | - 3.6232 | + 94.3396 | 0 | 0 | 0 | - 1 | - 1 | - 9 | - 10 | + 15 | + 9 | - 1 | - 16 | - 9 |
| $J-g'$ | - 4.9702 | - 15.5763 | - 8 | 0 | + 3 | 0 | - 5 | - 151 | 0 | + 54 | + 151 | - 5 | - 53 | 0 |
| J | - 7.9114 | - 7.1942 | 0 | + 2 | 0 | + 3 | - 44 | - 1 | - 46 | + 7 | + 1 | - 44 | - 7 | - 46 |
| $2J-3g'$ | - 2.9028 | + 12.6422 | 0 | 0 | 0 | 0 | 0 | + 3 | - 1 | - 1 | - 3 | 0 | 0 | - 1 |
| $2J-2g'$ | - 3.7078 | + 232.720 | + 3 | 0 | + 256 | + 1 | + 1 | + 54 | + 5 | - 1158 | - 54 | + 1 | + 1164 | + 3 |
| $2J-g'$ | - 5.1308 | - 14.1844 | + 2 | - 1 | - 1 | 0 | + 13 | + 30 | + 6 | - 12 | - 31 | + 13 | + 15 | + 6 |
| $3J-3g'$ | - 2.9568 | + 13.7363 | + 1 | 0 | + 1 | 0 | + 11 | + 13 | 0 | + 22 | - 13 | - 1 | - 21 | 0 |
| $3J-2g'$ | - 3.7965 | - 497.760 | 0 | + 1 | - 8 | - 258 | - 11 | 0 | + 429 | - 14 | 0 | - 11 | + 15 | + 431 |
| $3J-g'$ | - 5.3022 | - 13.0208 | 0 | 0 | 0 | 0 | - 4 | + 1 | - 2 | 0 | - 1 | - 4 | + 1 | - 2 |

LUNAR ARGUMENT $N = 2D - g = g' + 2\pi - 2g'$.

| Planetary Argument. | ν | ν' | l_s | l_c | l'_s | l'_c | $2e_s$ | $2e_c$ | $2e'_s$ | $2e'_c$ | $2e\pi_s$ | $2e\pi_c$ | $2e\pi'_s$ | $2e\pi'_c$ |
|---------------------|--------|--------|-------|-------|--------|--------|--------|--------|---------|---------|-----------|-----------|------------|------------|
| $v-g'$ | 1.1042 | 1.231 | - 6 | 0 | + 47 | 0 | 0 | - 33 | 0 | + 239 | + 32 | 0 | - 237 | 0 |
| $2v-3g'$ | 1.1395 | 1.190 | - 10 | + 4 | + 20 | + 1 | - 10 | - 48 | - 20 | + 100 | + 47 | - 11 | - 99 | - 21 |
| $2v-2g'$ | 1.0500 | 1.307 | + 10 | 0 | - 69 | 0 | 0 | + 75 | - 3 | - 342 | - 74 | 0 | + 341 | - 3 |
| $3v-5g'$ | 1.1770 | 1.152 | - 4 | + 5 | + 4 | + 4 | - 21 | - 28 | - 16 | + 21 | + 27 | - 22 | - 20 | - 17 |
| $3v-4g'$ | 1.0828 | 1.261 | - 1 | 0 | + 18 | + 5 | - 1 | - 5 | - 19 | + 89 | + 5 | - 1 | - 89 | - 19 |
| $3v-3g'$ | 1.008 | 1.392 | + 10 | 0 | - 7 | 0 | + 1 | + 57 | - 1 | - 35 | - 55 | + 1 | + 35 | - 1 |
| $2m-2g'$ | 1.2679 | 1.0765 | - 23 | 0 | + 3 | 0 | + 3 | - 116 | 0 | + 17 | + 121 | 0 | - 16 | 0 |
| $2m-g'$ | 1.1581 | 1.1708 | + 9 | - 6 | - 9 | - 7 | + 30 | + 42 | + 35 | - 46 | - 42 | + 29 | + 44 | + 34 |
| $4m-3g'$ | 1.2602 | 1.0821 | + 2 | - 2 | 0 | 0 | + 20 | + 19 | + 4 | - 3 | - 19 | + 19 | + 3 | + 4 |
| $J-2g'$ | 1.3976 | 0.9979 | + 9 | - 6 | - 9 | 0 | - 5 | - 38 | + 1 | - 1 | + 36 | - 5 | 0 | + 1 |
| $J-g'$ | 1.2653 | 1.0784 | - 81 | 0 | + 10 | 0 | - 13 | - 416 | 0 | + 59 | + 415 | - 13 | - 59 | 0 |
| J | 1.1559 | 1.1730 | - 1 | + 16 | + 1 | + 16 | - 74 | - 2 | - 84 | + 14 | + 1 | - 74 | - 13 | - 84 |
| $2J-3g'$ | 1.5456 | 0.9340 | + 3 | 0 | 0 | 0 | - 2 | + 19 | + 1 | 0 | - 19 | - 2 | 0 | + 1 |
| $2J-2g'$ | 1.3854 | 1.0042 | + 44 | 0 | + 8 | 0 | + 3 | + 215 | 0 | + 45 | - 211 | + 3 | - 45 | 0 |
| $2J-g'$ | 1.2553 | 1.0858 | + 15 | - 5 | - 4 | - 4 | + 34 | + 81 | + 8 | - 13 | - 81 | + 34 | + 13 | + 8 |
| $3J-3g'$ | 1.5307 | 0.9395 | + 17 | 0 | - 3 | 0 | - 3 | + 73 | 0 | - 19 | - 72 | - 3 | + 18 | 0 |
| $3J-2g'$ | 1.3734 | 1.0106 | 0 | + 10 | 0 | - 1 | - 42 | - 3 | + 7 | 0 | + 3 | - 42 | 0 | + 7 |
| $3J-g'$ | 1.2455 | 1.0933 | 0 | 0 | 0 | 0 | - 10 | + 2 | - 2 | 0 | - 2 | - 10 | 0 | - 2 |

LUNAR ARGUMENT $2D = 2g + 2\pi - 2g'$.

| Planetary Argument. | ν | ν' | l_s | l_o | l'_s | l'_o | $2e_s$ | $2e_o$ | $2e'_s$ | $2e'_o$ | $2e\pi_s$ | $2e\pi_o$ | $2e\pi'_s$ | $2e\pi'_o$ |
|---------------------|-------|--------|-------|-------|--------|--------|--------|--------|---------|---------|-----------|-----------|------------|------------|
| $V-g'$ | +527 | +554 | + 21 | 0 | -122 | 0 | 0 | 0 | 0 | -1 | + 2 | 0 | -10 | 0 |
| $2V-2g'$ | +514 | +569 | - 43 | 0 | +172 | 0 | 0 | -1 | 0 | +2 | - 4 | 0 | +14 | 0 |
| $2M-2g'$ | +562 | +521 | + 59 | + 2 | - 11 | 0 | 0 | +1 | 0 | -1 | + 5 | 0 | - 1 | 0 |
| $J-g'$ | +561 | +521 | +212 | - 6 | - 36 | 0 | 0 | +2 | 0 | -1 | +17 | 0 | - 3 | 0 |
| J | +539 | +542 | + 1 | -39 | - 7 | -45 | +1 | 0 | +1 | 0 | + 1 | -4 | - 1 | -4 |
| $2J-2g'$ | +584 | +503 | -106 | + 2 | - 23 | 0 | 0 | -2 | 0 | 0 | - 9 | 0 | - 3 | 0 |

LUNAR ARGUMENT $2D + g = 3g + 2\pi - 2g'$.

| Planetary Argument. | ν | ν' | l_s | l_o | l'_s | l'_o | $2e_s$ | $2e_o$ | $2e'_s$ | $2e'_o$ | $2e\pi_s$ | $2e\pi_o$ | $2e\pi'_s$ | $2e\pi'_o$ |
|---------------------|-------|--------|-------|-------|--------|--------|--------|--------|---------|---------|-----------|-----------|------------|------------|
| $V-g'$ | +346 | +358 | +1 | 0 | -4 | 0 | 0 | - 3 | 0 | +22 | - 4 | 0 | +23 | 0 |
| $2V-2g'$ | +341 | +364 | -1 | 0 | +6 | 0 | 0 | + 8 | 0 | -31 | + 8 | 0 | -31 | 0 |
| $2M-2g'$ | +361 | +343 | +2 | 0 | -1 | 0 | 0 | -11 | 0 | + 2 | -11 | 0 | + 2 | 0 |
| $J-g'$ | +361 | +344 | +7 | 0 | -1 | 0 | -1 | -39 | 0 | + 7 | -38 | +1 | + 7 | 0 |
| $2J-2g'$ | +370 | +336 | -3 | 0 | -1 | 0 | 0 | +18 | 0 | + 5 | +18 | 0 | + 5 | 0 |

LUNAR ARGUMENT $2\lambda - 2D$.

| | γ_s | γ_o | γ'_s | γ'_o | | γ_s | γ_o | γ'_s | γ'_o |
|----------|------------|------------|-------------|-------------|----------|------------|------------|-------------|-------------|
| $V-g'$ | 0 | +13 | 0 | - 5 | $4M-3g'$ | -1 | - 1 | -1 | + 1 |
| $2V-3g'$ | +1 | + 7 | +1 | - 4 | $4M-2g'$ | +1 | 0 | +1 | +14 |
| $2V-2g'$ | 0 | -14 | 0 | +17 | $J-2g'$ | -1 | 0 | 0 | - 1 |
| $3V-4g'$ | +1 | + 4 | 0 | - 1 | $J-g'$ | 0 | +11 | +1 | -19 |
| $3V-5g'$ | +1 | + 2 | +2 | - 2 | J | +6 | + 1 | +6 | 0 |
| $4V-4g'$ | 0 | 0 | 0 | -24 | $2J-3g'$ | 0 | 0 | 0 | 0 |
| $M-g'$ | 0 | + 1 | 0 | - 1 | $2J-2g'$ | 0 | +25 | 0 | + 7 |
| $2M-2g'$ | 0 | + 3 | 0 | - 5 | $2J-g'$ | -1 | - 2 | -2 | + 4 |
| $2M-g'$ | 0 | - 3 | 0 | - 4 | $3J-3g'$ | 0 | - 6 | 0 | + 2 |
| $3M-3g'$ | 0 | 0 | 0 | 0 | $3J-2g'$ | -3 | 0 | +1 | 0 |
| $3M-2g'$ | -1 | - 1 | -1 | + 1 | $3J-g'$ | 0 | 0 | +1 | 0 |

§ 76. *Reduction to inequalities of true longitude and collection of results.*

To complete the work it is necessary to transform the elemental inequalities into inequalities of the coördinates. As already remarked, the parallax appears to contain no sensible terms arising from the action of the planets; only inequalities of longitude and latitude are therefore considered. In the case of terms of very long period the transformation to true longitude is unnecessary, because these terms can best be used and compared as elemental inequalities. A precise classification can not, however, be made between the terms which are to be transformed and those which are not. What has actually been done is to retain as elemental inequalities those depending on the longitude of the Moon's node, because though they may

ultimately be transformed for use into the inequalities of the coördinates, they are to be combined with terms arising from the compression of the Earth having the same argument. The two Venus-terms of very long period have not been transformed because, as already remarked, they can be most conveniently applied to the elements. To transform the other terms put δv , the perturbations in longitude in orbit. Then

$$v = l + 2e \sin g + \frac{5}{4}e^2 \sin 2g$$

$$\delta v = \delta l + 2\delta e \sin g + \frac{5}{2}e\delta e \sin 2g + 2e\delta g \cos g + \frac{5}{2}e^2\delta g \cos 2g$$

Substituting

$$\delta l = l_c \cos G + l_s \sin G \quad \delta \pi = \pi_c \cos G + \pi_s \sin G \quad \delta e = e_c \cos G + e_s \sin G$$

$$\delta l - \delta \pi = \delta g = g_c \cos G + G_s \sin G$$

we shall have

$$\begin{aligned} \delta v &= \delta l + 2e_s \sin G \sin g + 2e_c \cos G \sin g \\ &\quad + 2eg_c \cos G \cos g + 2eg_s \sin G \cos g \\ &\quad + \frac{5}{2}ee_s \sin G \sin 2g + \frac{5}{2}ee_c \cos G \sin 2g \\ &\quad + \frac{5}{2}e^2g_c \cos G \cos 2g + \frac{5}{2}e^2g_s \sin G \cos 2g \\ &= \delta l - (e_s - eg_c) \cos (G + g) + (e_c + eg_s) \sin (G + g) \\ &\quad + (e_s + eg_c) \cos (G - g) - (e_c - eg_s) \sin (G - g) \\ &\quad - \frac{5}{4}e(e_s - eg_c) \cos (G + 2g) + \frac{5}{4}e(e_c + eg_s) \sin (G + 2g) \\ &\quad + \frac{5}{4}e(e_s + eg_c) \cos (G - 2g) - \frac{5}{4}e(e_c - eg_s) \sin (G - 2g) \end{aligned}$$

In nearly or quite all cases we may drop terms of the second order in e and use

$$\begin{aligned} \delta v &= l_c \cos G + l_s \sin G + [e(l_c - \pi_c) - e_s] \cos (G + g) + [e(l_s - \pi_s) + e_s] \sin (G + g) \\ &\quad + [e(l_c - \pi_c) + e_s] \cos (G - g) + [e(l_s - \pi_s) - e_s] \sin (G - g) \end{aligned}$$

The subsequent processes are so simple and familiar as to scarcely need statement. All terms of δv depending on the same argument are combined into two, one depending on the sine, the other on the cosine of the argument. Their values are shown for each argument in the following table. The two terms are then combined into a monomial satisfying the equation

$$v_s \sin G + v_c \cos G = \delta v \sin (G + A)$$

Terms of which the coefficient δv was less than $0''.003$, have generally, but not always, been dropped. It will be seen that even exceeding this limit there are more than 150 periodic inequalities. These are so arranged that any one argument can, it is hoped, readily be found on a system which will be evident by a little examination.

The constituents of the arguments, including π , are all measured from the Earth's perihelion ($\pi = 99^\circ.5$). The secular variations of the coefficients of the periodic terms are omitted, because they can better be derived by varying the eccentricity of the Earth's orbit in the expressions for the inequalities due to the Sun's action.

PERIODIC INEQUALITIES OF THE TRUE LONGITUDE.

ACTION OF VENUS.

| Argument. | v_c | v_s | δv | A | Argument. | v_c | v_s | δv | A |
|----------------|-------|-------|------------|-------|------------------|-------|-------|------------|-------|
| $v-2g'$ | -.001 | +.055 | .055 | 359.0 | $g+2\pi-3v+g'$ | .000 | -.014 | .014 | 180.0 |
| $v-g'$ | +.001 | -.882 | .882 | 179.9 | $g+2\pi-3v+2g'$ | +.012 | +.051 | .053 | 13.2 |
| v | -.000 | -.014 | .014 | 184.0 | $g+2\pi-3v+3g'$ | +.014 | +.016 | .021 | 41.2 |
| $2v-4g'$ | -.004 | +.003 | .005 | 306.8 | $g+2\pi-2v$ | +.001 | -.174 | .174 | 180.0 |
| $2v-3g'$ | +.096 | -.340 | .354 | 164.3 | $g+2\pi-2v+g'$ | +.011 | +.070 | .071 | 9.0 |
| $2v-2g'$ | +.005 | +.401 | .401 | 0.7 | $g+2\pi-v-g'$ | .000 | +.146 | .146 | 0.0 |
| $3v-5g'$ | +.060 | -.056 | .082 | 133.0 | $g+2\pi+v-3g'$ | .000 | -.025 | .025 | 180.0 |
| $3v-4g'$ | +.040 | -.191 | .197 | 168.3 | $g+2\pi+2v-5g'$ | +.011 | -.040 | .041 | 164.5 |
| $3v-3g'$ | +.001 | -.037 | .037 | 178.4 | $g+2\pi+2v-4g'$ | .000 | +.142 | .142 | 0.0 |
| $5v-8g'$ | +.018 | -.015 | .023 | 129.8 | $g+2\pi+3v-7g'$ | +.017 | -.019 | .026 | 138.2 |
| $g-5v+8g'$ | +.004 | +.003 | .005 | 53.2 | $g+2\pi+3v-5g'$ | +.002 | -.646 | .646 | 179.8 |
| $g-3v+3g'$ | .000 | +.008 | .008 | 0.0 | $g+2\pi+5v-8g'$ | +.005 | -.024 | .025 | 168.3 |
| $g-3v+4g'$ | +.008 | +.040 | .041 | 11.3 | $g+2\pi+6v-10g'$ | -.051 | +.066 | .083 | 322.3 |
| $g-3v+5g'$ | +.015 | +.018 | .023 | 39.8 | | | | | |
| $g-2v+2g'$ | +.001 | -.093 | .093 | 180.0 | $2g+2\pi-3v+g'$ | .000 | -.035 | .035 | 180.0 |
| $g-2v+3g'$ | +.018 | +.080 | .082 | 12.6 | $2g+2\pi-3v+2g'$ | +.019 | +.090 | .092 | 11.9 |
| $g-v$ | .000 | -.004 | .004 | 180.0 | $2g+2\pi-3v+3g'$ | +.016 | +.020 | .026 | 38.7 |
| $g-v+g'$ | .000 | +.166 | .166 | 0.0 | $2g+2\pi-2v$ | +.003 | -.142 | .143 | 178.8 |
| $g-v+2g'$ | .000 | -.003 | .003 | 180.0 | $2g+2\pi-2v+g'$ | +.020 | +.100 | .102 | 11.3 |
| $g+v-2g'$ | .000 | +.003 | .003 | 0.0 | $2g+2\pi-v-g'$ | .000 | +.096 | .096 | 0.0 |
| $g+v-g'$ | .000 | -.149 | .149 | 180.0 | $2g+2\pi+v-3g'$ | .000 | -.008 | .008 | 180.0 |
| $g+v$ | .000 | -.004 | .004 | 180.0 | $2g+2\pi+2v-5g'$ | +.010 | -.048 | .049 | 168.3 |
| $g+2v-3g'$ | +.018 | -.078 | .080 | 167.0 | $2g+2\pi+2v-4g'$ | .000 | +.024 | .024 | 0.0 |
| $g+2v-2g'$ | +.001 | +.071 | .071 | 0.6 | $2g+2\pi+3v-7g'$ | +.022 | -.027 | .035 | 140.8 |
| $g+3v-5g'$ | +.015 | -.016 | .022 | 136.9 | $2g+2\pi+3v-6g'$ | +.001 | -.005 | .005 | 168.7 |
| $g+3v-4g'$ | +.008 | -.036 | .037 | 167.5 | $2g+2\pi+3v-5g'$ | -.001 | +.056 | .056 | 359.0 |
| $g+3v-3g'$ | .000 | -.006 | .006 | 180.0 | | | | | |
| $g+5v-8g'$ | +.004 | -.003 | .005 | 126.8 | $3g+2\pi-2v$ | .000 | +.009 | .009 | 0.0 |
| $2\pi-2v$ | .000 | -.009 | .009 | 180.0 | $3g+2\pi-v-g'$ | .000 | -.006 | .006 | 180.0 |
| $2\pi-2v+g'$ | +.001 | +.003 | .003 | 18.4 | | | | | |
| $2\pi-v-g'$ | .000 | +.007 | .007 | 0.0 | $4g+2\pi-2v$ | .000 | +.003 | .003 | 0.0 |
| $2\pi+2v-4g'$ | .000 | +.008 | .008 | 0.0 | $4g+2\pi-v-g'$ | .000 | -.002 | .002 | 180.0 |
| $2\pi+3v-5g'$ | .000 | +.072 | .072 | 0.0 | | | | | |
| $2\pi+6v-10g'$ | -.037 | +.050 | .062 | 323.5 | $2\pi-g+3v-5g'$ | .000 | +.003 | .003 | 0.0 |
| | | | | | $2\pi-g+6v-10g'$ | -.002 | +.002 | .003 | 315.0 |

ACTION OF MARS.

| Argument. | v_c | v_s | δv | A | Argument. | v_c | v_s | δv | A |
|------------|-------|-------|------------|-------|------------------|-------|-------|------------|-------|
| M-g' | +.001 | -.011 | .011 | 174.3 | $2\pi-2M-g'$ | .000 | +.002 | .002 | 0.0 |
| M | -.001 | -.030 | .030 | 181.9 | $2\pi-2M-4g'$ | .000 | -.004 | .004 | 180.0 |
| 2M-2g' | .000 | -.224 | .224 | 180.0 | $g+2\pi-4M$ | +.011 | -.001 | .011 | 95.2 |
| 2M-g' | -.193 | +.317 | .372 | 328.7 | $g+2\pi-4M+g'$ | -.004 | -.003 | .005 | 233.2 |
| 3M-3g' | .000 | +.014 | .014 | 0.0 | $g+2\pi-3M$ | -.004 | -.004 | .006 | 225.0 |
| 3M-2g' | -.031 | +.029 | .042 | 313.1 | $g+2\pi-3M+g'$ | .000 | +.006 | .006 | 0.0 |
| 4M-3g' | -.035 | +.032 | .047 | 312.4 | $g+2\pi-2M+g'$ | -.026 | -.034 | .043 | 217.4 |
| 4M-2g' | +.095 | +.002 | .095 | 88.8 | $g+2\pi-2M$ | .000 | +.017 | .017 | 0.0 |
| 5M-3g' | -.020 | +.023 | .030 | 319.0 | $g+2\pi-M-g'$ | .000 | +.004 | .004 | 0.0 |
| $g-4M+2g'$ | +.017 | -.002 | .017 | 96.8 | $g+2\pi+M-3g'$ | .000 | -.005 | .005 | 180.0 |
| $g-4M+3g'$ | -.007 | -.007 | .010 | 225.0 | $g+2\pi+2M-4g'$ | .000 | -.066 | .066 | 180.0 |
| $g-3M+2g'$ | -.006 | -.006 | .009 | 225.0 | $g+2\pi+2M-3g'$ | -.023 | +.034 | .041 | 325.9 |
| $g-3M+3g'$ | .000 | -.003 | .003 | 180.0 | $g+2\pi+3M-5g'$ | .000 | +.003 | .003 | 0.0 |
| $g-2M+g'$ | -.035 | -.042 | .055 | 219.4 | $g+2\pi+3M-4g'$ | -.006 | +.006 | .009 | 315.0 |
| $g-2M+2g'$ | .000 | +.043 | .043 | 0.0 | $g+2\pi+4M-5g'$ | -.009 | +.009 | .013 | 315.0 |
| $g-M$ | .000 | +.003 | .003 | 0.0 | $g+2\pi+4M-4g'$ | +.009 | +.001 | .009 | 83.7 |
| $g-M+g'$ | .000 | +.004 | .004 | 0.0 | $2g+2\pi-4M+g'$ | -.004 | -.003 | .005 | 233.2 |
| $g+M-g'$ | .000 | -.004 | .004 | 180.0 | $2g+2\pi-2M-g'$ | -.035 | -.046 | .058 | 217.3 |
| $g+M$ | .000 | -.003 | .003 | 180.0 | $2g+2\pi-2M$ | .000 | +.006 | .006 | 0.0 |
| $g+2M-2g'$ | .000 | -.048 | .048 | 180.0 | $2g+2\pi+2M-4g'$ | .000 | -.050 | .050 | 180.0 |
| $g+2M-g'$ | -.036 | +.042 | .055 | 319.4 | $2g+2\pi+2M-3g'$ | -.030 | +.042 | .052 | 324.5 |
| $g+3M-2g'$ | -.006 | +.006 | .009 | 315.0 | $2g+2\pi+4M-5g'$ | -.020 | +.019 | .028 | 313.5 |
| $g+3M-3g'$ | .000 | +.003 | .003 | 0.0 | $3g+2\pi+2M-4g'$ | .000 | +.004 | .004 | 0.0 |
| $g+4M-2g'$ | +.017 | +.002 | .017 | 83.2 | | | | | |
| $g+4M-3g'$ | -.007 | +.007 | .010 | 315.0 | | | | | |

ACTION OF JUPITER.

| Argument. | v_c | v_s | δv | A | Argument. | v_c | v_s | δv | A |
|---------------|-------|-------|------------|-------|------------------|-------|--------|------------|-------|
| J-2g' | +.004 | -.015 | .016 | 165.1 | $g+2\pi-3J$ | -.445 | -.015 | .045 | 268.0 |
| $g-J-g'$ | +.015 | -.741 | .741 | 178.8 | $g+2\pi-3J+g'$ | .000 | +0.018 | 0.018 | 0.0 |
| J | +.070 | +.169 | .183 | 22.5 | $g+2\pi-2J-g'$ | -.010 | -0.016 | 0.019 | 212.0 |
| $2J-3g'$ | .000 | +.006 | .006 | 0.0 | $g+2\pi-2J$ | -.005 | -1.140 | 1.140 | 180.2 |
| $2J-2g'$ | -.001 | +.242 | .242 | 359.8 | $g+2\pi-J-2g'$ | +.062 | +0.008 | 0.062 | 82.7 |
| $2J-g'$ | -.059 | +.183 | .193 | 342.2 | $g+2\pi-J-g'$ | .000 | +0.064 | 0.064 | 0.0 |
| $3J-3g'$ | +.001 | +.009 | .009 | 6.4 | $g+2\pi-J$ | +.010 | +0.015 | 0.018 | 33.7 |
| $3J-2g'$ | +.042 | -.002 | .042 | 177.2 | $g+2\pi+J-4g'$ | +.001 | -0.018 | 0.018 | 176.8 |
| $3J-g'$ | -.024 | +.005 | .024 | 281.8 | $g+2\pi+J-3g'$ | +.004 | -0.230 | 0.230 | 179.0 |
| $g-3J+g'$ | +.002 | -.002 | .003 | 135.0 | $g+2\pi+J-2g'$ | +.060 | -0.003 | 0.060 | 92.9 |
| $g-3J+2g'$ | +.010 | .000 | .010 | 90.0 | $g+2\pi+2J-4g'$ | +.001 | +0.098 | 0.098 | 0.7 |
| $g-3J+3g'$ | .000 | -.004 | .004 | 180.0 | $g+2\pi+2J-3g'$ | -.018 | +0.045 | 0.048 | 338.2 |
| $g-2J+g'$ | +.005 | -.032 | .032 | 179.1 | $g+2\pi+3J-5g'$ | +.001 | +0.030 | 0.030 | 1.9 |
| $g-2J+2g'$ | .000 | -.045 | .045 | 180.0 | $g+2\pi+3J-4g'$ | +.021 | -0.001 | 0.021 | 92.8 |
| $g-J+g'$ | +.004 | +.140 | .140 | 1.6 | $g+2\pi+3J-3g'$ | +.004 | +0.001 | 0.004 | 75.9 |
| $g-J+2g'$ | +.001 | +.006 | .006 | 9.6 | $2g+2\pi-3J$ | -.007 | 0.000 | 0.007 | 270.0 |
| $g-J$ | +.036 | +.011 | .038 | 73.0 | $2g+2\pi-3J+g'$ | .000 | -0.018 | 0.018 | 180.0 |
| $g+J-2g'$ | +.001 | -.006 | .006 | 170.4 | $2g+2\pi-2J-g'$ | -.008 | -0.013 | 0.015 | 211.6 |
| $g+J-g'$ | +.004 | -.163 | .163 | 178.6 | $2g+2\pi-2J$ | .000 | +0.018 | 0.018 | 0.0 |
| $g+J$ | +.036 | -.011 | .038 | 107.0 | $2g+2\pi-J-2g'$ | +.040 | +0.006 | 0.040 | 81.5 |
| $g+2J-2g'$ | .000 | +.064 | .064 | 0.0 | $2g+2\pi-J-g'$ | .000 | +0.016 | 0.016 | 0.0 |
| $g+2J-g'$ | +.005 | +.036 | .036 | 7.9 | $2g+2\pi+J-4g'$ | +.005 | -0.038 | 0.038 | 172.5 |
| $g+3J-3g'$ | .000 | +.003 | .003 | 0.0 | $2g+2\pi+J-3g'$ | +.006 | -0.168 | 0.168 | 177.9 |
| $g+3J-2g'$ | +.010 | .000 | .010 | 90.0 | $2g+2\pi+J-2g'$ | +.036 | 0.000 | 0.036 | 90.0 |
| $g+3J-g'$ | +.002 | +.002 | .003 | 45.0 | $2g+2\pi+2J-5g'$ | +.002 | +0.019 | 0.019 | 6.0 |
| $2\pi-3J$ | -.258 | -.008 | .258 | 268.2 | $2g+2\pi+2J-4g'$ | -.001 | +0.092 | 0.092 | 359.3 |
| $2\pi-2J$ | .000 | +.256 | .256 | 0.0 | $2g+2\pi+2J-3g'$ | -.035 | +0.082 | 0.089 | 336.9 |
| $2\pi-J-2g'$ | +.004 | .000 | .004 | 90.0 | $2g+2\pi+3J-5g'$ | +.003 | +0.074 | 0.074 | 2.3 |
| $2\pi+J-3g'$ | .000 | -.011 | .011 | 180.0 | $2g+2\pi+3J-4g'$ | +.042 | -0.003 | 0.042 | 94.0 |
| $2\pi+J-2g'$ | +.004 | .000 | .004 | 90.0 | $2g+2\pi+3J-3g'$ | +.010 | +0.002 | 0.010 | 78.5 |
| $2\pi+J-g'$ | .000 | -.011 | .011 | 180.0 | $3g+2\pi+J-3g'$ | .000 | +0.011 | 0.011 | 0.0 |
| $2\pi+2J-4g'$ | .000 | +.004 | .004 | 0.0 | $3g+2\pi+2J-4g'$ | .000 | -0.006 | 0.006 | 180.0 |
| $2\pi+2J-3g'$ | -.001 | +.003 | .003 | 341.6 | $2\pi-g-2J$ | .000 | +0.010 | 0.010 | 0.0 |
| | | | | | $2\pi-g-3J$ | -.015 | -0.001 | 0.015 | 183.8 |

ACTION OF SATURN.

| Argument. | v_c | v_s | δv | A | Argument. | v_c | v_s | δv | A |
|-----------|-------|-------|------------|-------|-----------|-------|--------|------------|-------|
| S | +.016 | +.048 | .051 | 18.4 | $g+S$ | +.001 | +.004 | 0.004 | 14.1 |
| $S-g'$ | .000 | -.040 | .040 | 180.0 | $g+S-g'$ | .000 | -0.008 | 0.008 | 180.0 |
| $2S-g'$ | -.001 | +.011 | .011 | 354.8 | $g-S$ | +.001 | -0.004 | 0.004 | 165.9 |
| $2S-2g'$ | .000 | +.008 | .008 | 0.0 | $g-S+g'$ | .000 | +0.008 | 0.008 | 0.0 |

§ 77. *Inequalities of the elements which have not been reduced to inequalities of the longitude.*

Mean longitude.

$$l = l_0 + nt + 5''.80 T^2 + 0''.0020 T^3 + 14''.77 \sin(18v - 16g' - g + 228^\circ 54') \\ + 0''.247 \sin(8v - 13g' + 86^\circ.4) + 0''.030 \sin \theta - 0''.273 \cos \theta$$

Longitude of Perigee.

$$\pi = \pi_0 + \pi_1 t + 253''.22 T - 38''.49 T^2 - 0''.013 T^3 + 0''.47 \sin(18v - 16g' - g + 228^\circ.5) \\ - 0''.67 \sin(8v - 13g' + 86^\circ.4) - 0''.10 \sin \theta + 0''.80 \cos \theta$$

Longitude of Node.

$$\theta = \theta_0 + \theta_1 t - 137''.85 T + 7''.62 T^2 + 0''.0026 T^3 + 2''.55 \sin \theta - 17''.33 \cos \theta \quad (1800) \\ + 2''.31 \sin \theta - 17''.36 \cos \theta \quad (1900)$$

Sin $\frac{1}{2}$ Inclination.

$$\delta\gamma = -0''.115 \cos \theta - 0''.769 \sin \theta \quad (1800) \\ - 0''.104 \cos \theta - 0''.770 \sin \theta \quad (1900)$$

Hence:

Inclination.

$$\delta I = -0''.230 \cos \theta - 1''.539 \sin \theta \quad (1800) \\ - 0''.208 \cos \theta - 1''.541 \sin \theta \quad (1900)$$

It may be found advisable, in the construction of new lunar tables, to include also the term

$$\delta l = 0''.256 \sin(2\pi - 2J)$$

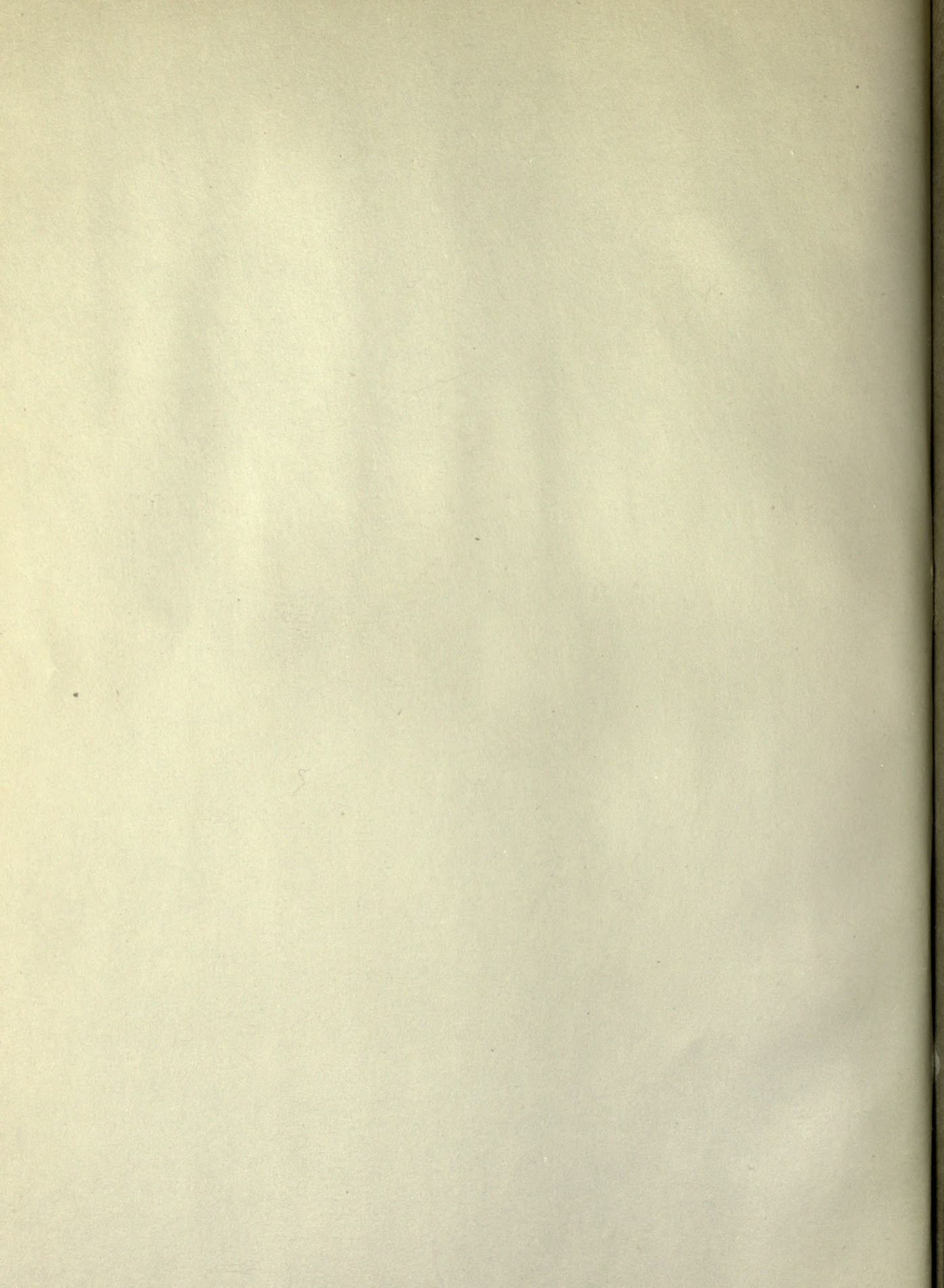
in the mean longitude. The effect of including this term in the preceding transformations is that the Jovian evection, and the coefficient of the term of argument $2\pi - 2J - g$, have each received the increment $+0''.014$. Hence, if the term were included in the mean longitude, the coefficient of the Jovian evection would be $-1''.154$, and of the other term named $-0''.004$.

§ 78. *Remarks on the Possibility of Unknown Terms of Long Period.* In his *Researches on the Motion of the Moon*, published in 1878,* the author found that the representation of the Moon's mean longitude during the period from 1650 to 1875 showed a discrepancy between existing theory and observation which might be represented by a term having a period of two or three centuries, and a coefficient of about $15''$. This coefficient may be somewhat reduced by the introduction of the improved values of the terms of short period now available, but it does not seem likely that the deviation can be brought below $10''$. One hypothesis on which the discrepancy might be explained is that of minute fluctuations in the

* *Washington Observations for 1875*, App. II, p. 268. See also *Monthly Notices, Royal Astronomical Society*, vol. LXIII, March, 1903, p. 316.

Earth's diurnal rotation, which might be produced by the motion of solids and fluids on its surface. Observations of transits of Mercury leave scarcely more than a possibility of changes in the measure of time having the magnitude required to explain the deviation. The observed phenomena, therefore, point very strongly to the inference that there must be some term of long period still undiscovered in the actual mean motion of the Moon. The preceding researches seem to remove the possibility that there can be any undiscovered term in the action of the planets. It is true that there are two possible classes of inequality which are not considered in the present work. One of these has the solar parallax as a factor, and may arise from two sources; one the development of the potential to terms of higher order than the principal ones; the other to the parallactic terms in the Moon's coördinates. The author had intended to carry the development of R and Ω_p one step further, so as to include these terms. But, on examining the periods of the inequalities that might thus arise, none were found that could lead to any important term.

Yet another class of terms comprises those of the second order arising from the action of the planets being modified by their mutual perturbations. An examination which I believe to be exhaustive was therefore made for terms of long period of this class. None have been found, and the writer believes that none can exist more important than one of $0''.018$ computed by Radau. This term has the argument $5S - 2J$ of the great inequality between Jupiter and Saturn. In this connection it may be again remarked that, in determining the action of Venus in the present work, the mutual perturbations of Venus and the Earth have been taken account of. But no change is thus produced except in the Hansenian term of long period.



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