







# TABLES,

# METEOROLOGICAL AND PHYSICAL,

PREPARED FOR

#### THE SMITHSONIAN INSTITUTION.

v.1 nu .3,

BY

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## PREFACE

#### TO THE FIRST EDITION.

To PROF. JOSEPH HENRY,

Secretary of the Smithsonian Institution.

SIR, -

In compliance with your instructions, I have prepared the collection of Meteorological Tables contained in the following pages. I have endeavored to render it useful, not only to the observers engaged in the system of Meteorological Observations now in operation under the direction of the Smithsonian Institution, for whom it was immediately designed, but also to any Meteorologist who may desire to compare and to work out portions of the vast amount of Meteorological Observations already accumulated in the stores of science.

The reduction of the observations and the extensive comparisons, without which Meteorology can do but little, require an amount of mechanical labor which renders it impossible for most observers to deduce for themselves the results of their own observations. The difficulty is still further increased by the diversity of the thermometrical and barometrical scales which Meteorologists, faithful to old habits rather than to science and to reason, choose to retain, notwithstanding the additional labor they thus gratuitously assume to themselves. To relieve the Meteorologist of a great portion of this labor, by means of tables sufficiently extensive to render calculations and even interpolations unnecessary, is to save his time and his forces in favor of science itself, and thus materially contribute to its advancement. But most of the tables useful in Meteorology being scattered through many volumes, which are often not of easy access, this collection will be, it is hoped, acceptable to the friends of Meteorology, and will supply a want very much felt in this department of the physical sciences.

In the selection of the matter, I have been guided by the idea that the tables which I sought for my own use might also be those most likely to be wanted by others. But I wish the following to be considered as a first collection, containing only the tables most appropriate to the present purpose. They are, therefore, arranged in different and independent series, with distinct paging, but constituting together a frame-work into which any tables may be readily inserted when wanted, either to make the collection more complete, or to present a choice of tables calculated from somewhat different elements, or adapted to various methods of calculation.

The measurement of heights by means of the barometer being intimately connected with Meteorology, it was thought not inappropriate to admit into this collection Hypsometrical Tables, destined to render this kind of calculations more easy and more rapid, and thus to increase the taste for a method so useful in physical geography. I have preferred the tables of Delcros, as uniting in the greatest degree simplicity and accuracy. Those of Gauss, Bessel, and Baily may be given afterwards.

Every table contains directions for its use, when necessary; moreover, the indication of the elements used in its calculation, and of the source from which it has been taken. When no remark is made as to this last point, the table has been expressly calculated for this volume.

Very respectfully,

Your obedient servant,

A. GUYOT.

Cambridge, Mass., December 15th, 1851.

#### PREFACE

#### TO THE SECOND EDITION.

To PROF. JOSEPH HENRY,

Secretary of the Smithsonian Institution.

SIR, -

In sending to you the Meteorological Tables composing the first edition of this volume, published in 1852, I expressed the desire that they be considered as a first collection, containing the tables most needed at the time by the meteorological observers engaged in the system carried on under the supervision of the Smithsonian Institution, but destined to be increased. It was in that expectation, I remarked, that the tables had been arranged in independent series, as a kind of framework, into which a larger number could readily be inserted. It seemed, indeed, highly desirable to offer to the Meteorologist and Physical Geographer, not only the tables they daily need for working out the results of their observations, but also such a variety of tables, computed from different elements, or by different methods, or adapted to different measures, as to enable every one to choose among them those that he most approves, and at the same time properly to compare and to appreciate the results obtained by others.

Thanks to the congenial spirit with which the elevated views of the founder of the Smithsonian Institution are carried out, that character of general usefulness is not wanting in the present volume. With your agreement, the present edition contains more than three times as much matter as the first; and a rapid indication of the additions will suffice to justify them, and to show that, in selecting or calculating the new tables, the object just mentioned was constantly kept in view

As to the tables in the first edition, I must remark that, several of them having been printed in my absence, the copy prepared for the printer, in which decimals had to be left out, failed to give always the nearest value. Though these errors are too small to have any importance whatsoever in Meteorology, a careful revision of all the tables on the original computations was made, and they were corrected in the present edition. The few actual misprints which were discovered are indicated in a table of errata to the first edition.

In the Thermometrical series six small tables have been added; they were prepared for converting into each other differential results given in degrees of any one of the three thermometrical scales, irrespective of their zero point.

The Hygrometrical series has been entirely reorganized. It only contained five tables, all in French measures, and the Appendix. It is now composed of twenty-seven, arranged in three divisions. In the first are found ten tables, based on Regnault's hygrometrical constants, both in French and in English measures, in two corresponding sets, for the use of the psychrometer, the dew-point instruments, and for computing the weight of vapor in the air. The whole set in English measures, and Table V. in French measures, have been prepared for this edition. Being based on the best elements we now possess, they are given here for ordinary use. The second division contains the seven most important tables published in the Greenwich Observations, and Glaisher's extensive Psychrometrical Table. These tables being much used in England, and the results obtained by them exhibiting no inconsiderable differences from those derived from the preceding ones, they are indispensable for comparing these results. The third division, composed of ten miscellaneous tables, furnishes the means of comparing the different values of the force and the weight of vapor, especially those which have frequently been used in Germany, and also of reducing the indications of Saussure's Hair-Hygrometer to the ordinary scale of moisture. The Appendix has remained as in the first edition, but all the tables have been revised and corrected.

The Barometrical series, now in four divisions, has been increased from twelve to twenty-eight tables. Excepting three small tables for capillary action, all the new ones have been computed for this edition. The comparison, now so much needed, of the Russian barometer with the other scales, appears here for the first time.

The Hypsometrical series is almost entirely new. It contained only Delcros's table for barometric and Regnault's table for thermometric measurements, besides two auxiliary tables and the thirteen small tables of the Appendix. It now offers twenty-three tables for barometrical measurement of heights, in which all the principal formulæ and scales are represented; three for the measurement of heights by the thermometer, in French and in English measures; and a rich Appendix of forty-four tables, more extensive and convenient than those in the old set, which afford the means of readily converting into each other all the measures usually employed for indicating altitudes.

The series of Meteorological Corrections for periodic and non-periodic variations, for all parts of the world, mostly due to the untiring industry of Professor Dove, is an addition which will surely be appreciated by those who know how difficult access to the original tables is for most Meteorol-

ogists. A few tables have been added to Dove's collection, computed by Glaisher, Captain Lefroy, and by myself. Most of the tables refer to temperature, only two to moisture. Two tables of Barometrical Corrections have been placed in the Hypsometrical series, where they were needed, until they can be joined by others to make a set in this series, which still awaits new contributions, especially for these last two departments.

The Miscellaneous series is but begun. I have prepared a list of useful tables, which would be no doubt welcome to the lovers of Terrestrial Physics, and which may be published at some future occasion, if you should then

find it expedient.

The present collection being designed, not for the scientific only, but for the observers at large, the propriety of the explicit and popular form of the explanations which accompany the tables, and of the directions for using them, will readily be understood.

I close by the remark, that, in every instance, the works from which the tables were taken have been carefully noted, and due credit given to their authors. For all the tables without author's names, I am myself responsible.

I remain, Sir,

Very respectfully, yours,

A. GUYOT.

PRINCETON, N. J., December, 1857.

### PREFACE

#### TO THE THIRD EDITION.

A NEW series of Hygrometrical Tables, based on Regnault's Table of Elastic Forces of Vapor, has been published by Mr. Glaisher, in London, 1856. As. however, the Psychrometrical Table has not been computed from Regnault's formula, but by means of empirical factors, the results differ from those contained in Table VII. B. A table containing Glaisher's empirical factors, therefore, has been added, and will be found on page 144 B.

Table XVIII. of the Barometrical set, C, page 72, of the Second Edition, for reducing to the freezing point the Barometers with glass or wooden scales, copied from the Instructions of the Royal Society of London, and which is reprinted in most of the English works on Meteorology, having been found erroneous, a new table has been computed and substituted for it. As a large number of observers still use barometers with wooden scales, it was found advisable to enable them to make the needed interpolations at sight, by giving the corrections for every degree of the thermometer, from 0° to 100° Fahr., and for barometric heights ranging between 26 and 31 inches.

The small Table VI. D, page 48, of the Hypsometrical Tables by the writer, having been found useful for rapid computation of approximate results, a larger one of the same description, which allows to make at sight every interpolation, has been added, on page 92, as Table XIX'. The scientific traveller, wishing to determine, when ascending a mountain, the elevation of the physical or geological phenomena that he meets with, such as the stations of remarkable plants, limits of zones of vegetation, - the geologist who uses the aneroid barometer for geological sections, - the engineer who wishes to know, on the ground, approximately, his results, - will find it convenient to obtain the relative heights indicated by their instrument by a simple multiplication. The use of the table is explained page D 90.

Some of the decimals in the smaller Table VI. D, page 48, above mentioned, have been slightly altered in order to make both tables agree.

In set E of Meteorological Corrections, a table of corrections derived by Professor C. Dewey from the hourly observations of Professor Snell, at Amherst College, has been added, which will be of service especially to the numerous observers in New England and in the neighboring States.

The errata indicated in the Second Edition, and a few unimportant ones found since, have been corrected. No other changes have been made in this edition.

A. GUYOT.

I. – III.

### GENERAL COMPARISON

OF

# THE THERMOMETRICAL SCALES,

OR

## TABLES

showing the corresponding values of each full degree of fahrenheit's, centigrade, and reaumur's thermometers, from +212° to -39° fahrenheit.

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## THE THERMOMETRICAL SCALES

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#### COMPARISON OF THE THERMOMETRICAL SCALES.

THE first three tables of this set give a simultaneous comparison of the three scales mostly used at present in Meteorology, and especially of the portion of the scales not comprised in the more extensive tables which follow them. They form thus a complement to these last tables; but as most of the temperatures contained in them do not occur in Meteorology, the comparison of the full degrees was found sufficient.

These three tables have been taken from E. L. Schubarth's Collection of Physical Tables. Berlin, 1836.

Tables IV. to IX. being more useful to the Meteorologist, the calculation has been carried out for every tenth of a degree. Tables VII. and IX. are from the *Annuaire Météorologique de France*; the others have been calculated.

A comparison of the Centigrade and Fahrenheit degrees near the boiling point, for every tenth of a degree, for the sake of the comparison of standard thermometers, will be found at the end of Table VI.

Tables X. to XV. will be found useful for comparing differential results, such as ranges of temperature, and any relative amount expressed in degrees of different scales, without reference to their respective zeros.

# I. COMPARISON OF FAHRENHEIT'S THERMOMETRICAL SCALE WITH THE CENTIGRADE AND REAUMUR'S.

 $x^{\circ}$  Fahr. =  $(x^{\circ} - 32^{\circ}) \frac{5}{9}$  Centig. =  $(x^{\circ} - 32^{\circ}) \frac{4}{9}$  Reaum.

Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumu
Att. I	CON N		WO IS		251854	6 162	e direct	(4 ( ) Th
+212	+100.00	+80.00	+172	+77.78	+62.22	+132	+55.56	+44.44
211	99.44	79.56	171	77.22	61.78	131	55.00	44.00
210	98.89	79.11	170	76.67	61.33	130	54.44	43.56
209	98.33	78.67	169	76.11	60.89	129	53.89	43.11
208	97.78	78.22	168	75.56	60.44	128	53.33	42.67
207	97.22	77.78	167	75.00	60.00	127	52.78	42.22
206	96.67	77.33	166	74.44	59.56	126	52.22	41.78
205	96.11	76.89	165	73.89	59.11	125	51.67	41.33
204	95.56	76.44	164	73.33	58.67	124	51.11	40.89
203	95.00	76.00	163	72.78	58.22	123	50.56	40.44
202	94.44	75.56	162	72.22	57.78	122	50.00	40.00
201	93.89	75.11	161	71.67	57.33	121	49.44	39.56
200	93.33	74.67	160	71.11	56.89	120	48.89	39.11
199	92.78	74.22	159	70.56	56.44	119	48.33	38.67
198	92.22	73.78	158 -	70.00	56.00	118	.47.78	38.22
197	91.67	73.33	157	69.44	55.56	117	47.22	37.78
196	91.11	72.89	156	68.89	55.11	116	46.67	37.33
195	90.56	72.44	155	68.33	54.67	115	46.11	36.89
194	90.00	72.00	154	67.78	54.22	114	45.56	36.44
193	89.44	71.56	153	67.22	53.78	113	45.00	36.00
192	88.89	71.11	152	66.67	53.33	112	44.44	35.56
191	88.33	70.67	151	66.11	52.89	111	43.89	35.11
190	87.78	70.22	150	65.56	52.44	110	43.33	34.67
189	87.22	69.78	149	65.00	52.00	109	42.78	34.22
188	86.67	69.33	148	64.44	51.56	108	42.22	33.78
187	86.11	68.89	147	63.89	51.11	107	41.67	33.33
186	85.56	68.44	146	63.33	50.67	106	41.11	32.89
185	85.00	68.00	145	62.78	50.22	105	40.56	32.44
184	84.44	67.56	144	62.22	49.78	104	40.00	32.00
183	83.89	67.11	143	61.67	49.33	103	39.44	31.56
182	83.33	66.67	142	61.11	48.89	102	38.89	31.11
181	82.78	66.22	141	60.56	48.44	101	38.33	30.67
180	82.22	65.78	140	60.00	48.00	100	37.78	30.22
179	81.67	65.33	139	59.44	47.56	99	37.22	29.79
178	81.11	64.89	138	58.89	47.11	98	36.67	29.33
177	80.56	64.44	137	58.33	46.67	97	36.11	28.89
176	80.00	64.00	136	57.78	46.22	96	35.56	28.44
175	79.44	63.56	135	57.22	45.78	95	35.00	28.00
174	78.89	63.11	134	56.67	45.33	94	34.44	27.56
173	78.33	62.67	133	56.11	44.89	93	33.89	27.11

Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaum
	awami	phi Sie		200	( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (	A C = 1C	n and exe	
+92	+33.33	+26.67	+48	+ 8.89	+ 7.11	+ 4	-15.56	-12.4
91	32.78	26.22	47	8.33	6.67	3	-16.11	-12.4
90	32.22	25.78	46	7.78	6.22	2	-16.67	-13.3
89	31.67	25.33	45	7.22	5.78	1	-17.22	-13.78
88	31.11	24.89	44	6.67	5.33	Ô	-17.78	-14.2
87	30.56	24.44	43	6.11	4.89	- 1	-18.33	-14.6
86	30.00	24.00	42	5.56	4.44	- 2	-18.89	-15.1
85	29.44	23.56	41	5.00	4.00	- 3	-19.44	-15.5
84	28.89	23.11	40	4.44	3.56	- 4	-20.00	-16.0
83	28.33	22.67	39	3.89	3.11	- 5	-20.56	-16.4
82	27.78	22.22	38	3.33	2.67	- 6	-21.11	-16.8
81	27.22	21.78	37	2.78	2.22	- 7	-21.67	-17.3
80	26.67	21.33	36	2.22	1.78	- 8	-22.22	-17.78
79	26.11	20.89	35	1.67	1.33	- 9	-22.78	-18.2
78	25.56	20.44	34	1.11	0.89	-10	-23.33	-18.6
77	25.00	20.00	33	0.56	0.44	-11	-23.89	-19.1
76	24.44	19.56	32	0.00	0.00	-12	-24.44	-19.5
75	23.89	19.11	31	- 0.56	- 0.44	-13	-25.00	-20.0
74	23.33	18.67	30	- 1.11	- 0.89	-14	-25.56	-20.4
73	22.78	18.22	29	- 1.67	- 1.33	-15	-26.11	-20.8
72	22.22	17.78	28	- 2.22	- 1.78	-16	-26.67	-21.3
71	21.67	17.33	27	- 2.78	- 2.22	-17	-27.22	-21.78
70	21.11	16.89	26	- 3.33	- 2.67	-18	-27.78	-22.2
69	20.56	16.44	25	- 3.89	- 3.11	-19	-28.33	-22.6
68	20.00	16.00	24	- 4.44	- 3.56	-20	-28.89	-23.1
67	19.44	15.56	23	- 5.00	- 4.00	-21	-29.44	-23.50
66	18.89	15.11	22	- 5.56	- 4.44	-22	-30.00	-24.00
65	18.33	14.67	21	- 6.11	- 4.89	-23	-30.56	-24.44
64	17.78	14.22	20	- 6.67	- 5.33	-24	-31.11	-24.89
63	17.22	13.78	19	- 7.22	- 5.78	-25	-31.67	-25.33
62	16.67	13.33	18	- 7.78	- 6.22	-26	-32.22	-25.78
61	16.11	12.89	17	- 8.33	- 6.67	-27	-32.78	-26.22
60	15.56	12.44	16	- 8.89	- 7.11	-28	-33.33	-26.67
59	15.00	12.00	15	- 9.44	- 7.56	-29	-33.89	-27.11
58	14.44	11.56	14	-10.00	- 8.00	-30	-34.44	-27.56
57	13.89	11.11	13	-10.56	- 8.44	-31	-35.00	-28.00
56	13.33	10.67	12	-11.11	- 8.89	-32	-35.56	-28.44
55	12.78	10.22	11	-11.67	- 9.33	-33	-36.11	-28.89
54	12.22	9.78	10	-12.22	- 9.78	-34	-36.67	-29.33
53	11.67	9.33	9	-12.78	-10.22	-35	-37.22	-29.78
52	11.11	8.89	8	-13.33	-10.67	-36	-37.78	-30.22
51	10.56	8.44	7	-13.89	-11.11	-37	-38.33	-30.67
50	10.00	8.00	6	-14.44	-11.56	-38	-38.89	-31.11

For the Continuation see Table IV. and V.

# II. COMPARISON OF THE CENTIGRADE THERMOMETER WITH REAUMUR'S AND FAHRENHEIT'S.

 $x^{\circ}$  Centig. =  $(32 + \frac{9}{5} x^{\circ})$  Fahr. =  $\frac{4}{5} x^{\circ}$  Reaum.

Centig.	Reaumur.	Fahrenheit.	Centig.	Reaumur.	Fahrenheit.	Centig.	Reaumur.	Fahrenheit
+100	+80.0	+212.0	+83	+66.4	+181.4	+66	+52.8	+150.8
99	79.2	210.2	82	65.6	179.6	65	52.0	149.0
98	78.4	208.4	81	64.8	177.8	64	51.2	147.2
97	77.6	206.6	80	64.0	176.0	63	50.4	145.4
96	76.8	204.8	79	63.2	174.2	62	49.6	143.6
95	76.0	203.0	78	62.4	172.4	61	48.8	141.8
94 .	75.2	201.2	77	61.6	170.6	60	48.0	140.0
93	74.4	199.4	76	60.8	168.8	59	47.2	138.2
92	73.6	197.6	75	60.0	167.0	58	46.4	136.4
91	72.8	195.8	74	59.2	165.2	57	45.6	134.6
90	72.0	194.0	73	58.4	163.4	56	44.8	132.8
89	71.2	192.2	72	57.6	161.6	55	44.0	131.0
88	70.4	190.4	71	56.8	159.8	54	43.2	129.2
87	69.6	188.6	70	56.0	158.0	53	42.4	127.4
86	68.8	186.8	69	55.2	156.2	52	41.6	125.6
85	68.0	185.0	68	54.4	154.4	51	40.8	123.8
84	67.2	183.2	67	53.6	152.6	50	40.0	122.0

For the Continuation see Tables V. and VI.

# III. COMPARISON OF REAUMUR'S THERMOMETER WITH FAHRENHEIT'S AND THE CENTIGRADE.

 $x^{\circ}$  Reaum. =  $(32^{\circ} + \frac{9}{4} x^{\circ})$  Fahr. =  $\frac{5}{4} x^{\circ}$  Centig.

Reaumur.	Fahrenheit.	Centigrade.	Reaumur.	Fahrenheit.	Centigrade.	Reaumur.	Fahrenheit.	Centigrade
+80	+212.00	+100.00	+66	+180.50	+82.50	+52	+149.00	+65.00
79	209.75	98.75	65	178.25	81.25	51	146.75	63.75
78	207.50	97.50	64	176.00	80.00	50	144.50	62.50
77	205.25	96.25	63	173.75	78.75	49	142.25	61.25
76	203.00	95.00	62	171.50	77.50	48	140.00	60.00
75	200.75	93.75	61	169.25	76.25	47	137.75	58.75
* 74	198.50	92.50	60	167.00	75.00	46	135.50	57.50
73	196.25	91.25	59	164.75	73.75	45	133.25	56.25
72	194.00	90.00	58	162.50	72.50	44	131.00	55.00
71	191.75	88.75	57	160.25	71.25	43	128.75	53.75
70	189.50	87.50	56	158.00	70.00	42	126.50	52.50
69	187.25	86.25	55	155.75	68.75	41	124.25	51.25
68	185.00	85.00	54	153.50	67.50	40	122.00	50.00
67	182.75	83.75	53	151.25	66.25	39	119.75	48.75

For the Continuation see Tables VIII. and IX.

IV. - V.

#### COMPARISON

OF

## FAHRENHEIT'S THERMOMETER

WITH

THE CENTIGRADE AND WITH THAT OF REAUMUR,

OR

#### TABLES

FOR CONVERTING THE DEGREES OF FAHRENHEIT INTO CENTIGRADE DEGREES AND INTO DEGREES OF REAUMUR;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF A DEGREE, FROM +122° TO -76° FAHRENHEIT.

The Foliablesian po Laura but the con-

Degrees of					Tenths of	Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
+122	Centig.	Centig.	Centig.	Centig.	Centig.	Centig. +50.28	Centig.	Centig.	Centig.	Centie
121	+50.00	+50.06 49.50	+50.11	+50.17 49.61	+50.22	49.72	+50.33 49.78	+50.39 49.83	+50.44	+50.5
120	49.44	49.94	49.56	49.06	49.67	49.17	49.22	49.28	49.89	49.9
119	48.33	48.39	48.44	48.50	48.56	48.61	48.67	48.72	48.78	48.8
118	47.78	47.83	47.89	47.94	48.00	48.06	48.11	48.17	48.22	48.2
117	47.22	47.28	47.33	47.39	47.44	47.50	47.56	47.61	47.67	47.7
116	46.67	46.72	46.78	46.83	46.89	46.94	47.00	47.06	47.11	47.1
115	46.11	46.17	46.22	46.28	46.33	46.39	46.44	46.50	46.56	46.6
114	45.56	45.61	45.67	45.72	45.78	45.83	45.89	45.94	46.00	46.0
113	45.00	45.06	45.11	45.17	45.22	45.28	45.33	45.39	45.44	45.5
112	44.44	44.50	44.56	44.61	44.67	44.72	44.78	44.83	44.89	44.9
111	43.89	43.94	44.00	44.06	44.11	44.17	44.22	44.28	44.33	44.3
110	43.33	43.39	43.44	43.50	43.56	43.61	43.67	43.72	43.78	43.8
109	42.78	42.83	42.89	42.94	43.00	43.06	43.11	43.17	43.22	43.2
108	42.22	42.28	42.33	42.39	42.44	42.50	42.56	42.61	42.67	42.7
107	41.67	41.72	41.78	41.83	41.89	41.94	42.00	42.06	42.11	42.1
106	41.11	41.17	41.22	41.28	41.33	41.39	41.44	41.50	41.56	41.6
105	40.56	40.61	40.67	40.72	40.78	40.83	40.89	40.94	41.00	41.0
104	40.00	40.06	40.11	40.17	40.22	40.28	40.33	40.39	40.44	40.50
103	39.44	39.50	39.56	39.61	39.67	39.72	39.78	39.83	39.89	39.9
102	38.89	38.94	39.00	39.06	39.11	39.17	39.22	39.28	39.33	39.39
101	38.33	38.39	38.44	38.50	38.56	38.61	38.67	38.72	38.78	38.83
100	37.78	37.83	37.89	37.94	38.00	38.06	38.11	38.17	38.22	38.28
99	37.22	37.28	37.33	37.39	37.44	37.50	37.56	37.61	37.67	37.72
98	36.67	36.72	36.78	36.83	36.89	36.94	37.00	37.06	37.11	37.17
97 96	36.11	36.17	36.22	36.28	36.33	36.39	36.44	36.50	36.56	36.61
95	35.56	35.61	35.67	35.72	35.78	35.83	35.89	35.94	36.00	36.00
94	35.00 34.44	35.06 34.50	35.11 34.56	35.17 34.61	35.22 34.67	35.28 34.72	35.33 34.78	35.39	35.44 34.89	35.50
93	33.89	33.94	34.00	34.06	34.11	34.17	34.22	34.28	34.33	34.39
92	33.33	33.39	33.44	33.50	33.56	33.61	33.67	33.72	33.78	33.88
91	32.78	32.83	32.89	32.94	33.00	33.06	33.11	33.17	33.22	33.28
90	32.22	32.28	32.33	32.39	32.44	32.50	32.56	32.61	32.67	32.72
89	31.67	31.72	31.78	31.83	31.89	31.94	32.00	32.06	32.11	33.17
88	31.11	31.17	31.22	31.28	31.33	31.39	31.44	31.50	31.56	31.61
87	30.56	30.61	30.67	30.72	30.78	30.83	30.89	30.94	31.00	31.06
86	30.00	30.06	30.11	30.17	30.22	30.28	30.33	30.39	30.44	30.50
85	29.44	29.50	29.56	29.61	29.67	29.72	29.78	29.83	29.89	29.94
84 83	28.89 28.33	28.94 28.39	29.00 28.44	29.06 28.50	29.11 28.56	29.17 28.61	29.22 28.67	29.28 28.72	29.33	29.39 28.83
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Degrees of Fahren-	1			A Real	Tenths of	Degrees.				
heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
100	Centig.	Centig.	Centig.	Centig.	Centig.	Centig. +28.06	Centig.	Centig.	Centig.	Centi
+82	+27.78	+27.83	+27.89	+27.94	+28.00		+28.11	+28.17	+28.22	+28.2
81	27.22	27.28	27.33	27.39	27.44	27.50	27.56	27.61	27.67	27.
80	26.67	26.72	26.78	26.83	26.89	26.94	27.00	27.06	27.11	27.
79	26.11	26.17	26.22	26.28	26.33	26.39	26.44	26.50	26.56	26.
78	25.56	25.61	25.67	25.72	25.78	25.83	25.89	25.94	26.00	26.0
77	25.00	25.06	25.11	25.17	25.22	25.28	25.33	25.39	25.44	25.
76	24.44	24.50	24.56	24.61	24.67	24.72	24.78	24.83	24.89	24.9
75	23.89	23.94	24.00	24.06	24.11	24.17	24.22	24.28	24.33	24.5
74	23.33	23.39	23.44	23.50	23.56	23.61	23.67	23.72	23.78	23.8
73	22.78	22.83	22.89	22.94	23.00	23.06	23.11	23.17	23.22	23.2
72	22.22	22.28	22.33	22.39	22.44	22.50	22.56	22.61	22.67	22.7
71	21.67	21.72	21.78	21.83	21.89	21.94	22.00	22.06	22.11	22.1
70	21.11	21.17	21.22	21.28	21.33	21.39	21.44	21.50	21.56	21.6
69	20.56	20.61	20.67	20.72	20.78	20.83	20.89	20.94	21.00	21.0
68	20.00	20.06	20.11	20.17	20.22	20.28	20.33	20.39	20.44	20.5
67	19.44	19.50	19.56	19.61	19.67	19.72	19.78	19.83	19.89	19.9
66	18.89	18.94	19.00	19.06	19.11	19.17	19.78	19.88	19.33	19.3
65	18.33	18.39	18.44	18.50	18.56	18.61	18.67	18.72	18.78	18.8
64	17.78	17.83	17.89	17.94	18.00	18.06	18.11	18.17	18.22	18.2
63	17.22	17.28	17.33	17.39	17.44	17.50	17.56	17.61	17.67	17.7
	60									
62	16.67	16.72	16.78	16.83	16.89	16.94	17.00	17.06	17.11	17.1
61	16.11	16.17	16.22	16.28	16.33	16.39	16.44	16.50	16.56	16.6
60	15.56	15.61	15.67	15.72	15.78	15.83	15.89	15.94	16.00	16.0
59	15.00	15.06	15.11	15.17	15.22	15.28	15.33	15.39	15.44	15.5
58	14.44	14.50	14.56	14.61	14.67	14.72	14.78	14.83	14.89	14.9
57	13.89	13.94	14.00	14.06	14.11	14.17	14.22	14.28	14.33	14.3
56	13.33	13.39	13.44	13.50	13.56	13.61	13.67	13.72	13.78	13.8
55	12.78	12.83	12.89	12.94	13.00	13.06	13.11	13.17	13.22	13.2
54	12.22	12.28	12.33	12.39	12.44	12.50	12.56	12.61	12.67	12.7
53	11.67	11.72	11.78	11.83	11.89	11.94	12.00	12.06	12.11	12.1
52	11.11	11.17	11.22	11.28	11.33	11.39	11.44	11.50	11.56	11.6
51	10.56	10.61	10.67	10.72	10.78	10.83	10.89	10.94	11.00	11.0
50	10.00	10.06	10.11	10.17	10.22	10.28	10.33	10.39	10.44	10.5
49	9.44	9.50	9.56	9.61	9.67	9.72	9.78	9.83	9.89	9.9
48	8.89	8.94	9.00	9.06	9.11	9.17	9.22	9.28	9.33	9.3
47	8.33	8.39	8.44	8.50	8.56	8.61	8.67	8.72	8.78	8.8
46	7.78	7.83	7.89	7.94	8.00	8.06	8.11	8.17	8.22	8.2
45	7.22	7.28	7.33	7.39	7.44	7.50	7.56	7.61	7.67	7.7
44	6.67	6.72	6.78	6.83	6.89	6.94	7.00	7.06	7.11	7.1
43	6.11	6.17	6.22	6.28	6.33	6.39	6.44	6.50	6.56	6.6
.4	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Degrees of					Tenths o	f Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centig.									
+42	+5.56	+5.61 5.06	+5.67	+5.72	+5.78	+5.83 5.28	+5.89	+5.94	+6.00	+6.06
41	4.44	4.50	5.11	5.17	5.22	4.72	5.33 4.78	4.83	4.89	5.50 4.94
39	3.89	3.94	4.00	4.06	4.11	4.17	4.22	4.28	4.33	4.39
38	3.33	3.39	3.44	3.50	3.56	3.61	3.67	3.72	3.78	3.83
37	2.78	2.83	2.89	2.94	3.00	3.06	3.11	3.17	3.22	3.28
36	2.22	2.28	2.33	2.39	2.44	2.50	2.56	2.61	2.67	2.72
35	1.67	1.72	1.78	1.83	1.89	1.94	2.00	2.06	2.11	2.17
34	1.11	1.17	1.22	1.28	1.33	1.39	1.44	1.50	1.56	1.61
33	0.56	0.61	0.67	0.72	0.78	0.83	0.89	0.94	1.00	1.06
32	0.00	0.06	0.11	0.17	0.22	0.28	0.33	0.39	0.44	0.50
31	- 0.56	- 0.50 - 1.06	- 0.44	- 0.39	- 0.33	- 0.28	- 0.22	- 0.17	- 0.11	- 0.06
30 29	- 1.11 - 1.67	- 1.61	- 1.00 - 1.56	-0.94 $-1.50$	- 0.89 - 1.44	- 0.83 - 1.39	- 0.78 - 1.33	- 0.72 - 1.28	- 0.67 - 1.22	- 0.61 - 1.17
28	- 2.22	- 2.17	- 2.11	- 2.06	- 2.00	- 1.94	- 1.89	- 1.83	- 1.78	- 1.72
20			2	2.00	2.00	1.01	1.03	1.00	1	1.12
27	- 2.78	- 2.72	- 2.67	- 2.61	- 2.56	- 2.50	- 2.44	- 2.39	- 2.33	- 2.28
26	- 3.33	- 3.28	- 3.22	- 3.17	- 3.11	- 3.06	- 3.00	- 2.94	- 2.89	- 2.83
25	- 3.89	- 3.83	- 3.78	- 3.72	- 3.67	- 3.61	- 3.56	- 3.50	- 3.44	- 3.39
24	- 4.44	- 4.39	- 4.33	- 4.28	- 4.22	- 4.17	- 4.11	- 4.06	- 4.00	- 3.94
23	- 5.00	- 4.94	- 4.89	- 4.83	- 4.78	- 4.72	- 4.67	- 4.61	- 4.56	- 4.50
22	- 5.56	- 5.50	- 5.44	- 5.39	- 5.33	- 5.28	- 5.22	- 5.17	- 5.11	- 5.06
21	- 6.11	- 6.06	- 6.00	- 5.94	- 5.89	- 5.83	- 5.78	- 5.72	- 5.67	- 5.61
20	- 6.67	- 6.61	- 6.56	- 6.50	- 6.44	- 6.39	- 6.33	- 6.28	- 6.22	- 6.17
19	- 7.22	- 7.17	- 7.11	- 7.06	- 7.00	- 6.94	- 6.89	- 6.83	- 6.78	- 6.72
18	- 7.78	- 7.72	- 7.67	- 7.61	- 7.56	<b>- 7.50</b>	- 7.44	- 7.39	- 7.33	<b>- 7.28</b>
17	- 8.33	- 8.28	- 8.22	- 8.17	- 8.11	- 8.06	- 8.00	- 7.94	- 7.89	- 7.83
16	- 8.89	- 8.83	- 8.78	- 8.72	- 8.67	- 8.61	- 8.56	- 8.50	- 8.44	- 8.39
15 14	- 9.44 -10.00	- 9.39 - 9.94	- 9.33	- 9.28 - 9.83	- 9.22	-9.17 $-9.72$	- 9.11	- 9.06	- 9.00	- 8.94
13	-10.00	- 9.94 -11.50	- 9.89 -10.44	- 9.83 -10.39	- 9.78 -10.33	- 9.72 -10.28	- 9.67 -10.22	- 9.61 -10.17	- 9.56 -10.11	- 9.50 -10.06
12	-11.11	-11.06	-11.00	-10.94	-10.89	-10.83	-10.78	-10.72	-10.67	-10.61
11	-11.67	-11.61	-11.56	-11.50	-11.44	-11.39	-11.33	-11.28	-11.22	-11.17
10	-12.22	-12.17	-12.11	-12.06	-12.00	-11.94	-11.89	-11.83	-11.78	-11.72
9	-12.78	-12.72	-12.67	-12.61	-12.56	-12.50	-12.44	-12.39	-12.33	-12.28
8	-13.33	-13.28	-13.22	-13.17	-13.11	-13.06	-13.00	-12.94	-12.89	-12.83
7	-13.89	-13.83	-13.78	-13.72	-13.67	-13.61	-13.56	-13.50	-13.44	-13.39
6	-14.44	-14.39	-14.33	-14.28	-14.22	-14.17	-14.11	-14.06	-14.00	-13.94
5	-15.00	-14.94	-14.89	-14.83	-14.78	-14.72	-14.67	-14.61	-14.56	-14.50
3	-15.56 $-16.11$	-15.50 -16.06	-15.44 $-16.00$	-15.39 -15.94	-15.33 -15.89	-15.28 -15.83	-15.22 $-15.78$	-15.17 $-15.72$	-15.11 -15.67	-15.06 $-15.61$
					-	50.00				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

					Tenths of	f Degrees.				
Degrees of Fahren- heit.		F	1				1*	1		
neit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
+ 2	-16.67 $-17.22$	-16.61 -17.17	-16.56 -17.11	-16.50 -17.06	-16.44 $-17.00$	-16.39 -16.94	-16.33 -16.89	-16.28 -16.83	-16.22 -16.78	-16.17 16.72
0	-17.78	-17.72	-17.67	-17.61	-17.56	-17.50	-17.44	-17.39	-17.33	-17.28
- 0	-17.78	-17.83	-17.89	-17.94	-18.00	-18.06	-18.11	-18.17	-18.22	-18.28
- 1	-18.33	-18.39	-18.44	-18.50	-18.56	-18.61	-18.67	-18.72	-18.78	-18.83
- 2	-18.89	-18.94	-19.00	-19.06	-19.11	-19.17	-19.22	-19.28	-19.33	-19.39
- 3	-19.44	-19.50	-19.56	-19.61	-19.67	-19.72	-19.78	-19.83	-19.89	-19.94
- 4	-20.00	-20.06	-20.11	-20.17	-20.22	-20.28	-20.33	-20.39	-20.44	-20.50
- 5	-20.56	-20.61	-20.67	-20.72	-20.78	-20.83	-20.89	-20.94	-21.00	-21.06
- 6	-21.11	-21.17	-21.22	-21.28	-21.33	-21.39	-21.44	-21.50	-21.56	-21.61
- 7	-21.67	-21.72	-21.78	-21.83	-21.89	-21.94	-22.00	-22.06	-22.11	-22.17
- 8	-22.22	-22.28	-22.33	-22.39	-22.44	-22.50	-22.56	-22.61	-22.67	-22.72
- 9	-22.78	-22.83	-22.89	-22.94	-23.00	-23.06	-23.11	-23.17	-23.22	-23.28
-10	-23.33	-23.39	-23.44	-23.50	-23.56	-23.61	-23.67	-23.72	-23.78	-23.83
-11	-23.89	-23.94	-24.00	-24.06	-24.11	-24.17	-24.22	-24.28	-24.33	-24.39
-12	-24.44	-24.50	-24.56	-24.61	-24.67	-24.72	-24.78	-24.83	-24.89	-24.94
-13	-25.00	-25.06	-25.11	-25.17	-25.22	-25.28	-25.33	-25.39	-25.44	-25.50
-14	-25.56	-25.61	-25.67	-25.72	-25.78	-25.83	-25.89	-25.94	-26.00	-26.06
-15	-26.11	-26.17	-26.22	-26.28	-26.33	-26.39	-26.44	-26.50	-26.56	-26.61
-16	-26.67	-26.72	-26.78	-26.83	-26.89	-26.94	-27.00	-27.06	-27.11	-27.17
-17	-27.22	-27.28	-27.33	-27.39	-27.44	-27.50	-27.56	-27.61	-27.67	-27.72
-18	-27.78	-27.83	-27.89	-27.94	-28.00	-28.06	-28.11	-28.17	-28.22	-28.28
-19	-28.33	-28.39	-28.44	-28.50	-28.56	-28.61	-28.67	-28.72	-28.78	-28.83
$-20 \\ -21$	-28.89 $-29.44$	-28.94 $-29.50$	-29.00 -29.56	-29.06 -29.61	-29.11	-29.17 $-29.72$	-29.22 -29.78	-29.28	-29.33	-29.39
-21	-23.44	-29.50	-29.50	-25.01	-29.67	-29.12	-49.10	-29.83	-29.89	-29.94
-22	-30.00	-30.06	-30.11	-30.17	-30.22	-30.28	-30.33	-30.39	-30.44	-30.50
-23	-30.56	-30.61	-30.67	-30.72	-30.78	-30.83	-30.89	-30.94	-31.00	-31.06
-24	-31.11 -31.67	-31.17 -31.72	-31.22 -31.78	-31.28 -31.83	-31.33	-31.39 -31.94	-31.44 -32.00	-31.50	-31.56	-31.61
-25 -26	-31.67 $-32.22$	-31.72 -32.28	-31.78	-31.83 -32.39	-31.89 -32.44	-31.94 -32.50 .	-32.00 $-32.56$	-32.06 -32.61	-32.11 -32.67	-32.17 -32.72
20	02.22	OM•MO	OM100	O.M.00	02.44	onioo ,	02.00	02.01	02.01	02.12
-27	-32.78	-32.83	-32.89	-32.94	-33.00	-33.06	-33.11	-33.17	-33.22	-33.28
-28	-33.33	-33.39	-33.44	-33.50	-33.56	-33.61	-33.67	-33.72	-33.78	-33.83
-29	-33.89	-33.94	-34.00	-34.06	-34.11	-34.17	-34.22	-34.28	-34.33	-34.39
-30 -31	-34.44 -35.00	-34.50 -35.06	-34.56 $-35.11$	-34.61 -35.17	-34.67 -35.22	-34.72 -35.28	-34.78 -35.33	-34.83 -35.39	-34.89 -35.44	-34.94 -35.50
-91	-55.00	-55.00	-99.11	-00.17	-50.22	30.23	-00.00	-50.39	-55.44	-55.50
-32	-35.56	-35.61	-35.67	-35.72	-35.78	-35.83	-35.89	-35.94	-36.00	-36.06
-33	-36.11	-36.17	-36.22	-36.28	-36.33	-36.39	-36.44	-36.50	-36.56	-36.61
-34	-36.67	-36.72	-36.78	-36.83	-36.89	-36.94	-37.00	-37.06	-37.11	-37.17
-35 -36	-37.22 -37.78	-37.28 -37.83	-37.33 -37.89	-37.39 -37.94	-37.44 -38.00	-37.50 -38.06	-37.56 -38.11	-37.61 $-38.17$	-37.67 -38.22	-37.72 $-38.28$
			4.27							
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Degrees of Fahren-					Tenths of	Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.
VAVALE OF	Centig.									
-37	-38.33	-38.39	-38.44	-38.50	-38.56	-38.61	-38.67	-38.72	-38.78	-38.83
-38	-38.89	-38.94	-39.00	-39.06	-39.11	-39.17	-39.22	-39.28	-39.33	-39.39
-39	-39.44	-39.50	-39.56	-39.61	-39.67	-39.72 -40.28	-39.78	-39.83 -40.39	-39.89	-39.94
-40 -41	-40.00 $-40.56$	-40.06 -40.61	-40.11 -40.67	-40.17	-40.22 -40.78	-40.28 $-40.83$	-40.33 -40.89	-40.39 $-40.94$	-40.44 -41.00	-40.50 -41.06
-41	-40.50	-40.01	-40.07	-40.72	-40.78	-40.00	-40.89	-40.94	-41.00	-41.00
-42	-41.11	-41.17	-41.22	-41.28	-41.33	-41.39	-41.44	-41.50	-41.56	-41.61
-43	-41.67	-41.72	-41.78	-41.83	-41.89	-41.94	-42.00	-42.06	-42.11	-42.17
-44	-42.22	-42.28	-42.33	-42.39	-42.44	-42.50	-42.56	-42.61	-42.67	-42.72
-45	-42.78	-42.83	-42.89	-42.94	-43.00	-43.06	-43.11	-43.17	-43.22	-43.28
-46	-43.33	-43.39	-43.44	-43.50	-43.56	-43.61	-43.67	-43.72	-43.78	-43.83
-47	-43.89	-43.94	-44.00	-44.06	-44.11	-44.17	-44.22	-44.28	-44.33	-44.39
-48	-44.44	-44.50	-44.56	-44.61	-44.67	-44.72	-44.78	-44.83	-44.89	-44.94
-49	-45.00	-45.06	-45.11	-45.17	-45.22	-45.28	-45.33	-45.39	-45.44	-45.50
-50	-45.56	-45.61	-45.67	-45.72	-45.78	-45.83	-45.89	-45.94	-46.00	-46.06
-51	-46.11	-46.17	-46.22	-46.28	-46.33	-46.39	-46.44	-46.50	-46.56	-46.61
			40 00	10.00	10.00	10.04	47 00	47 06	-47.11	-47.17
-52	-46.67	-46.72	-46.78	-46.83	-46.89	-46.94 $-47.50$	-47.00 $-47.56$	-47.06 $-47.61$	-47.11 $-47.67$	-47.72
-53 -54	-47.22 $-47.78$	-47.28	-47.33 -47.89	-47.39 $-47.94$	-47.44 -48.00	-47.30 $-48.06$	-48.11	-48.17	-48.22	-48.28
-55	-48.33	-47.83 -48.39	-48.44	-47.94 $-48.50$	-48.56	-48.61	-48.67	-48.72	-48.78	-48.83
-56	-48.89	-48.94	-49.00	-49.06	-49.11	-49.17	-49.22	-49.28	-49.33	-49.39
State of	area l	n see il			200	*	Shipping.			
-57	-49.44	-49.50	-49.56	-49.61	-49.67	-49.72	-49.78	-49.83	-49.89	-49.94
-58	-50.00	-50.06	-50.11	-50.17	-50.22	-50.28	-50.33	-50.39 $-50.94$	-50.44 -51.00	-50.50 -51.06
-59	-50.56	-50.61	-50.67	-50.72	-50.78	-50.83 $-51.39$	-50.89 -51.44	-51.50	-51.56	-51.61
-60 -61	-51.11 -51.67	-51.17 -51.72	-51.22 -51.78	-51.28 -51.83	-51.33 -51.89	-51.94	-51.44 $-52.00$	-52.06	-52.11	-52.17
-01	-51.67	-51.72	-91.70	-51.05	-51.65	-51.54	-52.00	32.00	02.11	02.11
-62	-52.22	-52.28	-52.33	-52.39	-52.44	-52.50	-52.56	-52.61	-52.67	-52.79
-63	-52.78	-52.83	-52.89	-52.94	-53.00	-53.06	-53.11	-53.17	-53.22	-53.28
-64	-53.33	-53.39	-53.44	-53.50	-53.56	-53.61	-53.67	-53.72	-53.78	-53.83
-65	-53.89	-53.94	-54.00	-54.06	-54.11	-54.17	-54.22	-54.28	-54.33	-54.39
-66	-54.44	-54.50	-54.56	-54.61	-54.67	-54.72	-54.78	-54.83	-54.89	-54.9
-67	-55.00	-55.06	-55.11	-55.17	-55.22	-55.28	-55.33	-55.39	-55.44	-55.50
-68	-55.56	-55.61	-55.67	-55.72	-55.78	-55.83	-55.89	-55.94	-56.00	-56.00
-69	-56.11	-56.17	-56.22	-56.28	-56.33	-56.39	-56.44	-56.50	-56.56	-56.6
-70	-56.67	-56.72	-56.78	-56.83	-56.89	-56.94	-57.00	-57.06	-57.11	-57.1
-71	-57.22	-57.28	-57.33	-57.39	-57.44	-57.50	-57.56	-57.61	-57.67	-57.79
-	E	EM OS	57 00	-57.94	-58.00	-58.06	-58.11	-58.16	-58.22	-58.28
-72 -72	-57.78 -58 33	-57.83 -58.39	-57.89 -58.44	-58.50	-58.56	-58.61	-58.67	-58.72	-58.78	-58.83
-73 -74	-58.33 -58.89	-58.94	-59.00	-59.06	-59.11	-59.17	-59.22	-59.28	-59.33	-59.39
-74 -75	-59.44	-59.50	-59.56	-59.61	-59.67	-59.72	-59.78	-59.83	-59.89	-59.94
<b>-76</b>	-60.00	-60.06	-60.11	-60.17	-60.22	-60.28	-60.33	-60.39	-60.44	-60.50
	-	-	0	9		K	a	lly lly	0	
	0.	1.	. 2.	3.	4.	5.	6.	7.	8.	9.

Degrees of	THE RESIDENCE	100			Tenths of	a Degree.			5 7, 96	The series			
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
+122	Reaumur.	Reaumur. +40.04		Reaumur. +40.13	Reaumur. +40.18	Reaumur. +40.22	Reaumur. +40.27	Reaumur.		Reaumu			
	1770		+40.09			Contract of the second	The second	+40.31	+40.36	+40.40			
121	39.56	39.60	39.64	39.69	39.73	39.78	39.82	39.87	39.91	39.9			
120	39.11	39.16	39.20	39.24	39.29	39.33	39.38	39.42	39.47	39.5			
119	38.67	38.71	38.76	38.80	38.84	38.89	38.93	38.98	39.02	39.0			
118	38.22	38.27	38.31	38.36	38.40	38.44	38.49	38.53	38.58	38.6			
117	37.78	37.82	37.87	37.91	37.96	38.00	38.04	38.09	38.13	38.1			
116	37.33	37.38	37.42	37.47	37.51	37.56	37.60	37.64	37.69	37.7			
115	36.89	36.93	36.98	37.02	37.07	37.11	37.16	37.20	37.24	37.2			
114	36.44	36.49	36.53	36.58	36.62	36.67	36.71	36.76	36.80	36.8			
113	36.00	36.04	36.09	36.13	36.18	36.22	36.27	36.31	36.36	36.4			
112	35.56	35.60	35.64	35.69	35.73	35.78	35.82	35.87	35.91	35.9			
111	35.11	35.16	35.20	35.24	35.29	35.33	35.38	35.42	35.47	35.5			
110	34.67	34.71	34.76	34.80	34.84	34.89	34.93	34.98	35.02	35.0			
109	34.22	34.27	34.31	34.36	34.40	34.44	34.49	34.53	34.58	34.6			
108	33.78	33.82	33.87	33.91	33.96	34.00	34.04	34.09	34.13	34.1			
107	33.33	33.38	33.42	33.47	33.51	33.56	33.60	33.64	33.69	33.7			
103	32.89	32.93	32.98	33.02	33.07	33.11	33.16	33.20	33.24	33.2			
105	32.44	32.49	32.53	32.58	32.62	32.67	32.71	32.76	32.80	32.8			
104	32.00	32.04	32.09	32.13	32.18	32.22	32.27	32.31	32.36	32.4			
103	31.56	31.60	31.64	31.69	31.73	31.78	31.82	31.87	31.91	31.9			
102	31.11	31.16	31.20	31.24	31.29	31.33	31.38	31.42	31.47	31.5			
101	30.67	30.71	30.76	30.80	30.84	30.89	30.93	30.98	31.02	31.0			
100	30.22	30.27	30.31	30.36	30.40	30.44	30.49	30.53	30.58	30.6			
99	29.78	29.82	29.87	29.91	29.96	30.00	30.04	30.09	30.13	30.1			
98	29.33	29.38	29.42	29.47	29.51	29.56	29.60	29.64	29.69	29.7			
97	28.89	28.93	28.98	29.02	29.07	29.11	29.16	29.20	29.24	29.2			
96	28.44	28.49	28.53	28.58	28.62	28.67	28.71	28.76	28.80	28.8			
95	28.00	28.04	28.09	28.13	28.18	28.22	28.27	28.31	28.36	28.4			
94	27.56	27.60	27.64	27.69	27.73	27.78	27.82	27.87	27.91	27.9			
93	27.11	27.16	27.20	27.24	27.29	27.33	27.38	27.42	27.47	27.5			
92	26.67	26.71	26.76	26.80	26.84	26.89	26.93	26.98	27.02	27.0			
91	26.22	26.27	26.31	26.36	26.40	26.44	26.49	26.53	26.58	26.6			
90	25.78	25.82	25.87	25.91	25.96	26.00	The state of the state of	26.09	With Mr. P.	2.2			
89	25.33	25.38	25.42	25.47		and the second of	26.04	Chief L.	26.13	26.1			
88	24.89	24.93	24.98	25.47	25.51 25.07	25.56 25.11	25.60 25.16	25.64 25.20	25.69 25.24	25.2			
87	24.44	24.40	04.50	04.50	Marie 1	Like i		1,23-1					
86	24.44	24.49	24.53	24.58	24.62	24.67	24.71	24.76	24.80	24.8			
1		24.04	24.09	24.13	24.18	24.22	24.27	24.31	24.36	24.4			
85	23.56	23.60	23.64	23.69	23.73	23.78	23.82	23.87	23.91	23.9			
84	23.11	23.16	23.20	23.24	23.29	23.33	23.38	23.42	23.47	23.5			
83 82	22.67	22.71 22.27	22.76 22.31	22.80 22.36	22.84 22.40	22.89	22.93	22.98	23.02 22.58	23.0			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

Degrees of Fahren- heit.	Tenths of a Degree.									
	0.	. 1.	2.	.3.	4.,	5.	6.	7.	s.	9.
1 1	Reaumur.		Reaumur.	Reaumur.	Reaumur.	Management of the Control of the Con	Reaumur.	Reaumur.	Reaumur.	Reaum
+81	+21.78	+21.82	+21.87	+21.91	+21.96	+22.00	+22.04	+22.09	+22.13	+22.1
80	21.33	21.38	21.42	21.47	21.51	21.56	21.60	21.64	21.69	21.7
79	20.89	20.93	20.98	21.02	21.07	21.11	21.16	21.20	21.24	21.2
78	20.44	20.49	20.53	20.58	20.62	20.67	20.71	20.76	20.80	20.8
77	20.00	20.04	20.09	20.13	20.18	20.22	20.27	20.31	20.36	20.4
76	19.56	19.60	19.64	19.69	19.73	19.78	19.82	19.87	19.91	19.9
75	19.11	19.16	19.20	19.24	19.29	19.33	19.38	19.42	19.47	19.5
74	18.67	18.71	18.76	18.80	18 84	18.89	18.93	18.98	19.02	19.0
73	18.22	18.27	18.31	18.36	18.40	18.44	18.49	18.53	18.58	18.6
72	17.78	17.82	17.87	17.91	17.96	18.00	18.04	18.09	18.13	18.1
71	17.33	17.38	17.42	17.47	17.51	17.56	17.60	17.64	17.69	17.7
70	16.89	16.93	16.98	17.02	17.07	17.11	17.16	17.20	17.24	17.2
69	16.44	16.49	16.53	16.58	16.62	16.67	16.71	16.76	16.80	16.8
68	16.00	16.04	16.09	16.13	16.18	16.22	16.27	16.31	16.36	16.4
67	15.56	15.60	15.64	15.69	15.73	15.78	15.82	15.87	15.91	15.9
66	15.11	15.16	15.20	15.24	15.29	15.33	15.38	15.42	15.47	15.5
65	14.67	14.71	14.76	14.80	14.84	14.89	14.93	14.98	15.02	15.0
64	14.22	14.27	14.31	14.36	14.40	14.44	14.49	14.53	14.58	14.6
63	13.78	13.82	13.87	13.91	13 96	14.00	14.04	14.09	14.13	14.1
62	13.33	13.38	13.42	13.47	13.51	13.56	13.60	13.64	13.69	13.7
61	12.89	12.93	12.98	13.02	13.07	13.11	13.16	13.20	13.24	13.2
60	12.44	12.49	12.53	12.58	12.62	12.67	-12.71	12.76	12.80	12.8
59	12.00	12.04	12.09	12.13	12.18	12.22	12.27	12.31	12.36	12.4
58	11.56	11.60	11.64	11.69	11.73	11.78	11.82	11.87	11.91	11.9
57	11.11	11.16	11.20	11.24	11.29	11.33	11.38	11.42	11.47	11.5
56	10.67	10.71	10.76	10.80	10.84	10.89	10.93	10.98	11.02	11.0
55	10.22	10.27	10.31	10.36	10.40	10.44	10.49	10.53	10.58	10.6
54	9.78	9.82	9.87	9.91	9.96	10.00	10.04	10.09	10.13	10.1
53	9.33	9.38	9.42	9.47	9.51	9.56	9.60	9.64	9.69	9.7
52	8.89	8.93	8.98	9.02	9.07	9.11	9.16	9.20	9.24	9.2
51	8.44	8.49	8.53	8.58	8.62	8.67	8.71	8.76	8.80	8.8
50	8.00	8.04	8.09	8.13	8.18	8.22	8.27	8.31	8.36	8.4
49	7.56	7.60	7.64	7.69	7.73	7.78	7.82	7.87	7.91	7.9
48	7.11	7.16	7.20	7.24	7.29	7.33	7.38	7.42	7.47	7.5
47	6.67	6.71	6.76	6.80	6.84	6.89	6.93	6.98	7.02	7.0
46	6.22	6.27	6.31	6.36	6.40	6.44	6.49	6.53	6.58	6.6
45	5.78	5.82	5.87	5.91	5.96	6.00	6.04	6.09	6.13	6.1
44	5 33	5.38	5.42	5.47	5.51	5.56	5.60	5.64	5.69	5.7
43	4.89	4.93	4.98	5.02	5.07	-5.11	5.16	5.20	5.24	5.2
42	4.44	4.49	4.53	4.58	4.62	4.67	4.71	4.76	4.80	4.8
41	4.00	4.04	4.09	4.13	4.18	4.22	4.27	4.31	4.36	4.4

Degrees of Fahren- heit.	Tenths of a Degree.									
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
HARRIE TO	Reaumur	Reaumur.	Reaumui							
+40	+ 3.56	+ 3.60	+ 3.64	+ 3.69	+ 3.73	+ 3.78	+ 3.82	+ 3.87	+ 3.91	+ 3.96
39	3.11	3.16	3.20	3.24	3.29	3.33	3.38	3.42	3.47	3.51
38	2.67	2.71	2.76	2.80	2.84	2.89	2.93	2.98	3.02	3.07
37	2.22	2.27	2.31	2.36	2.40	2.44	2.49	2.53	2.58	2.62
36	1.78	1.82	1.87	1.91	1.96	2.00	2.04	2.09	2.13	2.18
35	1.33	1.38	1.42	1.47	1.51	1.56	1.60	1.64	1.69	1.73
34	0.89	0.93	0.98	1.02	1.07	1.11	1.16	1.20	1.24	1.29
33	0.44	0.49	0.53	0.58	0.62	0.67	0.71	0.76	0.80	0.84
32	0.00	0.04	0.09	0.13	0.18	0.22	0.27	0.31	0.36	0.40
31	- 0.44	- 0.40	- 0.36	- 0.31	- 0.27	- 0.22	- 0.18	- 0.13	- 0.09	- 0.04
30	- 0.89	- 0.84	- 0.80	- 0.76	- 0.71	- 0.67	- 0.62	- 0.58	- 0.53	- 0.49
29	- 1.33	- 1.29	- 1.24	- 1.20	- 1.16	- 1.11	- 1.07	- 1.02	- 0.98	- 0.98
28	- 1.78	- 1.73	- 1.69	- 1.64	- 1.60	- 1.56	- 1.51	- 1.47	- 1.42	- 1.38
27	- 2.22	- 2.18	- 2.13	- 2.09	- 2.04	- 2.00	- 1.96	- 1.91	- 1.87	- 1.89
26	- 2.67	- 2.62	- 2.58	- 2.53	- 2.49	- 2.44	- 2.40	- 2.36	- 2.31	- 2.27
25	- 3.11	- 3.07	- 3.02	- 2.98	- 2.93	- 2.89	- 2.84	- 2.80	- 2.76	- 2.7
24	- 3.56	- 3.51	- 3.47	- 3.42	- 3.38	- 3.33	- 3.29	- 3.24	- 3.20	- 3.1
23	- 4.00	- 3.96	- 3.91	- 3.87	- 3.82	- 3.78	- 3.73	- 3.69	- 3.64	- 3.6
22	- 4.44	- 4.40	- 4.36	- 4.31	- 4.27	- 4.22	- 4.18	- 4.13	- 4.09	- 4.0
21	- 4.89	- 4.84	- 4.80	- 4.76	- 4.71	- 4.67	- 4.62	- 4.58	- 4.53	- 4.4
20	- 5.33	- 5.29	- 5.24	- 5.20	- 5.16	- 5.11	- 5.07	- 5.02	- 4.98	- 4.9
19	- 5.78	- 5.73	- 5.69	- 5.64	- 5.60	- 5.56	- 5.51	- 5.47	- 5.42	- 5.3
18	- 6.22	- 6.18	- 6.13	- 6.09	- 6.04	- 6.00	- 5.96	- 5.91	- 5.87	- 5.8
17	- 6.67	- 6.62	- 6.58	- 6.53	- 6.49	- 6.44	- 6.40	- 6.36	- 6.31	- 6.2
16	- 7.11	- 7.07	- 7.02	- 6.98	- 6.93	- 6.89	- 6.84	- 6.80	- 6.76	- 6.7
15	- 7.56	- 7.51	- 7.47	- 7.42	- 7.38	- 7.33	- 7.29	- 7.24	- 7.20	- 7.1
14	- 8.00	- 7.96	- 7.91	- 7.87	- 7.82	- 7.78	- 7.73	- 7.69	- 7.64	- 7.6
13	- 8.44	- 8.40	- 8.36	- 8.31	- 8.27	- 8.22	- 8.18	- 8.13	- 8.09	- 8.0
12	- 8.89	- 8.84	- 8.80	- 8.76	- 8.71	- 8.67	- 8.62	- 8.58	- 8.53	- 8.4
11	- 9.33	- 9.29	- 9.24	- 9.20	- 9.16	- 9.11	- 9.07	- 9.02	- 8.98	- 8.9
10	- 9.78	- 9.73	- 9.69	- 9.64	- 9.60	- 9.56	- 9.51	- 9.47	- 9.42	- 9.3
9	-10.22	-10.18	-10.13	-10.09	-10.04	-10.00	- 9.96	- 9.91	- 9.87	- 9.8
8	-10.67	-10.62	-10.58	-10.53	-10.49	-10.44	-10.40	-10.36	-10.31	-10.2
7	-11.11	-11.07	-11.02	-10.98	-10.93	-10.89	-10.84	-10.80	-10.76	-10.7
6	-11.56	-11.51	-11.47	-11.42	-11.38	-11.33	-11.29	-11.24	-11.20	-11.1
5	-12.00	-11.96	-11.91	-11.87	-11.82	-11.78	-11.73	-11.69	-11.64	-11.6
4	-12.44	-12.40	-12.36	-12.31	-12.27	-12.22	-12.18	-12.13	-12.09	-12.0
3	-12.89	-12.84	-12.80	-12.76	-12.71	-12.67	-12.62	-12.58	-12.53	-12.4
2	-13.33	-13.29	-13.24	-13.20	-13.16	-13.11	-13.07	-12.02	-12.98	-12.9
1	-13.78	-13.73	-13.69	-13.64	-13.60	-13.56	-13.51	-13.47	-13.42	-13.3
+ 0	-14.22	-14.18	-14.13	-14.09	-14.04	-14.00	-13.96	-13.91	-13.87	-13.8
Have i	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Degrees of Fahren-		Tenths of a Degree.									
Fahren- he it.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	
- 0	-14.22	-14.27	-14.31	-14.36	-14.40	-14.44	-14.49	-14.53	-14.58	-14.62	
- 1	-14.67	-14.71	-14.76	-14.80	-14.84	-14.89	-14.93	-14.98	-15.02	-15.07	
- 2	-15.11	-15.16	-15.20	-15.24	-15.29	-15.33	-15.38	-15.42	-15.47	-15.51	
- 3	-15.56	-15.60	-15.64	-15.69	-15.73	-15.78	-15.82	-15.87	-15.91	-15.96	
- 4	-16.00	-16.04	-16.09	-16.13	-16.18	-16.22	-16.27	-16.31	-16.36	-16.40	
- 5	-16.44	-16.49	-16.53	-16.58	-16.62	-16.67	-16.71	-16.76	-16.80	-16.84	
- 6	-16.89	-17.93	-16.98	-17.02	-17.07	-17.11	-17.16	-17.20	-17.24	-17.29	
- 7	-17.33	-17.38	-17.42	-17.47	-17.51	-17.56	-17.60	-17.64	-17.69	-17.73	
-8	-17.78	-18.82	-17.87	-17.91	-17.96	-18.00	-18.04	-18.09	-18.13	-18.18	
- 9	-18.22	-18.27	-18.31	-18.36	-18.40	-18.44	-18.49	-18.53	-18.58	-18.62	
-10	-18.67	-18.71	-18.76	-18.80	-18.84	-18.89	-18.93	-18.98	-19.02	-19.07	
-11	-19.11	-19.16	-19.20	-19.24	-19.29	-19.33	-19.38	-19.42	-19.47	-19.51	
-12	-19.56	-19.60	-19.64	-19.69	-19.73	-19.78	-19.82	-19.87	-19.91	-19.96	
-13	-20.00	-20.04	-20.09	-20.13	-20.18	-20.22	-20.27	-20.31	-20.36	-20.40	
-14	-20.44	-20.49	-20.53	-20.58	-20.62	-20.67	-20.71	-20.76	-20.80	-20.84	
-15	-20.89	-20.93	-20.98	-21.02	-21.07	-21.11	-21.16	-21.20	-21.24	-21.29	
-16	-21.33	-21.38	-21.42	-21.47	-21.51	-21.56	-21.60	-21.64	-21.69	-21.73	
-17	-21.78	-21.82	-21.87	-21.91	-21.96	-22.00	-22.04	-22.09	-22.13	-22.18	
-18	-22.22	-22.27	-22.31	-22.36	-22.40	-22.44	-22.49	-22.53	-22.58	-22.62	
-19	-22.67	-22.71	-22.76	-22.80	-22.84	-22.89	-22.93	-22.98	-23.02	-23.07	
-20	-23.11	-23.16	-23.20	-23.24	-23.29	-23.33	-23.38	-23.42	-23.47	-23.51	
-21	-23.56	-23.60	-23.64	-23.69	-23.73	-23.78	-23.82	-23.87	-23.91	-23.96	
-22	-24.00	-24.04	-24.09	-24.13	-24.18	-24.22	-24.27	-24.31	-24.36	-24.40	
-23	-24.44	-24.49	-24.53	-24.58	-24.62	-24.67	-24.71	-24.76	-24.80	-24.84	
-24	-24.89	-24.93	-24.98	-25.02	-25.07	-25.11	-25.16	-25.20	-25.24	-25.29	
-25	-25.33	-25.38	-25.42	-25.47	-25.51	-25.56	-25.60	-25.64	-25.69	-25.73	
-26	-25.78	-25.82	-25.87	-25.91	-25.96	-26.00	-26.04	-26.09	-26.13	-26.18	
-27	-26.22	-26.27	-26.31	-26.36	-26.40	-26.44	-26.49	-26.53	-26.58	-26.62	
-28	-26.67	-26.71	-26.76	-26.80	-26.84	-26.89	-26.93	-26.98	-27.02	-27.07	
-29	-27.11	-27.16	-27.20	-27.24	-27.29	-27.33	-27.38	-27.42	-27.47	-27.51	
-30	-27.56	-27.60	-27.64	-27.69	-27.73	-27.78	-27.82	-27.87	-27.91	-27.96	
-31	-28.00	-28.04	-28.09	-28.13	-28.18	-28.22	-28.27	-28.31	-28.36	-28.40	
-32	-28.44	-28.49	-28.53	-28.58	-28.62	-28.67	-28.71	-28.76	-28.80	-28.84	
-33	-28.89	-28.93	-28.98	-29.02	-29.07	-29.11	-29.16	-29.20	-29.24	-29.29	
-34	-29.33	-29.38	-29.42	-29.47	-29.51	-29.56	-29.60	-29.64	-29.69	-29.73	
-35	-29.78	-29.82	-29.87	-29.91	-29.96	-30.00	-30.04	-30.09	-30.13	-30.18	
-36	-30.22	-30.27	-30.31	-30.36	-30.40	-30.44	-30.49	-30.53	-30.58	-30.62	
-37	-30.67	-30.71	-30.76	-30.80	-30.84	-30.89	-30.93	-30.98	-31.02	-31.07	
-38	-31.11	-31.16	-31.20	-31.24	-31.29	-31.33	-31.38	-31.42	-31.47	-31.51	
-39	-31.56	-31.60	-31.64	-31.69	-31.73	-31.78	-31.82	-31.87	-31.91	-31.96	
-40	-32.00	-30.04	-30.09	-30.13	-30.18	-30.22	-30.27	-30.31	-30.36	-30.40	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

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从是是1995年1996年198日 1985年198日 1985年198日 1985年198日 1985年1985年1985年1985年1985年1985年1985年1985年	
图 1000 (11) 图第7图图 10图4 图图4 图图4 图图4 图图4 图图	
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## VI.-VII.

# COMPARISON

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in the feels will be a selected

## THE CENTIGRADE THERMOMETER

WITH

THE THERMOMETERS OF FAHRENHEIT AND OF REAUMUR.

OR

#### TABLES

FOR CONVERTING CENTIGRADE DEGREES INTO DEGREES OF FAHRENHEIT

AND OF REAUMUR;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF A DEGREE, FROM +50° TO -54° CENTIGRADE.

THE THERESONE THE PARTIES AND OF CEANING

#### TABLES

and the construction of the contract of the co

CONTROL THE CONTROL OF TO THE POST IN CHARGE OF A TRACE WAS A CONTROL OF THE POST OF THE P

				e tent an	Tenths of	Degrees.				
entigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
150	Fahren.	Fahren.	Fahren.	Fahren. +122.54	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahrer
+50	+122.00	+122.18 120.38			1	+122.90		+123.26	+123.44 121.64	+123.6
49	118.40		120.56	120.74	120.92	121.10	121.28	121.46	119.84	121.8
48	116.60	118.58 116.78	118.76 116.96	118.94	119.12	119.30	119.48 117.68	119.66 117.86	118.04	120.
46	114.80	114.98	115.16	115.34	117.32 115.52	117.50 115.70	117.08	116.06	116.24	118.
45	113.00	113.18	113.36	113.54	113.72	113.90	114.08	114.26	114.44	114.
44	111.20	111.38	111.56	111.74	111.92	112.10	112.28	112.46	112.64	112.
43	109.40	109.58	109.76	109.94	110.12	110.30	110.48	110.66	110.84	111.
42	107.60	107.78	107.96	108.14	108.32	108.50	108.68	108.86	109.04	109.
41	105.80	105.98	106.16	106.34	106.52	106.70	106.88	107.06	107.24	107.
40	104.00	104.18	104.36	104.54	104.72	104.90	105.08	105.26	105.44	105.
39	102.20	102.38	102.56	102.74	102.92	103.10	103.28	103.46	103.64	103.
38	100.40	100.58	100.76	100.94	101.12	101.30	101.48	101.66	101.84	102.
37	98.60	98.78	98.96	99.14	99.32	99.50	99.68	99.86	100.04	100.
36	96.80	96.98	97.16	97.34	97.52	97.70	97.88	98.06	98.24	98.
35	95.00	95.18	95.36	95.54	95.72	95.90	96.08	96.26	96.44	96.
34	93.20	93.38	93.56	93.74	93.92	94.10	94.28	94.46	94.64	94.
33	91.40	91.58	91.76	91.94	92.12	92.30	92.48	92.66	92.84	93.
32	89.60	89.78	89.96	90.14	90.32	90.50	90.68	90.86	91.04	91.
31	87.80	87.98	88.16	88.34	88.52	88.70	88.88	89.06	89.24	89.
30	86.00	86.18	86.36	86.54	86.72	86.90	87.08	87.26	87.44	87.
29	84.20	84.38	84.56	84.74	84.92	85.10	85.28	85.46	85.64	85.
28	82.40	82.58	82.76	82.94	83.12	83.30	83.48	83.66	83.84	.84.
27	80.60	80.78	80.96	81.14	81.32	81.50	81.68	81.86	82.04	82.
26	78.80	78.98	79.16	79.34	79.52	79.70	79.88	80.06	80.24	80.
25	77.00	77.18	77.36	77.54	77.72	77.90	78.08	78.26	78.44	78.
24	75.20	75.38	75.56	75.74	75.92	76.10	76.28	76.46	76.64	76.
23	73.40	73.58	73.76	73.94	74.12	74.30	74.48	74.66	74.84	75.
22	71.60	71.78	71.96	72.14	72.32	72.50	72.68	72.86	73.04	73.
21	69.80	69.98	70.16	70.34	70.52	70.70	70.88	71.06	71.24	71.
20	68.00	68.18	68.36	68.54	68.72	68.90	69.08	69.26	69.44	69.
19	66.20	66.38	66.56	66.74	66.92	67.10	67.28	67.46	67.64	67.
18	64.40	64.58	64.76	64.94	65.12	65.30	65.48	65.66	65.84	66.
17	62.60	62.78	62.96	63.14	63.32	63.50	63.68	63.86	64.04	64.5
16	60.80	60.98	61.16	61.34	61.52	61.70	61.88	62.06	62.24	62.
15	59.00	59.18	59.36	59.54	59.72	59.90	60.08	60.26	60.44	60.6
14	57.20	57.38	57.56	57.74	57.92	58.10	58.28	58.46	58.64	58.8
13	55.40	55.58	55.76	55.94	56.12	56.30	56.48	56.66	56.84	57.0
12	53.60	53.78	53.96	54.14	54.32	54.50	54.68	54.86	55.04	55.
11	51.80	51.98	52.16	52.34	52.52	52.70	52.88	53.06	53.24	53.4
1857	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

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				ang Bil	Tenths o	of Degrees.				
Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
110	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren. +50.90	Fahren.	Fahren.	Fahren. +51.44	Fahren.
+10	+50.00	+50.18	+50.36	+50.54	+50.72 48.92	49.10	+51.08	+51.26	49.64	+51.62
9	48.20	48.38	48.56	48.74	45.92	49.10	49.28	49.46	47.84	49.82
7	46.40	46.58	46.76	45.14	45.32	45.50	45.68	45.86	46.04	48.02
6	42.80	42.98	43.16	43.34	43.52	43.70	43.88	44.06	44.24	44.42
5	41.00	41.18	41.36	41.54	41.72	41.90	42.08	42.26	42.44	42.62
4	39.20	39.38	39.56	39.74	39.92	40.10	40.28	40.46	40.64	40.82
3	37.40	37.58	37.76	37.94	38.12	38.30	38.48	38.66	38.84	39.02
2	35.60	35.78	35.96	36.14	36.32	36.50	36.68	36.86	37.04	37.22
1	33.80	33.98	34.16	34.34	34.52	34.70	34.88	35.06	35.24	35.42
0	32.00	32.18	32.36	32.54	32.72	32.90	33.08	33.26	33.44	33.62
-0	32.00	31.82	31.64	31.46	31.28	31.10	30.92	30.74	30.56	30.38
- 1	30.20	30.02	29.84	29.66	29.48	29.30	29.12	28.94	28.76	28.58
- 2	28.40	28.22	28.04	27.86	27.68	27.50	27.32	27.14	26.96	26.78
- 3	26.60	26.42	26.24	26.06	25.88	25.70	25.52	25.34	25.16	24.98
- 4	24.80	24.62	24.44	24.26	24.08	23.90	23.72	23.54	23.36	23.18
- 5	23.00	22.82	22.64	22.46	22.28	22.10	21.92	21.74	21.56	21.38
- 6	21.20	21.02	20.84	20.66	20.48	20.30	20.12	19.94	19.76	19.58
- 7	19.40	19.22	19.04	18.86	18.68	18.50	18.32	18.14	17.96	17.78
- 8	17.60	17.42	17.24	17.06	16.88	16.70	16.52	16.34	16.16	15.98
- 9	15.80	15.62	15.44	15.26	15.08	14.90	14.72	14.54	14.36	14.18
-10	14.00	13.82	13.64	13.46	13.28	13.10	12.92	12.74	12.56	12.38
-11	12.20	12.02	11.84	11.66	11.48	11.30	11.12	10.94	10.76	10.58
-12	10.40	10.22	10.04	9.86	9.68	9.50	9.32	9.14	8.96	8.78
-13	8.60	8.42	8.24	8.06	7.88	7.70	7.52	7.34	7.16	6.98
-14	6.80	6.62	6.44	6.26	6.08	5.90	5.72	5.54	5.36	5.18
-15	5.00	4.82	4.64	4.46	4.28	4.10	3.92	3.74	3.56	3.38
-16	3.20	3.02	2.84	2.66	2.48	2.30	2.12	1.94	1.76	1.58
-17	1.40	1.22	1.04	0.86	0.68	0.50	0.32	0.14	- 0.04	- 0.22
-18	- 0.40	- 0.58	- 0.76	- 0.94	- 1.12	- 1.30	- 1.48	- 1.66	- 1.84	- 2.02
-19	- 2.20	- 2.38	- 2.56	- 2.74	- 2.92	- 3.10	- 3.28	- 3.46	- 3.64	- 3.82
-20	- 4.00	4.18	- 4.36	- 4.54	- 4.72	- 4.90	- 5.08	- 5.26	- 5.44	- 5.62
-21	- 5.80	- 5.98	- 6.16	- 6.34	- 6.52	- 6.70	- 6.88	- 7.06	- 7.24	- 7.42
-22	- 7.60	- 7.78	- 7.96	- 8.14	- 8.32	- 8.50	- 8.68	- 8.86	- 9.04	- 9.22
-23	- 9.40	- 9.58	- 9.76	- 9.94	-10.12	-10.30	-10.48	-10.66	-10.84	-11.02
-24	-11.20	-11.38	-11.56	-11.74	-11.92	-12.10	-12.28	-12.46	-12.64	-12.82
-25	-13.00	-13.18	-13.36	-13.54	-13.72	-13.90	-14.08	-14.26	-14.44	-14.62
-26	-14.80	-14.98	-15.16	-15.34	-15.52	-15.70	-15.88	-16.06	-16.24	-16.42
-27	-16.60	-16.78	-16.96	-17.14	-17.32	-17.50	-17.68	-17.86	-18.04	-18.22
-28	-18.40	-18.58	-18.76	-18.94	-19.12	-19.30	-19.48	-19.66	-19.84	-20.02
-29	-20.20	-20.38	-20.56	-20.74	-20.92	-21.10	-21.28	-21.46	-21.64	-21.82
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

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				- 480	Tenths of	Degrees.				
Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.
on EW	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.
-30	-22.00	-22.18	-22.36	-22.54	-22.72	-22.90	-23.08	-23.26	-23.44	-23.62
-31	-23.80	-23.98	-24.16	-24.34	-24.52	-24.70	-24.88	-25.06	-25.24	-25.42
-32	-25.60	-25.78	-25.96	-26.14	-26.32	-26.50	-26.68	-26.86	-27.04	-27.22
-33	-27.40	-27.58	-27.76	-27.94	-28.12	-28.30	-28.48	-28.66	-28.84	-29.02
-34	-29.20	-29.38	-29.56	-29.74	-29.92	-30.10	-30.28	-30.46	-30.64	-30.82
-35	-31.00	-31.18	-31.36	-31.54	-31.72	-31.90	-32.08	-32.26	-32.44	-32.62
-36	-32.80	-32.98	-33.16	-33.34	-31.72 $-33.52$	-33.70	-33.88	-34.06	-34.24	-34.42
-30 -37	-34.60	-34.78	-34.96	-35.14	-35.32	-35.50	-35.68	-35.86	-36.04	-36.22
-38	-36.40	-36.58	-36.76	-36.94	-37.12	-37.30	-37.48	-37.66	-37.84	-38.02
-39	-38.20	<b>-38.38</b>	-38.56	-38.74	-38.92	-39.10	-39.28	-39.46	-39.64	-39.82
-00	90.20	-30.00	00.00	90.11	00.02	50.10	00.20	00120	00.01	
-40	-40.00	-40.18	-40.36	-40.54	-40.72	-40.90	-41.08	-41.26	-41.44	-41.62
-41	-41.80	-41.98	-42.16	-42.34	-42.52	-42.70	-42.88	-43.06	-43.24	-43.42
-42	-43.60	-43.78	-43.96	-44.14	-44.32	-44.50	-44.68	-44.86	-45.04	-45.22
-43	-45.40	-45.58	-45.76	-45.94	-46.12	-46.30	-46.48	-46.66	-46.84	-47.02
-44	-47.20	-47.38	-47.56	-47.74	47.92	-48.10	-48.28	-48.46	-48.64	-48.82
Tal ca		2000	100		Karana 3	e i di	N 6 8 11 1	20 Feb.	at the bill	STATE OF
-45	-49.00	-49.18	-49.36	-49.54	-49.72	-49.90	-50.08	-50.26	-50.44	-50.62
-46	-50.80	-50.98	-51.16	-51.34	-51.52	-51.70	-51.88	-52.06	-52.24	-52.42
-47	-52.60	-52.78	-52.96	-53.14	-53.32	-53.50	-53.68	-53.86	-54.04	-54.22
-48	-54.40	-54.58	-54.76	-54.94	-55.12	-55.30	-55.48	-55.66	-55.84	-56.02
-49	-56.20	-56.38	-56.56	-56.74	-56.92	-57.10	-57.28	-57.46	-57.64	-57.82
D. China	The April	200	TAKE I	CHAPTER !	BEARING .	parties 1	11 (120)	BEST A	part I h	7/
-50	-58.00	-58.18	-58.36	-58.54	-58.72	-58.90	-59.08	-59.26	-59.44	-59.62
-51	-59.80	-59.98	-60.16	-60.34	-60.52	-60.70	-60.88	-61.06	-61.24	-61.42
-52	-61.60	-61.78	-61.96	-62.14	-62.32	-62.50	-62.68	-62.86	-63.04	-63.22
-53	-63.40	-63.58	-63.76	-63.94	-64.12	-64.30	-64.48	-64.66	-64.84	-65.02
-54	-65.20	-65.38	-65.56	-65.74	-65.92	-66.10	-66.28	-66.46	-66.64	-66.82

TABLE FOR COMPARING THE CENTIGRADE AND FAHRENHEIT'S THERMOMETERS NEAR THE BOILING POINT.

Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
Passar I	Fahren.									
100	212.00	212.18	212.36	212.54	212.72	212.90	213.08	213.26	213.44	213.62
99 .	210.20	210.38	210.56	210.74	210.92	211.10	211.28	211.46	211.64	211.82
98	208.40	208.58	208.76	208.94	209.12	209.30	209.48	209.66	209.84	210.02
97	206.60	206.78	206.96	207.14	207.32	207.50	207.68	207.86	208.04	208.22
96	204.80	204.98	205.16	205.34	205.52	205.70	205.88	206.06	206.24	206.42
95	203.00	203.18	203.36	203.54	203.72	203.90	204.08	204.26	204.44	204.62
94	201.20	201.38	201.56	201.74	201.92	202.10	202.28	202.46	202.64	202.82
93	199.40	199.58	199.76	199.94	200.12	200.30	200.48	200 66	200.84	201.09
92	197.60	197.78	197.96	198.14	198.32	198.50	198.68	198.86	199.04	199.22
91	195.80	195.98	196.16	196.34	196.52	196.70	196.88	197.06	197.24	197.45
90	194.00	194.18	194.36	194.54	194.72	194.90	195.08	195.26	195.44	195.63
89	192.20	192.38	192.56	192.74	192.92	193.10	193.28	193.46	193.64	193.8

				4-7-2	Tenths of	Degrees.				
Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
+40	Reaum. +32.00	Reaum. +32.08	Reaum. +32.16	Reaum. +32.24	Reaum. +32.32	Reaum. +32.40	Reaum. +32.48	Reaum. +32.56	Reaum. +32.64	Reaum. +32.72
39	31.20	31.28	31.36	31.44	31.52	31.60	31.68	31.76	31.84	31.92
38	30.40	30.48	30.56	30.64	30.72	30.80	30.88	30.96	31.04	31.12
37	29.60	29.68	29.76	29.84	29.92	30.00	30.08	30.16	30.24	30.32
36	28.80	28.88	28.96	29.04	29.12	29.20	29.28	29.36	29.44	29.52
35	28.00	28.08	28.16	28.24	28.32	28.40	28.48	28.56	28.64	28.72
34	27.20	27.28	27.36	27.44	27.52	27.60	27.68	27.76	27.84	27.92
33	26.40	26.48	25.56	26.64	26.72	26.80	26.88	26.96	27.04	27.12
32	25.60	25.68	25.76	25.84	25.92	26.00	26.08	26.16	26.24	26.32
31	24.80	24.88	24.96	25.04	25.12	25.20	25.28	25.36	25.44	25.52
30	24.00	24.08	24.16	24.24	25.32	24.40	24.48	24.56	24.64	24.72
29	23.20	23.28	23.36	23.44	23.52	23.60	23.68	23.76	23.84	23.92
28	22.40	22.48	22.56	22.64	22.72	22.80	22.88	22.96	23.04	23.12
27	21.60	21.68	21.76	21.84	21.92	22.00	22.08	22.16	22.24	22.32
26	20.80	20.88	20.96	21.04	21.12	21.20	21.28	21.36	21.44	21.52
25	20.00	20.08	20.16	20.24	20.32	20.40	20.48	20.56	20.64	20.72
24	19.20	19.28	19.36	19.44	19.52	19.60	19.68	19.76	19.84	19.92
23	18.40	18.48	18.56	18.64	18.72	18.80	18.88	18.96	19.04	19.12
22	17.60	17.68	17.76	17.84	17.92	18.00	18.08	18.16	18.24	18.32
21	16.80	16.88	16.96	17.04	17.12	17.20	17.28	17.36	17.44	17.52
20	16.00	16.08	16.16	16.24	16.32	16.40	16.48	16.56	16.64	16.72
19	15.20	15.28	15.36	15.44	15.52	15.60	15.68	15.76	15.84	15.92
18	14.40	14.48	14.56	14.64	14.72	14.80	14.88	14.96	15.04	15.12
17	13.60	13.68	13.76	13.84	13.92	14.00	14.08	14.16	14.24	14.32
16	12.80	12.88	12.96	13.04	13.12	13.20	13.28	13.36	13.44	13.52
15	12.00	12.08	12.16	12.24	12.32	12.40	12.48	12.56	12.64	12.72
14	11.20	11.28	11.36	11.44	11.52	11.60	11.68	11.76	11.84	11.92
13	10.40	10.48	10.56	10.64	10.72	10.80	10.88	10.96	11.04	11.12
12	9.60	9.68	9.76	9.84	9.92	10.00	10.08	10.16	10.24	10.32
11	8.80	8.88	8.96	9.04	9.12	9.20	9.28	9.36	9.44	9.52
10	8.00	8.08	8.16	8.24	8.32	8.40	8.48	8.56	8.64	8.72
9	7.20	7.28	7.36	7.44	7.52	7.60	7.68	7.76	7.84	7.92
8	6.40	6.48	6.56	6.64	6.72	6.80	6.88	6.96	7.04	7.12
7	5.60	5.68	5.76	5.84	5.92	6.00	6.08	6.16	6.24	6.32
6	4.80	4.88	4.96	5.04	5.12	5.20	5.28	5.36	5.44	5.52
5	4.00	4.08	4.16	4.24	4.32	4.40	4.48	4.56	4.64	4.72
4	3.20	3.28	3.36	3.44	3.52	3.60	3.68	3.76	3.84	3.92
3	2.40	2.48	2.56	2.64	2.72	2.80	2.88	2.96	3.04	3.12
2	1.60	1.68	1.76	1.84	1.92	2.00	2.08	2.16	2.24	2.32
1 2	0.80	0.88	0.96	1.04	1.12	1.20	1.28	1.36	1.44	1.52
ō	0.00	0.08	0.16	0.24	0.32	0.40	0.48	0.56	0.64	0.72
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

A

# VIII.-IX.

# COMPARISON

the barrier for the barrier, regard

Charles and the OF A MADI CALLED TO MADI

### REAUMUR'S THERMOMETER

WITH

THE THERMOMETER OF FAHRENHEIT AND THE CENTIGRADE THERMOMETER,

OR

### TABLES

FOR CONVERTING DEGREES OF REAUMUR INTO DEGREES OF FAHRENHEIT
AND INTO CENTIGRADE DEGREES;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF A DEGREE,

FROM +40° TO -40° REAUMUR.

					Tenths of	f Degrees.				
Degrees of Reaumur.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
1.40	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahre
+40	119.75	+122.22		+122.67		+123.12		0.74	+123.80	
39	117.50	119.97 117.72	120.20 117.95	120.42 118.17	120.65 118.40	120.87 118.62	121.10 118.85	121.32	121.55	121.
37	117.50	115.47	115.70	115.92	116.15	116.02	116.60	119.07 116.82	119.30	119.
36	113.00	113.22	113.45	113.67	113.90		114.35	114.57	117.05 114.80	117. 115.
35	110.75	110.97	111.20	111.42	111.65	111.87	112.10	112.32	112.55	112.
34	108.50	108.72	108.95	109.17	109.40	109.62	109.85	110.07	110.30	110.
33	106.25	106.47	106.70	106.92	107.15	107.37	107.60	107.82	108.05	108.
32	104.00	104.22	104.45	104.67	104.90	105.12	105.35	105.57	105.80	106.
31	101.75	101.97	102.20	102.42	102.65	102.87	103.10	103.32	103.55	103.
30	99.50	99.72	99.95	100.17	100.40	100.62	100.85	101.07	101.30	101.
29	97.25	97.47	97.70	97.92	98.15	98.37	98.60	98.82	99.05	99.
28	95.00	95.22	95.45	95.67	95.90	96.12	96.35	96.57	96.80	97.
27	92.75	92.97	93.20	93.42	93.65	93.87	94.10	94.32	94.55	94.
26	90.50	90.72	90.95	91.17	91.40	91.62	91.85	92.07	92.30	92.
25	88.25	88.47	88.70	88.92	89.15	89.37	89.60	89.82	90.05	90.
24	86.00	86.22	86.45	86.67	86.90	87.12	87.35	87.57	87.80	88.
23	83.75	83.97	84.20	84.42	84.65	84.87	85.10	85.32	85.55	85.
22	81.50	81.72	81.95	82.17	82.40	82.62	82.85	83.07	83.30	83.
21	79.25	79.47	79.70	79.92	80.15	80.37	80.60	80.82	81.05	81.5
20	77.00	77.22	77.45	77.67	77.90	78.12	78.35	78.57	78.80	79.0
19	74.75	74.97	75.20	75.42	75.65	75.87	76.10	76.32	76.55	76.7
18	72.50	72.72	72.95	73.17	73.40	73.62	73.85	74.07	74.30	74.
17	70.25	70.47	70.70	70.92	71.15	71.37	71.60	71.82	72.05	72.2
16	68.00	68.22	68.45	68.67	68.90	69.12	69.35	69.57	69.80	70.0
15	65.75	65.97	66.20	66.42	66.65	66.87	67.10	67.32	67.55	67.
14	63.50	63.72	63.95	64.17	64.40	64.62	64.85	65.07	65.30	65.
13	61.25	61.47	61.70	61.92	62.15	62.37	62.60	62.82	63.05	63.2
12	59.00	59.22	59.45	59.67	59.90	60.12	60.35	60.57	60.80	61.0
11	756.75	56.97	57.20	57.42	57.65	57.87	58.10	58.32	58.55	58.7
100	54.50	54.72	54.95	55.17	55.40	55.62	55.85	56.07	56.30	56.5
9	52.25	52.47	52.70	52.92	53.15	53.37	53.60	53.82	54.05	54.2
8	50.00	50.22	50.45	50.67	50.90	51.12	51.35	51.57	51.80	52.0
7	47.75	47.97	48.20	48.42	48.65	48.87	49.10	49.32	49.55	49.7
6	45.50	45.72	45.95	46.17	46.40	46.62	46.85	47.07	47.30	47.5
5	43.25	43.47	43.70	43.92	44.15	44.37	44.60	44.82	45.05	45.2
4	41.00	41.22	41.45	41.67	41.90	42.12	42.35	42.57	42.80	43.0
3	38.75	38.97	39.20	39.42	39.65	39.87	40.10	40.32	40.55	40.7
2	36.50	36.72	36.95	37.17	37.40	37.62	37.85	38.07	38.30	38.5
1	34.25	34.47	34.70	34.92	35.15	35.37	35.60	35.82	36.05	36.2
-400	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

A

AV.				personal services	Tenths of	f Degrees.				
Degrees of Reaumur.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.
+ 0	+32.00	+32.22	+32.45	+32.67	+32.90	+33.12	+33.35	+33.57	+33.80	+34.02
- 0	32.00	31.77	31.55	31.32	31.10	30.87	30.65	30.42	30.20	29.97
- 1	29.75	29.52	29.30	29.07	28.85	28.62	28.40	28.17	27.95	27.72
- 2	27.50	27.27	27.05	26.82	26.60	26.37	26.15	25.92	25.70	25.47
- 3	25.25	25.02	24.80	24.57	24.35	24.12	23.90	23.67	23.45	23.22
- 4	23.00	22.77	22.55	22.32	22.10	21.87	21.65	21.42	21.20	20.97
- 5	20.75	20.52	20.30	20.07	19.85	19.62	19.40	19.17	18.95	18.72
- 6	18.50	18.27	18.05	17.82	17.60	17.37	17.15	16.92	16.70	16.47
-7	16.25	16.02	15.80	15.57	15.35	15.12	14.90	14.67	14.45	14.22
-8	14.00	13.77	13.55	13.32	13.10	12.87	12.65	12.42	12.20	11.97
- 9	11.75	11.52	11.30	11.07	10.85	10.62	10.40	10.17	9.95	9.72
-10	9.50	9.27	9.05	8.82	8.60	8.37	8.15	7.92	7.70	7.47
-11	7.25	7.02	6.80	6.57	6.35	6.12	5.90	5.67	5.45	5.22
-12	5.00	4.77	4.55	4.32	4.10	3.87	3.65	3.42	3.20	2.97
-13	2.75	2.52	2.30	2.07	1.85	1.62	1.40	1.17	0.95	0.72
-14	0.50	0.27	0.05	- 0.17	- 0.40	- 0.62	- 0.85	- 1.07	- 1.30	- 1.52
-15	- 1.75	- 1.97	- 2.20	- 2.42	- 2.65	- 2.87	- 3.10	- 3.32	- 3.55	- 3.77
-16	- 4.00	- 4.22	- 4.45	- 4.67	- 4.90	- 5.12	- 5.35	- 5.57	- 5.80	- 6.02
-17	- 6.25	- 6.47	- 6.70	- 6.92	- 7.15	- 7.37	- 7.60	- 7.82	- 8.05	- 8.27
-18	- 8.50	- 8.72	- 8.95	- 9.17	- 9.40	- 9.62	- 9.85	-10.07	-10.30	-10.52
-19	-10.75	-10.97	-11.20	-11.42	-11.65	-11.87	-12.10	-12.32	-12.55	-10.32 $-12.77$
-20	-13.00	-13.22	-13.45	-13.67	-13.90	-14.12	-14.35	-14.57	-14.80	-15.02
-21	-15.25	-15.47	-15.70	-15.92	-16.15	-16.37	-16.60	-16.82	-17.05	-17.27
-21 -22	-17.50	-17.72	-17.95	-18.17	-18.40	-18.62	-18.85	-19.07	-19.30	-19.52
-22 -23	1 P. L. C. L. S.	LOW DIS	-20.20	-20.42	-18.40 $-20.65$	-20.87	-21.10	-21.32	-21.55	-19.52 $-21.77$
	-19.75	-19.97		-20.42		-23.12	-21.10 $-23.35$	-21.52 $-23.57$	-23.80	-21.77 $-24.02$
-24	-22.00	-22.22	-22.45	-22.67	-22.90	-25.12	-23.33	-23.57	-25.50	-24.02
-25	-24.25	-24.47	-24.70	-24.92	-25.15	-25.37	-25.60	-25.82	-26.05	-26.27
-26	-26.50	-26.72	-26.95	-27.17	-27.40	-27.62	-27.85	-28.07	-28.30	-28.52
-27	-28.75	-28.97	-29.20	-29.42	-29.65	-29.87	-30.10	-30.32	-30.55	-30.77
-28	-31.00	-31.22	-31.45	-31.67	-31.90	-32.12	-32.35	-32.57	-32.80	-33.02
-29	-33.25	-33.47	-33.70	-33.92	-34.15	-34.37	-34.60	-34.82	-35.05	-35.27
-30	-35.50	-35.72	-35.95	-36.17	-36.40	-36.62	-36.85	-37.07	-37.30	37752
-31	-37.75	-37.97	-38.20	-38.42	-38.65	-38.87	-39.10	-39.32	-39.55	-39.77
-32	-40.00	-40.22	-40.45	-40.67	-40.90	-41.12	-41.35	-41.57	-41.80	-42.02
-33	-42.25	-42.47	-42.70	-42.92	-43.15	-43.37	-43.60	-43.82	-44.05	-44.27
-34	-44.50	-44.72	-44.95	-45.17	-45.40	-45.62	-45.85	-46.07	-46.30	-46.52
0.5	10 ===	10.00	4W 00	1W 10	45.05	4W 0=	40.30	10.00	40.55	46.7
-35	-46.75	-46.97	-47.20	-47.42	-47.65	-47.87	-48.10	-48.32	-48.55	-48.77
-36	-49.00	-49.22	-49.45	-49.67	-49.90	-50.12	-50.35	-50.57	-50.80	-51.02
-37	-51.25	-51.47	-51.70	-51.92	-52.15	-52.37	-52.60	-52.82	-53.05	-53.27
-38 -39	-53.50 -55.75	-53.72 -55.97	-53.95 -56.20	-54.17 -56.42	-54.40 -56.65	-54.62 -56.87	-54.85 -57.10	-55.07 -57.32	-55.30 -57.55	-55.52 $-57.77$
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DEMINE S	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

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37 36 35 34 33 32 31 30 29 28 27 26 25 24 23 22 21	46.25 45.00 43.75 42.50 41.25 40.00	46.38 45.13 43.88 42.63	46.50 45.25	46.63			49.50	49.63	49.75	49.8
36 35 34 33 32 31 30 29 28 27 26 25 24 23 22 21	45.00 43.75 42.50 41.25 40.00	45.13 43.88 42.63	45.25		16 75	48.13	48.25	48.38	48.50	48.6
35 34 33 32 31 30 29 28 27 26 25 24 23 22 21	43.75 42.50 41.25 40.00	43.88 42.63	in the second	45.38	40.70	46.88	47.00	47.13	47.25	47.3
34 33 32 31 30 29 28 27 26 25 24 23 22 21	42.50 41.25 40.00	42.63	44.00		45.50	45.63	45.75	45.88	46.00	46.1
33 32 31 30 29 28 27 26 25 24 23 22 21	41.25		1	44.13	44.25	44.38	44.50	44.63	44.75	44.8
32 31 30 29 28 27 26 25 24 23 22 21	40.00	41 00	42.75	42.88	43.00	43.13	43.25	43.38	43.50	43.6
30 29 28 27 26 25 24 23 22 21		41.38	41.50	41.63	41.75	41.88	42.00	42.13	42.25	42.3
30 29 28 27 26 25 24 23 22 21	38.75	40.13	40.25	40.38	40.50	40.63	40.75	40.88	41.00	41.1
29 28 27 26 25 24 23 22 21		38.88	39.00	39.13	39.25	39.38	39.50	39.63	39.75	39.8
28 27 26 25 24 23 22 21	37.50	37.63	37.75	37.88	38.00	38.13	38.25	38.38	38.50	38.6
28 27 26 25 24 23 22 21	36.25	36.38	36.50	36.63	36.75	36.88	37.00	37.13	37.25	37.3
27 26 25 24 23 22 21 20	35.00	35.13	35.25	35.38	35.50	35.63	35.75	35.88	36.00	36.1
26 25 24 23 22 21 20	33.75	33.88	34.00	34.13	34.25	34.38	34.50	34.63	34.75	34.8
24 23 22 21 20	32.50	32.63	32.75	32.88	33.00	33.13	33.25	33.38	33.50	33.6
24 23 22 21 20	31.25	31.38	31.50	31.63	31.75	31.88	32.00	32.13	32.25	32.3
23 22 21 20	30.00	30.13	30.25	30.38	30.50	30.63	30.75	30.88	31.00	31.1
22 21 20	28.75	28.88	29.00	29.13	29.25	29.38	29.50	29.63	29.75	29.8
21 20	27.50	27.63	27.75	27.88	28.00	28.13	28.25	28.38	28.50	28.6
	26.25	26.38	26.50	26.63	26.75	26.88	27.00	27.13	27.25	27.3
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19	25.00	25.13	25.25	25.38	25.50	25.63	25.75	25.88	26.00	26.1
	23.75	23.88	24.00	24.13	24.25	24.38	24.50	24.63	24.75	24.8
18	22.50	22.63	22.75	22.88	23.00	23.13	23.25	23.38	23.50	23.6
17	21.25	21.38	21.50	21.63	21.75	21.88	22.00	22.13	22.25	22.3
16	20.00	20.13	20.25	20.38	20.50	20.63	20.75	20.88	21.00	21.1
15	18.75	18.88	19.00	19.13	19.25	19.38	19.50	19.63	19.75	19.8
14	17.50	17.63	17.75	17.88	18.00	18.13	18.25	18.38	18.50	18.6
13	16.25	16.38	16.50	16.63	16.75	16.88	17.00	17.13	17.25	17.3
12	15.00	15.13	15.25	15.38	15.50	15.63	15.75	15.88	16.00	16.1
11	13.75	13.88	14.00	14.13	14.25	14.38	14.50	14.63	14.75	14.8
10	12.50	12.63	12.75	12.88	13.00	13.13	13.25	13.38	13.50	13.6
9	11.25	11.38	11.50	11.63	11.75	11.88	12.00	12.13	12.25	12.3
8	10.00	10.13	10.25	10.38	10.50	10.63	10.75	10.88	11.00	11.1
7	8.75	8.88	9.00	9.13	9.25	9.38	9.50	9.63	9.75	9.8
6	7.50	7.63	7.75	7.88	8.00	8.13	8.25	8.38	8.50	8.6
5	6.25	6.38	6.50	6.63	6.75	6.88	7.00	7.13	7.25	7.3
4	5.00	5.13	5.25	5.38	5.50	5.63	5.75	5.88	6.00	6.1
3	3.75	3.88	4.00	4.13	4.25	4.38	4.50	4.63	4.75	4.8
2	2.50	2.63	2.75	2.88	3.00	3.13	3.25	3.38	3.50	3.6
1	1.25	1.38	1.50	1.63	1.75	1.88	2.00	2.13	2.25	2.3
0	0.00	0.13	0.25	0.38	0.50	0.63	0.75	0.88	1.00	1.1

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### TABLES

FOR

### COMPARING THERMOMETRICAL DIFFERENCES

EXPRESSED IN DEGREES OF DIFFERENT SCALES,

IRRESPECTIVE OF THEIR ZERO POINT.

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# X. NUMBER OF DEGREES OF FAHRENHEIT == NUMBER OF CENTIGRADE DEGREES. 4° Reaumur = 5° Centigrade = 9° Fahrenheit.

Degrees					Tenths of	a Degree.				
of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	. 7.	S.	9.
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
0	0.00	0.06	0.11	0.17	0.22	0.28	0.33	0.39	0.44	0.50
1	0.56	0.61	0.67	0.72	0.78	0.83	0.89	0.94	1.00	1.06
2	1.11	1.17	1.22	1.28	1.33	1.39	1.44	1.50	1.56	1.61
3	1.67	1.72	1.78	1.83	1.89	1.94	2.00	2.06	2.11	2.22
4	2.22	2.28	2.33	2.39	2.44	2.50	2.56	2.61	2.67	2.72
5	2.78	2.83	2.89	2.94	3.00	3.06	3.11	3.17	3.22	3.28
6	3.33	3.39	3.44	3.50	3.56	3.61	3.67	4.72	3.78	3.83
7	3.89	3.94	4.00	4.06	4.11	4.17	4.22	4.28	4.33	4.39
8	4.44	4.50	4.56	4.61	4.67	4.72	4.78	4.83	4.89	4.94
9	5.00	5.06	5.11	5.17	5.22	5.28	5.32	5.39	5.44	5.50

### XI. NUMBER OF DEGREES OF FAHRENHEIT = NUMBER OF DEGREES OF REAUMUR.

Degrees					Tenths of	a Degree.				
of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.
0	0.00	0.04	0.09	0.13	0.18	0.22	0.27	0.31	0.36	0 40
1	0.44	0.49	0.53	0.58	0.62	0.67	0.71	0.76	0.80	0.84
2	0.89	0.93	0.98	1.02	1.07	1.11	1.16	1.20	1.24	1.29
3	1.33	1.38	1.42	1.47	1.51	1.56	1.60	1.64	1.69	1.73
4	1.78	1.82	1.87	1.91	1.96	2.00	2.04	2.09	2.13	2.18
	The second		THE			200		Alpha F		
5	2.22	2.27	2.31	2.36	2.40	2.44	2.49	2.53	2.58	2.62
6	2.67	2.71	2.76	2.80	2.84	2.89	2.93	2.98	3.02	3.07
7	3.11	3.16	3.20	3.24	3.29	3.33	3.38	3.42	3.47	3.51
8	3.56	3.60	3.64	3.69	3.73	3.78	3.82	3.87	3.91	3.96
9	4.00	4.04	4.09	4.13	4.18	4.22	4.27	4.31	4.36	4.40

#### XII. NUMBER OF CENTIGRADE DEGREES = NUMBER OF DEGREES OF REAUMUR.

				11444	Tenths of	a Degree.				
Centig. Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
N/H	Reaumur.	Reaumur	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.
0	0.00	0.08	0.16	0.24	0.32	0.40	0.48	0.56	0.64	0.72
1	0.80	0.88	0.96	1.04	1.12	1.20	1.28	1.36	1.44	1.52
2	1.60	1.68	1.76	1.84	1.92	2.00	2.08	2.16	2.24	2.32
3	2.40	2.48	2.56	2.64	2.72	2.80	2.88	2.96	3.04	3.12
4	3.20	3.28	3.36	3.44	3.52	3.60	3.68	3.76	3.84	3.92
5	4.00	4.08	4.16	4.24	4.32	4.40	4.48	4.56	4.64	4.72
6	4.80	4.88	4.96	5.04	5.12	5.20	5.28	5.36	5.44	5.52
7	5.60	5.68	5.76	5.84	5.92	6.00	6.08	6.16	6.24	6.32
8	6.40	6.48	6.56	6.64	6.72	6.80	6.88	6.96	7.04	7.12
9	7.20	7.28	7.36	7.44	7.52	7.60	7.68	7.76	7.84	7.92

XIII. NUMBER OF CENTIGRADE DEGREES = NUMBER OF DEGREES OF FAHRENHEIT.

4° Reaumur = 5° Centigrade = 9° Fahrenheit.

					Tenths of	a Degree.				
Centig. Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.
0	0.00	0.18	0.36	0.54	0.72	0.90	1.08	1.26	1.44	1.62
1	1.80	1.98	2.16	2.34	2.52	2.70	2.88	3.06	3.24	3.42
2	3.60	3.78	3.96	4.14	4.32	4.50	4.68	4.86	5.04	5.22
3	5.40	5.58	5.76	5.94	6.12	6.30	6.48	6.66	6.84	7.02
4	7.20	7.38	7.56	7.74	7.92	8.10	8.28	8.46	8.64	8.82
5	9.00	9.18	9.36	9.54	9.72	9.90	10.08	10.26	10.44	10.62
6	10.80	10.98	11.16	11.34	11.52	11.70	11.88	12.06	12.24	12.42
7	12.60	12.78	12.96	13.14	13.32	13.50	13.68	13.86	14.04	14.22
. 8	14.40	14.58	14.76	14.94	15.12	15.30	15.48	15.66	15.84	16.02
9	16.20	16.38	16.56	16.74	16.92	17.10	17.28	17.46	17.64	17.82

XIV. NUMBER OF DEGREES OF REAUMUR = NUMBER OF CENTIGRADE DEGREES.

Degrees of Reaum.	Tenths of a Degree.												
	0.	1.	2.	3.	4.	5.	6.	7.	S.	9.			
1500	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.			
0	0.00	0.12	0.25	0.37	0.50	0.62	0.75	0.87	1.00	1.12			
1	1.25	1.37	1.50	1.62	1.75	1.87	2.00	2.12	2.25	2.37			
2	2.50	2.62	2.75	2.87	3.00	3.12	3.25	3.37	3.50	3.62			
3	3.75	3.87	4.00	4.12	4.25	4.37	4.50	4.62	4.75	4.87			
4	5.00	5.12	5.25	5.37	5.50	5.62	5.75	5.87	6.00	6.12			
5	6.25	6.37	6.50	6.62	6.75	6.87	7.00	7.12	7.25	7.37			
6	7.50	7.62	7.75	7.87	8.00	8.12	8.25	8.37	8.50	8.62			
7	8.75	8.87	9.00	9.12	9.25	9.37	9.50	9.62	9.75	9.87			
8	10.00	10.12	10.25	10.37	10.50	10.62	10.75	10.87	11.00	11.12			
9	11.25	11.37	11.50	11.62	11.75	11.87	12.00	12.12	12.25	12.37			

XV. NUMBER OF DEGREES OF REAUMUR = NUMBER OF DEGREES OF FAHRENHEIT.

Degrees	Tenths of a Degree,													
of Reaum.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.				
0	0.00	0.22	0.45	0.67	0.90	1.12	1.35	1.57	1.80	2.02				
1	2.25	2.47	2.70	2.92	3.15	3.37	3.60	3.82	4.05	4.27				
2	4.50	4.72	4.95	5.17	5.40	5.62	5.85	6.07	6.30	6.52				
3	6.75	6.97	7.20	7.42	7.65	7.87	8.10	8.32	8.55	8.77				
4	9.00	9.22	9.45	9.67	9.90	10.12	10.35	10.57	10.80	11.02				
. 5	11.25	11.47	11.70	11.92	12.15	12.37	12.60	12.82	13.05	13.27				
6	13.50	13.72	13.95	14.17	14.40	14.62	14.85	15.07	15.30	15.52				
7	15.75	15.97	16.20	16.42	16.65	16.87	17.10	17.32	17.55	17.77				
8	18.00	18.22	18.45	18.67	18.90	19.12	19.35	19.57	19.80	20.02				
9	20.25	20.47	20.70	20.92	21.15	21.37	21.60	21.82	22.05	22,27				

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# METEOROLOGICAL TABLES.

II.

HYGROMETRICAL TABLES.

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### HYGROMETRICAL TABLES.

HYGROMETERS, or instruments used for determining the amount of aqueous vapor present in the air, are of three classes. In the first, we find the hygrometers based on the absorption of moisture by hygroscopic substances, the best of which is Saussure's Hair-Hygrometer; in the second class, the Psychrometer, or wet-bulb thermometer, which gives the temperature of evaporation; in the third, the various instruments designed for ascertaining the temperature of the dew-point. From the data furnished by each of these instruments, and a table of the elastic forces of vapor at different temperatures, the humidity of the air can be deduced with more or less accuracy.

The use of the hygroscopic substances as hygrometers having been nearly given up on account of the inaccuracy of the results, the variability of the instruments, and the difficulty, if not impossibility, of making them comparable, the psychrometer and the dew-point instruments represent the two methods now usually employed in Meteorology. The following set, therefore, contains extensive tables, in French and English measures, for deducing the hygrometrical condition of the atmosphere from the indications of the Psychrometer and of the dew-point instruments, to which have been added tables of the weight of vapor, in a given space, at different temperatures, — an element often needed in Meteorology.

As, however, the results deduced from the same data furnished by the observations may considerably differ, according to the values of the elastic force of vapor, and the formulæ used in the computation, the tables have been arranged in two series.

The first series contains Regnault's table of the elastic forces of vapor, with tables of the three kinds above mentioned, together with a corresponding set in English measures. Tables V. to X. have been computed for this volume.

The second series gives the table of elastic forces of vapor deduced from Dalton's experiments, and adopted in the Greenwich Observations, together with the various tables based on it.

B

#### HYGROMETRICAL TABLES.

A third series of miscellaneous tables furnishes the means of comparing the different values of the elastic force and weight of vapor determined by various physicists, as well as the results of Saussure's Hair-Hygrometer, with those obtained by other methods.

An Appendix, containing tables for comparing the quantity of rain-water indicated in different measures, closes the set.

Though the first series of tables, based on Regnault's table of tensions, is recommended for ordinary use, as being derived from the determinations which seem to deserve the greatest degree of confidence, it was thought expedient to give also the Greenwich tables, which have been, and still are, so extensively used in England, in order to enable meteorologists to judge of the differences which exist between the results obtained by them and those deduced from the constants of Regnault and others.

The bowever, the results sinduced from the same state. Imprefied for the observer,

# PRACTICAL TABLES,

IN

FRENCH MEASURES,

BASED ON REGNAULT'S HYGROMETRICAL CONSTANTS.

# PRACTICAL TABLES

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### TABLE

OF

### THE ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES,

BY REGNAULT.

This table contains the elastic forces of vapor corresponding to every tenth of a degree of temperature between — 35° and + 40° Centigrade, as determined by the experiments of V. Regnault, made by order of the French government, for the purpose of establishing the numerical value of the elements which enter into the computations concerning the steam-engine. These results are generally considered as the most accurate science possesses at present. They are published in the Mémoires de l'Institut, Tom. XXI.; and more correctly in Regnault's Etudes sur l'Hygrométrie, in the Annales de Chimie et de Physique. In Vol. XV. Regnault gives the table of elastic forces for every tenth of a degree from —10° to +35° Centigrade, which is reprinted in Table I. The numbers below —10° and above +35°, in the same table, have been taken from another table for every full degree, previously published in Vol. XI. p. 333 of the same periodical, and in the same volume of the Mémoires de l'Institut, extending from —32° to +230°.

It should be remarked, however, that the numbers below zero, in the two tables just mentioned, having been computed from different formulas of interpolation, slightly disagree. In order to establish a continuity, therefore, the numbers in Table I. corresponding to full degrees from  $-10^{\circ}$  to  $-35^{\circ}$  have been formed by starting from the value due to  $-10^{\circ}$  in the larger table of Regnault, and subtracting from it the difference between  $-10^{\circ}$  and  $-11^{\circ}$  in the other table, in order to find the value of  $-11^{\circ}$ , and so on, by subtracting successively the corresponding differences to  $-35^{\circ}$ . For the fractions of degrees below  $-10^{\circ}$ , the mean values have been adopted as sufficiently accurate for meteorological purposes.

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### I. ELASTIC FORCE OF AQUEOUS VAPOR,

#### EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES.

By REGNAULT.

Tempera-		B. #14.7	le his		Tenths of	f Degrees.	Since 1			
ture Centigrade.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
-35	0.221	0.219	0.216	0.214	0.211	0.209	0.207	0.204	0.202	0.199
-34	0.247	0.244	0.242	0.249	0.237	0.234	0.231	0.229	0.226	0.224
-33	0.275	0.272	0.269	0.267	0.264	0.261	0.258	0.255	0.253	0.250
-32	0.305	0.302	0.299	0.296	0.293	0.290	0.287	0.284	0.281	0.278
-31	0.337	0.334	0.331	0.327	0.324	0.321	0.318	0.315	0.311	0.308
-30	0.371	0.368	0.364	0.361	0.357	0.354	0.351	0.347	0.344	0.340
-29	0.409	0.405	0.401	0.398	0.394	0.390	0.386	0.382	0.379	0.375
-28	0.449	0.445	0.441	0.437	0.433	0.429	0.425	0.421	0.417	0.413
-27	0.493	0.489	0.484	0.480	0.475	0.471	0.467	0.462	0.458	0.453
-26	0.540	0.535	0.531	0.526	0.521	0.516	0.512	0.507	0.502	0.498
-25	0.590	0.585	0.580	0.575	0.570	0.565	0.560	0.555	0.550	0.545
-24	0.645	0.639	0.634	0.628	0.623	0.617	0.612	0.606	0.601	0.595
-23	0.704	0.698	0.692	0.686	0.680	0.674	0.669	0.663	0.657	0.651
-22	0.768	0.762	0.755	0.749	0.742	0.736	0.730	0.723	0.717	0.710
-21	0.838	0.831	0.824	0.817	0.810	0.803	0.796	0.789	0.782	0.775
-20	0.912	0.905	0.897	0.890	0.882	0.875	0.868	0.860	0.853	0.845
-19	0.993	0.985	0.977	0.969	0.961	0.952	0.944	0.936	0.928	0.920
-18	1.080	1.071	1.063	1.054	1.045	1.036	1.028	1.019	1.010	1.002
-17	1.174	1.165	1.155	1.146	1.136	1.127	1.118	1.108	1.099	1.089
-16	1.275	1.265	1.255	1.245	1.235	1.224	1.214	1.204	1.194	1.184
-15	1.385	1.374	1.363	1.352	1.341	1.330	1.319	1.308	1.297	1.286
-14	1.503	1.491	1.479	1.468	1.456	1.444	1.432	1.420	1.409	1.397
-13	1.631	1.618	1.605	1.593	1.580	1.567	1.554	1.541	1.529	1.516
-12	1.768	1.754	1.741	1.727	1.713	1.699	1.686	1.672	1.658	1.645
-11	1.918	1.903	1.888	1.873	1.858	1.843	1.828	1.813	1.798	1.783
-10	2.078	2.062	2.046	2.030	2.014	1.998	1.982	1.966	1.950	1.934
-9	2.261	2.242	2.223	2.204	2.186	2.168	2.150	2.132	2.114	2.096
-8	2.456	2.436	2.416	2.396	2.376	2.356	2.337	2.318	2.299	2.280
-7	2.666	2.645	2.624	2.603	2.582	2.561	2.540	2.519	2.498	2.477
- 6	2.890	2.867	2.844	2.821	2.798	2.776	2.754	2.732	2.710	2.688
-5	3.131	3.106	3.082	3.058	3.034	3.010	2.986	2.962	2.938	2.914
- 4	3.387	3.361	3.335	3.309	3.283	3.257	3.231	3.206	3.181	3.156
- 3	3.662	3.634	3.606	3.578	3.550	3.522	3.495	3.468	3.441	3.414
-2	3.955	3.925	3.895	3.865	3.836	3.807	3.778	3.749	3.720	3.691
-1	4.267	4.235	4.203	4.371	4.140	4.109	4.078	4.047	4.016	3.985
- 0	4.600	4.565	4.531	4.497	4 463	4.430	4.397	4.364	4.331	4.299
	0.	1.	2.	3.	4.	5.	6.	7.	S.	9.

Centigrade					Tenths of	Degrees.				PAGE.
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
Q	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin
0	4.600	4.633	4.667	4.700	4.733	4.767	4.801	4.836	4.871	4.90
1	4.940	4.975	5.011	5.047	5.082	5.118	5.155	5.191	5.228	5.26
2	5.302	5.340	5.378	5.416 5.807	5.454	5.491 5.889	5.530	5.569 5.972	5.608 6.014	6.05
3 4	6.097	5.727 6.140	5.767 6.183	6.226	5.848 6.270	6.313	6.357	6.401	6.445	6.49
5	6.534	6.580	6.625	6.671	6.717	6.763	6.810	6.857	6.904	6.95
6	6.998	7.047	7.095	7.144	7.193	7.242	7.292	7.342	7.392	7.44
7	7.492	7.544	7.595	7.647	7.699	7.751	7.804	7.857	7.910	7.96
8	8.017	8.072	8.126	8.181	8.236	8.291	8.347	8.404	8.461	8.51
9	8.574	8.632	8.690	8.748	8.807	8.865	8.925	8.985	9.045	9.10
10	9.165	9.227	9.288	9.350	9.412	9.474	9.537	9.601	9.665	9.72
11	9.792	9.857	9.923	9.989	10.054	10.120	10.187	10.255	10.322	10.38
12	10.457	10.526	10.596	10.665	10.734	10.804	10.875	10.947	11.019	11.09
13	11.162	11.235	11.309	11.383	11.456	11.530	11.605	11.681	11.757	11.83
14	11.908	11.986	12.064	12.142	12.220	12.298	12.378	12.458	12.538	12.61
15	2.699	12.781	12.864	12.947	13.029	13.112	13.197	13.281	13.366	13.45
16	13.536	13.623	13.710	13.797	13.885	13.972	14.062	14.151	14.241	14.33
17	14.421	14.513	14.605	14.697	14.790	14.882	14.977	15.072	15.167	15.26
18	1.357	15.454	15.552	15.650	15.747	15.845	15.945	16.045	16.145	16.24
19	16346	16.449	16.552	16.655	16.758	16.861	16.967	17.073	17.179	17.28
20	17391	17.500	17.608	17.717	17.826	17.935	18.047	18.159	18.271	18.38
21	18.95	18.610	18.724	18.839	18.954	19.069	19.187	19.305	19.423	19.54
22	19.659	19.780	19.901	20.022	20.143	20.265	20.389	20.514	20.639	20.76
23	20.88	21.016	21.144	21.272	21.400	21.528	21.659	21.790	21.921	22.05
24	22.184	22.319	22.453	22.588	22.723	22.858	22.996	23.135	23.273	23.41
25	23.55	23.692	23.834	23.976	24.119	24.261	24.406	24.552	24.697	24.84
26	24.988	25.138	25.288	25.438	25.588	25.738	25.891	26.045	26.198	26.35
27	26.505	26.663	26.820	26.978	27.136	27.294	27.455	27.617	27.778	27.93
28	28.101	28.267	28.433	28.599	28.765	28.931	29.101	29.271	29.441	29.61
29	29.782	29.956	30.131	30.305	30.479	30.654	30.833	31.011	31.190	31.36
30	31.548	1.729	31.911	32.094	32.278	32.463	32.650	32.837	33.026	33.21
31	33.406	3.596	33.787	33.980	34.174	34.368	34.564	34.761	34.959	35.15
32	35.359	3,559	35.760	35.962	36.165	36.370	36.576	36.783	36.991	37.20
33	37.410	37621	37.832	38.045	38.258	38.473	38.689	38.906	39.124	39.34
34 35	39.565 41.827	39 86 42.59	40.007 42.293	40.230 42.527	40.455	40.680	40.907 43.238	41.135	41.364 43.717	41.59
92	44.00	144	44.000	44.000	45 300	45 407	45 003	45.000	10.504	10 :
36	44.201 46.691	44.45	44.690	44.936	45.183	45.431	45.681	45.932	46.184	46.43
37 38	49.302	49.57	47.203 49.839	50.110	47.721 50.382	47.981 50.655	48.243 50.929	48.506 51.205	48.770	49.03
39	52.039	52.320	52.602	52.885	53.170	53.456	53.743	54.032	51.481 54.322	51.75
40	54.906	55.200		55.793	56.091	56.391	56.692	56.994	57.298	57.60
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

### PSYCHROMETRICAL TABLES.

GIVING IMMEDIATELY THE FORCE OF AQUEOUS VAPOR AND THE RELATIVE HUMIDITY FROM THE INDICATIONS OF THE PSYCHROMETER.

CALCULATED BY M. T. HAEGHENS.

In his Etudes sur l'Hygrométrie,\* M. V. Regnault discusses the theoretical bases of the formula of the Psychrometer, given by M. August, which was,

$$x = f' - \frac{0.568(t-t')}{640-t'}h,$$

in which h represents the height of the barometer; t the temperature of the air given by the dry-bulb thermometer; t' the temperature of the wet-bulb thermometer; f' the force of aqueous vapor in the saturated air at a temperature equal to t'; x he elastic force of aqueous vapor which exists in the air at the time of the observation.

After having modified some of the numerical values, which form the coefficients, M. Regnault adopted this formula,

 $x = f' - \frac{0.429 (t - t')}{610 - t'} h$ 

But comparative experiments, made by himself, showed that by substituting the coefficient 0.480 for that of 0.429, the calculated results, and those obtained by direct observation, agree perfectly in the fractions of saturation, which are greater than 0.40. This formula thus modified, or

 $x = f' - \frac{0.480 (t - t')}{610 - t'} h,$ 

has been used for calculating the following tables. In that part of the tables which supposes the wet-bulb to be covered with a film of ice, or below the freezing point, the value 610 — t', which represents the latent heat of aqueous vapor, has been changed into this: 610 + 79 - t' = 689 - t'.

The only hypothesis made, is that of a mean barometric pressure h, equal to 755 millimetres. If we take into account the causes of errors inherent to the psychrometer, and to the tables of the force of vapor, by means of which the absolute force of vapor is calculated, as well as to the differences of these tensions, taken at temperatures differing only by one tenth of a degree, it will be obvious that he correction due to the variations of barometric pressure can almost always be neglected. Nevertheless, a separate table has been calculated, giving the correction o be applied to the numbers in the Psychrometrical Tables for the heights of the barometer between 650 and 800 millimetres. It will be found at the end of the tables.

The disposition of the tables is the following: -

The temperatures are noted in centigrade degrees; the elaste force of vapor in the air, or its pressure on the barometer, is expressed in millimetes of mercury; the rel-

<sup>\*</sup> Etudes sur l'Hygrométrie, par M. V. Regnault. Annales de Chimie et de Physique, 3<sup>me</sup> Série, Tom XV., 1845.
B

ative humidity is indicated in per cent. of the full saturation of the air at the corresponding temperature of the dry-bulb thermometer t.

The first vertical column contains the indications of the wet-bulb thermometer t', beginning with the temperatures below the freezing point, when the bulb is covered with ice, from  $-35^{\circ}$ , and continuing from the freezing point up to  $+35^{\circ}$  centigrade, the bulb being simply wet.

The second column gives the differences of the force of vapor for each tenth (0°.1) of a degree, between each full degree of the first column. It enables the observer to find out the correction for any fraction of a degree of the wet-bulb thermometer.

The following double columns give immediately the force of vapor and the relative humidity, corresponding to each degree of the wet-bulb, placed in the first column, on the same horizontal line, and to differences of the two thermometers, or to t-t', taken at every two tenths of a degree.

The horizontal column at the bottom indicates the mean difference, for each tenth of a degree, of the force of vapor contained in the same horizontal line. It gives the correction for the intermediate differences of the thermometers; 0.1, 0.3, 0.5, 0.7, 0.9, &c., &c.

To meet the wants arising from the extreme climate of North America, the tables of Mr. Haeghens have been extended from -15° to -35° centigrade, and from +30° to +35° of temperature of the wet-bulb, and to +40° of temperature of the dry-bulb thermometer. The forces of aqueous vapor of Regnault, as given in Table I., have been used for the calculations.

### Use of the Tables.

Enter the tables with the difference of the two thermometers, or t-t', and with the temperature of the wet-bulb thermometer t', taking the first three pages, when the temperature of the wet-bulb is below the freezing point; and the following ones when it is above the freezing point.

Seek first the column at the head of which you find the difference of the thermometers; go down as far as the horizontal line, at the beginning of which you see the temperature of the wet-bulb thermometer; there you find the force of vapor, and the relative humidity corresponding to your observation.

Two corrections for fractions may be required for a complete calculation of the force of vapor; one for the fractions of degrees of the wet-bulb thermometer; another for the intermediate differences of the two thermometers, viz. for 0.1, 0.3, 0.5, 0.7, &c.

The first correction for fractions of degrees of the wet-bulb thermometer is found by multiplying the decimal fraction by the number placed in the second vertical column next to the whole degree, which number is the value of a tenth of a degree. The product must be added to the value of the full degree given in the table, when the temperature of the wet-bulb is above the freezing point: it must be subtracted when the temperature is below the freezing point, and receives the sign —. This correction is too important to be neglected.

The second correction, less important, for the intermediate differences of the ther-

#### PSYCHROMETRICAL TABLES.

mometers, which are greater by one tenth than those indicated in the tables, is given in the horizontal column at the bottom of the page. It is constant and always subtractive.

### Examples of Calculation.

Difference of thermometers, or t-t'

Temperature of the wet-bulb thermometer,  $t' = 11^{\circ}.0$ .

We find, page 18, for t-t', fifth double column; and for t', first column,

The force of vapor in the air =  $9^{mm}$ .31.

Relative humidity,

Difference of thermometers, or t-t', = 7°.2.

Wet-bulb thermometer, or t',

We find, page 24, for t - t', = 7°.2, and  $t' = 17^{\circ}.0$ , force of vapor  $10^{\text{mm}}.02$ .

Additive correction for fraction  $0^{\circ}.9$ , or  $9 \times 0.09 = 0$ .81.

> Force of vapor in the air = 10 .83.

Relative humidity,

Difference of thermometers,  $t-t'=6^{\circ}.5$ .

Wet-bulb thermometer,  $t' = 23^{\circ}.6$ .

We find, page 23, for  $t'=23^{\circ}.0$ , and t-t', or difference,  $=6^{\circ}.4$ , force of vapor 16mm.94; applying immediately the correction found at the bottom of the page for one tenth more difference, or  $6^{\circ}.4 + 0.1 = 6^{\circ}.5$ , we have,

Force of vapor =  $16^{\text{mm}} \cdot .94 - 0.06$ , or

Additive correction for fraction 0.6 of the wet-bulb,  $6 \times 0.13 = 0$ .78.

> Force of vapor in the air = 17 .66.

Relative humidity,

The wet-bulb thermometer covered with ice.

Difference of thermometers,  $t-t'=2^{\circ}.8$ .

Wet-bulb thermometer (ice),  $t' = -8^{\circ}.5$ .

Page 17 gives for  $t-t'=2^{\circ}.8$ , and  $t'=-8^{\circ}.0$ , force of vapor =  $1^{\text{mm}}.0$ . Subtractive correction for fraction 0.5 of wet-bulb,  $5 \times 0.019 = -0$ .1.

Force of vapor in the air = 0

Relative humidity, 30.

#### II. PSYCHROMETRICAL TABLES.

Below the Freezing-Point; the Bulb covered with a Film of Ice.

		incern)		e t	t', Dif	ference of	Wet ar	nd Dry Bu	lb The	rmometer	8.		
Wet- Bulb Thermo- meter t'	Mean Vertical Differ-	0°.	0	0°.	.2	00.	4	0°.	6	00.	8	10	.0
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid ity.
0	Millim.	Millim.		Millim.		Millim.	- 18	Millim	- 2	Millim.		Millim.	
-35	0.003	0.22	100	0.12	53	61	W.	-1111		V1.003		Major 9	4.5
-34	0.003	0.25	100	0.15	58	0.05	18	2.12.3		1000			14
-33	0.003	0.27	100	0.17	62	0.07	26		20			117 13	1500
-32	0.003	0.30	100	0.20	66	0.10	33	1	11/1			100	me
-31		0.34	100	0.24	69	0.14	39	0.03	10				100
-30	0.004	0.00	100	0.00	m's	0	4.	0.00	1-			1 2 1	Bl-
100000	0.004	0.37		0.27	71	0.17	44	0.07	17	A STATE OF	7.7	100	
-29	0.004	0.41	100	0.31	74	0.21	46	0.11	25	00.	1		
-28	0.004	0.45	100	0.35	76	0.25	53	0.15	31	0.04	9	TO SE	
-27	0.005	0.49	100	0.39	78	0.29	57	0.19	36	0.09	17		
-26		0.54	100	0.44	80	0.34	60	0.24	41	0.13	23	0.03	6
0.5	0.005	0 *0	100	0.10			-	0.00					200
-25	0.005	0.59	100	0.49	81	0.39	63	0.29	46	0.18	29	0.08	12
-24	0.006	0.64	100	0.54	82	0.44	66	0.34	50	0.24	34	0.14	19
-23	0.006	0.70	100	0.60	84	0.50	69	0.40	53	0.30	39	0.19	25
-22	0.007	0.77	100	0.67	85	0.56	71	0.46	57	0.36	44	0.26	31
-21	0.001	0.84	100	0.74	86	0.63	73	0.53	60	0.43	48	0.33	36
Man Fi	0.008	911	10			13 37				1		7 3	
-20	0.008	0.91	100	0.81	87	0.71	75	0.61	63	0.50	51	0.40	40
-19	0.008	0.99	100	0.89	88	0.79	77	0.69	66	0.58	55	0.48	45
-18	0.009	1.08	100	0.98	89	0.87	78	0.77	68	0.67	58	0.57	48
-17	0.009	1.17	100	1.07	90	0.97	80	0.87	70	0.76	61	0.66	52
-16	0.010	1.27	100	1.17	90	1.07	81	1.97	72	0.86	63	0.76	55
	0.011			1013		110				The LUCK		-120	
-15	0.012	1.38	100	1.28	91	1.18	82	1.08	74	0.97	66	0.87	58
-14	0.012	1.50	100	1.40	92	1.30	83	1.19	76	1.09	68	0.99	61
-13	0.013	1.63	100	1.53	92	1.42	84	1.32	77	1.22	70	1.11	63
-12	0.014	1.77	100	1.66	93	1.56	85	1.46	78	1.35	71	1.25	65
-11	0.015	1.92	100	1.81	93	1.71	86	1.61	80	1.50	73	1.40	67
10	0.016	F P DE										1	
-10	1	2.08	100	1.97	94	1.87	87	1.77	81	1.66	75	1.56	69
- 9	0.019	2.26	100	2.16	94	2.05	88	1.95	82	1.85	76	1.74	71
-8	0.021	2.46	100	2.35	94	2.25	89	2.14	83	2.04	78	1.94	73
- 7	0.023	2.67	100	2.56	94	2.46	89	2.35	84	2.25	79	2.15	74
- 6	0.024	2.89	100	2.79	95	2.68	90	2.58	85	2.47	80	2.37	76
	0.025	By 8	46	02	1	818	130			de la	73	0.7	
- 5	Marie Co	3.13	100	3.03	95	2.92	90	2.82	86	2.71	81	2.61	77
- 4	0.028	3.39	100	3.28	95	3.18	91	3.07	87	2.97	82	2.86	78
- 3	0.029	3.66	100	3.56	96	3.45	92	3.35	87	3.24	83	3.14	79
- 2	0.031	3.96	100	3.85	96	3.75	92	3.64	88	3.54	84	3.43	80
-1	0.033	4.27	100	4.16	96	4.06	92	3.95	89	3.85	85	3.74	81
-0	0.034	4.60	100	4.50	96	4.40	93	4.29	89	4.19	86	4.08	82

#### PSYCHROMETRICAL TABLES.

Below the Freezing-Point; the Bulb covered with a Film of Ice.

11	MAX BLOO		,01011 01	- Trouble	8-1011		10 0016	ered with	« ZIIII	01 100.			
Wet-		A 1916=1		to t-	- t', Dii	ference of	f Wet a	nd Dry B	ulb The	ermomete	ers.		
Bulb Thermo- meter,	Mean Vertical Differ- ence for	10	.2	10.	4	10	.6	10	8	20	.0	20	.2
Centigrade Degrees.	each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.						
0	Millim.	Millim.		Millim.	Paul 3	Millim.		Millim.	a o	Millim.		Millim.	
-35 -34				III and		2 100	0 0			1 1 10	. 6	NE F	
-33		BIT SI				2 01		- 150	0 1 6	0 00	8	10.4	
-32			1	1 100	0 4	1 1 60	W   1	1 12	0 10	12 19	0.1	-	13-
-31		14								y way		PART	
-30					W I				THE R			WE !	UNS-
-30 -29	a Video	17		81			1 8	2 1 Au	90 0	0 2 22 0 6 20		41	
-28		2 . 00	0 1	6 VI	9 -1		- 1		9 1 6	0 10	014		150
-27	0.0	W 1 14	3	s. 12	1	1 19	0 1 1	2 1 27	4-10	1 , 10	0 1 9	12-12	00
-26					313							in the	
-25				113	7 1 3	4 1 50		5 5 5 5	219	1 19	31	4.1	
-24	Second 1	0.04	5			274-67	311	o F GR	2 1	1 1 1	314	0.1	140
-23	0.006	0.09	12	a 1 14	91	2 87			11		. 1	919.3	
-22	0.006	0.16	18	0.05	6	E 68	6 -1		0			Marie I	970 C
-21	0.007	0.23	24	0.12	13						1	50 to	
90	0-007	0.00	0 1	0.00	10	0.00	0 1	I I	0 0	4 LIG	0		
-20 -19	0.008	0.30	30	0.20	18 25	0.09	9 15	0.07	6	1 7 80	ATT 10	100	
-18	0.008	0.46	39	0.28	30	0.17	21	0.07	13	0.05	4		
-17	0.009	0.56	43	0.46	35	0.25	26	0.25	18	0.15	11	0.04	3
-16	0.010	0.66	47	0.56	39	0.45	31	0.35	24	0.25	16	0.14	9
ng se in	0.011		0 5	e 1 an					1 19	1			1
-15	0.013	0.77	50	0.66	43	0.56	36	0.46	29	0.36	22	0.25	15
-14 -13	0.013	0.88	53 56	0.78	46 50	0.68	40	0.58	33	0.47	27	0.37	21 25
-12	0.015	1.15	59	1.04	53	0.94	47	0.70	41	0.00	35	0.63	30
-11	0.017	1.30	61	1.19	55	1.09	50	0.99	44	0.88	39	0.78	34
	0.018	e 254			. 1	Marie 1	. 2.				14	DEAD.	1117
-10	0.019	1.46	63	1.35	58	1.25	52	1.15	47	1.04	42	0.94	38
- 9 - 8	0.021	1.64	66	1.53	61	1.43	56	1.33	51	1.22	46	1.12	41 45
-8	0.023	1.83	68	1.73	63 65	1.62	58 61	1.52	54 56	1.42	49 52	1.31	48
-6	0.024	2.26	71	2.16	67	2.06	63	1.73	59	1.85	55	1.74	51
	0.025					2.00		1.50		1.50		Egen de	
- 5	0.028	2.50	73	2.40	69	2.30	65	2.19	61	2.09	57	1.98	53
- 4	0.029	2.76	74	2.65	70	2.55	67	2.45	63	2.34	59	2.24	55
- 2 - 2	0.030	3.03	75	2.93	72	2.82	68	2.72	65	2.61	61	2.51	58 60
-1	0.031	3.33	77 78	3.22	73 75	3.12	70 71	3.01	66	3.22	63 65	3.11	62
100	ma-	9.04	10	0.00	15	3.43	/1	3.32	05	3.22	05	0.11	02
	-		- 1	1					200	1			

#### PSYCHROMETRICAL TABLES.

Below the Freezing-Point; the Bulb covered with a Film of Ice.

Wet-				t-	- t', Dif	ference of	Wet a	nd Dry Bu	ılb The	rmomete	rs.		
Bulb Thermo- meter t	Mean Vertical Differ- ence for	2°.	.4	20	.6	20.	.8	30	.0	3°	.2	30	.4
Centi- grade	each 0°.1.	解門	Rela-		Rela-		Rela-	The day	Rela-	1610 (LV.)	Rela-		Rela
Degrees.		Force of	tive Hu-	Force of	tive Hu-	Force of	Hu-	Force of	tive Hu-	Force of	tive Hu-	Force of	tive Hu-
	Section 1	Vapor.	mid- ity.	Vapor.	mid- ity.	Vapor.	mid- ity.	Vapor.	mid- ity.	Vapor.	mid- ity.	Vapor.	mid-
0	Millim.	Millim.		Millim.		Millim,		Millim.	1 3/8	Millim.		Millim.	199
-15		0.15	9	0.05	3	Maga		El fara				-61	-
-14	0.011	0.27	15	0.16	9	0.06	4	1 82.8			87	10.0	37
-13	0.013	0.39	20	0.29	14	0.19	9	0.08	4	1			
-12	0.013	0.53	25	0.42	19	0.32	14	0.22	10	0.11	5		
-11	0.015	0.68	29	0.57	24	0.47	19	0.36	15	0.26	10	0.16	6
	0.016			30.00		130						200	
-10	0.018	0.83	33	0.73	28	0.63	24	0.52	20	0.42	16	0.32	12
- 9	0.018	1.02	37	0.91	33	0.81	28	0.70	24	0.60	20	0.50	17
- 8	0.019	1.21	40	1.10	36	1.00	32	0.90	28	C.79	25	0.69	21
- 7	0.021	1.42	44	1.31	40	1.21	36	1.11	32	1.00	29	0.90	26
- 6	(1.022	1.64	47	1.54	43	1.43	40	1.33	36	1.22	33	1.12	30
Total I	0.024			ARY.							40 80	40 8	AV
- 5	0.025	1.88	50	1.77	46	1.67	43	1.57	40	1.46	36	1.36	33
4	0.023	2.13	52	2.03	49	1.92	46	1.82	43	1.71	40	1.61	37
- 3	0.027	2.40	.55	2.30	52	2.19	48	2.09	45	1.99	43	1.88	40
- 2	0.023	2.70	57	2.59	54	2.49	51	2.38	48	2.28	46	2.17	43
- 1	0.031	3.01	59	2.90	56	2.80	54	2.69	51	2.59	48	2.48	46
		tie kas	N/An	e lag		Line		The state of					
		30.	6	3°.	8	40.	0	40.	.2	40.	4	40.	6
		Millim.		Millim.		Millim.		Millim.	100	Millim.		Millim.	
7.0		PAIC		1 1 36		1 12/3		1563		Y			
-15	WALT T	1 10 10		MARKET						500	47	100	
-14		1 1 1 m	HI			1000					2 10	60	
-13	HELY !	3.433		e fight	-1	1 115	ALC:	7.50		13 25	504		
-12		0.05	2	36	1 1	400	AFT		2 .	9.	4		
-11	0.016	0.05	Z	0.5 000	al -	6205	Harri	The way	100	5	ing of		
-10	0.010	0.21	8	0.11	4	A No. 18		Sett, Se	3 245		130		
-10 - 9	0.018	0.21	13	0.11	9	0.19	6	0.08	3			418 5	
- 8	0.019	0.58	18	0.48	14	0.13	11	0.27	8	0.17	5	0.06	2
-7	0.021	0.79	22	0.48	19	0.59	16	0.48	13	0.38	10	0.27	7
- 6	0.022	1.01	26	0.03	23	0.81	20	0.70	17	0.60	15	0.49	12
	0.024	1.01		0.51			1 100	J 70 Cay	Ton	1 - 4 - 2 - 2	10		Kik
- 5	E-1550 4	1.25	30	1.15	27	1.04	24	0.94	22	0.83	19	0.73	16
- 4	0.025	1.50	34	1.40	31	1.30	28	1.19	26	1.09	23	0.98	20
- 3	0.027	1.78	37	1.67	34	1.57	32	1.46	29	1.36	27	1.25	24
- 2	0.029	2.07	40	1.96	37	1.86	35	1.75	33	1.65	30	1.54	28
-1	0.031	2.38	43	2.27	40	2.17	38	2.06	36	1.96	34	1.85	31
-		CATHOLIC PROPERTY.				C. C. Land				-			

Wet-		${f t}-{f t}'$ , Difference of Wet and Dry-Bulb Thermometers.											
Bulb Thermo- ineter.	Mean Vertical Differ-	0	.0	00.	2	0°.	4	<b>0</b> °.	6	0°.	8	10.	0
Centigrade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.						
0	Millim.	Millim.	(CIT)	Millim.		Millim		Millim.		Millim.		Millim.	
0	0.03	4.60	100	4.48	96	4.36	92	4.24	88	4.12	85	4.01	81
1	0.03	4.94	100	4.82	96	4.70	93	4.58	89	4.46	85	4.35	82
2	0.04	5.30	100	5.18	96	5:06	93	4.94	89	4.83	86	4.71	83
3	0.04	5.69	100	5.57	97	5.45	93	5.33	90	5.21	87	5.09	83
4	0.04	6.10	100	5.98	97	5.86	93	5.74	90	5.62	87	5.50	84
5		6.53	100	6.41	97	6.29	94	6.17	91	6.05	88	5.94	85
100	0.05			0.00	0	0.75		0.01	0.7	0 **	00	0.10	-
6	0.05	7.00	100	6.88	97	6.76	94	6.64	91	6.52 7.01	88	6.40	85
7 8	0.05	7.49	100	7.37	97	7.25	94	7.13	91 92	7.01	89 89	7.42	86
9	0.06	8.02	100		97	8.33	95	8.21	92	8.09	89	7.97	86
10	0.06	8.57 9.17	100	9.04	97	8.92	95	8.80	93	8.68	90	8.56	87
10	0.00	9.17	100	3.04	31	0.32	99	0.00	30	0.00	30	0.50	01
11	0.06	9.79	100	9.67	97	9.55	95	9.43	93	9.31	90	9.19	88
12	0.07	10.46	100	10.34	98	10.21	95	10.09	93	9.97	90	9.85	88
13	0.07	11.16	100	11.04	98	10.92	95	10.80	93	10.68	91	10.56	89
14	0.07	11.91	100	11.79	98	11.66	95	11.54	93	11.42	91	11.30	89
15	0.08	12.70	100	12.58	98	12.46	96	12.33	93	12.21	91	12.09	89
n John	0.08										1100		
16	Darright	13.54	100	13.41	98	13.29	96	13.17	94	13.05	92	12.93	90
17	0.09	14.42	100	14.30	98	14.18	96	14.05	94	13.93	92	13.81	90
18	0.09	15.36	100	15.23	98	15.11	96	14.99	94	14.87	92	14.75	90
19	0.10	16.35	100	16.22	98	16.10	96	15.98	94	15.86	92	15.73	91
20	0.10	17.39	100	17.27	98	17.15	96	17.02	94	16.90	92	16.78	91
	0.11	L. all	mag and	The last		The said				7.7			35.77
21	0.12	18.50	100	18.37	. 98	18.25	96	18.13	94	18.00	92	17.88	91
22	0.12	19.66	100	19.54	98	19.41	96	19.29	95	19.17	93	19.04	91
23	0.13	20.89	100	20.76	98	20.64	96	20.52	95	20.39	93	20.27	91
24	0.14	22.18	100	22.06	98	21.94	97	21.81	95	21.69	93	21.57	92
25	T BASE	23.55	100	23.43	98	23.30	97	23.18	95	23.05	93	22.93	92
90	0.14	04.00	100	04.00	00	94 -4	0=	04.00	0-	94 40	00	94.00	00
26 27	0.15	24.99	100	24.86	98	24.74	97	24.62	95	24.49 26.01	93 93	24.37 25.88	92 92
28	0.16	26.51 28.10	100	26.38	98 98	26.26 27.85	97 97	26.13 27.73	95 95	27.60	93	27.48	92
29	0.17	29.78	100	29.66	98	29.53	97	29.41	95	29.28	94	29.16	92
30	0.18	31.55	100	31.42	98	31.30	97	31.17	95	30.05	94	30.92	93
	0.19	31.00	100	01.47	00	91.90	"	31.11	00	30.00	0.1	50.02	00
31		33.40	100	33.28	98	33.15	97	33.03	96	32.90	94	32.78	93
32	0.20	35.36	100	35.23	99	35.11	97	34.98	96	34.86	94	34.73	93
33	0.21	37.41	100	37.28	99	37.16	98	37.03	96	36.91	94	36.78	93
34	0.22	39.56	100	39.43	99	39.31	98	39.18	96	39.06	94	38.93	93
35	0.23	41.83	100	41.70	99	41.58	98	41.45	96	41.33	95	41.20	93

W			$\mathbf{t}-\mathbf{t}$ , Difference of Wet and Dry-Bulb Thermometers.										
Wet- Bulb Thermo- meter.	Differ-	1°	.2	10.	4	1°.	6	1°.	8	2°.	0	2°.	2
Centi- grade Degrees	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
* 0	Millim.	Millim.	2	Millim.		Millim.		Millim.		Millim.		Millim.	
0	0.03	3.89	78	3.77	74	3.65	71	3.53	67	3.41	64	3.29	61
1	0.03	4.23	79	4.11	75	3.99	72	3.87	69	3.75	66	3.63	63
2	0.04	4.59	80	4.47	76	4.35	73	4.23	70	4.11	67	3.99	65
3	0.04	4.97	80	4.85	77	4.73	74	4.61	71	4.49	69	4.37	66
4	0.04	5.38	81	5.26	78	5.14	75	5.02	73	4.90	70	4.78	67
5		5.82	82	5.70	79	5.58	77	5.46	74	5.34	71	5.22	69
	0.05	6.00	00	0.10	00	001		F 00	_31	F 00	W0		
6	0.05	6.28	83 83	6.16	80	6.04	77	5.92	75	5.80	72	5.68	70
8	0.05	7.29	84	7.17	81	6.53 7.05	78 79	6.41	76 76	6.29 6.81	73	6.17	71 72
9	0.06	7.85	84	7.73	82	7.61	80	7.49	77	7.37	75	7.25	73
10	0.06	8.44	85	8.32	83	8.20	80	8.08	78	7.96	76	7.84	74
10	0.06	0.44	00	0.02	0.0	0.20	00	0.00	10	1.50	10	1.0-1	14
11		9.07	86	8.95	83	8.82	81	8.70	79	8.58	77	8.46	75
12	0.07	9.73	86	9.61	84	9.49	82	9.37	80	9.25	78	9.12	76
13	0.07	10.43	86	10.31	84	10.19	82	10.07	80	9.95	78	9.83	76
14	0.08	11.18	87	11.06	85	10.94	83	10.81	81	10.69	79	10.57	77
15	0.08	11.97	87	11.85	85	11.73	83	11.60	81	11.48	80	11.36	78
113 113	0.08	a kan	495	44.50		144.50			100	98.			
16	0.09	12.80	88	12.68	86	12.56	84	12.44	82	12.32	80	12.19	78
17	0.09	13.69	88	13.57	86	13.44	84	13.32	83	13.20	81	13.08	79
18	0.10	14.62	88	14.50	87	14.38	85	14.26	83	14.13	81	14.01	80
19	0.11	15.61	89	15.49	87	15.37	85	15.24	83	15.12	82	15.00	80
20		16.65	89	16.53	87	16.41	86	16.29	84	16.16	82	16.04	81
01	0.11		00	15 00	00		00				00		0.
21 22	0.12	17.76	89	17.63	88	17.51	86	17.39	84	17.27	83	17.14	81
23	0.12	18.92 20.15	90 90	18.80	88 88	18.67	86	18.55	85 85	18.43 19.65	83 83	18.30 19.53	82 82
24	0.13	21.44	90	21.32	88	21.20	87	21.07	85	20.95	84	20.82	82
25	0.14	22.81	90	22.68	89	22.56	87	22.44	86	22.31	84	22.19	83
	0.14	22.01	00	22.00	00	22.00	0.	22.11		22.01	0.	22.13	00
26	THE A	24.24	90	24.12	89	23.99	87	23.87	86	23.75	85	23.62	83
27	0.15	25.76	91	25.63	89	25.51	88	25.39	86	25.26	85	25.14	83
28	0.16	27.35	91	27.23	89	27.10	88	26.98	87	26.86	<b>§</b> 5	26.73	84
29	0.17	29.03	91	28.91	90	28.78	88	28.66	87	28.53	85	28.41	84
30		30.80	91	30.67	90	30.55	89	30.42	87	30.30	86	30.17	84
The I	0.19	PRINT	16	Wast.	199	Boure	No.			THE WAY	1	PR	
31	0.20	32.65	91	32.53	90	32.40	89	32.28	87	32.15	86	32.03	85
32	0.21	34.61	91	34.48	90	34.36	89	34.23	88	34.11	86	33.98	85
33	0.22	36.66	92	36.53	90	36.41	89	36.28	88	36.16	86	36.03	85
35	0.23	38.81	92 92	38.68	90	38.56 40.82	89	38.43	88 88	38.31	87	38.18	85
00		41.07	34	40.94	91	40.82	09	40.09	05	40.57	01	40.44	86

t - t', Difference of Wet and Dry-Bulb Thermometers. Wet-Mean Bulb Thermo Vertical 20.4 20.6 20.8 3°.0 30.2 30.4 meter. Differ-1 ence for Centi-Rela Rela. Rela-Rala Relagrade each 0º.1 Relative tive tive tive tive tive Degrees Force of Force of Force of Force of Force of Force of Hu-Humid-Hu-Hu-Hu-Vapor. Vapor. Vapor. Vapor. Vapor. Vapor. itv. mid mid midmidmidity. ity. itv. itv. itv. Millim. Willim Millim. Millim Millim. Millim. Millim 0 58 3.06 2.94 52 2.82 50 2.70 17 2.58 0 3.17 55 44 0.03 1 3.51 60 3.39 57 3.27 54 3.16 52 3.04 49 2.92 47 0.04 3.39 2 3.87 62 3.75 59 3.63 56 3.51 54 51 3.28 49 0.04 4.25 4.02 3 63 4.13 61 58 3.90 56 3.78 53 3.66 51 0.04 4 4.66 65 4.54 62 4.42 60 4.30 57 4.18 55 4.06 53 0.04 4.74 4.62 5 5.10 66 4.98 64 4.86 61 59 57 4.50 55 0.05 5.08 6 5.56 67 5.44 65 5.32 63 5.20 61 58 4.96 56 0.05 5.93 7 69 5.69 62 5.57 60 6.05 66 5.81 64 5.45 58 0.05 8 6.57 70 6.45 68 6.33 65 6.21 63 6.09 61 5.97 59 0.06 9 7.13 71 7.01 69 6.89 67 6.77 65 6.64 63 6.52 61 0.06 10 7.72 72 7.59 70 7.47 68 7.35 66 7.23 64 7.11 62 0.06 11 8.34 73 8.22 71 8.10 69 7.98 67 7.86 65 7.74 63 0.07 12 72 8.52 9.00 74 8.88 8.76 70 8.64 68 66 8.40 64 0.07 69 9.22 13 9.71 75 9.58 73 9.46 71 9.34 67 9.10 66 0.07 70 9.96 68 14 10.45 75 10.33 73 10.21 72 10.08 9.84 67 0.08 10.75 15 11.24 76 10.99 72 10.87 69 10.63 67 11.12 74 71 0.08 70 12.07 77 72 11.58 68 16 11.95 75 11.83 73 11.71 11.46 0.09 12.95 77 12.83 12.71 12.59 72 12.47 71 12.34 69 17 76 74 0.09 13.89 78 13.52 73 13.40 72 13.28 70 18 13.77 76 13.64 75 0.10 72 14.26 19 14.87 78 14.75 77 14.63 75 14.51 74 14.38 71 0.10 15.43 73 20 15.92 79 15.79 77 15.67 76 15.55 74 15.30 72 0.11 80 78 72 21 17.02 16.77 16.65 75 16.53 16.90 77 74 16,40 0.12 22 18.18 80 18.06 79 17.93 77 17.81 76 17.69 74 17.56 73 0.12 23 18.91 19.41 80 19.28 79 19.16 78 19.04 76 75 18.79 73 0.13 24 20.70 81 20.58 79 20.45 78 20.33 77 20.21 75 20.08 74 0:14 25 22.06 81 21.94 80 21.82 79 21.69 77 21.57 76 21.45 75 0.14 23.50 82 79 26 23.37 80 23.25 23.13 78 23,00 77 22.88 75 0.15 78 76 27 25.01 82 24.89 81 24.76 79 24.64 24.51 77 24.39 0.16 28 26.23 79 26.11 77 25.98 26.61 83 26.48 81 26.36 80 76 0.17 29 28.16 28.28 83 28.03 80 27.91 79 27.69 77 27.76 76 81 0.18 30 30.05 83 29.92 82 29.80 81 29.67 79 29.55 78 29.42 77 0.19 31 80 31.40 78 31.28 31.90 83 31.78 82 31.65 81 31.53 77 0.20 79 32 33.86 80 33.36 33.23 78 84 33.73 82 33.61 81 33.48 0.21 33 35.90 84 35.77 83 35.65 81 35.52 80 35.40 79 35.27 78 0.22 34 38.06 84 37.93 83 37.81 82 37.68 81 37.56 80 37.43 78 0.23 35 80 79 40.31 84 40.18 83 40.06 82 39.93 81 39.81 39.68

Wet-		$\mathbf{t}-\mathbf{t}'$ , Difference of Wet and Dry-Bulb Thermometers,												
Thermo- meter.	Mean Vertical Differ-	3°.6		<b>3</b> °.	8	<b>4</b> °.	0	<b>4</b> °.	2	<b>4</b> °.	4	<b>4</b> °.	6	
	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	
0	Millim.	Millim.		Millim.	1	Millim.		Millim.	707	Millim.		Millim.		
0	0.03	2.46	41	2.34	39	2.22	36	2.11	34	1.99	32	1.87	29	
1	0.03	2.80	44	2.68	42	2.56	39	2.44	37	2.32	35	2.20	32	
2	0.04	3.16	46	3.04	44	2.92	42	2.80	39	2.68	37	2.56	35	
3	0.04	3.54	49	3.42	46	3.30	44	3.18	42	3.06	40	2.94	38	
4	0.04	3.94	51	3.82	48	3.71	46	3.59	44	3.47	42	3.35	40	
5	<b>医医管室</b>	4.38	52	4.26	50	4.14	48	4.02	46	3.90	44	3.78	42	
	0.05											9		
6	0.05	4.84	54	4.72	52	4.60	50	4.48	48	4.36	46	4.24	44	
7	0.05	5.33	56	5.21	54	5.09	52	4.97	50	4.85	48	4.73	46	
8	0.06	5.85	57	5.73	56	5.61	54	5.49	52	5.37	50	5.25	48	
9	0.06	6.40	59	6.28	57	6.16	55	6.04	53	5.92	52	5.80	50	
10	0.00	6.99	60	6.87	58	6.75	57	6.63	55	6.51	53	6.39	52	
11	0.06	7.61	61	7.49	60	7.37	58	7.25	56	7.13	55	7.01	53	
12	0.07	8.28	62	8.15	61	8.03	59	7.91	58	7.79	56	7.67	55	
13	0.07	8.98	64	8.85	63	8.73	61	8.61	59	8.49	57	8.37	56	
14	0.07	9.72	65	9.60	63	9.48	62	9.35	60	9.23	59	9.11	57	
15	0.08	10.51	66	10.38	64	10.26	63	10.14	61	10.02	60	9.90	58	
-0	0.08	10.51	00	10.00	0.1	10.20	00	10.11	0.	20.02	00	0.00	00	
16		11.34	67	11.22	65	11.10	64	10.97	62	10.85	61	10.73	59	
17	0.09	12.22	68	12.10	67	11.98	65	11.85	63	11.73	62	11.61	61	
18	0.09	13.15	69	13.03	67	12.91	66	12.79	64	12.66	63	12.54	62	
19	0.10	14.14	69	14.02	68	13.89	66	13.77	65	13.65	64	13.53	62	
20	0.11	15.18	70	15.06	69	14.94	67	14,81	66	14.69	65	14.57	63	
	0.11						10	A CONTRACTOR OF THE PERSON OF						
21	0.12	16.28	71	16.16	69	16.04	68	15.91	67	15.79	65	15.67	64	
22	0.12	17.44	71	17.32	70	17.20	69	17.07	67	16.95	66	16.83	65	
23	0.12	18.67	72	18.54	71	18.42	69	18.30	68	18-17	67	18.05	66	
24	0.14	19.96	73	19.84	71	19.71	70	19.59	69	19.46	68	19.34	66	
25	ELECTION OF	21.32	73	21.20	72	21.07	71	20.95	70	20.83	68	20.70	67	
90	0.14	99		00.00	-	00.70		99.50	80	00.00	co	00.70		
26 27	0.15	22.75	74	22.63	73	22.50	71	22.38	70	22.26	69	22.13	68	
28	0.16	24.27	74	24.14	73	24.02	72	23.89	71	23.77	70	23.64	68	
29	0.17	25.86	75	25.73	74	25.61 27.29	72 73	25.48 27.16	71 72	25.36 27.04	70	25.24 26.91	69 70	
30	0.18	27.44	75 76	27.31 29.17	75	29.05	73	28.92	72	28.80	71	28.67	70	
00	0.19	23.30	.0	23.17	10	20.00	10	20.32	12	20.00	.1	20.07	.0	
31	E 111	31.15	76	31.03	75	30.90	74	30.78	73	30.65	72	30.53	71	
32	0.20	33.10	77	32.97	76	32.85	75	32.72	73	32.60	72	32.47	71	
33	0.21	35.15	77	35.02	76	34.90	75	34.77	74	34.65	73	34.52	72	
34	0.22	37.30	77	37.17	76	37.05	75	36.92	74	36.80	73	36.67	72	
35	0.23	39.56	78	39.43	77	39.31	76	39.18	74	39.06	73	38.93	72	
			2 1											

Wet-		$\mathbf{t}-\mathbf{t}'$ , Difference of Wet and Dry-Bulb Thermometers.											
Bulb Me Thermometer. Diff Centi-	Mean Vertical Differ-	4°.8		<b>5</b> °.	0	5°.	2	5°.	4	5°.	6	5°.	.8
	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.	Otali	Millim.	
0	0.03	1.75	27	1.63	25	1.51	23	1.39	21	1.27	19	1.15	17
1	0.04	2.08	30	1.97	28	1.85	26	1.73	24	1.61	22	1.49	20
2	0.04	2.44	33	2.32	31	2.20	29	2.08	27	1.96	25	1.85	23
3	0.04	2.82	36	2.70	34	2.58	32	2.46	30	2.34	28	2.22	26
4	0.04	3.23	38	3.11	36	2.99	34	2.87	33	2.75	31	2.63	29
5	0.04	3.66	40	3.54	39	3.42	37	3.30	35	3.18	33	3.06	32
	0.05	E LED G	115	Was will	1				L with		350	T. 35	
6	0.05	4.12	43	4.00	41	3.88	39	3.76	37	3.64	36	3.52	34
7	0.05	4.61	45	4.49	43	4.37	41	4.25	40	4.13	38	4.01	36
8	0.06	5.13	47	5.01	45	4.89	43	4.77	42	4.65	40	4.53	39
9	0.06	5.68	48	5.56	47	5.44	45	5.32	44	5.20	42	5.08	41
10	0.00	6.27	50	6.15	48	6.02	47	5.90	45	5.78	44	5.66	42
	0.06	2 Vans	A Roman	No.			4		100			50 E	35
11	0.07	6.89	52	6.77	50	6.65	49	6.53	47	6.40	46	6.28	44
. 12	0.07	7.55	53	7.43	52	7.31	50	7.18	49	7.06	47	6.94	46
13	0.07	8.25	55	8.13	53	8.01	52	7.88	50	7.76	49	7.64	47
14	0.08	8.99	56	8.87	54	8.75	53	8.62	51	8.50	50	8.38	49
15		9.78	57	9.65	55	9.53	54	9.41	53	9.29	51	9.17	50
	0.08	r Liver	Par	PANN		Contract l	1				110		
16	0.09	10.61	58	10.49	57	10.36	55	10.24	54	10.12	53	10.00	51
17	0.09	11.49	59	11.37	58	11.24	56	11.12	55	11.00	54	10.88	53
18	0.10	12.42	60	12.30	59	12.17	58	12.05	56	11.93	55	11.81	54
19	0.11	13.40	61	13.28	60	13.16	59	13.04	57	12.91	56	12.79	55
20	The same	14.44	62	14.32	61	14.20	60	14.08	58	13.95	57	13.83	56
200	0.11	100	The same			112307223	fam.		1000	1	100		1000
21	0.12	15.54	63	15.42	62	15.30	60	15.17	59	15.05	58	14.93	57
22	0.12	16.70	64	16.58	63	16.46	61	16.33	60	16.21	59	16.09	58
23	0.13	17.93	65	17.80	63	17.68	62	17.56	61	17.43	60	17.31	59
24	0.14	19.22	65	19.09	64	18.97	63	18.85	62	18.72	61	18.60	60
25	100	20.58	66	20.46	65	20.33	64	20.21	63	20.08	62	19.96	60
	0.14				40						00		
26	0.15	22.01	67	21.88	65	21.76	64	21.63	63	21.51	62	21.39	61
27	0.16	23.52	67	23.40	66	23.27	65	23.15	64	23.02	63	22.90	62
28	0.17	25.11	68	24.99	67	24.86	66	24.74	65	24.61	64	24.49	63
29	0.18	26.79	68	26.66	67	26.54	66	26.41	65	26.29	64	26.16	63
30	0.10	28.55	69	28.42	68	28.30	67	28.17	66	28.05	65	27.92	64
0.1	0.19	20.10		00.00	00	90.15	00	00.00	0=	00.00	cc	00.70	0=
31	0.20	30.40	70	30.28	69	30.15	68	30.03	67	29.90	66	29.78	65
32	0.21	32.35	70	32.22	69	32.10	68	31.97	67	31.85	66	31.72	65
33	0.22	34.40	71	34.27	70	34.15	69	34.02	68	33.90	67	33.77	66
34	0.23	36.55	71	36.42	70	36.30	69	36.17	68	36.05	67	35.92	66
35	14-16-1	38.80	71	38.68	70				124		80	RE S	

Wet- Bulb			$\mathbf{t}-\mathbf{t}'$ , Difference of Wet and Dry-Bulb Thermometers.											
Thermo- meter.	Mean Vertical Differ-	6°.0		6°.	2	<b>6</b> °.	4	<b>6</b> °.	6	6°.8		7°.0		
Centigrade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Rela- tive Hu- mid- ity.	
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.	7	Millim.		
0	0.03	1.04	15	0.92	13	0.80	11	0.68	9	0.56	8	0.44	6	
1	0.03	1.37	18	1.25	16	1.13	15	1.01	13	0.89	11	0.78	10	
2	0.04	1.73	22	1.61	20	1.49	18	1.37	16	1.25	15	1.13	13	
3	0.04	2.11	25	1.99	23	1.87	21	1.75	19	1.63	18	1.51	16	
4	0.04	2.51	28	2.39	26	2.27	24	2.15	23	2.03	21	1.91	19	
5	PRED	2.94	30	2.82	28	2.70	27	2.58	25	2.46	24	2.34	22	
	0.05	0.40	00	0.00	0.	0.70	90	2.04	90	0.00	00	0.00	0-	
6	0.05	3.40	33	3.28	31	3.16	29	3.04	28	2.92	26	2.80	25	
7 8	0.05	3.89	35 37	3.77 4.28	33 35	3.65 4.16	32	3.53	30	3.41 3.92	29 31	3.29	28 30	
9	0.06	4.96	39	4.84	38	4.71	36	4.59	35	4.47	33	4.35	32	
10	0.06	5.54	41	5.42	40	5.30	38	5.18	37	5.06	35	4.94	34	
10	0.06	0.04	41	0.42	40	0.50	90	0.10	0.	0.00	00	2.02	O.T.	
11	1 1 6	6.16	43	6.04	41	5.92	40	5.80	39	5.68	37	5.56	36	
12	0.07	6.82	44	6.70	43	6.58	42	6.46	41	6.34	39	6.22	38	
13	0.07	7.52	46	7.40	45	7.28	43	7.16	42	7.03	41	6.91	40	
14	0.07	8.26	47	8.14	46	8.02	45	7.90	44	7.77	43	7.65	41	
15	0.08	9.05	49	8.92	48	8.80	46	8.68	45	8.56	44	8.44	43	
	0.08	Jan.	Part of			- 1	100					50 11	and i	
16	0.09	9.88	50	9.75	49	9.63	48	9.51	47	9.39	45	9.27	44	
17	0.09	10.76	52	10.63	50	10.51	49	10.39	48	10.27	47	10.14	46	
18	0.10	11.69	53	11.56	51	11.44	50	11.32	49	11.20	48	11.07	47	
19	0.11	12.67	54	12.55	53	12.42	51	12.30	50	12.18	49	12.06	48	
20	0.11	13.71	55	13.58	54	13.46	53	13.34	52	13.22	50	13.09	49	
21	0.11	1401		14.00	-	1450		11.11	53	14.31	52	14.19	51	
22	0.12	14.81	56 57	14.68	55 56	14.56 15.72	54 55	14.44	54	15.47	53	15.35	51 52	
23	0.12	17.19	58	17.06	57	16.94	56	16.82	55	16.69	54	16.57	53	
24	0.13	18.48	59	18.35	58	18.23	56	18.11	55	17.98	54	17.86	53	
25	0.14	19.84	59	19.71	58	19.59	57	19.46	56	19.34	55	19.22	54	
	0.14	8 (9)								REH-		2		
26	0.15	21.26	60	21.14	59	21.01	58	20.89	57	20.77	56	20.64	55	
27	0.15	22.77	61	22.65	60	22.52	59	22.40	58	22.28	57	22.15	56	
28	0.10	24.36	62	24.24	61	24.11	60	23.99	59	23.86	58	23.74	57	
29	0.18	26.04	62	25.91	61	25.79	60	25.66	59	25.54	58	25.41	57	
30	WE T	27.80	63	27.67	62	27.55	61	27.42	60	27.30	59	27.17	58	
	0.19	20.05		20. 50	00	20.10	-	20.00	0.7	20.75	00	20.00		
31	0.20	29.65	64	29.53	63	29.40	62	29.28	61	29.15	60	29.03	59	
32	0.21	31.59	64	31.47	63	31.34	62	31.22	61	31.09	60	30.97	59	
33		33.64	65	33.51	64	33.39	63	33.26	62	33.14	61	33.01	60	
35	1 12		0.000								1			
-03														

				-CONTRACTOR									
Wet-		- wilker	- ixit	t-1	t', Diffe	erence of	Wet ar	d Dry-Bu	ilb The	rmometer	s.		
Bulb Thermo- meter.	Mean Vertical Differ-	70.2		7°.4 7°.6			70	8	8°.0		80	.2	
Centigrade Degrees.	grade each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim		Millim.		Millim.		Millim.	
0	0.03	0.32	4	0.20	3	0.09	1	Tax 6	100			100	1
1	0.03	0.66	8	0.54	7	0.42	5	0.30	4	0.18	2	0.06	- 1
2	0.04	1.01	12	0.89	10	0.77	9	0.65	7	0.53	6	0.41	4
3	0.04	1.39	15	1.27	13	1.15	12	1.03	11	0.91	9	0.79	8
4	0.04	1.79	18	1.67	16	1.55	15	1.43	14	1.31	13	1.19	11
5		2.22	21	2.10	19	1.98	18	1.86	17	1.74	16	1.62	14
6	0.05	2.78	24	2.66	23	2.44	21	2.32	20	2.20	18	2.08	17
7	0.05	3.16	26	3.04	25	2.92	24	2.80	22	2.68	21	2.56	20
8	0.05	3.68	29	3.56	27	3.44	26	3.32	25	3.20	24	3.08	22
9	0.06	4.23	31	4.11	30	3.99	28	3.87	27	3.75	26	3.63	25
10	0.06	4.82	33	4.70	32	4.57	30	4.45	29	4.33	28	4.21	27
1	0.06		1								11	10-11	
11		5.44	35	5.32	34	5.19	32	5.07	31	4.95	30	4.83	29
12	0.07	6.09	37	5.97	36	5.85	34	5.73	33	5.61	32	5.49	31
13	0.07	6.79	39	6.67	37	6.55	36	6.43	35	6.31	34	6.18	33
14	0.07	7.53	40	7.41	39	7.29	38	7.17	37	7.04	36	6.92	35
15	0.08	8.31	42	8.19	41	8.07	40	7.95	39	7.83	37	7.71	36
Control of	0.08	25.32	130					000			14	MARIE !	
16	0.09	9.14	43	9.02	42	8.90	41	8.78	40	8.66	39	8.53	38
17	0.09	10.02	45	9.90	44	9.78	43	9.66	42	9.53	40	9.41	39
18	0.10	10.95	46	10.83	45	10.71	44	10.58	43	10.46	42	10.34	41
19 20	0.10	11.93	47	11.81	46	11.69	45	11.56	44	11.44	43	11.32	42
20	0.11	12.97	48	12.85	47	12.72	46	12.60	45	12.48	44	12.36	43
21	0.11	14.07	50	13.94	49	13.82	48	13.70	47	13.58	46	13.45	45
22	0.12	15.22	51	15.10	50	14.98	49	14.85	48	14.73	47	14.61	46
23	0.12	16.45	52	16.32	51	16.20	50	16.08	49	15.95	48	15.83	47
24	0.13	17.73	52	17.61	52	17.49	51	17.36	50	17.24	49	17.12	48
25	0.14	19.09	53	18.97	52	18.85	52	18.72	51	18.60	50	18.47	49
	0.14		W. C									10 1	
26	0.15	20.52	54	20.39	53	20.27	52	20.14	51	20.02	51	19.90	50
27	0.15	22.03	55	21.90	54	21.78	53	21.65	52	21.53	51	21.41	51
28	0.17	23.61	55	23.49	54	23.36	53	23.24	53	23.11	52	22.99	51
29	0.18	25.29	56	25.16	55	25.04	54	24.91	54	24.79	53	24.66	52
30	0.19	27.05	57	26.92	56	26.80	55	26.67	55	26.55	54	26.42	53
31	453 1	28.90	58	28.78	57	28.65	56	28.53	55	28.40	55	28.27	54
32	0.20	30.85	59	30.72	58	30.60	57	30.47	56	30.35	56		
33		180	2.33	W. 180	18	19-13	12	in av	Fre	Tall 1		18	
34	3.3		136	7/19	20 3	4		70	- the		10	70.04	
35	SUL		13	AUS I	7			1		12.0	to		19
77 ESV E								2					

Wet-		ikesim(	emili e	t-t	', Diffe	rence of	Wet an	d Dry-Bu	lb <b>T</b> he	rmometers	1.		
Bulb Thermo- meter.	Mean Vertical Differ-	S°	.4	8°.	6	S°.	8	<b>9</b> °.	0	<b>9</b> °.	2	9°.	4
Centigrade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.	7 %	Millim.	
1					-								
2	0.04	0.30	3	0.18	2	0.06	1						
3	0.04	0.67	7	- 0.55	5	0.43	4	0.31	3	0.19	2	0.08	1
4	0.04	1.07	10	0.95	9	0.83	8	0.72	6	0.60	5	0.48	4
5		1.50	13	1.38	12	1.26	11	1.14	10	1.02	8	0.90	7
6	0.05	1.96	16	1.84	15	1.72	14	1.60	13	1.48	12	1.36	10
7	0.05	2.44	19	2.32	17	2.20	16	2.08	15	1.48	14	1.84	13
8	0.05	2.96	21	2.84	20	2.72	19	2.60	18	2.48	17	2.36	16
9	0.06	3.51	24	3.39	23	3.27	21	3.15	20	3.03	19	2.91	18
10	0.06	4.09	26	3.97	25	3.85	24	3.73	23	3.61	22	3.49	21
	0.06	The same		20.5	L.F		7.19					100	
11	0.07	4.71	28	4.59	.27	4.47	26	4.35	25	4.23	24	4.11	23
12	0.07	5.37	30	5.25	29	5.12	28	5.00	27	4.88	26	4.76	25
13	0.07	6.06	32	5.94	31	5.82	30	5.70	29	5.58	28	5.46	27
14 15	0.08	6.80 7.58	34 35	6.68 7.46	33 34	6.56 7.34	32 33	7.22	31	6.31 7.10	30	6.19	29 31
10	0.08	1.00	99	1.40	9.4	1.04	99	1.22	99	7.10	94	0.97	91
16	Second B	8.41	37	8.29	36	8.17	35	8.05	34	7.92	33	7.80	32
17	0.09	9.29	39	9.17	38	9.04	37	8.92	36	8.80	35	8.68	34
18	0.09	10.22	40	10.09	39	9.97	38	9.85	37	9.73	36	9.60	35
19	0.10	11.20	41	11.07	40	10.95	39	10.83	39	10.71	38	10.58	37
20		12.23	43	12.11	42	11.99	41	11.87	40	11.74	39	11.62	38
07	0.11		The Party		40	10.00		70.00					
21 22	0.12	13.33	44	13.21	43	13.08	42	12.96	41 42	12.84	40	12.71	40
23	0.12	14.48	45	14.36	44 45	14.24	43	14.12	42	13.99	41 42	13.87	41 42
24	0.13	16.99	47	16.87	46	16.75	45	16.62	44	16.50	44	16.37	43
25	0.14	18.35	48	18.22	47	18.10	46	17.98	45	17.86	45	17.73	44
	0.14			N. II			TELL			1	101	-	
26	0.15	19.77	49	19.65	48	19.52	47	19.40	46	19.27	46	19.15	45
27	0.16	21.28	50	21.16	49	21.03	48	20.91	47	20.78	47	20.66	46
28 29	0.17	22.86	51	22.74	50	22.61	49	22.49	48	22.36	47	22.24	47
30	0.18	24.54 26.30	51 52	24.41 26.17	51 51	24.29 26.05	50 51	24.16 25.92	49 50	24.04	48	23.91	47
90	0.19	20.30	02	20.17	91	20.00	91	23.92	50	23.80	49	25.67	48
31		28.16	53	28.03	52	27.91	51	27.78	51	9.00		用意	500
32		10000	FOR	U.S.				10-19-1		T. Y.	1	84	
33				4400			11	1			84	1	
34			Rad	5,4,9	10					104			1
35	BEWE		D. S.			UV TO	200		100	* 11 11	1.1	N. State	4

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0 06 mm.

Wet-		-Te-Spin	ilenves (2) ei	t-1	, Diffe	erence of	Wet an	d Dry-Bu	llb The	rmometer	s.		
Bulb Thermo- meter.	Mean Vertical Differ-	9	.6	9°.	8	100	.0	100	.2	100	.4	100	.6
Centi- grade Degrees.	ence for each 0° 1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.	2719	Millim.	
0					16								
1 2	SET IN		Phone .				11.0			1100	1		95
3		9				The Real	177		1000	1			
4		0.36	3	0.24	2	0.12	1					AN ASSESSMENT	
5	0.04	0.78	6	0.66	5	0.54	4	0.42	3	0.30	2	0.18	1
	0.05	101		1.10	_			0.00	-	0.00		0.00	
6	0.05	1.24	9	1.12	8	1.00	7 10	0.88	6 9	0.76 1.24	5	0.64	5
8	0.05	2.24	15	2.12	-14	2.00	13	1.88	12	1.76	11	1.64	10
9	0.06	2.79	17	2.66	16	2.54	16	2.42	15	2.30	14	2.18	13
10	0.06	3.37	20	3.25	19	3.13	18	3.00	17	2.88	16	2.76	15
	0.06										da	15-11-5	FIS
11	0.07	3.98	22 24	3.86 4.52	21 23	3.74	20 22	3.62 4.28	19 22	3.50 4.15	18 21	3.38 4.03	18 20
13	0.07	5.33	26	5.21	25	5.09	25	4.25	24	4.15	23	4.73	20
14	0.07	6.07	28	5.95	27	5.83	26	5.71	25	5.58	25	5.46	24
15	0.08	6.85	30	6.73	29	6.61	28	6.49	27	6.37	26	6.24	26
	0.08	THE STATE OF			11.5	4-					4-14	<b>33</b> 3 1 1 1 1	
16 17	0.09	7.68	31 33	7.56	31	7.44	30	7.31	29	7.19	28	7.07	27
18	0.09	8.56 9.48	35	9.36	32 34	8.31 9.24	31	8.19 9.11	31 32	8.07	30	7.94 8.87	29 30
19	0.10	10.46	36	10.34	35	10.22	34	10.09	33	9.97	33	9.85	32
20	0.11	11.50	37	11.37	36	11.25	36	11.13	35	11.01	34	10.88	33
	0.11										2 4	Louis I	
21	0.12	12.59	39	12.47	38	12.35	37	12.22	36	12.10	35	11.98	35
22 23	0.12	13.75	40	13.62	39	13.50 14.72	38 39	13.38 14.59	37	13.25	37	13.13 14.35	36
24	0.13	16.25	42	16.13	41	16.00	40	15.88	40	15.76	39	15.63	38
25	0.14	17.61	43	17.48	42	17.36	42	17.24	41	17.12	40	16.99	39
	0.14			'			N-11				Til		
26	0.15	19.02	44	18.90	43	18.78	42	18.65	42	18.53	41	18.40	40
27 28	0.16	20.54   22.12	45 46	20.41	44 45	20.29	43	20.16	43	20.04 21.62	42	19.91 21.50	41 42
29	0.17	23.79	47	23.66	46	23.54	44 45	23.41	44	23.29	44	23.16	43
30	0.18	25.55	48	25.42	47	25.30	46	SEP ST			2 4		10
07	0-4-1											5-1	
31 32		y 186	1	NE CO	AN	相談	86	NO.	194	7.00	17.5	7-48	
33		25		FOL					Very		3		
34	from the		11	LYSE!				Torquid		41-4	1		
35		190	131 6			1 - 5 - 1	2.0		1 . 49		1		

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.06 mm.

Wet-		7		t – t	', Diffe	rence of \	Vet an	d Dry-Bu	lb The	rmometers			
Bulb Thermo- meter.	Mean Vertical Differ-	10	°.8	110	.0	110	.2	110	.4	11°	.6	-11°	8
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor,	Relative Humid- ity.
0 1 2 3	Millim.	Millim.		Millim.	10 To	Millim.		Millim.		Millim.		Millim.	
5 6 7 8	0.05 0.05	0.52 1.00 1.52	4 7 9	0.40 0.88 1.40	3 6 9	0.28 0.76 1.27	2 5 8	0.16 0.64 1.15	1 4 7	0.52	3 6	0.40 0.91	2 5
9 10 11 12	0.06 0.06 0.06 0.07	2.06 2.64 3.26 3.91	12 14 17	1.94 2.52 3.14 3.79	11 14 16 18	1.82 2.40 3.02 3.67	10 13 15 17	1.70 2.28 2.90 3.55	10 12 14 17	1.58 2.16 2.77 3.43	9 11 14 16	1.46 2.04 2.65 3.31	8 11 13 15
13 14 15	0.07 0.07 0.08 0.08	4.61 5.34 6.12	21 23 25	4.49 5.22 6.00	20 22 24	4.36 5.10 5.88	19 21 23	4.24 4.98 5.76	19 21 22	4.12 4.86 5.63	18 20 22	4.00 4.73 5.51	17 19 21
16 17 18 19 20	0.09 0.09 0.10 0.10	6.95 7.82 8.75 9.73 10.76	27 28 29 31 33	6.83 7.70 8.63 9.60 10.64	26 27 29 30 32	6.70 7.58 8.50 9.48 10.51	25 27 28 30 31	6.58 7.46 8.38 9.36 10.39	24 26 27 29 30	6.46 7.33 8.26 9.24 10.27	23 25 27 28 30	6.34 7.21 8.14 9.11 10.15	22 24 26 28 29
21 22 23 24	0.11 0.12 0.12 0.13 0.14	11.85 13.01 14.22 15.51	34 35 36 38	11.73 12.88 14.10 15.39	33 34 36 37	11.61 12.76 13.98 15.27	32 34 35 36	11.48 12.64 13.85 15.15	32 33 34 35	11.36 12.51 13.73 15.02	31 32 34 35	11.24 12.39 13.61 14.90	30 32 33 34
25 26 27 28 29	0.14 0.15 0.16 0.17	18.28 19.79 21.37 23.04	39 39 40 41 42	16.74 18.16 19.67 21.25 22.91	38 39 40 41 42	16.62 18.03 19.54 21.12	38 39 40	16.49 17.91 19.42 21.00	36 37 38 39	16.37 17.78 19.29 20.87	36 37 38 39	16.24 17.66 19.17 20.75	35 36 37 38
30 31 32 33			18 kg		新 · 新 · 新 · 新 · 新 · · · · · · · · · · ·								
34 35													

Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.06$  mm.

		440157		t-t	, Diffe	rence of	Wet an	d Dry-Bu	lb <b>T</b> he	rmometer	3.		
Wet- Bulb Thermo- meter.	Mean Vertical Differ-	12	20.0	120	.2	12	.4	120	.6	12	.8	130	.0
Centigrade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
12	0.07	3.19	14	3.06	14	2.94	13	2.82	12	2.70	12	2.58	11
13	0.07	3.88	16	3.76	16	3.64	15	3.51	14	3.39	14	3.27	13
14	0.08	4.61	18	4.49	18	4.37	17	4.25	16	4.13	16	4.00	15
15	0.08	5.39	20	5.27	20	5.15	19	5.03	18	4.90	18	4.78	17
16	330	6.22	22	6.09	21	5.97	21	5.85	20	5.73	19	5.61	19
	0.09	- 00		0.0-	-		-						Ser
17	0.09	7.09	24	6.97	23	6.84	22	6.72	22	6.60	21	6.48	21
18	0.10	8.01	25 27	7.89	25 26	7.77	24 26	7.65	23 25	7.52	23	7.40	22
19 20	0.10	10.02	28	10.90	28	8.74	26	8.62	26	8.50	25	8.38	24
21	0.11	11.12	30	10.99	29	9.78	28	9.65	28	9.53	26	9.41	25 27
21	0.12	11.12	90	10.33	49	10.07	40	10.75	40	10.02	21	10.50	21
22	Bold B	12.27	31	12.14	30	12.02	30	11.90	29	11.77	28	11.65	28
23	0.12	13.48	32	13.36	31	13.23	31	13.11	30	12.99	29	12.86	29
24	0.13	14.78	33	14.65	33	14.53	32	14.40	31	14.28	31	14.16	30
25	0.14	16.11	35	15.99	34	15.87	33	15.74	33	15.62	32	15.50	31
26	0.14	17.54	36	17.42	35	17.29	34	17.17	34	17.04	33	16.92	33
PAGE	0.15	18 also	1	ALCOHOLD IN	9.0	Sales (	401	00000	200	ler a			
27	0.10	19.04	37	18.92	36	18.80	35	18.67	35	18.55	34	18.42	34
28	0.16	20.63	38	100.5	1,6	Alta I	40	113	7	" Ka	46		
			00	100	118								11
		13.	0,2	13°.	4	13°	.6	13°.	8	14°.	0		
	14	Millim.	Cock	Millim.	The last	Millim.	100	Millim.	1111	Millim.		Millim.	
12		2.46	10	2.34	10	2.22	9	2.09	8	1.97	8		
13	0.07	3.15	12	3.03	12	2.91	11	2.79	11	2.66	10	60 G L	
14	0.07	3.88	14	3.76	14	3.64	13	3.52	13	3.40	12	10.1	
15	0.08	4.66	16	4.54	16	4.42	15	4.29	15	4.17	14	W. P.	
16	0.08	5.48	18	5.36	18	5.24	17	5.12	16	5.00	16		
	0.09	4.0									Ties	0	
17	0.00	6.36	20	6.23	19	6.11	19	5.99	18	5.87	17	Tank Sa	
18	0.09	7.28	22	7.16	21	7.03	20	6.91	20	6.79	19		
19	0.10	8.25	23	8.13	22	8.01	22	7.89	21	7.76	21	PA-11	
20	0.10	9.29	25	9.16	24	9.04	23	8.92	23	8.80	22		
21		10.38	26	10.25	25	10.13	25	10.01	24	9.89	24		
	0.12			12 30			1			1		100	
22	0.12	11.53	27	11.40	27	11.28	26	11.16	26	11.03	25		Busi
23	0.13	12.74	28	12.62	28	12.49	27	12.37	27	12.25	26	500	233
24	0.14	14.02	30	13.90	29	13.77	29	13.65	28	13.53	27		The state of
25	0.14	15.37	31 32	15.25	30	15.12	30	15.00	29	14.88	29		NA J
26		16.80	52	16.67	51	16.55	31	16.42	30	16.30	30	0.0	94

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.06 mm.

Correction for the Barometrical Height.

	etrical					D	ifferen	ce of T	Thermo	meters	t — t'.				
Height	DEIOW.	10	20	30	40	50	60	70	80	90	10°	110	120	13°	14°
Add.	Subtr'ct.		-					147					-	10	
				21		v	Vet-Bu	lb abov	e the l	Freezin	g Point.		Will		
	941.4		PART				117	31 3			WHEN THE		127	X1917 11	M. G.
Millim.	Millim.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.
755	755	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
750	760	0.00	0.01	0.01	0.02	0.02	7 / 10	0.03	0.03	0.04	0.04	0.04	0.05	0.05	0.06
745	765	0.01	0.02	0.02	0.03	0.04	0.05	0.06	0.06	0.07	0.08	0.09	0.10	0.10	0.11
740	770	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.10	0.11	0.12	0.13	0.14	0.16	0.17
735	775	0.02	0.03	0.05	0.06	0.08	0.10	0.11	0.13	0.14	0.16	0.18	0.19	0.21	0.22
		0.00	0.04	0.06	0.08	0.10	0.12	0.14	0.16	0.10	0.20	0.22	0.24	0.26	0.28
730	780	0.02	0.04	0.06	0.08	0.10	0.12	0.14	0.16	0.18	0.24	0.26	0.24	0.20	0.28
725	785 790	0.02	0.06	0.08	0.11		0.17	0.20	0.13	0.25	0.28	0.31	0.34	0.36	0.39
720	795	0.03	0.06	0.10	0.13	0.16	0.19	0.22	0.26	0.29	0.32	0.35	0.38	0.42	0.45
710	800	0.04	0.07	0.11	177		0.22	0.25	0.29	0.32	0.36	0.40	0.43	0.47	0.50
110	000		200						40		of the	- Control		185	THRU.
700	66	0.04	0.09	0.13	0.18	0.22	0.26	0.31	0.35	0.40	0.44	0.48	0.53	0.57	0.62
690	66	0.05	0.10	0.16	0.21	0.26	0.31	0.36	0.42	0.47	0.52	0.57	0.62	0.68	0.73
680	66	0.06	0.12	0.18	0.24	0.30	0.36	0.42	0.48	0.54	0.60	0.66	0.72	0.78	0.84
670	66	0.07	0.14	0.20	0.27	0.34	0.41	0.48	0.54	0.61	0.68	0.75	0.82	0.88	0.95
660	66	0.08	0.15	0.23	0.30	0.38	0.46	0.53	0.61	0.68	0.76	0.84	0.91	0.99	1.06
15.118			S.				. 7						4.0	100	1000
650	66	0.08	0.17	0.25	0.34	0.42	0.50	0.59	0.67	0.76	0.84	0.92	1.01	1.09	1.18
		H. F. N			PESE	_		211	18	- Var			0.44		
No.	D. Sell-			ulb bel			NAME OF THE OWNER, OWNE								996
8/80	ellings.	100	Fiee	Zing I	OIII C.		1	70.	V A 3.0	DIT	OF C	TATO	ULAT	TON	112316
	102 3			0.00	0.00		70,	E.	AAM	LLL	OF (	ALC	ULAI	ION.	SHEET OF
755	755	0.00	the walls	0.00	A SHALL I	0.00	1		Wet	-bulb a	bove the	Freezi	ng Point	100	his b
750	760	0.00		0.01	0.01	0.02	114	t'=1	700	+	-t' =	80 2	h -	= 710m	m.
745	765	0.01	0.01	0.02	0.03	0.04	-						aromet	1	mm.
735	775	0.01	The state of		- F 7 3	0.07			55mm.	-	ce of				9.41
100							1	0					and 8°		0.30
730	780	0.02	0.04	0.05	0.07	0.09	Marie &		erigi.	Tam	26 -			1	0.77
725	785	0.02	0.04	0.06	0.08	0.11	AUG KO			r orce	of va	por	The last	1000	9.71
720	790	0.02	0.05	0.07	0.10	0.12	Gara								H450 7
715	795	0.03		1	Te - 12 2 2 2	0.14		The	mean	baro	metrica	al pres	sure, a	t a g	iven
710	800	0.03	0.06	0.09	0.13	0.16							o make		
700	66	0.04	0.08	0.12	0.15	0.19							st table		
690	66			0.14			100						number		
680	66			0.16									This		
670	66			0.18			1	M 10				C. 10/2   BCC)	, or the		
660	66	0.07	0.13	0.20	0.27	0.33							the de		
Tay I			-		18161		wl						ipon th		
650	66	0.07	0.15	0.22	0.29	0.36			esults						. 4
D	1	1	1		1		1	00	-						

## III.

## TABLE

GIVING AT SIGHT THE RELATIVE HUMIDITY DEDUCED FROM THE INDICA-

By M. T. HAEGHENS.

This table, which has been published in the Annuaire Météorologique de France for 1850, page 86, and following, has been calculated by Mr. Haeghens, using Regnault's Tables of Elastic Forces of Vapor. It gives directly the relative humidity, when the hygrometrical observations have been made by means of dew point instruments like those of Daniell, Regnault, Bache, and others.

These hygrometers are destined to find out the temperature of the dew point, that is the temperature to which it would be necessary to lower the temperature of the air, in order that this air be completely saturated by the aqueous vapor which it contained at the time of the observation.

The force of vapor contained in the air, or its absolute humidity, is thus the maximum of force of vapor which corresponds to the temperature of the dew point; it is given directly in the Table I. of the Elastic Forces of Vapor, by Regnault.

The ratio of that maximum of force of vapor at the temperature of the dew point to the force of vapor which corresponds, in the same table, to the temperature of the surrounding air at the time of the observation, is the *relative humidity*. This ratio is given in hundredths in the following table, which relieves the observer of the trouble of calculating it.

Let t = temperature of the air surrounding the instrument.

t' = temperature of the dew point.

t-t'= the difference between these two temperatures.

The first column, on the left, contains the temperature of the air t, in centigrade degrees. The following ones, headed with the differences, t-t', between the temperatures of the air and of the dew point, give the relative humidity corresponding to the two elements.

Temp. of the Air = t. Dew point = t. Difference t - t. Relative Humidity. Example: 10°.0 4°.4 5°.6 68

Should the temperature of the air t', or the difference t-t', fall between the numbers found in the columns, it is obvious, by glancing at the table, that an interpolation at sight will always be easy.

B

Temper-	2016	- Urasi		+/ T	)iffaran	ea of T	amnara	tures of	the D	ow Poi	nt and	of the	Air		
Temper- ature of the air.	00.0	00.0							- 10				1	1 00 0	00.0
t=	0°.0	0°.2	0°.4	0°.6	0°.8	1°.0	1°.2	1°.4	1°.6	1°.8	2°.0	2°.2	2°.4	2°.6	2°.8
Centig.	100	98	97	95	94	92	90	89	88	86	85	83	82	80	79
-8 -7	100	98	97	95	94	92	91	89	88	86	85	83	82	81	79
-6	100	98	97	95	94	92	91	89	88	87	85	84	82	81	80
-5	100	98	97	95	94	92	91	89	88	87	85	84	82	81	80
-4	100	98	97	95	94	92	91	89	88	87	85	84	83	81	80
-3	100	98	97	95	94	92	91	90	88	87	85	84	83	81	80
-2	100	98	97	95	94	93	91	90	88	87	86	84	83	82	80
-1	100	98	97	95	94	93	91	90	89	87	86	85	83	82	81
0	100	98	97	96	94	93	91	90	89	87	86	85	83	82	81
+1	100	99	97	96	95	93	92	90	89	88	86	85	84	83	81
2	100	99	97	96	95	93	92	91	89	88	87	85	84	83	82
3	100	99	97	96	95	93	92	91	89	88	87	86	84	83	82
4	100	99	97	96	95	93	92	91	89	88	87	86	85	83	82
5	100	99	97	96	95	93	92	91	90	88	87	86	85	83	82
6	100	99	97	96	95	93	92	91	90	88	87	86	85	84	82
7	100	99	97	96	95	93	92	91	90	89	87	86	85	84	83
8	100	99	97	96	95	93	92	91	90	89	87	86	85	84	83
9	100	99	97	96	95	94	92	91	90	89	87	86	85	84	83 83
10	100	99	97	96	95	94	92	91	90	89	87	86	85	84	18
11	100	99	97	96	95	94	92	91	90	89	87	86	85	84	83
12	100	99	97	96	95	94	92	91	90	89	88	87	85	84	83
13	100	99	97 98	96	95	94	92	91	90	89 89	88	87	85 86	84	83
14 15	100	99	98	96 96	95 95	94 94	93	91 91	90	89	88	87	86	84	83
1	allu B			E.W.S.	and it	10000		L. Keit	12.00	the State		TAGAL.	and.	12.2	283
16	100	99	98	96	95	94	93	91	90	89	88	87	86	85 85	84 84
17	100	99	98 98	96 96	95 95	94	93 93	91 92	90	89 89	88 88	87	86	85	84
19	100	99	98	96	95	94	93	92	91	89	88	87	86	85	84
20	100	99	98	96	95	94	93	92	91	89	88	87	86	85	84
21	100	99	98	96	95	94	93	92	91	90	88	87	86	85	84
22	100	99	98	96	95	94	93	92	91	90	89	87	86	85	84
23	100	99	98	96	95	94	93	92	91	90	89	88	86	85	84
24	100	99	98	97	95	94	93	92	91	90	89	88	87	85	84
25	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85
26	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85
27	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85
28	100	99	93	97	95	94	93	92	91	90	89	88	87	86	85
29	100	99	98	97	96	94 94	93	92	91	90	89 89	88	87	86	85 85
31	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
32	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
33	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
34	100	99	98	97	96	95	93	92	91	90	89	88	87	86	85
35	100	99	98	97	96	95	93	92	91	90	89	88	87	86	85
														<u> </u>	-

Temper-			t	t' = I	Differen	ce of T	'empera	tures of	the D	ew Poi	nt and	of the	Air.		
ature of tne air.	20.0							1							
t=	3°.0	3°.2	3.°4	3°.6	3°.8	4°.0	4°.2	4°.4	4°.6	4°.8	5°.0	5°.2	5°.4	5°.6	5°.8
Centig.	78	77	75	74	73	72	71	69	68	67	66	65	64	63	62
-7	78	77	75	74	73	72	71	69	68	67	66	65	64	63	62
-6	78	77	76	74	73	72	71	69	68	67	66	65	64	63	62
-5	79	77	76	75	73	72	71	70	68	67	66	65	64	63	62
-4	79	77	76	75	74	73	71	70	69	68	67	66	64	63	62
-3	79	77	76	75	74	73	72	70	69	68	67	66	65	64	63
-2	79	78	77	76	74	73	72	71	70	69	68	66	65	64	63
-1	79	78	77	76	75	73	72	71	70	69	68	67	66	65	64
0	80	78	77	76	75	74	73	71	70	69	68	67	66	65	64
+1	80	79	78	77	75	74	73	72	71	70	69	68	66	65	64
2	81	79	78	77	76	75	74	72	71	70	69	68	67	66	65
3	81	80	78	77	76	75	74	73	72	71	70	69	68	66	65
4	81	80	79	78	77	75	74	73	72	71	70	69	68	67	66
5	81	80	79	78	77	76	75	73	72	71	70	69	68	67	66
6	81	80	79	78	77	76	75	74	73	72	71	70	69	68	67
7	81	80	79	78	77	76	75	74	73	72	71	70	69	68	67
8	81	80	79	78	77	76	75	74	73	72	71	70	69	68	67
8	82	80	79	78	77	76	75	74	73	72	71	70	69	68	67
10	82	81	80	78	77	76	75	74	73	72	71	70	69	68	67
11	82	81	80	79	78	76	75	74	73	72	71	70	70	69	68
12	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
13	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
14	82	81	80	79	78 78	77	76	75	74	73	72	71	70	69	68
15	82	81	17,24	9 50 1					100	1	72		70		68
16	.82	81	80	79	78	77	76	75	74	73	72	71	71	70	69
17	83	81	80	79	78	77	76	75	74	73	73	72	71	70	69
18	83	82 82	81	80	79	78 78	77	76	75	74	73 73	72	71	70	69
19 20	83	82	81	80	79	78	77	76	75	74	73	72	71	70	69
						1.00		15	1						
21 22	83	82 82	81	80	79	78 78	77	76	75	74	73 73	72 73	71 72	70 71	70
23	83	82	81	80	79	78	77	76	75	74	74	73	72	71	70
24	83	82	81	80	79	78	77	77	76	75	74	73	72	71	70
25	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70
26	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70
27	84	83	82	81	80	79	78	77	76	75	74	73	72	71	-70
28	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70
29	84	83	82	81	80	79	78	77	76	75	75	74	73	72	71
30	84	83	82	81	80	79	78	77	76	76	75	74	73	72	71
31	84	83	82	81	80	79	78	77	77	76	75	74	73	72	71
32	84	83	82	81	80	79	79	78	77	76	75	74	73	72	72
33	84	83	82	81	80	80	79	78	77	76	75	74	73	72	72
34	85 85	84	83	82 82	81	80	79	78	77	76	75	74 75	74	73	72 72
35	99	04	03	82	91	1 00	19	18	177	1 70	75	1 15	14	13	12

Teniper			t	- t' =	Differe	nce of 7	Гетрега	tures of	the De	w Poin	t and of	the Air			
the air.	6°0	6°.2	6°.4	6°.6	6°.8	7°.0	7°.2	7°.4	7°.6	7°.8	8°.0	8°.2	8°.4	8°.6	8°.8
t=	0 0	0 .2	0 .4	0.0	0.0	1.0	1 .2	1 .4	1.0	1.0	0 .0	0 .2	0 .4	0.0	0 .0
Centig	100			60, 10			7.40	FU		100		16.5			
-7			e e ch												- (C)
-6	61	60	59	58	57	56			5 (6)		Kar.	resign.			
-5	61	60	59	58	58	57	56	55	54	53	52				
-4	62	61	60	59	58	57	56	55	54	53	52	76	10 7		
-3	62	61	60	59	58	57	56	55	54	53	53	52	51	50	49
-2	62	61	60	60	59	58	57	56	55	54	53	52	51	50	49
-1	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49
0	63	62	61	60	59	58	57	56	55	54	53	53	52	51	50
+1	63	62	61	61	60	58	58	57	56	55	54	53	52	51	51
2	64	63	62	61	60	59	58	57	56	55	55	54	53	52	51
3	64	63	62	62	60	60	59	58	57	56	55	54	53	53	52
4	65	64	63	62	61	60	59	58	57	56	56	55	54	53	52
5	65	64	63	62	62	61	60	59	58	57	56	55	54	54	53
6	66	65	64	63	62	61	60	59	58	57	57	56	55	54	53
7	66	65	64	63	62	61	60	60	59	58	57	56	55	55	54
8	66	65	64	63	62	62	61	60	59	58	57	56	56	55	54
9	66	65	64	64	63	62	61	60	59	58	58	57	56	55	54
10	67	66	65	64	63	62	61	60	59	59	58	57	56	55	55
11	67	66	65	64	63	62	61	61	60	59	58	57	56	56	55
12	67	66	65	64	63	62	62	61	60	59	58	57	57	56	55
13	67	66	65	64	64	63	62	61	60	59	59	58	57	56	55
14	67	66	66	65	64	63	62	61	60	60	59	58 58	57 57	56 57	56 56
15	67	67	66	65	64	63	62	61	61	60	59	30			5.00
16	68	67	66	65	64	63	63	62	61	60	59	58	58	57	56
17	68	67	66	65	64	64	63	62	61	60	59	59	58	57	56
18	68	67	66	65	65	64	63	62	61	60	60	59 59	58 58	57 58	57 57
19 20	68	67	67	66	65 65	64 64	63	62 63	62 62	61 61	60	59	59	58	57
		345				0.4	03	100			100		1900		
21	69	68	67	66	65	64	64	63	62	61	60	60	59	58	57
22	69	68	67	66	65	65	64	63	62 62	61 62	61	60	59 59	58 59	58 58
23 24	69	68	67	67	66	65 65	64	63 63	63	62	61	60	60	59	58
25	69	69	68	67	66	65	64	64	63	62	61	61	60	59	58
												. 0	00		70
26 27	70	69	68	67	66	65	65	64	63 63	62	61 62	61	60	59 59	58 59
28	70	69	68	67	66	66 66	65 65	64	63	63	62	61	60	60	59
29	70	69	69	68	67	66	65	64	64	63	62	61	61	60	59
30	70	69	69	68	67	66	65	65	64	63	62	62	61	60	59
31	70	70	69	68	67	66	66	65	64	63	62	62	61	60	60
32	71	70	69	68	67	67	66	65	64	64	63	62	61	61	60
33	71	70	69	68	68	67	66	65	64	64	63	62	61	61	60
34	71	70	69	69	68	67	66	66	65	64	63	62	62	61	60
35	71	70	70	69	68	67	66	66	65	64	63	63	62	61	60

В

Temper- ature of			t —	<b>t'</b> = I	Differen	ce of T	empera	tures o	f the D	ew Poi	nt and	of the	Air.		
the air.	9°.0	9°.2	9°.4	9°.6	9°.8	10°.0	10°.2	10°.4	10°.6	10°.8	11°.0	11 2	11°.4	11°.6	11°.8
Centig.								0-0	13		129				11.37
-8 -7								MI-Y							
-6					133		120	1 1	9 6		182	41	WA T		S- 1
-5		900		5.1	and .		15	141	HE		-	9			4-1
-4								-1-1	11	34 %		Division			
-3			E I B			1		345	111	64		4.	m (		
-2		1 139	5114				T is		16				10		
-1		316	2111						73	7					
0								14 1		Vê j		17			118
+1	50				9		44 (	H .	4 6	10 -	lat i	JA 3			. 41
2	50	49	49	48	47	46	4.75		8	11.	SY S	-		1	Ass
3	51	50	49	48	48	47	46	45	45	44	43				1
4	51 52	51	50 50	49	48	47	47	46	45	44	44	43	42	42	41
5		51		49	49	48	47	46	46	45	44	43	43		41
6	52	52	51	50	49	48	48	47	46	45	45	44	43	43	42
7 8	53 53	52 52	51 52	51 51	50 50	49	48	47	47	46 46	45 46	45 45	44	43	42
9	54	53	52	51	50	50	49	48	48	47	46	45	45	44	43
10	54	53	52	51	51	50	49	49	48	47	47	46	45	44	44
11	54	53	53	52	51	50	50	49	48	48	47	46	46	45	44
12	54	54	53	52	51	51	50	49	49	48	47	47	46	45	45
13	55	54	53	52	52	51	50	50	49	48	47	47	46	46	45
14	55	54	53	53	52	51	50	50	49	48	48	47	46	46	45
15	55	54	54	53	52	51	51	50	49	49	48	47	47	46	45
16	55	55	54	53	52	52	51	50	50	49	48	48	47	46	46
17	56	55	54	53	53	52	51	51	50	49	49	48	47	47	46
18 19	56 56	55 55	54 55	54 54	53 53	52 52	51 52	51 51	50 50	49 50	49	48	47	47	46
20	56	56	55	54	53	53	52	51	51	50	49	49	48	47	47
21	57	56	55	54	5.1	53	52	52	51	50	50	49	48	48	
21 22	57	56	55	54 55	54 54	53	53	52	51	50	50	49	48	48	47
23	57	56	56	55	54	53	53	52	51	51	50	49	49	48	48
21	57	57	56	55	54	54	53	52	52	51	50	50	49	48	48
25	58	57	56	55	55	54	53	53	52	51	51	50	49	49	48
26	58	57	56	56	55	54	53	53	52	51	51	50	50	49	48
27	58	57	56	56	55	54	54	53	52	52	51	50	50	49	48
28 29	58 58	57	57	56	55	55	54	53	53	52	51	51	50	49	49
30	59	58 58	57 57	56 57	56 56	55 55	54 54	53 54	53 53	52 52	52 52	51 51	50 51	50 50	49
100	59			13					FIRE	THE R	5.04		-	50	
31 32	59	58 58	57 58	57 57	56 56	55 56	55 55	54 54	53 54	53 53	52 52	51 52	51 51	50	49 50
33	59	59	58	57	56	56	55	54	54	53	52	52	51	51	50
34	60	59	58	57	57	56	55	55	54	53	53	52	52	51	50
35	60	59	58	58	57	56	56	55	54	54	53	52	52	51	50

Temper- ature of			t -	- <b>t</b> ' == 1	Differen	ce of T	Tempera	tures o	f the D	ew Poi	int and	of the	Air.		
the air.	12°.0	12°.2	12°.4	12°.6	12°.8	13°.0	13°.2	13°.4	13°.6	13°.8	14°.0	14°.2	14°.4	14°.6	14°.8
Centig.	7-7-														
-8 -7	1		eka :	not i	0.7	100					O Z	1000	600	N	A B
-6		High	1,11	a de	1910	200	- N		DEVIS.	FEET 1	311				
-5							Kall				1				
-4		188		7			919			1	19			A.3	
-3		ole of		Stum-	4										
-2										1024					
<del>-</del> 1														37	
0										ST INTE	Carl C				
+1								488			48	es tra		14.00	
2 3	14	A SECTION	N. Sec.	1								200700			1 1
4	40	40	39	38	38	37									7.07=
5	41	40	39	39	38	38	37	36	36	35	35				412
6	41	41	40	39	39	38	37	37	36	36	35	35	34	33	33
7	42	41	40	40	39	39	38	37	37	36	36	35	34	34	33
8	42	42	41	40	40	39	38	38	37	37	36	35	35	34	34
9	43	42 43	41 42	41	40	40	39	38	38	37	37	36	35	35	34
		100 11		41	41	40	39	39	38	38	37	36	36	35	35
11 12	44	43	42	42	41	40	40	39	39	38	37	37	36	36	35
13	44	43	43	42	41 42	41	40	40 40	39 39	38 39	38 38	37 38	37	36 37	36
14	45	44	43	43	42	42	41	40	40	39	39	38	37	37	36
15	45	44	44	43	42	42	41	41	40	39	39	38	38	37	37
16	45	44	44	43	43	42	41	41	40	40	39	39	38	38	37
17	45	45	44	43	43	42	42	41	41	40	39	39	38	38	37
18 19	46 46	45 45	44	44	43	43	42	41	41	40	40	39	39	38	38
20	46	45	45 45	44	43	43	42	42	41	41	40	39 40	39 39	38 39	38
21	46	46	45	45	44	43	4-	100	100.	100			442	39	38
22	47	46	45	45	44	43	43	42	42	41	41	40	39	39	39
23	47	46	46	45	45	44	43	43	42	42	41	41	40	39	39
24	47	47	46	45	45	44	44	43	42	42	41	41	40	40	39
25	47	47	46	46	45	44	44	43	43	42	42	41	41	40	39
26	48	47	46	46	45	45	44	44	43	42	42	41	41	40	40
27 28	48	47	47	46	45 46	45 45	44 45	44	43	43	42	42	41	40	40
29	48	48	47	47	46	45	45	44	44 44	43	42	42 42	41 42	41 41	40
30	49	48	47	47	46	46	45	45	44	43	43	42	42	41	41
31	49	48	48	47	46	46	45	45	44	44	43	43	42	42	41
32	49	49	48	47	47	46	46	45	45	44	43	43	42	42	41
33	49	49	48	48	47	46	46	45°	45	44	44	43	-43	42	42
34	50 50	49	49	48	47	47	46	46	45	44	44	43	43	42	42
	00	**	13	40	30	-21	40	40	40	44	44	44	43	43	42

#### TABLE IV.

FACTOR  $_{\mathbf{F}}^{100}$ , FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE OF THE AIR FROM ITS ABSOLUTE HUMIDITY, GIVEN IN MILLIMETRES.

#### BY HAEGHENS.

THE Relative Humidity, or the degree of moisture of the air, is the ratio of the quantity of vapor contained in the air to the quantity it could contain at the temperature observed, if fully saturated.

If we call

The force of vapor contained in the air = f,

The maximum of the force of vapor at the temperature of the air = F,

The point of saturation = 100,

we have the proportion,

Relative Humidity: 100::f:F,

and

 $\frac{f \times 100}{F}$  = Relative Humidity in Hundredths.

But as  $\frac{f \times 100}{F} = f \times \frac{100}{F}$ , it is obvious that the operation indicated by the former expression, viz.  $\frac{f \times 100}{F}$ , would be reduced to a simple multiplication, if we had a table of the factors  $\frac{100}{F}$ . Such a table is obtained by dividing the constant number 100 by each number in the Table of Elastic Forces of Vapor, and substituting the quetients to the tensions.

The following Table, taken from the Annuaire Météorologique de la France, for 1850, p. 79, gives the factor  $\frac{100}{F}$  for every tenth of a degree from -10 to  $+35^{\circ}$  Centigrade, corresponding to the Forces of Vapor in Table I.

#### USE OF THE TABLE.

The force of vapor contained in the air being given in millimetres, multiply the number expressing it by the factor in the table corresponding to the temperature of the air at the time of the observation; the result will be the Relative Humidity in Hundreaths.

## Examples.

- 1. Suppose the temperature of the air to be = 24° Centigrade.
  - " force of vapor in the air to be = 10.76 millimetres.

Opposite 24° is found in the table the factor 4.51.

Then  $10.76 \times 4.51 = 48.5$ , Relative Humidity in Hundredths.

- 2. Suppose the temperature of the air to be = 16.7.
  - " force of vapor in the air to be = 12.07.

Table gives for 16.7 the factor 7.07.

Then  $12.07 \times 7.07 = 85.3$ , Relative Humidity.

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t =					Tenths o	f Degrees.				" ,
Temp. of Air, lentig.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	48.1	48.5	48.9	49.3	49.7	50.1	50.5	50.9	51.4	51.8
-10	41.2	44.6	45.0	45.4	45.7	46.1	46.5	46.9	47.3	47.7
9	40.7	41.1	41.4	41.7	42.1	42.4	42.8	43.1	43.5	43.9
8 7	37.5	37.8	38.1	38.4	38.7	39.0	39.4	39.7	40.0	40.4
1	34.6	34.9	35.2	35.4	35.7	36.0	36.3	36.6	36.9	37.2
6	31.9	32.2	32.4	32.7	33.0	33.2	33.5	33.8	34.0	34.3
5	29.5	29.8	30.0	30.2	30.5	30.7	31.0	31.2	31.4	31.7
4	27.3	27.5	27.7	27.9	28.2	28.4	28.6	28.8	29.1	29.3
3 2	25.3	25.5	25.7	25.9	26.1	26.3	26.5	26.7	26.9	27.1
1	23.4	23.6	23.8	24.2	24.0	24.3	24.5	24.7	24.9	25.1
1	20.4	20.0	20.0	24.2	24.0	24.0	24.0	24.1	24.0	20.1
-0	21.7	21.9	22.1	22.2	22.4	22.6	22.8	22.9	23.1	23.3
+0	21.7	21.6	21.4	21.3	21.1	21.0	20.8	20.7	20.5	20.4
SWIT	00.0	00.1	00.0	10.0	10.0	10.5	70	10.0	mi/din	10.0
1	20.2	20.1	20.0	19.8	19.7	19.5	19.4	19.3	19.1	19.0
2	18.9	18.7	18.6	18.5	18.3	18.2	18.1	18.0	17.8	17.7
3	17.6	17.5	17.3	17.2	17.1	17.0	16.9	16.7	16.6	16.5
4	16.4	16.3	16.2	16.1	15.9	15.8	15.7	15.6	15.5	15.4
5	15.3	15.2	15.1	15.0	14.9	14.8	14.7	14.6	14.5	14.4
6	14.3	14.2	14.1	14.0 .	13.9	13.8	13.7	13.6	13.5	13.4
7	13.4	13.3	13.2	13.1	13.0	12.9	12.8	12.7	12.6	12.6
8	12.5	12.4	12.3	12.2	12.1	12.1	12.0	11.9	11.8	11.7
9	11.7	11.6	11.5	11.4	11.4	11.3	11.2	11.1	11.1	11.0
10	10.9	10.8	10.8	10.7	10.6	10.6	10.5	10.4	10.3	10.3
11	10.2	10.1	10.1	10.0	9.95	9.88	9.82	9.75	9.69	9.6
12	9.56	9.50	9.44	9.38	9.32	9.26	9.20	9.13	9.08	9.0
13	8.96	8.90	8.84	8.79	8.73	8.67	8.62	8.56	8.51	8.4
14	8.40	8.34	8.29	8.24	8.18	8.15	8.08	8.03	7.98	7.9
15	7.87	7.82	7.77	7.72	7.68	7.63	7.58	7.53	7.48	7.4
16	7.39	7.34	7.29	7.25	7.20	7.16	7.11	7.07	7.02	6.9
17	6.93	6.89	6.85	6.80	6.76	6.72	6.68	6.63	6.59	6.5
18	6.51	6.47	6.43	6.39	6.35	6.31	6.27	6.23	6.19	6.1
19	6.12	6.08	6.04	6.00	5.97	5.93	5.89	5.86	5.82	5.7
20	5.75	5.71	5.68	5.64	5.61	5.58	5.54	5.51	5.47	5.4
01		- 00	- 0.1	- 01	- 0-	- 04		F 10		
21	5.41 5.09	5.37	5.34	5.31	5.27	5.24	5.21	5.18	5.15	5.1
22	The state of	5.06 4.76	5.02	4.99	4.96	4.93	4.90	4.87	4.85	4.8
23	4.79		4.73	4.70	4.67	4.65	4.62	4.59	4.56	4.5
24 25	4.51 4.25	4.48	4.45	4.43	4.40	4.37	4.35	4.32	4.30	4.2
26	4.25	3.98	3.95	4.17	4.15	4.12 3.89	4.10	3.84	3.82	4.0
27	3.77	3.75	3.73	3.93	3.91 3.69	3.66	3.86 3.64	3.84	3.82	3.7
28	3.56	3.54	3.52	3.50	3.48	3.46	3.44	3.42	3.40	3.3
29	3.36	3.34	3.32	3.30	3.48	3.46	3.44	3.42	3.40	3.1
30	3.17	3.15	3.13	3.12	3.28	3.26	3.24	3.22	3.03	3.0
		125			B ( No. 10 ( NO.	S. Same	A CHARLES			THE PERSON
31	2.99	2.98	2.96	2.94	2.93	2.91	2.89	2.88	2.86	2.8
32	2.83	2.81	2.80	2.78	2.77	2.75	2.73	2.72	2.70	2.6
99	2.67	2.66	2.64	2.63	2.61	2.60	2.58	2.57	2.56	2.5
33	2.53	2.51	2.50	2.49	2.47	2.46	2.44	2.43	2.42	2.4

#### TABLE V.

#### WEIGHT OF VAPOR, IN GRAMMES,

CONTAINED IN A CUBIC METRE OF SATURATED AIR UNDER A BAROMETRIC PRESSURE OF 760 MILLIMETRES, AND AT TEMPERATURES BETWEEN  $-20^{\circ}$  AND  $+40^{\circ}$  CENTIGRADE.

The theoretic density of aqueous vapor is very nearly 0.622, or §, of the density of the air at the same temperature and pressure. Regnault's experiments gave similar results. From this ratio the weight of the vapor contained in a given volume of air, the temperature and humidity of which are known, can be computed.

If we call

t = the temperature of the air;

f = the elastic force of the vapor contained in the air at the time of the observation;

F= the maximum elastic force of vapor due to the temperature t, as given in the table;

p = the weight of the vapor contained in a litre of air at the temperature t, and with a force of vapor f;

P = the weight of vapor in a litre of air at the temperature t, and at full saturation, or F.

Then, 
$$p = 0.622 \frac{1.293223^{\text{gr.}}}{1 + 0.00367 t} \cdot \frac{f}{760^{\text{min.}}}$$

In which 1.293223 grammes is the weight of a litre of dry air, at the temperature of zero Centigrade, and under a barometric pressure of 760 millimetres, according to the determination of Regnault; 0.00367, the coefficient of the expansion of the air as found by the same; 760 millimetres, the assumed normal barometric pressure.

The weight of a litre of air given by Regnault in the Mémoires de l'Institut, Tom. XXI. p. 157, is 1.293187 grammes; but by correcting a slight error of computation (see E. Ritter, Mémoires de la Société Physique de Genève, Tom. XIII. p. 361), it becomes, as given above, 1.293223 grammes.

In order to obtain the weight of vapor in a cubic metre, or 1000 litres, of saturated air, the formula becomes,

$$P = 0.622 \, \frac{1293.223^{\text{gr.}}}{1 + 0.00367 \, t} \cdot \frac{F}{760^{\text{mm.}}}.$$

From this formula Table V. has been computed. The tensions due to the temperatures in the first column are placed opposite the weights of vapor; they are taken from Table I. It will be seen that, throughout the table, the number of grammes of vapor nearly corresponds to the number of millimetres of pressure expressing the tension.

The table of the weights of vapor given in Pouillet's Eléments des Physique, Tom. II. p. 707, being based on older values, gives results somewhat different. In that published by Becquerel, Eléments de Physique Terrestre, p. 354, Regnault's tensions and coefficient of expansion of the air have been used, but the value of the weight of vapor in a litre of air formerly determined by Biot and Arago, viz. 1.29954 grammes, has been retained.

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## V. WEIGHT OF VAPOR, IN GRAMMES,

## CONTAINED IN A CUBIC METRE OF SATURATED AIR,

At Temperatures between  $-20^{\circ}$  and  $+40^{\circ}$  Centigrade.

				11			
Temperature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Difference.	Temperature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Difference.
Centigrade.	Millimetres.	Grammes.	Grammes.	Centigrade.	Millimetres.	Grammes.	Grammes.
-20°	0.912	1.042		+10°	9.165	9.357	
-19	0.993	1.130	0.088	11	9.792	9.962	0.605
-18	1.080	1.224	0.094	12	10.457	10.601	0.639
-17	1.174	1.325	0.101	13	11.162	11.276	0.675
-16	1.275	1.434	0.109	14	11.908	11.988	0.712
	12.00		Mark Inc.		No. of Street		
Was Levis				100 200		E PURPLE	
-15	1.385	1.551	0.118	15	12.699	12.739	0.751
-14	1.503	1.678	0.127	16	13.536	13.532	0.793
-13	1.631	1.813	0.134	17	14.421	14.367	0.835
-12	1.768	1.957	0.145	18	15.357	15.247	0.880
-11	1.918	2.114	0.157	19	16.346	16.173	0.926
Emplo.					Company of		restart na
-10	2.078	2.283	0.169	20	17.391	17.148	0.975
- 9	2.261	2.475	0.192	21	18.495	18.174	1.026
- 8	2.456	2.678	0.203	22	19.659	19.253	1.078
- 7	2.666	2.896	0.218	23	20.888	20.387	1.134
- 6	2.890	3.128	0.232	24	22.184	21.579	1.192
DEVIS		The second		10 V 11 V 11	179		
In State of the		Na Sile of	0.010		1,117834		
- 5	3.131	3.376	0.248	25	23.550	22.831	1.252
- 4	3.387	3.638	0.262	26	24.988	24.144	1.313
- 3	3.662	3.919	0.281	27	26.505	25.524	1.380
- 2	3.955	4.217	0.298	28	28.101	26.971	1.447
- 1	4.267	4.534	0.317	29	29.782	28.489	1.519
					1		
			0.334				
0	4.600	4.869	The second second	30	31.548	30.079	1.589
+ 1	4.940	5.209	0.341	31	33.405	31.744	1.666
2	5.302	5.571	0.383	32	35.359	33.491	1.747
3	5.687	5.953	0.406	33	37.410	35.317	1.827
4	6.097	6.360	0.400	34	39.565	37.230	1.913
	Tay - 2 8	The state of		The state of	VI SUPER		18 5 5 5 5
			0.431			N. I. SHEET	2.001
5	6.534	6.791	0.451	35	41.827	39.231	2.001
6	6.998	7.247	0.484	36	44.201	41.323	2.092
7	7.492	7.731	0.484	. 37	46.691	43.510	2.187
8	8.017	8.243	0.512	38	49.302	45.795	2.285
9	8.574	8.785	0.572	39	52.039	48.182	2.387
+10	9.165	9.357	0.012	+40	54.906	50.674	2.492
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# PRACTICAL TABLES,

IN

## ENGLISH MEASURES,

BASED ON REGNAULT'S HYGROMETRICAL CONSTANTS.

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## VI.

## TABLE OF THE ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT,
REDUCED FROM REGNAULT'S TABLE.

THE values of the elastic force of vapor furnished by V. Regnault, which are found in Table I. of this Hygrometrical set, are derived from a series of experiments conducted, during several years, with great care, consummate skill, and all the means of precision which are at the disposal of modern science. The methods of investigation, and all the steps in each experiment, were minutely described and submitted to the judgment of the scientific, successively in separate papers in several volumes of the Annales de Chimie et de Physique, and collectively in his final Report to the Minister of Public Works, (see above, p. 9,) which fills Volume XXI. of the Mémoires de l'Institut de France. The confidence which has been deservedly granted to these determinations by nearly all scientific men, is increased by the fact that one of the best physicists and experimenters in Germany, Professor Magnus, came, about the same time, to results so little different, that both tables, for most purposes, may be considered identical. (Compare below, Table XXII.) It seems, therefore, that these values ought to be used in our hygrometrical tables, as has been done in France, in preference to the older and less reliable determinations on which they are based.

Though Regnault's table of the elastic force of vapor is considered, even, it is believed, by a majority of scientific men in England, as the most reliable which science now possesses, the author is not aware that any extensive reduction of it to English measures, such as is wanted for meteorological purposes, has been as yet published; still less a series of tables based on these values. Such a set of hygrometrical tables in English measures, corresponding to the preceding one in French measures, is offered here, which, it is hoped, supplies a real want felt by a large number of meteorologists.

Table VI. is Regnault's Table of the Elastic Force of Vapor as given in Table I., reduced to English measures, in which the fourth decimal is given in order to secure the third, and otherwise to facilitate the computations. From these values Tables VII. to X. have been computed.

## VI. ELASTIC FORCE OF AQUEOUS VAPOR,

## EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT.

## REDUCED FROM REGNAULT'S TABLE.

Temper-	Force of	20.00	Temper-	EST-100	f Vapor.	Temper		ce of Va		Temper		f Vapor.
Fahren- heit.	Tenths of	Degrees.	Fahren- heit.	Tenths of	Degrees.	Fahrer heit.		hs of De	grees.	Fahren heit.	Tenths o	f Degrees.
	0	0.5		0	0.5		0		.5		0	0.5
	Eng. In.	Eng. In.	11/2	Eng. In.	Eng. In.		Eng.		g. In.	0.0	Eng. In.	Eng. In.
-31	0.0087	0.0085	-19	0.0171	0.0167	- 8	0.03		0290	+ 2	0.0476	
-30	0.0092	0.0090	-18	0.0181	0.0176	- 7			0304	3	0.0498	-
-29 -28	0.0098	0.0095	-17 -16	0.0190	0.0185	- 6 - 5	0.03		0319 0335	5	0.0521	1
-27	0.0104	0.0107	-15	0.0200	0.0195	- 4			0351	6	0.0540	177 - 24
-26	0.0117	0.0107	-13 -14	0.0210	0.0205	- 3	0.0		0368	7	0.0570	1
-20	0.0117	0.0114	-14	0.0221	0.0210	- 3	0.0	570 0.	0300	L by -	0.0557	0.0011
-25	0.0124	0.0120	-13	0.0232	0.0227	- 2	0.0	395 0.	0386	8	0.0625	0.0639
-24	0.0131	0.0127	-12	0.0244	0.0238	- 1	0.0		0404	9	0.0654	Barrier Prins
-23	0.0124 0.0120 0.0131 0.0127 0.0138 0.0135 0.0146 0.0142 0.0154 0.0150 0.0163 0.0158		-11	0.0257	0.0250	- 0	0.0		0424	10	0.0684	100000
-22	0.0146	0.0142	-10	0.0270	0.0263	+ 0	0.0	134 0.	0444	11	0.0716	0.0732
-21	0.0154	0.0150	- 9	0.0283	0.0276	+ 1	0.0	154 0.	0465	12	0.0749	0.0766
-20	0.0163	0.0158	- 8	0.0297	0.0290	+ 2	0.0	176 0.	0487	+13	0.0783	0.0800
Temper- ature Fahren-	2010	1.7-14			Ten	ths of De	grees.					
heit.	0.	1.	2.	3	. 4	E.	5.	6.		7.	8.	9.
0	Eng. In.		1 0			In. E	og. In.	Eng. I	n. E	ng. In.	Eng. In.	Eng. In.
14	0.0818	1100000	1 3 5 1				.0837	0.084		.0845	0.0849	0.0853
15	0.0857	100000					.0877	0.088		.0885	0.0889	0.0893
16	0.0898	1 1 1 1 1 1 1 1 1 1	-	S.C. LAWYER			.0918	0.092		.0927	0.0931	0.0936
17	0.0940		A ITA IIIA III	10000	1991		.0962	0.096		.0971	0.0975	0.0980
18	0.0984	1000000	100000000	11/01/01		ALC: US	1007	0.101		1016	0.1021	0.1025
19	0.1030	0.1035	0.104	0.10	0.1	049 0	1054	0.105	9 0	.1064	0.1068	0.1073
20	0.1078	0.1088	0.108	8 0.10	93 0 1	098 0	.1103	0.110	8 0	1113	0.1118	0.1123
21	0.1128		4			201	1153	0.115		1164	0.1169	0.1174
22	0.1179			645 W. L. U.S.			1206	0.121	1000	1217	0.1222	0.1227
23	0.1233				CT 10 10 25 11		1260	0.126		1272	0.1277	0.1283
24	0.1289	0.1295				Court Live	1318	0.132		1329	0.1335	0.1341
25	0.1347	0.1353	0.135	9 0.13	65 0.1	371 0	1377	0.138	3 0.	1389	0.1395	0.1401
Books !	all victor	· KAN	15.50	A. Care	St Bak		-	-	1	COVI -	are in the	
26	0.1407	0.1413	0.141	9 0.14	26 0.1	432 0	1438	0.144	4 0.	1450	0.1457	0.1463
27	0.1469	0.1476	0.148	2 0.14	88 0.1	495 0	1501	0.150	8 0.	1514	0.1521	0.1527
28	0.1534	0.1540	0.154	7 0.15	53 0.1	560 0.	1567	0.157	3 0.	1580	0.1587	0.1593
29	0.1600	0.1607	0.161	3 0.16	20 0.1	627 0	1634	0.164	1 0.	1647	0.1654	0.1661
30	0.1668	THE RESERVE OF	The state of the s	10000	2 11 11 11 11		1703	0.171	0 0.	1717	0.1724	0.1732
31	0.1739	0.1746	0.175	3 0.17	60 0.1	767 0	1775	0.178	2 0.	1789	0.1796	0.1804

## Expressed in English Inches of Mercury for Temperatures of Fahrenheit.

Tempera-		i na terr	remeaus		Tenths o	f Degrees.	iosik za			in A
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.
32	0.1811	0.1818	0.1825	0.1833	0.1840	0.1847	0.1854	0.1861	0.1869	0.1876
33	0.1883	0.1891	0.1898	0.1906	0.1913	0.1921	0.1928	0.1936	0.1944	0.1951
34	0.1959	0.1967	0.1974	0.1982	0.1990	0.1998	0.2006	0.2013	0.2021	0.2029
35	0.2037	0.2045	0.2053	0.2061	0.2070	0.2077	0.2086	0.2094	0.2102	0.2111
36	0.2119	0.2127	0.2135	0.2144	0.2152	0.2161	0.2169	0.2178	0.2186	0.2195
37	0.2204	0.2212	0.2221	0.2230	0.2238	0.2247	0.2256	0.2265	0.2273	0.2282
38	0.2291	0.2300	0.2309	0.2318	0.2327	0.2336	0.2345	0.2354	0.2364	0.2373
39	0.2382	0.2391	0.2400	0.2410	0.2419	0.2428	0.2438	0.2447	0.2457	0.2466
40	0.2476	0.2485	0.2495	0.2504	0.2514	0.2524	0.2533	0.2543	0.2553	0.2563
41	0.2572	0.2582	0.2592	0.2602	0.2612	0.2622	0.2632	0.2642	0.2652	0.2662
42	0.2672	0.2682	0.2692	0.2702	0.2713	0.2723	0.2733	0.2744	0.2754	0.2764
43	0.2775	0.2785	0.2796	0.2807	0.2817	0.2828	0.2839	0.2850	0.2860	0.2871
44	0.2882	0.2893	0.2904	0.2915	0.2926	0.2937	0.2948	0.2960	0.2971	0.2982
45	0.2993	0.3005	0.3016	0.3028	0.3039	0.3050	0.3062	0.3074	0.3085	0.3097
46	0.3108	0.3120	0.3132	0.3144	0.3156	0.3168	0.3179	0.3191	0.3203	0.3215
47	0.3228	0.3240	0.3252	0.3264	0.3276	0.3289	0.3301	0.3313	0.3326	0.3338
48	0.3351	0.3363	0.3376	0.3388	0.3401	0.3414	0.3426	0.3439	0.3452	0.3465
49	0.3477	0.3490	0.3503	0.3516	0.3529	0.3542	0.3556	0.3569	0.3582	0.3595
50	0.3608	0.3622	0.3635	0.3648	0.3661	0.3675	0.3688	0.3702	0.3715	0.3729
51	0.3743	0.3756	0.3770	0.3784	0.3798	0.3812	0.3826	0.3840	0.3854	0.3868
	0.0000	0.0000	0.0011	BEN T	w( sale)		Mapa I			0 10=0
52	0.3882	0.3896	0.3911	0.3925	0.3939	0.3954	0.3968	0.3983	0.3997	0.4012
53 54	0.4027	0.4041	0.4056	0.4071	0.4086	0.4101	0.4116	0.4131	0.4146	0.4161
55	0.4176	0.4191	0.4207	0.4222	0.4237	0.4253	0.4268	0.4284	0.4299	0.4315
56	0.4331	0.4346	0.4362	0.4378	0.4394	0.4410	0.4426	0.4442	0.4458 0.4622	0.4474 0.4638
30	0.4430	0.4507	0.4525	0.4539	0.4556	0.4572	0.4589	0.4605	0.4022	0.4050
57	0.4655	0.4672	0.4689	0.4705	0.4722	0.4739	0.4756	0.4773	0.4791	0.4808
58	0.4825	0.4842	0.4859	0.4876	0.4894	0.4912	0.4929	0.4947	0.4964	0.4982
59	0.5000	0.5017	0.5035	0.5053	0.5071	0.5089	0.5107	0.5125	0.5143	0.5161
60	0.5179	0.5198	0.5216	0.5234	0.5253	0.5271	0.5290	0.5301	0.5328	0.5346
61	0.5365	0.5384	0.5403	0.5422	0.5441	0.5461	0.5480	0.5499	0.5519	0.5538
62	0.5558	0.5577	0.5597	0.5617	0.5636	0.5656	0.5676	0.5696	0.5716	0.5736
63	0.5756	0.5777	0.5797	0.5817	0.5838	0.5858	0.5879	0.5899	0.5920	0.5941
64	0.5962	0.5983	0.6004	0.6025	0.6046	0.6067	0.6088	0.6109	0.6131	0.6152
65	0.6173	0.6195	0.6217	0.6238	0.6260	0.6282	0.6304	0.6325	0.6347	0.6369
66	0.6392	0.6414	0.6436	0.6458	0.6481	0.6503	0.6525	0.6548	0.6571	0.6593
67	0.6616	0.6639	0.6662	0.6685	0.6708	0.6731	0.6754	0.6777	0.6800	0.6824
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT.

Tempera-					Tenths of	Degrees.				
ture of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.
68	0.6847	0.6870	0.6894	0.6917	0.6941	0.6965	0.6989	0.7012	0.7036	0.7060
69	0.7084	0.7108	0.7133	0.7157	0.7181	0.7206	0.7230	0.7255	0.7280	0.7305
70	0.7329	0.7354	0.7379	0.7405	0.7430	0.7455	0.7480	0.7506	0.7531	0.7557
71	0.7583	0.7609	0.7634	0.7660	0.7686	0.7712	0.7739	0.7765	0.7791	0.7818
72	0.7844	0.7871	0.7897	0.7924	0.7951	0.7978	0.8005	0.8032	0.8059	0.8086
73	0.8113	0.8141	0.8168	0.8196	0.8223	0.8251	0.8279	0.8307	0.8335	0.8363
74	0.8391	0.8419	0.8447	0.8476	0.8504	0.8533	0.8561	0.8590	0.8619	0.8648
75	0.8676	0.8705	0.8735	0.8764	0.8793	0.8822	0.8852	0.8881	0.8911	0.8940
76	0.8970	0.9000	0.9030	0.9060	0.9090	0.9120	0.9150	0.9180	0.9211	0.9241
77	0.9272	0.9302	0.9383	0.9364	0.9395	0.9426	0.9457	0.9488	0.9519	0.9550
78	0.9582	0.9613	0.9645	0.9677	0.9709	0.9740	0.9773	0.9805	0.9837	0.9869
79	0.9902	0.9934	0.9967	1.0000	1.0033	1.0065	1.0099	1.0132	1.0165	1.0198
80	1.0232	1.0265	1.0299	1.0332	1.0366	1.0400	1.0434	1.0468	1.0503	1.0537
81	1.0572	1.0606	1.0641	1.0675	1.0710	1.0745	1.0780	1.0815	1.0851	1.0886
82	1.0922	1.0957	1.0993	1.1028	1.1064	1.1100	1.1136	1.1172	1.1209	1.1245
	BARE!	7 5 5 5 6	6x + 22	Carlon Carlo	MED 144	ile III	44			
83	1.1281	1.1318	1.1354	1.1391	1.1428	1.1465	1.1502	1.1539	1.1576	1.1614
84	1.1651	1.1689	1.1726	1.1764	1.1802	1.1840	1.1878	1.1916	1.1954	1.1993
85	1.2031	1.2070	1.2108	1.2147	1.2186	1.2225	1.2264	1.2303	1.2342	1.2381
86	1.2421	1.2460	1.2500	1.2540	1.2580	1.2620	1.2660	1.2700	1.2740	1.2781
87	1.2821	1.2862	1.2903	1.2944	1.2985	1.3026	1.3068	1.3109	1.3151	1.3192
sane 1414	paller a	DEMONSTRA	r mu k	eiribide	dep 7	maA s	140076	utagos	d oblin	
88	1.3234	1.3276	1.3318	1.3361	1.3403	1.3445	1.3488	1.3531	1.3573	1.3616
89	1.3659	1.3703	1.3746	1.3789	1.3833	1.3877	1.3920	1.3964	1.4008	1.4053
90	1,4097	1.4141	1.4186	1.4230	1.4275	1.4320	1.4365	1.4410	1.4456	1.4501
91	1.4546	1.4592	1.4638	1.4684	1.4730	1.4776	1.4822	1.4869	1.4915	1.4962
92	1.5008	1.5055	1.5102	1.5149	1.5197	1.5244	1.5291	1.5339	1.5387	1.5435
				grayler	Con Assess	1 3 3	east orbi	in the later		geral)
93	1.5482	1.5531	1.5579	1.5627	1.5676	1.5724	1.5773	1.5822	1.5871	1.5920
94	1.5969	1.6018	1.6068	1.6117	1.6167	1.6217	1.6267	1.6317	1.6367	1.6417
95	1.6468	1.6518	1.6569	1.6620	1.6671	1.6722	1.6773	1.6825	1.6876	1.6928
96	1.6980	1.7032	1.7084	1.7137	1.7189	1.7242	1.7295	1.7348	1.7401	1.7454
97	1.7508	1.7561	1.7615	1.7669	1.7723	1.7777	1.7831	1.7886	1.7940	1.7995
98	1.8050	1.8105	1.8160	1.8215	1.8271	1.8327	1.8382	1.8438	1.8494	1.8551
99	1.8607	1.8664	1.8720	1.8777	1.8834	1 0007	1 9040	1.9006	1 0064	1.9121
100	1.9179	1.9237		1.9354	1.9412	1.8891		The second section is a second		1.9707
101	1.9766	1.9826	1.9295	ALCOHOL: NO	THE PROPERTY OF	1.9471	1.9530 2.0126	1.9589	1.9648 2.0247	2.0307
101	2.0368	2.0429	1.9885	1.9945	2.0005	2.0065	MARKET DESIGN	2.0186	And the second second	mir Dr. British and V
102	2.0985	2.1048	2.0490	2.0552	2.0613	2.0675	2.0737	2.0798	2.0861	2.0923 2.1553
104	2.0955	2.1681	2.1110 2.1745	2.1173 2.1810	2.1236 2.1874	2.1299 2.1939	2.1362 2.2004	2.1426	2.1489 2.2135	2.1553
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

#### VII.

## PSYCHROMETRICAL TABLES,

GIVING, IN ENGLISH INCHES OF MERCURY, THE ELASTIC FORCE OF VAPOR CONTAINED IN THE AIR, AND ITS RELATIVE HUMIDITY IN HUNDREDTHS;

DERIVED FROM THE INDICATIONS OF THE WET AND DRY BULB THERMOMETERS,
IN DEGREES OF FAHRENHEIT.

#### By A. GUYOT.\*

M. V. REGNAULT, in his Etudes sur l'Hygrométrie Annales de Chimie et de Physique, 3<sup>mp</sup> série, Tom. XV. p. 129, after having discussed the theoretical bases of the psychrometric formula given by August, and modified the numerical values of some of its coefficients, adopts the formula

$$x = f - \frac{0.480 (t - t')}{610 - t'} h$$

for temperatures above the freezing-point; and when the temperature of the wet thermometer is below the freezing-point, the bulb being covered with a film of ice,

$$x = f - \frac{0.480 (t - t')}{689 - t'} h$$

<sup>\*</sup> While this table was going through the press, a similar one, prepared by Prof. T. H. Coffin for his private use, was published by the Smithsonian Institution, in order to meet an urgent demand from many quarters. Being based on the same formula, it gives the same results, except, perhaps, in degrees below 14° Fahrenheit, where the tables show slight discrepancies. These unimportant differences arise from the fact that Prof. Coffin's table was computed from Regnault's tensions, as given in the first edition of this collection, while the author's table is based on the table of tensions as given in this second edition, in which the values below 14° Fahrenheit have been somewhat modified, for reasons given above. The following table gives also the relative humidity with one more decimal, which makes the interpolations more easy; and a column of differences for finding the values for fractions of t'. A table for reducing the results to another barometric height is added at the end of the table.

in which

x represents the force of vapor in the air at the time of the observation;

t, the temperature of the air in Centigrade degrees, indicated by the dry thermometer;

t', the temperature of evaporation given by the wet thermometer;

f, the force of vapor in a saturated air at the temperature t';

h, the height of the barometer.

Substituting the Fahrenheit scale for the Centigrade, the formula, for temperatures above the freezing-point, reads

$$x = f - \frac{0.480 \times \frac{5}{9}(t - t')}{610 - \frac{5}{8}(t' - 32^{\circ})} h = f - \frac{0.480(t - t')}{1130 - t'} h;$$

and below the freezing-point,

$$x = f - \frac{0.480 \times \frac{5}{9} (t - t')}{689 - \frac{5}{9} (t' - 32^{\circ})} h = f - \frac{0.480 (t - t')}{1240.2 - t'} h.$$

Making, further, h = 29.7 English inches, these formulæ become

$$x = f - \frac{0.480 (t - t')}{1130 - t'}$$
 29.7 =  $f - \frac{14.256 (t - t')}{1130 - t'}$ 

and

$$x = f - \frac{0.480 (t - t')}{1240.2 - t'} 29.7 = f - \frac{14.256 (t - t')}{1240.2 - t'}.$$

The mean barometric pressure for which the table has been computed, viz. 29.7 inches, is, within a small fraction, the same as that adopted in Haeghens's Tables, No. II., which is 755 millimetres = 29.725 Eng. inches. As that slight difference in the barometric pressure cannot cause, in the most extreme cases, a difference exceeding two thousandths of an inch in the elastic forces, the results in the two tables may be considered identical.

That barometric pressure, corresponding, in our latitudes, to a mean altitude of 250 to 300 feet above the sea, is likely to suit, without correction, the largest number of meteorological stations. Should the mean height of the barometer, in consequence of the elevation of the station, much differ from that adopted in the table, a constant correction can be determined, to be applied to the numbers in the table. At the end, page 72, will be found a table which furnishes that correction for barometric heights between 20 and 31 inches, and for values of t - t' between 2° and 26° Fahrenheit.

The effect of the irregular variations of the barometer at the same station can, in most cases, be neglected; for the error due to that cause will scarcely ever exceed those which may arise from the uncertainty of the very elements on which the tables are based.

#### ARRANGEMENT OF THE TABLES.

The same arrangement as is found in the Psychrometrical for the Centigrade scale has been adopted.

The first column at the left contains the indications of the wet-bulb thermometer, from -31° to 105° Fahrenheit.

The second column gives the differences of the force of vapor for each tenth of a degree, between each two consecutive full degrees in the first column. It enables the observer easily to find the values for the fractions of degrees of the wet thermometer.

The following double columns furnish the forces of vapor and the relative humidity corresponding to each full degree of the wet-bulb thermometer given in the first column in the same horizontal line, and to the difference of the two thermometers, or t-t', found at the head of each column, for every half-degree from 0° to 26°.5. The relative humidity, or the fraction of saturation, is given in hundredths, which is near enough for meteorological purposes; but one decimal more has been added, though separated by a point, in order to facilitate the interpolations.

At the bottom of each page is found the mean difference, for each tenth of a degree, between the forces of vapor on the same line. It gives the means of finding the values for the intermediate differences of t-t', not found in the tables.

#### USE OF THE TABLES.

Enter the tables with the difference of the two thermometers, or t-t', and the temperature of the wet-bulb thermometer, given by observation.

In the column headed by the observed difference of the thermometer, t-t', and on the horizontal line headed by the observed temperature of the wet thermometer, t', are found the force of vapor, and the relative humidity corresponding to these temperatures.

For the fractions of degrees of the wet thermometer, multiply the decimal fraction by the number placed in the second column between the full degree and the next, and add the product if the temperature is above, and subtract it if it is below zero Fahrenheit.

The intermediate values of t-t' not given in the table are found by subtracting the number in the line at the bottom of the page, multiplied by the number of additional tenths, from the value given in the table. This correction, being always very small, can usually be neglected.

For the relative humidity, interpolations at sight will generally suffice.

## Examples.

Dry thermometer,  $t = 50^{\circ}$  F. Wet thermometer,  $t' = 43^{\circ}$  F. Difference, or  $t - t' = 7^{\circ}$  F.

Page 58, we find for  $t-t'=7^{\circ}$  in the third double column, and for  $t'=43^{\circ}$  in the first column

Force of vapor in the air = 0.186 inch. Relative humidity in hundredths = 51

B

2. Dry thermometer,  $t = 88^{\circ}.5$  F. Wet thermometer,  $t' = 76^{\circ}.3$  F.

Difference,  $t-t'=12^{\circ}.2$  F.

Page 63, Table gives for t-t'=12 and  $t'=76^\circ$  = 0.735 inch.

Add for fraction of t' = 0.3,  $0.003 \times 3 = 0.009$ 

Subtract for fraction of  $t - t' = 0^{\circ}.2$ ,  $.0013 \times 2 = -0.003$ 

Force of vapor in the air = 0.741

Relative humidity = 55

Dry thermometer,  $t = -4^{\circ}.5 \text{ F.}$ 

Wet thermometer,  $t' = 6^{\circ}.0 \text{ F}.$ 

Difference,  $t - t' = 1^{\circ}.5$  F.

Page 50, Table gives for  $t-t'=1^{\circ}.5$  and  $t'=-6^{\circ}=0.016$  inch.

Subtract for fraction of t' = 0.5,  $0.0002 \times 5 = -0.001$ 

Force of vapor in the air = 0.015

Relative humidity = 45

3.

#### VII. PSYCHROMETRICAL TABLES.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

W-A	Mean		elin.					and Dry					
Wet- Bulb Thermo- meter	Vertical Difference of Force of Vapor	0°.	0	00.	5	10.	0	10.	5	2°.	0	2°.	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In		Eng. In.		Eng. In.	1	Eng. In.		Eng. In.	
-31	.00005	0.009	100	0.003	36.0			1	1/4				
-30	.00006	0.009	100	0.004	39.6		-						
-29 -28	.00008	0.010	100	0.004	42.9 46.1		4.43	and the life		2000			1
-28 -27	.00006	0.010	100	0.003	49.0		= 50	- Vive				14-18-1	
	alegali la	0.011	100	0.000	40.0		- 44	- T-9 6		2 400	1 4	mark to	
1 1	•00006	(0:0)-	0	0 X2 B			100			15miles	9 -14	EXILE:	X.
-26	.00007	0.012	100	0.006	51.8						D (IA)	116 3	
-25	.00007	0.012	100	0.007	54.4						1	100	
-24	.00008	0.013	100	0.008	56.8	WALL	1					1911	- naci
-23	.00008	0.014	100	0.008	59.0								
-22		0.015	100	0.009	61.0								
	.00008											-11-13	
-21		0.015	100	0.010	62.6	0.004	26.9	100		100	Alres		h)
-20	.00008	0.016	100	0.011	64.2	0.005	30.3						
-19	.00008	0.017	100	0.012	65.9	0.006	33.5	100	-				
-18	.00009	0.018	100	0.012	67.5	0.007	36.6				N I I I	110	
-17	•0001	0.019	100	0.013	69.0	0.008	39.5	100				1	
	.0001	1							- 14 8	3.5		kernes i	
10	10001	0.020	100	0.014	70.4	0.009	42.3	000		100			
-16 -15	.0001	0.021	100	0.014	70.4	0.009	44.9	0.004	19.4		of the	1	
-14	.0001	0.021	100	0.013	73.0	0.010	47.4	0.004	23.0	1076	The same	377	N. H
-13	-0001	0.023	100	0.018	74.3	0.012	49.8	0.007	26.4	Val and			The second
-12	.0001	0.024	100	0.019	75.4	0.013	51.9	0.008	29.5	45.20	Staff.	4.13 P	
						0.010	01.0	0.000		10.34	1 0		3100
HELD.	.0001				-11	1	أليور				-	7 1 1	
-11	.0001	0.026	100	0.020	76.5	0.014	53.9	0.009	32.5		Shirt	més i	
-10	.0001	0.027	100	0.021	77.5	0.016	55.7	0.010	35.3	0.005	15.6	46-14	
- 9	.0001	0.028	100	0.023	78.5	0.017	57.7	0.012	38.3	0.006	19.1	FULL	
- 8	.0001	0.030	100	0.024	79.4	0.018	59.4	0.013	40.6	0.007	22.5	P21/2	
- 7	•0001	0.031	100	0.026	80.3	0.020	61.1	0.014	43.0	0.009	25.7 28.4	0.005	12.9
- 6	.0002	0.033	100	0.027	81.1	0.021	62.7	0.016	45.4	0.010	40.4	0.000	12.5
- 5	NO L	0.034	100	0.029	81.8	0.023	64.5	0.017	47.6	0.012	31.7	0.006	16.4
- 4	.0002	0.036	100	0.030	82.5	0.025	65.8	0.019	49.8	0.014	34.5	0.008	19.8
- 3	.0002	0.038	100	0.032	83.2	0.026	67.1	0.021	51.7	0.015	36.9	0.010	22.5
2	.0002	0.039	100	0.034	83.9	0.028	68.3	0.023	53.5	0.017	39.3	0.011	25.8
-1	.0002	0.041	100	0.036	84.5	0.030	69.5	0.024	55.3	0.019	41.6	0.013	28.6
- 0	40002	0.043	100	0.038	85.0	0.032	71.0	0.026	57.0	0.021	43.8	0.015	31.
2512.5	15x 82	18-190		1				5.50	- 194				

Temperature, Fahrenheit. — Force of Vapor In English Inches. — Relative Humidity in Hundredths.

•	W.					oifference eezing-Poi		0.50					
Wet- Bulb Thermo- meter t	Mean Vertical Difference of Force of Vapor	00.	0	0°.	.5	10	.0	10	.5	200	.0	2°	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity
0		Eng. In.		Eng. In.		Eng. In.	9 4 7	Eng. In.		Eng. In.	194	Eng. In	
0	0.0002	0.043	100	0.038	85.0	0.032	70.7	0.026	57.0	0.021	43.8	0.015	31.3
1	.0002	0.045	100	0.040	85.6	0.034	71.8	0.028	58.6	0.023	46.0	0.017	33.9
2	.0002	0.047	100	0.042	86.2	0.036	73.0	0.031	60.2	0.025	48.0	0.019	36.4
3	.0002	0.050	100	0.044	86.7	0.038	74.0	0.033	61.8	0.027	50.0 52.0	0.022	38.8
4		0.052	100	0.046	87.2	0.041	75.0	0.035	63.3	0.030	92.0	0.024	*1.2
	.0002	PORT.	JU 9	A SE			ETB/g						
5	.0002	0.055	100	0.049	87.7	0.043	76.0	0.038	64.7	0.032	53.8	0.026	43.4
6	.0003	0.057	100	0.051	88.2	0.046	76.9	0.040	66.0	0.034	55.3	0.029	45.2
7	.0003	0.059	100	0.054	88.6	0.048	77.7	0.043	67.1	0.037	56.8	0.031	47.0
8	.0003	0.062	100	0.057	89.0 89.4	0.051	78.4	0.045	68.2 69.2	0.040	58.2 59.6	0.034	48.8
9		0.000	100	0.059	09.4	0.034	19.1	0.040	09.2	0.043	99.0	0.057	50.5
	.0003	W.		Sec. 1		y dit						TAPES.	Little
10	.0003	0.068	100	0.062	89.8	0.057	79.7	0.051	70.1	0.046	61.0	0.040	52.2
11	.0003	0.071	100	0.066	90.1	0.061	80.4	0.054	71.1	0.049	62.3	0.043	53.8
12	.0003	0.075	100	0.069	90.4	0.063	81.0	0.058	72.1	0.052	63.5	0.046	55.3
13	.0004	0.078	100	0.072	90.7	0.067	81.6	0.061	73.0	0.056	64.8	0.050	56.8
14		0.082	100	0.076	91.0	0.071	82.3	0.065	73.9	0.059	65.9	0.054	58.2
	.0004				Say 18				4 33 10			Versije	
15	DOD NO	0.086	100	0.080	91.3	0.074	82.9	0.069	74.8	0.063	67.1	0.057	59.7
16	-0004	0.090	100	0.084	91.6	0.078	83.4	0.073	75.7	0.067	68.2	0.061	61.0
17	.0004 .0004	0.094	100	0.088	91.9	0.083	84.0	0.077	76.5	0.071	69.2	0.066	62.3
18	.0004	0.098	100	0.093	92.1	0.087	84.5	0.081	77.2	0.076	70.2	0.070	63.5
19	*0000	0.103	100	0.097	92.4	0.092	85.0	0.086	78.0	0.080	71.2	0.075	64.7
	.0005											TANK!	
20		0.108	100	0.102	92.6	0.096	85.5	0.091	78.7	0.085	72.1	0.079	65.8
21	•0005	0.113	100	0.107	92.9	0.101	86.0	0.096	79.4	0.090	73.0	0.084	66.9
22	.0005 .0005	0.118	100	0.112	93.1	0.107	86.4	0.101	80.0	0.095	73.8	0.089	68.0
23	.0005	0.123	100	0.118	93.3	0.112	86.8	0.106	80.7	0.100	74.6	0.095	68.9
24	.0006	0.129	100	0.123	93.6	0.117	87.2	0.112	81.2	0.106	75.4	0.100	69.9
25	.0006	0.135	100	0.129	93.8	0.123	87.6	0.118	81.8	0.112	76.1	0.106	70.7
26	***************************************	0.141	100	0.135	94.0	0.129	88.0	0.123	82.4	0.117	76.8	0.112	71.6
27	-0006	0.141	100	0.133	94.1	0.125	88.3	0.123	82.9	0.117	77.5	0.112	72.5
28	.0006	0.147	100	0.141	94.3	0.130	88.7	0.136	83.4	0.124	78.2	0.115	73.3
29	.0007	0.160	100	0.154	94.5	0.149	89.0	0.143	83.9	0.137	78.8	0.131	74.0
30	-0007	0.167	100	0.161	94.7	0.155	89.3	0.150	84.3	0.144	79.4	0.138	74.8
31	.0007	0.174	100	0.168	94.8	0.162	89.6	0.157	84.8	0.151	80.0	0.145	75:6

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.0012.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

W	Water	Secure Secure	- gru		,			and Dry E					
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	3°.	0	3°.	5	40.	0	4°.	5	5°.	0	50	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid ity.
0		Eng. In.		Eng. In.	- 0	Eng. In.		Eng. In.	gost!	Eng. In.		Eng. In.	
0	0.0002	0.010	19.3	0.004	7.9	194 1 24		100		OF L	191	LOUIS	
1 2	.0002	0.012	22.3 25.3	0.006	14.7	13/12						HOM.	
3	.0002	0.014	28.1	0.010	17.8		mal.	200		1		10,55.	300
4	.0002	0.018	30.8	0.013	20.9	0.007	11.4	100		and the		ESPAIN.	- 2
	.0002	0.010	0010	0.010		0.001							
		0.021	33.4	0.015	23.8	0.010	14.6	4		-X-1-2		1000	
5	.0002	0.021	35.4	0.015	26.3	0.010	17.5	0.006	9.0	To Fig.	1	Sign.	
7	.0002	0.026	37.7	0.020	28.8	0.012	20.2	0.009	12.0			1,00c. T	
8	.0003	0.028	39.8	0.023	31.2	0.017	22.9	0.011	15.0			reaty.	
9	.0003	0.031	41.8	0.026	33.5	0.020	25.5	0.014	17.9	0.009	10.6	199	
	.0003									127		SW.	
10	1	0.034	43.8	0.029	35.7	0.023	28.0	0.017	20.6	0.012	13.6	9-17	157
11	.0003	0.037	45.7	0.032	37.9	0.026	30.4	0.020	23.3	0.014	16.4	0.009	9.
12	.0003	0.041	47.5	0.035	40.0	0.029	32.7	0.024	25.8	0.018	19.2	0.012	12.
13	.0003	0.044	49.2	0.039	42.0	0.033	35.0	0.027	28.3	0.022	21.9	0.016	15.
14	.0004	0.048	50.9	0.042	43.9	0.037	37.1	0.031	30.7	0.025	24.5	0.020	18.
	.0004									Full C		epita.	
15	Sed of	0.052	52.5	0.046	45.7	0.040	39.2	0.035	32.9	0.029	26.9	0.023	21.
16	.0004	0.056	54.1	0.050	47.5	0.044	41.2	0.039	35.1	0.033	29.3	0.027	23.
17	.0004	0.060	55.6	0.054	49.2	0.049	43.1	0.043	37.2	0.037	31.6	0.032	26.
18	.0004	0.065	57.0	0.059	50.9	0.053	44.9	0.047	39.2	0.042	33.7	0.036	28.
19	.0004	0.069	58.4	0.063	52.5	0.058	46.7	0.052	41.2	0.046	35.8	0.040	30.
	.0005						ANTI NE			26		min.	
20	15040	0.074	59.8	0.068	54.0	0.062	48.3	0.057	43.0	0.050	37.8	0.045	32.
21	.0005	0.079	61.0	0.073	55.4	0.067	50.0	0.062	44.7	0.056	39.7	0.050	34.
22	.0005	0.084	62.2	0.078	56.8	0.072	51.5	0.067	46.4	0.061	41.5	0.055	36.
23	.0005	0.089	63.4	0.083	58.1	0.078	52.9	0.072	48.0	0.066	43.3	0.061	38.
24	.0006	0.095	64.4	0.089	59.3	0.083	54.3	0.077	49.6	0.072	44.9	0.066	40.
25	-0006	0.100	65.5	0.095	60.5	0.089	55.6	0.083	51.0	0.078	46.5	0.072	42.
	0006								-				
26	0000	0.106	66.5	0.101	61.7	0.095	56.9	0.089	52.4	0.083	48.0	0.078	43.
27	-0006	0.113	67.5	0.107	62.8	0.101	58.2	0.095	53.8	0.090	49.6	0.084	45.
28	.0007	0.119	68.5	0.113	63.9	0.108	59.4	0.102	55.2	0.096	51.0	0.090	47.
29	.0007	0.126	69.4	0.120	64.9	0.114	60.6	0.108	56.4	0.103	52.4	0.097	48.
30	.0007	0.132	70.3	0.127	65.9	0.121	61.7	0.115	57.7	0.109	53.7	0.104	49.
31		0.139	71.2	0.134	66.9	0.128	62.8	0.122	58.8	0.116	55.0	0.111	51.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

						fference o		SERVICE STATE				).	
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	60.	.0	60	.5	70.	.0	70	.5	80.	.0	80	.5
Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.
0	8,572	Eng. In.		Eng. In.	sing!	Eng. In.	100	Eng. In.	to Art	Eng. In.	mall)	Eng In.	
12	0.0003	0.007	6.8	14.0	1-041	4			15	196 39		SPECIAL S	86.5
13	.0004	0.010	9.9	0.000		100		-010 II 28	FEB.	543		Eugy 1	PEA
14 15	.0004	0.014	12.8 15.7	0.008	7.5	0.006	5.4						27.3
16	.0004	0.018	18.4	0.012	13.3	0.010	8.4				201	806	(5.7)
	.0004	0.022		0.010	10.0	0.010	0.1						
17	.0004	0.026	21.0	0.020	16.0	0.015	11.3	0.009	6.7	10			28
18	.0005	0.030	23.5	0.025	18.6	0.019	14.0	0.013	9.6	0.008	5.3	100	ec.
19	.0005	0.035	25.8	0.029	21.2	0.023	16.6	0.018	12.3	0.012	8.2	0.006	4.2
20 21	.0005	0.040	28.1 30.3	0.034	23.5 25.8	0.028	19.0 21.5	0.022	15.0 17.5	0.017	11.0	0.011	7.1
21	.0005	0.011	30.0	0.059	29.0	0.055	21.0	0.027	17.5	0.022	10.0	0.016	9.0
22	E830 91	0.050	32.3	0.044	28.0	0.038	23.8	0.032	19.8	0.027	16.0	0.021	12.3
23	.0005	0.055	34.2	0.049	30.1	0.043	26.0	0.038	22.1	0.032	18.4	0.026	14.8
24	.0006	0.060	36.1	0.055	32.1	0.049	28.1	0.043	24.4	0.038	20.7	0.032	17.2
25	.0006	0.066	38.0	0.060	34.0	0.055	30.2	0.049	26.5	0.043	23.0	0.038	19.5
26	.0006	0.072	39.8	0.066	35.9	0.061	32.2	0.055	28.6	0.049	25.1	0.043	21.8
27	<b>经生活交易</b>	0.078	41.5	0.073	37.8	0.067	34.0	0.061	30.6	0.055	27.2	0.050	23.9
28	.0006	0.085	43.2	0.079	39.5	0.073	35.9	0.067	32.5	0.062	29.1	0.056	25.9
29	.0007	0.091	44.8	0.085	41.1	0.080	37.6	0.074	34.2	0.068	31.0	0.063	27.9
30	.0007	0.098	46.2	0.092	42.7	0.086	39.2	0.081	35.9	0.075	32.8	0.069	29.7
31	.0001	0.105	47.6	0.099	44.2	0.093	40.8	0.088	37.5	0.082	34.4	0.076	31.4
9.41		90	0	90	K	100		100	· *	110	•	1110	5
		- 3				10	.0	10					
	State 13	Eng. In.	141	Eng. In.	5.41	Eng. In.	5,615	Eng. In.	0034	Eng. In.		Eng. In.	000
20	0.0005	0.005	3.4						111		,	100	
21	.0005	0.010	6.1	0.005	2.7	0.00	0.0	BREW	N. P.	17 199	H.		
22	.0005	0.015	8.8	0.010	5.4	0.004	2.2		and the	经生活			
23	.0005	0.021	11.4	0.015	8.0	0.009	4.9 7.5	0.009	4.5	79.9.18		1	
25	.0006	0.020	16.2	0.026	13.1	0.020	10.0	0.005	7.1	0.009	4.2		
	.0006	0.502										100	
26	E10.013	0.038	18.5	0.032	15.4	0.026	12.4	0.021	9.5	0.015	6.8	0.009	4.1
27	.0006	0.044	20.7	0.038	17.7	0.032	14.7	0.027	11.9	0.021	9.2	0.015	6.5
28	.0007	0.050	22.8	0.045	19.9	0.039	16.9	0.033	14.2	0.027	11.5	0.022	8.9
29 30	.0007	0.057	24.9 26.7	0.051	21.9	0.045	19.0 21.0	0.040	16.3 18.4	0.034	13.7	0.028	11.1
31	.0007	0.004	28.5	0.065	25.7	0.052	22.9	0.053	20.3	0.041	17.8	0.035	15.3
		0.071	20.0	0.000		0.300		0.000	20.0	0.040	10	0.042	10.0
	4	Mea	n Horiz	contal Dif	ference	of Force	of Vap	or for eac	h 0°.1	= 0.0012.			

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

THE A	M	Annto-		t-t	, or Di	fference o	f Wet a	and Dry I	Bulb Th	ermomet	ers.		
Wet- Bulb hermo- meter	Mean Vertical Difference of Force of Vapor	00.	0	00.	5	10.	0	10.	5	20.	0	20.	.5
ahren- heit.	for each 00.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu mid ity
0	ay table	Eng. In.		Eng. In.	Jen Ki	Eng. In.	100	Eng. In.		Eng. In.	100	Eng. In.	-
32	0.0007	0.181	100	0.175	94.5	0.168	89.3	0.162	84.1	0.155	79.2	0.149	74.
33	.0008	0.188	100	0.182	94.7	0.175	89.5	0.169	84.5	0.162	79.7	0.156	75.
34	.0008	0.196	100	0.189	94.8	0.183	89.8	0.176	84.9	0.170	80.2	0.163	75
35	.0008	0.204	100	0.197	94.9	0.191	90.0	0.184	85.3	0.178	80.7	0.171	76
36	.0008	0.212	100	0.205	95.0	0.199	90.3	0.192	85.6	0.186	81.1	0.179	76
	.0009			- 3	- 450							10-10	
37	.0009	0.220	100	0.214	95.2	0.207	90.5	0.201	86.0	0.194	81.6	0.188	77
38	.0009	0.229	100	0.223	95.3	0.216	90.7	0.210	86.3	0.203	82.0	0.196	77
39	.0009	0.238	100	0.232	95.4	0.225	91.0	0.219	86.6	0.212	82.4	0.206	78
40	.0010	0.248	100	0.241	95.5	0.235	91.2	0.228	86.9	0.221	82.9	0.215	78
41	.0010	0.257	100	0.251	95.6	0.244	91,4	0.238	87.3	0.231	83.3	0.224	79
42	.0010	0.267	100	0.260	95.7	0.254	91.6	0.247	87.5	0.241	83.6	0.234	79
43	.0010	0.278	100	0.271	95.8	0.264	91.8	0.258	87.8	0.251	84.0	0.245	80
44	.0011	0.288	100	0.282	95.9	0.275	92.0	0.268	88.1	0.262	84.3	0.255	80
	.0011	0.299	100	0.293	96.0	0.286	92.1	0.280	88.3	0.273	84.7	0.266	81
45	.0011	0.311	100	0.304	96.1	0.297	92.3	0.291	88.6	0.284	85.0	0.278	81
40	.0012	0.511	100	0.004	30.1	0.231	92.0	0.231	00.0	0.204	00.0	0.210	01
47	tion AT a	0.323	100	0.316	96.2	0.310	92.5	0.303	88.8	0.297	85.3	0.290	81
48	.0012	0.335	100	0.329	96.2	0.322	92.6	0.315	89.0	0.309	85.6	0.302	82
49	.0013	0.348	100	0.341	96.3	0.335	92.7	0.328	89.3	0.321	85.9	0.315	82
50	.0013	0.361	100	0.354	96.4	0.348	92.9	0.341	89.5	0.334	86.1	0.328	82
51	.0013	0.374	100	0.368	96.5	0.361	93.0	0.354	89.7	0.348	86.4	0.341	83
01	.0014		100	0,000	20.0	0.001	00.0	0.001	00	0.010	00.1	0.011	-
52		0.388	100	0.382	96.5	0.375	93.2	0.369	89.9	0.362	86.7	0.355	83
53	.0014	0.403	100	0.396	96.6	0.389	93.3	0.383	90.1	0.376	86.9	0.370	83
54	.0015	0.418	100	0.411	96.7	0.404	93.4	0.398	90.2	0.391	87.2	0.385	84
55	.0015	0.433	100	0.426	96.7	0.420	93.5	0.413	90.4	0.407	87.4	0.400	84
56	-0016	0.449	100	0.442	96.8	0.436	93.6	0.429	90.6	0.422	87.6	0.416	84
1	.0016			er char	1 3	CHIEN	1	Kuinu	111		Yang j	100	Vis
57		0.466	100	0.459	96.8	0.452	93.7	0.446	90.7	0.439	87.8	0.432	85
58	.0017	0.482	100	0.476	96.9	0.469	93.9	0.463	90.9	0.456	88.0	0.449	85
59	-0017	0.500	100	0.493	96.9	0.487	94.0	0.480	91.0	0.473	88.2	0.467	85
60	.0018	0.518	100	0.511	97.0	0.505	94.1	0.498	91.2	0.491	88.4	0.485	85
61	.0019	0.537	100	0.530	97.0	0.523	94.2	0.517	91.3	0.510	88.6	0.503	85
62	.0019	0.556	100	0.549	07.3	0 5 10	010	0 500	01 -	0.590	99.0	0.522	86
	.0020	0.576		72 125 125	97.1	0.542	94.2	0.536	91.5	0.529	88.8	0.542	86
63 64	.0020	0.596	100	0.569	97.1	0.562	94.3	0.556	91.6	0.549	89.0	0.542	86
	.0021	0.596	100	0.589	97.2	0.583	94.4	0.576	91.7	0.569	89.1	600000000000000000000000000000000000000	1000
65	.0022	0.639	100	0.611	97.2	0.604	94.5	0.597	91.9	0.591	89.3	0.584	86
66	•0023	0.662	100	0.633	97.3	0.626	94.6	0.619	92.0	0.612	89.5	0.606	87
67		0.002	100	0.655	97.3	0.648	94.7	0.642	92.1	0.635	89.6	0.628	87.

Temperature, Fahrenheit. — Force of Vapor in English Inches — Relative Humidity in Hundredths.

		A (8.5%)		t - 1	t', or Di	fference o	of Wet	and Dry	Bulb T	hermome	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	0°.	0	00.	.5	6.1%	.0	10	.5	20.	.0	20	.5
Fahren- heit.	for each 00.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.	ve.	Eng. In.	7	Eng. In.		Eng. In.		Eng In.	
68	0.0023	0.685	100	0.678	97.3	0.671	94.7	0.665	92.2	0.658	89.8	0.651	87.3
69	.0024	0.708	100	0.702	97.4	0.695	94.8	0.688	92.3	0.682	89.9	0.675	87.5
70	.0025	0.733	100	0.726	97.4	0.720	94.9	0.713	92.4	0.706	90.0	0.699	87.7
71 72	.0026	0.758	100	0.752	97.5	0.745	95.0	0.738	92.5	0.731	90.2	0.725	87.9
12	.0027	0.704	100	0.778	97.5	0.771	95.0	0.764	92.7	0.757	90.3	0.751	88.0
73	HOR TO	0.811	100	0.805	97.5	0.798	95.1	0.791	92.7	0.784	90.4	0.778	88.2
74	.0028	0.839	100	0.832	97.6	0.826	95.2	0.819	92.8	0.812	90.6	0.805	88.3
75	.0028	0.868	100	0.861	97.6	0.854	95.2	0.847	92.9	0.841	90.7	0.834	88.5
76	.0030	0.897	100	0.890	97.6	0.883	95.3	0.877	93.0	0.870	90.8	0.863	88.6
77		0.927	100	0.920	97.7	0.914	95.4	0.907	93.1	0.900	90.9	0.893	88.8
	.0031												
78	.0032	0.958	100	0.951	97.7	0.945	95.4	0.938	93.2	0.931	91.0	0.924	88.9
79	.0033	0.990	100	0.983	97.7	0.977	95.5	0.970	93.3	0.963	91.1	0.956	89.0
80	.0034	1.023	100	1.016	97.7	1.010	95.5	1.003	93.4	0.996	91.2	0.989	89.2
81	.0035	1.057	100	1.050	97.8	1.044	95.6	1.037	93.4	1.030	91.3	1.023	89.3
82	.0036	1.092	100	1.085	97.8	1.079	95.6	1.072	93.5	1.065	91.4	1.058	89.4
83	.0030	1.128	100	1.121	97.8	1.115	95.7	1.108	93.6	1.101	91.5	1.094	89.5
84	.0037	1.165	100	1.158	97.8	1.152	95.7	1.145	93.6	1.138	91.6	1.131	89.6
85	.0038	1.203	100	1.196	97.9	1.189	95.8	1.183	93.7	1.176	91.7	1.169	89.7
86	.0039	1.242	100	1.235	97.9	1.228	95.8	1.222	93.8	1.215	91.8	1.208	89.8
87	-0040	1.282	100	1.275	97.9	1.268	95.9	1.263	93.8	1.256	91.9	1.249	90.0
	.0041						11	in a				357	
88	.0042	1.323	100	1.317	97.9	1.310	95.9	1.303	93.9	1.296	92.0	1.289	90.1
89	.0044	1.366	100	1.359	97.9	1.352	95.9	1.345	94.0	1.339	92.0	1.332	90.2
90	.0045	1.410	100	1.403	98.0	1.396	96.0	1.389	94.0	1.382	92.1	1.375	90.3
91	.0046	1.455	100	1.448	98.0	1.441	96.0	1.434	94.1	1.427	92.2	1.420	90.3
92	1870.10	1.501	100	1.494	98.0	1.487	96.1	1.480	94.1	1.473	92.3	1.466	90.4
93	•0048	1.548	100	1.541	98.0	1.535	96.1	1.528	94.2	1.521	92.4	1.514	90.5
94	.0049	1.545	100	1.590	98.1	1.583	96.1	1.576	94.3	1.569	92.4	1.562	90.6
95	.0050	1.647	100	1.640	98.1	1.633	96.2	1.626	94.3	1.619	92.4	1.612	90.7
96	.0051	1.698	100	1.691	98.1	1.684	96.2	1.677	94.4	1.670	92.6	1.664	90.8
97	.00å3	1.751	100	1.744	98.1	1.739	96.2	1.730	94.4	1.723	92.6	1.716	90.9
98	.0054	1.805	100	1.798	98.1	1.791	96.3	1.784	94.5	1.777	92.7	1.770	90.9
Ey-	.0056				013	10 140	WH	193 15	844				30.0
99		1.861	100	1.854	98.1	1.847	96.3	1.840	94.5	1.833	92.8	1.826	91.0
100	-0057	1,918	100	1.911	98.2	1.904	96.3	1.897	94.6	1.890	92.8	1.883	91.1
101	.0059 .0060	1.977	100	1.970	98.2	1.963	96.4	1.956	94.6	1.949	92.9	1.942	91.2
102	.0060	2.037	100	2.030	98.2	2.023	96.4	2.016	94.7	2.009	92.9	2.002	91.2
103	.0062	2.098	100	2.092	98.2	2.085	96.4	2.078	94.7	2.071	93.0	2.064	91.3
104	.0003	2.162	100	2.155	98.2	2.148	96.5	2.141	94.7	2.134	93.1	2.127	91.4

Mean Horizontal Difference of Force of Vapor for each 00.1 = 0.0013.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

		STHERE		t-1	t', or D	ifference	of Wet	and Dry	Bulb T	hermome	ters.		
Wet- Bulb hermo- meter	Mean Vertical Difference of Force of Vapor	3°.	0	3°.	.5	40.	0	4°.	5	5°.	0	<b>5</b> °.	.5
ahren- heit.	for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu mid ity
0	1000	Eng. In.	CO.	Eng. In.		Eng. In.		Eng. In.		Eng. In.	A.C.	Eng. In.	
32	0.0007	0.142	69.8	0.136	65.3	0.129	61.0	0.123	56.8	0.116	52.7	0.110	48.
33	.0007	0.149	70.5	0.143	66.1	0.136	61.9	0.130	57.7	0.123	53.7	0.117	50.
34	.0008	0.157	71.2	0.150	66.9	0.144	62.8	0.137	58.6	0.131	54.7	0.124	51.
35	.0008	0.165	71.9	0.158	67.7	0.152	63.6	0.145	59.5	0.139	55.7	0.132	52
36	27/1627	0.173	72.6	0.166	68.5	0.160	64.5	0.153	60.5	0.147	56.7	0.140	53
37	.0008	0.181	73.2	0.175	69.2	0.168	65.3	0.162	61.4	0.155	57.7	0.149	54
38	•0009	0.190	73.8	0.175	69.9	0.108	66.1	0.102	62.3	0.164	58.7	0.145	55
39	.0009	0.190	74.4	0.192	70.6	0.186	66.9	0.179	63.2	0.173	59.7	0.166	56
40	•0010	0.208	75.0	0.202	71.3	0.195	67.7	0.189	64.1	0.182	60.7	0.176	57
41	.0010	0.218	75.6	0.211	72.0	0.205	68.4	0.198	65.0	0.192	61.7	0.185	58
7.4	.0010	0.210	.0.0	0.211		0.200	0001	0.100	00.0	0.102			
42	2010	0.228	76.2	0.221	72.6	0.215	69.1	0.208	65.7	0.202	62.4	0.195	59
43	.0010	0.238	76.7	0.232	73.2	0.225	69.8	0.219	66.3	0.212	63.1	0.205	60
44	.0011	0.249	77.2	0.242	73.7	0.236	70.4	0.229	67.0	0.223	63.8	0.216	61
45	.0011	0.260	77.7	0.253	74.3	0.247	71.0	0.240	67.6	0.234	64.6	0.227	61
46	.0011	0.271	78.1	0.265	74.8	0.258	71.6	0.252	68.3	0.245	65.3	0.238	62
	.0012		12.00	La Bus		and an		and was		· Marie	118	OF SERVICE	-
47	.0012	0.283	78.6	0.277	75.3	0.270	72.2	0.264	68.9	0.257	66.0	0.250	63.
48	.0013	0.296	79.0	0.289	75.8	0.282	72.7	0.276	69.6	0.269	66.7	0.263	64
49	.0013	0.308	79.4	0.302	76.3	0.295	73.3	0.288	70.2	0.282	67.4	0.275	64.
50	.0013	0.321	79.8	0.315	76.7	0.308	73.8	0.301	70.9	0.295	68.1	0.288	65.
51	•0014	0.335	80.2	0.328	77.2	0.321	74.3	0.315	71.4	0.308	68.7	0.302	66
52	ESCHOOL SECTION	0.349	80.5	0.342	77.6	0.335	74.7	0.329	71.9	0.322	69.2	0.315	66
53	-0014	0.363	80.9	0.356	78.0	0.350	75.2	0.343	72.5	0.336	69.8	0.330	67
54	-0015	0.378	81.2	0.371	78.4	0.365	75.6	0.358	72.9	0.351	70.3	0.345	67
55	-0015	0.393	81.6	0.387	78.8	0.380	76.1	0.373	73.4	0.367	70.8	0.360	68
56	-0016	0.409	81.9	0.403	79.1	0.396	76.5	0.389	73.9	0.383	71.3	0.376	68
-	-0016				S. K.	au linu	11.3	40.00		- office			-
57	.0017	0.426	82.2	0.419	79.5	0.412	76.9	0.406	74.3	0.399	71.8	0.392	69.
58	-0017	0.443	82.5	0.436	79.8	0.429	77.2	0.423	74.8	0.416	72.3	0.409	69
59	.0018	0.460	82.8	0.453	80.2	0.447	77.6	0.440	75.1	0.433	72.7	0.427	70
60	.0019	0.478	83.1	0.471	80.5	0.465	78.0	0.458	75.5	0.451	73.1	0.445	70
61		0.497	83.3	0.490	80.8	0.483	78.3	0.477	75.9	0.470	73.5	0.463	71
62	.0019	0.516	83.6	0.509	81.1	0.502	78.6	0.496	76.3	0.489	74.0	0.482	71
63	.0020	0.536	83.8	0.529	81.4	0.502	79.0	0.490	76.6	0.409	74.3	0.502	72
64	.0020	0.556	84.1	0.549	81.7	0.543	79.0	0.536	77.0	0.529	74.7	0.523	72
65	.0021	0.577	84.3	0.570	81.9	0.564	79.6	0.557	77.3	0.550	75.1	0.544	72
66	.0022	0.599	84.6	0.592	82.2	0.586	79.9	0.579	77.6	0.572	75.4	0.566	73
67	.0023	0.622	84.8	0.615	82.4	0.608	80.2	0.601	78.0	0.595	75.8	0.588	73
0.	terlali	0.022	04.0	0.019	02.4	0.000	30.2	0.001	10.0	0.000		3.000	

Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.0013$ .

#### PSYCHROMETRI CAL TABLES.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

Decision   Port   Por					t-t	', or Di	ifference o	of Wet	and Dry	Bulb Tl	hermomet	ers.		
Relation of Force   Febrush   Force of Hundre	Bulb	Vertical	O. Feet				70 m		2		es vo			
Part		of Force	3°.	0	3 °.	5	40.	0	40.	5	5°.	0	50.	5
	t'	of Vapor		Dala		D.1-		Dala		Dela		Dala	-	D-1-
			3		1000						1	tive	300	Rela
						Hu-								Hu
Color   Colo	37 1	1.0	vapor.		vapor.		rapor.	ity.	vapor.		vapor.		vapor.	mid ity.
68	0		Eng. In.	19 G	Eng. In.		Eng. In.	0.8	Eng. In.	V-	Eng. In.		Eng. In.	4
99		0.0004		85.0		82.7		80.4		78.3		76.1	0.611	74.
70	69	COLUMNS	0.668	85.2	0.661	82.9	0.655	80.7	0.648	78.6	0.641	76.4	0.635	74.
72	70	7. SEC. 18. C.	0.693	85.4	0.686	83.2	0.679	81.0	0.672	78.8	0.666	76.8	0.659	74.
72         .0086         0.744         85.8         0.737         83.6         0.731         81.5         0.724         79.4         0.718         77.4         0.710         7           73         .0028         0.771         86.0         0.764         83.8         0.757         81.7         0.751         79.7         0.744         77.6         0.737         7           74         .0029         0.856         86.3         0.820         84.2         0.781         82.2         0.807         89.2         0.779         0.765         7         9         0.772         77.9         0.765         7         0.030         0.856         86.5         0.880         84.2         0.814         82.2         0.807         80.2         0.800         78.2         0.793         7         0.030         0.887         86.7         0.880         84.6         0.873         82.6         0.866         80.6         0.860         78.7         0.823         7         0.881         0.033         0.998         87.1         0.976         85.1         0.969         81.3         0.995         78.9         0.884         7         0.949         81.5         0.969         81.3         0.955         79.4	1325/113	C . C . C . C . C	12011 22111	85.6	0.711		0.704	81.2	0.698	79.1	0.691	77.1	0.684	75.
73         .0028         0.771         86.0         0.764         83.5         0.757         81.7         0.751         79.7         0.744         77.6         0.737         7           74         .0028         0.799         86.2         0.792         84.0         0.785         81.9         0.778         79.9         0.772         77.9         0.765         7         7         0.039         0.856         86.5         0.850         84.4         0.843         82.4         0.836         80.4         0.829         78.4         0.823         7         0.033         0.988         86.7         0.880         84.6         0.873         82.6         0.866         80.6         0.860         78.7         0.853         7         0.918         86.8         0.911         84.5         0.904         82.8         0.897         80.8         0.890         78.9         0.884         0.892         79.0         0.943         85.0         0.994         87.0         0.943         85.0         0.996         83.2         0.962         81.1         0.992         81.1         0.992         79.2         0.916         8         0.982         83.1         0.998         89.1         0.992         99.1	S. E. Street, S.	.0026	12 5 Part 1	85.8	0.737		SEL CHARLE	81.5	0.724	79.4	0.718	77.4	0.710	75.
74         .0038		.0027										1.00	Ø(0.4	
74	73	0020	0.771	86.0	0.764	83.8	0.757	81.7	0.751	79.7	0.744	77.6	0.737	75.
75         .0028	74	23.7 E20.0P10.7	0.799	86.2	0.792	84.0	0.785	81.9	0.778	79.9	0.772	77.9	0.765	76.
76         .0039         0.856         86.5         0.850         84.4         0.843         82.4         0.836         80.4         0.829         78.4         0.823         78.7         0.830         84.6         0.873         82.6         0.866         80.6         0.860         78.7         0.853         3           78         .0031         0.918         86.8         0.911         84.8         0.904         82.8         0.897         80.8         0.890         78.9         0.884         7         0.919         87.0         0.943         85.0         0.936         83.0         0.929         81.1         0.922         79.2         0.916         78.9         0.884         2.0962         81.3         0.955         79.4         0.949         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982         79.7         0.982	75	E112-14-14-15-7	0.827	86.3	0.820	84.2	0.814	82.2	0.807	80.2	0.800	78.2	0.793	76.
77         .0030 .0031         0.887         86.7         0.880         84.6         0.873         82.6         0.866         80.6         0.860         78.7         0.853         3           78         .0031         0.918         86.8         0.911         84.8         0.904         82.8         0.897         80.8         0.890         78.9         0.884           79         .0033         0.949         87.0         0.943         85.0         0.936         83.0         0.929         81.1         0.922         79.2         0.916         6           81         .0034         1.016         87.3         1.010         85.3         1.003         83.4         0.996         81.5         0.989         79.7         0.982         7           82         .0035         1.051         87.4         1.045         85.5         1.038         83.6         1.031         81.7         1.024         79.9         1.017           83         .0036         1.051         87.4         1.045         85.5         1.038         83.6         1.031         81.7         1.024         79.9         1.017           84         .0037         1.242         87.5         1.177	19890 7 1	100000000000000000000000000000000000000	0.856	86.5	0.850	84.4	0.843	82.4	0.836	80.4	0.829	78.4	0.823	76.
78         .0031         0.918         86.8         0.911         84.8         0.904         82.8         0.897         80.8         0.890         78.9         0.884         78.0         0.943         85.0         0.936         83.0         0.929         81.1         0.922         79.2         0.916         38.0         0.982         87.1         0.976         85.1         0.969         83.2         0.962         81.3         0.955         79.4         0.949         93.2         0.962         81.3         0.955         79.4         0.949         93.2         0.962         81.3         0.955         79.4         0.949         93.2         0.962         81.3         0.955         79.4         0.949         93.2         0.962         81.5         0.989         79.7         0.982         20.962         81.9         1.080         80.3         1.091         1.080         80.3         1.099         80.3         1.091         1.096         80.3         1.091         1.096         80.3         1.090         80.3         1.099         80.3         1.090         80.3         1.090         80.3         1.090         80.3         1.090         80.3         1.090         80.3         1.090         80.3         <	10000000	•0030	CE11 - SECT A	86.7	0.880	84.6	0.873	82.6	0.866	80.6	0.860	78.7	0.853	76.
78         .0082         0.918         86.8         0.911         84.8         0.904         82.8         0.897         80.8         0.890         78.9         0.884         5         0.936         83.0         0.929         81.1         0.922         79.2         0.916         7         0.916         7         0.916         7         0.916         7         0.916         7         0.916         7         0.916         7         0.916         7         0.916         7         0.916         7         0.916         7         0.916         7         0.92         9.71         0.976         85.1         0.969         83.2         0.962         81.3         0.955         79.4         0.949         7         0.982         7         0.982         7         0.982         7         0.982         7         0.982         7         0.942         1.051         87.4         1.045         85.5         1.038         83.4         0.996         81.5         0.989         79.7         0.982         7         0.982         7         0.982         7         0.982         7         0.982         7         0.982         7         0.982         7         0.982         7         0.982		.0031			N/Stab				1			1 2	10-14	
79         .0033         0.949         87.0         0.943         85.0         0.936         83.0         0.929         81.1         0.922         79.2         0.916         79.2         0.916         81         0.0034         1.016         87.3         1.010         85.3         1.003         83.4         0.996         81.5         0.989         79.7         0.982         81.3         1.082         82.0         1.017	78	84 X 18 X	0.918	86.8	0.911	84.8	0.904	82.8	0.897	80.8	0.890	78.9	0.884	77.
80         .0034 .0034 81         0.982 .0035         87.1 1.016         0.976 85.3         85.1 1.003         0.969 83.4         83.2 0.962         0.962 	100000117	DOLLAR SHEET	FBCS URD B	87.0	0.943	85.0	0.936	83.0	0.929	81.1	0.922	79.2	0.916	77.
81       .0034	1000000	NEWSPERSON.	CONTRACTOR IN	87.1	0.976	85.1	0.969	83.2	0.962	81.3	0.955	79.4	0.949	77.
82       .0035       1.051       87.4       1.045       85.5       1.038       83.6       1.031       81.7       1.024       79.9       1.017       7         83       .0037       1.124       87.7       1.117       85.8       1.111       83.7       1.067       81.9       1.060       80.1       1.053       3         85       .0039       1.162       87.8       1.155       85.9       1.148       84.1       1.142       82.3       1.135       80.5       1.128       3         87       .0040       1.242       88.1       1.235       86.2       1.228       84.4       1.222       82.6       1.215       80.9       1.208       7         88       .0041       1.282       88.2       1.276       86.3       1.269       84.6       1.262       82.8       1.255       81.1       1.248       7         89       .0042       1.325       88.3       1.318       86.5       1.311       84.7       1.304       83.0       1.297       81.3       1.291       7         90       .0044       1.369       88.4       1.362       86.6       1.355       84.9       1.348       83.1       1.341<	100000	120000000000000000000000000000000000000	420 1150 1	12000 To 1	NAME OF TAXABLE PARTY.		Vi. 20, 1955 in		Land 5 1 1 10		1 to 12 to 1			77.
83	DESCRIPTION OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TW	.0035	SECTION.	1516 (0.7)	S-1437.E.S.	ACC 25-11	100 CH 510 CH		3 1 3 4 5		A STREET, STREET,			78.
83       .0037       1.087       87.5       1.080       85.6       1.074       83.7       1.067       81.9       1.060       80.1       1.053       7         85       .0038       1.124       87.7       1.117       85.8       1.111       83.9       1.104       82.1       1.096       80.3       1.090       7         86       .0039       1.201       87.9       1.194       86.1       1.187       84.2       1.181       82.4       1.174       80.7       1.167       7         87       .0040       1.242       88.1       1.235       86.2       1.228       84.4       1.222       82.6       1.215       80.9       1.208       7         89       .0041       1.232       88.2       1.276       86.3       1.269       84.6       1.262       82.8       1.255       81.1       1.248       7         90       .0042       1.325       88.3       1.318       86.5       1.311       84.7       1.304       83.0       1.297       81.3       1.291       7         91       .0045       1.413       88.5       1.407       86.7       1.400       85.0       1.348       83.1       1.341<	02	.0036	1.001	0111	1.010	00.0	1.000		1.001	0101	1.021			
84         .0037	83	10 10 10	1.037	87.5	1.080	85.6	1.074	83.7	1.067	81.9	1.060	80.1	1.053	78.
85         .0038	120000000000000000000000000000000000000	.0037	CONTRACTOR AND ADDRESS OF	DHAL	WITH THE REAL PROPERTY.			83.9	1.104	82.1	1.096	80.3	1.090	78.
86         .0039         1.201         87.9         1.194         86.1         1.187         84.2         1.181         82.4         1.174         80.7         1.167         7           87         .0040         1.242         88.1         1.235         86.2         1.228         84.4         1.222         82.6         1.215         80.9         1.208         7           88         .0041         1.232         88.2         1.276         86.3         1.269         84.6         1.262         82.8         1.255         81.1         1.248         7           90         .0044         1.369         88.4         1.362         86.6         1.355         84.9         1.348         83.0         1.297         81.3         1.291         7           91         .0045         1.413         88.5         1.407         86.7         1.400         85.0         1.393         83.3         1.386         81.6         1.379         8           92         .0047         1.507         88.7         1.500         87.0         1.493         85.3         1.486         83.6         1.432         81.8         1.425         8           93         1.507         88.7 </td <td>DESCRIPTION OF THE PERSON OF T</td> <td>.0038</td> <td>16.75 ( 10.05 ( 6.7)</td> <td>2010 20</td> <td>95.41112.633</td> <td></td> <td>10.002100</td> <td></td> <td>DO TO HINCO</td> <td></td> <td>BULL STREET</td> <td></td> <td>CANADA SELECTION</td> <td>78.</td>	DESCRIPTION OF THE PERSON OF T	.0038	16.75 ( 10.05 ( 6.7)	2010 20	95.41112.633		10.002100		DO TO HINCO		BULL STREET		CANADA SELECTION	78.
87         .0040         1.242         88.1         1.235         86.2         1.228         84.4         1.222         82.6         1.215         80.9         1.208         7           88         .0041         1.282         88.2         1.276         86.3         1.269         84.6         1.262         82.8         1.255         81.1         1.248         7           90         .0044         1.325         88.3         1.318         86.5         1.311         84.7         1.304         83.0         1.297         81.3         1.291         7           91         .0045         1.369         88.4         1.362         86.6         1.355         84.9         1.348         83.1         1.341         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.334         81.4         1.4	43.74E   14	.0039	Section and the second	30 G 31L	CAT IN TAXABLE				Contract of the contract of th			21/2/2007		79.
88	4000 127	•0040	45) 22 Rein 25	260991302	120 D40 521		NE E-126.1		DR 7. DE 607		D 1.9(00)	(1) B > 200	N - 21	79.
88       1.282       88.2       1.276       86.3       1.269       84.6       1.262       82.8       1.255       81.1       1.248       7         89       .0044       1.325       88.3       1.318       86.5       1.311       84.7       1.304       83.0       1.297       81.3       1.291       7         90       .0045       1.369       88.4       1.362       86.6       1.355       84.9       1.348       83.1       1.341       81.4       1.334       7         91       .0046       1.460       88.6       1.453       86.9       1.446       85.0       1.393       83.3       1.386       81.6       1.379       8         93       .0047       1.507       88.7       1.500       87.0       1.493       85.3       1.486       83.6       1.480       82.0       1.473       8         94       .0049       1.556       88.8       1.549       87.1       1.542       85.4       1.535       83.8       1.528       82.1       1.473       8         95       .0050       1.666       88.9       1.599       87.2       1.592       85.5       1.585       83.9       1.578       82.3 </td <td>01</td> <td>0041</td> <td>1.244</td> <td>00.1</td> <td>1.200</td> <td>00.2</td> <td>1.220</td> <td>0.4.4</td> <td>1.222</td> <td>04.0</td> <td>1.210</td> <td>00.5</td> <td>1.200</td> <td></td>	01	0041	1.244	00.1	1.200	00.2	1.220	0.4.4	1.222	04.0	1.210	00.5	1.200	
89         .0042         1.325         88.3         1.318         86.5         1.311         84.7         1.304         83.0         1.297         81.3         1.291         7           90         .0044         1.369         88.4         1.362         86.6         1.355         84.9         1.348         83.1         1.341         81.4         1.334         7           91         .0045         1.413         88.5         1.407         86.7         1.400         85.0         1.393         83.3         1.386         81.6         1.379         8           92         .0046         1.460         88.6         1.453         86.9         1.446         85.1         1.439         83.4         1.432         81.8         1.425         8           93         .0047         1.556         88.7         1.500         87.0         1.493         85.3         1.486         83.6         1.480         82.0         1.473         8           95         .0050         1.666         88.9         1.599         87.2         1.592         85.5         1.585         83.9         1.578         82.3         1.571         8           96         .0051         1.667<	88	.0041	1.282	88.2	1.276	86.3	1.269	84.6	1.262	82.8	1.255	81.1	1.248	79.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4000	.0042	A	LEDYS TILL	TALES BUSINESS		Market 19 11				1	0.000		79.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	900001-1-3	.0044		30/9/35			Jan Control		CL DODGER		0.00	THE COST		79.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CONTRACTOR OF THE PARTY OF THE	.0045	SECTION 1.15 TO 100 TO	STREET, STATE OF		A 100 To	THE RESERVE					CORPORATION	10 A 11 TO 12	80.0
93	Marie Control	.0046	120 0 220	100 C			10-11-050-07		SAY STATE		COLUMN TO SERVICE STATE OF THE PARTY OF THE	1200 1000	(125-1267-1	80.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	34	0047	1.400	00.0	1.400	00.9	1.440	30.1	1.400	00.4	1.402	01.0	1.720	20.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	93	•0047	1.507	88.7	1.500	87.0	1.493	85.3	1.486	83.6	1.480	82.0	1.473	80.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	SCREET, 1	.0019	100 F COLOR C	2011.15	800 S L 702 S L		DRAW GROUN		100 1100 17			1100 110		80.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	100000000000000000000000000000000000000	.0050	Control of the Contro	40000			10 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	2016-2017	A CONTRACTOR	1011011	THE PARTY OF THE	COLD AND A		80.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.000	.0051	COLUMN TO A STATE OF	23750	25.5 (6.20 (6.5)				The best of the		0.000	THE OWNER	ALC: NO. 1	80.
98	COLUMN TO SERVICE SERV	.0052	335-1150-0-3	1150 to 1	CARL COLORS		428-140-353-3L		DOMESTIC STREET,		1335 7003	124	5300 1 SEC. 14	81.6
99		.0054	STATE OF STREET	18 1		.61	1 11 11 11 11 11				24.	100	Control of the Control	81.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	30		1.704	03.4	1.797	81.0	1.750	00.0	1.749	0.4.0	1.100	02.1	1.123	01.
100     -0087     1.876     89.4     1.869     87.8     1.863     86.2     1.856     84.6     1.849     83.0     1.842     8       101     -0068     1.935     89.5     1.928     87.9     1.921     86.3     1.914     84.7     1.907     83.2     1.900     8       102     -0060     1.995     89.6     1.988     88.0     1.981     86.4     1.974     84.8     1.967     83.3     1.961     8       103     -0062     2.057     89.7     2.050     88.1     2.043     86.5     2.036     84.9     2.029     83.4     2.022     8	99	.0055	1.819	89.3	1.812	87.7	1.805	86.0	1.798	84.4	1.792	S2.9	1.785	81.
101 -0068 1.935 89.5 1.928 87.9 1.921 86.3 1.914 84.7 1.907 83.2 1.900 8 102 -0060 1.995 89.6 1.988 88.0 1.981 86.4 1.974 84.8 1.967 83.3 1.961 8 103 -0062 2.057 89.7 2.050 88.1 2.043 86.5 2.036 84.9 2.029 83.4 2.022 8	STATE SHE	-0057	A CONTRACTOR OF THE PARTY OF TH	437.37.3	WITH SHEET		100 100		VIII 10 10		0.000		CONTRACTOR OF	81.
102   .0060   1.995   89.6   1.988   88.0   1.981   86.4   1.974   84.8   1.967   83.3   1.961   81.0062   2.057   89.7   2.050   88.1   2.043   86.5   2.036   84.9   2.029   83.4   2.022   2.022   2.022   2.022   2.022   2.022   2.022   2.022   2.022   2.022   2.022   2.022   2.022   2.022	THE RESERVE AND ADDRESS.	.0058	COLUMN TO SERVICE	100 E 25 J	ELECTION OF						The William	1200	THE RESERVE OF	81.
103   .0062   2.057   89.7   2.050   88.1   2.043   86.5   2.036   84.9   2.029   83.4   2.022   8	Name and Address of the Owner, where the Owner, which is the Own	.0060	100 DO DO DO	352,000	100-104(-15)		52 3 TO 2 A		Mr. Branchine		CHARLES OF	A	2011/12/11	81.8
ongo l	12000-0	.0062		32 A Sec. 1	CO SUPERIOR		1500 1000				I 2500	College Street	ALL PROPERTY.	81.5
	103	.0063	2.057	89.8	2.030	88.2	2.106	86.6	2.099	85.1	2.029	83.5	2.022	82.

Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.0013$ .

Temperature, Fahrenheit. - Force of Vapor in English Inches. - Relative Humidity in Hundredths

Wet- Bulb Thermo- meter t' Fahren- heit.	Mean Vertical Difference of Force of Vapor for each 0°.1.	$\mathbf{t} - \mathbf{t}',$ or Difference of Wet and Dry Bulb Thermometers.												
		6°.0		6°.5		70.0		70.5		80.0		80.5		
		Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hunidity	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid ity.	
0		Eng. In.		Eng. In.	917	Eng. In.		Eng. In.		Eng. In.	01.0	Eng. In.	00	
32	0.0007	0.103	45.0	0.097	41.4	0.090	37.9	0.084	34.5	0.077	31.2 32.8	0.071	28. 29.	
33	.0007	0.110	46.3	0.104	42.7	0.097	39.3	0.091	36.0 37.4	0.084	34.3	0.075	31.	
35	.0008	0.118	48.8	0.111	45.3	0.103	42.0	0.106	38.8	0.100	35.7	0.093	32.	
36	.0008	0.134	50.0	0.127	46.6	0.121	43.3	0.114	40.2	0.108	37.2	0.101	34.	
37	.0009	0.142	51.1	0.136	47.8	0.129	44.6	0.123	41.6	0.116	38.6	0.109	35.	
38	.0009	0.151	52.2	0.144	49.0	0.138	45.9	0.131	42.9	0.125	40.0	0.118	37.	
39	.0009	0.160	53.3	0.153	50.1	0.147	47.1	0.140	44.1	0.134	41.3	0.127	38.	
40	.0010	0.169	54.3	0.163	51.3	0.156	48.3	0.149	45.4	0.143	42.6	0.136	39.	
41	.0010	0.179	55.4	0.172	52.3	0.166	49.4	0.159	46.6	0.153	43.9	0.146	41.	
42	200	0.189	56.3	0.182	53.4	0.175	50.5	0.169	47.7	0.162	45.0	0.156	42.	
43	.0010	0.199	57.2	0.192	54.3	0.186	51.5	0.179	48.8	0.173	46.1	0.166	43.	
44	.0011	0.209	58.1	0.203	55.3	0.196	52.5	0.190	49.8	0.183	47.2	0.177	44.	
45	.0011	0.220	59.0	0.214	56.2	0.207	53.5	0.201	50.8	0.194	48.3	0.188	45.	
46	.0011	0.232	59.8	0.225	57.0	0.219	54.4	0.212	51.8	0.206	49.3	0.198	46.	
.~	.0012		20.0	0.000		0.001	55.2	0.224	-0-	0.01#	50.2	0.211	47.	
47	.0012	0.244	60.6	0.237	57.9 58.7	0.231	56.1	0.224	52.7 53.6	0.217	51.2	0.211	48.	
49	.0013	0.269	62.0	0.243	59.4	0.255	56.9	0.249	54.5	0.242	52.1	0.236	49.	
50	.0013	0.282	62.7	0.275	60.2	0.268	57.7	0.262	55.3	0.255	52.9	0.249	50.	
51	.0013	0.295	63.4	0.288	60.9	0.282	58.4	0.275	56.1	0.269	53.7	0.262	51.	
	.0014								- 17		PER			
52	0014	0.309	64.1	0.302	61.6	0.296	59.2	0.289	56.8	0.282	54.6	0.276	52.	
53	.0014	0.323	64.7	0.317	62.3	0.310	59.9	0.303	57.6	0.297	55.3	0.290	53.	
54	.0015	0.338	65.3	0.332	62.9	0.325	60.6	0.318	58.3	0.312	56.1	0.305	53.	
55 56	.0016	0.354	65.9 66.5	0.347	63.5	0.340	61.2	0.334	59.0	0.327	56.8 57.5	0.320	54.	
57	.0017	0.386	67.0	0.379	64.7	0.373	62.5	0.366	60.3	0.359	58.2	0.353	56.	
58	-0017	0.403	67.5	0.396	65.3	0.389	63.1	0.383	60.9	0.376	58.8	0.369	56	
59	-0017	0.420	68.0	0.413	65.8	0.407	63.6	0.400	61.5	0.393	59.5	0.387	57	
60	.0018	0.438	68.5	0.431	66.3	0.425	64.2	0.418	62.1	0.411	60.1	0.405	58.	
61	.0018	0.457	69.0	0.450	66.9	0.443	64.7	0.436	62.7	0.430	60.7	0.423	58.	
62	.0019	0.476	69.5	0.469	67.4	0.462	65.3	0.456	63.2	0.449	61.3	0.442	59.	
63	.0020	0.495	70.0	0.489	67.8	0.482	65.8	0.475	63.8	0.469	61.8	0.462	59.	
64	.0021	0.516	70.4	0.509	68.3	0.503	66.3	0.496	64.3	0.489	62.4	0.483	60.	
65	-0021	0.537	70.8	0.530	68.8	0.524	66.8	0.517	64.8	0.510	62.9	0.504	61.	
66	.0022	0.559	71.2	0.552	69.2	0.545	67.2	0.539	65.3	0.532	63.4	0.525	61.	
67	.0023	0.581	71.6	0.575	69.6	0.568	67.7	0.561	65.7	0.554	63.9	0.549	62	

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.0013.

Temperature, Fahrenheit. - Force of Vapor in English Inches - Relative Humidity in Hundredths.

Wet- Bulb Thermo- meter t! Fahren- heit.	Mean Vertical Difference of Force of Vapor for each 0°.1.	t — t', or Difference of Wet and Dry Bulb Thermometers.												
		60.0		60.5		70.0		70.5		80.0		80.5		
		Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity	Force of Vapor.	Relative Hu- mid ity.	
0	- Total	Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng In.	-	
68	0.0024	0.604	72.0	0.597	70.0	0.591	68.1	0.584	66.2	0.577	64.4	0.571	62.	
69	.0024	0.628	72.4	0.621	70.4	0.614	68.5	0.608	66.6	0.601	64.8	0.594	63.0	
70	.0025	0.652	72.7	0.646	70.8	0.639	68.9	0.632	67.1	0.625	65.3	0.619	63.	
71	.0026	0.678	73.1	0.671	71.2	0.664	69.3	0.657	67.5	0.651	65.7	0.644	64.0	
72	.0027	0.704	73.4	0.697	71.5	0.690	69.7	0.683	67.9	0.677	66.1	0.670	64.	
73	100	0.730	73.8	0.724	71.9	0.717	70.1	0.710	68.3	0.703	66.5	0.697	64.8	
74	.0028	0.758	74.1	0.751	72.2	0.745	70.4	0.738	68.7	0.731	66.9	0.724	65.8	
75	.0029	0.787	74.4	0.780	72.6	0.773	70.8	0.766	69.0	0.760	67.3	0.753	65.7	
76	.0030	0.816	74.7	0.809	72.9	0.802	71.1	0.796	69.4	0.789	67.7	0.782	66.1	
77	.0030	0.846	75.0	0.839	73.2	0.832	71.4	0.826	69.7	0.819	68.1	0.812	66.4	
	.0031	0.540	10.0	0.003	10.2	0.002	11.2	0.020	05.1	0.015	00.1	0.012	00.	
78	1000	0.877	75.3	0.870	73.5	0.863	71.8	0.857	70.1	0.850	68.4	0.843	66.8	
79	.0032	0.909	75.6	0.902	73.8	0.895	72.1	0.888	70.4	0.882	68.8	0.875	67.2	
80	.0033	0.942	75.8	0.935	74.1	0.928	72.4	0.921	70.7	0.915	69.1	0.908	67.8	
81	.0034	0.976	76.1	0.969	74.4	0.962	72.7	0.955	71.0	0.948	69.4	0.942	67.9	
82	.0035	1.011	76.4	1.004	74.6	0.997	73.0	0.990	71.3	0.983	69.8	0.977	68.2	
	.0036							-		111100		130		
83	0007	1.046	76.6	1.040	74.9	1.033	73.3	1.026	71.6	1.019	70.1	1.012	68.5	
84	.0037	1.083	76.8	1.077	75.2	1.070	73.5	1.063	71.9	1.056	70.4	1.049	68.8	
85	.0038	1.121	77.1	1.114	75.4	1.108	73.8	1.101	72.2	1.094	70.7	1.087	69.1	
86	100 M 12 M	1.160	77.3	1.153	75.7	1.147	74.1	1.140	72.5	1.133	70.9	1.126	69.4	
87	.0639	1.201	77.5	1.194	75.9	1.187	74.3	1.181	72.7	1.174	71.2	1.167	69.7	
	.0040	to the							AL .					
88	.0042	1.241	77.7	1.235	76.1	1.228	74.6	1.221	73.0	1.214	71.5	1.207	70.0	
89	.0044	1.284	78.0	1.277	76.4	1.270	74.8	1.263	73.3	1.256	71.8	1.250	70.3	
90	.0045	1.327	78.2	1.321	76.6	1.314	75.0	1.307	73.5	1.300	72.0	1.293	70.6	
91	.0046	1.372	78.4	1.365	76.8	1.359	75.3	1.352	73.7	1.345	72.3	1.338	70.8	
92	The fire	1.418	78.6	1.412	77.0	1.405	75.5	1.398	74.0	1.391	72.5	1.384	71.1	
93	.0047	1.466	*O O	1 450	mm 0	1.452	75.7	1.445	74.2	1.438	72.8	1.431	71.3	
94	.0049	1.514	78.8 79.0	1.459	77.2	1.501	75.9	1.494	74.4	1.487	73.0	1.480	71.6	
95	.0050		15.300		7.37	1.550	76.1	1.544	74.7	1.537	73.2	1.530	71.8	
96	.0051	1.564	79.1	1.557	77.6 77.8	1.602	76.3	1.595	74.9	1.588	73.4	1.581	72.1	
97	.0052	1.668	79.3 79.5	1.661	78.0	1.654	76.5	1.647	75.1	1.640	73.7	1.633	72.3	
98	.0054	1.722			78.2	1.708	76.7	1.701	75.3	1.694	73.9	1.688	72.5	
20	.0056	1.722	79.7	1.715	10.2	1.100	10.7	1.701	10.0	1.034	10.0	1.000	12.0	
99	.0000	1.778	79.8	1.771	78.4	1.764	76.9	1.757	75.5	1.750	74.1	1.743	72.7	
100	.0057	1.835	80.0	1.828	78.5	1.821	77.1	1.814	75.7	1.807	74.3	1.800	72.9	
101	.0059	1.893	80.2	1.887	78.7	1.880	77.3	1.873	75.9	1.866	74.5	1.859	73.2	
102	.0060	1.954	80.3	1.947	78.9	1.940	77.4	1.933	76.1	1.926	74.7	1.919	73.4	
103	.0061	2.015	80.5	2.008	79.0	2.001	77.6	1.994	76.2	1.937	74.9	1.980	73.6	
104	.0063	2.078	80.6	2.071	79.2	2.064	77.8	2.057	76.4	2.051	75.1	2.044	73.8	

Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.0018$ .

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

Wet- Bulb Thermo- meter t: Fahren- heit.	Mean Vertical Difference of Force of Vapor for each 0°1.	$\mathbf{t}-\mathbf{t}',$ or Difference of Wet and Dry Bulb Thermometers.												
		9°.0		9°.5		10°.0		100.5		110.0		110.5		
		Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relativ Hu mid ity	
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	44	Eng. In		
32		0.064	25.0	0.058	22.0	0.051	19.2	0.045	16.4	0.038	13.8	0.032	11.	
33	0 0007	0.071	26.7	0.065	23.8	0.058	21.0	0.052	18.3	0.045	15.7	0.039	13.	
34	.0007	0.079	28.3	0.072	25.5	0.066	22.7	0.059	20.1	0.053	17.5	0.046	15.	
35	•0008	0.087	29.9	0.080	27.1	0.074	24.4	0.067	21.8	0.061	19.3	0.054	16.	
36	.0008	0.095	31.4	0.088	28.7	0.082	26.0	0.075	23.5	0.069	21.1	0.062	18	
	.0008		313	- 11								BAC P		
37	.0009	0.103	33.0	0.096	30.3	0.090	27.6	0.083	25.2	0.077	22.8	0.070	20.	
38	.0009	0.112	34.4	0.105	31.8	0.099	29.2	0.092	26.8	0.086	24.4	0.079	22	
39	.0009	0.121	35.9	0.114	33.3	0.108	30.7	0.101	28.4	0.094	26.1	0.088	23	
40	.0009	0.130	37.3	0.123	34.8	0.117	32.2	0.110	29.9	0.104	27.6	0.097	25	
41	.0010	0.139	38.6	0.133	36.2	0.126	33.7	0.120	31.4	0.113	29.2	0.107	27	
	.0010	military	CEVE	en l'aut	NFO			No. You			2.1			
42	.0010	0.149	39.9	0.143	37.5	0.136	35.0	0.130	32.8	0.123	30.6	0.116	28	
43	.0010	0.160	41.1	0.153	38.7	0.146	36.3	0.140	34.1	0.133	32.0	0.127	29	
44	.0011	0.170	42.3	0.163	39.9	0.157	37.6	0.150	35.4	0.144	33.3	0.137	31	
45	.0011	0.181	43.4	0.175	41.1	0.168	38.8	0.161	36.7	0.155	34.6	0.148	32	
46	.0011	0.192	44.5	0.186	42.2	0.179	39.9	0.173	37.9	0.166	35.8	0.160	33.	
out !	.0012	No.			1.00	an Tierla		0.000	20.0			0.787		
47	.0012	0.204	45.5	0.198	43.3	0.191	41.1	0.185	39.0	0.178	37.0	0.171	35.	
48	.0012	0.217	46.5	0.210	44.3	0.203	42.1	0.197	40.1	0.190	38.1	0.184	36	
49	.0013	0.229	47.5	0.222	45.3	0.216	43.2	0.209	41.2	0.203	39.2	0.196	37.	
50	.0013	0.242	48.4	0.235	46.3	0.229	44.2	0.222	42.2	0.216	40.2	0.209	38.	
51		0.255	49.3	0.249	47.2	0.242	45.2	0.236	43.2	0.229	41.2	0.222	39.	
	.0014	0.000	-00	0.000	10 -	0.000		0.249	44.1	0.243	12.0	0.236	40.	
52	.0015	0.269	50.2	0.263	48.1	0.256	46.1	0.249	45.1	0.243	42.2	0.250	41.	
53	.0015	0.284	51.1	0.277	49.0	0.270	47.0	1000	100000	100 May 100 Ma	43.2	0.265	450	
54	.0015	0.298	51.9	0.292	49.8	0.285	47.9	0.279	46.0	0.272	44.1	0.203	42.	
55	.0016	0.314	52.7	0.307	50.7	0.300	48.7	0.294	46.8	0.287	45.0	0.296	44.	
56	0010	0.330	53.5	0.323	51.4	0.316	49.5	0.310	41.1	0.505	45.9	0.290	44	
57	•0016	0.346	54.3	0.339	52.2	0.333	50.3	0.326	48.5	0.319	46.7	0.313	44.	
58	.0017	0.363	55.0	0.356	52.9	0.350	51.1	0.343	49.2	0.336	47.5	0.330	45.	
59	.0017	0.380	55.7	0.373	53.6	0.367	51.8	0.360	50.0	0.354	48.2	0.347	46.	
60	.0018	0.398	56.4	0.391	54.3	0.385	52.5	0.378	50.7	0.371	49.0	0.365	47.	
61	.0018	0.416	57.0	0.410	55.0	0.403	53.2	0.396	51.4	0.390	49.7	0.383	48	
	-0019	0.110	33	3.1.3	30.3	3.103	30.2	1	\$ 100	5			= 11	
62	1.0.01	0.436	57.6	0.429	55.6	0.422	53.9	0.416	52.1	0.409	50.4	0.402	48.	
63	•0020	0.455	58.2	0.449	56.3	0.442	54.5	0.435	52.8	0.429	51.1	0.422	49.	
64	.0021	0.476	58.8	0.469	56.9	0.462	55.1	0.456	53.4	0.449	51.8	0.442	50.	
65	.0021	0.497	59.3	0.490	57.5	0.483	55.8	0.477	54.1	0.470	52.4	0.463	50.	
66	.0022	0.519	59.9	0.512	58.0	0.505	56.3	0.498	54.7	0.492	53.1	0.485	51.	
67	.0023	0.542	60.3	0.534	58.6	0.527	56.9	0.521	55.3	0.514	53.7	0.507	52.	
			415	10 1 350		CULTO		\$7.400	ST ST	2 4 8 7 8	地區部		10	

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.0013.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

144		elitate)		t-1	t', or Di	ifference o	f Wet	and Dry I	Bulb Th	nermomet	ers.		
meter	Mean Vertical Difference of Force	9°.	0	90.	5	100	.0	100	.5	110	.0	110	.5
t <sup>†</sup> Sahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid ity.
0	348	Eng. In.		Eng. In.	100	Eng. In.		Eng. In.		Eng. In.		Eng. In.	
68	0.0024	0.564	60.8	0.557	59.1	0.550	57.4	0.544	55.8	0.537	54.2	0.530	52.
69	.0025	0.588	61.3	0.581	59.6	0.574	58.0	0.567	56.4	0.561	54.8	0.554	53.
70	.0025	0.612	61.8	0.605	60.1	0.598	58.5	0.592	56.9	0.585	55.4	0.578	53.
71	.0026	0.637	62.3	0.630	60.6	0.624	59.0	0.617	57.4	0.610	55.9	0.603	54.
72	1	0.663	62.7	0.656	61.1	0.650	59.5	0.643	58.0	0.636	56.4	0.629	54.
20	.0027	0 200	62.0	0.000	61.0	0 000	60.0	0.000	50 4	0 669	56.9	0.650	55
73	.0027	0.390	63.2 63.6	0.683	61.6	0.677	60.0	0.670	58.4 58.9	0.663	57.4	0.656	55. 56.
74	•0028	28-1327	12.490	0.711	62.0	0.704		16-11-09-2		0.691		0.684	56.
75	.0029	0.746	64.0	0.739	62.5	0.733	60.9	0.726	59.4 59.8	0.719	57.9	0.712	56.
76	.0030	0.775	64.4	0.769	62.9	0.762	61.3	0.755		100 To 100 To 100	58.4	0.741	
77	.0031	0.805	64.8	0.799	63.3	0.792	61.8	0.785	60.3	0.778	58.8	0.772	57.
78	.0031	0.836	65.2	0.829	63.7	0.823	62.2	0.816	60.7	0.809	59.2	0.802	57.
79	.0032	0.868	65.6	0.861	64.1	0.855	62.6	0.848	61.1	0.841	59.7	0.834	58.
80	.0033	0.901	66.0	0.894	64.5	0.897	63.0	0.881	61.5	0.874	60.1	0.867	58.
81	.0034	0.935	66.3	0.928	64.8	0.921	63.4	0.914	61.9	0.908	60.5	0.901	59.
	.0035	0.970	66.7	0.963	65.2	0.956	63.7	0.949	62.3	0.943	60.9	0.936	59.
82	.0036	0.970	00.7	0.903	05.4	0.950	03.7	0.949	04.5	0.945	00.0	0.950	55.
83	.0030	1.006	67.0	0.999	65.5	0.992	64.1	0.985	62.7	0.978	61.3	0.972	59.
84	.0037	1.042	67.3	1.036	65.9	1.029	64.4	1.022	63.0	1.015	61.7	1.008	60.
85	.0038	1.080	67.7	1.073	66.2	1.067	64.8	1.060	63.4	1.053	62.0	1.046	60.
86	.0039	1.119	68.0	1.112	66.5	1.106	65.1	1.099	63.7	1.092	62.4	1.085	61.
87	•0040	1.160	68.3	1.153	66.8	1.146	65.4	1.140	64.1	1.133	62.7	1.126	61.
	.0041	1.100	00.0	1.100	00.0	1.110	00.1	2.12.10	01.1	1.100	- 1594		
88	1201	1.200	68.6	1.194	67.1	1.187	65.8	1.180	64.4	1.173	63.1	1.166	61.
89	.0042	1.243	68.9	1.236	67.4	1.229	66.1	1.222	64.7	1.215	63.4	1.208	62.
90	.0044	1.286	69.1	1.279	67.7	1.273	66.4	1.266	65.0	1.259	63.7	1.252	62.
91	.0045	1.331	69.4	1.324	68.0	1.317	66.7	1.311	65.3	1.304	64.0	1.297	62.
92	.0046	1.377	69.7	1.370	68.3	1.363	67.0	1.357	65.6	1.350	64.3	1.343	63.
	-0047	10 - 100		en Transe	214	Sic Sended	at l	J. David		2		1005	
93	0040	1.425	69.9	1.418	68.6	1.411	67.2	1.404	65.9	1.397	64.6	1.390	63.
94	.0048	1.473	70.2	1.466	68.8	1.459	67.5	1.452	66.2	1.446	64.9	1.439	63.
95	.0050	1.523	70.4	1.516	69.1	1.509	67.8	1.502	66.5	1.495	65.2	1.488	64.
96	Total Control	1.574	70.7	1.567	69.4	1.560	68.0	1.553	66.7	1.546	65.5	1.539	64.
97	.0053 .0054	1.627	70.9	1.620	69.6	1.613	68.3	1.606	67.0	1.599	65.8	1.592	64.
98	00-4 E 91	1.681	71.2	1.674	69.8	1.667	68.5	1.660	67.3	1.653	66.0	1.646	64.
000	.0056			1 200			00.0		0		00.0		0-
99	.0057	1.736	71.4	E - L - L - 23.5 31	70.1	MATERIAL SECTION	68.8	1.716	67.5	1.709	66.3	1.702	65.
100	.0058	1.793	71.6	1.786	70.3	1.780	69.0	1.773	67.8	1.766	66.5	1.759	65.
101	.0060	1.852	71.8	1.845	70.5	100000	69.3	1.831	68.0	1.824	66.8	1.817	65.
102	.0062	1.912	72.0	1.905	70.8	THE CONTRACTOR	69.5	1.891	68.2	1.884	67.0	1.877	65.
103	.0063	1.974	3.00	1.967	71.0	1.960	69.7	1.953	68.5	1.946	67.3	1.939	66.
104	1	2.037	72.5	2.030	71.2	2.023	69.9	2.016	68.7	2.009	67.5	2.002	66.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

Wet-	Mean	spiture		t-t	', or Di	fference o	of Wet	and Dry I	Bulb Th	nermomet	ers.		
Bulb hermo- meter	Vertical Difference of Force of Vapor	120	0.0	120	.5	139	.0	139	.5	149	0.0	14	·.5
ahren- heit.	for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rel tiv Hu mid ity
0		Eng. In.	We !	Eng. In.	anti	Eng. In.		Eng. In.	300	Eng. In.		Eng. In.	
32	0.0007	0.025	8.8	0.019	6.4	0.012	4.1	100	01,30	30 100		1000	
33	.0007	0.032	10.8	0.026	8.4	0.019	6.2	0.013	4.0	84,64	147(1		18
34	.0007	0.040	12.7	0.033	10.4	0.027	8.2	0.020	6.0	0.014	4.1		943
35	.0008	0.048	14.6	0.041	12.3	0.034	10.1	0.028	8.0	0.021	6.1	0.015	4
36	E(1)   1	0.056	16.4	0.049	14.2	0.042	12.0	0.036	10.0	0.029	8.1	0.023	6.
37	.0008	0.064	18.2	0.057	16.0	0.051	13.9	0.044	11.9	0.038	10.0	0.031	8
38	.0009	0.004	19.9	0.066	17.8	0.051	15.7	0.053	13.7	0.038	11.9	0.040	10
39	.0009	0.072	21.6	0.000	19.5	0.068	17.5	0.062	15.5	0.046	13.7	0.040	11
40	.0009	0.001	23.3	0.084	21.2	0.008	19.2	0.002	17.2	0.064	15.4	0.058	13
41	.0010	0.100	24.9	0.094	22.8	0.018	20.8	0.071	18.9	0.004	17.1	0.067	15
7.1	.0010	0.100	24.0	0.034	1	0.037	20.0	0.001	10.9	0.014	11	0.007	10
42	60 m3 00	0.110	26.4	0.103	24.3	0.097	22.4	0.090	20.5	0.084	18.6	0.077	16
43	.0010	0.120	27.8	0.114	25.8	0.107	23.9	0.100	22.0	0.095	20.1	0.087	18
44	•0011	0.131	29.2	0.124	27.2	0.118	25.3	0.111	23.5	0.104	21.5	0.098	19
45	.0011	0.142	30.5	0.135	28.6	0.129	26.7	0.122	24.9	0.115	22.9	0.109	21.
46	.0011	0.153	31.8	0.146	30.0	0.140	28.1	0.133	26.3	0.127	24.3	0.119	22.
	.0012	- 11/1		6					7				
47	.0012	0.165	33.0	0.158	31.2	0.152	29.3	0.145	27.6	0.138	25 7	0.132	24
48	.0012	0.177	34.2	0.170	32.4	0.164	30.6	0.157	28.8	0.151	27.0	0.144	25.
49	.0013	0.190	35.3	0.183	33.5	0.176	31.7	0.170	30.0	0.163	28.3	0.157	26
50	.0013	0.202	36.4	0.196	34.6	0.189	32.9	0.183	31.2	0.176	29.5	0.169	27
51	.0014	0.216	37.5	0.209	35.7	0.202	34.0	0.196	32.3	0.189	30.7	0.183	29
	.0014		00.4	0.000	200	0.000				0 000	07.0	0.000	00
52	.0014	0.229	38.5	0.223	36.8	0.216	35.1	0.210	33.4	0.203	31.8	0.196	30.
53	.0015	0.244	39.5	0.237	37.8	0.231	36.1	0.224	34.5	0.217	32.9	0.211	31.
54	.0015	0.259	40.5	0.252	38.8	0.245	37.1	0.239	35.5	0.232	34.0	0.226	32.
55 56	.0016	0.274	41.5	0.267	39.8	0.261	38.1	0.254	36.5	0.247	35.0 35.9	0.241	
90	SHE FEE	0.290	42.4	0.283	40.7	0.276	39.1	0.270	37.5	0.263	33.9	0.207	34.
57	.0016	0.306	43.2	0.299	41.6	0.293	40.0	0.286	38.4	0.280	36.9	0.273	35.
58	.0017	0.323	44.1	0.316	42.4	0.310	40.8	0.303	39.3	0.296	37.8	0.290	36.
59	.0017	0.340	44.9	0.334	43.3	0.327	41.7	0.320	40.1	0.314	38.7	0.307	37.
60	.0018	0.358	45.7	0.351	44.1	0.345	42.5	0.338	41.0	0.331	39.5	0.325	38.
61	.0018	0.376	46.4	0.370	44.9	0.363	43.3	0.356	41.8	0.350	40.3	0.343	38.
0000	.0019						TIL		H	- 19/5			
62		0.396	47.2	0.389	45.6	0.382	44.1	0.376	42.6	0.369	11.2	0.362	39.
63	.0020	0.415	47.9	0.409	46.4	0.402	44.8	0.395	43.4	0.389	41.9	0.382	40.
64	.0021	0.436	48.6	0.429	47.1	0.422	45.6	0.416	44.1	0.409	42.7	0.402	41.
65	•0021	0.457	49.3	0.450	47.8	0.443	46.3	0.437	44.8	0.431	43.4	0.423	42.
66	.0022	0.478	49.9	0.472	48.4	0.465	47.0	0.458	45.5	0.452	44.1	0.445	42.
67	.0023	0.501	50.6	0.494	49.1	0.487	47.6	0.481	46.2	0.474	44.8	0.467	43.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

		*********		t-	t', or D	ifference (	of Wet	and Dry	Bulb T	hermome	ters.		
Wet- Bulb hermo- meter	Mean Vertical Difference of Force of Vapor	120	.0	120	.5	130	.0	139	.5	149	.0	14	.5
t'ahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.
0	AC SHE	Eng. In.		Eng. In.	112 15	Eng. In.	1800	Eng. In.	i entr	Eng. In.		Eng In.	39
68	0.0024	0.524	51.2	0.517	49.7	0.510	48.3	0.503	46.9	0.497	45.5	0.490	44.
69	.0024	0.547	51.8	0.541	50.3	0.534	48.9	0.527	47.5	0.520	46.1	0.514	44.
70	.0025	0.572	52.4	0.565	50.9	0.558	49.5	0.551	48.1	0.545	46.8	0.538	45.
71	.0026	0.597	52.9	0.590	51.5	0.583	50.1	0.577	48.7	0.570	47.4	0.563	46.
72	.0026	0.623	53.5	0.616	52.1	0.609	50.7	0.603	49.3	0.596	48.0	0.589	46.
73	Sec. 35.	0.650	54.0	0.643	52.6	0.636	51.3	0.629	49.9	0.623	48.6	0.616	47.
74	0027	0.677	54.5	0.670	53.2	0.664	51.8	0.657	50.5	0.650	49.2	0.643	47.
75	.0023	0.705	55.0	0.699	53.7	0.692	52.3	0.685	51.0	0.678	49.7	0.672	48.
76	.0029	0.735	55.5	0.728	54.2	0.721	52.9	0.714	51.5	0.708	50.3	0.701	48.
77	.0030	0.765	56.0	0.759	54.7	0.752	53.4	0.745	52.1	0.739	50.8	0.731	49.
	.0031	000	00.0	0.105	01	0.132	00.4	0.140	04.1	0.103	00.0	0.1.51	10.0
78		0.796	56.5	0.782	55.2	0.782	53.8	0.775	52.5	0.768	51.3	0.762	50.0
79	.0032	0.827	56.9	0.821	55.6	0.814	54.3	0.807	53.0	0.800	51.8	0.794	50.
80	.0033	0.860	57.3	0.853	56.1	0.847	54.8	0.840	53.5	0.833	52.2	0.826	51.0
81	•0034	0.894	57.8	0.887	56.5	0.880	55.2	0.874	53.9	0.867	52.7	0.860	51.
82	.0035	0.929	58.2	0.922	56.9	0.915	55.6	0.909	54.4	0.902	53.2	0.895	51.9
	.0036	Sale Con	SW.			3						REED.	
83	.0037	0.965	58.6	0.958	57.3	0.951	56.1	0.944	54.8	0.937	53.6	0.931	52
84	.0038	1.002	59.0	0.995	57.7	0.988	56.5	0.981	55.2	0.974	54.0	0.968	52.5
85	.0039	1.039	59.4	1.033	58.1	1.026	56.8	1.019	55.6	1.012	54.4	1.005	53.2
86	.0040	1.078	59.7	1.071	58.5	1.065	57.2	1.058	56.0	1.051	54.8	1.044	53.6
87		1.119	60.1	1.112	58.8	1.105	57.6	1.099	56.4	1.092	55.2	1.085	54.0
88	.0041	1 150	60 =	1 150	F0.9	1 1 10	FO 0	1 100	FC 0	1 100	0	1 10-	- 4
89	.0042	1.159	60.5	1.152	59.2	1.146	58.0	1.139	56.8	1.132	55.6	1.125	54.
90	.0044	120000000000000000000000000000000000000	Section It's	1.195	59.6	1.188	58.3	1.181	57.1	1.174	56.0	1.167	54.8
91	-0045	1.245	61.3	1.238	59.9	1.231	58.7	1.225	57.5	1.218	56.3	1.211	55.2
92	.0046	1.290	61.6	1.283	60.2	1.276	59.0	1.269	57.9	1.263	66.7	1.256	55.6
34	.0047	1.336	61.9	1.329	60.6	1.322	59.4	1.315	58.2	1.309	57.0	1.302	55.9
93	.0041	1.383	62.2	1.376	60.9	1.370	59.7	1.363	58.5	1.356	57.4	1.349	56.8
94	.0049	1.432	62.5	1.425	61.2	1.418	60.0	1.411	58.9	1.404	57.7	1.397	56.6
95	.0050	1.482	62.7	1.475	61.5	1.468	60.4	1.461	59.2	1.454	58.1	1.447	57.0
96	.0051	1.533	63.0	1.526	61.8	1.519	60.7	1.512	59.5	1.505	58.4	1.498	57.3
97	.0052	1.585	63.3	1.578	62.1	1.571	61.0	1.564	59.8	1.558	58.7	1.551	57.6
98	.0054	1.639	63.6	1.632	62.4	1.625	61.3	1.618	60.1	1.612	59.0	1.605	57.9
100	.0056			1.002		1.020		3.010			30.0		31.0
99		1.695	63.9	1.688	62.7	1.681	61.6	1.674	60.4	1.667	59.3	1.660	58.2
100	.0057	1.752	64.2	1.745	63.0	1.738	62.0	1.731	60.7	1.724	59.6	1.717	58.5
101	.0059	1.810	64.4	1.803	63.2	1.797	62.3	1.790	61.0	1.783	59.9	1.776	58.8
102	•0060	1.870	64.7	1.863	63.5	1.857	62.6	1.850	61.3	CONTRACTOR OF THE PARTY.	60.2	1.836	59.1
103	.0062	1.932	64.9	1.925	63.8	1.918	62.9	1.911	61.5	1.904	60.4	1.897	59.4
104	-0063	1.995	65.2	1.988	64.0	1.981	63.2	1.974	61.8	1.967	60.7	1.960	59.6

Temperature, Fahrenheit. - Force of Vapor in English Inches. - Relative Humidity in Hundredths.

Wet-	Mean	A BIT	instead	t-1	t', or D	ifference o	of Wet	and Dry I	Bulb Th	nermomet	ers.		
Bulb Thermo- meter	Vertical Difference of Force of Vapor	150	.0	150	.5	169	.0	160	.5	179	.0	170	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu mid ity
0	16 300	Eng. In.	1464	Eng. In.		Eng. In.	Sur l	Eng. In.	a	Eng. In.	nus!	Eng. In.	
32										113		HOTE	
34		San			i di	Turni G						1990	13
35	the state of	And the				Care la					- 81	250	10
36	a second	0.016	4.4	unicas	est of	SARI V				in the	0.00		1.0
	0.0009	0.00-	0.4	0.010	4.0	411						nere d	
37	.0009	0.025	6.4 8.3	0.018	4.6 6.5	0.020	4.8	0.014	3.2	34			4 195
39	.0009	0.033	10.1	0.027	8.4	0.020	6.7	0.014	5.1	0.016	3.6	0.010	2
40	.0009	0.051	11.9	0.045	10.1	0.038	8.5	0.032	6.9	0.025	5.4	0.019	3
41	.0010	0.061	13.6	0.054	11.8	0.048	10.3	0.041	8.7	0.035	7.2	0.028	5
42	.0010	0.071	15.1	0.064	13.4	0.058	11.9	0.051	10.3	0.044	8.8	0.038	7
43	.0011	0.081	16.6	0.074	15.0	0.068	13.4	0.061	11.9	0.055	10.4	0.048	9
44	.0011	0.091	18.1	0.085	16.5	0.078	15.0	0.072	13.5	0.065	12.0	0.058	10
45	.0011	0.102	19.6	0.096	18.0	0.089	16.5	0.083	15.0	0.076	13.5	0.069	12
46	.0012	0.114	21.0	0.107	19.4	0.100	17.9	0.094	16.4	0.087	15.0	0.081	13.
47	Park S	0.125	22.4	0.119	20.8	0.112	19.3	0.106	17.9	0.099	16.5	0.092	15.
48	.0012	0.137	23.8	0.131	22.2	0.124	20.7	0.118	19.3	0.111	17.9	0.104	16
49	.0013	0.150	25.1	0.143	23.6	0.137	22.1	0.130	20.7	0.124	19.3	0.117	17.
50	.0013	0.163	26.4	0.156	24.9	0.150	23.4	0.143	22.0	0.136	20.6	0.130	19.
51		0.176	27.6	0.169	26.1	0.163	24.6	0.156	23.2	0.150	21.9	0.143	20.
52	•0014	0.190	28.7	0.183	27.3	0.177	25.8	0.170	24.4	0.163	23.1	0.157	21.
53	.0014	0.204	29.9	0.197	28.4	0.191	27.0	0.184	25.6	0.178	24.3	0.171	23.
54	.0015	0.219	30.9	0.212	29.5	0.206	28.1	0.199	26.7	0.192	25.4	0.186	24.
55	.0015	0.234	32.0	0.228	30.6	0.221	29.2	0.214	27.8	0.208	26.5	0.201	25.
56	STEEL ST	0.250	33.0	0.243	31.6	0.237	30.2	0.230	28.9	0.223	27.6	0.217	26.
57	•0016	0.266	34.0	0.260	32.6	0.253	31.2	0.246	29.9	0.240	28.6	0.233	27
58	.0017	0.283	34.9	0.276	33.5	0.270	32.2	0.268	30.8	0.256	29.6	0.249	28
59	•0017	0.300	35.8	0.294	34.4	0.287	33.1	0.280	31.8	0.274	30.5	0.267	29.
60	•0018	0.318	36.7	0.311	35.3	0.305	34.0	0.298	32.7	0.291	31.4	0.285	30.
61	•0019	0.336	37.5	0.330	36.2	0.323	34.9	0.316	33.6	0.310	32.4	0.303	31.
	•0019	0.000	00	0.010	00.0	0.040	05 =	0.000	0.4 -	0.000	00.0	0.200	20
62 63	.0020	0.356	38.4	0.349	37.0	0.342	35.7 36.6	0.336	34.5	0.329	33.2	0.322	32.
64	-0020	0.375	39.2	0.369	37.9 38.7	0.362	37.4	0.355	36.1	0.349	34.1	0.342	33.
65	.0021	0.330	40.7	0.359	39.4	0.302	38.2	0.396	36.9	0.390	35.7	0.383	34.
66	.0022	0.438	41.5	0.431	40.2	0.425	38.9	0.418	37.7	0.411	36.5	0.405	35.
67	.0023	0.460	42.2	0.454	40.9	0.447	39.6	0.440	38.4	0.434	37.2	0.427	36.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t-t	, or Di	ifference (	of Wet	and Dry	Bulb Tl	hermomet	ers.		
meter	Mean Vertical Difference of Force	150	.0	150	.5	160	.0	169	.5	170	.0	170	.5
t <sup>†</sup> Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.	7	Eng. In.	Val.	Eng. In.	
68	0.0024	0.483	42.8	0.477	41.6	0.470	40.3	0.463	39.1	0.456	37.9	0.450	36.8
69	.0024	0.507	43.5	0.500	42.3	0.594	41.0	0.487	39.8	0.480	38.7	0.473	37.5
70	.0024	0.531	44.2	0.524	42.9	0.518	41.7	0.511	40.5	0.504	39.3	0.498	38.2
71	.0026	0.556	44.8	0.550	43.6	0.543	42.4	0.536	41.2	0.529	40.0	0.523	38.9
72		0.582	45.4	0.576	44.2	0.569	43.0	0.562	41.8	0.555	40.7	0.549	39.5
<b>#0</b>	.0027	0 000	46.0	0 000	110	0.596	43.6	0.589	42.4	0.582	41.3	0.575	40.2
73 74	.0028	0.609	46.6	0.602	44.8	0.623	44.2	0.616	43.0	0.610	41.9	0.603	40.2
75	.0028	0.665	47.2	0.658	46.0	0.651	44.8	0.645	43.6	0.638	42.5	0.631	41.4
76	.0029	0.694	47.7	0.687	46.5	0.681	45.4	0.674	44.2	0.667	43.1	0.660	42.0
77	•0030	0.724	48.2	0.717	47.1	0.711	45.9	0.704	44.8	0.697	43.6	0.690	42.6
	.0031	0	10.2	0			20.0						
78	0,00	0.755	48.8	0.748	47.6	0.741	46.4	0.735	45.3	0.728	44.2	0.721	43.1
79	.0032	0.787	49.3	0.780	48.1	0.773	47.0	0.766	45.8	0.760	44.7	0.753	43.7
80	.0033	0.820	49.8	0.813	48.6	0.806	47.5	0.799	46.4	0.792	45.3	0.786	44.2
81	.0034	0.853	50.3	0.847	49.1	0.840	48.0	0.833	46.9	0.826	45.8	0.819	44.6
82	•0035	0.888	50.7	0.881	49.6	0.875	48.5	0.868	47.4	0.861	46.3	0.854	45.1
Mary 1850	.0036												
83	.0037	0.924	51.2	0.917	50.0	0.910	48.9	0.903	47.8	0.897	46.8	0.890	45.6
84	.0038	0.961	51.6	0.954	50.5	0.947	49.4	0.940	48.3	0.933	47.2	0.927	46.2
85	.0039	0.998	52.1	0.992	50.9	0.985	49.8	0.978	48.7	0.971	47.7	0.964	46.6
86	.0040	1.037	52.5	1.030	51.3	1.024	50.3	1.017	49.2	1.010	48.1	1.003	47.1
87	ALC: NO.	1.078	52.9	1.071	51.8	1.064	50.7	1.058	49.6	1.051	48.6	1.044	47.5
00	.0041		70.0			7 705	-11	7 000	F0.0	1 001	49.0	1.084	48.0
88	.0042	1.118	53.3	1.111	52.2	1.105	51.1	1.098	50.0	1.091	49.4	1.126	48.4
89 90	.0044	1.161	53.7	1.154	52.6	1.147	51.5	1.140	50.4	1.133	49.4	1.170	48.8
91	.0045	1.204	54.1	1.197	53.0	1.190	52.3	1.183	51.2	1.221	50.2	1.215	49.2
92	.0046	1.249	54.5 54.8	1.242	53.4	1.281	52.7	1.274	51.6	1.267	50.6	1.260	49.6
34	.0048	1.290	94.0	1.288	00.7	1.201	02.1	1.214	01.0	1.207	00.0	2.200	20.0
93	Mark of F	1.342	55.2	1.335	54.1	1.328	53.0	1.321	52.0	1.315	51.0	1.308	50.0
94	.0049	1.390	55.5	1.384	54.4	1.377	53.4	1.370	52.4	1.363	51.4	1.356	50.4
95	.0050	1.440	55.9	1.433	54.8	1.426	53.7	1.420	52.7	1.413	51.7	1.406	50.7
96	.0051	1.491	56.2	1.484	55.1	1.477	54.1	1.471	53.1	1.464	52.1	1.457	51.1
97	•0053	1.544	56.5	1.537	55.5	1.530	54.4	1.523	53.4	1.516	52.4	1.509	51.5
98	.0054	1.598	56.8	1.591	55.8	1.584	54.8	1.577	53.8	1.570	52.8	1.563	51.8
1 325	.0056	GUEST IN	dentil.	RAME OF		1991 31	10-7	STATE 21	STATE OF	458			
99	-0057	1.653	57.2	1.646	56.1	1.639	55.1	1.633	54.1	1.626	53.1	1.619	52.1
100	.0059	1.710	57.5	1.703	56.4	1.696	55.4	1.690	54.4	1.683	53.4	1.676	52.5
101	•0060	1.769	57.8	1.762	56.7	1.755	55.7	1.748	54.7	1.741	53.7	1.734	52.8
102	.0062	1.829	58.0	1.822	57.0	1.815	56.0	1.809	55.0	1.802	54.0	1.794	53.1
103	.0063	1.890	58.3	1.883	57.3	1.876	56.3	1.869	55.3	1.863	54.3	1.856	53.4
104	***************************************	1.953	58.6	1.946	57.6	1.939	56.6	1.932	55.6	1.925	54.6	1.919	53.7
	960	Mo	- TT	gontal Di	œ	-673	of Wan	on for one	1. 00 1	0.0019			3

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

		acoustic and the second	(Perford	t-1	t', or Di	fference (	of Wet	and Dry	Bulb T	hermome	ters.		
Wet- Bulb Thermo- meter t'	Mean Vertical Difference of Force of Vapor	18	°.0	18	°.5	19	°.0	199	.5	20	°.0	20	°.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humidity.
0		Eng. In.		Eng. In.	- XVALV	Eng. In.		Eng. In.		Eng. In.		Eng. In.	- 19
32 33	ger led le	Exe Ca		W. L.		E43.24	3.0	200	W.C.	Lab II	100	1001.5	
34	near and as	324 . 1	all.	-06-1	avi i	BIRBA	del	ed Fig	SSAI	SARAR	call!	\$1,37,1	
35		ding	all a	CA ja	in the last	10 - 18	100	- 106 1	uni I	1/6/5	100	ACC.	763
36	Dr and B	· 信	Low I	10 10	no!	1-10-16	10.50	att la	0.0	484	1	(HOCO)	
5	100 fill 1	Crat Le		100		- x 0	- 1						
37 38	Lean!	12.50		alla file			2.0			1000	10.30	Mary 1	3
39	15 yette	34		Di A	and to	CH2 LI	20.5		201	Co T L Lord		Meth.	
40	5 k. st. 1	0.012	2.5	LAI A	Table !	ster A	ocalul.	State	2.61	6.71	and of	HERA.	
41	0.0010	0.022	4.3	0.015	3.0	0.009	1.6	Contract of the last	gaid.	Leiden S	20.11	Bureau	38
	.0010		4.00	av.								1805	100
42	.0010	0.031	6.0	0.025	4.6	0.018	3.3	0.012	2.1	LIGIOUS I		Med 3. T	
43	.0011	0.041	7.6	0.035	6.3	0.028	5.0	0.022	3.7	0.015	2.6	0.010	0.6
44	.0011	0.052	9.2	0.045	7.9	0.039	6.6 8.2	0.032	5.4 7.0	0.026	4.3 5.9	0.019	3.5
46	.0011	0.074	12.3	0.068	11.0	0.050	9.7	0.054	8.5	0.037	7.5	0.030	6.
	.0012	0.011	12.0	0.000	11.0	0.001	J	0.001	0.0	0.040		0.011	
47	.0012	0.086	13.8	0.079	12.5	0.073	11.2	0.066	10.0	0.059	9.0	0.053	7.
48	.0012	0.098	15.2	0.091	13.9	0.085	12.7	0.078	11.5	0.072	10.4	0.065	9.3
49	.0013	0.110	16.6	0.104	15.4	0.097	14.1	0.091	12.9	0.084	11.9	0.077	10.
50 51	.0013	0.123	18.0	0.117	16.7	0.110	15.5	0.103	14.4	0.097	13.2	0.090	12.
91	.0014	0.130	19.5	0.150	18.0	0.123	16.8	0.117	15.7	0.110	14.5	0.103	10.
52		0.150	20.5	0.144	19.3	0.137	18.1	0.130	16.9	0.124	15.7	0.117	14.6
53	.0014	0.164	21.7	0.158	20.5	0.151	19.3	0.145	18.2	0.138	16.9	0.131	15.8
54	.0015 .0015	0.179	22.9	0.173	21.7	0.166	20.5	0.159	19.3	0.152	18.1	0.146	17.0
55	.0015	0.194	24.0	0.188	22.8	0.181	21.6	0.174	20.5	0.168	19.2	0.161	18.2
56	1 E 5 U 1 ( )	0.210	25.1	0.203	23.9	0.197	22.7	0.190	21.6	0.184	20.4	0.177	19.5
57	•0016	0.226	26.1	0.220	24.9	0.213	23.8	0.206	22.7	0.200	21.5	0.193	20.4
58	.0017	0.243	27.1	0.236	25.9	0.230	24.8	0.223	23.7	0.217	22.6	0.210	21.
59	-0017	0.260	28.1	0.254	26.9	0.247	25.8	0.240	24.7	0.234	23.6	0.227	22.6
60	•0018	0.278	29.0	0.271	27.9	0.265	26.8	0.258	25.7	0.251	24.6	0.245	23.6
61	.0019	0.296	30.0	0.290	28.8	0.283	27.7	0.276	26.6	0.270	25.5	0.263	24.5
62	.0019	0.316	30.9	0.309	29.7	0.302	28.6	0.295	27.5	0.289	26.5	0.282	25.4
63	.0020	0.335	31.7	0.328	30.6	0.302	29.5	0.233	28.4	0.308	27.4	0.302	26.4
64	•0020	0.355	32.6	0.349	31.5	0.342	30.4	0.335	29.3	0.329	28.2	0.322	27.2
65	•0021	0.376	33.4	0.370	32.3	0.363	31.2	0.356	30.1	0.350	29.1	0.343	28.1
66	.0022	0.398	34.2	0.391	33.1	0.385	32.0	0.378	30.9	0.371	29.9	0.364	28.9
67	.0023	0.420	34.9	0.414	33.8	0.407	32.8	0.400	31.7	0.393	30.7	0.387	29.7
		100	N - 1 Mg		SKUD	100 KB	A.F.	15 3	45.6	1150 11	200	ME GI	171

Temperature, Fahrenheit. -- Force of Vapor in English Inches -- Relative Humidity in Hundredths.

777.4	Mana			t-t	, or Di	fference o	f Wet a	and Dry I	Bulb Th	ermomet	ers.		
Wet- Bulb hermo- meter	of Force	189	.0	180	.5	199	.0	199	.5	200	.0	20	·.5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu mid ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	Virginia.	Eng. In.	-
68	0.0024	0.443	35.7	0.436	34.6	0.430	33.5	0.423	32.5	0.416	31.4	0.409	30.
69	.0025	0:467	36.4	0.460	35.3	0.453	34.2	0.446	33.2	0.440	32.2	0.433	31.
70	.0025	0.491	37.1	0.484	36.0	0.477	35.0	0.471	33.9	0.464	32.9	0.457	31.
71	.0026	0.516	37.8	0.509	36.7	0.502	35.7	0.496	34.6	0.489	33.6	0.482	32.
72	.0020	0.542	38.5	0.535	37.4	0.528	36.3	0.522	35.3	0.515	34.3	0.508	33.
	.0026	DE TA				195					100		
73	.0027	0.569	39.1	0.562	38.0	0.555	37.0	0.548	36.0	0.542	35.0	0.535	34.
74	.0028	0.596	39.7	0.589	38.7	0.583	37.7	0.576	36.6	0.569	35.7	0.562	34.
75	.0029	0.624	40.3	0.618	39.3	0.611	38.3	0.604	37.3	0.597	36.3	0.591	35.
76	.0030	0.654	40.9	0.647	39.9	0.640	38.9	0.633	37.9	0.627	36.9	0.620	35.
77	100	0.683	41.5	0.677	40.5	0.670	39.5	0.663	38.5	0.656	37.5	0.650	36.
	.0031	MILE						1			- 11		-
78	.0032	0.714	42.1	0.707	41.0	0.701	40.0	0.694	39.0	0.687	38.1	0.680	37.
79	.0033	0.746	42.6	0.739	41.6	0.732	40.6	0.726	39.6	0.719	38.6	0.712	37.
80	.0034	0.779	43.2	0.772	42.1	0.765	41.1	0.758	40.2	0.752	39.2	0.745	38.
81	.0035	0.813	43.7	0.806	42.7	0.799	41.7	0.792	40.7	0.785	39.7	0.779	38.
82		0.847	44.2	0.840	43.2	0.834	42.2	0.827	41.2	0.820	40.2	0.813	39.
	.0036											Coll State	
83	.0036	0.883	44.7	0.876	43.7	0.869	42.7	0.863	41.7	0.856	40.7	0.849	39.
84	.0038	0.920	45.2	0.913	44.2	0.906	43.2	0.899	42.2	0.893	41.3	0.886	40.
85	.0039	0.958	45.6	0.951	44.6	0.944	43.7	0.937	42.7	0.930	41.8	0.923	40.
86	.0040	0.996	46.1	0.989	45.1	0.983	44.1	0.976	43.2	0.969	42.3	0.962	41.
87	.0040	1.037	46.5	1.030	45.6	1.023	44.6	1.017	43.6	1.010	42.7	1.003	41.
88		1.077	47.0	1.070	46.0	1.064	45.0	1.057	44.1	1.050	43.2	1.043	42.
89.	.0042	1.119	47.4	1.113	46.4	1.106	45.5	1.099	44.5	1.092	43.6	1.085	42.
90	.0043	1.163	47.8	1.156	46.9	1.149	45.9	1.142	45.0	1.136	44.1	1.129	43.
91	.0045	1.208	48.2	1.201	47.3	1.194	46.3	1.187	45.4	1.180	44.5	1.173	43.
92	.0047	1.254	48.6	1.247	47.7	1.240	46.7	1.233	45.8	1.226	44.9	1.219	44.
-	.0048					- 7						E MINIS	
93	.0049	1.301	49.0	1.294	48.1	1.287	47.1	1.280	46.2	1.273	45.3	1.266	•44.
94	.0049	1.349	49.4	1.342	48.4	1.335	47.5	1.329	46.6	1.322	45.7	1.315	44.
95	.0051	1.399	49.8	1.392	48.8	1.385	47.9	1.378	47.0	1.371	46.1	1.364	45.
96	.0051	1.450	50.1	1.443	49.2	1.436	48.3	1.429	47.3	1.422	46.5	1.415	45.
97	.0053	1.502	50.5	1.495	49.5	1.489	48.6	1.482	47.7	1.475	46.8	1.468	46.0
98	•0054	1.556	50.8	1.549	49.9	1.543	49.0	1.536	48.1	1.529	47.2	1.522	46.
0.5	.0055			AP NO	EGE		10	18.11		757 14	2083	The state of	
99	.0057	1.612	51.2	1.605	50.2	1.598	49.3	1.591	48.4	1.584	47.5	1.577	46.
100	.0058	1.669	51.5	1.662	50.6	1.655	49.7	1.648	48.8	1.641	47.9	1.634	47.0
101	.0058	1.727	51.8	1.720	50.9	1.713	50.0	1.706	49.1	1.700	48.2	1.693	47.
102	.0060	1.787	52.2	1.780	51.2	1.773	50.3	1.766	49.4	1.759	48.6	1.753	47.
103	.0062	1.849	52.5	1.842	51.5	1.835	50.7	1.828	49.8	1.821	48.9	1.814	48.0
104	.0003	1.912	52.8	1.905	51.9	1.898	51.0	1.891	50.1	1.884	49.2	1.877	48.4

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

Wet	N.		zmicšad	t-	t', or D	oifference	of Wet	and Dry	Bulb T	hermome	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	21	°.0	21	°.5	22	°.0	22	•.5	23	°.0	23	°.5
Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rel tive Hu mid ity
0	at house	Eng. In.	Set	Eng. In.		Eng. In.	KE	Eng. In.	1	Eng. In	LIV.	Eng. In.	
32	BOX OF	TAR THE	1207	AC 16	-	38 0	2-0	Light Lan	1.18	100	1412 T		7
33 34		1000	1940	CE I	191	112 3		154	-175		AT IN		- 10
35	WALLS					10515	1.2	CHE PARS	1	- 57.			
36	AUDIT OF					- 44 10		LINE NO	Suran		0.73		
	Tarrey .	3.15	V-		-		-vell	400		TV.	O.M.		18
37	<b>開開が</b>	Ken I	44	104 14	Atl.		4.8 9	ENE OF	Stine?	REL N			1
38		NE C	1901	Lan A		ALS IN	E-63	TU 15		- F 1 Mg			181
39	V		15-01	CHALL S	DI AND	MIS E	-41	LAR III		SUL DE			
41			Bryll.		BOATS IS	CAROLI IS	10.97	-B#9.54		6.00			
71		San Pa		7100		-60	- 7 1	100		1735.401	Witte !		1
42	hink at	A 10	teaf	ine de		LEE O	- ale		e all	32.0	e de la	THE PARTY	
43	PERAT			Equ. 5	Cap L	SEE LES	15.19	-20	ounds				
44	0.0011	0.013	2.0	NO B	TOTAL S	100	it all	and in	Silver	Jan 19	in the	-	
45	.0011	0.023	3.7	0.017	2.6	0.010	1.6	1144	F. 78 p	Lipita.	-2	EARL A	P
46		0.035	5.2	0.028	4.2	0.022	3.1	0.015	2.1	A COLD	Sign !		-33
47	.0012	0.046	6.8	0.040	5.7	0.033	4.7	0.027	3.7	0.020	2.7	0.013	1.
48	.0012	0.058	8.2	0.052	7.2	0.045	6.2	0.039	5.2	0.032	4.2	0.025	3.
49	.0013	0.071	9.7	0.064	8.6	0.058	7.6	0.051	6.6	0.044	5.7	0.038	4.
50	.0013	0.084	11.0	0.077	10.0	0.070	9.0	0.064	8.0	0.057	7.1	0.051	6.
51	•0013	0.097	12.3	0.090	11.3	0.084	10.3	0.077	9.3	0.070	8.3	0.064	7.
52	.0014	0.110	13.5	0.104	12.5	0.097	11.5	0.091	10.6	0.084	9.6	0.077	8.
53	.0014	0.125	14.8	0.104	13.7	0.097	12.8	0.105	11.8	0.098	10.9	0.077	9.
54	.0015	0.139	16.0	0.133	14.9	0.126	14.0	0.120	13.0	0.113	12.1	0.106	11.
55	.0015	0.155	17.1	0.148	16.1	0.141	15.1	0.135	14.2	0.128	13.3	0.121	12.
.56	.0016	0.170	18.2	0.164	17.2	0.157	16.3	0.150	15.3	0.144	14.4	0.137	13.
57	-0016	0.186	70.4	0.700		0.100		0 - 0-		0.700			
58	-0017	0.186	19.4	0.180	18.4	0.173	17.4	0.167	16.5 17.6	0.160	15.6	0.153	14.
59	-0017	0.220	21.5	0.197	20.6	0.190	18.5 19.6	0.183	18.7	0.177	17.7	0.170	16.
60	<b>-0018</b>	0.238	22.5	0.231	21.6	0.225	20.6	0.218	19.6	0.211	18.7	0.205	17.8
61	-0019	0.256	23.4	0.250	22.5	0.243	21.5	0.236	20.6	0.230	19.7	0.223	18.8
00	-0019	0.0==					and h	14 1					
62 63	.0020	0.275	24.4	0.269	23.5	0.262	22.4	0.255	21.5	0.249	20.6	0.242	19.
64	.0020	0.295	25.3 26.1	0.288	24.4 25.3	0.282	23.3	0.275	22.4	0.268	21.5	0.262	20.
65	.0021	0.336	27.0	0.330	26.1	0.302	24.2	0.295	23.3	0.289	23.3	0.282	22.
66	.0022	0.358	27.9	0.351	27.0	0.344	26.0	0.338	25.1	0.331	24.2	0.324	23.
67	-0023	0.380	28.7	0.373	27.8	0.367	26.8	0.360	25.9	0.353	25.0	0.346	24.5
1125	and it	New york		Nee Ed	Page 1		No. of Street, or other Persons	100	455		2.1	To had	

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t-1	t', or D	ifference (	of Wet	and Dry	Bulb T	hermomet	ers.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	210	.0	21	.5	220	.0	220	.5	23	0.0	23	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor,	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	115/2	Eng. In.		Eng. In.		Eng. In.	girl.	Eng. In.	Apple	Eng. In.		Eng. In.	7 4
68	0.0024	0.403	29.5	0.396	28.5	0.389	27.6	0.383	26.7	0.376	25.8	0.369	25.0
69	.0024	0.426	30.2	0.420	29.3	0.413	28.4	0.406	27.5	0.399	26.6	0.393	25.8
70	.0025	0.451	31.0	0.444	30.1	0.437	29.1	0.430	28.2	0.424	27.4	0.417	26.5
71	.0026	0.476	31.7	0.469	30.8	0.462	29.9	0.455	29.0	0.449	28.1	0.442	27.3 28.0
72	.0027	0.501	32.4	0.495	31.5	0.488	30.6	0.481	29.7	0.475	40.0	0.468	20.0
73	.0021	0.528	33.1	0.521	32.2	0.515	31.3	0.508	30.4	0.501	29.5	0.494	28.7
74	.0028	0.556	33.8	0.549	32.8	0.542	31.9	0.535	31.1	0.529	30.2	0.522	29.4
75	.0028	0.584	34.4	0.577	33.5	0.570	32.6	0.564	31.7	0.557	30.9	0.550	30.0
76	.0029	0.613	35.0	0.606	34.1	0.599	33.2	0.593	32.3	0.586	31.5	0.579	30.7
77	•0030	0.643	35.6	0.636	34.7	0.629	33.8	0.623	33.0	0.616	32.1	0.609	31.3
	.0031		123										
78	.0032	0.674	36.2	0.667	35.3	0.660	34.4	0.653	33.6	0.647	32.7	0.640	31.9
79	.0032	0.705	36.8	0.699	35.9	0.692	35.0	0.685	34.2	0.678	33.3	0.671	32.5
80		0.738	37.4	0.731	36.5	0.724	35.6	0.718	34.7	0.711	33.9	0.704	33.1
81	.0034	0.772	37.9	0.765	37.0	0.758	36.1	0.751	35.3	0.745	34.5	0.738	33.5
82	•0035	0.806	38.4	0.800	37.6	0.793	36.7	0.786	35.8	0.779	35.0	0.772	34.2
	.0036										0	0.000	
83	.0037	0.842	39.0	0.835	38.1	0.829	37.2	0.822	36.4	0.815	35.5	0.808	34.7
84	.0038	0.879	39.5	0.872	38.6	0.865	37.7	0.858	36.9	0.852	36.1	0.845	35.2
85	.0039	0.917	40.0	0.910	39.1	0.903	38.2	0.896	37.4	0.889	36.6	0.882	35.8
86	-0040	0.955	40.4	0.948	39.6	0.942	38.7	0.935	37.9	0.928	37.1	0.921	36.3
87		0.995	40.9	0.988	40.1	0.981	39.2	0.975	38.4	0.968	37.5	0.961	36.7
88	.0041	1.036	41.4	1.029	40.5	1.022	39.7	1.016	38.8	1.009	38.0	1.002	37.2
89	.0042	1.030	41.3	1.071	41.0	1.065	40.1	1.058	39.3	1.051	38.5	1.044	37.7
90	.0044	1.122	42.3	1.115	41.4	1.108	40.6	1.101	39.7	1.094	38.9	1.088	38.1
91	.0045	1.166	42.7	1.160	41.9	1.153	41.0	1.146	40.2	1.139	39.4	1.132	38.6
92	.0046	1.212	43.1	1.206	42.3	1.199	41.4	1.192	40.6	1.185	39.8	1.178	39.0
	.0048	1.012	,	2.200							100	R San	
93		1.260	43.5	1.253	42.7	1.246	41.9	1.239	41.0	1.232	40.2	1.225	39.4
94	.0049	1.308	43.9	1.301	43.1	1.294	42.3	1.287	41.4	1.280	40.6	1.274	39.9
95	.0050	1.358	44.3	1.351	43.5	1.344	42.7	1.337	41.8	1.330	41.0	1.323	40.3
96	•0051	1.408	44.7	1.402	43.9	1.395	43.0	1.388	42.2	1.381	41.4	1.374	40.7
97	.0053	1.461	45.1	1.454	44.3	1.447	43.4	1.440	42.6	1.433	41.8	1.426	41.1
98	•0054	1.515	45.5	1.508	44.6	1.501	43.8	1.494	43.0	1.487	42.2	1.480	41.4
0.0	.0056							2	40		40.0		43.0
99	.0057	1.570	45.8	1.563	45.0	1.556	44.2	1.550	43.4	1.543	42.6	1.536	41.8
100	.0059	1.627	46.2	1.620	45.4	1.613	44.5	1.607	43.7	1.600	43.0	1.593	42.2
101	.0060	1.686	46.5	1.679	45.7	1.672	44.9	1.665	44.1	1.658	43.3	1.651	42.5
102	.0062	1.746	46.8	1.739	46.0	1.732	45.2	1.725	44.4	1.718	43.7	1.711	42.9
103	.0063	1.807	47.2	1.800	46.4	1.793	45.6	1.786	44.8	1.779	44.0	1.772	43.2
104		1.870	47.5	1.863	46.7	1.856	45.9	1.849	45.1	1.842	44.3	1.835	

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

Wet-	Mean			t	t', or Di	Herence (	or Wet a	and Dry I	sulb Th	hermomet	ers.	Han 4	
Bulb Thermo- meter	Vertical Difference of Force of Vapor	24	0.0	24	°.5	25	0.0	250	.5	260	.0	26	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid ity.						
0		Eng. In.	348	Eng. In.	8.5	Eng. In.		Eng. In.		Eng. In.	178	Eng. In.	
32 33			*									Samuel .	
34		12-1							NE I				
35	1000	100		are h			9.0	win ve	12.0			Seller I	
36	Y	Wills &	3		2417	· .	-15	- == 0	1,00				3
0.00		(LEIS)	3									190.8	
37 38		1	100			1				3013		nudes,	1
39			- 8	72 7	2				-01				
40		- (2) A	1 65		J. of	Lan I						Burn. B	
41			kalin.	Laber 1	SIN	de la	1.11	-18/11	3.0	124.17		27 VI - S	3
			7						18			1000	
42			AV AV	100			O.B.	1000	40			Date Charles	
43	Valle V			COCH LIT		7.1		1000		7 444		Attests In	118
45				Viete I	TV at the			7777					
46				24.7	die.		and the						
	A SURI	218	1 / / /					111				Season !	
47	A	0.000	å.	0.010				J		VF115			A.
48	0.0013	0.019	2.4 3.9	0.012	1.5 3.0	0.018	2.2	0.011	1.3		ni-Sil	ALC: U	
50	.0013	0.031	5.2	0.025	4.4	0.018	3.6	0.024	2.7	0.018	2.0	0.011	1.
51	.0013	0.057	6.5	0.051	5.7	0.031	4.9	0.024	4.1	0.031	3.3	0.024	2.
The T	.0014									7.6			
52	.0014	0.071	7.8	0.064	7.0	0.058	6.1	0.051	5.3	0.044	4.6	0.038	3.
53	.0015	0.085	9.1	0.078	8.2	0.072	7.4	0.065	6.6	0.058	5.8	0.052	5.
54 55	.0015	0.100	10.3	0.093	9.4	0.086	8.6	0.080	7.8	0.073	7.0	0.067	7.
56	.0016	0.115	11.5	0.108	10.6	0.102	9.8	0.095	10.2	0.104	9.4	0.002	8.
00	.0016	0.130	32.1	0.124	11.0	0.117	11.0	0.111	1012	0.104	0.1	0.001	
57	.0017	0.147	13.8	0.140	13.0	0.133	12.1	0.127	11.3	0.120	10.6	0.113	9.
58	-0017	0.163	14.9	0.157	14.1	0.150	13.2	0.143	12.5	0.137	11.7	0.130	10.
59	.0018	0.180	16.0	0.174	15.2	0.167	14.3	0.161	13.6	0.154	12.8	0.147	12.
60	.0019	0.198	17.0	0.191	16.1	0.185	15.3	0.178	14.6 15.5	0.172	13.8	0.165	14.
V1	.0019	0.216	17.9	0.210	17.1	0.203	16.3	0.196	19.0	0.190	12.1	3.100	
62		0.235	18.9	0.229	18.1	0.222	17.2	0.215	16.5	0.209	15.7	0.202	15.
63	.0020 .0020	0.255	19.8	0.248	19.0	0.242	18.2	0.235	17.4	0.228	16.6	0.222	15.
64	.0020	0.275	20.7	0.269	19.9	0.262	19.1	0.255	18.3	0.248	17.5	0.242	16.
65	.0022	0.296	21.6	0.289	20.8	0.283	20.0	0.276	19.2	0.269	18.4	0.263	17.
66	•0023	0.318	22.5	0.311	21.7	0.304	20.9	0.297	20.1	0.291	19.3	0.306	19.
07		0.340	23.3	0.333	22.5	0.326	21.7	0.320	40.9	0.919	20.2	0.000	10.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t-t	, or Di	fference o	f Wet a	and Dry I	Bulb Th	nermomet	ers.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	240	.0	24	.5	250	.0	25	.5	260	.0	26	.5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.	544	Eng. In.	N 81	Eng. In.		Eng. In.		Eng. In.		Eng In.	197
68	0.0024	0.363	24.2	0.356	23.3	0.349	22.5	0.342	21.8	0.336	21.8	0.329	20.3
69	.0024	0.386	24.9	0.379	24.1	0.373	23.3	0.366	22.6	0.359	21.8	0.352	21.
70	.0025	0.410	25.7	0.403	24.9	0.397	24.1	0.390	23.3	0.383	22.6	0.377	21.9
71	.0026	0.435	26.4	0.428	25.6	0.422	24.9	0.415	24.1	0.408	23.3	0.402	22.
72	0035	0.461	27.2	0.454	26.4	0.448	25.6	0.441	24.8	0.434	24.1	0.427	23.
	.0027	0 400	07.0	0 .00	0.7.1	0	00.0	0.400	05.5	0.403	010	0.454	01
73	.0028	0.488	27.9	0.481	27.1	0.474	26.3	0.467	25.5	0.461	24.8	0.454	24.
74	.0028	0.515	28.5	0.508	27.7	0.502	27.0	0.495	26.2	0.488	25.5	0.481	24.
75	-0029	0.543	29.2	0.537	28.4	0.530	27.6	0.523	26.8	0.516	26.1	0.510	25.
76	.0030	0.572	29.8	0.566	29.1	0.559	28.3	0.552	27.4	0.545	26.8	0.539	26.
77	.0031	0.602	30.5	0.595	29.7	0.589	28.9	0.582	28.0	0.575	27.4	0.568	26.
78	.0031	0.633	31.1	0.626	30.3	0.619	29.5	0.613	28.7	0.606	28.0	0.599	27.
79	.0032	0.665	31.7	0.658	30.9	0.651	30.1	0.644	29.3	0.638	28.6	0.631	27.
	.0033	0.697	32.3	0.691	31.5	0.684	30.7	0.677	29.9	0.670	29.2	0.663	28.
80	-0034	0.037	32.8		32.1	0.717	31.3	0.711	30.5	0.704	29.8	0.697	29.
81	.0035	0.766	33.4	0.724	1	0.752	100	THE CO.			30.4	0.732	29.
82	.0036	0.700	99.4	0.759	32.6	0.752	31.8	0.745	31.0	0.738	50.4	0.752	49.
83	.0030	0.801	33.9	0.795	33.2	0.788	32.4	0.781	31.6	0.774	30.9	0.767	30.5
84	.0037	0.838	34.5	0.831	33.7	0.824	32.9	0.818	32.1	0.811	31.5	0.804	30.
85	.0038	0.876	35.0	0.869	34.2	0.862	33.4	0.855	32.7	0.848	32.0	0.842	31.
86	.0039	0.914	35.5	0.908	34.7	0.901	33.9	0.894	33.2	0.887	32.5	0.880	31.8
87	.0040	0.954	36.0	0.947	35.2	0.940	34.4	0.934	33.7	0.927	33.0	0.920	32.
01	.0041	0.334	30.0	0.947	30.2	0.340	94.4	0.334	30.7	0.521	00.0	0.020	02.0
88	Lec av	0.995	36.4	0.988	35.7	0.981	34.9	0.975	34.2	0.968	33.5	0.961	32.
89	.0042	1.037	36.9	1.030	36.1	1.024	35.4	1.017	34.7	1.010	33.9	1.003	33.5
90	.0044	1.081	37.4	1.074	36.6	1.067	35.8	1.060	35.1	1.053	34.4	1.046	33.
91	.0045	1.125	37.8	1.118	37.1	1.112	36.3	1.105	35.6	1.098	34.9	1.091	34.5
92	.0046	1.171	38.2	1.164	37.5	1.157	36.7	1.151	36.0	1.144	35.3	1.137	34.6
	.0048		7 19	1	97 10	THE STATE OF	1	2-715		2119	17		
93	4	1.218	38.7	1.211	37.9	1.205	37.1	1.198	36.5	1.191	35.7	1.184	35.0
94	.0049	1.267	39.1	1.260	38.3	1.253	37.5	1.246	36.9	1.239	36.2	1.232	35.
95	.0050	1.316	39.5	1.309	38.7	1.302	37.9	1.296	37.3	1.289	36.6	1.282	35.
96	.0051	1.367	39.9	1.360	39.1	1.353	38.3	1.346	37.7	1.340	37.0	1.333	36.
97	.0053	1.420	40.3	1.413	39.5	1.406	38.7	1.399	38.1	1.392	37.4	1.385	36.
98	.0054	1.473	40.7	1.467	39.9	1.460	39.1	1.453	38.5	1.446	37.8	1.439	37.
1 700	.0056	Part of	1,34	The state of			00 -		00.6		00.0		
99	.0057	1.529	41.1	1.522	40.3	1.515	39.5	1.508	38.9	1.501	38.2	1.494	37.
100	.0059	1.586	41.4	1.579	40.7	1.572	39.9	1.565	39.2	1.558	38.5	1.551	37.
101	.0060	1.644	41.8	1.637	41.0	1.630	40.3	1.623	39.6	1.616	38.9	1.609	38.
102	.0062	1.704	42.2	1.697	41.4	1.690	40.7	1.683	40.0	1.676	39.3	1.669	38.
103	.0063	1.765	42.5	1.758	41.8	1.751	41.0	1.745	40.3	1.738	39.6	1.731	38.
104	.0003	1.828	42.8	1.821	42.1	1.814	41.4	1.807	40.7	1.800	40.0	1.793	39.3

Correction for Barometrical Height above or below the Normal Height of 29.7 inches.

Baromet-	-		1100	Diffe	erence of	Thermo	meters,	or t-1	r Fahren	nheit.			
Height.	20	40	60	80	10°	12°	140	16°	180	20°	220	240	26°
					Wet 1	Bulb abo	ve the F	reezing-	Point.				14. W
Eng. In.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch
31.0	001	002	003	005	006	007	008	009	010	012	013	014	015
30.5	.001	.001	.002	.003	.004	.004	.005	.006	.006	.007	.008	.009	.009
30.0	000	000	001	001	001	002	002	002	002	003	003	003	00
29.5 29.0	+.000	+.000	+.001	+.001	+.001	+.001	+.001	+.001	+.002	+.002	+.002	+.002	+.002
28.5	.001	.001	.002	.003	.003	.004	.004	.005	.006	.006	.007	.008	.008
20.0	.001	.002	.003	.004	.005	.000	.007	.009	.010	.011	.012	.013	.014
28.0	.001	.003	.005	.006	.008	.009	.011	.012	.014	.015	.017	.018	.020
27.5	.002	.004	.006	.007	.010	.012	.014	.016	.018	.020	.022	.024	.026
27.0	.002	.005	.007	.009	012	.014	.017	.019	.022	.024	.027	.029	.031
26.5	.003	.006	.008	.011	.014	.017	.020	.023	.026	.029	.031	.034	.037
26.0	.003	.006	.010	.013	.016	.020	.023	.026	.030	.033	.036	.040	.042
25.5	.004	.007	.011	.014	.019	.022	.025	.030	.034	.037	.041	.045	.049
25.0		000	070	010	001	005	020	000	000	0.10	0.10	0=0	
24.0	.004	.008	.012	.016	.021	.025	.028	.033	.038	.042	.046	.050	.055
23.0	.005	.010	.015	.020	.025	.030	.034	.040	.046	.051	.056	.061	
22.0	.006	.012	.018	.023	.030	.035	.041	.047	.054	.060	.066	.072	.078
21.0	.008	.015	.023	.030	.038	.046	.053	.062	.070	.003	.085	.093	.101
20.0	+.008	+.017	+.026	+.034	+.043	+.051	+.059	+.069	+.078	+.086	+.095	+.104	+.113
			020	1.001						1.000			
			ulb belo					1	SVIJET			100 E	
		Fre	ezing-Po	int.		14-36	EXA	MPLI	E OF	CALC	CULAT	TION.	
31.0	001	002	003	004	006		1	Vet Bull	b above t	he Freez	ing-Poi	at.	
30.5	.001	.001	.002	.003	.003	t' :			$-\mathbf{t}' =$		1000		5 in.
30.0	000	000	001	001	001				s give f				
29.5	+.000	+.000	+.000	+.001	+.001				27.9 in		Force		Inch.
29.0	.001	.001	.002	.002	.003	Vap							0.403
28.5	.001	.002	.003	.004	.005	A	dditive	correct	tion, in	this t	able, fe	or	
	1.11	1 418 2	in a think	HE S	ST FE	B =	26.5 i	nches,	and 10°	2 2 1		=	0.014
23.0	.001	.003	.004	.005	.007	THE STO	Co	rrected	Force	of Var	oor	. =	0.417
27.5	.002	.003	.005	.007	.009	( E	13.14				47 85		ditor
27.0	.002	.004	.006	.008	.011	T	he mea	n baror	netrical	pressu	re, at a	given	place
26.5	.002	.005	.007	.010	.013				eing kr				
26.0	.003	.006	.009	.012	.014				may be				
25.5	.003	.007	.010	.013	.016				neans of				
25.0	.003	.007	.011	.015	.018				ied to				
24.0	.003	.007	.011	.015	.018				ce of va				
23.0	.005	.010	.016	.018	.022				g for t				
22.0	.006	.012	.018	.021		1.00			ir. Th			-	
21.0	.006	.014	.020	.027	.034				hat me				
20.0	+.007	+.015		+.030		1		f the re				Post	
	P. Lan	100	1		PALYE IN	La el		- TO 100	Mario Sp				3

#### TABLE VIII.

FOR DEDUCING THE RELATIVE HUMIDITY OF THE AIR FROM THE INDICATIONS, IN ENGLISH MEASURES, OF THE DEW-POINT INSTRUMENTS.

The object of every Dew-Point instrument is to ascertain, by causing a part of the apparatus to cool, the temperature at which the vapor contained in the air begins to condense, in the shape of light dew, on the cooled portion of the instrument. It is obvious that this is the temperature at which the atmosphere itself, if cooled likewise, would be fully saturated by the amount of vapor present in the air at the time of the observation.

The temperature of the dew-point being known, all the hygrometrical conditions of the air can be easily deduced from it.

The Absolute Humidity, or the total amount of vapor in the atmosphere, is expressed by the number, in the Tables of Elastic Forces of Vapor, due to that temperature.

The Relative Humidity, or the degree of moisture, being the ratio of the quantity of vapor actually contained in the air to the quantity it could contain if fully saturated, is expressed by the proportion

Relative Humidity: 1:: Force of Vapor at Dew-Point: Maximum Force of Vapor.

Calling the

Force of Vapor at the Temperature of the Dew-Point, f; Force of Vapor at the Temperature of the Air, F;

then

Relative Humidity =  $\frac{f}{F}$ .

It is thus found by dividing the force of vapor due, in the Table of Elastic Forces, to the temperature of the dew-point, by the maximum of the force of vapor due, in the same table, to the temperature of the air at the time of the observation. F being always greater than f, when the air is not saturated, the Relative Humidity is expressed by a fraction, which is termed the *fraction of saturation*. Making the point of saturation = 100, in order to obtain this fraction in hundredths, we have

Relative Humidity =  $\frac{f \times 100}{F}$ .

### Example.

Suppose the

Temperature of the Air, or t, to be  $= 43^{\circ}$  F.

Temperature of the Dew-Point, or t', to be  $= 35^{\circ}$  F.

Difference between the two, or t-t', to be = 8° F.

Taking in Table VI. the Elastic Forces due to t and t', we have

Force of Vapor at  $t' = \frac{.2087 \times 100}{.2775} = 73.4$ , Relative Humidity in Hundredths.

The following Table VIII. gives, in hundredths, the fraction of saturation, or Relative Humidity, corresponding to each degree of t', or of the temperature of the air, from 0° to 104°; and for every half degree of t—t', or of the difference between the temperature of the air and of the dew-point, from 0.°5 to 24.°5. Regnault's Table of Elastic Forces of Vapor, reduced to English measures, has been used in the computation.

Though the fraction of saturation expressed in hundredths indicates the Relative Humidity with sufficient accuracy, the thousandths have been added to facilitate, as remarked above in the preface to the Psychrometrical Tables, the interpolations for any number falling between those given in the table.

### USE OF THE TABLE.

### Example.

Temperature of Air, or t, being = 62° F. Temperature of the Dew-Point, or t', = 53° F. Difference, or t-t', = 9° F.

Find out the Relative Humidity.

In the column of temperatures, the first on the left, find 62°; on the same horizontal line, in the column headed 9°, is found 72.4, which is the Relative Humidity required.

Should it seem desirable to compute the Relative Humidity for values of t-1' not contained in the table, the factors given below in Table IX. may be used. It may be seen, however, that an interpolation at sight will always suffice for meteorological purposes.

## VIII.

### FOR DEDUCING THE RELATIVE HUMIDITY OF THE AIR,

FROM THE INDICATIONS OF DEW-POINT INSTRUMENTS.

Relative Humidity expressed in Hundredths, full Saturation being = 100.

Temper- ature	W-1917 19. 153	$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Temperat	ures of the	Air and of	f the Dew-	Point. — F	hrenheit.	
of Air, Fahren- heit.	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
0°	100.	97.7	95.4	93.2	91.0	88.9	86.8	84.8	82.8	80.9
1	100.	97.7	95.5	93.3	91.1	89.0	86.9	84.9	82.9	81.0
2	100.	97.7	95.5	93.3	91.2	89.1	87.0	85.0	83.0	81.1
3	100.	97.8	95.5	93.4	91.2	89.2	87.1	85.1	83.1	81.2
4	100.	97.8	95.6	93.4	91.3	89.2	87.2	85.2	83.2	81.3
March 1	S., S.	Falls I	100	Thursday.	NEW OF		1875	1.00	The state of	
5	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.3	83.3	81.4
6	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.3	83.3	81.5
7	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.3	83.4	81.5
8	100.	97.8	95.6	93.5	91.3	89.3	87.3	85.3	83.4	81.5
9	100.	97.8	95.6	93.5	91.3	89.3	87.3	85.3	83.4	81.5
	Part I	177 1	0.12.0	75.56.27	Y-75		No.	3.10		
10	100.	97.8	95.6	93.4	91.3	89.3	87.3	85.3	83.4	81.5
11	100.	97.8	95.6	93.4	91.3	89.3	87.3	85.3	83.4	81.6
12	100.	97.8	95.5	93.4	91.3	89.3	87.3	85.4	83.4	81.6
13	100.	97.8	95.5	93.4	91.3	89.3	87.3	85.4	83.5	81.6
14	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.4	83.5	81.7
	<b>WEST</b>	1918				malov con		-	Service of the servic	MEN
15	100.	97.7	95.5	93.4	91.3	89.4	87.4	85.5	83.5	81.7
16	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.4	83.5	81.6
17	100.	97.7	95.5	93.4	91.3	89.3	87.3	83.3	83.4	81.6
18	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.3	83.4	81.5
19	100.	97.8	95.5	93.4	91.3	89.3	87.2	85.2	83.3	81.4
	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5

75

Temper-		$\mathbf{t} - \mathbf{t}^{t} = 1$	Difference o	of Tempera	tures of the	e Air and o	f the Dew-	Point. — F	ahrenheit.	
ature of Air, Fahren- heit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
0°	79.0	77.2	75.4	73.6	71.9	70.1	69.5	66.9	65.3	63.7
1	79.1	77.3	75.5	73.7	72.0	70.2	68.6	67.0	65.4	63.8
2	79.2	77.4	75.6	73.8	72.1	70.3	68.7	67.1	65.5	64.0
3	79.3	77.5	75.7	73.9	72.2	70.5	68.8	67.2	65.6	64.1
. 4	79.4	77.6	75.8	74.0	72.3	70.6	68.9	67.3	65.7	64.2
5	79.5	77.7	75.9	74.1	72.4	70.7	69.1	67.4	65.8	64.4
6	79.6	77.8	76.0	74.2	72.5	70.8	69.2	67.6	66.0	64.5
7	79.6	77.8	76.0	74.3	72.6	70.9	69.3	67.7	66.1	64.6
8	79.6	77.9	76.1	74.4	72.7	71.0	69.4	67.8	66.2	64.7
9	79.7	77.9	76.1	74.4	72.7	71.1	69.5	67.9	66.3	64.8
10	79.7	77.9	76.2	74.5	72.8	71.2	69.6	68.0	66.4	64.9
11	79.7	78.0	76.2	74.5	72.8	71.2	69.6	68.0	66.5	64.9
12	79.8	78.0	76.2	74.5	72.9	71.2	69.6	68.0	66.5	65.0
13	79.8	78.0	76.3	74.6	72.9	71.3	69.6	68.1	66.5	65.0
14	79.8	78.1	76.3	74.6	72.9	71.3	69.6	68.1	66.5	65.1
15	79.8	78.1	76.3	74.6	72.9	71.3	69.7	68.1	66.6	65.1
16	79.8	78.0	76.2	74.5	72.9	71.2	69.6	68.1	66.5	65.1
17	79.7	77.9	76.1	74.5	72.8	71.2	69.6	68.0	66.5	65.0
18	79.6	77.8	76.1	74.4	72.7	71.1	69.5	68.0	66.5	65.0
19	79.6	77.8	76.0	74.3	72.7	71.1	69.5	68.0	66.4	65.0
		1110	70.0	71.0	12.1	11.1	05.0	03.0	00.4	0010
	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.5
	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.5
0° 1					<b>12.0</b> 56.3	- 4				
0°	10.0	60.7	<b>11.0</b> 59.2	11.5 57.7	12.0	<b>12.5</b> 54.9	<b>13.0</b> 53.6	13.5 52.3	14.0 51.0	<b>14.5</b> 49.8
0° 1	10.0 62.1 62.3	60.7 60.8	59.2 59.3	57.7 57.9	12.0 56.3 56.5	12.5 54.9 55.1	13.0 53.6 53.7	13.5 52.3 52.5	51.0 51.2	14.5 49.8 50.0
0° 1 2	62.1 62.3 62.4	60.7 60.8 61.0	59.2 59.3 59.5	57.7 57.9 58.1	56.3 56.5 56.6	12.5 54.9 55.1 55.3	13.0 53.6 53.7 53.9	52.3 52.5 52.7	51.0 51.2 51.4	49.8 50.0 50.1
0° 1 2 3	62.1 62.3 62.4 62.6	60.7 60.8 61.0 61.1 61.3	59.2 59.3 59.5 59.6	57.7 57.9 58.1 58.2	56.3 56.5 56.6 56.8 57.0	12.5 54.9 55.1 55.3 55.5 55.7	53.6 53.7 53.9 54.1 54.3	52.3 52.5 52.7 52.8	51.0 51.2 51.4 51.5	49.8 50.0 50.1 50.3
0° 1 2 3 4	62.1 62.3 62.4 62.6 62.7	60.7 60.8 61.0 61.1	59.2 59.3 59.5 59.6 59.8	57.7 57.9 58.1 58.2 58.4	56.3 56.5 56.6 56.8	12.5 54.9 55.1 55.3 55.5	53.6 53.7 53.9 54.1	52.3 52.5 52.7 52.8 53.0	51.0 51.2 51.4 51.5 51.7	49.8 50.0 50.1 50.3 50.5
0° 1 2 3 4	62.1 62.3 62.4 62.6 62.7 62.9	60.7 60.8 61.0 61.1 61.3 61.4	59.2 59.3 59.5 59.6 59.8 60.0	57.7 57.9 58.1 58.2 58.4 58.6	56.3 56.5 56.6 56.8 57.0	12.5 54.9 55.1 55.3 55.5 55.7 55.8	53.6 53.7 53.9 54.1 54.3	52.3 52.5 52.7 52.8 53.0	51.0 51.2 51.4 51.5 51.7	49.8 50.0 50.1 50.3 50.5
0° 1 2 3 4 5 6 7 8	62.1 62.3 62.4 62.6 62.7 62.9 63.0	60.7 60.8 61.0 61.1 61.3 61.4 61.5	59.2 59.3 59.5 59.6 59.8 60.0 60.1	57.7 57.9 58.1 58.2 58.4 58.6 58.7	56.3 56.5 56.6 56.8 57.0 57.2 57.3	12.5 54.9 55.1 55.3 55.5 55.7 55.8 55.9	53.6 53.7 53.9 54.1 54.3 54.5 54.6	52.3 52.5 52.7 52.8 53.0 53.2 53.3	51.0 51.2 51.4 51.5 51.7 51.9 52.0	49.8 50.0 50.1 50.3 50.5 50.7 50.8
0° 1 2 3 4 5 6 7	62.1 62.3 62.4 62.6 62.7 62.9 63.0 63.1	60.7 60.8 61.0 61.1 61.3 61.4 61.5 61.7	59.2 59.3 59.5 59.6 59.8 60.0 60.1 60.2	57.7 57.9 58.1 58.2 58.4 58.6 58.7 58.8	56.3 56.5 56.6 56.8 57.0 57.2 57.3 57.4	54.9 55.1 55.3 55.5 55.7 55.8 55.9 56.0	53.6 53.7 53.9 54.1 54.3 54.5 54.6 54.7	52.3 52.5 52.7 52.8 53.0 53.2 53.3 53.4	51.0 51.2 51.4 51.5 51.7 51.9 52.0 52.1	49.8 50.0 50.1 50.3 50.5 50.7 50.8 50.9
0° 1 2 3 4 5 6 7 8	62.1 62.3 62.4 62.6 62.7 62.9 63.0 63.1 63.2	60.7 60.8 61.0 61.1 61.3 61.4 61.5 61.7 61.8	59.2 59.3 59.5 59.6 59.8 60.0 60.1 60.2 60.3	57.7 57.9 58.1 58.2 58.4 58.6 58.7 58.8 58.9	56.3 56.5 56.6 56.8 57.0 57.2 57.3 57.4 57.5	54.9 55.1 55.3 55.5 55.7 55.8 55.9 56.0 56.2	53.6 53.7 53.9 54.1 54.3 54.5 54.6 54.7 54.8	52.3 52.5 52.7 52.8 53.0 53.2 53.3 53.4 53.5	51.0 51.2 51.4 51.5 51.7 51.9 52.0 52.1 52.3	49.8 50.0 50.1 50.3 50.5 50.7 50.8 50.9 51.0
0° 1 2 3 4 5 6 7 8 9	62.1 62.3 62.4 62.6 62.7 62.9 63.0 63.1 63.2 63.3	60.7 60.8 61.0 61.1 61.3 61.4 61.5 61.7 61.8 61.9	59.2 59.3 59.5 59.6 59.8 60.0 60.1 60.2 60.3 60.4	57.7 57.9 58.1 58.2 58.4 58.6 58.7 58.8 58.9 59.0	56.3 56.5 56.6 56.8 57.0 57.2 57.3 57.4 57.5 57.6	12.5 54.9 55.1 55.3 55.5 55.7 55.8 55.9 56.0 56.2 56.3	53.6 53.7 53.9 54.1 54.3 54.5 54.6 54.7 54.8 54.9	52.3 52.5 52.7 52.8 53.0 53.2 53.3 53.4 53.5 53.6	51.0 51.2 51.4 51.5 51.7 51.9 52.0 52.1 52.3 52.4	49.8 50.0 50.1 50.3 50.5 50.7 50.8 50.9 51.0 51.2
0° 1 2 3 4 5 6 7 8 9	62.1 62.3 62.4 62.6 62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5	60.7 60.8 61.0 61.1 61.3 61.4 61.5 61.7 61.8 61.9	59.2 59.3 59.5 59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.6	57.7 57.9 58.1 58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3	56.3 56.5 56.6 56.8 57.0 57.2 57.3 57.4 57.5 57.6 57.7	54.9 55.1 55.3 55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6	53.6 53.7 53.9 54.1 54.3 54.5 54.6 54.7 54.8 54.9	52.3 52.5 52.7 52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8	51.0 51.2 51.4 51.5 51.7 51.9 52.0 52.1 52.3 52.4	49.8 50.0 50.1 50.3 50.5 50.7 50.8 50.9 51.0 51.2 51.3 51.4 51.5
0° 1 2 3 4 5 6 7 8 9 10 11 12 13	62.1 62.3 62.4 62.6 62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5 63.5	60.7 60.8 61.0 61.1 61.3 61.4 61.5 61.7 61.8 61.9 62.1 62.1 62.1 62.2	59.2 59.3 59.5 59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.6 60.6	57.7 57.9 58.1 58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3 59.3	56.3 56.5 56.6 56.8 57.0 57.2 57.3 57.4 57.5 57.6	54.9 55.1 55.3 55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6 56.6	53.6 53.7 53.9 54.1 54.3 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2 55.3	52.3 52.5 52.7 52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 53.9 54.0 54.1	51.0 51.2 51.4 51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7 52.8	49.8 50.0 50.1 50.3 50.5 50.7 50.8 50.9 51.0 51.2 51.3 51.4 51.5 51.6
0° 1 2 3 4 5 6 7 8 9	62.1 62.3 62.4 62.6 62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5	60.7 60.8 61.0 61.1 61.3 61.4 61.5 61.7 61.8 61.9	59.2 59.3 59.5 59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.6	57.7 57.9 58.1 58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3	56.3 56.5 56.6 56.8 57.0 57.2 57.3 57.4 57.5 57.6 57.7	54.9 55.1 55.3 55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6	53.6 53.7 53.9 54.1 54.3 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2	52.3 52.5 52.7 52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 53.9 54.0	51.0 51.2 51.4 51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7	49.8 50.0 50.1 50.3 50.5 50.7 50.8 50.9 51.0 51.2 51.3 51.4 51.5
0° 1 2 3 4 5 6 7 8 9 10 11 12 13 14	62.1 62.3 62.4 62.6 62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5 63.5	60.7 60.8 61.0 61.1 61.3 61.4 61.5 61.7 61.8 61.9 62.1 62.1 62.1 62.2 62.3	59.2 59.3 59.5 59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.6 60.6	57.7 57.9 58.1 58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3 59.3	56.3 56.5 56.6 56.8 57.0 57.2 57.3 57.4 57.5 57.6	54.9 55.1 55.3 55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6 56.6	53.6 53.7 53.9 54.1 54.3 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2 55.3	52.3 52.5 52.7 52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 53.9 54.0 54.1	51.0 51.2 51.4 51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7 52.8	49.8 50.0 50.1 50.3 50.5 50.7 50.8 50.9 51.0 51.2 51.3 51.4 51.5 51.6
0° 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	62.1 62.3 62.4 62.6 62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5 63.5 63.6	60.7 60.8 61.0 61.1 61.3 61.4 61.5 61.7 61.8 61.9 62.1 62.1 62.1 62.2 62.3 62.3	59.2 59.3 59.5 59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.6 60.7 60.8	57.7 57.9 58.1 58.2 58.4 58.6 58.7 58.8 59.0 59.1 59.2 59.3 59.3 59.4	56.3 56.5 56.6 56.8 57.0 57.2 57.3 57.4 57.5 57.6 57.7 57.8 57.9 58.0 58.1	54.9 55.1 55.3 55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6 56.6 56.6	53.6 53.7 53.9 54.1 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2 55.3 55.4	52.3 52.5 52.7 52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 53.9 54.0 54.1 54.2	51.0 51.2 51.4 51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7 52.8 52.9	49.8 50.0 50.1 50.3 50.5 50.7 50.8 50.9 51.0 51.2 51.3 51.4 51.5 51.6 51.7
0° 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	62.1 62.3 62.4 62.6 62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5 63.5 63.6 63.6 63.6 63.6	60.7 60.8 61.0 61.1 61.3 61.4 61.5 61.7 61.8 61.9 62.1 62.1 62.2 62.3 62.3 62.3 62.2	59.2 59.3 59.5 59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.7 60.8 60.8 60.8	57.7 57.9 58.1 58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3 59.3 59.4 59.5 59.5	56.3 56.5 56.6 56.8 57.0 57.2 57.3 57.4 57.5 57.6 57.7 57.8 57.9 58.0 58.1 58.1 58.1	54.9 55.1 55.3 55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6 56.6 56.7	53.6 53.7 53.9 54.1 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2 55.3 55.4 55.5 55.5 55.5	52.3 52.5 52.7 52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 53.9 54.0 54.1 54.2	51.0 51.2 51.4 51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7 52.8 52.9 53.0 53.0 53.0 53.0	49.8 50.0 50.1 50.3 50.5 50.7 50.8 50.9 51.0 51.2 51.3 51.4 51.5 51.6 51.7
0° 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	62.1 62.3 62.4 62.6 62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5 63.5 63.6	60.7 60.8 61.0 61.1 61.3 61.4 61.5 61.7 61.8 61.9 62.1 62.1 62.1 62.2 62.3 62.3	59.2 59.3 59.5 59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.6 60.7 60.8 60.8	57.7 57.9 58.1 58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3 59.3 59.4 59.5	56.3 56.5 56.6 56.8 57.0 57.2 57.3 57.4 57.5 57.6 57.7 57.8 57.9 58.0 58.1	54.9 55.1 55.3 55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6 56.6 56.7	53.6 53.7 53.9 54.1 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2 55.3 55.4	52.3 52.5 52.7 52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 53.9 54.0 54.1 54.2	51.0 51.2 51.4 51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7 52.8 52.9 53.0 53.0 53.0	49.8 50.0 50.1 50.3 50.5 50.7 50.8 50.9 51.0 51.2 51.3 51.4 51.5 51.6 51.7

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Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Tempera	tures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
Fahren- heit.	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5
0°	48.5	47.3	46.1	45.0	43.9	42.8	41.6	40.6	39.5	38.5
1	48.7	47.5	46.3	45.2	44.0	42.9	41.8	40.8	39.7	38.7
2	48.9	47.7	46.5	45.4	44.2	43.1	42.0	41.0	39.9	38.9
3	49.1	47.9	46.7	45.5	44.4	43.3	42.2	41.2	40.2	39.2
4	49.3	48.1	46.9	45.7	44.6	43.5	42.4	41.4	40.4	39.4
	123	BO P	P =4 -	~ 0	Total !	MAN THE	# Sept.	Three or	THE T	18%
5	49.4	48.2	47.1	45.9	44.8	43.7	42.6	41.6	40.6	39.6
6	49.6	48.4	47.2	46.1	44.9	43.9	42.8	41.8	40.7	39.8
7	49.7	48.5	47.3	46.2	45.1	44.0	42.9	41.9	40.9	39.9
8	49.8	48.7	47.5	46.4	45.3	44.2	43.1	42.1	41.1	40.1
9	50.0	48.8	47.6	46.5	45.4	44.3	43.3	42.2	41.2	40.2
10	50.1	48.9	47.8	46.7	45.6	44.5	43.4	42.4	41.4	40.4
11	50.2	49.0	47.9	46.8	45.7	44.6	43.5	42.5	41.5	40.5
12	50.3	49.1	48.0	46.9	45.8	44.7	43.6	42.6	41.6	40.6
13	50.4	49.2	48.1	47.0	45.9	44.8	43.7	42.7	41.7	40.7
14	50.5	49.3	48.2	47.1	46.0	44.9	43.8	42.8	41.8	40.8
	50 G	40.4	40.0	470	40.1	45.0	40.0	40.0	43.0	10.0
15	50.6	49.4	48.3	47.2	46.1	45.0	43.9	42.9	41.9	40.9
16	50.6	49.5	48.3	47.2	46.1	45.0	44.0	43.0	41.9	41.0
17 18	50.6	49.5	48.3	47.2	46.1	45.0 45.0	44.0	43.0	42.0	41.0
19	50.6	49.5	48.3	47.3	46.2	45.1	44.1	43.1	42.0	41.1
	7.15	4000	440		US CALL LA					
	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.5
0°	37.5	36.5	35.5	34.6	33.7	32.8	31.9	31.0	30.2	29.3
1	37.7	36.8	35.8	34.8	33.9	33.0	32.1	31.3	30.4	29.6
2	37.9	37.0	36.0	35.1	34.2	33.3	32.4	31.5	30.7	29.9
3	38.2	37.2	36.2	35.3	34.4	33.5	32.6	31.8	30.9	30.1
4	38.4	37.4	36.5	35.6	34.6	33.8	32.9	32.0	31.2	30.4
5	38.6	37.7	36.7	35.8	34.9	34.0	33.1	32.3	31.4	30.6
6	38.8	37.8	36.9	36.0	35.0	34.2	33.3	32.5	31.6	30.8
7	38.9	38.0	37.0	36.1	35.2	34.3	33.5	32.6	31.8	31.0
8	39.1	38.1	37.2	36.3	35.4	34.5	33.6	32.8	32.1	31.2
9	39.2	38.3	37.3	36.4	35.5	34.7	33.8	33.0	32.3	31.4
10	39.4	38.4	37.5	36.6	35.7	34.8	34.0	33.1	32.5	31.6
11	39.5	38.6	37.6	36.7	35.8	35.0	34.1	33.3	32.6	31.7
12	39.6	38.7	37.8	36.9	36.0	35.1	34.2	33.4	32.7	31.8
13	39.8	38.8	37.9	37.0	36.1	35.2	34.4	33.6	32.8	32.0
14	39.9	39.0	38.0	37.1	36.2	35.4	34.5	33.7	32.9	32.1
15	100	20.1	90.0	0.00	96.4	95.5	04-	00.0		The same
15 16	40.0	39.1	38.2	37.3	36.4	35.5	34.7	33.9	33.0	32.2
17	40.0	39.1 39.2	38.2 38.2	37.3	36.4	35.6	34.7	33.9	33.1	32.3
		of the second second second		37.4	36.5	35.6	34.8	34.0	33.1	32.4
18	40.1	39.2	38.3	37.4	36.5	35.7	34.8	34.0	33.2	32.4

Temper- ature of Air,	TVE TOS	$\mathbf{t} - \mathbf{t}' = 1$	Difference of	of Tempera	tures of th	e Air and o	of the Dew-	Point. — F	ahrenheit.	
Sahren- heit.	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.
20°	100.	97.8	95.6	93.4	91.3	89.2	87.2	85.2	83.2	81
21	100.	97.8	95.6	93.4	91.3	89.3	87.3	85.3	83.3	81
22	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.4	83.4	81
23	100.	97.8	95.6	93.5	91.4	89.4	87.4	85.5	83.5	81
24	100.	97.8	95.7	93.5	91.5	89.5	87.5	85.5	83.6	81
25	100.	97.8	. 95.7	93.6	91.5	89.5	87.6	85.6	83.7	81
26	100.	97.8	95.7	93.6	91.6	89.6	87.7	85.7	83.8	82
27	100.	97.9	95.8	93.7	91.7	89.7	87.8	85.9	84.0	82
28	100.	97.9	95.8	93.8	91.8	89.8	87.9	86.0	84.1	82
29	100.	97.9	95.9	93.8	91.8	89.9	88.0	86.1	84.2	82
30	100.	97.9	95.9	93.9	91.9	90.0	88.1	86.2	84.3	82
31	100.	98.0	96.0	94.0	92.0	90.1	88.2	86.4	84.5	82
32	100.	98.0	96.0	94.0	92.1	90.2	88.4	86.6	84.7	83
33	100.	98.0	96.1	94.1	92.2	90.4	88.6	86.7	84.9	83
34	100.	98.0	96.1	94.2	92.3	90.5	88.7	86.9	85.1	83
35	100.	98.0	96.1	94.3	92.4	90.6	88.9	87.1	85.3	83
36	100.	98.1	96.2	94.3	92.5	90.7	88.9	87.1	85.4	83
37	100.	98.1	96.2	94.3	92.5	90.7	88.9	87.2	85.4	83
38	100.	98.1	96.2	94.3	92.5	90.7	89.0	87.2	85.5	83
39	100.	98.1	96.2	94.3	92.5	90.7	89.0	87.2	85.5	83
40	100.	98.1	96.2	94.4	92.5	90.8	89.0	87.3	85.6	83
41	100.	98.1	96.2	94.4	92.6	90.8	89.1	87.3	85.7	84
42	100.	98.1	96.2	94.4	92.6	90.8	89.1	87.4	85.7	84
43	100.	98.1	96.3	94.4	92.6	90.9	89.2	87.5	85.8	84
44	100.	98.1	96.3	94.5	92.7	90.9	89.2	87.5	85.9	84
45	100.	98.1	96.3	94.5	92.7	91.0	89.3	87.6	85.9	84
46	100.	98.1	96.3	94.5	92.7	91.0	89.3	87.6	86.0	84
47	100.	98.1	96.3	94.5	92.8	91.0	89.3	87.7	86.0	84
48	100.	98.2	96.3	94.6	92.8	91.1	89.4	87.7	86.1	84
49	100.	98.2	96.4	94.6	92.8	91.1	89.4	87.7	86.1	84
50	100.	98.2	96.4	94.6	92.9	91.1	89.4	87.8	86.2	84
51	100.	98.2	96.4	94.6	92.9	91.2	89.5	87.8	86.2	84
52	100.	98.2	96.4	94.6	92.9	91.2	89.5	87.9	86.3	84
53	100.	98.2	96.4	94.7	92.9	91.2	89.6	87.9	86.3	84
54	100.	98.2	96.4	94.7	93.0	91.3	89.6	88.0	86.4	84
55 56	100.	98.2 98.2	96.5	94.7	93.0	91.3	89.7 89.7	88.0 88.1	86.4 86.5	84
a Harri	The same	12550.3	96.5	94.7	Callet d	91.4	8.24	Par Liberton	K INDEED	1
57 58	100.	98.2 98.2	96.5 96.5	94.8	93.1 93.1	91.4 91.4	89.7	88.1 88.2	86.5	85 85
59	100.	98.2	96.5	94.8	93.1	91.5	89.8	88.2	86.6	85
60	100.	98.2	96.5	94.8	93.2	91.5	89.9	88.3	86.7	85
61	100.	98.3	96.5	94.9	93.2	91.5	89.9	88.3	86.7	85
62	100.	98.3	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85
	0.0	0.5	1.0							-

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Temperat	tures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
Fahren- heit.	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
62°	100.	98.3	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.3
63	100.	98.3	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.3
64	100.	98.3	96.6	94.9	93.3	91.6	90.0	88.5	86.9	85.3
65	100.	98.3	96.6	94.9	93.3	91.7	90.1	88.5	86.9	85.4
66	100.	98.3	96.6	94.9	93.3	91.7	90.1	88.5	87.0	85.4
67	100.	98.3	96.6	95.0	93.3	91.7	90.1	88.6	87.0	85.5
-68	100.	98.3	96.6	95.0	93.4	91.8	90.2	88.6	87.1	85.5
69	100.	98.3.	96.6	95.0	93.4	91.8	90.2	88.7	87.2	85.6
70	100.	98.3	96.7	95.0	93.4	91.8	90.3	88.7	87.2	85.7
71	100.	98.3	96.7	95.0	93.4	91.9	90.3	88.8	87.2	85.8
72	100.	98.3	96.7	95.1	93.5	91.9	90.3	88.8	87.3	85.8
73	100.	98.3	96.7	95.1	93.5	91.9	90.4	88.8	87.3	85.9
74	100.	98.3	96.7	95.1	93.5	91.9	90.4	88.9	87.4	85.9
75	100.	98.3	96.7	95.1	93.5	92.0	90.4	88.9	87.4	86.0
76	100.	98.3	96.7	95.1	93.6	92.0	90.5	89.0	87.5	86.0
77	100.	98.4	96.7	95.2	93.6	92.0	90.5	89.0	87.5	86.1
73	100.	98.4	96.7	95.2	93.6	92.1	90.5	89.1	87.6	86.1
79	100.	93.4	96.8	95.2	93.6	92.1	90.6	89.1	87.6	86.2
80	100.	98.4	96.8	95.2	93.6	92.1	90.6	89.1	87.7	86 2
81	100.	98.4	96.8	95.2	93.7	92.1	90.6	89.2	87.7	86.8
82	100.	98.4	96.8	95.2	93.7	92.2	90.7	89.2	87.8	86.8
83	100.	98.4	96.8	95.3	93.7	92.2	90.7	89.3	87.8	86.4
84	100.	98.4	96.8	95.3	93.7	92.2	90.8	89.3	87.8	86.4
85	100.	98.4	96.8	95.3	93.8	92.3	90.8	89.3	87.9	86.5
86	100.	98.4	96.8	95.3	93.8	92.3	90.8	89.4	87.9	86.5
87	100.	98.4	96.9	95.3	93.8	92.3	90.9	89.4	88.0	86.6
88	100.	98.4	96.9	95.3	93.8	92.3	90.9	89.4	88.0	86.6
89	100.	98.4	96.9	95.4	93.9	92.4	90.9	89.5	88.1	86.7
90	100.	98.4	96.9	95.4	93.9	92.4	91.0	89.5	88.1	86.7
91	100.	98.4	96.9	95.4	93.9	92.4	91.0	89.6	88.2	86.8
92	100.	98.5	96.9	95.4	93.9	92.5	91.0	89.6	88.2	86.8
93	100.	98.5	96.9	95.4	93.9	92.5	91.1	89.6	88.2	86.9
94	100.	98.5	96.9	95.4	94.0	92.5	91.1	89.7	88.3	86.9
95	100.	98.5	97.0	95.5	94.0	92.5	91.1	89.7	88.3	87.0
96	100.	98.5	97.0	95.5	94.0	92.6	91.2	89.7	88.4	87.0
			97.0	95.5	94.0	92.6	91.2	89.8	88.4	
97 93	100.	98.5 98.5	97.0	95.5	94.0	92.6	91.2	89.8	88.4	87.1 87.1
99	100.	98.5	97.0	95.5	94.1	92.7	91:3	89.9	88.5	87.1
100	100.	98.5	97.0	95.6	94.1	92.7	91.3	89.9		
	C. V. C. C. C.	The second second		The same of the sa	The state of the s		The state of the state of the	The same of the sa	88.5	87.2
101	100.	98.5	97.0	95.6	94.1	92.7	91.3	89.9	88.6	87.2
102	100.	98.5	97.0	95.6	94.2	92.7	91.4	90.0	88.6	87.3
103	100.	98.5 98.5	97.0 97.0	95.6 95.6	94.2	92.8 92.8	91.4	90.0	88.7	87.4
1			-		-	_				
	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5

Temper- ature		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Temperat	tures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
20°	79.5	77.7	75.9	74.2	72.6	71.0	69.4	67.9	66.4	64.9
21	79.6	77.8	76.0	74.3	72.7	71.1	69.5	68.0	66.4	65.0
22	79.7	77.9	76.1	74.4	72.8	71.2	69.6	68.0	66.5	65.0
23	79.8	78.0	76.2	74.6	72.9	71.3	69.6	68.1	66.5	65.0
24	79.9	78.1	76.4	74.7	73.0	71.4	69.7	68.1	66.6	65.1
25	80.0	78.2	76.5	74.8	73.1	71.5	69.8	68.2	66.6	65.1
26	80.2	78.4	76.6	74.9	73.2	71.7	70.0	68.4	66.8	65.5
27	80.3	78.5	76.8	75.1	73.4	71.8	70.1	68.6	67:0	65.
28	80.5	78.7	76.9	75.2	73.6	72.0	70.3	68.8	67.2	65.
29	80.6	78.8	77.1	75.4	73.7	72.1	70.5	68.9	67.4	65.
30	80.7	78.9	77.2	75.6	73.9	72.3	70.7	69.1	67.6	66.
31	81.0	79.2	77.5	75.8	74.2	72.6	71.0	69.4	67.9	66.
32	81.2	79.4	77.7	76.1	74.4	72.8	71.3	69.7	68.2	66.
33	81.4	79.7	78.0	76.4	74.7	73.1	71.5	70.0	68.5	67.
34	81.7	79.9	78.3	.76.6	75.0	73.4	71.8	70.3	68.8	67.
35	81.9	80.2	78.5	76.9	75.3	73.7	72.1	70.6	69.1	67.
36	82.0	80.3	78.6	77.0	75.4	73.9	72.3	70.8	69.3	67.
37	82.0	80.4	78.8	77.2	75.6	74.0	72.5	71.0	69.5	68.
38	82.1	80.5	78.9	77.3	75.8	74.2	72.7	71.2	69.8	68.
39	82.2	80.6	79.0	77.4	75.9	74.4	72.9	71.5	70.0	68.
40	82.3	80.7	79.1	77.6	76.1	74.6	73.2	71.7	70.2	68.
41	82.4	80.8	79.2	77.7	76.2	74.7	73.2	71.8	70.3	68.
42	82.5	80.9	79.3	77.8	76.3	74.8	73.3	71.9	70.5	69.
43	82.5	80.9.	79.4	77.9	76.4	74.9	73.4	72.0	70.6	69.
44	82.6	81.0	79.5	78.0	76.5	75.0	73.5	72.1	70.7	69.
45	82.7	81.1	79.6	78.0	76.5	75.1	73.6	72.2	70.8	69.
46	82.8	81.2	79.6	78.1	76.6	75.1	73.7	72.3	70.9	69.
47	82.8	81.2	79.7	78.2	76.7	75.2	73.8	72.4	71.0	69.
48	82.9	81.3	79.8	78.2	76.8	75.3	73.9	72.5	71.1	69.
49 50	82.9 83.0	81.3 81.4	79.8	78.3 78.4	76.8 76.9	75.4 75.5	74.0 74.0	72.6	71.2 71.3	69.
1 1	83.0	81.5	80.0	78.5					71.4	70.
51 52	83.1	81.5	80.0	78.5	77.0	75.5 75.6	74.1 74.2	72.8	71.4	70.
53	83.2	81.6	80.1	78.6	77.2	75.7	74.2	72.9	71.6	70.
54	83.2	81.7	80.2	78.7	77.2	75.8	74.4	73.0	71.7	70.
55	83.3	81.8	80.3	78.8	77.3	75.9	74.5	73.1	71.8	70.
56	83.4	81.8	80.3	78.9	77.4	76.0	74.6	73.2	71.9	70.
57	83.4	81.9	80.4	78.9	77.5	76.1	74.7	73.3	72.0	70.
58	83.5	82.0	80.5	79.0	77.6	76.2	74.8	73.4	72.1	70.
59	83.6	82.0	80.6	79.1	77.7	76.2	74.9	73.5	72.2	70.
60	83.6	82.1	80.6	79.2	77.7	76.3	75.0	73.6	72.3	71.
61	83.7	82.2	80.7	79.2	77.8	76.4	75.0	73.7	72.4	71.0
62	83.7	82.2	80.8	79.3	77.9	76.5	75.1	73.8	72.4	71.
	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5

Temperature of Air,		t — t' == I	difference of	f Temperat	tures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
62°	83.7	82.2	80.8	79.3	77.9	76.5	75.1	73.8	72.4	71.1
63	83.8	82.3	80.8	79.4	78.0	76.6	75.2	73.9	72.5	71.2
64	83.9	82.4	80.9	79.5	78.1	76.7	75.3	74.0	72.6	71.3
65	83.9	82.4	81.0	79.6	78.1	76.8	75.4	74.0	72.7	71.4
66	84.0	82.5	81.1	79.6	78.2	76.8	75.5	74.1	72.8	71.5
67	84.0	82.6	81.1	79.7	78.3	76.9	75.6	74.2	72.9	71.6
68	84.1	82.6	81.2	79.8	78.4	77.0	75.7	74.3	73.0	71.7
69	84.2	82.7	81.3	79.9	78.5	77.1	75.7	74.4	73.1	71.8
70	84.2	82.8	81.3	79.9	78.5	77.2	75.8	74.5	73.2	71.9
71	84.3	82.8	81.4	80.0	78.6	77.3	75.9	74.6	73.3	72.0
72	84.3	82.9	81.5	80.1	78.7	77.3	76.0	74.7	73.4	72.1
73	84.4	83.0	81.5	80.1	78.7	77.4	76.1	74.8	73.5	72.2
74	84.5	83.0	81.6	80.2	78.8	77.5	76.2	74.9	73.6	72.3
75	84.5	83.1	81.7	80.3	78.9	77.6	76.2	74.9	73.7	72.4
76	84.6	83.1	81.7	80.4	78.9	77.7	76.3	75.0	73.7	72.5
77	84.6	83.2	81.8	80.4	79.0	77.7	76.4	75.1	73.8	72.6
78	84.7	83.3	81.9	80.5	79.1	77.8	76.5	75.2	73.9	72.7
79	84.7	83.3	81.9	80.6	79.1	77.9	76.6	75.3	74.0	72.8
80	84.8	83.4	82.0	80.6	79.2	78.0	76.7	75.4	74.1	72.9
81	84.9	83.5	82.1	80.7	79.3	78.0	76.7	75.5	74.2	73.0
82	84.9	83.5	82.1	80.8	79.4	78.1	76.8	75.5	74.3	73.0
83	85.0	83.6	82.2	80.8	79.4	78.2	76.9	75.6	74.4	73.1
84	85.0	83.6	82.3	80.9	79.5	78.3	77.0	75.7	74.5	73.2
85	85.1	83.7	82.3	81.0	79.6	78.4	77.1	75.8	74.6	73.3
86	85.1	83.7	82.4	81.1	79.7	78.4	77.1	75.9	74.6	73.4
87	85.2	83.8	82.5	81.1	79.8	78.5	77.2	76.0	74.7	73.5
88	85.2	83.9	82.5	81.2	79.9	78.6	77.3	76.1	74.8	73.6
89	85.3	83.9	82.6	81.3	79.9	78.7	77.4	76.1	74.9	73.7
90	85.3	84.0	82.6	81.3	80.0	78.7	77.5	76.2	75.0	73.8
91	85.4	84.0	82.7	81.4	80.1	78.8	77.5	76.3	75.1	73.9
92	85.4	84.1	82.8	81.5	80.2	78.9	77.6	76.4	75.2	74.0
93	85.5		82.8		80.2	79.0	77.7	76.5	75.2	74.0
143303	The same of the sa	84.2	82.9	81.5	80.3	79.0	77.8	76.6	75.3	
94 95	85.6	84.2	83.0	81.6	80.4	79.0	77.9	76.6	75.4	74.1
96	85.6 85.7	84.3 84.3	83.0	81.7 81.7	80.4	79.1	77.9	76.7	75.5	74.2
97	85.7	84.4	83.1	81.8	80.5	79.3	78.0	76.8	75.6	74.4
93	85.8	84.4	83.1	81.9	80.6	79.3	78.1	76.9	75.7	74.5
1			83.2		80.7	79.4	78.2			
99	85.8 85.9	84.5	The same of	81.9 82.0	80.7	79.4	78.3	77.0	75.8	74.6
101	85.9	84.6	83.3 83.3	82.0	80.7	79.6	78.3	77.0	75.8	74.7
101	86.0	84.6 84.7	83.4	82.0	80.9	79.6	78.4	77.2	75.9 76.0	74.8
103	86.0		83.4	82.1	80.9	79.7	78.5	77.3		The state of the s
103	86.1	84.7 84.8	83.4	82.2	81.0	79.7	78.6	77.4	76.1	74.9 75.0
		-					_			
	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = 1$	Difference o	of Tempera	tures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
Fahren- heit.	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.
20°	63.5	62.1	60.6	59.3	58.0	56.6	55.4	54.1	52.9	51.7
21	63.5	62.1	60.7	59.3	58.0	56.6	55.4	54.2	53.0	51.8
22	63.5	62.1	60.7	59.4	58.0	56.7	55.5	54.2	53.0	51.8
23	63.6	62.1	60.7	59.4	58.0	56.7	55.5	54.3	53.0	51.9
24	63.6	62.1	60.7	59.4	58.1	56.8	55.5	54.3	53.1°	51.9
25	63.6	62.1	60.7	59.4	58.1	56.8	55.6	54.4	53.1	52.0
26	63.8	62.3	60.9	59.6	58.3	57.0	55.7	54.5	53.3	52.1
27	64.0	62.5	61.1	59.8	58.5	57.2	55.9	54.6	53.4	52.2
23	64.2	62.7	61.3	60.0	58.6	57.3	56.0	54.8	53.5	52.3
29	64.4	63.0	61.5	60.2	58.8	57.5	56.2	54.9	53.7	52.4
30	64.6	63.2	61.8	60.4	59.0	57.7	56.3	55.1	53.8	52.6
31	64.9	63.5	62.1	60.7	59.3	58.0	56.6	55.4	54.1	52.9
32	65.2	63.8	62.4	61.0	59.6	58.3	57.0	55.7	54.4	53.2
33	65.5	64.1	62.7	61.3	59.9	58.6	57.3	56.0	54.7	53.5
34	65.8	64.4	63.0	61.6	60.2	58.9	57.6	56.3	55.0	53.8
35	66.1	64.7	63.3	61.9	60.5	59.2	57.9	56.6	55.4	54.1
36	66.4	64.9	63.5	62.1	60.8	59.5	58.2	56.9	- 55.6	54.4
37	66.6	65.2	63.8	62.4	61.1	59.8	58.5	57.2	55.9	54.7
38	66.9	65.5	64.1	62.7	61.4	60.1	58.8	57.5	56.2	55.0
39	67.1	65.7	64.4	63.0	61.7	60.3	59.1	57.8	56.5	55.3
40	67.4	66.0	64.6	63.3	62.0	60.6	59.4	58.1	56.8	55.6
41	67.5	66.1	64.8	63.5	62.1	60.9	59.6	58.3	57.1	55.9
42	67.7	66.3	65.0	63.6	62.3	61.1	59.8	58.6	57.3	56.1
43	67.8	66.4	65.1	63.8	62.5	61.3	60.0	58.8	57.6	56.4
44	67.9	66.6	65.3	64.0	62.7	61.5	60.3	59.0	57.8	56.6
45	68.1	66.7	65.4	64.2	62.9	61.7	60.5	59.3	58.1	56.9
46	63.2	66.9	65.6	64.3	63.0	61.8	60.6	59.4	58.2	57.0
47	68.3	67.0	65.7	64.4	63.2	61.9	60.7	59.5	58.3	57.2
48	68.4	67.1	65.8	64.5	63.3	62.0	60.8	59.6	58.5	57.3
49	68.5	67.2	65.9	64.6	63.4	62.1	61.0	59.8	58.6	57.4
50	68.6	67.3	66.0	64.7	63.5	62.2	61.1	59.9	58.7	57.6
51	68.7	67.4	66.1	64.9	63.6	62.4	61.2	60.0	58.9	57.7
52	68.8	67.5	66.2	65.0	63.7	62.5	61.3	60.1	59.0	57.8
53	68.9	67.6	66.4	65.1	63.9	62.6	61.4	60.3	59.1	58.0
54	69.0	67.7	66.5	65.2	64.0	62.7	61.6	60.4	59.2	58.1
55	69.1	67.8	66.6	65.3	64.1	62.9	61.7	60.5	59.4	58.2
56	69.2	67.9	66.7	65.4	64.2	63.0	61.8	60.6	59.5	58.4
57	69.3	68.1	66.8	65.6	64.3	63.1	61.9	60.8	59.6	58.5
58	69.5	68.2	66.9	65.7	64.4	63.2	62.1	60.9	59.8	58.6
59	69.6	68.3	67.0	65.8	64.6	63.4	62.2	61.0	59.9	58 8
60	69.7	68.4	67.1	65.9	64.7	63.5	62.3	61.2	60.0	58.9
61	69.8	68.5	67.2	66.0	64.8	63.6	62.4	61.3	60.1	59.0
62	69.9	68.6	67.4	66.1	64.9	63.7	62.6	61.4	60.3	59.1
1000	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.6

Temper- ature of Air,		€-E=1	Juierence o	i Temperat	ures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
Fahren- heit.	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.
62°	69.9	68.6	67.4	66.1	64.9	63.7	62.6	61.4	60.3	59.1
63	70.0	68.7	67.5	66.2	65.0	63.8	62.7	61.5	60.4	59.3
64	70.1	68.8	67.6	66.3	65.1	64.0	62.8	61.6	60.5	59.4
65	70.2	68.9	67.7	66.5	65.3	64.1	62.9	61.8	60.6	59.5
66	70.3	69.0	67.8	66.6	65.4	64.2	63.0	61.9	60.8	59.
67	70.4	69.1	67.9	66.7	65.5	64.3	63.2	62.0	60.9	59.8
68	70.5	69.2	68.0	66.8	65.6	64.4	63.3	62.1	61.0	59.
69	70.6	69.3	68.1	66.9	65.7	64.5	63.4	62.3	61.1	60.0
70	70.7	69.4	68.2	67.0	65.8	64.7	63.5	62.4	61.3	60.
71	70.8	69.5	68.3	67.1	65.9	64.8	63.6	62.5	61.4	60.
72	70.9	69.6	68.4	67.2	66.0	64.9	63.7	62.6	61.5	60.
73	71.0	69.7	68.5	67.3	66.2	65.0	63.9	62.7	61.6	60.
74	71.1	69.8	68.6	67.4	66.3	65.1	64.0	62.8	61.7	60.
75	71.1	69.9	68.7	67.5	66.4	65.2	64.1	63.0	61.9	60.
76	71.2	70.0	68.8	67.6	66.5	65.3	64.2	63.1	62.0	60.
77	71.3	70.1	68.9	67.8	66.6	65.5	64.3	63.2	62.1	61.
78	71.4	70.2	69.0	67.9	66.7	65.6	64.4	63.3	62.2	61.
79	71.5	70.3	69.1	68.0	66.8	65.7	64.5	63.4	62.3	61.
80	71.6	70.4	69.2	68.1	66.9	65.8	64.7	63.6	62.5	61.
81	71.7	70.5	69.3	68.2	67.0	65.9	64.8	63.7	62.6	61.
82	71.8	70.6	69.4	68.3	67.1	66.0	64.9	63.8	62.7	61.
83	71.9	70.7	69.5	68.4	67.2	66.1	65.0	63.9	62.8	61.
84	72.0	70.8	69.6	68.5	67.3	66.2	65.1	64.0	62.9	61.
85	72.1	70.9	69.7	68.6	67.4	66.3	65.2	64.1	63.0	62.0
86	72.2	71.0	69.8	68.7	67.5	66.4	65.3	64.2	63.2	62.
87	72.3	71.1	69.9	68.8	67.7	66.5	65.4	64.4	63.3	62.
88	72.4	71.2	70.0	68.9	67.8	66.6	65.5	64.5	63.4	62.
89	72.5	71.3	70.1	69.0	67.9	66.8	65.7	64.6	63.5	62.
90	72.6	71.4	70.2	69.1	68.0	66.9	65.8	64.7	63.6	62.
91 92	72.7	71.4	70.3	69.2 69.3	68.1 68.2	67.0 67.1	65.9 66.0	64.8 64.9	63.7 63.9	62.
	1563				4 5					
93	72.9	71.6	70.5	69.4	68.3	67.2	66.1	65.0	64.0	62.9
94	72.9	71.7	70.6	69.5	68.4	67.3	66.2	65.1	64.1	63.6
95	73.0	71.8	70.7	69.6	68.5	67.4	66.3	65.2	64.2	63.2
96	73.1	71.9	70.8	69.7	68.6	67.5	66.4	65.4	64.3	63.3
97 98	73.2 73.3	72.0 72.1	70.9	69.8 69.9	68.7 68.8	67.6 67.7	66.5 66.6	65.5 65.6	64.4 64.5	63.4
99	73.4	72.3	71.1	70.0	68.9	67.8	66.7	65.7	64.6	63.6
100	73.5	72.4	71.2	70.1	69.0	67.9	66.8	65.8	64.8	63.7
101	73.6	72.5	71.3	70.2	69.1	68.0	67.0	65.9	64.9	63.9
102	73.7	72.6	71.4	70.3	69.2	68.1	67.1	66.0	65.0	
103	73.8	72.7	71.5	70.4	69.3	68.2	67.2	66.1	65.1	64.0
103	73.9	72.8	71.6	70.5	69.4	68.3	67.3	66.2	65.2	64.5
	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.

Temper- ature of Air,	all scores	$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Tempera	tures of the	Air and o	f the Dew-	Point.—F	ahrenheit.	
of Air, Fahren- heit.	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5
20°	50.6	49.5	48.4	47.3	46.2	45.1	44.1	43.1	42.1	41.2
21	50.6	49.5	48.4	47.3	46.2	45.1	44.2	43.2	42.2	41.2
22	50.7	49.5	48.4	47.4	46.3	45.2	44.2	43.2	42.2	41.3
23	50.7	49.6	48.5	47.4	46.3	45.2	44.2	43.3	42.3	41.3
24	50.7	49.6	48.5	47.4	46.4	45.3	44.3	43.3	42.3	41.4
25	50.8	49.7	48.5	47.5	46.4	45.4	44.3	43.3	42.4	41.4
26	50.9	49.8	48.6	47.6	46.5	45.4	44.4	43.4	42.4	41.5
27	51.0	49.9	48.7	47.7	46.6	45.5	44.5	43.5	42.5	41.6
28	51.1	50.0	48.8	47.7	46.7	45.6	44.6	43.6	42.6	41.6
29	51.2	50.1	48.9	47.8	46.8	45.7	44.7	43.7	42.7	41.7
30	51.4	50.2	49.0	47.9	46.8	45.8	44.7	43.7	42.7	41.8
31	51.7	50.5	49.4	48.2	47.1	46.1	45.0	44.0	43.0	42.0
32	52.0	50.8	49.7	48.5	47.4	46.4	45.3	44.3	43.3	42.3
33	52.3	51.1	50.0	48.8	47.7	46.6	45.6	44.5	43.5	42.5
34	52.6	51.4	50.3	49.1	48.0	46.9	45.9	44.8	43.8	42.8
35	52.9	51.7	50.6	49.4	48.3	47.2	46.1	45.1	44.1	43.0
36	53.2	52.0	50.9	49.7	48.6	47.5	46.4	45.4	44.4	43.3
37	53.5	52.3	51.2	50.0	48.9	47.8	46.7	45.7	44.7	43.6
38	53.8	52.6	51.5	50.3	49.2	48.1	47.0	46.0	45.0	43.9
39	54.1	52.9	51.8	50.6	49.5	48.4	47.3	46.3	45.3	44.2
40	54.4	53.2	52.1	50.9	49.8	48.7	47.6	46.6	45.6	44.5
41	54.7	53.5	52.3	51.2	50.1	49.0	47.9	46.9	45.8	44.8
42	54.9	53.8	52.6	51.5	50.4	49.3	48.2	47.2	46.1	45.1
43	55.2	54.0	52.9	51.8	50.7	49.6	48.5	47.5	46.4	45.4
44	55.5	54.3	53.2	52.1	50.9	49.9	48.8	47.7	46.7	45.7
45	55.7	54.6	53.4	52.3	51.2	50.2	49.1	48.0	47.0	46.0
46	55.9	54.7	53.6	52.5	51.4	50.4	49.3	48.3	47.2	46.2
47	56.0	54.9	53.8	52.7	51.6	50.6	49.5	48.5	47.5	46.5
48	56.2	55.0	54.0	52.9	51.8	50.8	49.8	48.7	47.7	46.7
49	56.3	55.2	54.1	53.1	52.0	51.0	50.0	49.0	47.9	47.0
50	56.5	55.4	54.3	53.2	52.2	51.2	50.2	49.2	48.2	47.2
51	56.6	55.5	54.4	53.4	52.3	51.3	50.3	49.3	48.3	47.4
52	56.7	55.6	54.6	53.5	52.5	51.5	50.5	49.5	48.5	47.5
53	56.9	55.8	54.7	53.6	52.6	51.6	50.6	49.6	48.6	47.7
54	57.0	55.9	54.8	53.8	52.7	51.7	50.7	49.8	48.8	47.8
55	57.1	56.0	55.0	53.9	52.9	51.9	50.9	49.9	48.9	48.0
56	57.3	56.2	55.1	54.1	53.0	52.0	51.0	50.0	49.1	48.1
57	57.4	56.3	55.2	54.2	53.2	52.2	51.2	50.2	49.2	48.3
58	57.5	56.4	55.4	54.3	53.3	52.3	51.3	50.3	49.4	48.4
59	57.7	56.6	55.5	54.5	53.4	52.4	51.4	50.5	49.5	48.6
60	57.8	56.7	55.6	54.6	53.6	52.6	51.6	50.6	49.7	48.7
61	57.9	56.8	55.8	54.7	53.7	52.7	51.7	50.8	49.8	48.9
62	58.0	57.0	55.9	54.9	53.8	52.8	51.9	50.9	49.9	49.0
BAL.	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5

Cemper-	All The Ar	$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	oifference o	f Temperat	ures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.
62°	58.0	57.0	55.9	54.9	53.8	52.8	51.9	50.9	49.9	49.0
63	58.2	57.1	56.0	55.0	54.0	53.0	52.0	51.0	50.1	49.1
64	58.3	57.2	56.2	55.1	54.1	53.1	52.1	51.2	50.2	49.3
65	58.4	57.4	56.3	55.3	54.3	53.3	52.3	51.3	50.4	49.4
66	58.6	57.5	56.4	55.4	54.4	53.4	52.4	51.5	50.5	49.6
67	58.7	57.6	56.6	55.5	54.5	53.5	52.6	51.6	50.6	49.7
68	58.8	57.8	56.7	55.7	54.7	53.7	52.7	51.7	50.8	49.9
69	59.0	57.9	56.8	55.8	54.8	53.8	52.8	51.9	50.9	50.0
70	59.1	58.0	57.0	55.9	54.9	53.9	53.0	52.0	51.1	50.1
71	59.2	58.2	57.1	56.1	55.1	54.1	53.1	52.1	51.2	50.3
72	59.3	58.3	57.2	56.2	55.2	54.2	53.2	52.3	51.3	50.4
73	59.5	58.4	57.4	56.3	55.3	54.3	53.4	52.4	51.5	50.6
74	59.6	58.5	57.5	56.5	55.5	54.5	53.5	52.6	51.6	50.7
75	59.7	58.7	57.6	56.6	55.6	54.6	53.6	52.7	51.7	50.8
76	59.8	58.8	57.8	56.7	55.7	54.7	53.8	52.8	51.9	51.0
77	60.0	58.9	57.9	56.9	55.9	54.9	53.9	53.0	52.0	51.1
78	60.1	59.1	58.0	57.0	56.0	55.0	54.0	53.1	52.2	51.2
79	60.2	59.2	58.1	57.1	56.1	55.1	54.2	53.2	52.3	51.4
80	60.3	59.3	58.3	57.3	56.3	55.3	54.3	53.4	52.4	51.5
81	60.5	59.4	58.4	57.4	56.4	55.4	54.5	53.5	52.6	51.7
82	60.6	59.6	58.5	57.5	56.5	55.5	54.6	53.6	52.7	51.8
83	60.7	59.7	58.6	57.6	56.6	55.7	54.7	53.8	52.8	51.9
84	60.8	59.8	58.8	57.8	56.8	55.8	54.8	53.9	53.0	52.1
85	60.9	59.9	58.9	57.9	56.9	55.9	55.0	54.0	53.1	52.2
86	61.1	60.0	59.0	58.0	57.0	56.1	55.1	54.2	53.2	52.3
87	61.2	60.2	59.1	58.1	57.2	56.2	55.2	54.3	53.4	52.5
88	61.3	60.3	59.3	58.3	57.3	56.3	55.4	54.4	53.5	52.6
89	61.4	60.4	59.4	58.4	57.4	56.5	55.5	54.6	53.7	52.7
90	61.6	60.5	59.5	58.5	57.6	56.6	55.6	54.7	53.8	52.9
91	61.7	60.7	59.6	58.7	57.7	56.7	55.8	54.8	53.9	53.0
92	61.8	60.8	59.8	58.8	57.8	56.9	55.9	55.0	54.1	53.2
93	61.9	60.9	59.9	58.9	57.9	57.0	56.0	55.1	54.2	53.3
94	62.0	61.0	60.0	59.0	58.1	57.1	56.2	55.2	54.3	53.4
95	62.1	61.1	60.1	59.2	58.2	57.2	56.3	55.4	54.5	53.6
96	62.3	61.3	60.3	59.3	58.3	57.4	56.4	55.5	54.6	53.7
97	62.4	61.4	60.4	59.4	58.4	57.5	56.5	55.6	54.7	53.8
98	62.5	61.5	60.5	59.5	58.6	57.6	56.7	55.8	54.9	54.0
99°	62.6	61.6	60.6	59.6	58.7	57.7	56.8	55.9	55.0	54.1
100	62.7	61.7	60.7	59.8	58.8	57.9	56.9	56.0	55.1	54.2
101	62.8	61.9	60.9	59.9	58.9	58.0	57.1	56.2	55.3	54.4
102	63.0	62.0	61.0	60.0	59.1	58.1	57.2	56.3	55.4	54.5
103	63.1	62.1	61.1	60.1	59.2	58.3	57.3	56.4	55.5	54.6
104	63.2	62.2	61.2	60.3	59.3	58.4	57.5	56.6	55.7	54.8
18.8	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5

Fahren- heit.	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.6
20°	40.2	39.3	38.4	37.5	36.6	35.8	34.9	34.1	33.3	32.5
21	40.3	39.4	38.4	37.6	36.7	35.8	35.0	34.2	33.4	32.6
22	40.3	39.4	38.5	37.6	36.8	35.9	35.1	34.3	33.5	32.7
23	40.4	39.5	38.6	37.7	36.8	36.0	35.2	34.4	33.6	32.8
24	40.4	39.6	38.6	37.8	36.9	36.1	35.2	34.4	33.6	32.9
25	40.5	39.6	38.7	37.8	37.0	36.2	35.3	34.5	33.7	33.0
26	40.5	39.7	38.8	37.9	37.0	36.2	35.4	34.6	33.8	33.1
27	40.6	39.7	38.8	38.0	37.1	36.3	35.5	34.7	33.9	33.1
28	40.7	39.8	38.9	38.0	37.2	36.3	35.5	34.7	34.0	33.2
29	40.8	39.9	38.9	38.1	37.2	36.4	35.6	34.8	34.0	33.3
30	40.8	39.9	39.0	38.1	37.3	36.5	35.7	34.9	34.1	33.4
31	41.1	40.2	39.2	38.4	37.5	36.7	35.9	35.1	34.3	33.6
32	41.3	40.4	39.5	38.6	37.7	37.0	36.1	35.3	34.5	33.8
33	41.6	40.6	39.7	38.8	38.0	37.2	36.3	35.5	34.7	34.0
34	41.8	40.9	39.9	39.1	38.2	37.4	36.5	35.7	34.9	34.2
35	42.1	41.1	40.2	39.3	38.4	37.7	36.7	35.9	35.1	34.4
36	42.3	41.4	40.4	39.6	38.7	37.9	37.0	36.2	35.4	34.6
37	42.6	41.7	40.7	39.8	38.9	38.2	37.2	36.4	35.6	34.8
38	42.8	42.0	41.0	40.1	39.2	38.4	37.5	36.6	35.8	35.0
39	43.1	42.3	41.3	40.4	39.5	38.6	37.7	36.9	36.0	35.2
40	43.3	42.6	41.6	40.7	39.8	38.9	38.0	37.1	36.3	35.4
41	43.7	42.9	41.9	41.0	40.0	39.1	38.3	37.4	36.5	35.7
42	44.0	43.2	42.2	41.2	40.3	39.4	38.5	37.7	36.8	36.0
43	44.3	43.4	42.5	41.5	40.6	39.7	38.8	38.0	37.1	36.3
44	44.7	43.7	42.8	41.8	40.9	40.0	39.1	38.2	37.4	36.6
45	45.0	44.0	43.1	42.1	41.2	40.3	39.4	38.5	37.7	36.8
46	45.2	44.3	43.3	42.4	41.4	40.5	39.7	38.8	37.9	37.1
47	45.5	44.5	43.6	42.6	41.7	40.8	39.9	39.1	38.2	37.4
48	45.7	44.8	43.8	42.9	42.0	41.1	40.2	39.3	38.5	37.6
49	46.0	45.0	44.1	43.2	42.2	41.3	40.5	39.6	38.7	37.9
50	46.2	45.3	44.3	43.4	42.5	41.6	40.7	39.9	39.0	37.2
51	46.4	45.4	44.5	43.6	42.7	41.8	40.9	40.1	39.2	38.4
52	46.6	45.5	44.7	43.8	42.9	42.0	41.2	40.3	39.5	38.6
53	46.7	45.8	44.9	44.0	43.1	42.2	41.4	40.5	39.7	38.9
54	46.9	46.0	45.1	44.2	43.3	42.4	41.6	40.8	39.9	39.1
55	47.0	46.1	45.2	44.4	43.5	42.6	41.8	41.0	40.1	39.3
56	47.2	46.3	45.4	44.5	43.6	42.8	42.0	41.1	40.3	39.5
57	47.3	46.4	45.5	44.7	43.8	42.9	42.1	41.3	40.5	39.6
58	47.5	46.6	45.7	44.8	43.9	43.1	42.3	41.4	40.6	39.8
59	47.6	46.7	45.8	45.0	44.1	43.2	42.4	41.6	40.8	40.0
60	47.8	46.9	46.0	45.1	44.2	43.4	42.5	41.7	40.9	40.1
61	47.9	47.0	46.1	45.3	44.4	43.5	42.7	41.9	41.1	40.3
62	48.1	47.2	46.3	45.4	44.5	43.7	42.8	42.0	41.2	40.4

Temper- ature		$\mathbf{t}-\mathbf{t}'=$ Difference of Temperatures of the Air and of the Dew-Point. — Fahrenheit.											
of Air, Fahren- heit.	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.			
62°	48.1	47.2	46.3	45.4	44.5	43.7	42.8	42.0	41.2	40.4			
63	48.2	47.3	46.4	45.5	44.7	43.8	43.0	42.2	41.4	40.6			
64	48.4	47.5	46.6	45.7	44.8	44.0	43.1	42.3	41.5	40.7			
65	48.6	47.6	46.7	45.8	45.0	44.1	43.3	42.5	41.7	40.9			
66	48.7	47.8	46.9	46.0	45.1	44.3	43.4	42.6	41.8	41.0			
67	48.8	47.9	47.0	46.1	45.3	44.4	43.6	42.8	42.0	41.2			
68	48.9	48.0	47.2	46.3	45.4	44.6	43.7	42.9	42.1	41.3			
69	49.1	48.2	47.3	46.4	45.6	44.7	43.9	43.1	42.3	41.5			
70	49.2	48.3	47.4	46.6	45.7	44.9	44.0	43.2	42.4	41.6			
71	49.4	48.5	47.6	46.7	45.9	45.0	44.2	43.4	42.6	41.8			
72	49.5	48.6	47.7	46.9	46.0	45.2	44.3	43.5	42.7	41.9			
73	49.6	48.8	47.9	47.0	46.1	45.3	44.5	43.7	42.9	42.1			
74	49.8	48.9	48.0	47.1	46.3	45.4	44.6	43.8	43.0	42.2			
75	49.9	49.0	48.2	47.3	46.4	45.6	44.8	44.0	43.1	42.4			
76	50.1	49.2	48.3	47.4	46.6	45.7	44.9	44.1	43.3	42.5			
77	50.2	49.3	48.5	47.6	46.7	45.9	45.1	44.2	43.4	42.6			
78	50.3	49.5	48.6	47.7	46.9	46.0	45.2	44.4	43.6	42.8			
79	50.5	49.6	48.7	47.8	47.0	46.2	45.3	44.5	43.7	43.0			
80	50.6	49.7	48.9	48.0	47.2	46.3	45.5	44.7	43.9	43.1			
81	50.8	49.9	49.0	48.1	47.3	46.5	45.6	44.8	44.0	43.2			
82	50.9	50.0	49.2	48.3	47.4	46.6	45.8	45.0	44.2	43.4			
83	51.0	50.1	49.3	48.4	47.6	46.8	45.9	45.1	44.3	43.8			
84	51.2	50.3	49.4	48.6	47.7	46.9	46.1	45.3	44.5	43.7			
85	51.3	50.4	49.6	48.7	47.9	47.0	46.2	45.4	44.6	43.8			
86	51.4	50.6	49.7	48.8	48.0	47.2	46.4	45.6	44.8	44.0			
87	51.6	50.7	49.8	49.0	48.1	47.3	46.5	45.7	44.9	44.1			
88	51.7	50.8	50.0	49.1	48.3	47.5	46.6	45.8	45.0	44.3			
89	51.9	51.0	50.1	49.3	48.4	47.6	46.8	46.0	45.2	44.			
90	52.0	51.1	50.3	49.4	48.6	47.7	46.9	46.1	45.3	44.0			
91	52.1	51.3	50.4	49.5	48.7	47.9	47.1	46.3	45.5	44.			
92	52.3	51.4	50.5	49.7	48.8	48.0	47.2	46.4	45.6	44.8			
93	52.4	51.5	50.7	49.8	49.0	48.2	47.4	46.6	45.8	45.0			
94	52.5	51.7	50.8	50.0	49.1	48.3	47.5	46.7	45.9	45.			
95	52.7	51.8	50.9	50.1	49.3	48.4	47.6	46.8	46.1	45.3			
96	52.8	51.9	51.1	50.2	49.4	48.6	47.8	47.0	46.2	45.4			
97 98	52.9 53.1	52.1 52.2	51.2 51.4	50.4 50.5	49.5	48.7	47.9 48.1	47.1 47.3	46.3	45.0			
4				11.19.192		Course on the	to have been	I due to the	Si mon				
99	53.2 53.4	52.3 52.5	51.5 51.6	50.6 50.8	49.8 50.0	49.0	48.2	47.4	46.6	45.9			
101	53.5	52.6	51.8	50.9	50.1	49.3	48.5	47.7	46.9	46.2			
102	53.6	52.8	51.9	51.1	50.2	49.4	48.6	47.8	47.1	46.8			
103	53.8	52.9	52.0	51.2	50.4	49.6	48.8	48.0	47.2	46.4			
104	53.9	53.0	52.2	51.3	50.5	49.7	48.9	48.1	47.3	46.6			
12.3	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.			

#### TABLE IX.

FACTOR 100 FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE OF THE AIR, EXPRESSED IN HUNDREDTHS, FROM ITS ABSOLUTE HUMIDITY GIVEN IN ENGLISH MEASURES.

THE Relative Humidity, or the degree of moisture of the air, is, as explained above, the ratio of the quantity of vapor contained in the air to the quantity it could contain at the temperature observed, if fully saturated.

If we call

The force of vapor contained in the air = f,

The maximum of the force of vapor at the temperature of the air = F,

The point of saturation = 100,

we have the proportion,

Relative Humidity: 100::f:F,

and

 $f_{F}^{\times 100}$  = Relative Humidity in Hundredths.

But as  $\frac{f \times 100}{F} = f \times \frac{100}{F}$ , it is obvious that the operation indicated by the former expression, viz.  $\frac{f \times 100}{F}$ , would be reduced to a simple multiplication, if we had a table of the factors  $\frac{100}{F}$ . Such a table is obtained by dividing the constant number 100 by each number in the Table of Elastic Forces of Vapor, and substituting the quotients for the tensions, or forces of vapor.

The following Table gives the factor  $\frac{100}{F}$  for every tenth of a degree from 0° to 104° Fahrenheit, corresponding to the Forces of Vapor in Table VI., or Regnault's table reduced to English measures.

#### USE OF THE TABLE.

The force of vapor contained in the air, or its absolute humidity, being given in English measures, multiply the number expressing it by the factor in the table corresponding to the temperature of the air at the time of the observation; the result will be the Relative Humidity in Hundredths.

### Examples.

Suppose the temperature of the air to be = 60° Fahrenheit.
 " force of vapor in the air to be = .388 English inch.

Opposite 60° is found in the table the factor 193.1.

Then  $0.388 \times 193.1 = 74.9$ , Relative Humidity in Hundredths.

Suppose the temperature of the air to be = 74°.5 Fahrenheit.
 " force of vapor in the air to be = .650 English inch.
 Table gives for 74°.5 the factor 117.2.

Then  $0.650 \times 117.2 = 76.2$ , Relative Humidity required.

# IX. FACTOR $\frac{100}{F}$ , FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE OF THE AIR,

## EXPRESSED IN HUNDREDTHS, FROM ITS ABSOLUTE HUMIDITY GIVEN IN ENGLISH INCHES.

Temper-					Tenths of Degrees.							
of Air, Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
0°	2306	2295	2285	2275	2264	2254	2243	2233	2222	2211		
1	2201	2191	2181	2171	2162	2152	2142	2132	2122	2111		
2	2101	2092	2083	2074	2064	2055	2045	2036	2026	2017		
3	2007	1998	1990	1981	1972	1963	1954	1945	1936	1927		
4	1918	1910	1901	1893	1885	1876	1868	1859	1851	1842		
5	1834	1826	1818	1810	1802	1794	1786	1777	1769	1761		
6	1753	1745	1738	1730	1722	1714	1707	1699	1691	1683		
7	1675	1668	1660	1653	1646	1638	1631	1623	1616	1608		
8	1600	1594	1587	1580	1572	1565	1558	1551	1544	1537		
9	1529	1523	1516	1509	1503	1496	1489	1482	1475	1469		
10	1462	1455	1449	1443	1436	1430	1423	1417	1410	1404		
11	1397	1391	1385	1379	1373	1367	1361	1355	1348	1342		
12	1336	1330	1324	1319	1313	1307	1301	1295	1289	1284		
13	1278	1272	1267	1261	1255	1250	1244	1239	1233	1228		
14	1222	1217	1211	1206	1200	1195	1189	1184	1178	1173		
15	1167	1162	1157	1151	1146	1141	1136	1130	1125 -	1120		
16	1114	1109	1104	1099	1094	1089	1084	1079	1074	1069		
17	1064	1059	1055	1050	1045	1040	1035	1031	1026	1021		
18	1016	1012	1007	1003	998.2	993.6	989.1	984.5	979.9	975		
19	970.6	966.4	962.2	957.9	953.7	949.4	945.0	940.7	936.3	931		
20	927.5	923.5	919.5	915.5	911.4	907.4	903.3	899.1	895.0	890		
21	886.7	882.9	879.1	875.3	871.4	867.6	863.7	859.8	855.8	851		
22	847.9	844.3	840.7	837.1	833.4	829.8	826.1	822.4	818.7	815		
23	811.2	807.8	804.3	800.8	797.3	793.8	790.2	786.7	783.1	779		
24	775.9	772.6	769.3	766.0	762.7	759.3	756.0	752.6	749.2	745		
25	742.4	739.3	736.2	733.0	729.9	726.7	723.5	720.3	717.1	713		
26	710.6	707.7	704.7	701.8	698.8	695.8	692.8	689.7	686.7	683		
27	680.5	677.8	675.0	672.1	669.3	666.5	663.6	660.7	657.8	654		
28	652.0	649.4	646.7	644.1	641.4	638.7	636.0	633.3	630.5	627.		
29	625.0	622.5	620.0	617.5	614.9	612.4	609.8	607.2	604.6	602.		
30	599.4 575.1	597.1	594.7 570.7	592.3 568.4	589.9 566.2	587.4 563.9	585.0 561.6	582.6 559.2	580.1 556.9	577		
						000.5				1004		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

Temper- ature of Air,	Tenths of Degrees.											
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
32°	552.2	550.0	547.8	545.7	543.6	541.4	539.3	537.2	535.1	533.		
33	530.9	528.8	526.8	524.7	522.7	520.6	518.6	516.5	514.5	512.		
34	510.5	508.5	506.5	504.5	502.5	500.5	498.6	496.6	494.7	492.		
35	490.8	488.9	487.0	485.1	483.2	481.3	479.4	477.5	475.6	473.		
36	471.9	470.1	468.2	466.4	464.6	462.8	461.0	459.2	457.4	455.		
37	453.8	452.0	450.3	448.5	446.8	445.0	443.3	441.6	439.9	438.		
38	436.4	434.7	433.1	431.4	429.7	428.0	426.4	424.7	423.1	421.		
39	419.8	418.2	416.6	415.0	413.4	411.8	410.2	408.6	407.0	405.		
40	403.9	402.4	400.8	399.3	397.8	396.2	394.7	393.2	391.7	290.		
41	388.7	387.2	385.8	384.3	382.9	381.4	380.0	378.5	377.1	375.		
42	374.3	372.9	371.5	370.0	368.6	367.3	365.9	364.5	363.1	361.		
43	360.4	359.0	357.6	356.3	354.9	353.6	352.3	350.9	349.6	348.		
44	347.0	345.6	344.3	343.0	341.7	340.4	339.2	337.9	336.6	335.		
45	334.1	332.8	331.6	330.3	328.1	327.8	326.6	325.4	324.1	322.		
46	321.7	320.5	319.3	318.1	316.9	315.7	314.5	313.3	312.2	311.		
	309.8	308.7	307.5	306.4	305.2	904.1	202.0	001.0	200 =	200		
47	298.5	297.3	296.2	295.1	294.0	304.1	302.9	301.8	300.7	299.		
49	287.6	286.5	285.4	284.4	283.3	292.9 282.3	291.9	290.8 280.2	289.7	288. 278.		
50	277.1	276.1	275.1	274.1	273.1	272.1	271.1	270.1	269.1	268.		
51	267.2	266.2	265.2	264.3	263.3	262.3	261.4	260.4	259.5	258.		
			20012	20110	200.0	20210	20111	20014	200.0	250.		
52	257.6	256.6	255.7	254.8	253.8	252.9	252.0	251.1	250.2	249.		
53	248.3	247.4	246.5	245.6	244.7	243.9	243.0	242.1	241.2	240.		
54	239.5	238.6	237.7	236.9	236.0	235.1	234.3	233.4	232.6	231.		
55	230.9	230.1	229.2	228.4	227.6	226.8	225.9	225.1	224.3	223.		
56	222.7	221.9	221.1	220.3	219.5	218.7	217.9	217.1	216.4	215.		
57	214.8	214.0	213.3	212.5	211.8	211.0	210.2	209.5	208.7	208.		
58	207.3	206.5	205.8	205.0	204.3	203.6	202.9	209.5	201.4	208.		
59	200.0	199.3	198.6	197.9	197.2	196.5	195.8	195.1	194.4	193.		
60	193.1	192.4	191.7	191.0	190.4	189.7	189.0	188.4	187.7	187.		
61	.186.4	185.7	185.1	184.4	183.8	183.1	182.5	181.8	181.2	180.		
62	179.9	179.3	178.7	178.0	177.4	176.8	176.2	175.6	174.9	174.		
63	173.7	173.1	172.5	171.9	171.3	170.7	170.1	169.5	168.9	168.		
64	167.7	167.1	166.6	166.0	165.4	164.8	164.3	163.7	163.1	162.		
65	162.0	161.4	160.9	160.3	159.7	159.2	158.6	158.1	157.5	157.		
66	156.5	155.9	155.4	154.8	154.3	153.8	153.2	152.7	152.2	151.		
67	151.1	150.6	150.1	149.6	149.1	148.6	148.1	147.6	147.1	146.6		
22	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

Temper-		Tenths of Degrees.											
of Air, Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.			
68°	146.0	145.6	145.1	144.6	144.1	143.6	143.1	142.6	142.1	141.6			
69	141.2	140.7	140.2	139.7	139.2	138.8	138.3	137.8	137.4	136.9			
70	136.4	136.0	135.5	135.1	134.6	134.1	133.7	133.2	132.8	132.9			
71	131.9	131.4	131.0	130.5	130.1	129.7	129.2	128.8	128.3	127.9			
72	127.5	127.1	126.6	126.2	125.8	125.3	124.9	124.5	124.1	123.7			
73	123.3	122.8	122.4	122.0	121.6	121.2	120.8	120.4	120.0	119.6			
74	119.2	118.8	118.4	118.0	117.6	117.2	116.8	116.4	116.0	115.6			
75	115.3	114.9	114.5	114.1	113.7	113.3	113.0	112.6	112.2	111.9			
76	111.5	111.1	110.7	110.4	110.0	109.6	109.3	108.9	108.6	108.2			
77	107.9	107.5	107.1	106.8	106.4	106.1	105.7	105.4	105.1	104.7			
78	104.4	104.0	103.7	103.3	103.0	102.7	102.3	102.0	101.7	101.8			
79	101.0	100.7	100.3	100.0	99.68	99.35	99.02	98.70	98.38	98.0			
80	97.73	97.42	97.10	96.78	96.47	96.15	95.84	95.52	95.21	94.9			
81	94.59	94.29	93.98	93.67	93.37	93.06	92.76	92.46	92.16	91.8			
82	91.56	91.26	90.97	90.67	90.38	90.09	89.80	89.51	89.22	88.9			
83	88.64	88.36	88.07	87.79	87.50	87.22	86.94	86.66	86.38	86.1			
84	85.83	85.55	85.27	85.00	84.73	84.46	84.19	83.92	83.65	83.3			
85	83.12	82.85	82.59	82.32	82.06	81.80	81.54	81.28	81.02	80.7			
86	80.51	80.25	80.00	79.74	79.49	79.24	78.99	78.74	78.49	78.2			
87	77.99	77.75	77.50	77.26	77.01	76.77	76.52	76.28	76.04	75.8			
								wo 0.7					
88	75.56	75.32	75.08	74.85	74.61	74.37	74.14	73.91	73.67	73.4			
89	73.21	72.98	72.75	72.52	72.29	72.06	71.84	71.61	71.39	71.1			
90	70.94	70.72	70.49	70.27	70.05	69.83	69.61	69.39	69.18	68.9			
91	68.74	68.53	68.32	68.10	67.89	67.68	67.47	67.26	67.05	66.8			
92	66.63	66.42	66.22	66.01	65.81	65.60	65.40	65.19	64.99	64.7			
93	64.59	64.39	64.19	63.99	63.79	63.59	63.40	63.20	63.01	62.8			
94	62.62	62.43	62.24	62.04	61.85	61.66	61.47	61.29	61.10	60.9			
95	60.72	60.54	60.35 58.53	60.17	59.98	59.80	59.62	59.43	59.25	59.0			
96 97	58.89 57.12	58.71 56.94	56.77	58.35 56.60	58.17 56.42	58.00 56.25	57.82	57.64 55.91	57.47	57.2 55.5			
98	55.40	55.23	55.06	54.90	54.73	54.56	54.40	54.23	54.07	53.9			
00	53.74	53.58	53.42	53.26	53:09	52.93	52.77	52.61	52.45	E0.0			
99 100	52.14	51.98	51.82	51.67	51.51	51.36	51.20	51.05	50.90	52.3 50.7			
101	50.59	50.44	50.29	50.14	49.99	49.84	49.69	49.54	49.39	49.2			
102	49.10	48.95	48.80	48.66	48.51	48.37	48.22	48.08	47.94	49.2			
103	47.65	47.51	47.37	47.23	47.09	46.95	46.81	46.67	46.53	46.4			
104	46.26	46.12	45.99	45.85	45.72	45.58	45.45	45.31	45.18	45.0			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

#### TABLE X.

### WEIGHT OF VAPOR, IN GRAINS TROY,

CONTAINED IN A CUBIC FOOT OF SATURATED AIR, UNDER A BAROMETRIC PRESSURE OF 30 ENGLISH INCHES, AT TEMPERATURES BETWEEN 0° AND 105° FAHRENHEIT.

The weight of a litre of dry air at the temperature of zero Centigrade, or 32° Fahrenheit, and under a barometric pressure of 760 millimetres, as determined by the experiments of Regnault (Mémoires de l'Institut, Tom. XXI. p. 157), and corrected for a slight error of computation (see above, p. 38), is 1.293223 grammes. The coefficient of expansion of the air, according to the same physicist, is 0.00367 for 1° Centigrade; and the theoretic density of vapor is nearly 0.622, or \(\frac{1}{8}\), of that of the air at the same temperature and pressure. From these elements the weight of the vapor contained in a determined volume of air, the temperature and humidity of which are known, can be deduced.

Reducing these values to English measures, 1 litre being = 61.02705 cubic inches, and 1 gramme = 15.43208 grains Troy, we have

1.293223 grammes = 19.9571208 grains,

and

61.027051 cubic inches: 19.9571208 grains:: 1 cubic inch: 0.32702 grain.

Therefore, the weight of a cubic foot of dry air, at 32° Fahrenheit, under a pressure of 760 millimetres, or 29.922 English inches, is = 0.32702 grain  $\times$  1728 = 565.0923 grains Troy. Under a barometric pressure of 30 inches, it becomes

$$\frac{30}{29.922} \times 565.0923 = 566.5654$$
 grains.

The coefficient for the expansion of the air becomes 0.0020361 of its bulk for 1° Fahrenheit.

Now, if we call

t =the temperature of the air;

W = the weight of vapor in a saturated air at the temperature t;

F = the maximum of the force of vapor due to the temperature t, as given in the tables;

then the weight of the vapor contained in a cubic foot of saturated air is given by the formula

$$W = 0.622 \; \frac{566.5654 \; \text{grains}}{1 + 0.002036 \times (t - 32^{\circ})} \; \cdot \; \frac{\text{F}}{30};$$

from which the values in Table X. have been computed. The forces of vapor due to the temperatures in the first column are those of Regnault, as given in Table VI.

It is evident, that, in order to find the weight of the vapor contained in the air at any state of humidity and pressure, it suffices to substitute for the normal values of  $\frac{\mathbf{F}}{30}$  the force of vapor and the barometric pressure given by the observation.

## X. WEIGHT OF VAPOR, IN GRAINS TROY,

## CONTAINED IN A CUBIC FOOT OF SATURATED AIR, AT TEMPERATURES BETWEEN 0° AND 105° FAHRENHEIT.

Temper-	Force	Weight		Temper-	Force	Weight		Temper-	Force	Weight	
ature	of Vapor	of Vapor	Differ- ence.	ature	of Vapor	of Vapor	Differ- ence.	ature	of Vapor	of Vapor	Differ- ence.
Air,	in Eng.	in	CHOC.	Air,	in Eng.	in	OHOU.	Air,	in Eng.	in	ОПОО
Fahren.	Inches.	Grains.		Fahren.	Inches.	Grains.		Fahren.	Inches.	Grains.	
0°	0.043	0.545	0.024	35°	0.204	2.379	0.090	70°	0.733	7.992	0.26
1	0.045	0.569	0.024	36	0.212	2.469	0.093	71	0.758	8.252	0.26
2	0.048	0.595	0.023	37	0.220	2.563	0.097	72	0.784	8.521	0.20
3	0.050	0.621	0.021	38	0.229	2.659	0.100	73	0.811	8.797	0.28
4	0.052	0.649	0.028	39	0.238	2.759	0.103	74	0.839	9.081	0.29
5	0.055	0.678	0.000	40	0.248	2.862	0.100	75	0.868	9.372	0.00
6	0.057	0.708	0.030	41	0.257	2.967	0.106	76	0.897	9.670	0.29
7	0.060	0.739	0.031	42	0.267	3.076	0.109	77	0.927	9.977	0.30
8	0.062	0.772	0.033	43	0.277	3.189	0.113	78	0.958	10.292	0.31
9	0.065	0.806	0.034	44	0.288	3.306	0.116	79	0.990	10.616	0.32
10	0.068	0.841	0.037	45	0.299	3.426	0.124	80	1.023	10.949	0.34
11	0.072	0.878	0.037	46	0.311	3.550	0.124	81	1.057	11.291	0.35
12	0.075	0.916	0.038	47	0.323	3.679	0.129	82	1.092	11.643	0.36
13	0.078	0.957	0.040	48	0.335	3.811	0.137	83	1.128	12.005	0.37
14	0.082	0.999	0.042	49	0.348	3.948	0.131	84	1.165	12.376	0.38
15	0.086	1.043	0.046	50	0.361	4.089	0.145	85	1.203	12.756	0.39
16	0.090	1.090	0.049	51	0.374	4.234	0.149	86	1.242	13.146	0.40
17	0.094	1.138	0.049	52	0.388	4.383	0.149	87	1.282	13.546	0.41
18	0.098	1.190	0.053	53	0.403	4.537	0.159	88	1.323	13.957	0.42
19	0.103	1.243	0.055	54	0.418	4.696	0.163	89	1.366	14.378	0.43
20	0.108	1.298	0.057	55	0.433	4.860	0.168	90	1.410	14.810	0.44
21	0.113	1.355	0.059	56	0.449	5.028	0.174	91	1.455	15.254	0.45
22	0.118	1.415	0.062	57	0.466	5.202	0.179	92	1.501	15.709	0.46
23	0.123	1.476	0.064	58	0.482	5.381	0.185	93	1.548	16.176	0.47
24	0.129	1.540	0.066	59	0.500	5.566	0.190	94	1.597	16.654	0.49
25	0.135	1.606	0.068	60	0.518	5.756	0.196	95	1.647	17.145	0.50
26	0.141	1.674	0.070	61	0.537	5.952	0.202	96	1.698	17.648	0.51
27	0.147	1.745	0.073	62	0.556	6.154	0.208	97	1.751	18.164	0.52
28	0.153	1.817	0.075	63	0.576	6.361	0.214	98	1.805	18.693	0.54
29	0.160	1.892	0.077	64	0.596	6.575	0.220	99	1.861	19.235	0.55
30	0.167	1.969	0.077	65	0.617	6.795	0.226	100	1.918	19.790	0.56
31	0.174	2.046	0.080	66	0.639	7.021	0.232	101	1.977	20.357	0.58
32	0.181	2.126	0.082	67	0.662	7.253	0.239	102	2.037	20.938	0.59
33	0.188	2.208	0.084	68	0.685	7.493	0.246	103	2.099	21.535	0.61
34	0.196	2.292	0.087	69	0.708	7.739	0.253	104	2.162	22.146	0.62
35	0.204	2.379	1 9	70	0.733	7.992		105	2.227	22.771	0.02

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The state of												
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## PRACTICAL TABLES,

IN

## ENGLISH MEASURES,

BASED ON THE HYGROMETRICAL CONSTANTS ADOPTED IN THE . GREENWICH OBSERVATIONS.

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### TABLE

OF

#### THE ELASTIC FORCES OF AQUEOUS VAPOR,

UNDER A PRESSURE OF 30 INCHES, EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT, ADOPTED IN THE GREENWICH OBSERVATIONS.

This table contains the values of the elastic force of vapor for temperatures from 0° to 90° Fahrenheit, derived from Dalton's experiments by Biot's formula, by Anderson, and published in Edinburgh Encyclopædia, Art. Hygrometry. It is republished, without the last decimal, in the volumes of the Greenwich Magnetic and Meteorological Observations, and on it are based the various hygrometrical tables published by Mr. Glaisher, either in the Greenwich volumes, or separately, most of which will be found below, Tables XII. to XVII.

Since Dalton published his experiments, numerous attempts have been made by various skilful physicists to determine with greater accuracy the elastic force of vapor. Dr. Ure in England, Regnault in France, and Magnus in Germany, deserve in this respect a special notice.

The last two experimenters having arrived simultaneously at results nearly identical, and their experiments having been conducted with all the care that modern science requires, and the means that it can secure, their determinations seem to command an especial confidence, and to deserve the preference over all others. It is, therefore, much to be regretted that the usefulness of the following otherwise so valuable tables, the formation of which involved so much labor, is in a measure impaired by the fact that they were computed from elements which cannot be regarded as the most reliable we now possess.

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# TABLE

OF THE

# ELASTIC FORCE OF AQUEOUS VAPOR,

UNDER A BAROMETRIC PRESSURE OF 30 INCHES, EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT.

#### From the Greenwich Observations.

Temper-			7.08/0	Ste no	Tenths of	Degrees.	FARAF	ench!	(20,15	e isani
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
°	Eng. In. 0.061	Eng. In. 0.061	Eng. In. 0.062	Eng. In. 0.062	Eng. In. 0.062	Eng. In. 0.062	Eng. In. 0.063	Eng. In. 0.063	Eng. In. 0.063	Eng. In 0.063
1	0.064	0.064	0.064	0.064	0.065	0.065	0.065	0.065	0.066	0.066
2	0.066	0.066	0.067	0.067	0.067	0.067	0.068	0.068	0.068	0.068
3	0.069	0.069	0.069	0.069	0.070	0.070	0.070	0.071	0.071	0.071
4	0.071	0.072	0.072	0.072	0.072	0.073	0.073	0.073	0.073	0.074
5	0.074	0.074	0.075	0.075	0.075	0.075	0.076	0.076	0.076	0.077
6	0.077	0.077	0.077	0.078	0.078	0.078	0.079	0.079	0.079	0.080
7	0.080	0.080	0.080	0.081	0.081	0.081	0.082	0.082	0.082	0.083
8	0.083	0.083	0.083	0.084	0.084	0.084	0.085	0.085	0.085	0.086
9	0.086	0.086	0.087	0.087	0.087	0.088	0.088	0.088	0.089	0.089
10	0.089	0.090	0.090	0.090	0.091	0.091	0.091	0.092	0.092	0.092
11	0.093	0.093	0.093	0.094	0.094	0.094	0.095	0.095	0.096	0.096
12	0.096	0.097	0.097	0.097	0.098	0.098	0.098	0.099	0.099	0.099
13	0.100	0.100	0.101	0.101	0.101	0.102	0.102	0.102	0.103	0.103
14	0.104	0.104	0.104	0.105	0.105	0.106	0.106	0.106	0.107	0.107
15	0.108	0.108	0.108	0.109	0.109	0.110	0.110	0.110	0.111	0.111
16	0.112	0.112	0.112	0.113	0.113	0.114	0.114	0.115	0.115	0.115
17	0.116	0.116	0.117	0.117	0.118	0.118	0.118	0.119	0.119	0.120
18	0.120	0.121	0.121	0.121	0.122	0.122	0.123	0.123	0.124	0.124
19	0.125	0.125	0.126	0.126	0.126	0.127	0.127	0.128	0.128	0.129
20	0.129	0.130	0.130	0.131	0.131	0.132	0.132	0.133	0.133	0,134
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

From the Greenwich Observations.

Temper-					Teaths of	Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In. 0.137	Eng. In. 0.137	Eng. In. 0.138	Eng. In. 0.138	Eng. Ir 0.139
21	0.134	0.135	0.135	0.136	0.136					
22	0.139	0.140	0.140	0.141 0.146	0.141	0.142	0.142	0.143	0.143	0.144
23	0.144	0.145	0.145			0.147	0.147	0.148	0.148	0.145
24	0.150	0.150	0.151	0.152	0.152	0.152	0.158	0.155	0.160	0.160
25	0.155	0.156	0.190	0.197	0.157	0.100	0.100	0.199	0.100	0.100
26	0.161	0.161	0.162	0.163	0.163	0.164	0.164	0.165	0.165	0.166
27	0.167	0.167	0.168	0.168	0.169	0.170	0.170	0.171	0.172	0.172
28	0.173	0.173	0.174	0.175	0.175	0.176	0.177	0.177	0.178	0.178
29	0.179	0.180	0.180	0.181	0.182	0.182	0.183	0.184	0.184	0.185
30	0.186	0.186	0.187	0.188	0.188	0.189	0.190	0.190	0.191	0.192
	4	0.400	0.104	0.104	0.105	0.100	0.10*	0.10*	0.100	0.100
31	0.192	0.193	0.194	0.194	0.195	0.196	0.197	0.197	0.198	0.198
32	0.199	0.200	0.201	0.201	0.202	0.203	0.204	0.204	0.205	-
33	0.207	0.207	0.208	0.209		0.210	0.211	0.212	0.213	0.213
34	0.214	0.215	0.216	0.216	0.217	0.218	0.219	0.219	0.220	0.22
35	0.222	0.223	0.223	0.224	0.225	0.226	0.227	0.227	0.228	0.229
36	0.230	0.231	0.231	0.232	0.233	0.234	0.235	0.235	0.236	0.23
37	0.238	0.239	0.240	0.240	0.241	0.242	0.243	0.244	0.245	0.24
38	0.246	0.247	0.248	0.249	0.250	0.251	0.252	0.253	0.253	0.25
39	0.255	0.256	0.257	0.258	0.259	0.260	0.261	0.262	0.263	0.26
40	0.264	0.265	0.266	0.267	0.268	0.269	0.270	0.271	0.272	0.27
ala:	often s	amon !	MATE AND A	THE Y		0.00	PP (	1000	HILE	
41	0.274	0.275	0.276	0.277	0.278	0.279	0.280	0.281	0.282	0.28
42	0.283	0.284	0.285	0.286	0.287	0.288	0.289	0.290	0.291	0.29
43	0.293	0.295	0.296	0.297	0.298	0.299	0.300	0.301	0.302	0.30
44	0.304	0.305	0.306	0.307	0.308	0.309	0.310	0.311	0.312	0.313
45	0.315	0.316	0.317	0.318	0.319	0.320	0.321	0.322	0.323	0.32
	0.000	0.00#	0.000	0.000	0.000	0.001	0.000	0.000	0.005	Λ 99
46	0.326	0.327	0.328	0.329	0.330	0.331	0.332	0.333	0.335	0.33
48	0.337	0.338	0.339	0.340	0.342	100000000000000000000000000000000000000	0.344	0.345	0.346	0.34
48	0.349	0.350	0.351	0.352	0.354	0.355	0.356	0.357	0.358	0.36
50	0.361	0.362	0.363	0.365	0.366	0.367	0.368	0.370	0.371	0.38
00	0.013	0.019	0.010	0.511	0.019	0.000	0.301	0.002	0.003	0.000
51	0.386	0.388	0.389	0.390	0.392	0.393	0.394	0.396	0.397	0.398
52	0.400	0.401	0.402	0.404	0.405	0.407	0.408	0.409	0.411	0.41
53	0.414	0.415	0.416	0.418	0.419	0.421	0.422	0.423	0.425	0.420
54 55	0.428	0.429 0.444	0.431 0.445	0.432 0.447	0.434 0.449	0.435 0.450	0.437 0.452	0.438 0.453	0.440 0.455	0.41
			0.110	0.111	0.443	0.400	0.402	0.400	0.100	0.30
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

70

# ELASTIC FORCE OF AQUEOUS VAPOR.

From the Greenwich Observations.

Fahren- heit.				40000	Tenths of	Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In
56	0.458	0.459	0.461	0.462	0.464	0.465	0.467	0.469	0.470	0.472
57	0.473	0.475	0.476	0.478	0.480	0.481	0.483	0.485	0.486	0.488
58	0.489	0.491	0.493	0.494	0.496	0.498	0.499	0.501	0.503	0.504
59	0.506	0.508	0.509	0.511	0.513	0.515	0.516	0.518	0.520	0.521
60	0.523	0.525	0.527	0.528	0.530	0.532	0.534	0.536	0.537	0.539
F 6044	OWNER	Toll all all	a study		T MY	BRK 1	Make a	MIN D	T 111 4	05.617
61	0.541	0.543	0.544	0.546	0.548	0.550	0.552	0.554	0.555	0.557
62	0.559	0.561	0.563	0.565	0.567	0.568	0.570	0.572	0.574	0.576
63	0.578	0.580	0.582	0.584	0.586	0.588	0.590	0.591	0.593	0.595
64	0.597	0.599	0.601	0.603	0.605	0.607	0.609	0.611	0.613	0.615
65	0.617	0.619	0.621	0.623	0.626	0.628	0.630	0.632	0.634	0.636
	1.0164	es mi	1989 14	i de To	at or h		2.5		en data	
66	0.638	0.640	0.642	0.644	0.646	0.648	0.651	0.653	0.655	0.657
67	0.659	0.661	0.664	0.666	0.668	0.670	0.672	0.674	0.677	0.679
68	0.681	0.684	0.686	0.688	0.690	0.692	0.695	0.697	0.699	0.701
69	0.704	0.706	0.708	0.711	0.713	0.715	0.717	0.720	0.722	0.725
70	0.727	0.729	0.732	0.734	0.736	0.739	0.741	0.744	0.746	0.748
	0.121	0.125	0.702	0.104	0.100	0.103	0	0.141	0.740	0.140
77	0.751	0.753	0.756	0.758	0.761	0.763	0 700	0.500	0.771	0.773
71 72	0.751	0.733	0.781		0.785	1 (TAMED 17)	0.766	0.768	10000	0.713
73	0.776	0.803	0.781	0.783	0.785	0.787	0.790	0.792	0.795 0.822	0.797
74	0.827	0.830	0.832	0.835	0.838	0.814	0.817	0.819	0.849	0.824
75	0.854	0.857	0.860	0.862	0.865	0.868	0.871	0.840	0.876	0.879
10	0.004	0.007	0.000	0.002	0.005	0.000	0.071	0.073	0.010	0.075
wo .	0.000	0.005	0.00=	0.000	0.000	0.000	0.000	0.000	0.00=	0.000
76	0.882	0.885	0.887	0.890	0.893	0.896	0.899	0.902	0.905	0.908
77	0.910	0.913	0.916	0.919	0.922	0.925	0.928	0.931	0.934	0.937
78	0.940	0.943	0.946	0.949	0.952	0.955	0.958	0.961	0.964	0.967
79 80	0.970	0.973	0.976	0.979	0.983	0.986	0.989	0.992	0.995	0.998
80	1.001	1.005	1.008	1.011	1.014	1.017	1.021	1.024	1.027	1.030
0.							- 0-0	5	- 000	
81	1.034	1.037	1.040	1.043	1.047	1.050	1.053	1.057	1.060	1.063
82	1.067	1.069	1.073	1.077	1.080	1.083	1.087	1.090	1.094	1.097
83	1.101	1.104	1.108	1.111	1.114	1.118	1.121	1.125	1.129	1.132
84	1.136	1.139	1.143	1.146	1.150	1.153	1.157	1.160	1.164	1.167
85	1.171	1.175	1.178	1.182	1.186	1.190	1.193	1.197	1.201	1.205
100	E G F LE Y		1000	1	3411					
86	1.209	1.212	1.216	1.220	1.224	1.228	1.232	1.235	1.239	1.243
87	1.247	1.251	1.255	1.258	1.262	1.266	1.270	1.274	1.278	1.282
88	1.286	1.290	1.294	1.298	1.302	1.306	1.310	1.314	1.318	1.322
89	1.326	1.330	1.335 1.376	1.339	1.343	1.347	1.351	1.355	1.359	1.364
90	1.368	1.372	1.910	1.001	1.385	1.389	1.393	1.397	1.402	1.406
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

### XII.

## PSYCHROMETRICAL TABLE,

GIVING THE TEMPERATURE OF THE DEW-POINT, THE FORCE AND THE WEIGHT OF VAPOR IN THE ATMOSPHERE, AND ITS RELATIVE HUMIDITY, DEDUCED FROM THE INDICATIONS OF THE PSYCHROMETER, OR DRY AND WET BULB THERMOMETERS.

#### By James Glaisher.

This elaborate table, first published in London, in 1847, in pamphlet form, by J. Glaisher, of the Royal Observatory at Greenwich, is based on the tables of elastic forces of vapor deduced from Dalton's experiments, and given above, Table XI.

The weight of a cubic foot of dry air at 32° Fahrenheit, and under the barometric pressure of 30 inches, which has been adopted by Glaisher, and from which the weight of vapor in a cubic foot of air is derived, is the mean of the determinations obtained by Shuckburgh and by Biot and Arago, which is 563.2154 grains Troy; 563 being the number actually used in the calculations. See Preface to the Table, p. 13, and also the Greenwich Meteorological Observations for 1842, p. xlvi.

The coefficient of the expansion of air which has been employed is that determined by the experiments of Gay-Lussac, according to which the air expands 0.00375 of its bulk for 1° Centigrade, or  $\frac{1}{480}$  for 1° Fahrenheit.

All these values, as may be seen by comparing Tables VI. and XI. of the elastic forces, and also page 92, materially differ from those more recently determined with great care by Regnault, and on which are based the Psychrometrical Tables given above, page 50 et seq. This will account for the no inconsiderable differences often found between the results in the two tables derived from the same data. A few examples, taken from various parts of the tables, may be given here, in order to enable the meteorologist to judge of the amount of the discrepancies which may occur in the results when computed from different hygrometrical constants.

1. Suppose the temperature of the air indicated by the dry thermometer ter to be  $= 10^{\circ} \text{ F}$ .

The temperature of evaporation indicated by the wet thermometer  $= 9^{\circ} \text{ F}$ .

Difference  $= 10^{\circ} \text{ F}$ .

Then, Glaisher's table gives,

The Force of Vapor = 0.065 inch. The Relative Humidity = 0.730

Guyot's table gives,

The Force of Vapor = 0.054 inch.

The Relative Humidity = 0.791

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2. By observation we have,

Dry Thermometer  $= 50^{\circ}$  F.

Wet Thermometer = 40° F.

Difference = 10° F.

Then, by Glaisher's table, we find,

Force of Vapor = 0.186 inch.

Relative Humidity = 0.495

And by Guyot's table, we find,

Force of Vapor = 0.117 inch.

Relative Humidity = 0.322

3. The reading of the

Dry Thermometer is = 90° F.

Wet Thermometer is  $= 70^{\circ}$  F.

Difference = 20° F.

By Glaisher's table we have,

Force of Vapor = 0.523 inch.

Relative Humidity = 0.381

And by Guyot's table,

Force of Vapor = 0.464 inch.

Relative Humidity = 0.329

The temperatures of the Dew-Point, given in Glaisher's tables, have been computed by means of the empirical factors given below, page 140, and in the manner there described. See Preface to the Table, page 11.

## ARRANGEMENT OF THE TABLE.

In the first two columns, at the left, are found the indications, in degrees of Fahrenheit, of the dry and wet bulb thermometers. In the following columns, in their order, and opposite to each of the temperatures of the wet thermometer, are given the temperature of the dew-point; the force of vapor, in English inches; the weight of vapor, in grains, contained in a cubic foot of air; the amount of the same required for saturation; and the relative humidity in thousandths, corresponding to the difference of temperature between the two thermometers. The second half of the page, at the right, furnishes, in seven columns, the weight, in grains, of a cubic foot of air, under various barometric pressures from 28 to 31 inches, and in the different hygrometric conditions indicated by the differences of the two thermometers. These numbers have been computed in the manner described below, page 142.

The range of the table extends from 10° to 90° of the dry thermometer, or of the temperature of the air. From 10° to 34° Fahrenheit the results are calculated for every second, third, and fifth of a degree of the wet thermometer, and for extreme differences of the temperature of evaporation ranging from 2° to 5° below the temperature of the air. From 34° to 90° the results are given only for every full degree of the wet thermometer, and for extreme differences gradually increasing

B

#### PSYCHROMETRICAL TABLE.

from 5° to 25°. This range falls short of the wants of the extreme climate of North America, where temperatures above 90° and far below 10° are of usual occurrence over a great portion of the continent. The same may be said of the range of the differences between the two thermometers in the first part of the table. The double interpolation for the fractions of degrees of both thermometers being rather too large to be neglected, its application becomes inconvenient.

#### USE OF THE TABLE.

Enter the table with the observed temperatures of the dry and wet bulb thermometers. On the same line as the last, and in their appropriate columns, the results deduced from these data will be found.

## Example.

The observation has given,

Temperature of the air by the dry thermometer = 62° F

Temperature of evaporation by the wet-bulb thermometer  $= 53^{\circ}$  F.

Page 129, find in the first column, headed Reading of the Dry Thermometer, the temperature of 62°, and in the second, that of the wet, 53°. On the line beginning with 53° are found, in their respective columns, the results deduced from these data, viz.:—

The temperature of the Dew-point  $= 46^{\circ}.7$  F.

The force of vapor in the air = 0.333 inch.

The weight of vapor in a cubic foot of air = 3.72 grains.

The amount of vapor required for saturation = 2.53 grains.

The relative humidity in thousandths = 0.595

	ding	Temp.	Force	Wei of V	ight apor	Hu-		Weigh	t in Grain	as of a Cu	ibic Foot	of Air.	
mon	neter,	of Dew-	of Vapor	In a	for	midity, Satura-		Height o	of the Bar	ometer i	n English	Inches.	Tayle III
		Point, Fahr.	English	Cubic Foot of Air.	Sat'n. of aCu- bic Ft.	tion = 1.000.	in.	in.	in.	in.	in.	in.	in.
Dry.	Wet.	3 (6)	Inches.	Air.	of Air.		28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr. 589.4	gr. 599.2	gr. 609.0
10	9.8	10.0	0.089	1.11	0.00	1.000 0.946	550.1 550.2	560.0	569.8 569.9	579.6 579.7	589.5	599.3	609.1
15	9.6	6.6	0.079	0.98	0.13	0.883	550.2	560.1	569.9	579.7	589.5	599.3	609.1
0.1	9.4	4.9	0.074	0.92	0.19	0.829	550.2	560.1	569.9	579.7	589.5	599.3	609.1
	9.2	3.2	0.069	0.86	0.25	0.775	550.3	560.2	570.0	579.8	589.6	599.4	609.2
	9.0	1.5	0.065	0.81	0.30	0.730	550.3	560.3	570.0	579.8	589.6	599.4	609.3
11	11.0	11.0	0.093	1.15	0.00	1.000	548.9	558.7	568.5	578.3	588.1	597.9	607.7
5.7	10.8	9.3	0.087	1.08	0.07	0.939	548.9	558.7	568.5	578.3	588.1	597.9	607.7
	10.6	7.6	0.082	1.02	0.13	0.887	549.0	558.8	568.6	578.4	588.2	598.0	607.8
700	10.4	5.9	0.077	0.96	0.19	0.835	549.0	558.8	568.6	578.4	588.2	598.0	607.8
	10.2	4.2	0.072	0.90	0.25	0.783	549.0	558.8	568.6	578.4	588.2	598.0	607.8
7.6	10.0	2.5	0.067	0.84	0.31	0.731	549.1	558.9	568.7	578.6	588.3	598.1	607.9
Ad	9.8	0.8	0.063	0.78	0.37	0.679	549.1	558.9	568.7	578.6	588.3	598.1	607.9
12	12.0	12.0	0.096	1.19	0.00	1.000	547.7	557.5	567.2	577.0	586.8	596.6	606.4
4.9	11.8	10.3	0.090	1.12	0.07	0.942	547.7	557.5	567.2	577.0	586.8	596.6	606.4
0.0	11.6	8.6	0.085	1.05	0.14	0.883	547.8	557.6	567.3	577.1	586.9	596.7	606.5
100	11.4	6.9	0.080	0.99	0.20	0.832	547.8	557.6	567.3	577.1	586.9	596.7	606.5
Das 1	11.2	5.2	0.075	0.93	0.26	0.782	547.8	557.6	567.3	577.1	586.9	596.7	606.5
	11.0	3.5	0.070	0.87	0.32	0.731	547.9	557.7	567.4	577.2	587.0	596.8	606.6
	10.8	1.8	0.066	0.81	0.38	0.681	547.9	557.7	567.4	577.2	587.0	596.8	606.6
	10.6	0.1	0.061	0.76	0.43	0.639	547.9	557.7	567.4	577.2	587.0	596.8	606.6
13	13.0	13.0	0.100	1.24	0.00	1.000	546.5	556.3	566.0	575.8	585.5	595.3	605.0
9.8	12.8	11.3	0.094	1.16	0.08	0.936	546.5	556.3	566.0	575.8	585.5	595.3	605.0
7.28	12.6	9.6	0.088	1.08	0.16	0.871	546.6	556.4	566.1	575.9	585.6	595.4	605.1
	12.4	7.9	0.083	1.02	0.22	0.823	546.7	556.5	566.2	576.0	585.7	595.5	605.2
	12.2	6.2	0.077	0.97	0.27	0.783	546.7	556.5	566.2	576.0 576.0	585.7 585.7	595.5 595.5	605.2
	11.8	4.5 2.8	0.073	0.91	0.33	0.734	546.7	556.5 556.6	566.2 566.3	576.1	585.8	595.6	605.3
	11.6	1.1	0.064	0.79	0.45	0.637	546.8	556.6	566.3	576.1	585.8	595.6	605.3
14	140		0.104	1 00	0.00	1 000	F 15 0	=== 0	FOIN	574.4	584.2	594.0	603.7
14	14.0	14.0	0.104	1.28	0.00	1.000	545.3 545.3	555.0 555.0	564.7	574.4	584.2	594.0	603.7
2.71	13.6	10.6	0.091	1.12	0.08	0.935	545.4	555.1	564.8	574.5	584.3	594.1	603.8
1	13.4	8.9	0.086	1.06	0.22	0.828	545.4	555.1	564.8	574.5	584.3	594.1	603.8
	13.2	7.2	0.080	1.00	0.28	0.782	545.4	555.1	564.8	574.5	584.3	594.1	603.8
	13.0	5.5	0.075	0.93	0.35	0.727	545.5	555.2	564.9	574.6	584.4	594.2	603.9
	12.8	3.8	0.071	0.87	0.41	0.680	545.5	555.2	564.9	574.6	584.4	594.2	603.9
	12.6	2.1	0.066	0.82	0.46	0.641	545.6	555.3	565.0	574.7	584.5	594.2	603.9
15	15.0	15.0	0.108	1.32	0.00	1.000	544.0	553.8	563.5	573.2	582.9		602.3
10.0	14.8	13.3	The second second	1.24	-			553.8	The second		582.9		
	14.6	11.6	The second second	1.16			A STATE OF THE PARTY OF THE PAR		1000	ALC: UNITED BY	583.0	10/7/35/35	602.4
	14.4	9.9	The second	1000		1	The state of the s	1 110	And the second		12 THE R. P.	100 Carlotte 11 11	602.4
	14.2	8.2		1.04		4 Tal 100				10113.66143	1000	The same of the	THE REAL PROPERTY.
	14.0											0.00	1
	13.8	11			4 44 44	The state of the s	The State of the S		1	3432	583.1 583.2		155000
<u></u>	D	11 0.1	1 01000	10.00	70.21	1 010 74	105	1004.1	70000	101010	1 000.2	004.0	1 002.0

	ading Ther-	Temp.	Force		apor	Hu-		Weigh	t in Grai	ns of a Cu	ubic Foot	of Air.	
	meter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
16	16.0	16.0	0.112	1.37	0.00	1.000	542.8	552.5	56212	571.9	581.6	591.3	601.0
	15.8	14.3	0.105	1.29	0.08	0.942	542.9	552.6	562.3	572.0	581.7	591.4	601.
741	15.6	12.6	0.098	1.21	0.16	0.883	542.9	552.6	562.3	572.0	581.7	591.4	601.
	15.4	10.9	0.092	1.14	0.23	0.832	543.0	552.7	562.4	572.1	581.8	591.5	601.
	15.2	9.2	0.087	1.07	0.30	0.781	543.0	552.7	562.4	572.1	581.8	591.5	601.
Vic.	15.0	7.5	0.081	1.00	0.37	0.730	543.0	552.7	562.4	572.1	581.8	591.5	601.
170	14.8	5.8	0.076	0.94	0.43	0.686	543.1	552.8	562.5	572.1	581.9	591.6	601.
	14.6	4.1	0.072	0.88	0.49	0.643	543.1	552.8	562.5	572.1	581.9	591.6	601.
17	17.0	17.0	0.116	1.41	0.00	1.000	541.3	551.0	560.8	570.5	580.1	589.8	599.
10.	16.8	15.3	0.109	1.33	0.08	0.943	541.3	551.0	560.8	570.5	580.1	589.8	599.
MA	16.6	13.6	0.102	1.25	0.16	0.897	541.4	551.1	560.9	570.6	580.2	589.9	599.
148	16.4	11.9	0.096	1.17	0.24	0.830	541.4	551.1	560.9	570.6	580.2	589.9	599.
150	16.2	10.2	0.090	1.10	0.31	0.780	541.5	551.2	561.0	570.7	580.3	590.0	599.
	16.0	8.5	0.084	1.03	0.38	0.730	541.5	551.2	561.0	570.7	580.3	590.0	599.
179	15.8	6.8	0.079	0.97	0.44	0.688	541.5	551.2	561.0	570.7	580.3	590.0	599.
	15.6	5.1	0.074	0.91	0.50	0.646	541.6	551.3	561.1	570.8	580.4	590.1	599.
18	18.0	18.0	0.120	1.47	0.00	1.000	540.5	550.2	559.8	569.5	579.1	588.8	598.
	17.8	16.3	0.113	1.38	0.09	0.939	540.5	550.2	559.8	569.5	579.1	588.8	598.
	17.6	14.6	0.106	1.29	0.18	0.878	540.6	550.3	559.9	569.6	579.2	588.9	598.
FO.	17.4	12.9	0.099	1.21	0.26	0.824	540.6	550.3	559.9	569.6	579.2	588.9	598.
100	17.2	11.2	0.093	1.14	0.33	0.776	540.7	550.4	560.0	569.7	579.3	589.0	598.
4.2	17.0	9.5	0.088	1.07	0.40	0.728	540.7	550.4	560.0	569.7	579.3	589.0	598.
	16.8	7.8	0.082	1.01	0.46	0.688	540.7	550.5	560.1	569.8	579.3	589.0	598.
à	16.6	6.1	0.077	0.95	0.52	0.647	540.8	550.6	560.2	569.9	579.4	589.1	598.
19	19.0	19.0	0.125	1.52	0.00	1.000	539.3	548.9	558.5	568.2	577.8	587.5	597.
	18.8	17.3	0.117	1.43	0.09	0.941	539.3	548.9	558.5	568.2	577.8	587.5	597.
1	18.6	15.6	0.110	1.34	0.18	0.882	539.4	549.0	558.6	568.3	577.9	587.6	597.
rub.	18.4	13.9	0.103	1.26	0.26	0.829	539.4	549.0	558.6	568.3	577.9	587.6	597.
	18.2	12.2	0.097	1.18	0.34	0.776	539.5	549.1	558.7	568.4	578.0	587.7	597.
	18.0	10.5	0.091	1.11	0.41	0.730	539.5	549.1	558.7	568.4	578.0	587.7	597.
123	17.8	8.8	0.085	1.04	0.48	0.684	539.6	549.2	558.8	568.5	578.1	587.8	597.
	17.6	7.1	0.080	0.98	0.54	0.645	539.6	549.2	558.8	568.5	578.1	587.8	597.
20	20.0	20.0	0.129	1.58	0.00	1.000	538.1	547.7	557.3	566.9	576.5	586.1	595.
	19.8	18.3	0.121	1.48	0.10	0.937	538.2	547.8	557.4	567.0	576.6	586.2	595.
	19.6	16.6	0.114	1.38	0.20	0.874	538.3	547.9	557.5	567.1	575.7	586.3	595.
	19.4	14.9	0.107	1.30	0.28	0.823	538.3	547.9	557.5	567.1	576.7	586.3	595.
	19.2	13.2	0.101	1.23	0.35	0.779	538.3	547.9	557.5	567.1	576.7	586.3	595.
	19.0	11.5	0.094	1.15	0.43	0.728	538.4	548.0	557.6	567.2	576.8	586.4	596.
	18.8	9.8	0.089	1.08	0.50	0.684	538.4	548.0	557.6	567.2	576.8	586.4	596.
	18.6	8.1	0.083	1.01	0.57	0.639	538.5	548.1	557.7	567.3	576.9	586.5	596.
	18.4	6.4	0.078	0.95	0.63	0.601	538.5	548.1	557.7	567.3	576.9	586.5	596.
					0.00	0.301	000.0	040.1	001.1	007.0	0.0.3	000.0	000.
	1		Ph (4)	GP.	985		1163	30%	100			0,819	
	1	JI .			TATE OF	SHE!	A PRICE	3 P 4 P	100	Printer State	100		

	ding Ther-	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grai	as of a Cu	ibic Foot	of Air.	
mon	neter,	of Dew-	of Vapor	In a	Reqd.	midity, Satura-		Height o	of the Bar	rometer i	n English	Inches.	del.
		Point, Fahr.	in English Inches.	Foot of Air.	Sat'n. of aCu- bic Ft.	tion = 1.000.	in.	in.	in.	in.	in.	in.	in.
Dry.	Wet.		Theres.	A.I.	of Air.	S. J. Brit	28.0	28.5	29.0	29.5	30.0	30.5	31.0
21	91.0	21.0	in. 0.134	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr. 575.3	gr. 584.9	gr. 594.5
41	21.0	19.3	0.134	1.63	0.00	1.000	537.0 537.0	546.6 546.6	556.1 556.1	565.7 565.7	575.3	584.9	594.5
	20.6	17.6	0.118	1.44	0.19	0.884	537.1	546.7	556.2	565.8	575.4	585.0	594.6
	20.4	15.9	0.111	1.36	0.27	0.835	537.1	546.7	556.2	565.8	575.4	585.0	594.6
	20.2	14.2	0.104	1.28	0.35	0.785	537.2	546.8	556.3	565.9	575.5	585.1	594.
364	20.0	12.5	0.098	1.20	0.43	0.736	537.2	546.8	556.3	565.9	575.5	585.1	594.
10	19.8	10.8	0.092	1.12	0.51	0.687	537.3	546.9	556.4	566.0	575.6	585.2	594.8
	19.6	9.1	0.086	1.05	0.58	0.644	537.3	546.9	556.4	566.0	575.6	585.2	594.
	19.4	7.4	0.081	0.99	0.64	0.607	537.3	546.9	556.4	566.0	575.6	585.2	594.8
22	22.0	22.0	0.139	1.69	0.00	1.000	535.7	545.3	554.9	564.5	574.0	583.6	593.
	21.8	20.3	0.131	1.59	0.10	0.941	535.8	545.4	555.0	564.6	574.1	583.7	593.
	21.6	18.6	0.123	1.49	0.20	0.882	535.8 535.9	545.4 545.5	555.0 555.1	564.6 564.7	574.1 574.2	583.7 583.8	593.5
	21.2	15.2	0.113	1.31	0.25	0.775	535.9	545.5	555.1	564.7	574.2	583.8	593.
	21.0	13.5	0.102	1.23	0.46	0.728	536.0	545.6	555.2	564.8	574.3	583.9	593.
100	20.8	11.8	0.096	1.16	0.40	0.686	536.0	545.6	555.2	564.8	574.3	583.9	593.
100	20.6	10.1	0.090	1.09	0.60	0.645	536.1	545.7	555.3	564.9	574.4	584.0	593.
10	20.4	8.4	0.084	1.02	0.67	0.604	536.1	545.7	555.3	564.9	574.4	584.0	593.
100 100 100 100 100 100 100 100 100 100	20.2	6.7	0.079	0.96	0.73	0.568	536.1	545.7	555.3	564.9	574.4	584.0	593.
00	20.0	200							J			-	
23	23.0	23.0	0.144	1.75	0.00	1.000	534.6	544.2	553.7	563.3	572.8	582.4	591.
	22.6	21.3 19.6	0.136	1.65	0.10	0.943	534.6	544.2 544.3	553.7 553.8	563.3 563.4	572.8 572.9	582.4 582.5	591.5 592.6
	22.4	17.9	0.127	1.45	0.30	0.829	534.7	544.3	553.8	563.4	572.9	582.5	592.
ins	22.2	16.2	0.112	1.36	0.39	0.777	534.8	544.4	553.9	563.5	573.0	582.6	592.
	22.0	14.5	0.106	1.28	0.47	0.731	534.8	544.4	553.9	563.5	573.0	582.6	592.
148	21.8	12.8	0.099	1.21	0.54	0.691	534.9	544.5	554.0	563.6	573.1	582.7	592.
中華	21.6	11.1	0.093	1.13	0.62	0.646	534.9	544.5	554.0	563.6	573.1	582.7	592.
1	21.4	9.4	0.087	1.06	0.69	0.606	535.0	544.6	554.1	563.7	573.2	582.8	592.
	21.2	7.7	0.082	1.00	0.75	0.571	535.0	544.6	554.1	563.7	573.2	582.8	592.
9.4	94.0	94.0	0.750	1.01	0.00	1 000	F00	F40.5		F00 6		*0	
24	24.0	24.0	0.150	1.81	0.00	1.000	533.4	542.9 543.0	552.4 552.5	562.0 562.1	571.5 571.6	581.1	590. 590.
1	23.6	11			0.09	0.901	533.5		552.5		571.6	1	590.
	23.4		0.127	1	0.26	0.856	A STATE OF THE PARTY OF THE PAR	200 000	100000	THE RESERVED A	571.7		590.
	23.2	18.2	0.121	1	0.35	0.807	533.6	543.2	552.6		571.7	581.3	590.
	23.0	16.7	0.115	1.38	0.43	0.762	533.7	543.3	552.7	562.3	571.8	581.4	590.
	22.8	15.2	0.108	The second	The Late of the La	0.724	M - 30 (5 M) - (3)	The state of	100000	1.15	571.8	A CONTRACTOR OF	100
	22.6	13.8	0.103	1.24	0.57	0.685	533.7	46319708-13			571.8	581.4	
T'S	22.4	12.3	0.097		1	0.652	W. W. S. S. S. L. C.	543.4	100000000000000000000000000000000000000	The state of the state of	THE PARTY OF	581.5	100 miles
	22.2	10.8	0.091	1.12	0.69	0.634	533.8	543.4	552.8	562.4	571.9	581.5	591.

Res	ding Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ns of a Cu	able Foot	of Air.	
mon	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	30.0	30.5	in. 31.0
0	0	0	in.	gr.	gr.	1.000	gr. 532.3	gr.	gr.	gr.	gr.	gr.	gr. 589.3
25	25.0	25.0	0.155	1.87	0.00	0.952	532.3	541.8 541.8	551.3 551.3	560.8 560.8	570.3 570.3	579.8 579.8	589.3
	24.6	22.4	0.141	1.70	0.17	0.909	532.4	541.9	551.4	560.9	570.4	579.9	589.4
inco	24.4	21.2	0.135	1.62	0.25	0.867	532.4	541.9	551.4	560.9	570.4	579.9	589.4
	24.2	19.9	0.129	1.55	0.32	0.829	532.4	541.9	551.4	560.9	570.4	579.9	589.4
	24.0	18.6	0.123	1.48	0.49	0.791	532.5	542.0	551.5	561.0	570.5	580.0	589.5
	23.8	17.3	0.117	1.41	0.46	0.754	532.5	542.0	.551.5	561.0	570.5	580.0	589.5
1	23.6	16.0	0.112	1.34	0.53	0.717	532.6	542.1	551.6	561.1	570.6	580.1	589.6
	23.4	14.8	0.107	1.28	0.59	0.685	532.6	542.1	551.6	561.1	570.6	580.1	589.6
	23.2	13.5	0.102	1.22	0.65	0.653	532.6	542.1	551.6	561.1	570.6	580.1	589.6
26	26.0	26.0	0.161	1.93	0.00	1.000	531.1	540.6	550.0	559.5	569.0	578.5	588.0
	25.8	24.8	0.154	1.85	0.08	0.959	531.2	540.7	550.1	559.6	569.1	578.6	588.1
	25.6	23.6	0.147	1.78	0.15	0.923	531.2	540.7	550.1	559.6	569.1	578.6	588.1
	25.4	22.3	0.141	1.70	0.23	0.881	531.2	540.7	550.1	559.6	569.1	578.6	588.1
	25.2	21.2	0.135	1.62	0.31	0.839	531.3	540.8	550.2	559.7	569.2	578.7	588.2
	25.0	19.9	0.129	1.55	0.38	0.804	531.3	540.8	550.2	559.7	569.2	578.7	588.2
7570	24.8	18.7	0.123	1.48	0.45	0.767	531.4	540.9	550.3	559.8	569.3	578.8	588.3
	24.6	17.5	0.118	1.41	0.52	0.731	531.4	540.9	550.3	559.8	569.3	578.8	588.3
Op.	24.4	16.2	0.112	1.35	0.58	0.700	531.4	540.9	550.3	559.8	569.3	578.8	588.3
	24.2	15.0	0.108	1.29	0.64	0.668	531.5	541.0	550.4	559.9	569.4	578.9	588.4
(6. B)	100	100	-1/19	75 ES	- X2	C.F.	100	nengi	ince.	TI U	3 11 17	and the	A 18
27	27.0	27.0	0.167	2.00	0.00	1.000	529.9	539.4	548.9	558.4	567.8	577.3	586.7
	26.7	25.2	0.156	1.88	0.12	0.940	529.9	539.4	548.9	558.4	567.8	577.4	586.8
100	26.4	23.3	0.146	1.76	0.24	0.880	530.0 530.1	539.5 539.6	549.0 549.1	558.5 558.6	567.9 568.0	577.5 577.6	586.9 587.0
	25.8	19.7	0.128	1.53	0.47	0.765	530.1	539.6	549.1	558.6	568.0	577.6	587.0
918	25.5	17.8	0.119	1.43	0.57	0.715	520.0	E20 7	540.0	EE0 #	568.1	577.7	587.1
*	25.2	16.0	0.119	1.43	0.66	0.715	530.2 530.3	539.7 539.8	549.2	558.7 558.8	568.2	577.8	587.2
	24.9	14.2	0.104	1.26	0.74	0.630	530.3	539.8	549.3	558.8	568.2	577.8	587.2
	24.6	12.4	0.098	1.17	0.83	0.585	530.4	539.9	549.4	558.9	568.3	577.9	587.3
	24.3	10.5	0.091	1.09	0.91	0.545	530.5	540.0	549.5	559.0	568.3	577.9	587.3
			148	100	1/2-1/1		75.16		1		. 1		#1
28	28.0	28.0	0.173	2.07	0.00	1.000	528.7	538.1	547.6	557.0	566.5	575.9	585.4
9.8	27.7	26.3	1			0.942					566.6		585.5
20.55	27.4	24.6	0.153	1.84	0.23	0.889	528.9	538.3	547.8	557.2	566.7	576.1	585.6
	27.1	22.9	0.144	1.73	0.34	0.836	528.9	538.3	547.8	557.2	566.7	576.1	585.6
	26.8	21.2	0.135	1.62	0.45	0.783	529.0	538.4	547.9	557.3	566.8	576.2	585.7
	26.5	19.4	0.126	1.52	0.55	0.734	529.1	538.5	548.0	557.4	566.9	576.3	585.8
	26.2	17.7	0.119	1.42	0.65	0.686	529.1	538.5	1		566.9	576.3	585.8
	25.9	16.0	0.112	1.34	0.73	0.648	529.2	538.6	548.1	557.5	567.0	576.4	585.9
	25.6	14.3	0.105	1.26	0.82	0.604	529.2	538.6	548.1		567.0	576.4	585.9
	20.3	12.6	0.098	1.18	0.89	0.571	529.2	538.6	548.1	557.5	567.0	576.4	585.9

I					We	ight	1			70.00				
	of !	ading Ther-	Temp.	Force	of V	apor Read.	Hu-		Weigh	t in Grain	ns of a Cr	ıbic Foot	of Air.	
		neter, ahr.	of Dew-	of Vapor	In a	for	midity, Satura-	1	Height o	of the Ba	rometer i	n English	Inches.	100
1			Point, Fahr.	in English	Cubic Foot of		tion = 1.000.	in.	in.	in.	in.	in.	in.	in.
	Dry.	Wet.	5 04	Inches.	Air.	of Air.	1	28.0	28.5	29.0	29.5	30.0	30.5	31.0
1	0	0	0	in.	gr.	gr.	an L	gr.	gr.	gr.	gr.	gr.	gr.	gr.
	29	29.0	29.0	0.179	2.14	0.00	1.000	527.6	537.0	546.5	555.9	565.3	574.7	584.1
	TO THE	28.7	27.5	0.170	2.03 1.92	0.11	0.949	527.7	537.1	546.6	556.0	565.4	574.8	584.2
		28.1	24.5	0.151	1.82	0.22	0.898	527.7 527.8	537.1 537.2	546.6 546.7	556.0 556.1	565.4 565.5	574.8 574.9	584.2 584.3
		27.8	23.0	0.144	1.73	0.41	0.809	527.8	537.2	546.7	556.1	565.5	574.9	584.3
		William .		114		14		02110	00112	0 10				
		27.5	21.5	0.137	1.64	0.50	0.766	527.9	537.3	546.7	556.2	565.6	575.0	584.5
		27.2	20.0	0.129	1.55	0.59	0.725	528.0	537.4	546.8	556.2	565.7	575.1	584.6
		26.9	18.5 17.0	0.122	1.47	0.67	0.687	528.0	537.4	546.8	556.3	565.7	575.2	584.6
		26.3	15.5	0.110	1.38 1.30	0.76	0.617	528.1 528.1	537.5 537.5	546.9 546.9	556.4 556.4	565.8 565.8	575.3 575.3	584.7 584.7
		20.0	10.0	3.110	1.00	0.04	0.017	040.1	991.9	940.9	000.4	000.0	010.0	004.1
								17.54						
	30	30.0	30.0	0.186	2.21	0.00	1.000	526.5	535.9	545.3	554.7	564.1	573.5	582.9
1		29.7	28.6	0.177	2.10	0.11	0.951	526.5	535.9	545.3	554.7	564.1	573.5	582.9
		29.4	25.9	0.160	2.00	0.21	0.905	526.6 526.7	536.0 536.1	545.4	554.8 554.9	564.2 564.3	573.6 573.7	583.0 583.1
	0.0	28.8	24.5	0.152	1.82	0.39	0.824	526.7	536.1	545.5 545.5	554.9	564.3	573.7	583.1
		20.0		0.102		0.00	0.022	020.1	000.1	040.0	004.0	004.0	010.1	000.1
		28.5	23.1	0.145	1.73	0.48	0.783	526.8	536.2	545.6	555.0	564.4	573.8	583.2
1		28.2	21.7	0.138	1.64	0.57	0.742	526.8	536.2	545.6	555.0	564.4	573.8	583.2
		27.9	20.3	0.131	1.56	0.65	0.706	526.9	536.3	545.7	555.1	564.5	573.9	583.3
		27.6	19.0	0.125	1.49	0.72	0.674	526.9	536.3	545.7	555.1	564.5	573.9	583.3
		27.3	17.6	0.118	1.42	0.79	0.643	527.0	536.4	545.8	555.2	564.6	574.0	583.4
1	SINS		10/16		Aut.								. 9	100
1	31	31.0	31.0	0.192	2.29	0.00	1.000	525.4	534.7	544.1	553.5	562.9	572.3	581.7
	0.00	30.7	29.9	0.185	2.20	0.09	0.961	525.4	534.7	544.1	553.5	562.9	572.3	581.7
		30.4	28.8	0.178	2.12	0.17	0.926	525.5	534.8	544.2	553.6	563.0	572.4	581.8
		30.1	27.7	0.171	2.04	0.25	0.891	525.5	534.8	544.2	553.6	563.0	572.4	581.8
	177	29.8	26.6	0.164	1.95	0.34	0.852	525.6	534.9	544.3	553.7	563.1	572.5	581.9
		29.5	25.5	0.158	1.87	0.42	0.817	525.6	534.9	544.3	553.7	563.1	572.5	581.9
	1	29.2	24.4	0.152	1.80	0.49	0.786	525.6	534.9	544.3	553.7	563.1	572.5	581.9
	1	28.9	23.4	0.146	1.73	0.56	0.756	525.7	535.0	544.4	553.8	563.2	572.6	582.0
		28.6	22.3	0.141	1.67	0.62	0.729	525.7	535.0	544.4	553.8	563.2	572.6	582.0
	P	28.3	21.2	0.135	1.60	0.69	0.699	525.7	535.0	544.4	553.8	563.2	572.6	582.0
	444	1		1							1025			To all
	32	32.0	32.0	0.199	2.37	0.00	1.000	524.2	533.5	542.9	552.3	561.6	570.9	580.3
	1.5	31.6			2.27	0.10	0.958		533.6	543.0	552.4	561.7	571.0	580.4
	S A	31.2	29.5	0.182	2.17	0.20	0.916	524.4	533.7	543.1	552.5	561.8	571.1	580.5
		30.8	28.3	0.175	2.07	0.30	0.874	524.4	533.7	543.1	552.5	561.8	571.1	580.6
		30.4	27.0	0.167	1.98	0.39	0.836	524.5	533.8	543.2	552.6	561.9	571.2	580.6
	1	30.0	25.8	0.160	1.90	0.47	0.802	524.5	533.8	543.2	552.6	561.9	571.2	580.6
	Day.	29.6	24.6	0.153	1.82	0.55	0.768	524.6		Contract to the contract of	552.7	562.0	571.3	580.7
	1300	29.2	23.3	0.146	1.74	0.63	0.735	524.6	533.9	543.3	552.7	562.0	571.3	580.7
	TANK .	28.8	22.1	0.140	1.67	0.70	0.705	524.6		543.3	552.7	562.0	571.3	580.7
		28.4	20.8	0.133	1.60	0.77	0.675	524.7	534.0	543.4	552.8	562.1	571.4	580.8

Po	ading				ight			Weigh	t in Grai	ns of a Cı	shia Foot	of Air	
of	Ther-	Temp.	Force of	of V	apor Reqd.	Hu- midity,	The last	Tr Ciga	o zii Gzai	us of a or	1010 1000	01 1111	
	meter,	Dew-	Vapor	In a Cubic	for Sat'n.	Satura- tion =		Height o	of the Bar	rometer i	n English	Inches.	
		Fahr.	English Inches.		of aCu- bic Ft.	1.000.	in.						
Dry.	Wet.		ZHOHOD.	1100	of Air.		28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	- 000	gr.						
33	33.0	33.0	0.207	2.45	0.00	1.000	523.0	532.3	541.7	551.1	560.4	569.7	579.1
E181	32.5	31.6	0.197	2.33	0.12	0.951	523.1 523.2	532.5 532.6	541.8 541.9	551.2 551.3	560.5 560.6	569.8 569.9	579.2 579.3
	32.0	28.8	0.187	2.11	0.23	0.862	523.3	532.7	542.0	551.4	560.7	570.0	579.4
	31.0	27.4	0.169	2.01	0.44	0.821	523.3	532.7	542.0	551.4	560.7	570.0	579.4
37.87	30.5	26.0	0.161	1.91	0.54	0.780	523.4	532.8	542.1	551.5	560.8	570.1	579.5
	30.0	24.6	0.153	1.82	0.63	0.743	523.4	532.8	542.1	551.5	560.8	570.1	579.5
	29.5 29.0	23.2	0.145	1.65	0.80	0.711	523.5 523.5	532.9 532.9	542.2 542.2	551.6 551.6	560.9 560.9	570.2 570.2	579.6 579.6
	28.5	20.4	0.131	1.57	0.88	0.641	523.6	533.0	542.2	551.7	561.0	570.3	579.7
	20.0		0.701				525.5	555.5	012.0	551.,	551.0	0.0.0	
	010	04.0	0.071	0.50	0.00	1 000		F07 2	× 10 c	F 40 0	***	F.00 -	
34	34.0	34.0	0.214	2.53	0.00	1.000	521.9 522.0	531.2 531.4	540.6	549.9	559.2	568.5 568.6	577.8 577.9
	33.5	31.4	0.204	2.42	0.11	0.957	522.0	531.4	540.7 540.7	550.0 550.0	559.3 559.3	568.6	577.9
	32.5	30.1	0.186	2.21	0.32	0.874	522.1	531.5	540.8	550.1	559.4	568.7	578.0
	32.0	28.8	0.178	2.11	0.42	0.834	522.1	531.5	540.8	550.1	559.4	568.7	578.0
4.9	31.5	27.5	0.170	2.01	0.52	0.795	522.2	531.6	540.9	550.2	559.5	568.8	578.1
	31.0	26.2	0.162	1.91	0.62	0.755	522.3	531.7	541.0	550.3	559.6	568.9	578.2
	30.5	24.9	0.155	1.83	0.70	0.724	522.3 522.4	531.7 531.8	541.0 541.1	550.3 550.4	559.6 559.7	568.9 569.0	578.2 578.3
	29.5	22.3	0.141	1.67	0.86	0.660	522.4	531.8	541.1	550.4	559.7	569.0	578.3
	29.0	21.0	0.134	1.59	0.94	0.629	522.5	531.9	541.2	550.5	559.8	569.1	578.4
			1 0									The !	
0.5	. 05	25.0	0.000	9.69	0.00	1 000	F00.0	F00.1	F00.4	F 40 W	FF0.0	EC# 9	576.6
35	35	35.0 32.5	0.222	2.62	0.00	1.000 0.916	520.8 520.9	530.1 530.2	539.4 539.5	548.7 548.8	558.0 558.1	567.3 567.4	576.7
	33	30.0	0.186	2.19	0.43	0.836	521.0	530.2	539.6	548.9	558.3	567.5	576.8
4.9	32	27.5	0.170	2.00	0.62	0.764	521.1	530.4	539.7	549.0	558.4	567.6	576.9
	31	25.0	0.155	1.83	0.79	0.698	521.2	530.5	539.8	549.1	558.5	567.7	577.0
- 1	00	00.5	0.1.0	1.00	001	0.0	-	200.0	400.0	F 10.0	THO O	KOF 0	FWF 1
	30 29	22.5	0.142	1.68	0.94	0.641	521.3	530.6	539.9	549.2	558.6	567.8	577.1 577.2
	29	17.5	0.129	1.53	1.09	0.584	521.3 521.4	530.8	540.0 540.1	549.3 549.4	558.6 558.7	567.9 568.0	577.3
	27	15.0	0.108	1.27	1.35	0.485	521.5	530.9	540.2	549.5	558.7	568.1	577.4
Take I					3							86	1 14
1	9.0	00.0	0.0	1		1044	1					****	
36	36	36.0	0.230	2.71	0.00	1.000	519.7	529.0	538.3	547.5	556.8	566.1	575.4
	34	31.0	0.210	2.48	0.23	0.915	519.8 519.9	529.1 529.2	538.4	547.6	556.9 557.0	566.2 566.3	575.5 575.6
	33	28.5	0.132	2.07	0.64	0.764	520.0	529.3	538.5 538.6	547.8	557.1	566.4	575.7
100	32	26.0	0.161	1.89	0.82	0.698	520.1	529.4	538.7	547.9	557.2	566.5	575.8
	0.1	90 -							E A				
1100	31	23.5	0.147	1.74	0.97	0.642	520.2	529.5	538.8	548.0	557.3	566.6	575.9
	30 29	21.0	0.134	1.58	1.13	0.583	520.3	529.6	538.9	548.1	557.4	566.7 566.8	576.0 576.1
	28	16.0	0.112	1.45	1.39	0.535	520.4 520.5	529.7 529.8	539.0 539.1	548.2 548.3	557.5 557.6	566.9	576.2
			100	102	1.00	3.101	520.0	020.0	000.1	010.0	551.0	300.0	
	D												

	ading Ther-	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grain	as of a Cu	ibic Foot	of Air.	
mor	neter,	of Dew-	of Vapor	Ina	Reqd.	midity, Satura-		Height o	of the Bar	rometer i	n English	Inches.	
		Point, Fahr.	in English	Cubic Foot of		tion = 1.000.							-
Dry.	Wet.	175	Inches.	Air.	of Air.		28.0	28.5	29.0	29.5	30.0	30.5	31.
37	37	37.0	in. 0.238	gr. 2.80	gr. 0.00	1.000	gr. 518.6	gr. 527.8	gr. 537.1	gr. 546.3	gr. 555.6	gr. 564.8	gr. 574.
5	36	34.5	0.218	2.56	0.24	0.914	518.7	527.9	537.2	546.4	555.7	564.9	574.
4.85	35	32.0	0.199	2.35	0.45	0.839	518.8	528.0	537.3	546.5	555.8	565.0	574.
	34	29.5	0.182	2.14	0.66	0.764	518.9	528.1	537.4	546.6	555.9	565.1	574.
1	33	27.0	0.167	1.96	0.84	0.700	519.0	528.2	537.5	546.7	556.0	565.2	574.
-	32	24.5	0.152	1.79	1.01	0.640	519.1	528.3	537.6	546.8	556.1	565.3	574.
	31	22.0	0.139	1.64	1.16	0.586	519.2	528.4	537.7	546.9	556.2	565.4	574.
G.A	30 29	19.5	0.127	1.50	1.30	0.536	519.3	528.5	537.8	547.1	556.3	565.5	574. 574.
	29	17.0	0.116	1.37	1.43	0.489	519.4	528.6	537.9	547.2	556.4	565.6	574.
38	38	38.0	0.246	2.89	0.00	1.000	517.4	526.6	535.9	545.1	554.4	563.6	572.
	37	35.5	0.226	2.65	0.24	0.917	517.5	526.7	536.0	545.2	554.5	563.7	573.
	36	33.0	0.207	2.43	0.46	0.841	517.6	526.8	536.1	545.3	554.6	563.8	573.
	35	30.5	0.189	2.22	0.67	0.768	517.7	526.9	536.2	545.4	554.7	563.9	573.
AE .	34	28.0	0.173	2.03	0.86	0.703	517.8	527.0	536.3	545.5	554.8	564.0	573.
311	33	25.5	0.158	1.85	1.04	0.640	517.9	527.1	536.4	545.6	554.9	564.1	573.
Heis Heis	32	23.0	0.144	1.70	1.19	0.588	518.0	527.2	536.5	545.7	555.0	564.2	573.
	31	20.5	0.132	1.54	1.35	0.533	518.1	527.3	536.6	545.8	555.1	564.3	573.
	30	18.0	0.120	1.39	1.50	0.481	518.2	527.4	536.7	545.9	555.2	564.4	573.
39	39	39.0	0.255	2.99	0.00	1.000	516.3	525.5	534.7	543.9	553.2	562.4	571.
	38	36.5	0.234	2.74	0.25	0.917	516.4	525.6	534.8	544.0	553.3	562.5	571.
	37	34.0	0.214	2.51	0.48	0.840	516.5	525.7	534.9	544.1	553.4	562.6	571.
	36	31.5	0.196	2.30	0.69	0.769	516.6	525.8	535.0	544.2	553.5	562.7	571.
. 20	35	29.0	0.179	2.10	0.89	0.703	516.7	525.9	535.1	544.3	553.6	562.8	572.
	34	26.5	0.164	1.91	1.08	0.639	516.8	526.0	535.2	544.4	553.7	562.9	572.
	33	24.0	0.150	1.76	1.23	0.589	516.9	526.1	535.3	544.5	553.8	563.0	572.
	32	21.5	0.137	1.60	1.39	0.535	517.0	526.2	535.4	544.6	553.9	563.1	572.
	31	19.0	0.125	1.46	1.53	0.488	517.1	526.3	535.6	544.8	554.1	563.3	572.
	30	16.5	0.114	1.32	1.67	0.442	517.2	526.4	535.7	544.9	554.2	563.4	572.
40	40	40.0	0.264	3.09	0.00	1.000	515.2	524.4	533.6	542.8	552.0	561.2	570.
	39	37.8	0.245	2.86	0.23	0.926	515.3	524.5	533.7	542.9	552.1	561.3	570.
Vins	38	35.6	0.227	2.65	0.44	0.858	515.4	524.6	533.8	543.0	552.2	561.4	570.
Pito	37	33.4		1144-11 149-27	0.64	0.793	515.5		533.9	543.1	552.3	561.5	570.
12.7	36	31.2	0.194	2.27	0.82	0.734	515.6	524.8	534.0	543.2	552.4	561.6	570.
	35	29.0	0.179	2.09	1.00	0.676	515.7		534.1	543.3	552.5	561.7	570.
	34	26.8	0.165	1.94	1.15	0.628	515.8		10000	Sec. 15 / Gulby 3	552.6	561.8	571.
Va.	33 32	24.6	0.153	1.79 1.65	1.30	0.579	515.9 516.0	525.1 525.2	534.3	COLUMN TO A STATE OF THE PARTY	552.7	561.9	571.
	31	20.2	100 100 100 100	1.53	1.56	0.534	516.1	525.3	534.4 534.5	28 1000	552.8 552.9	562.0 562.1	571. 571.
	30	18.0	and the same	1.42	1.67	0.459	516.1	525.3	534.5	The Control of	553.0	562.2	571.
	ELS.		BUTES	D-UTS!	77-125	100	GNA	19 3	XI VA	\$ 1 MEST	0000	\$ 1 kd d	

Rea	ding	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grai	as of a Cu	ubic Foot	of Air.	
mon	neter,	of Dew-Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height	of the Ba	rometer i	n Englis	h Inches	02
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	in. 30.0	30.5	31.0
0	0	0	in.	gr.	gr.	<b>7</b> 000	gr.						
41	41	41.0	0.274	3.19 2.96	0.00	1.000 0.928	514.1 514.2	523.3 523.4	532.5 532.6	541.6 541.7	550.8 550.9	560.0	569.2 569.3
	40 39	38.8	0.235	2.74	0.45	0.859	514.2	523.5	532.7	541.7	551.0	560.2	569.4
	38	34.4	0.233	2.54	0.65	0.796	514.4	523.6	532.8	541.9	551.1	560.3	569.5
	37	32.2	0.201	2.35	0.84	0.737	514.5	523.7	532.9	542.0	551.2	560.4	569.6
	36	30.0	0.186	2.16	1.03	0.677	514.6	523.8	533.0	542.1	551.3	560.5	569.7
	100		2 1 1 1 1 1	5 00	45 E		CT - 174	Date D	13. 13	1 1833	44.63	\$00.00	CHASI!
	35	27.8	0.172	2.01	1.18	0.630	514.7 514.8	523.9	533.1 533.2	542.2 542.3	551.4	560.6 560.7	569.8 569.9
	34	25.6	0.158	1.85	1.48	0.536	514.9	524.0 524.1	533.3	542.4	551.5 551.6	560.8	570.0
	33 32	21.2	0.146	1.58	1.61	0.495	514.9	524.1	533.3	542.4	551.7	560.9	570.1
3.5	31	19.0	0.135	1.46	1.73	0.458	515.0	524.1	533.4	542.6	551.8	561.0	570.1
1	91	10.0	0.120	1.40		0.100	01010	027.2	00011	0.12.0	001.0	50110	0.0.2
42	42	42.0	0.283	3.30	0.00	1.000	513.0	522.2	531.3	540.5	549.6	558.8	567 9
	41	39.8	0.263	3.06	0.24	0.927	513.1	522.3	531.4	540.6	549.7	558.9	568.0
	40	37.6	0.243	2.83	0.47	0.858	513.2	522.4	531.5	540.7	549.9	559.0	568.1
	39	35.4	0.225	2.63	0.67	0.797	513.3	522.5	531.6	540.8	550.0	559.1	568.2
	38	33.2	0.208	2.43	0.87	0.736	513.4	522.6	531.7	540.9	550.1	559.2	568.3
	37	31.0	0.192	2.24	1.06	0.679	513.5	522.7	531.8	541.0	550.2	559.3	568.4
	36	28.8	0.178	2.08	1.22	0.631	513.6	522.8	531.9	541.1	550.3	559.4	568.5
	35	26.6	0.164	1.91	1.39	0.579	513.7	522.9	532.0	541.2	550.4	559.5	568.6
	34	24.4	0.152	1.77	1.53	0.536	513.8	523.0	532.1	541.3	550.5	559.6	568.7
	33	22.2	0.140	1.63	1.67	0.494	513.9	523.1	532.2	541.4	550.6	559.7	568.8
	32	20.0	0.129	1.51	1.79	0.458	513.9	523.1	532.3	541.5	550.6	559.8	569.0
43	40	40.0	0.000	0 (7	0.00	7 000	F11 0	F00.0	F00 1	F00 0	F 40 4		F00 F
45	43 42	43.0	0.293	3.41	0.00	1.000	511.8 511.9	520.9	530.1	539.3 539.4	548.4	557.5 557.7	566.7 566.9
1	41	38.6	0.272	3.16 2.93	0.25	0.859	512.0	521.0 521.1	530.2	539.4	548.7	557.8	567.0
	40	36.4	0.232	2.71	0.70	0.795	512.1	521.1	530.4	539.6	548.8	557.9	567.1
	39	34.2	0.216	2.51	0.90	0.736	512.2	521.3	530.5	539.7	548.9	558.0	567.2
	38	32.0	0.199	2.32	1.09	0.680	512.3	521.4	530.7	539.8	549.0	558.1	567.3
			79 1 Take	1 30	THE REAL PROPERTY.	A-4 F -	HAR N	DY by	TENT!			WILL TO	ALT VI
1473	37	29.8	0.184	2.15 1.98	1.26	0.630	512.4 512.5	521.5 521.6	530.8	539.9 540.0	549.1	558.2 558.3	567.4 567.5
1000	35	25.4	0.170	1.98	1.43 1.59	0.581	512.5	521.6	530.9 531.0	540.0	549.2	558.4	567.6
	34	23.2	0.157	1.69	1.72	0.554	512.7	521.7	531.1	540.1	549.4	558.5	567.7
	33	21.0	0.134	1.56	1.85	0.458	512.9	522.0	531.2	540.3	549.5	558.6	567.8
100	100	4.113	10 00			198	114 9	0.2	1	2.0.0	4 0.1	_ 101	100
44	44	44.0	0.304	3.52	0.00	1.000	510.8	519.9	529.0	538.1	547.3	556.4	565.5
	43	41.8	0.282	3.27	0.25	0.929	510.9	520.0	529.1	538.2	547.5	556.5	565.7
1	42	39.6	0.261	3.02	0.50	0.858	511.0	520.1	529.2	538.3	547.6	556.6	565.8
1 3	41	37.4	0.241	2.80	0.72	0.796	511.1	520.2	529.3	538.4	547.7	556.7	565.9
	40	35.2	0.223	2.60	0.92	0.739	511.2	520.3	529.4	538.5	547.8	556.8	566.0
	39	33.0	0.207	2.40	1.12	0.682	511.3	520.4	529.5	538.6	547.9	556.9	566.1
	38	30.8	0.191	2.22	1.30	0.631	511.4	520.5	529.6	538.7	548.0	557.0	566.2
1000	37	28.6	0.177	2.05	1.47	0.582	511.5	520.6	529.7	538.8	548.1	557.1	566.3
	36	26.4	0.163	1.89	1.63	0.537	511.6	520.7	529.8	538.9	548.2	557.2	566.4
	35	24.2	0.151	1.75	1.77	0.497	511.7	520.8	529.9	539.0	548.3	557.3	566.5
	34	22.0	0.139	1.62	1.90	0.460	511.7	520.8	530.0	539.1	548.3	557.4	566.6

of	ding Ther-	Temp.	Force of	of V	apor Read.	Hu-		Weigh	t in Grain	ns of a Ci	ubic Foot	t of Air.	
	neter, ahr.	of Dew-	Vapor	In a Cubic	for Sat'n.	midity, Satura-		Height	of the Ba	rometer i	in Englis	h Inches	103
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.		tion = 1.000.	28.0	28.5	29.0	29.5	30.0	in. 30.5	31.0
0	0	0	in.	gr.	gr.	7.000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
45	45	45.0	0.315	3.64	0.00	1.000	509.7	518.8	527.9	537.0	546.1	555.2	564.3
V 400	44	42.9	0.292	3.39	0.25	0.931	509.8	518.9	528.0	537.1	546.3	555.3	564.
	43 42	38.7	0.212	2.92	0.72	0.802	509.9 510.0	519.0 519.1	528.1 528.2	537.2 537.3	546.4 546.5	555.5	564.
1	41	36.6	0.235	2.70	0.12	0.742	510.1	519.2	528.3	537.4	546.6	555.6	564.
. 50	40	34.5	0.218	2.52	1.12	0.692	510.2	519.3	528.4	537.5	546.7	555.7	564.
	39	32.4	0.202	2.34	1.30	0.643	10 TO	519.4	528.5	537.6	546.8	555.8	
	38	30.3	0.202	2.16	1.48	0.593	510.3 510.4	519.4	528.6	537.7	546.9	555.9	565. 565.
	37	28.2	0.174	2.01	1.63	0.552	510.4	519.6	528.7	537.8	547.0	556.0	565.
1	36	26.1	0.161	1.87	1.77	0.514	510.6	519.7	528.8	537.9	547.1	556.1	565.
6.19	35	24.0	0.150	1.73	1.91	0.475	510.7	519.8	528.9	538.0	547.2	556.3	565.
9,04					1	0.110	010	010.0	020.0	000.0	01112	000.0	000.
46	46	46.0	0.326	3.76	0.00	1.000	508.6	517.7	526.7	535.8	544.9	554.0	563.
	45	43.9	0.303	3.50	0.26	0.931	508.7	517.8	526.8	535.9	545.0	554.1	563.
183	44	41.8	0.282	3.25	0.51	0.864	508.8	517.9	526.9	536.0	545.1	554.2	563.
hair	43	39.7	0.262	3.02	0.74	0.803	508.9	518.0	527.0	536.1	545.2	554.3	563.
120	42	37.6	0.243	2.80	0.96	0.745	509.0	518.1	527.2	536.3	545.4	554.5	563.
9,181	41	35.5	0.226	2.61	1.15	0.694	509.1	518.2	527.3	536.4	545.5	554.6	563.
62	40	33.4	0.210	2.42	1.34	0.643	509.2	518.3	527.4	536.5	545.6	554.7	563.
	39	31.3	0.194	2.24	1.52	0.596	509.3	518.4	527.5	536.6	545.7	554.8	563.
	38	29.2	0.180	2.08	1.68	0.553	509.4	518.5	527.6	536.7	545.8	554.9	564.
	37	27.1	0.167	1.93	1.83	0.514	509.5	518.6	527.7	536.8	545.9	555.0	564.
	36	25.0	0.155	1.79	1.97	0.476	509.5	518.6	527.7	536.8	545.9	555.0	564.
47	47	47.0	0.337	3.88	0.00	1.000	507.5	516.5	525.6	534.7	543.8	552.8	561.9
1	46	44.9	0.313	3.62	0.26	0.933	507.6	516.6	525.7	534.8	543.9	552.9	562.0
1	45	42.8	0.291	3.36	0.52	0.866	507.8	516.7	525.9	535.0	544.1	553.1	562.2
May	44	40.7	0.271	3.12	0.76	0.804	507.9	516.8	526.0	535.1	544.2	553.2	562.
	43	38.6	0.252	2.90	0.98	0.747	508.0	516.9	526.1	535.2	544.3	553.3	562.4
4,1	42	36.5	0.234	2.70	1.18	0.696	508.1	517.0	526.2	535.3	544.4	553.4	562.5
	41	34.4	0.217	2.51	1.37	0.647	508.2	517.1	526.3	535.4	544.5	553.5	562.6
ETV	40	32.3	0.201	2.32	1.56	0.598	508.3	517.2	526.4	535.5	544.6	553.6	562.7
7.15	39	30.2	0.187	2.16	1.72	0.557	508.4	517.3	526.5	535.6	544.7	553.7	562.8
	38	28.1	0.173	2.00	1.88	0.515	508.5	517.4	526.6	535.7	544.8	553.8	562.9
	37	26.0	0.161	1.85	2.03	0.477	508.5	517.6	526.7	535.8	544.9	554.0	563.1
48	48	48.0	0.349	4.01	0.00	1.000	506.4	515.4	524.5	533.5	542.6	551 6	560.7
40	47	45.9	0.324	3.73	0.00	0.930	506.5		524.6	533.7	542.8	551.6 551.8	560.9
130	46	43.8	0.302	3.47	0.28	0.865	506.6	515.5 515.6	524.7	533.8	542.9	551.9	561.0
142	45	41.7	0.302	3.23	0.78	0.805	506.7	515.7	524.8	533.9	543.0	552.0	561.1
6,19	44	39.6	0.261	3.00	1.01	0.748	506.8	515.8	524.9	534.0	543.1	552.1	561.2
1	43	37.5	0.242	2.79	1.22	0.696	506.9	515.9	525.0	534.1	543.2	552.2	561.3
0.00	42	35.4	0.225	2.60	1.41	0.648	507.0	516.0	525.1	- 174 800	543.3	177	
1	41	33.3	0.225	2.40	1.61	0.598	507.1	516.1	525.2	534.2 534.4	543.5	552.3 552.5	561.4
949	40	31.2	0.194	2.24	1.77	0.558	507.2	516.2	525.3	534.5	543.5	552.5	561.6
244	39	29.1	0.180	2.07	1.94	0.516	507.3	516.3	525.4	534.6	543.6	552.6	561.6
1	38	27.0	0.167	1.92	2.09	0.479	507.4	516.4	525.5	534.7	543.6	552.7	561.7
	37	24.9	0.155	1.77	2.24	0.441			525.6	534.7		552.8	901.1

	leading		7		ight apor			Weigh	t in Grai	ns of a Cu	ıbic Foot	of Air.	
	f Ther- ometer, Fahr.	Temp. of Dew-	Force of Vapor in	In a	Reqd. for Sat'n.	Hu- midity, Satura- tion ==		Height o	of the Bar	rometer i	n English	Inches.	7 - 1 7 - 1 7 - 1
Dry	Wet.	Point, Fahr.	English Inches.	Foot of Air.		1.000.	in. 28.0	in. 28.5	in. 29.0	29.5	30.0	in. 30.5	in. 31.0
		0	in.	gr.	gr.	1 000	gr.						
49	49	49.0	0.361	4.14 3.85	0.00	1.000 0.930	505.3 505.4	514.3 514.4	523.3 523.4	532.3 532.4	541.4 541.5	550.4 550.5	559.4 559.5
	47	46.9	0.312	3.59	0.55	0.867	505.6	514.6	523.6	532.6	541.7	550.7	559.7
	46	42.7	0.290	3.34	0.80	0.807	505.7	514.7	523.7	532.7	541.8	550.8	559.8
	45	40.6	0.270	3.10	1.04	0.749	505.9	514.9	523.8	532.9	542.0	551.0	560.0
	44	38.5	0.251	2.88	1.26	0.696	506.0	515.0	523.9	533.0	542.1	551.1	560.1
	43	36.4	0.233	2.68	1.46	0.647	506.1	515.1	524.0	533.1	542.2	551.2	560.2
	42	34.3	0.216	2.49	1.65	0.601	506.2	515.2	524.1	533.2	542.3	551.3	560.3
	41	32.2	0.201	2.32	1.82	0.560	506.3	515.3	524.2	533.3	542.4	551.4	560.4
	40	30.1	0.186	2.14	2.00	0.517	506.3	515.3	524.3	533.4	542.5	551.5	560.5
	39	28.0	0.173	1.99	2.15	0.481	506.4	515.4	524.4	533.5	542.6	551.6	560.6
	38	25.9	0.160	1.84	2.30	0.444	506.4	515.4	524.4	533.5	542.6	551.6	560.6
50		50.0	0.373	4.28	0.00	1.000	504.1	513.1	522.1	531.1	540.2	549.2	558.2
	49	48.0	0.349	3.99	0.29	0.932	504.2	513.2	522.2	531.2	540.3	549.3	558.3
	48	46.0	0.326	3.73	0.55	0.871	504.4	513.4	522.4	531.4	540.5	549.5	558.5
	47	44.0	0.304	3.48	0.80	0.813	504.5	513.5	522.5	531.5	540.6	549.6 549.7	558.6
	46 45	42.0	0.283	3.25	1.03	0.759	504.6	513.6 513.8	522.6	531.6 531.8	540.7 540.9	549.7	558.7 558.9
	45	38.0	0.246	2.82	1.46	0.659	504.8 504.9	513.9	522.8 522.9	532.0	541.0	550.0	559.0
	43	36.0	0.230	2.63	1.65	0.614	505.1	514.1	523.1	532.1	541.2	550.2	559.2
	42	34.0	0.214	2.45	1.83	0.572	505.2	514.2	523.2	532.2	541.3	550.3	559.3
	41	32.0	0.199	2.28	2.00	0.533	505.3	514.3	523.3	532.3	541.4	550.4	559.4
	40	30.0	0.186	2.12	2.16	0.495	505.4	514.4	523.4	532.4	541.5	550.5	559.5
	39	28.0	0.173	1.97	2.31	0.460	505.5	514.5	523.5	532.5	541.6	550.6	559.6
51	51	51.0	0.386	4.42	0.00	1.000	503.1	512.1	521.1	530.0	539.0	548.0	557.0
	50	49.0	0.361	4.12	0.30	0.932	503.2	512.2	521.2	530.1	539.1	548.1	557.1
	49	47.0	0.337	3.85	0.57	0.871	503.3	512.3	521.3	530.3	539.3	548.3	557.3
	48	45.0	0.315	3.60	0.82	0.814	503.4	512.4	521.4	530.4	539.4	548.4	557.4
	47	43.0	0.293	3.36	1.06	0.760	503.5	512.5	521.5	530.5	539.5	548.5	557.5
	46	41.0	0.274	3.13	1.29	0.708	503.7	512.7	521.7	530.7	539.7	548.7	557.7
	45	39.0	0.255	2.92	1.50	0.661	503.8	512.8	521.8	530.8	539.8	548.8	557.8
	44	37.0	0.238	2.72	1.70	0.615	503.9	512.9	521.9	530.9	539.9	548.9	557.9
	43	35.0	0.222	2.54	1.88	0.575	504.0	513.0	522.0	531.0	540.0	549.0	558.0
	42	33.0	0.207	2.36	2.06	0.534	504.1	513.1	522.1	531.1	540.1	549.1	558.1
	41 40	31.0	0.192	2.20	2.22	0.498	504.2	513.2	522.2	531.2	540.3	549.3 549.4	558.3 558.4
55		52.0	0.179	2.05	0.00	1.000	504.3 502.1	513.3 511.0	522.3 520.0	531.3 528.9	540.4	546.8	555.8
	51	50.0	0.400	4.26	0.00	0.934	502.1	511.1	520.0	529.0	538.0	546.9	555.9
	50	48.0	0.349	3.98	0.58	0.873	502.4	511.3	520.3	529.2	538.2	547.1	556.1
	49	46.0	0.326	3.72	0.84	0.816	502.5	511.4	520.4	529.3	538.3	547.2	556.2
	48	44.0	0.304	3.47	1.09	0.761	502.6	511.5	520.5	529.4	538.4	547.3	556.3
	47	42.0	1	3.23	1.33	0.709	502.8	511.7	520.7	529.6	538.6	547.5	556.5
	46	40.0	0.264	3.02	1.54	0.662	502.9	511.8	520.8	529.7	538.7	547.6	556.6
	45	38.0	0.246	2.81	1.75	0.616	502.9	511.9	520.9	529.8	538.8	547.8	556.8
	44	36.0	0.230	2.63	1.93	0.577	503.1	512.0	521.0	529.9	539.0	548.0	557.0
	43	34.0	0.214	2.44	2.12	0.535	503.2	512.1	521.1	530.0	539.1	548.1	557.1
	42	32.0	0.199	2.28	2.28	0.500	503.3	512.3	521.3	530.2	539.2	548.2	557.2
	41	30.0	0.186	2.13	2.43	0.467	503.4	512.4	521.4	530.3	539.3	548.3	557.3

	ding	Temp.	Force		ight apor	Hu-		Weigh	t in Graiı	ns of a Cu	abic Foot	of Air.	
mor	neter, ahr.	of Dew-Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height	of the Ba	rometer i	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr. 509.8	gr.	gr. 527.7	gr. 536.7	gr. 545.6	gr. 554.6
53	53 52	53.0	0.414	4.71	0.00	1.000	500.9	510.0	518.8 519.0	527.9	536.9	545.8	554.8
5.50	51	49.0	0.361	4.11	0.60	0.873	501.2	510.1	519.1	528.0	537.0	545.9	554.9
1.63	50	47.0	0.337	3.84	0.87	0.815	501.4	510.3	519.3	528.2	537.2	546.1	555.1
6.53	49	45.0	0.315	3.58	1.13	0.760	501.5	510.4	519.4	528.3	537.3	546.2	555.2
V.14	48	43.0	0.293	3.34	1.37	0.709	501.6	510.5	519.5	528.4	537.4	546.3	555.9
	47	41.0	0.274	3.12	1.59	0.662	501.7	510.6	519.6	528.5	537.5	546.4	555.4
0.00	46	39.0	0.255	2.91	1.80	0.618	501.8	510.7	519.7	528.6	537.6	546.5	555.8
9.20	45	37.0	0.238	2.71	2.00	0.575	502.0	510.9	519.9	528.8	537.8	546.7	555.7
7	44	35.0	0.222	2.53	2.18	0.537	502.1	511.0	520.0	528.9	537.9	546.8	555.8
H. C.	43	33.0	0.207	2.35	2.36	0.499	502.1	511.0	520.0	528.9	538.0	546.9	555.9
T EV	42	31.0	0.192	2.18	2.53	0.463	502.2	511.1	520.1	529.0	538.1	547.0	556.0
			0 400		0.00	7 000	400.0	F00.0		F00 =			FF0 .
54	54	54.0	0.428	4.86	0.00	1.000	499.9	508.8	517.8	526.7	535.6	544.5	553.5
10.43	53	52.0	0.400	4.54	0.32	0.934	500.0	508.9	517.9	526.8	535.7	544.6	553.6 553.8
7.00	52	50.0	0.373	3.96	0.61	0.875	500.2	509.1	518.1	527.0	535.9	544.8 544.9	553.9
20	51	48.0	0.349	3.70	1.16	0.815	500.3	509.2 509.3	518.2 518.3	527.1 527.2	536.0 536.1	545.0	554.0
9.70	50	GRADA		72 17.	MELES	MAN B.	10th 1:37	20030	723.40		. TALLET	7	
9 ze	49	44.0	0.304	3.45	1.41	0.709	500.6	509.5	518.5	527.4	536.3	545.2	554.2
19 54	48	42.0	0.283	3.23	1.63	0.665	500.7	509.6	518.6	527.5	536.4	545.3	554.3
6.79	47	40.0	0.264	3.01	1.85	0.619	500.8	509.7	518.7	527.6	536.5	545.4	554.4
B-01	46	38.0	0.246	2.80	2.06	0.576	500.9	509.8	518.8	527.7 527.8	536.7 536.8	545.6 545.7	554.7
1800	45	300 100	The Party of	2.61	2.25	0.537	501.0	509.9	518.9		A STATE OF		19 198
3-10	44	34.0	0.214	2.43	2.43	0.500	501.1	510.0	519.0	527.9	536.9	545.8	554.8
B. I'	43	32.0	0.199	2.27	2.59	0.467	501.2	510.1	519.1	528.0	537.0	545.9	554.9
27:17	42	30.0	0.186	2.10	2.76	0.432	501.3	510.2	519.2	528.1	537.1	546.0	555.1 555.1
	41 40	28.0	0.173	1.96	3.04	0.403	501.4	510.3 510.4	519.3 519.4	528.2 528.3	537.2 537.3	546.1 546.2	555.2
-	40	20.0	0.101	1.82	3.04	0.375	501.5	310.4	919.4	340.0	201.0	040.2	00012
55	55	55.0	0.442	5.02	0.00	1.000	498.8	507.7	516.6	525.5	534.4	543.3	552.2
1	54	53.3	0.418	4.74	0.28	0.944	499.0	507.9	516.8	525.7	534.6	543.5	552.4
0914	53	51.6	0.394	4.46	0.56	0.888	499.1	508.0	516.9	525.8	534.7	543.6	552.5
1	52	49.9	0.372	4.23	0.79	0.843	499.3	508.2	517.1	526.0	534.9	543.8	552.7
141	51	48.2	0.351	3.98	1.04	0.793	499.4	508.3	517.2	526.1	535.0	543.9	552.8
101	50	46.5	0.331	3.76	1.26	0.749	499.5	508.4	517.3	526.2	535.1	544.0	552.9
1-1	49	44.8	0.312	3.55	1.47	0.707	499.7	508.6	517.5	526.3	535.3	544.2	553.1
1000	48	43.1	0.295	3.34	1.68	0.665	499.8	508.7	517.6	526.5	535.4	544.3	553.3
947	47	41.4	0.278	3.14	1.88	0.626	499.8	508.7	517.6	526.6	535.5	544.4	553.4
	46	39.7	0.262	2.97	2.05	0.591	499.9	508.8	517.7	526.7	535.6	544-5	553.5
	45	38.0	0.246	2.79	2.23	0.556	500.0	508.9	517.9	526.8	535.7	544.6	553.6
17.7.	44	36.3	0.232	2.64	2.38	0.526	500.1	509.0	518.0	526.9	535.8	544.7	553.7
40	43	34.6	0.219	2.47	2.55	0.492	500.2	509.1	518.1	527.0	535.9	544.8	553.8
	42	32.9	0.206	2.32	2.70	0.462	500.3	509.2	518.2	527.1	536.0	544.9	553.9
	41	31.2	0.194	2.20	2.82	0.438	500.4	509.3	518.3	527.1	536.0	544.9	554.0
BEE	40	29.5	0.182	2.07	2.95	0.412	500.5	509.3	518.4	527.2	536.1	545.0	554.1
	39	27.8	0.172	1.95	3.07	0.388	500.6	509.4	518.5	527.3	536.2	545.1	554.2
US	38	26.1	0.161	1.83	3.19	0.365	500.7	509.5	518.6	527.4	536.2	545.1	554.2

Dry. Wet.  0 0 56 56 55 54 53 52 51    50 49 48 47 46 45 41 44 43 42 41 40 39 55 55 54 55 54 53 8 6 55 54 53 8 6 55 55 54 55 8 55 55 55 55 55 55 55 55 55 55 55 5	of Dew-Point, Fahr.  56.0 54.3 52.6 50.9 49.2 47.5 45.8 44.1 42.4 40.7 39.0 37.3	of Vapor in English Inches.  in. 0.458 0.432 0.408 0.385 0.363 0.343 0.323 0.305	In a Cubic Foot of Air.  gr. 5.18 4.89 4.61 4.37 4.11 3.87	Reqd. for Sat'n. of a Cubic Ft. of Air. gr. 0.00 0.29 0.57 0.81 1.07 1.31	midity, Satura- tion = 1.000. 1.000 0.944 0.890 0.844	gr. 497.7 497.9	28.5 gr. 506.6	in. 29.0 gr. 515.5	29.5 gr. 524.4	in. 30.0 gr. 533.2	in. 30.5 gr.	in. 31.0
Dry. Wet.    0   0   0   0	56.0 54.3 52.6 50.9 49.2 47.5 45.8 44.1 42.4 40.7 39.0	in. 0.458 0.432 0.408 0.385 0.363 0.343 0.323 0.305	gr. 5.18 4.89 4.61 4.37 4.11 3.87	bic Ft. of Air. 	1.000 0.944 0.890	gr. 497.7 497.9	28.5 gr. 506.6	29.0 gr.	29.5 gr.	30.0 gr.	30.5	31.0
56 56 55 54 53 52 51 50 49 48 47 46 45 41 40 39 57 57 56 55 54 53 8	56.0 54.3 52.6 50.9 49.2 47.5 45.8 44.1 42.4 40.7 39.0	0.458 0.432 0.408 0.385 0.363 0.343 0.323 0.305	5.18 4.89 4.61 4.37 4.11 3.87	0.00 0.29 0.57 0.81 1.07	0.944 0.890	497.7 497.9	506.6	CONTRACTOR AND ADDRESS OF THE PARTY OF THE P	Contract Con	The state of the s	gr.	ore
55 54 53 52 51 50 49 48 47 46 45 41 43 42 41 40 39 57 56 55 54 53 54 53 54 55 54 55 56 56 56 57 56 56 56 56 56 56 56 56 56 56	54.3 52.6 50.9 49.2 47.5 45.8 44.1 42.4 40.7 39.0	0.432 0.408 0.385 0.363 0.343 0.323 0.305	4.89 4.61 4.37 4.11 3.87	0.29 0.57 0.81 1.07	0.944 0.890	497.9		010.0			542.1	551.0
54 53 52 51 50 49 48 47 46 45 44 43 44 41 40 39 57 57 56 55 54 53	52.6 50.9 49.2 47.5 45.8 44.1 42.4 40.7 39.0	0.408 0.385 0.363 0.343 0.323 0.305	4.61 4.37 4.11 3.87	0.57 0.81 1.07	0.890		506.8	515.7	524.6	533.4	542.3	551.2
52 51 50 49 48 47 46 45 41 43 42 41 40 39 57 57 56 55 54 53	49.2 47.5 45.8 44.1 42.4 40.7 39.0	0.363 0.343 0.323 0.305	4.11 3.87	1.07	0 844	498.0	506.9	515.8	524.7	533.5	542.4	551.3
51 50 49 48 47 46 45 44 43 42 41 40 39 57 56 55 54 53	47.5 45.8 44.1 42.4 40.7 39.0	0.343 0.323 0.305	3.87		0.044	498.2	507.1	516.0	524.9	533.7	542.6	551.5
50 49 48 47 46 45 41 43 42 41 40 39 57 57 56 55 54 53	45.8 44.1 42.4 40.7 39.0	0.323 0.305		1 27	0.793	498.3	507.2	516.1	525.0	533.8	542.7	551.6
49 48 47 46 45 41 43 42 41 40 39 57 57 56 55 54 53	44.1 42.4 40.7 39.0	0.305	9.00	1.01	0.747	498.4	507.3	516.2	525.1	533.9	542.8	551.7
48 47 46 45 41 43 42 41 40 39 57 57 56 55 54 53	42.4 40.7 39.0		3.66	1.52	0.706	498.6	507.5	516.4	525.3	534.1	543.0	551.9
47 46 45 41 43 42 41 40 39 57 57 56 55 54 53	40.7 39.0		3.45	1.73	0.666	498.6	507.5	516.4	525.3	534.2	543.1	552.0
46 45 44 43 42 41 40 39 57 57 56 55 54 53 8	39.0	0.287	3.25	1.93	0.627	498.7	507.6	516.5	525.4	534.3	543.2	552.1
45 44 43 42 41 40 39 57 57 56 55 54 53 6		0.271	3.07	2.11	0.593	498.8	507.7	516.6	525.5	534.4	543.3	552.2
44 43 42 41 40 39 57 57 56 55 54 53	37.3	0.255	2.89	2.29	0.558	498.9	507.8	516.7	525.6	534.5	543.4	552.3
43 42 41 40 39 57 57 56 55 54 53 6		0.240	2.73	2.45	0.527	499.0	507.9	516.8	525.7	534.6	543.5	552.4
42 41 40 39 57 57 56 55 54 53	35.6	0.227	2.56	2.62	0.494	499.1	508.0	516.9	525.8	534.7	543.6	552.5
41 40 39 57 57 56 55 54 53 6	33.9	0.213	2.41	2.77	0.465	499.2	508.1	517.0	525.9	534.8	543.7	552.6
57 57 56 55 54 53 6	32.2	0.201	2.27	2.91	0.438	499.3	508.2	517.1	526.0	534.9	543.8	552.7
57 57 56 55 54 53 53	30.5	0.189	2.14	3.04	0.413	499.4	508.3	517.2	526.1	535.0	543.9	552.8
57 57 56 55 54 53 53 53	28.8	0.178	2.01	3.17	0.388	499.5	508.4	517.3	526.2	535.1	544.1	552.9
56 55 54 53	27.1	0.167	1.89	3.29	0.365	499.5	508.4	517.3	526.2	535.1	544.1	552.9
56 55 54 53		J. 183						200		F (-)		
55 54 53	57.0	0.473	5.34	0.00	1.000	496.6	505.5	514.4	523.2	532.1	540.9	549.8
54 53	55.3	0.447	5.05	0.29	0.946	496.8	505.7	514.6	523.4	532.3	541.1	550.0
53	53.6	0.422	4.76	0.58	0.891	496.9	505.8	514.7	523.5	532.4	541.2	550.1
	51.9	0.398	4.50	0.84	0.843	497.1	506.0	514.9	523.7	532.6	541.4	550.3
52	50.2	0.376	4.25	1.09	0.796	497.2	506.1	515.0	523.8	532.7	541.5	550.4
	48.5	0.355	4.00	1.34	0.749	497.3	506.2	515.1	523.9	532.8	541.6	550.5
51	46.8	0.335	3.78	1.56	0.709	497.5	506.4	515.3	524.1	533.0	541.8	550.7
	45.1	0.316	3.56	1.78	0.667	497.6	506.5	515.4	524.2	533.1	541.9	550.8
49	43.4	0.298	3.36	1.98	0.629	497.7	506.6	515.5	524.3	533.2	542.0	550.9
	41.7	0.281	3.17	2.17	0.594	497.8	506.7	515.6	524.4	533.3	542.1	551.0
11 1 11	40.0	0.264	2.99	2.35	0.560	497.9	506.8	515.7	524.5	533.4	542.2	551.2
46	38.3	0.249	2.81	2.53	0.526	498.0	506.9	515.8	524.6	533.5	542.3	551.3
45	36.6	0.235	2.65	2.69	0.496	498.1	507.0	515.9	524.7	533.6	542.4	551.4
	34.9	0.221	2.50	2.84	0.468	498.2	507.1	516.0	524.8	533.7	542.5	551.5
	33.2	0.208	2.35	2.99	0.440	498.3	507.2	516.1	524.9	533.8	542.6	551.6
	31.5	0.196	2.21	3.13	0.414	498.3	507.2	516.1	524.9	533.8	542.6	551.6
11 11	29.8	0.184	2.08	3.26	0.390	498.4	507.3	516.2	525.1	533.9	542.7	551.7
40	28.1	0.173	1.96	3.38	0.367	498.5	507.4	516.3	525.2	534.0	542.8	551.8
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				+			100					
		Ball Ball										
	CONT.								TO LET			-

of	ading Ther- meter,	Temp.	Force of		apor Reqd.	Hu- midity,		Weigh	t in Grain	ns of a Cu	ibic Foot	of Air.	h will
	ahr.	Dew- Point,	Vapor in	In a Cubic	for Sat'n.	Satura- tion =	ar Halel	Height o	of the Bar	rometer in	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	in. 30.0	in. 30.5	in. 31.0
o 58	o 58	58.0	in. 0.489	gr. 5.51	gr. 0.00	1.000	gr. 495.5	gr. 504.3	gr. 513.2	gr. 522.0	gr. 530.9	gr. 539.7	gr. 548.6
•00	57	56.3	0.462	5.21	0.30	0.946	495.7	504.5	513.4	522.2	531.1	539.9	548.
	56	54.6	0.437	4.92	0.59	0.893	495.8	504.6	513.5	522.3	531.2	540.0	548.
	55	52.9	0.412	4.64	0.87	0.842	496.0	504.8	513.7	522.5	531.4	540.2	549.
	54	51.2	0.389	4.39	1.12	0.797	496.1	504.9	513.8	522.7	531.6	540.4	549.
	53	49.5	0.367	4.14	1.37	0.751	496.2	505.0	513.9	522.8	531.7	540.5	549.
	52	47.8	0.346	3.90	1.61	0.708	496.4	505.2	514.1	523.0	531.9	540.7	549.
	51	46.1	0.327	3.68	1.83	0.668	496.5	505.2	514.2	523.1	532.0	540.8	549
	50	44.4	0.308	3.48	2.03	0.632	496.6	505.4	514.3	523.2	532.1	540.9	549.
	49	42.7	0.290	3.28	2.23	0.595	496.7	505.5	514.4	523.3	532.2	541.0	549.
	48	41.0	0.274	3.08	2.43	0.559	496.8	505.6	514.5	523.4	532.3	541.1	550.
KE	47	39.3	0.258	2.91	2.60	0.528	496.9	505.7	514.6	523.5	532.4	541.2	550.
	46	37.6	0.243	2.74	2.77	0.497	497.0	505.8	514.7	523.6	532.5	541.3	550
	45	35.9	0.229	2.58	2.93	0.469	497.1	505.9	514.8	523.7	532.6	541.4	550
	44	34.2	0.216	2.43	3.08	0.441	497.2	506.0	514.9	523.8	532.7	541.5	550
	43	32.5	0.203	2.29	3.22	0.416	497.3	506.1	515.1	523.9	532.8	541.6	550
	42	30.8	0.191	2.15	3.36	0.390	497.4	506.2	515.2	524.1	532.9	541.7	550
	41	29.1	0.180	2.03	3.48	0.368	497.5	506.3	515.3	524.2	533.0	541.8	550
	40	27.4	0.169	1.91	3.60	0.347	497.5	506.3	515.3	524.2	533.0	541.8	550
	a lang	1 100	en 1996	10 18.	70.12	tio a.	NEW YORK	100 X	att res	FIYE	0 151	17 34	
59	59	59.0	0.506	5.69	0.00	1.000	494.5	503.3	512.2	521.0	529.8	538.6	547.
	58	57.3	0.478	5.37	0.32	0.944	494.6	503.4	512.3	521.1	529.9	538.7	547
	57	55.6	0.452	5.08	0.61	0.893	494.7	503.5	512.4	521.2	530.0	538.8	547
	56	53.9	0.426	4.79	0.90	0.842	494.8	503.6	512.5	521.3	530.1	538.9	547
	55 54	52.2	0.402	4.53	1.16	0.796	494.9	503.7 503.9	512.6 512.8	521.4 521.6	530.3 530.5	539.1 539.3	548. 548.
	34	30.3	0.500	4.20	1.41	0.152	495.1	303.9	312.8	521.0	330.3	000.0	040
	53	48.8	0.358	4.03	1.66	0.708	495.3	504.1	513.0	521.8	530.7	539.5	548.
	52	47.1	0.338	3.80	1.89	0.668	495.4	504.2	513.1	521.9	530.8	539.6	548.
	51	45.4	0.319	3.60	2.09	0.633	495.5	504.3	513.2	522.0	530.9	539.7	548.
	50	43.7	0.301	3.39	2.30	0.596	495.7	504.5	513.4	522.2 522.3	531.1 531.2	539.9	548. 548.
	49	42.0	0.283	3.19	2.50	0.561	495.8 495.9	504.6 504.7	513.4 513.5	522.4	531.3	540.0	549
	47	38.6	0.252	2.84	2.85	0.499	496.0	504.8	513.6	522.5	531.4	540.2	549.
	46	36.9	0.237	2.67	3.02	0.469	496.1	504.9	513.7	522.6	531.5	540.3	549.
	45	35.2	0.223	2.51	3.18	0.441	496.2	505.0	513.8	522.7	531.6	540.4	549.
	44	33.5	0.210	2.37	3.32	0.417	496.3	505.1	513.9	522.8	531.7	540.5	549.
	43	31.8	0.198	2.23	3.46	0.392	496.4	505.2	514.1	522.9	531.8	540.6	549.
	42	30.1	0.186	2.09	3.60	0.367	496.5	505.3	514.2	523.0	531.9	540.7	549.
	41	28.4	0.175	1.97	3.72	0.346	496.6	505.4	514.3	523.1	532.0	540.8	549.
	40	26.7	0.165	1.85	3.84	0.325	496.6	505.4	514.3	523.1	532.0	540.8	549.
	11/20			1000		SELE	100	5,512.	lina de	et e	10100	i di si	
	13.2.0	I II		1048	Tunia.	EQUITOR .	Lead in	1000	10	LIVE TO	Ballan.	010 31	116

	ading Ther-	Temp.	Force		ight Vapor	Hu-		Weigh	t in Grai	ns of a C	ıbic Foot	of Air.	
mon	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height	of the Ba	rometer	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.		1.000.	2.8.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr. 502.2	gr.	gr.	gr.	gr.	gr.
60	60 59	60.0	0.523	5.87	0.00	1.000	493.4	502.4	511.0 511.2	519.8 520.0	528.6 528.8	537.4	546.2 546.4
	58	56.6	0.467	5.24	0.63	0.893	493.7	502.5	511.3	520.1	528.9	537.7	546.5
200	57	54.9	0.441	4.95	0.92	0.843	493.8	502.6	511.4	520.2	529.0	537.8	546.6
	56	53.2	0.416	4.68	1.19	0.797	494.0	502.8	511.6	520.4	529.2	538.0	546.8
	55	51.5	0.393	4.41	1.46	0.751	494.2	503.0	511.8	520.6	529.4	538.2	547.0
RH	54	49.8	0.371	4.17	1.70	0.710	494.4	503.2	512.0	520.8	529.6	538.4	547.2
	53	48.1	0.350	3.92	1.95	0.668	494.5	503.3	512.1	520.9	529.7	538.5	547.4
71	52	46.4	0.330	3.70	2.17	0.630	494.7	503.4	512.3	521.1	529.9	538.7	547.6
	51	44.7	0.311	3.49	2.38	0.595	494.8	503.5	512.4	521.2	530.0	538.8	547.7
	50	43.0	0.293	3.29	2.58	0.561	494.8	503.6	512.5	521.3	530.1	538.9	547.8
1120	49	41.3	0.277	3.10	2.77	0.528	494.9	503.7	512.6	521.4	530.2	539.0	547.9
M. S	48	39.6	0.261	2.93	2.94	0.499	495.0	503.8	512.7	521.5	530.3	539.1	548.0
	47	37.9	0.246	2.75	3.12	0.468	495.1	503.9	512.8	521.6	530.4	539.2	548.1
	46	36.2	0.231	2.60	3.27	0.443	495.2	504.0	512.9	521.7	530.5	539.3	548.2
Suin	45	34.5	0.218	2.45	3.42	0.417	495.3	504.1	513.0	521.8	530.6	539.4	548.3
	44	32.8	0.205	2.31	3.56	0.394	495.4	504.2	513.1	521.9	530.7	539.5	548.4
	43	31.1	0.193	2.17	3.70	0.370	495.5	504.3	513.2	522.0	530.8	539.6	548.5
	42	29.4	0.182	2.04	3.83	0.348	495.6	504.4	513.3	522.1	530.9	539.7	548.6
15	41	27.7	0.171	1.92	3.95	0.327	495.6	504.4	513.3	522.1	530.9	539.7	548.7
		dist		E 18		00.0		ad B	19 1 1		1 30		
61	61	61.0	0.541	6.06	0.00	1.000	492.3	501.1	509.9	518.7	527.5	536.3	545.1
-	60	59.3	0.511	5.72	0.34	0.944	492.5	501.3	510.1	518.9	527.7	536.5	545.3
	59	57.6	0.483	5.40	0.66	0.891	492.6	501.4	510.2	519.0	527.8	536.6	545.4
	58 57	55.9 54.2	0.456	5.11	0.95	0.843	492.8	501.6 501.8	510.4 510.6	519.2 519.4	528.0 528.2	536.8 537.0	545.6 545.8
3,4	0.	04.2	0.401	4.00	1.20	0.131	499.0	301.0	510.0	515.4	040.4	337.0	343.0
Second	56	52.5	0.407	4.55	1.51	0.751	493.1	501.9	510.7	519.5	528.3	537.1	545.9
344	55	50.8	0.383	4.30	1.76	0.710	493.3	502.1	510.9	519.7	528.5	537.3	546.1
3,11	54	49.1	0.362	4.05	2.01	0.668	493.4	502.2	511.0	519.8	528.6	537.4	546.2
	53 52	47.4	0.342	3.83	2.23	0.632	493.5	502.3 502.4	511.1 511.2	519.9 520.0	528.7 528.8	537.5 537.6	546.3 546.4
	i de				10-13	enselp.	100.0	302.4	311.2	323.0		30110	210.1
17	51	44.0	0.304	3.40	2.66	0.561	493.8	502.6	511.4	520.2	529.0	537.8	546.6
1	50	42.3	0.286	3.21	2.85	0.530	493.9	502.7	511.5	520.3	529.1	537.9	546.7
	49 48	40.6 38.9	0.270	3.02	3.04	0.498	494.0	502.8	511.6	520.4	529.2	538.0	546.8
188	47	37.2	0.240	2.69	3.21	0.470	494.1	502.9	511.7 511.8	520.5 520.6	529.3 529.4	538.1 538.2	546.9 547.0
				2.03	0.01	0.444	434.2	909.0	911.0	920.0	040.4	000.2	041.0
9.55	46	35.5	0.226	2.53	3.53	0.417	494.3	503.1	511.9	520.7	529.5	538.3	547.1
-	45	33.8	0.213	2.38	3.68		494.4	503.2	512.0		529.6	C 45 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5	547.2
	44	32.1	0.200	2.24	3.82	0.370	494.5	-503.3	512.1	The second second	529.7	538.5	547.3
	43 42	30.4	0.188	2.11	3.95	0.348	494.6	503.4	512.2	521.0	529.8	538.6	547.4
	41	27.0	0.177	1.99	4.07	0.328	494.7	503.5	512.3 512.3	521.1	529.9	538.7 538.7	547.5 547.5
1 1		1		1.01	4.10	0.509	434.1	003.0	012.5	021.1	029.9	990.1	047.0

	ding	Temp.	Force	We of V	ight apor.	Hu-		Weigh	t in Grain	ns of a Cu	ıbic Foot	of Air.	
mon	neter,	of Dew-	of Vapor	In a	for	midity, Satura-		Height	of the Ba	rometer i	n Englis	h Inches.	175
1		Point, Fahr.	in English	Cubic Foot of	Sat'n. of aCu-	tion = 1.000.	in.	in.	in.	in.	in.	in.	in.
Dry.	Wet.		Inches.	Air.	of Air.		28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
62	62 61	62.0	0.559	6.25 5.91	0.00	1.000	491.2	499.9	508.7	517.5 517.7	526.3 526.5	535.1 535.3	543.9
No.	60	58.6	0.499	5.58	0.67	0.893	491.5	500.2	509.0	517.8	526.6	535.4	544.2
. 7	59	56.9	0.472	5.27	0.98	0.843	491.7	500.4	509.2	518.0	526.8	535.6	544.4
1,150	58	55.2	0.445	4.99	1.26	0.798	491.9	500.6	509.4	518.2	527.0	535.8	544.6
	57	53.5	0.421	4.70	1.55	0.752	492.0	500.7	509.5	518.3	527.1	535.9	544.7
	56	51.8	0.397	4.44	1.81	0.710	492.1	500.7	509.5	518.4	527.3	536.1	544.9
2.0	55	50.1	0.375	4.19	2.06	0.670	492.2	500.9	509.7	518.5	527.4	536.2	545.0
2.4	54	48.4	0.354	3.95	2.30	0.632	492.4	501.1	509.9	518.7	527.6	536.4	545.2
1	53	46.7	0.333	3.72	2.53	0.595	492.5	501.3	510.1	518.9	527.7	536.5	545.8
No. of London	52	45.0	0.315	3.52	2.73	0.563	492.7	501.5	510.3	519.1	527.9	536.7	545.5
	51	43.3	0.297	3.31	2.94	0.530	492.8	501.6	510.4	519.2	528.0	536.8	545.6
201	50	41.6	0.280	3.13	3.12	0.501	492.9	501.7	510.5	519.3	528.1	536.9	545.7
To A	49	39.9	0.263	2.95	3.30	0.472	493.0	501.8	510.6	519.4	528.2	537.0	545.8
185	48	38.2	0.248	2.77	3.48	0.443	493.1	501.9	510.7	519.5	528.3	537.1	545.9
9.0	47	36.5	0.234	2.61	3.64	0.418	493.2	502.0	510.8	519.6	528.4	537.2	546.0
7.9	46	34.8	0.220	2.47	3.78	0.395	493.3	502.1	510.9	519.7	528.5	537.3	546.
	45	33.1	0.207	2.32	3.93	0.371	493.3	502.1	511.0	519.7	528.6	537.3	546.
1	44	31.4	0.195	2.18	4.07	0.349	493.4	502.2	511.0	519.8	528.6	537.4	546.2
	43	29.7	0.184	2.06	4.19	0.330	493.4	502.2	511.1	519.8	528.6	537.4	546.2
	42	28.0	0.173	1.94	4.31	0.311	493.5	502.3	511.2	519.9	528.7	537.5	546.5
	41	26.3	0.163	1.83	4.42	0.293	493.6	502.4	511.3	520.0	528.8	537.6	546.4
8					- 1				Control of				0 20
63	63	63.0	0.578	6.45	0.00	1.000	490.2	498.9	507.7	516.4	525.2	533.9	542.7
(0.3)	62	61.3	0.546	6.10	0.35	0.946	490.4	499.1	507.9	516.6	525.4	534.1	542.9
Bish	61	59.6	0.516	5.76	0.69	0.893	490.5	499.2	508.0	516.7	525.5	534.2	543.0
30	60	57.9	0.488	5.44	1.01	0.843	490.7	499.4	508.2	516.9	525.7	534.4	543.2
	59	56.2	0.461	5.15	1.30	0.798,	490.9	499.6	508.4	517.1	525.9	534.6	543.4
300	58	54.5	0.435	4.86	1.59	0.753	491.0	499.7	508.5	517.2	526.0	534.7	543.5
1000	57	52.8	0.411	4.59	1.86	0.712	491.1	499.8	508.6	517.3	526.2	534.9	543.7
	56	51.1	0.388	4.33	2.12	0.671	491.2	499.9	508.7	517.4	526.3	535.0	543.8
	55	49.4	0.366	4.09	2.36	0.634	491.3	500.0	508.8	517.5	526.4	535.1	543.9
	54	47.7	0.345	3.85	2.60	0.597	491.5	500.2	509.0	517:7	526.6	535.3	544.1
175-75	53	46.0	0.326	3.63	2.82	0.563	491.7	500.4	509.2	518.0	526.8	535.5	544.3
	52	44.3	0.307	3.43	3.02	0.532	491.8	500.5	509.3	518.1	526.9	535.6	544.4
11-11	51	42.6	0.289	3.24	3.21	0.502	491.9	500.6	509.4	518.2	527.0	535.7	544.5
	50	39.2	0.273	3.05 2.07	3.40	0.473	492.0	500.7 500.8	509.5 509.6	518.3 518.4	527.1 527.2	535.8 535.9	544.7
Re	48	37.5	0.237	2.71	3.74	0.420	492.1	500.9	509.7	518.5	527.3	536.0	544.8
			A COLUMN			MILES IN			1000			63 1 (8)	
	47 46	35.8	0.228	2.56	3.89	0.397	492.3	501.0 501.1	509.8 509.9	518.6	527.4 527.5	536.1	544.9
	46	34.1 32.4	0.215	2.41	4.19	0.374	492.4	501.1	510.0	518.7 518.8	527.6	536.2 536.3	545.0 545.1
Fig.	44	30.7	0.190	2.13	4.32	0.330	492.5	501.2	510.0	518.8	527.6	536.3	545.1
30	43	29.0	0.179	2.00	4.45	0.310	492.6	501.3	510.1	518.9	527.7	536.4	545.2
Carl.	42	27.3	0.168	1.87		0.290	492.7				527.8	536.5	545.3

Re	ading	Macro	Force	We of V	ight	17		Weigh	t in Grain	ns of a Cu	ıbic Foot	of Air.	
mo	Ther- meter,	Temp. of Dew-	of Vapor	Ina	Reqd.	Hu- midity, Satura-		Height o	of the Ba	rometer i	n English	Inches.	
		Point, Fahr.	in English	Foot of	Sat'n. of aCu-	tion = 1.000.					155		
Dry.	Wet.	Faur.	Inches.	Air.	bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
64	64	64.0	0.597	6.65	0.00	1.000	489.1	497.8	506.6 506.8	515.3 515.5	524.0 524.2	532.7 532.9	541.5 541.7
1	62	60.6	0.534	5.94	0.71	0.893	489.5	498.2	507.0	515.7	524.4	533.1	541.9
1970	61	58.9	0.504	5.61	1.04	0.843	489.7	498.4	507.2	515.9	524.6	533.3	542.1
	60	57.2	0.476	5.31	1.34	0.798	489.9	498.6	507.4	516.1	524.8	533.5	542.3
	59	55.5	0.450	5.01	1.64	0.753	490.0	498.7	507.5	516.2	524.9	533.6	542.4
y been	58	53.8	0.425	4.73	1.92	0.711	490.1	498.8	507.6	516.3	525.1	533.8	542.6
1	57	52.1	0.401	4.47	2.18	0.672	490.2	498.9	507.7	516.4	525.2	533.9	542.7
Sec.	56	50.4	0.379	4.23	2.42	0.636	490.4	499.1	507.9	516.6	525.4	534.1	542.9
	55	48.7	0.357	3.98	2.67	0.598	490.5	499.2	508.0	516.7	525.5	534.2	543.0
	54	47.0	0.337	3.75	2.90	0.564	490.7	499.4	508.2	516,9	525.7	534.4	543.2
	53	45.3	0.318	3.55	3.10	0.534	490.8	499.5	508.3	517.0	525.8	534.5	543.3
	52	43.6	0.300	3.34	3.31	0.502	490.9	499.6	508.4	517.1	525.9	534.6	543.4
	51 50	41.9	0.282	3.15	3.50	0.473	491.0	499.7	508.5	517.2 517.4	526.0	534.7	543.5
	49	38.5	0.251	2.79	3.86	0.419	491.2	500.0	508.7	517.4	526.1 526.2	534.9 535.0	543.7
- Ale	48	36.8	0.236	2.63	4.02	0.396	491.4	500.0	508.9	517.6	526.3	535.1	543.8 543.9
	47	35.1	0.223	2.47	4.18	0.372	491.5	500.2	509.0	517.7	526.4	535.2	544.0
- 10	46	33.4	0.210	2.33	4.32	0.351	491.6	500.3	509.1	517.8	526.5	535.3	544.1
	45	31.7	0.197	2.19	4.46	0.330	491.7	500.4	509.2	517.9	526.6	535.4	544.2
	44	30.0	0.186	2.06	4.59	0.310	491.7	500.4	509.2	517.9	526.6	535.4	544.2
	43	28.3	0.175	1.94	4.71	0.292	491.8	500.5	509.3	518.0	526.7	535.5	544.3
	42	26.6	0.164	1.83	4.82	0.275	491.9	500.6	509.4	518.1	526.8	535.6	544.4
			200							- 4			
65	65	65.0	0.617	6.87	0.00	1.000	488.1	496.8	505.5	514.2	522.9	531.6	540.3
13.6	64	63.4	0.586	6.51	0.36	0.947	488.3	497.0	505.7	514.4	523.1	531.8	540.5
3.0	63	61.8	0.555	6.17	0.70	0.898	488.5	497.2	505.9	514.6	523.3	532.0	540.7
	62	60.2	0.527	5.85	1.02	0.851	488.7	497.4	506.1	514.8	523.5	532.2	540.9
	61	58.6	0.499	5.55	1.32	0.808	488.9	497.6	506.3	515.0	523.7	532.4	541.1
118	60	57.0	0.473	5.25	1.62	0.765	489.0	497.7	506.5	515.2	523.9	532.6	541.3
1 1 2 2	59	55.4	0.449	4.98	1.89	0.725	489.1	497.8	506.6	515.3	524.0	532.7	541.5
	58	53.8	0.425	4.72	2.15	0.687	489.3	498.0	506.8	515.5	524.2	532.9	541.7
1.524	57	52.2	0.402	4.47	2.40	0.651	489.4	498.1	506.9	515.6	524.3	533.0	541.8
0.0	56 55	50.6	0.381	4.23	2.64	0.616	489.6	498.3	507.1	515.8	524.5	533.2	542.0
-	54	49.0	0.361	4.01	2.86	0.584	489.7	498.4	507.2	515.9	524.6	533.3	542.1
	53	45.8	0.342	3.79	3.08	0.552	489.8	498.5	507.3	516.0	524.7 524.8	533.4	542.2
	52	44.2	0.306	3.39	3.48	0.324	489.9	498.6 498.7	507.4	516.1 516.2	524.8	533.5 533.6	542.3 542.4
1	51	42.6	0.289	3.22	3.65	0.469	490.1	498.8	507.6	516.3	525.0	533.7	542.5
	50	41.0	0.274	3.04	3.83	0.442	490.2	498.9	507.7	516.4	525.1	533.8	542.6
1 1993	49	39.4	0.259	2.87	4.00	0.418	490.3	499.0	507.8	516.5	525.2	533.9	542.7
	48	37.8	0.245	2.72	4.15	0.396	490.3	499.0	507.8	516.5	525.2	533.9	542.7
	47	36.2	0.231	2.57	4.30	0.374	490.4	499.1	507.9	516.6	525.3	534.0	542.8
	46	34.6	0.219	2.43	4.44	0.354	490.5	499.2	508.0.	516.7	525.4	534.1	542.9
	45	33.0	0.207	2.31	4.56	0.336	490.6	499.3	508.1	516.8	525.5	534.2	543.0
	44	31.4	0.195	2.17	4.70	0.316	490.7	499.4	508.2	516.9	525.6	534.3	543.1
1	43	29.8	0.184	2.05	4.82	0.299	490.7		508.2	516.9	525.6	534.3	543.1
100	42	28.2	0.174	1.94	4.93	0.283	490.8	499.5	508.3	517.0	525.7	534.4	543.2

-		1		317	lab #		1		04,07				
	eading Ther-	Temp.	Force	of V	apor	Hu-		Weigh	t in Grain	as of a Cu	abic Foot	of Air.	
m	ometer, Fahr.	of Dew-	of Vapor	Ina	Reqd.	midity, Satura-		Height	of the Ba	rometer i	n English	h Inches.	
		Point, Fahr.	in English	Cubic	Sat'n. of aCu-	tion =					V/ ==		
Dry	. Wet.	Fanr.	Inches.	Air.	bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
	0 0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
66	1 7 6 1	66.0	0.638	7.08	0.00	1.000	487.0	495.7	504.4	513.1	521.8	530.5	539.2
	65	64.4	0.605	6.72	0.36	0.949	487.2	495.9	504.6 504.7	513.3 513.4	522.0 522.1	530.7 530.8	539.4 539.5
	63	61.2	0.574	6.04	1.04	0.853	487.5	496.2	504.7	513.4	522.1	531.0	539.7
1	62	59.6	0.516	5.72	1.36	0.808	487.7	496.4	505.1	513.8	522.5	531.2	539.9
1	61	58.0	0.489	5.42	1.66	0.766	487.9	496.6	505.3	514.0	522.7	531.4	540.1
		B 87	7 11		1200		(A. 17)	41.74	A PARK	0.2.10		MILE	
	60	56.4	0.464	5.14	1.94	0.726	488.0	496.7	505.4	514.1	522.8	531.5	540.2
10.0	59	54.8	0.440	4.88	2.20	0.689	488.1	496.8	505.5	514.2	523.0	531.7	540.4
145	58	53.2	0.416	4.62	2.46	0.652	488.2	496.9	505.6	514.3	523.1	531.8	540.5
	57	51.6	0.394	4.37	2.71	0.619	488.4	497.1	505.8	514.5	523.3	532.0	540.7
	56	50.0	0.373	4.15	2.93	0.586	488.5	497.2	505.9	514.6	523.4	532.1	540.8
	55	40.4	0.354	3.92	3.16	0.553	488.6	497.3	506.1	514.8	523.5	532.2	541.0
1	54	46.8	0.335	3.72	3.36	0.525	488.8	497.5	506.3	515.0	523.7	532.4	541.2
127	53	45.2	0.317	3.51	3.57	0.496	488.9	497.6	506.4	515.1	523.8	532.5	541.3
	52	43.6	0.300	3.33	3.75	0.470	489.0	497.7	506.5	515.2	523.9	532.6	541.4
1	51	42.0	0.283	3.14	3.94	0.443	489.1	497.8	506.6	515.3	524.0	532.7	541.5
18.9	50	40.4	0.268	2.97	4.11	0.419	489.2	497.9	506.7	515.4	524.1	532.8	541.6
	49	38.8	0.253	2.81	4.27	0.397	489.3	498.0	506.8	515.5	524.2	532.9	541.7
	48	37.2	0.240	2.66	4.42	0.376	489.4	498.1	506.9	515.6	524.3	533.0	541.8
	47	35.6	0.227	2.51	4.57	0.355	489.4	498.1	506.9	515.6	524.3	533.0	541.8
	46	34.0	0.214	2.37	4.71	0.335	489.5	498.2	507.0	515.7	524.4	533.1	541.9
	45	32.4	0.202	2.24	4.84	0.316	489.6	498.3	507.1	515.8	524.5	533.2	542.0
	44	30.8	0.191	2.12	4.96	0.299	489.7	498.4	507.2	515.9	524.6	533.3	542.1
	43	29.2	0.180	2.00	5.08	0.283	489.7	498.4	507.2	515.9	524.6	533.3	542.1
							E M						
67	67	67.0	0.659	7.30	0.00	1.000	485.9	494.6	503.3	512.0	520.6	529.3	538.0
100	66	65.4	0.626	6.93	0.37	0.949	486.1	494.8	503.5	512.2	520.8	529.5	538.2
	65	63.8	0.593	6.55	0.75	0.897	486.3	495.0	503.7	512.4	521.0	529.7	538.4
	64	62.2	0.563	6.23	1.07	0.853	486.5	495.2	503.9	512.6	521.2	529.9	538.6
	63	60.6	0.534	5.91	1.39	0.810	486.7	495.4	504.1	512.8	521.4	530.1	538.8
	62	59.0	0.506	5.60	1.70	0.767	486.8	495.5	504.2	512.9	521.6	530.3	539.0
	61	57.4	0.480	5.31	1.99	0.728	486.9	495.6	504.3	513.0	521.7	530.4	539.1
	60	55.8	0.455	5.04	2.26	0.691	487.1	495.8	504.5	513.2	521.9	530.6	539.3
	59	54.2	0.431	4.77	2.53	0.653	487.2	495.9	504.6	513.3	522.0	530.7	539.4
2	58	52.6	0.408	4.52	2.78	0.619	487.3	496.0	504.7	513.4	522.1	530.8	539.5
	57	51.0	0.386	4.28	3.02	0.586	487.5	THE REAL PROPERTY.	504.9	513.6	1000	531.0	539.7
	56	49.4	0.366	4.05	3.25	0.555	487.6	496.3	505.0	513.7	522.4	531.1	539.8
	55	47.8	0.346	3.83	3.47	0.524	487.8	496.5	505.1	513.8	522.6	531.2	549.9
	54	46.2	0.328	3.62	3.68	0.496	487.9	496.6	505.2	513.9	522.7	531.3	540.0
	53	44.6	0.310	3.43	3.87	0.470	488.0	496.7	505.3	514.0	522.8	531.4	540.1
	52	43.0	0.293	3.25	4.05	0.445	488.1	496.8	504.4	514.1	522.9	531.5	540.2
	51	41.4	0.278	3.08	4.22	0.422	488 2	496.9	505.5	514.2	523.0	531.6	540.3
1	50	39.8	0.263	2.91	4.39	0.399		497.1			523.1	531.8	540.5
	49	38.2	0.248	P-100-0-0-0	4.55	0.377	1 11 11 11 11			The second second	523.2		
	D	1	3.2.3		1100		100.0		1 300.0	321.0	7 7 7 7 7	301.0	

of '	ading Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ns of a Cu	ibic Foot	of Air.	
mon	neter,	of Dew-Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	in. 29.0	29.5	30.0	in. 30.5	in. 31.0
0	0	0	in.	gr.	gr.	0.955	gr.	gr.	gr.	gr.	gr.	gr.	gr.
67	49 48	38.2 36.6	0.248	2.75	4.55	0.377	488.5	497.2	505.8 505.9	514.5 514.6	523.2 523.3	531.9 532.0	540.6 540.7
	47	35.0	0.222	2.46	4.84	0.337	488.7	497.4	505.9	514.7	523.4	532.1	540.8
	46	33.4	0.210	2.32	4.98	0.318	488.7	497.4	506.0	514.7	523.4	532.1	540.8
li ne	45	31.8	0.198	2.19	5.11	0.301	488.8	497.5	506.1	514.8	523.5	532.2	540.9
	44	30.2	0.187	2.07	5.23	0.284	488.9	497.6	506.2	514.9	523.6	532.3	541.0
68	68	68.0	0.681	7.53	0.00	1.000	484.9	493.5	502.2	510.8	519.5	528.1	536.8
00	67	66.4	0.646	7.15	0.38	0.949	485.1	493.8	502.2	511.1	519.7	528.4	537.1
20	66	64.8	0.613	6.77	0.76	0.899	485.3	494.0	502.6	511.2	519.9	528.6	537.3
4.7	65	63.2	0.582	6.43	1.10	0.854	485.5	494.2	502.8	511.4	520.1	528.8	537.5
0.1	64	61.6	0.552	6.10	1.43	0.810	485.7	494.4	503.0	511.6	520.3	529.0	537.7
	63	60.0	0.523	5.78	1.75	0.768	485.8	494.5	503.1	511.8	520.5	529.2	537.9
PIE	62	58.4	0.496	5.47	2.06	0.726	485.9	494.6	503.3	512.0	520.7	529.4	538.1
13	61	56.8	0.470	5.20	2.33	0.691	486.0	494.7	503.4	512.1	520.8	529.5	538.3
1,-	60	55.2	0.445	4.93	2.60	0.655	486.2	494.9	503.6	512.3	521.0	529.7	538.5
23	59	53.6	0.422	4.67	2.86	0.620	486.3	495.0	503.7	512.4	521.1	529.8	538.6
13.5	58	52.0	0.400	4.42	3.11	0.587	486.4	495.1	503.8	512.5	521.2	529.9	538.6
3,1	57	50.4	0.379	4.19	3.34	0.556	486.6	495.3	504.0	512.7	521.4	530.1	538.8
	56	48.8	0.358	3.96	3.57	0.526	486.7	495.4	504.1	512.8	521.5	530.2	538.9
	55	47.2	0.339	3.75	3.78	0.498	486.8	495.5	504.2	512.9	521.6	530.3	539.0
	54	45.6	0.321	3.54	3.99	0.470	486.9	495.6	504.3	513.0	521.7	530.4	539.1
1.8	53 52	44.0	0.304	3.35	4.18	0.445	487.0	495.7	504.4	513.1	521.8 521.9	530.5	539.2
	51	40.8	0.272	3.00	4.53	0.421	487.1	495.8 495.9	504.5 504.6	513.2 513.3	522.0	530.6 530.7	539.4
	180		V.HO		STE		1078.5	le constitution	-050				150
	50 49	39.2 37.6	0.257	2.84	4.69	0.377	487.3	496.0	504.7	513.4	522.1	530.8	539.5
	48	36.0	0.243	2.68	4.85	0.356	487.4	496.1	504.8	513.5 513.6	522.2 522.3	530.9 531.0	539.7
4.04	47	34.4	0.230	2.40	5.13	0.319	487.6	496.3	505.0	513.7	522.4	531.1	539.8
10	46	32.8	0.205	2.27	5.26	0.302	487.6	496.3	505.0	513.7	522.4	531.1	539.8
	45	31.2	0.194	2.15	5.38	0.286	487.7	496.4	505.1	513.8	522.5	531.2	539.9
	44	29.6	0.183	2.04	5.49	0.271	487.8	496.5	505.2	513.9	522.6	531.3	540.0
69	69	69.0	0.704	7.76	0.00	1.000	483.8	492.4	501.1	509.7	518.3	527.0	535.0
N. T.	68	67.4	0.668	7.37	0.39	0.950	484.0	492.6	501.3	509.9	518.5	527.2	535.8
	67	65.8	0.634	7.00	0.76	0.902	484.2	492.8	501.5	510.1	518.7	527.4	536.0
	66	64.2	0.601	6.63	1.13	0.854	484.4	493.0	501.7	510.3	518.9	527.6	536.2
200	65	62.6	0.570	6.29	1.47	0.810	484.6	493.2	501.9	510.5	519.1	527.8	536.4
D.811	64	61.0	0.541	5.97	1.79	0.769	484.8	493.4	502.1	510.7	519.3	528.0	536.6
30	63	59.4	0.513	5.65	2.11	0.728	485.0	493.6	502.3	510.9	519.5	528.2	536.8
	62	57.8	0.486	5.37	2.39	0.693	485.1	493.7	502.4	511.0	519.6	528.3	536.9
	61	56.2	0.461	5.09	2.67	0.657	485.1	493.7	502.6	511.2	519.8	528.5	537.1
	59	54.6 53.0	0.437	4.82	2.94	0.621	485.2	493.9	502.7	511.3	519.9	528.6	537.3
	58	51.4	0.392		3.19	0.589	485.4	494.1	502.8	511.5 511.6	520.1 520.2	528.8 528.9	537.6

	ading Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ns of a Cu	ibic Foot	of Air.	
mor	neter, ahr.	of Dew-	of Vapor in	In a Cubic	for Sat'n.	midity, Satura-		Height o	of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.		tion = 1.000.	28.0	in. 28.5	29.0	29.5	30.0	in. 30.5	31.0
69	o 58	o 51.4	in. 0.392	gr. 4.33	gr. 3.43	0.558	gr. 485.5	gr. 494.2	gr. 502.9	gr. 511.6	gr. 520.2	gr. 528.9	gr. 537.6
00	57	49.8	0.371	4.09	3.67	0.527	485.7	494.4	503.1	511.8	520.4	529.1	537.8
	56	48.2	0.351	3.87	3.89	0.499	485.8	494.5	503.2	511.9	520.5	529.2	537.9
3	55	46.6	0.332	3.66	4.10	0.472	485.9	494.6	503.3	512.0	520.6	529.3	538.0
i uși	54	45.0	0.315	3.47	4.29	0.447	486.0	494.7	503.4	512.1	520.7	529.4	538.1
7.4	53	43.4	0.298	3.29	4.47	0.424	486.1	494.8	503.5	512.2	520.8	529.5	538.2
10.7	52	41.8	0.282	3.11	4.65	0.401	486.2	494.9	503.6	512.3	520.9	529.6	538.3
	51	40.2	0.266	2.94	4.82	0.379	486.3	495.0	503.7	512.4	521.0	529.7	538.4
- 3.2	50	38.6	0.252	2.78	4.98	0.358	486.4	495.1	503.8	512.5	521.1	529.8	538.5
34	49	37.0	0.238	2.63	5.13	0.339	486.5	495.2	503.9	512.6	521.2	529.9	538.6
0,5	48	35.4	0.225	2.49	5.27	0.321	486.6	495.3	504.0	512.7	521.3	530.0	538.7
7.8	47	33.8	0.213	2.34	5.42	0.302	486.7	495.4	504.1	512.8	521.4	530.1	538.8
	46 45	32.2	0.201	2.20	5.56	0.284	486.8	495.5	504.2	512.9 512.9	521.5	530.2 530.2	538.9 538.9
1	40	50.0	0.190	2.00	5.70	0.200	486.8	490.0	504.2	512.9	521.5	950.2	990.9
				B. 1.5		Track of							
70	70	70.0	0.727	8.00	0.00	1.000	482.8	491.4	500.0	508.6	517.2	525.8	534.4
10	69	68.5	0.692	7.62	0.38	0.953	483.0	491.4	500.0	508.8	517.4	526.0	534.4
	68	67.0	0.659	7.26	0.74	0.907	483.2	491.8	500.4	509.0	517.6	526.2	534.8
	67	65.5	0.628	6.91	1.09	0.865	483.3	491.9	500.5	509.1	517.7	526.3	534.9
7700	66	64.0	0.597	6.57	1.43	0.822	483.5	492.1	500.7	509.3	517.9	526.5	535.1
1	65	62.5	0.568	6.25	1.75	0.781	483.7	492.3	500.9	509.5	518.1	526.7	535.3
	64	61.0	0.541	5.95	2.05	0.744	483.8	492.4	501.0	509.6	518.3	526.9	535.5
35.00	00	50 E	0 515	F 00		0 700	4040	400.0	FO. 0	F00.0	F10 F	E07 1	E95 W
20	63 62	59.5	0.515	5.66	2.34 2.62	0.708	484.0	492.6 492.8	501.2	509.8 510.0	518.5 518.7	527.1 527.3	535.7 535.9
Line	61	56.5	0.465	5.12	2.88	0.640	484.3	492.9	501.4	510.1	518.8	527.4	536.0
0.3	60	55.0	0.442	4.87	3.13	0.609	484.4	493.0	501.6	510.2	518.9	527.5	536.1
4.9	59	53.5	0.421	4.62	3.38	0.578	484.6	493.2	501.8	510.4	519.1	527.7	536.3
9.6	58	52.0	0.400	4.40	3.60	0.550	484.7	493.3	501.9	510.5	519.2	527.8	536.4
	57	50.5	0.380	4.18	3.82	0.522	484.8	493.4	502.0	510.6	519.3	527.9	536.5
1	56	49.0	0.361	3.96	4.04	0.495	484.9	493.5	502.1	510.7	519.4	528.0	536.6
	55	47.5	0.343	3.76	4.24	0.433	485.1	493.7	502.1	510.9	519.6	528.2	536.8
	54	46.0	0.326	3.57	4.43	0.446	485.2	493.8	502.4	511.0	519.7	528.3	536.9
THE S	53	44.5	0.309	3.40	4.60	0.425	485.3	493.9	502.5	511.1	519.8	528.4	537.0
	52	43.0	0.292	3.23	4.77	0.404	485.4	494.0	502.6	511.2	519.9	528.5	537.1
1	51	41.5	0.279	3.07	4.93	0.384	485.5	494.1	502.7	511.3	520.0	528.6	537.2
	50	40.0	0.264	2.81	5.19	0.351	485.5	494.1	502.7	511.3	520.0	528.6	537.2
	49	38.5	0.251	2.76	5.24	0.345	485.6	494.2	502.8	511.4	520.1	528.7	537.3
	48	37.0	0.238	2.63	5.37	0.329	485.7	494.3	502.9	511.5	520.1	528.8	537.4
	47	35.5	0.226	2.50	5.50	0.313	485.8	494.4	503.0	511.6	520.3	528.9	537.5
	46	34.0	0.214	2.37	5.63	0.296	485.8	494.4	503.0	511.6	520.3	528.9	537.5
	45	32.5	0.203	2.24	5.76	0.280	485.9	494.5	503.1	511.7	520.4	529.0	537.6
	44	31.0	0.192	2.12	5.88	0.265	486.0	494.6	503.2	511.8	520.5	529.1	537.7
1	43	29.5	0.182	2.01	5.99	0.251	486.1	494.7	503.3	511.9	520.6	529.2	537.8

Res	ding	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grain	as of a Ci	abic Foot	of Air.	
mor	neter,	of Dew-	of Vapor	Ina	Reqd.	midity, Satura-		Height	of the Ba	rometer	in Englis	h Inches	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.	Sat'n. of aCu- bic Ft. of Air.	tion = 1.000.	in. 28.0	in. 28.5	in. 29.0	in. 29.5	in. 30.0	in. 30.5	in. 31.0
0 71	° 71	° 71.0	in. 0.751	gr. 8.25	gr. 0.00	1.000	gr. 481.6	gr. 490.2	gr. 498.8	gr. 507.4	gr. 516.0	gr 524.6	gr. 533.2
	70	69.5	0.715	7.86	0.39	0.953	481.8	490.4	499.0	507.6	516.2	524.8	533.4
10	69	68.0	0.681	7.48	0.77	0.907	482.0	490.6	499.2	507.8	516.4	525.0	533.6
-100	68	66.5	0.648	7.13	1.12	0.865	482.2	490.8	499.4	508.0	516.6	525.2	533.8
	67	65.0	0.617	6.79	1.46	0.823	482.4	491.0	499.6	508.2	516.8	525.4	534.0
7.00	66	63.5	0.588	6.45	1.80	0.782	482.6	491.2	499.8	508.4	517.0	525.6	534.2
	65	62.0	0.559	6.14	2.11	0.744	482.8	491.4	500.0	508.6	517.2	525.8	534.4
	64	60.5	0.532	5.85	2.40	0.709	483.0	491.6	500.2	508.8	517.4	526.0	534.6
	63	59.0	0.506	5.56	2.69	0.674	483.1	491.7	500.3	508.9	517.5	526.1	534.7
	62	57.5	0.481	5.28	2.97	0.640	483.2	491.8	500.4	509.0	517.7	526.3	534.9
	61	56.0	0.458	5.03	3.22	0.609	483.3	491.9	500.5	509.1	517.8	526.4	535.0
	60	54.5	0.435	4.78	3.47	0.579	483.5	492.1	500.7	509.3 509.4	518.0	526.6 526.7	535.1
88	59 58	51.5	0.414	4.34	3.94	0.522	483.8	492.4	501.0	509.4	518.1 518.3	526.9	535.4
	00	01.0	0.000	1.02	0.01	0.022	100.0	102.1	001.0	000.0	010.0	020.0	000.5
	57	50.0	0.373	4.10	4.15	0.497	483.9	492.5	501.1	509.7	518.4	527.0	535.5
18.1	56	48.5	0.355	3.89	4.36	0.471	484.0	492.6	501.2	509.9	518.5	527.1	535.6
	55	47.0	0.337	3.69	4.56	0.447	484.1	492.7	501.3	510.0	518.6	527.2	535.7
	54	45.5	0.320	3.51	4.74	0.425	484.2	492.8	501.4	510.1	518.7	527.3	535.8
	53	44.0	0.304	3.33	4.92	0.404	484.3	492.9	501.5	510.2	518.8	527.4	535.9
6.0	52	42.5	0.288	3.16	5.09	0.383	484.4	493.0	501.6	510.3	518.9	527.5	536.0
315	51	41.0	0.274	3.00	5.25	0.364	484.5	493.1	501.7	510.4	519.0	527.6	536.1
	50	39.5	0.260	2.85	5.40	0.345	484.6	493.2	501.8	510.5	519.1	527.7	536.2
	49	38.0	0.246	2.70	5.55	0.327	484.7	493.3	501.9	510.6	519.2	527.8	536.3
100	48	36.5	0.234	2.57	5.68	0.312	484.7	493.3	501.9	510.6	519.2	527.8	536.3
1000	47	35.0	0.222	2.44	5.81	0.296	484.8	493.4	502.0	510.7	519.3	527.9	536.4
	46	33.5	0.210	2.31	5.94	0.280	484.9	493.5	502.1	510.8	519.4	528.0	536.5
5-7	45	32.0	0.199	2.19	6.06	0.265	485.0	493.6	502.2	510.9	519.5	528.1	536.6
194	44	30.5	0.189	2.08	6.17	0.252	485.0	493.6	502.2	510.9	519.5	528.1	536.6
IN SA			id il	100	esplo o		ALERY D	Marke S	View In	1,5 (3)	Hall S	On i	
72	72	72.0	0.776	8.50	0.00	1.000	480.6	489.2	497.8	506.4	514.9	523.5	532.1
10-31	71	70.5	0.739	8.10	0.40	0.953	480.8	489.4	498.0	506.5	515.1	523.7	532.3
19.4	70	69.0	0.704	7.71	0.79	0.907	481.0	489.6	498.2	506.7	515.3	523.9	532.5
217	69	67.5	0.670	7.35	1.15	0.865	481.2	489.8	498.4	506.9	515.5	524.1	532.7
	68	66.0	0.638	7.00	1.50	0.824	481.4	490.0	498.5	507.1	515.7	524.3	532.9
	67	64.5	0.607	6.66	1.84	0.784	481.6	490.2	498.7	507.3	515.9	524.5	533.1
17.	66	63.0	0.578	6.33	2.17	0.745	481.7	490.3	498.8	507.4	516.1	524.7	533.3
	65	61.5	0.550	6.03	2.47	0.710	481.8	490.4	499.0	507.6	516.2	524.8	533.4
1	64	60.0	0.523	5.73	2.77	0.674	482.0	490.6	499.2	507.8	516.4	525.0	533.6
199	63	58.5	0.498	5.45	3.05	0.641	482.1	490.7	499.3	507.9	516.5	525.1	533.7
	62	57.0	0.473	5.18	3.32	0.610	482.3	490.9	499.5	508.1	516.7	525.3	533.9
	61	55.5	0.450	4.93	3.57	0.580	482.5	491.1	499.7	508.3	516.9	525.5	534.1
	60	54.0	0.428	4.68	3.82	0.551	482.6	491.2	499.8	508.4	517.0	525.6	534.2
	59	52.5	0.407	4.45	4.05	0.523	482.8	491.4	500.0	508.6	517.2	525.8	534.4

of	ading Ther-	Temp.	Force of		ght apor Reqd.	Hu-		Weigh	t in Grain	ns of a Cu	bic Foot	of Air.	
	neter,	Dew-	Vapor	In a Cubic	for Sat'n.	midity, Satura-		Height o	of the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.			tion = 1.000.	in. 28.0	in. 28.5	29.0	in. 29.5	30.0	in. 30.5	31.0
0	0	0	in.	gr.	gr.	0.500	gr.	gr.	gr.	gr.	gr.	gr.	gr.
72	59	52.5	0.407	4.45	4.05	0.523	482.8	491.4	500.0	508.6 508.7	517.2 517.3	525.8 525.9	534.4 534.5
	58 57	51.0	0.367	4.23	4.48	0.498	482.9 483.0	491.5	500.1	508.8	517.4	526.0	534.6
	56	48.0	0.349	3.82	4.48	0.449	483.1	491.7	500.2	508.9	517.5	526.1	534.7
8.77	55	46.5	0.331	3.63	4.87	0.427	483.2	491.8	500.4	509.0	517.6	526.2	534.8
100	54	45.0	0.315	3.45	5.05	0.406	483.3	491.9	500.5	509.1	517.7	526.2	534.9
10 14	53	43.5	0.299	3.28	5.22	0.386	483.3	492.0	500.6	509.2	517.8	526.3	535.0
	la ke			9								11111111	
L	52	42.0	0.283	3.11	5.39	0.366	483.5	492.1	500.7	509.3	517.9	526.4	535.1
27-20	51	40.5	0.269	2.95	5.55	0.347	483.6	492.2	500.8	509.4	518.0	526.5	535.2
-m-12	50	39.0	0.255	2.80	5.70	0.329	483.7	492.3	500.9	509.5	518.1	526.6	535.3
1	49	37.5	0.242	2.66	5.84	0.313	483.8	492.4	501.0	509.6	518.2	526.7	535.4
4.5	48	36.0	0.230	2.52	5.98	0.296	483.8	492:4	501.0	509.6	518.2	526.7	535.4
100	47	34.5	0.218	2.39	6.11	0.281	483.9	492.5	501.2	509.7	518.3	526.8	535.5
	46	33.0	0.207	2.27	6.23	0.267	484.0	492.6	501.3	509.8	518.4	526.9	535.6
	45	31.5	0.196	2.16	6.34	0.254	484.1	492.7	501.3	509.9	518.5	527.1	535.7
				1213		0.5		5. 16. 1 h	1318		7 6		+
73	73	73.0	0.801	8.76	0.00	1.000	479.6	488.1	496.7	505.2	513.8	522.3	530.9
13	72	71.5	0.736	8.35	0.41	0.953	479.8	488.3	496.9	505.4	514.0	522.5	531.1
21	71	70.0	0.727	7.95	0.81	0.908	480.0	488.5	497.1	505.6	514.2	522.7	531.8
17.51	70	68.5	0.692	7.57	1.19	0.864	480.2	488.7	497.3	505.8	514.4	522.9	531.5
Q.E	69	67.0	0.659	7.21	1.55	0.823	480.4	488.9	497.5	506.0	514.6	523.1	531.7
	68	65.5	0.628	6.87	1.89	0.784	480.5	489.0	497.6	506.1	514.8	523.3	531.9
3.0	67	64.0	0.597	6.53	2.23	0.745	480.7	489.2	497.8	506.3	515.0	523.5	532.1
10-54	00	00 -	0 700			0.000		19 644			-	700.0	
1	66	62.5	0.568	6.22	2.54	0.710	480.8	489.3	497.9	506.4	515.1	523.6	532.2
day.	65	61.0	0.541	5.92	2.84	0.676	481.0	489.5	498.1	506.6	515.3	523.8	532.4
1	64	59.5 58.0	0.515	5.63	3.13	0.643	481.1	489.6	498.2	506.8	515.4 515.6	524.0 524.2	532.6
The W	62	56.5	0.489	5.34	3.42	0.610	481.4	489.8	498.4	507.0	515.8	524.4	533.0
Testi	61	55.0	0.442	4.84	3.92	0.553	481.6	490.0	498.8	507.4	516.0	524.4	533.2
	60	53.5	0.421	4.59	4.17	0.524	481.7	490.3	498.9	507.5	516.1	524.7	533.3
	1.1.		1.0			100		DOT .	100	1	434		1136
1	59	52.0	0.400	4.37	4.39	0.499	481.8	490.4	499.0	507.6	516.2	524.8	533.4
	58	50.5	0.380	4.16	4.60	0.475	482.0	490.6	499.2	507.8	516.4	525.0	533.6
	57	49.0	0.361	3.94	4.82	0.450	482.1	490.7	499.3	507.9	516.5	525.1	533.7
	56	47.5	0.343	3.74	5.02	0.427	482.2	490.8	499.4	508.0	516.6	525.2	533.8
1	55	46.0	0.326	3.56	5.20	0.406	482.3	490.9	499.5	508.1	516.7	525.3	533.9
M	54	44.5	0.309	3.38	5.38	0.386	482.4	491.0	499.6	508.2	516.8	525.4	534.0
	53	45.0	0.293	3.21	0.00	0.300	482.5	491.1	499.7	508.3	516.9	525.5	534.1
	52	41.5	0.279	3.05	5.71	0.348	482.6	491.2	499.8	508.4	517.0	525.6	534.2
13.4	51	40.0	0.264	2.89	5.87	0.330	482.7		1	508.5	517.1	525.7	534.3
	50	38.5	0.251	2.74	6.02	0.313	482.8	1	500.0	508.6	517:2	525.8	534.4
10-8	49	37.0	0.238	2.60	6.16	0.297	482.9	491.5	100 00 00 00	1 10.00	517.2	525.8	534.4
1	48	35.5	0.226	2.47	6.29	0.282	483.0	491.6	500.1	508.7	517.3	525.9	534.5
	47	34.0	0.214			0.267	483.1	ALL DEL STORY	The second	Charles March	517.4		534.6
	46	32.5	0.203	2.22	6.54	0.253	433.3	491.9	500.4	509.1	517.6	526.2	534.8

Res	ading Ther-	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grai	as of a Cu	ubic Foot	of Air.			
mor	meter, ahr.	of Dew-	Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =	Height of the Barometer in English Inches.								
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.		1.000.	28.0	28.5	29.0	29.5	in. 30.0	30.5	31.0		
0	0	0	in.	gr.	gr.	- 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.		
74	74	74.0	0.827	9.04	0.00	1.000	478.4	486.9	495.5	504.0	512.6	521.1	529.7		
100	73	72.5	0.787	8.20	0.44	0.907	478.8	487.3	495.9	504.2 504.4	512.8 513.0	521.3	529.9		
	72 71	69.5	0.751	7.81	1.23	0.864	479.0	487.5	496.1	504.4	513.2	521.5	530.1 530.3		
14.8	70	68.0	0.681	7.44	1.60	0.823	479.2	487.7	496.3	504.8	513.4	521.9	530.5		
388	69	66.5	0.648	7.08	1.96	0.783	479.4	487.9	496.5	505.0	513.6	522.1	530.7		
	68	65.0	0.617	6.75	2.29	0.747	479.6	488.1	496.7	505.2	513.8	522.3	530.9		
9,43	67	63.5	0.588	6.41	2.63	0.709	479.8	488.3	496.9	505.4	514.0	522.5	531.1		
12.0	66	62.0	0.559	6.10	2.94	0.675	480.0	488.5	497.1	505.6	514.2	522.7	531.3		
	65	60.5	0.532	5.81	3.23	0.643	480.1	488.7	497.3	505.9	514.4	522.9	531.5		
149	64	59.0	0.506	5.52	3.52	0.611	480.3	488.9	497.5	506.1	514.6	523.2	531.8		
	63	57.5	0.481	5.24	3.80	0.580	480.5	489.1	497.7	506.3	514.8	523.4	532.0		
	62	56.0	0.458	4.99	4.05	0.552	480.6	489.2	497.8	506.4	514.9	523.5	532.1		
	61	54.5	0.435	4.75	4.29	0.525	480.7	489.3	497.9	506.5	515.0	523.6	532.2		
	60	53.0	0.414	4.52	4.52	0.500	480.9	489.5	498.1	506.7	515.2	523.8	532.4		
	59	51.5	0.393	4.29	4.75	0.475	481.0	489.6	498.2	506.8	515.3	523.9	532.5		
70.19	58	50.0	0.373	4.08	4.96	0.451	481.1	489.7	498.3	506.9	515.4	524.0	532.6		
1	57	48.5	0.355	3.86	5.18	0.427	481.2	489.8	498.4	507.0	515.5	524.1	532.7		
1	56	47.0	0.337	3.66	5.38	0.405	481.3	489.9	498.5	507.1	515.6	524.2	532.8		
1	55	45.5	0.320	3.48	5.56	0.385	481.4	490.0	498.6	507.2	515.7	524.3	532.9		
	54	44.0	0.304	3.32	5.72	0.367	481.5	490.1	498.7	507.3	515.8	524.4	533.0		
	53	42.5	0.288	3.15	5.89	0.348	481.6	490.2	498.8	507.4	515.9	524.5	533.1		
	52	41.0	0.274	2.99	6.05	0.331	481.7	490.3	498.9	507.5	516.0	524.6	533.2		
	51	39.5	0.260	2.83	6.21	0.313	481.8	490.4	499.0	507.6	516.1	524.7	533.3		
	50	38.0	0.246	2.69	6.35	0.298	481.9	490.5	499.1	507.7	516.2	524.8	533.4		
1	49	36.5	0.234	2.55	6.49	0.282	481.9	490.5	499.1	507.7	516.2	524.8	533.4		
	48	35.0	0.222	2.42	6.62	0.268	482.0	490.6	499.2	507.8	516.3	524.9	533.5		
10-6	47	33.5	0.210	2.30	6.74	0.254	482.1	490.7	499.2	507.9	516.4	525.0	533.6		
10.11			lani i	m m		Met S		Star 1	1.5	15	will a	Mil H			
75	75	75.0	0.854	9.31	0.00	1.000	477.4	485.9	494.4	502.9	511.5	520.0	528.5		
	74	73.5	0.814	8.87	0.44	0.953	477.6	486.1	494.6	503.1	511.7	520.2	528.7		
	73	72.0	0.776	8.45	0.86	0.908	477.8	486.3	494.8	503.3	511.9	520.4	528.9		
	72	70.5	0.739	8.05	1.26	0.865	478.0	486.5	495.0	503.5	512.1	520.6	529.1		
6.0	71	69.0	0.704	7.67	1.64	0.824	478.2	486.7	495.2	503.7	512.3	520.8	529.3		
1401	70	67.5	0.670	7.30	2.01	0.784	478.3	486.8	495.3	503.8	512.5	521.0	529.5		
BU	69	66.0	0.638	6.95	2.36	0.746	478.5	487.0	495.5	504.0	512.7	521.2	529.7		
	68	64.5	0.607	6.62	2.69	0.711	478.7	487.2	495.7	504.2	512.9	521.4	529.9		
1	67	63.0	0.578	6.30	3.01	0.677	478.9	487.4	495.9	504.4	513.1	521.6	530.1		
19	66	61.5	0.550	5.99	3.32	0.643	479.1	487.6	496.1	504.6	513.3	521.8	530.3		
11.33	65 64	60.0 58.5	0.523	5.69	3.62	0.611	479.3	487.8	496.4	504.9	513.5	522.0	530.6		
	63	57.0	0.498	5.42 5.15	3.89	0.582	479.5	488.0	496.6	505.1	513.7	522.2	530.8		
3 45	62	55.5	0.450	4.90	4.41	0.553	479.6	488.1	496.7	505.2	513.8	522.3	530.9		
		1 30.0	0.400	1.00	4.41	0.020	4/9./	484.2	496.8	505.3	513.9	522.4	531.0		

	ding	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	as of a Cu	ibic Foot	of Air.	1
mon	neter,	of Dew- Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	of the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	in. 28.0	28.5	29.0	29.5	30.0	in. 30.5	in. 31.0
0	0	0	in.	gr.	gr.	0.500	gr.	gr.	gr.	gr.	gr.	gr.	gr.
75	62 61	55.5	0.450	4.90	4.41	0.526	479.7 479.9	488.2 488.4	496.8	505.3 505.5	513.9 514.1	522.4 522.6	531.0 531.2
	60	52.5	0.425	4.43	4.88	0.476	480.0	488.5	497.1	505.6	514.2	522.7	531.3
350	59	51.0	0.386	4.21	5.10	0.452	480.1	488.6	497.2	505.7	514.3	522.8	531.4
1.7	58	49.5	0.367	4.00	5.31	0.429	480.3	488.8	497.4	505.9	514.5	523.0	531.6
-	57	48.0	0.349	3.79	5.52	0.407	480.4	488.9	497.5	506.0	514.6	523.1	531.7
12.3	56	46.5	0.331	3.60	5.71	0.387	480.5	489.0	497.6	506.1	514.7	523.2	531.8
3.50	55	45.0	0.315	3.42	5.89	0.367	480.6	489.1	497.7	506.2	514.8	523.3	531.9
	54	43.5	0.299	3.25	6.06	0.349	480.7	489.2	497.8	506.3	514.9	523.4	532.0
	53	42.0	0.283	3.09	6.22	0.332	480.8	489.3	497.9	506.4	515.0	523.5	532.1
4	52	40.5	0.269	2.93	6.38	0.315	480.8	489.3	497.9	506.4	515.0	523.5	532.1
安元 日	51	39.0	0.255	2.78	6.53	0.299	480.9	489.4	498.0	506.5	515.1	523.6	532.2
1	50	37.5	0.242	2.64	6.67	0.284	481.0	489.5	498.1	506.6	515.2	523.7	532.3
-	49	36.0	0.230	2.51	6.80	0.270	481.1	489.6	498.2	506.7	515.3	523.8	532.4
L.	48	34.5	0.218	2.39	6.92	0.257	481.2	489.7	498.3	506.8	515.4	523.9	532.5
								Laure				1 3 6	
76	76	76.0	0.882	9.60	0.00	1.000	476.3	484.8	493.3	501.8	510.3	518.8	527.8
10	75	74.5	0.840	9.14	0.46	0.952	476.6	485.1	493.6	502.1	510.6	519.1	527.6
	74	73.0	0.801	8.71	0.89	0.907	476.8	485.3	493.8	502.3	510.8	519.3	527.8
4.55	73	71.5	0.763	8.30	1.30	0.865	477.0	485.5	494.0	502.6	511.1	519.6	528.1
6.4	72	70.0	0.727	7.90	1.70	0.823	477.2	485.7	494.3	502.8	511.3	519.8	528.3
	71	68.5	0.692	7.53	2.07	0.784	477.4	485.9	494.5	503.0	511.5	520.0	528.5
9.44	70	67.0	0.659	7.17	2.43	0.747	477.6	486.1	494.7	503.2	511.7	520.2	528.7
9,20	69	65.5	0.628	6.83	2.77	0.711	477.8	486.3	494.9	503.4	511.9	520.4	528.9
2000	68	64.0	0.597	6.49	3.11	0.676	477.9	486.4	495.0	503.6	512.1	520.6	529.2
1000	67	62.5	0.568	6.16	3.44	0.642	478.1	486.6	465.2	503.8	512.3	520.8	529.4
201	66	61.0	0.541	5.88	3.72	0.613	478.2	486.7	495.3	503.9	512.4	520.9	529.5
1837	65	59.5	0.515	5.59	4.01	0.582	478.3	486.8	495.4	504.0	512.5	521.0	529.6
	64	58.0	0.489	5.31	4.29	0.553	478.5	487.0	495.6	504.2	512.7	521.2	529.8
	63	56.5	0.465	5.06	4.54	0.527	478.6	487.1	495.7	504.3	512.8	521.3	529.9
- 45	62	55.0	0.442	4.81	4.79	0.501	478.8	487.3	495.9	504.5	513.0	521.5	530.1
22.34	61	53.5	0.421	4.57	5.03	0.476	479.0	487.5	496.1	504.7	513.2	521.7	530.3
1	60	52.0	0.400	4.34	5.26	0.452	479.1	487.6	496.2	504.8	513.3	521.8	530.4
	59	50.5	0.380	4.13	5.47	0.430	499.2	487.7	496.3	504.9	513.4	521.9	530.
	58	49.0	0.361	3.92	5.68	0.408	499.3	487.8	496.4	505.0	513.5	522.0	530.6
	57	47.5	0.343	3.73	5.87	0.389	499.4	487.9	496.5	505.1	513.6	522.1	530.7
	56	46.0	0.326	3.54	6.06	0.369	499.5	488.0	496.6	505.2	513.7	522.2	530.8
	55	44.5	0.309	3.36	6.24	0.351	499.6	488.1	496.7	505.3	513.8	522.3	530.9
,	54	43.0		3.19	4 2 3	0.332	499.7		Maria de Santo		Carried Street	522.4	531.0
	53	41.5	0.279	3.03	1 1000 1000	0.316	499.8	1	Taring the same of		a 3,50-30,67	522.5	531.
188	52	40.0	0.264	1	The Late of the la	0.301	499.9	Total Control	The second second		Activities and the second	522.6	531.2
1	51	38.5	0.251	2.73	6.87	0.284	500.0	4	1	F			531.5
	50	37.0			100000000000000000000000000000000000000	0.269	500.1		The second second	1007	514.3	522.8	531.4
10:1	49	35.5	0.226	2.46	7.14	0.256	500.2	488.7	497.3	505.9	514.4	522.9	531.5

Res	ding	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grain	ns of a Cu	ıbic Foot	of Air.	
mon	neter,	of Dew-	of Vapor in	In a Cubic	for Sat'n	midity, Satura- tion =		Height o	of the Ba	rometer i	n Englis	h Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.		1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
77	77	77.0	0.910	9.89	0.00	1.000 0.953	475.3	483.8	492.3	500.8	509.2 509.4	517.7	526.2 526.4
513	76 75	74.0	0.827	8.99	0.90	0.909	475.7	484.2	492.7	501.2	509.6	518.1	526.6
	74	72.5	0.787	8.57	1.32	0.867	475.9	484.4	492.9	501.4	509.9	518.4	526.9
	73	71.0	0.751	8.15	1.74	0.824	476.1	484.6	493.1	501.6	510.1	518.6	527.1
	72	69.5	0.715	7.77	2.12	0.786	476.3	484.8	493.3	501.8	510.3	518.8	527.3
	71	68.0	0.681	7.40	2.49	0.748	476.5	485.0	493.5	502.0	510.5	519.0	527.5
	70	66.5	0.648	7.04	2.85	0.712	476.7	485.2	493.7	502.2	510.7	519.2	527.7
	69	65.0	0.617	6.71	3.18	0.678	476.9	485.4	493.9	502.4	510.9	519.4	527.9
E	68	63.5	0.588	6.37	3.52	0.644	477.0	485.6	494.1	502.6	511.1	519.6	528.1
196	67	62.0	0.559	6.06	3.83	0.613	477.2	485.8	494.3	502.8	511.3	519.8	528.3
	66	60.5	0.532	5.77	4.12	0.583	477.4	486.0	494.5	503.0	511.5	520.0	528.5
100	65	59.0	0.506	5.49	4.40	0.556	477.5	486.1	494.6	503.1	511.6	520.1	528.6
	64	57.5	0.481	5.21	4.68	0.527	477.7	486.3	494.8	503.3	511.8	520.3	528.8
	63	56.0	0.458	4.96	4.93	0.501	477.9	486.5	495.0	503.5	512.0	520.5	529.0
	62	54.5	0.435	4.70	5.19	0.476	478.0	486.6	495.1	503.7	512.1	520.6	529.1
ATE	61	53.0	0.414	4.49	5.40	0.454	478.0	486.6	495.1	503.7	512.2	520.7	529.3
100	60	51.5	0.393	4.26	5.63	0.431	478.1	486.7	495.2	503.8	512.3	520.8	529.4
	59	50.0	0.373	4.05	5.84	0.410	478.2	486.8	495.3	503.9	512.4	520.9	529.5
	58	48.5	0.355	3.85	6.04	0.389	478.3	486.9	495.4	504.0	512.5	521.0	529.6
	57	47.0	0.337	3.65	6.24	0.369	478.5	487.1	495.6	504.1	512.7	521.2	529.8
	56	45.5	0.320	3.47	6.42	0.351	478.6	487.2	495.7	504.2	512.8	521.3	529.9
	55	44.0	0.304	3.29	6.60	0.333	478.7	487.3	495.8	504.3	512.9	521.4	530.0
	54	42.5	0.288	3.13	6.76	0.317	478.8	487.4	495.9	504.4	513.0	521.5	530.1
	53	41.0	0.274	2.97	6.92	0.301	478.9	487.5	496.0	504.5	513.1	521.6	530.2
	52	39.5	0.260	2.82	7.07	0.285	479.0	487.6	496.1	504.6	513.2	521.7	530.3
	51 50	38.0	0.246	2.67 2.53	7.22	0.270	479.1	487.7	496.2	504.7	513.3 513.3	521.8 521.8	530.4
	30	30.5	0.204	2.00	1.50	0.230	413.1	401.1	430.2	504.7	310.0	521.0	330.4
	THE				OF SE	**	70	Barrier 1	100	dir Tal	10 Ta	0.00	
78	78	78.0	0.940	10.19	0.00	1.000	474.1	482.5	491.0	499.4	508.0	516.4	524.9
L Polity	77	76.5	0.896	9.72	0.47	0.954	474.4	482.9	491.4	499.9	508.3	516.7	525.2
1	76	75.0	0.854	9.25	0.94	0.908	474.7	483.2	491.6	500.1	508.6	517.1	525.6
	75	73.5	0.814	8.82	1.37	0.865	474.9	483.4	491.8	500.3	508.8	517.3	525.8
	74	72.0	0.776	8.40	1.79	0.824	475.2	483.7	492.1	500.6	509.1	517.6	526.1
721	73 72	70.5 69.0	0.739	8.00	The state of the s	0.785	475.4	483.9	492.3	500.8	500.3	517.8	526.3
		05.0	0.704	7.62	2.57	0.748	475.6	484.1	492.5	501.0	509.5	518.0	526.5
	71	67.5	0.670	7.25	2.94	0.711	475.8	484.3		501.2	509.7	518.2	526.7
	70	66.0	0.638	6.91	1	0.678	475.9	484.4		501.4	509.9	518.4	526.9
	69	64.5	0.607	6.58		0.646	476.1	484.6	1	501.6	510.1	518.6	527.1
	68	63.0	0.578	6.26	1	0.614	476.3	484.8	1	501.8	510.3	1	527.3
	67	61.5	0.550		4.23	0.585	476.4	484.9	493.4	501.9	510.4	1 4 1 1 1 1	527.4
	66	60.0	0.523	1 - F - 2 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	4.53	0.555	476.6			502.1	510.6	The second second	527.6
	1 09	58.5	0.498	5.38	4.81	0.528	476.8	485.3	493.8	502.3	510.8	519.3	527.8

	ading Ther-	Temp.	Force	Wei of V	-	Hu-		Weight	t in Grain	ns of a Cu	ibie Foot	of Air.	
mo	meter,	of Dew- Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	of the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	in. 28.0	in. 28.5	in. 29.0	29.5	30.0	in. 30.5	in. 31.0
0	0	0	in.	gr.	gr.	0.500	gr.	gr.	gr.	gr.	gr.	gr.	gr.
78	65 64	58.5 57.0	0.498	5.38 5.12	4.81 5.07	0.528	476.8 476.8	485.3	493.8	502.3 502.4	510.8 510.9	519.3 519.4	527.8 527.9
7-10	63	55.5	0.450	4.88	5.31	0.302	476.9	485.4	494.0	502.4	511.0	519.5	528.0
	62	54.0	0.428	4.63	5.56	0.454	477.1	485.6	494.2	502.7	511.2	519.7	528.2
7	61	52.5	0.407	4.40	5.79	0.432	477.2	485.7	494.3	502.8	511.3	519.8	528.3
	60	51.0	0.386	4.18	6.01	0.409	477.3	485.8	494.4	502.9	511.4	519.9	528.4
1.0	59	49.5	0.367	3.98	6.21	0.391	477.4	485.9	494.5	503.0	511.5	520.0	528.5
	58	48.0	0.349	3.78	6.41	0.371	477.5	486.0	494.6	503.1	511.6	520.1	528.6
1	57	46.5	0.331	3.59	6.60	0.352	477.6	486.1	494.7	503.2	511.7	520.2	528.7
	56	45.0	0.315	3.41	6.78	0.335	477.8	486.3	494.8	503.3	511.9	520.4	528.9
379	55	43.5	0.299	3.24	6.95	0.318	477.9	486.4	494.9	503.4	512.0	520.5	529.0
-	54	42.0	0.283	3.07	7.12	0.301	478.0	486.5	495.0	503.5	512.1	520.6	529.1
	53	40.5	0.269	2.92	7.27	0.287	478.1	486.5	495.0	503.5	512.1	520.6	529.1
	52	39.0	0.255	2.77	7.42	0.272	478.2	486.6	495.1	503.6	512.2	520.7	529.2
	51	37.5	0.242	2.63	7.56	0.258	478.3	486.7	495.2	503.7	512.3	520.8	529.3
0,30	139	S S S S	MI LO	813	20 3	2 15	The Late	Life H	70 H 1	7 15911	10. 00		
79	79	79.0	0.970	10.50	0.00	1.000	473.1	481.5	490.0	498.4	506.9	515.3	523.8
	78	77.5	0.925	10.01	0.49	0.953	473.4	481.8	490.3	498.7	507.2	515.6	524.1
	77	76.0	0.882	9.54	0.96	0.909	473.7	482.1	490.6	499.0	507.5	515.9	524.4
	76	74.5	0.840	9.10	1.40	0.867	473.8	482.2	490.7	499.2	507.7	516.2	524.7
	75	73.0	0.801	8.66	1.84	0.825	474.0	482.4	490.9	499.4	507.9	516.4	524.9
177	74	71.5	0.763	8.25	2.25	0.786	474.3	482.7	491.2	499.7	508.2	516.7	525.2
5.55	73	70.0	0.727	7.86	2.64	0.749	474.5	482.9	491.4	499.9	508.4	516.9	525.4
100	72	68.5	0.692	7.48	3.02	0.712	474.7	483.1	491.6	500.1	508.6	517.1	525.6
1	71	67.0	0.659	7.12	Land -	0.678	474.9	483.4	491.9	500.4	508.8	517.3	525.8
130	70	65.5	0.628	6.79	3.71	0.647	475.1	483.6	462.1	500.6	509.0	517.5	526.0
	69	64.0	0.597	6.45	4.05	0.614	475.3	483.8	492.3	500.8	509.2	517.7	526.2
	68	62.5	0.568	6.14	4.36	0.585	475.4	483.9	492.4	500.9	509.3	517.8	526.3
	67	61.0	0.541	5.84	1	0.556	475.6	484.1	492.6	501.1	509.5	518.0	526.5
	66	59.5	0.515	5.55	4.95	0.529	475.7	484.2	492.7	501.2	509.6	518.1	526.6
1	65	58.0	0.489	5.28	5.22	0.503	475.8	484.3	492.8	501.3	509.8	518.3	526.8
	64	56.5	0.465	5.02		0.478	476.0	484.5	493.0	501.5	510.0	518.5	527.0
1	63	55.0	0.442	4.78	1	0.455	476.1	484.6	493.1	501.6	510.1	518.6	527.1
	62	53.5	0.421	4.54	5.96	0.432	476.3	484.8	493.3	501.8	510.3	518.8	527.3
6.0	61	52.0	0.400	4.31	6.19	0.410	476.4	484.9	493.4	501.9	510.4	518.9	527.4
0 3	60	50.5	0.380	4.10		0.390	476.5	485.0		502.0	510.5	519.0	527.5
	59	49.0	0.361	3.90	6.60	0.371	476.6	485.1	493.6	502.1	510.6	519.1	527.6
	58	47.5	0.343	3.71	6.79	0.353	476.7	485.2	493.7	502.2	510.7	519.2	527.7
	57	46.0	0.326	3.52	6.98	0.335	476.8		The second second	502.3	510.8	519.3	527.8
	56	44.5	0.309	3.34	1	0.318	476.9	485.4	493.9	502.4	510.9	519.4	527.9
	55	43.0	0.293	3.17		0.301	477.0		100	502.5	511.0	519.5	528.0
	54	41.5	0.279	3.01		0.287	477.1		100000	502.6	511.1	519.6	528.1
	53	40.0	0.264	1 200	7.64	The second second	477.2		- C-100 - 100 - 100	502.7	511.2	519.7	528.2
	52	38.5	0.251	2.72	7.78	0.260	477.3	485.8	494.3	502.8	511.3	519.8	528.3

	eading	m.	Force		ight apor	Hu-		Weight	t in Grain	ıs of a Cu	ıbic Foot	of Air.			
m	Ther- ometer, Fahr.	Temp. of Dew-	of Vapor	In a for Cubic Sat'r		or Satura-	Height of the Barometer in English Inches.								
Dry	. Wet.	Point, Fahr.	English Inches.	Foot of Air.		tion = 1.000.	in. 28.0	in. 28.5	in. 29.0	in. 29.5	30.0	30.5	31.0		
0	0	0	in.	gr.	gr.	7 100	gr.	gr.	gr.	gr.	gr.	gr.	gr		
80		80.0	1.001	10.81	0.00	1.000	472.0	480.4	488.9	497.3	505.7	514.1	522.6		
	79	78.5	0.955	10.31	0.50	0.954	472.3	480.7	489.1	497.5	506.0	514.4	522.9		
	78	77.0	0.910	9.83	0.98	0.909	472.5	480.9	489.4	497.9	506.3	514.7	523.2		
	77	75.5	0.868	9.37	1.44	0.867	472.7	481.1	489.6	498.1	506.5	514.9	523.4		
	76	74.0	0.827	8.93	1.88	0.826	473.0	481.4	489.9	498.4	506.8	515.2	523.7		
	75	72.5	0.787	8.50	2.31	0.786	473.2	481.6	490.1	498.6	507.0	515.4	523.9		
	74	71.0	0.751	8.11	2.70	0.750	473.4	481.8	490.3	498.8	507.2	515.6	524.1		
	73	69.5	0.715	7.71	3.10	0.713	473.6	482.1	490.6	499.1	507.5	515.9	524.4		
	72	68.0	0.681	7.35	3.46	0.680	473.8	482.3	490.8	499.3	507.7	516.1	524.4		
	71	66.5	0.648	6.99	3.82	0.647	474.0	482.5	491.0	499.5	507.9	516.3	524.8		
	70	65.0	0.617	6.66	4.15	0.616	474.2	482.7	491.2	499.7	508.1	516.5	525.0		
	69	63.5	0.588	6.33	4.48	0.586	474.4	482.9	491.4	499.9	508.3	516.7	525.2		
1	68	62.0	0.559	6.03	4.78	0.558	474.5	483.0	491.5	500.0	508.4	516.8	525.3		
	67	60.5	0.532	5.74	5.07	0.531	474.7	483.2	491.7	500.2	508.6	517.0	525.5		
								1					1		
	66	59.0	0.506	5.45	5.36	0.504	474.9	483.4	491.9	500.4	508.8	517.2	525.7		
	65	57.5	0.481	5.18	5.63	0.479	475.0	483.5	492.0	500.5	508.9	517.3	525.8		
.	64	56.0	0.458	4.93	5.96	0.456	475.2	483.7	492.2	500.7	509.1	517.5	526.0		
	63	54.5	0.435	4.69	6.12	0.434	475.3	483.8	492.3	500.8	509.2	517.6	526.1		
	62	53.0 51.5	0.414	4.46	6.35	0.413	475.4	483.9	492.4	500.9	509.3	517.7	526.2		
	61	50.0	0.393	4.23	6.58	0.391 0.372	475.5	484.1	492.5	501.0	509.4	517.8 517.9	526.3 526.4		
	60	30.0	0.075	4.02	0.15	0.512	475.0	404.1	492.0	501.1	505.5	517.9	340.4		
	59	48.5	0.355	3.82	6.99	0.353	475.7	484.2	492.7	501.2	509.6	518.0	526.5		
	58	47.0	0.337	3.63	7.18	0.336	475.9	484.4	492.9	501.4	509.8	518.2	526.7		
	57	45.5	0.320	3.45	7.36	0.319	476.0	484.5	493.1	501.5	509.9	518.3	526.8		
	56	44.0	0.304	3.27	7.54	0.302	476.1	484.6	493.2	501.6	510.0	518.4	526.9		
	55	42.5	0.288	3.11	7.70	0.288	476.2	484.7	493.3	501.7	510.1	518.5	527.0		
	54	41.0	0.274	2.96	7.85	0.274	476.3	484.8	493.4	501.8	510.2	518.6	527.1		
	53	39.5	0.260	2.82	7.99	0.261	476.3	484.8	493.4	501.8	510.2	518.6	527.1		
140	1		1 1	K E			Ta es	V. 18	130	46	A Ad	170			
81	81	81.0	1.034	11.14	0.00	1.000	471.0	479.4	487.8	496.2	504.6	513.0	521.4		
	80	79.5	0.986	10.62	0.52	0.953	471.3	479.7	488.1	496.5	504.9	513.3	521.7		
	79	78.0	0.940	10.13	1.01	0.910	471.5	479.9	488.4	496.8	505.2	513.6	522.1		
	78	76.5	0.896	9.65	1.49	0.866	471.7	480.1	488.6	497.0	505.4	513.8 514.1	522.3		
	76	73.5	0.854	9.20	1.94 2.37	0.826	472.0 472.2	480.4	488.9	497.3	505.7	514.1	522.6 522.8		
	75	72.0	0.776	77. (2	2.79	0.750	472.5	480.9		497.8	506.2	172 100	523.1		
,			31110	0.00	4.10	31100	112.0	400.9	100.4	101.0	500.2	011.0	020.1		
	74	70.5	0.739	7.95	3.19	0.713	472.6	481.0	489.5	497.9	506.4	514.8	523.3		
	73	69.0	0.704	7.57	1027 19 19	0.680	472.8	481.2	489.7	498.1	506.6	515.0	523.5		
	72	67.5	0.670	7.21	3.93	0.647	473.0	481.4	489.9	498.3	506.8	515.2	523.7		
	71	66.0	0.638	6.87	4.27	0.617	473.2	481.6	490.1	498.5	507.0	515.4	523.9		
	70	64.5	0.607	6.54	The second second	0.587	473.4	481.8	490.3	498.7	507.2	515.6	524.1		
	69	63.0	0.578		4.92	0.558	473.6	482.0	490.5	498.9	507.4	515.8	524.3		
	68	61.5	0.550	5.92	5.22	0.531	473.7	482.2	490.7	499.1	507.6	516.0	524.5		

of	ding Ther-	Temp.	Force of	Wei of V	ght apor Regd.	Hu-	7)									
	neter,	of Dew- Point,	Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	f the Bar	rometer i	English	Inches.				
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	30.0	30.5	in. 31.0			
0	0	0	in. 0.550	gr. 5.92	gr.	0.531	gr.	gr.	gr.	gr.	gr.	gr.	gr.			
81	68 67	61.5	0.523	5.62	5.22 5.52	0.505	473.7	482.2	490.7	499.1	507.6	516.0	524.6			
	66	58.5	0.498	5.31	5.83	0.477	474.0	482.5	491.0	499.4	507.9	516.3	524.8			
	65	57.0	0.473	5.08	6.06	0.456	474.1	482.6	491.1	499.5	508.0	516.4	524.			
100	64	55.5	0.450	4.84	6.30	0.434	474.3	482.8	491.3	499.7	508.2	516.6	525.			
	63	54.0	0.428	4.60	6.54	0.413	474.4	482.9	491.4	499.8	508.3	516.7	525.			
1.17	62	52.5	0.407	4.37	6.77	0.392	474.5	483.0	491.5	499.9	508.4	516.8	525.			
T.	61	51.0	0.206	4.75	6.00	0 272	1716	400 1	401.6	500.0	E00 E	E16.0	505			
	61		0.386	4.15	100000	0.373	474.6	483.1	491.6	500.0	508.5	516.9	525.			
	60	49.5	0.367	3.95	7.19	0.355	474.7	483.2	491.7	500.1	508.6	517.0	525.			
ZO S	59	1	0.349	3.75			474.9	483.4	491.9	500.3	508.8	517.2	525.			
Maril:	58	46.5	0.331	3.56	1	0.320	475.0	483.5	492.0	500.4	508.9	517.3	525. 525.			
	57		0.315	3.38			475.1	483.6	492.1	500.5	Total Control	517.4	1			
	56	43.5	0.299	77. 1 77.	7.93	0.289	475.2	483.7	492.2	500.6	509.1	517.5	526.			
	55	42.0	0.283	3.05		0.274	475.3	483.8	492.3	500.7	509.2	517.6	526.			
	54	40.5	0.269	2.90	8.24	0.260	475.3	483.8	492.3	500.7	509.2	517.6	526.			
						001		19	. The second				1.4			
82	82	82.0	1.067	11.47	0.00	1.000	470.0	478.4	486.8	495.2	503.5	511.9	520.			
	81	80.5	1.017	10.94	0.53	0.954	470.3	478.7	487.0	495.4	503.8	512.2	520.			
	80	79.0	0.970	10.44	1.03	0.910	470.6	479.0	487.3	495.7	504.1	512.5	520.			
	79	77.5	0.925	9.95	1.52	0.868	470.7	479.1	487.5	495.9	504.3	512.7	521.			
	78	76.0	0.882	9.49	1.98	0.827	471.0	479.4	487.8	496.2	504.6	513.0	521.			
	77	74.5	0.840	9.03	2.44	0.787	471.2	479.6	488.0	496.4	504.8	513.2	521.			
	76	73.0	0.801	8.60	2.87	0.750	471.5	479.9	488.3	496.7	505.1	513.5	521.			
	75	71.5	0.763	8.19	3.28	0.714	471.6	480.0	488.5	496.9	505.3	513.7	522.			
	74	70.0	0.727	7.81	17.00	0.681	471.8	480.2	488.6	497.1	505.5	513.9	522.			
	73	68.5	0.692	7.43	1000	0.648	472.0	480.4	488.8	497.3	505.7	514.1	522.			
	72	67.0	0.659	7.08	POCC P	0.618	472.2	480.6	489.0	497.5	505.9	514.3	522.			
	71	65.5	0.628	6.75	197715	0.588	472.4	480.8	489.2	497.7	506.1	514.5	523.			
	70	64.0	0.597	6.41	COROLE	0.559	472.5	480.8	489.4	497.9	506.3	514.7	523.			
	69	62.5	0.568	6.10		0.532	472.6	481.0	489.5	498.0	506.4	514.8	523.			
	68	61.0	0.541	5.81	5.66	0.507	472.8	481.2	489.7	498.2	506.6	515.0	523.			
	67	59.5	0.515	5.52		0.481	473.0	481.4	489.9	498.4	506.8	515.2	523			
	66	58.0	0.489	5.25		0.458	473.1	481.5	490.0	498.5	506.9	515.3	523.			
	65	56.5	0.465	4.99	The second second	0.435	473.2	481.6	490.1	498.6	507.0	515.4	523.			
	64	55.0	0.442	4.75		0.414	473.4	481.8	490.3	498.8	507.2	515.6	524			
	63	53.5	0.421	4.51	100000000000000000000000000000000000000	0.393	473.5	482.0	490.5	499.0	507.4	515.8	524.			
	62	52.0	0.400			1	473.6	482.1	490.6	499.1	507.5	515.9	524.			
2019	61	50.5	0.380	4.08	7.39	0.356	473.7	482.2	490.7	499.2	507.6	516.0	524.			
	60	49.0	0.361	3.87	1	0.337	473.8		490.8	499.3	507.7	516.1	524			
	59	47.5	0.343	3.68	120	0.320	473.9		490.9	499.4	507.7	516.2	524			
	58	46.0	0.326	3.50		0.305	474.0	-	491.0	499.4	507.9	516.3	524.			
4.1	57	44.5	0.309	3.32		0.303	474.1		491.1	499.6	508.0	516.4	524			
15	56	43.0	0.293		8.32	0.239	474.2		491.1	499.0	508.1	516.5	524.			
	55	41.5		1	8.48				491.3				1			

	ading Ther-	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grain	ns of a Cu	abic Foot	of Air.	George Co.
mor	meter,	of Dew-	of Vapor in	In a Cubic	for Sat'n.	midity, Satura-		Height o	of the Bar	rometer i	n Englis	h Inches.	SALT.
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	tion = 1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
83	83	83.0	1.101	11.82	0.00	0.953	468.8	477.2	485.5	493.9	502.3	510.6 511.0	519.0 519.4
100	82	81.5	1.001	10.75	1.07	0.909	469.4	477.8	486.1	494.5	502.9	511.3	519.7
	81 80	78.5	0.955	10.25	1.57	0.868	469.7	478.1	486.4	494.8	503.2	511.6	520.0
13	79	77.0	0.910	9.78	2.04	0.828	470.0	478.4	486.7	495.1	503.5	511.9	520.3
	78	75.5	0.868	9.31	2.51	0.786	470.3	478.7	487.0	495.4	503.8	512.2	520.6
	77	74.0	0.827	8.88	2.94	0.751	470.5	478.9	487.2	495.6	504.0	512.4	520.8
		112		_ 1119									
9.0	76	72.5	0.787	8.45	3.37	0.715	470.6	479.0	487.4	495.8	504.2	512.6	521.0
	75	71.0	0.751	8.05	3.77	0.681	470.8	479.2	487.6	496.0	504.4	512.8	521.2
1000	74	69.5	0.715	7.66	4.16	0.647	471.0	479.4	487.8	496.2	504.6	513.0	521.4
133	73	68.0	0.681	7.30	4.52	0.618	471.2	479.6	488.0	496.4	504.8	513.2	521.6
	72	66.5	0.648	6.95	4.87	0.588	471.4	479.8	488.2	496.6	505.0	513.4	521.8
25	71 70	65.0	0.617	6.62	5.20 5.53	0.560	471.6	480.0	488.4	496.8 497.0	505.2 505.4	513.6 513.8	522.0 522.3
100	70	00.0	0.000	0.23	0.00	0.555	4/1./	400.1	400.0	497.0	505.4	313.0	022.0
	69	62.0	0.559	5.99	5.83	0.507	471.9	480.3	488.7	497.2	505.6	514.0	522.5
	68	60.5	0.532	5.70	6.12	0.482	472.0	480.4	488.8	497.3	505.7	514.1	522.6
	67	59.0	0.506	5.42	6.40	0.459	472.2	480.6	489.0	497.5	505.9	514.3	522.8
9,4	66	57.5	0.481	5.15	6.67	0.435	472.4	480.8	489.2	497.7	506.1	514.5	523.0
-	65	56.0	0.458	4.90	6.92	0.414	472.4	480.8	489.3	497.8	506.2	514.6	523.1
59	64	54.5	0.435	4.66	7.18	0.394	472.5	480.9	489.4	497.9	506.3	514.7	523.2
	63	53.0	0.414	4.43	7.39	0.375	472.7	481.1	489.6	498.1	506.5	514.9	523.4
			10 200	US LES	28 0	200	C. C. C. C.	5.0	Le le	9 100		2 02	
	62	51.5	0.393	4.21	7.61	0.356	472.8	481.2	489.7	498.2	506.6	515.0	523.5
100	61	50.0	0.373	4.00	7.82	0.339	472.9	481.3	489.8	498.3	506.7	515.1	523.6
	60	48.5	0.355	3.80	8.02	0.322	473.1	481.4	489.9	498.4	506.8	515.2	523.7 523.8
1	59 58	45.5	0.320	3.60	8.22	0.305	473.2 473.3	481.5 481.6	490.0	498.5 498.6	506.9	515.3 515.4	523.9
8.5	57	44.0	0.304	3.25	8.57	0.276	473.4	481.7	490.2	498.7	507.1	515.5	524.0
	56	42.5	0.288	3.09	8.73	0.261	473.5	481.8	490.3	498.8	507.2	515.6	524.1
1						-	19 (0				-U U.	0 1 13	
			To Line	ER LES		MA PR	100 P	6.0	0.0 913	G 1284	-0.10	TO SE	1 13
84	84	84.0	1.136	12.17	0.00	1.000	467.8	476.2	484.5	492.7	501.2	509.6	517.9
	83	82.5	1.083	11.61	0.56	0.954	468.1	476.4	484.8	493.2	501.5	509.8	518.2
1	82	81.0	1.034	11.07	1.10	0.910	468.4	476.7	485.1	493.5	501.8	510.1	518.5
124	81	79.5	0.986	10.55	1.62	0.867	468.6	476.9	485.4	493.7	502.1	510.5	518.8
18	80	78.0	0.940	10.07	2.10	0.827	468.9	477.3	485.7	494.0	502.4	510.8	519.1
192	79	76.5	0.896	9.59	2.58	0.788	469.1	477.5	485.9	494.2	502.6	511.0	519.3
	78	75.0	0.854	9.14	3.03	0.751	469.4	477.8	486.1	494.5	502.9	511.3	519.7
	22	P(0 =	0014	0 ~~	0 10	0	100 0	400.0	400.0	40 : -	F00 -		270.0
	77 76	73.5	0.814	8.71		0.716	469.6	478.0	486.3	494.7	503.1	511.5	519.9
	75	70.5	0.776	8.30 7.90	3.87	0.682	469.8	478.2		494.9	503.3	511.7 512.0	520.1 520.4
	74	69.0	0.704	7.53		0.619	470.1	478.5 478.7	486.8	495.2 495.4	503.8	512.0	520.4
	73	67.5	0.670	7.17	5.00	0.589	470.5	478.9	487.2	495.4	504.0	512.4	520.8
	72	66.0	0.638	6.83		0.561	470.6			495.8	504.2	512.6	521.0
1	71	64.5	0.607	- 172	5.67	0.534		479.1		495.9			

	ading Ther-	Temp.	Force		apor	Hu-	W	Weigh	t in Grain	as of a Cu	ibic Foot	of Air.	
mo	meter, ahr.	of Dew- Point,	Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	of the Ba	rometer i	n English	Inches.	What.
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in. 0.607	gr.	gr.	0 594	gr.	gr.	gr.	gr.	gr.	gr.	gr. 521.1
84	71 70	64.5	0.578	6.50		0.534	470.7	479.1	487.5	495.9	504.3	512.7 512.9	521.3
	69	61.5	0.550	5.87	777	0.308	1	479.5	487.9	496.3	504.7	513.1	521.
	68	60.0	0.523	5.59	6.58	0.459	471.1	479.6	488.0	496.4	504.8	513.2	521.
	67	58.5	0.498	5.31		0.436	471.4	479.8	488.2	496.6	505.0	513.4	521.8
	66	57.0	0.473	5.05	Line Control	0.415	471.6	480.0	488.3	496.7	505.2	513.6	522.
	65	55.5	0.450	4.81	1	0.395	471.6	480.0	488.4	496.8	505.3	513.7	522.2
	00	00.0	0.100	4.01		0.000	411.0	200.0	400.4	200.0	000.0	010	022
	64	54.0	0.428	4.57	7.60	0.375	471.7	480.1	488.5	496.9	505.4	513.8	522.3
	63	52.5	0.407	4.35	7.82	0.357	471.8	480.2	488.6	497.0	505.5	513.9	522.4
	62	51.0	0.386	4.13	8.04	0.339	471.9	480.4	488.8	497.2	505.7	514.0	522.
	61	49.5	0.367	3.93	8.24	0.323	472.1	480.5	488.9	497.3	505.8	514.1	522.
	60	48.0	0.349	3.73	8.44	0.306	472.2	480.6	489.0	497.4	505.9	514.2	522.
	59	46.5	0.331	3.55	8.62	0.292	472.3	480.7	489.1	497.5	506.0	514.3	522.8
	58	45.0	0.315	3.37	8.80	0.277	472.4	480.8	489.2	497.6	506.1	514.4	522.
	57	43.5	0.299	3.20	8.97	0.263	472.5	480.9	489.3	497.7	506.2	514.5	523.0
	93 Q		Mid La	ME TO	this c	7000	Santa	# 62 V To	t shift	2.	100 TE	100	
	in la		norte.	Take 1	de la	in the late	110	F-72	MAL	and the	175 12		
85	85	85.0	1.171	12.53	TO COLLEGE	1.000	466.8	475.2	483.5	491.8	500.1	508.5	516.
	84	83.5	1.118	11.95	renne	0.954	467.1	475.4	483.7	492.1	500.4	508.7	517.
	83	82.0	1.067	11.40	117752	0.910	467.3	475.6	484.0	492.4	500.7	509.0	517.
	82	80.5	1.017	10.87	1,1900000000000000000000000000000000000	0.868	467.6	475.9	484.3	492.7	501.0	509.3	517.
	81	79.0	0.970	10.38		0.829	467.8	476.1	484.5	492.9	501.2	509.5	517.
	80	77.5	0.925	9.89	1 22	0.789	468.1	476.4	484.8	493.2	501.5	509.8	518.
	79	76.0	0.882	9.43	3.10	0.753	468.4	476.7	485.1	493.5	501.8	510.1	518.
	78	74.5	0.840	8.98	3.55	0.717	468.6	476.9	485.3	493.7	502.0	510.3	518.
	77	73.0	0.801	8.55	1 500	0.682	468.7	477.1	485.5	493.9	502.2	510.5	518.
	76	71.5	0.763	8.15	METAL I	0.650	469.0	477.4	485.8	494.2	502.5	510.8	519.
N.	75	70.0	0.727	7.76		0.619	469.2	477.6	486.0	494.4	502.7	511.0	519.
	74	68.5	0.692	7.39	100	0.589	469.4	477.8	486.2	494.6	502.9	511.2	519.
	73	67.0	0.659	7.04	G. A.	0.562	469.7	478.1	486.5	494.9	503.2	511.5	519.
	72	65.5	0.628	6.71		0.536	469.9	478.3	486.7	495.1	503.4	511.7	520.
									-				
	'71	64.0	0.597	6.37	6.16	0.508	470.1	478.5	486.9	495.3	503.6	511.9	520.
Sign	70	62.5	0.568	6.07	6.46	0.484	470.3	478.7	487.1	495.5	503.8	512.1	520.
Paris	69	61.0	0.541	5.77	6.76	0.460	470.5	478.9	487.2	495.6	504.0	512.4	520.
80	68	59.5	0.515	5.48	7.05	0.437	470.6	479.0	487.3	495.7	504.1	513.5	520.
680	67	58.0	0.489	5.21	7.32	0.415	470.6	479.0	487.4	495.8	504.2	512.6	521.
	.66	56.5	0.465	4.96		0.396	470.7	479.1	487.5	495.9	504.3	512.7	521.
100	65	55.0	0.442	4.72	7.81	0.377	470.8	479.2	487.6	496.0	504.4	512.8	521.
I a			0 10-			0.000	4000	1000	100	100	-01-	***	
1	64	53.5	0.421	4.49	A COLUMN TO SE	1 4 5 7 F. A	470.9			496.1	504.5	512.9	521.
	63	52.0	Charles of the Control of the Contro		100000000000000000000000000000000000000	1	471.1	1	1	496.3	504.7	513.1	521.
M.	62	50.5	0.380	1	100000	The second second	471.2			496.4	504.8	513.2	521.
139	61	49.0	0.361	3.85	1000000	10 THO BUT	471.3			496.5	504.9	513.3	521.
	60	47.5	0.343	3.66		0.292	471.4	1	110000	496.6	505.0	513.4	521.
33	59	46.0	The second second			A CAST COLOR	471.5	1000000	The second second	496.7	505.1	513.5	521.
2.8	58	44.5	0.309	3.31	9.22	0.264	471.6	480.1	488.5	496.8	505.2	513.6	522

	ading		F	We of V	ight apor			Weigh	t in Grain	ns of a Cu	ibic Foot	of Air.	-vlat-b-
mor	Ther- neter,	Temp.	Force of Vapor	Ina	Reqd.	Hu- midity,		Height (	of the Ba	rometer i	n English	h Inches	6
II.	ahr.	Point,	in English	Cubic Foot of	Sat'n.	Satura- tion =	200	Hoight	I the ba	l dilleter i	II Zugusi	I III III II	
Dry.	Wet.	Fahr.	Inches.	Air.	bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
86	86	86.0	1.209	12.91	0.00	1.000	465.7	474.0	482.3	490.6	498.9	507.2	515.5
1	85	84.5	1.153	12.31	0.60	0.954 $0.910$	466.0	474.3	482.6	490.9	499.2	507.5 507.8	515.8 516.1
	84 83	81.5	1.050	11.20	1.71	0.868	466.5	474.8	483.2	491.5	499.8	508.1	516.5
	82	80.0	1.001	10.69	2.22	0.828	466.8	475.1	483.5	491.8	500.1	508.4	516.8
1	81	78.5	0.955	10.19	2.72	0.789	467.1	475.4	483.8	492.1	500.4	508.7	517.1
To a	80	77.0	0.910	9.71	3.20	0.752	467.3	475.6	484.0	492.3	500.7	509.0	517.4
	-1						Cities I	Select 1		- Land		4334	
	79	75.5	0.868	9.25	3.66	0.717	467.5	475.8	484.2	492.5	500.9	509.2	517.6
	78	74.0	0.827	8.82	4.09	0.683	467.8	476.1	484.5	492.8	501.2	509.5	517.9
	77	72.5	0.787	8.40	4.51	0.651	468.0	476.3	484.7	493.0	501.4	509.7	518.1
	76	71.0	0.751	8.00	4.91	0.619	468.2	476.5	484.9	493.2	501.6	509.9	518.3
	75	69.5	0.715	7.62	5.29	0.590	468.3	476.6	485.0	493.4	501.8	510.2	518.6
15	74	68.0	0.681	7.26	5.65	0.562	468.5	476.8	485.2	493.6	502.0	510.4	518.8
1991	73	66.5	0.648	6.91	6.00	0.535	468.8	477.1	485.5	493.9	502.2	510.6	519.0
	72	65.0	0.617	6.58	6.33	0.509	468.9	477.2	485.6	494.0	502.4	510.8	519.2
	71	63.5	0.588	6.26	6.65	0.485	469.1	477.4	485.8	494.2	502.4	511.0	519.4
	70	62.0	0.559	5.95	6.96	0.461	469.2	477.5	485.9	494.3	502.7	511.1	519.5
	69	60.5	0.532	5.66	7.25	0.438	469.4	477.7	486.1	494.5	502.9	511.3	519.7
	68	59.0	0.506	5.38	7.53	0.417	469.6	477.9	486.3	494.7	503.1	511.5	519.9
1	67	57.5	0.481	5.11	7.80	0.396	469.8	478.1	486.5	494.9	503.3	511.7	520.1
	66	56.0	0.458	4.87	8.04	0.377	469.9	478.2	486.6	495.0	503.4	511.8	520.2
					3557		The state of					Cathorn City	
	65	54.5	0.435	4.63	8.28	0.359	470.0	478.3	486.7	495.1	503.5	511.9	520.3
0.001	64	53.0	0.414	4.40	8.51	0.341	470.1	478.4	486.8	495.1	503.6	512.0	520.4
	63	51.5	0.393	4.19	8.72	0.325	470.2	478.5	486.9	495.2	503.7	512.1	520.5
2	62	50.0	0.373	3.98	8.93	0.308	470.4	478.7	487.1	495.4	503.9	512.2	520.7
	61	48.5	0.355	3.78	9.13	0.293	470.5	478.8	487.2	495.5	504.0	512.3	520.8
	60 59	47.0	0.337	3.59	9.32	0.278	470.6	478.9	487.4	495.6	504.1	512.4 512.5	520.9 521.0
	99	40.0	0.520	3.40	9.51	0.263	470.7	479.0	401.4	490.7	504.2	312.5	021.0
			10	172			100		A. Carlo	Fill I S	ALT.	95-0 US	Fe Ki
87	87	87.0	1.247	13.29	0.00	1.000	464 =	472.8	481.1	489.4	497.7	506.0	514.3
01	86	85.5	1.190	12.68	0.61	0.954	464.5	472.8	481.4	489.4	497.7	506.3	514.6
	85	84.0	1.136	12.10	1.19	0.910	465.1	473.4	481.7	490.0	498.3	506.6	514.9
1	84	82.5	1.083	11.54	1.75	0.868	465.4	473.7	482.0	490.3	498.6	506.9	515.2
	83	81.0	1.034	11.01	2.28	0.828	465.7	474.0	482.3	490.6	498.9	507.2	515.5
1	82	79.5	0.986	10.49	2.80	0.789	466.0	474.3	482.6	490.9	499.2	507.5	515.8
	81	78.0	0.940	10.01		0.753	466.3	474.6	482.9	491.2	499.5	507.8	516.1
				4	TELET			- 1					
	80	76.5	0.896	9.54	3.75	0.718	466.5	474.8	483.1	491.4	499.8	508.1	516.5
	79	75.0	0.854	9.09	4.20	0.684	466.8	475.1	483.5	491.8	500.1	508.4	516.8
	78	73.5	0.814	8.66	4.63	0.652	467.0	475.3	483.7	492.0	500.3	508.6	517.0
Evolu	77	72.0	0.776	8.24	5.05	0.620	467.2	475.5	483.9	492.2	500.5	508.8	517.2
8	76 75	70.5 69.0	0.739	7.85	5.44	0.591	467.3	475.6	484.0	492.3	500.7	509.0	517.4
-30	74	67.5	0.701	7.48	5.81 6.17	0.563	467.5	475.8	484.2	492.5	500.9	509.2 509.4	517.6
	11	01.0	0.070	1.12	0.17	0.536	407.7	476.0	484.4	492.7	501.1	009.4	517.8

of '	ding Ther-	Temp.	Force		apor	Hu-		Weigh	t in Grain	ıs of a Çu	ibic Foot	of Air.	
	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	of the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	in. 30.5	in. 31.0
0	0	0	in.	gr.	gr.	0.596	gr.	gr.	gr.	gr.	gr.	gr.	gr.
87	74 73	66.0	0.670	7.12 6.78	6.17	0.536	467.7	476.0 476.2	484.4	492.7	501.1	509.4 509.6	517.8 518.0
-	72	64.5	0.607	6.46	6.83	0.486	468.1	476.4	484.8	493.1	501.5	509.8	518.2
	71	63.0	0.578	6.14	7.15	0.462	468.3	476.6	485.0	493.3	501.7	510.1	518.
	70	61.5	0.550	5.85	7.44	0.440	468.4	476.7	485.1	493.5	501.9	510.3	518.
	69	60.0	0.523	5.56	7.73	0.418	468.5	476.9	485.3	493.7	502.0	510.4	518.8
	68	58.5	0.498	5.28	8.01	0.397	468.7	477.1	485.5	493.9	502.2	510.6	519.
	67	57.0	0.473	5.02	8.27	0.378	468.8	477.2	485.6	494.0	502.3	510.7	519.
	66	55.5	0.450	4.77	8.52	0.359	468.9	477.3	485.7	494.1	502.4	510.7	519.
	65	54.0	0.428	4.54	8.75	0.342	469.1	477.5	485.9	494.3	502.6	510.9	519.
	64	52.5	0.407	4.33	8.96	0.326	469.2	477.6	486.1	494.4	.02.7	511.0	519.
1.2	63	51.0	0.386	4.12	9.17	0.310	469.3	477.7	486.2	494.5	.02.8	511.1	519.
L'as	62	49.5	0.367	3.91	9.38	0.294	469.4	477.8	486.3	494.6	502.9	511.2	519.
600	61	48.0	0.349	3.71	9.58	0.279	469.6	477.9	486.5	494.8	503.1	511.4	519.
	60	46.5	0.331	3.51	9.78	0.264	469.7	478.1	486.6	494.9	503.2	511.5	520.
11	29	9 5	64 K	4394	44	1		-6.50			9 6,5	AR RE	
88	88	88.0	1.286	13.68	0.00	1.000	463.5	471.7	480.0	488.3	496.6	504.8	513.
00	87	86.5	1.228	13.06	FF 0 1 59	0.954	463.8	472.0	480.3	488.6	496.9	505.1	513.
	86	85.0	1.171	12.46		0.911	464.2	472.4	480.7	489.0	497.3	505.6	513.
	85	83.5	1.118	11.88	1.80	0.868	464.4	472.7	481.0	489.3	497.6	505.9	514.
	84	82.0	1.067	11.34	2.34	0.829	464.7	473.0	481.3	489.6	497.9	506.2	514.
	83	80.5	1.017	10.81	2.87	0.790	465.0	473.3	481.6	489.9	498.2	506.5	514.
1	82	79.0	0.970	10.31	3.37	0.754	465.2	473.5	481.8	490.1	498.4	506.7	515.
shi	81	77.5	0.925	9.83	3.85	0.718	465.5	473.8	482.1	490.4	498.7	507.0	515.
0.7	80	76.0	0.882	9.37	105.00	0.685	465.8	474.1	482.4	490.7	499.0	507.3	515.
	79	74.5	0.840	8.93		0.653	466.1	474.4	482.7	491.0	499.3	507.6	515.
	78	73.0	0.801	8.50	5.18	COLUMN TO THE REAL PROPERTY.	466.3	474.6	482.9	491.2	499.5	507.8	516.
	77	71.5	0.763	8.09	5.59	0.591	466.4	474.7	483.0	491.3	499.7	508.0	516.
1	76	70.0	0.727	7.71	5.97	0.563	466.6	474.9	483.2	491.5	499.9	508.2	516.
	75	68.5	0.692	7.34	6.34	0.537	466.8	475.1	483.4	491.7	500.1	508.4	516.
2.34	74	67.0	0.659	6.99	6.69	0.511	467.0	475.3	483.6	491.9	500.3	508.6	517.
E	73	65.5	0.628	6.66			467.2	475.5	483.8	492.1	500.5	508.8	517.
in the	72	64.0	0.597	6.33			467.4	475.7	484.0	492.3	500.7	509.0	517.
Fig.	71	62.5	0.568	6.03		1002	467.4	475.7	484.0	492.4	500.8	509.1	517.
1150	70	61.0	0.541	5.74	7.94	0.420	467.6	475.9	484.2	492.6	501.0	509.3	517.
4	69	59.5	0.515	5.45	8.23	0.398	467.7	476.0	484.3	492.7	501.2	509.4	517.
-	68	58.0	0.489	5.18	8.50	0.378	467.9	476.2	484.5	492.9	501.3	509.6	518.
	67	56.5	0.465	4.93	8.75	0.359	468.1	476.4	484.7	493.1	501.5	509.8	518.
ATAK	66	55.0	0.442	4.69	8.99	0.342	468.2	476.5	484.8	493.2	501.6	509.9	518.
5.9%	65	53.5	0.421	4.47	9.21	0.326	469.3	476.6	484.9	493.3	501,7	510.0	518.
4.54	64	52.0	0.400	4.25		0.310	468.4	1		493.4	501.8	510.1	518.
Section 1	63	50.5	0.380	4.04	The second		468.6	476.9	100000	493.6	502.0	510.3	518.
The Party	62	49.0	0.361	3.83		0.280	468.7	477.1	485.4	493.7	502.1	510.4	518.

6.1

Res	ading Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ıs of a Cı	ıbic Foot	of Air.	1.6.1
moi	neter, ahr.	of Dew-Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height	of the Ba	rometer i	n English	h Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.		1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr 0.00	1.000	gr.	gr. 470.6	gr.	gr.	gr.	gr.	gr.
89	89 88	89.0	1.326	14.08	0.64	0.954	462.4	470.9	478.9	487.1	495.4	503.6 503.9	511.9 512.2
	87	86.0	1.209	12.84	1.24	0.912	463.0	471.2	479.5	487.8	496.1	504.4	512.7
7.10	86	84.5	1.153	12.24	1.84	0.869	463.3	471.5	479.8	488.1	496.4	504.7	513.0
Teen	85	83.0	1.101	11.68	2.40	0.830	463.6	471.8	480.1	488.4	496.7	505.0	513.3
3.17	84	81.5	1.050	11.13	2.95	0.791	464.0	472.2	480.5	488.8	497.1	505.4	513.7
	83	80.0	1.001	10.62	3.46	0.754	464.2	472.5	480.8	489.1	497.4	505.7	514.0
10,00	82	78.5	0.955	10.13	3.95	0.719	464.4	472.7	481.0	489.3	497.6	505.9	514.2
N. Pr	81	77.0	0.910	9.66	4.42	0.686	464.7	473.0	481.3	489.6	497.9	506.2	514.5
以特	80	75.5	0.868	9.20	4.88	0.653	464.9	473.2	481.5	489.8	498.1	506.4	514.7
493	79	74.0	0.827	8.77	5.31	0.623	465.2	473.5	481.8	490.1	498.4	506.7	515.0
10.83	78	72.5	0.787	8.35	5.73	0.593	465.4	473.7	482.0	490.3	498.6	506.9	515.2
-	77	71.0	0.751	7.96	6.12	0.565	465.6	473.9	482.2	490.5	498.8	507.1	515.4
	76	69.5	0.715	7.57	6.51	0.537	465.8	474.1	482.4	490.7	499.0	507.3	515.7
	75	68.0	0.681	7.21	6.87	0.512	466.0	474.3	482.6	490.9	499.2	507.5	515.8
	74	66.5	0.648	6.87	7.21	0.488	466.2	474.5	482.8	491.1	499.4	507.7	516.0
14.12	73	65.0	0.617	6.54	7.54	0.465	466.3	474.6	482.9	491.2	499.6	507.9	516.3
	72	63.5	0.588	6.22	7.86	0.442	466.5	474.8	483.1	491.4	499.8	508.1	516.5
	71	62.0	0.559	5.91	8.17	0.420	466.7	475.0	483.3	491.7	500.0	508.3	516.7
	70	60.5	0.532	5.62	8.46	0.399	466.8	475.1	483.4	491.8	500.1	508.4	516.8
	69	59.0	0.506	5.35	8.73	0.380	467.0	475.3	483.6	492.0	500.3	508.6	517.0
B) F (	68	57.5	0.481	5.08	9.00	0.361	467.1	475.4	483.7	492.1	500.4	508.7	517.1
	67	56.0	0.458	4.84	9.24	0.343	467.2	475.5	483.8	492.2	500.5	508.8	517.2
	66	54.5	0.435	4.61	9.47	0.327	467.4	475.7	483.9	492.4	500.7	509.1	517.4
	65	53.0	0.414	4.39	9.69	0.312	467.5	475.8	484.1	492.5	500.8	509.2	517.5
	64	51.5	0.393	4.17	9.91	0.296	467.6	475.9	484.2	492.6	500.9	509.3	517.6
12.5	63	50.0	0.373	3.96	10.12	0.281	467.7	476.1	484.3	492.7	501.0	509.4	517.7
	62	48.5	0.355	3.76	10.32	0.267	467.8	476.2	484.4	492.8	501.1	509.5	517.8
		60	11/1		M. T.	1- 1	N YE	0 115	1 15	4111	1111	1 10	Total
90	90	90.0	1.368	14.50	0.00	1.000	461.3	469.5	477.8	486.0	494.3	502.5	510.8
	89	88.5	1.306	13.84	0.66	0.954	461.6	469.8	478.1	486.3	494.6	502.8	511.1
	88	87.0	1.247	13.22	1.28	0.910	462.0	470.2	478.5	486.7	495.0	503.2	511.5
100	87	85.5	1.190	12.61	1.89	0.870	462.3	470.5	478.8	487.0	495.3	503.5	511.8
111	86	84.0	1.136	12.03	2.47	0.830	462.7	470.9	479.2	487.4	495.7	503.9	512.1
	85	82.5	1.083	11.47	3.03	0.791	463.0	471.2	479.5	487.7	496.0	504.2	512.5
	84	81.0	1.034	10.94	3.56	0.755	463.2	471.5	479.8	488.0	496.3	504.5	512.8
	83	79.5	0.986	10.43	4.07	0.719	463.4	471.7	480.0	488.2	496.5	504.7	513.0
1	82	78.0	0.940	9.95	4.55	0.686	463.7	472.0	480.3	488.5	496.8	505.0	513.3
	81	76.5	0.896	9.48	5.02	0.653	464.0	472.3	480.6	488.8	497.1	505.3	513.6
1 4 8	80	75.0	0.854	9.03	5.47	0.622	464.2	472.5		488.9	497.3	505.5	513.9
	79	73.5	0.814	8.61	5.89	0.594	464.3	472.6	480.9	489.1	497.5	505.7	514.1
	78	72.0	0.776	8.20		0.565	464.5	472.8	481.1	489.3	497.7	505.9	514.3
	77	70.5	0.739	7.80	6.70	0.538	464.7	473.0	481.3	489.5	497.9	506.1	514.5

of	ading Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ns of a Cr	ibic Foot	of Air.	
	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	of the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	30.0	in. 30.5	in. 31.0
90	77	70.5	in. 0.739	gr. 7.80	gr. 6.70	0.538	gr. 464.7	gr. 473.0	gr. 481.3	gr. 489.5	gr. 497.9	gr. 506.1	gr. 514.5
	76	69.0	0.704	7.43	7.07		465.0	473.3	481.6	489.8	498.2	506.4	514.8
5.69	75	67.5	0.670	7.08	7.42	0.488	465.2	473.5	481.8	490.0	498.4	506.6	515.0
	74	66.0	0.638	6.74	7.76	0.465	465.4	473.7	482.0	490.2	498.6	506.8	515.2
men's	73	64.5	0.607	6.42	8.08	0.443	465.6	473.9	482.2	490.4	498.8	507.0	515.4
7 48	72	63.0	0.578	6.10	8.40	0.421	465.7	474.0	482.3	490.5	498.9	507.1	515.5
	71	61.5	0.550	5.81	8.69	0.400	465.9	474.2	482.5	490.7	499.1	507.3	515.7
	70	60.0	0.523	5.52	8.98	0.381	466.1	474.4	482.8	491.0	499.3	507.5	515.9
	69	58.5	0.498	5.25	9.25	0.362	466.2	474.5	482.9	491.1	499.4	507.6	516.0
	68	57.0	0.473	4.99	9.51	0.344	466.4	474.7	483.1	491.3	499.6	507.8	516.2
HILL	67	55.5	0.450	4.74	9.76	0.327	466.5	474.8	483.2	491.4	499.7	507.9	516.3
	66	54.0	0.428	4.52	9.98	0.312	466.6	474.9	483.3	491.5	499.8	508.0-	516.4
	65	52.5	0.407	4.30	10.20	0.297	466.7	475.0	483.4	491.6	499.9	508.1	516.5
	64	51.0	0.386	4.09	10.41	0.282	466.9	475.2	483.6	491.8	500.1	508.3	516.6
	63	49.5	0.367	3.90	10.60	0.269	467.0	475.3	483.7	491.9	500.2	508.4	516.7

THE PURE SHEET SHEET WAS A SHEET OF THE

#### TABLE XIII.

FACTORS FOR COMPUTING THE FORCE OF VAPOR, FROM THE READINGS OF THE PSYCHROMETER, BY APJOHN'S FORMULA.

Dr. Apjohn's formula for deducing the force of vapor, and the temperature of the dew-point, from the readings of the Psychrometer, as given in the Proceedings of the Royal Irish Academy for 1840, is

$$f'' = f' - \frac{d}{88} \times \frac{h}{30},$$

when the readings of the wet-bulb thermometer are above 32° Fahr., in which formula

f'' = the force of vapor at the temperature of the dew-point in degrees of Fahr.,

f' = the force of vapor at the temperature of evaporation given by the wet-bulb thermometer,

d = the difference between the readings of the dry and wet thermometers,

h = the height of the barometer in English inches at the time of the observation. When the readings of the wet-bulb thermometer are below 32° Fahr., and the bulb is covered with ice, the formula becomes

$$f'' = f' - \frac{d}{96} \times \frac{h}{80}.$$

The factors in the following table, which is taken from the Greenwich Observations for 1843, represent  $\frac{d}{88} \times \frac{1}{20}$  and  $\frac{d}{26} \times \frac{1}{20}$ , computed for all differences between the wet and dry bulb thermometers, or values of d, from 0° to 21°.

#### USE OF THE TABLE.

To find out the force of vapor in the air, and the temperature of the dew-point, by means of these factors, let the factor corresponding to d, or the difference between the wet and dry thermometer in the first column, be multiplied into the observed height of the barometer, and subtract the result from the force of vapor, in Table XI., due to the temperature of evaporation, indicated by the wet-bulb thermometer; the rest is the force of vapor in the air at the time of the observation; and the temperature of the dew-point is that which is due to it in Table XI.

#### EXAMPLE.

The observation gives,

Dry-bulb thermometer = 79° Fahr., or the temperature of the air.

Wet-bulb " = 69° " or temperature of evaporation.

Difference 10°

Height of barometer 29.7 English inches.

In the Table, 2d part, is found, — factor for a difference of  $10^{\circ} = 0.00379 \times 29.7$ , or height of barometer = 0.113, which, subtracted from the force of vapor due to 69°, in Table XI., = 0.704 - 0.113, gives force of vapor in the air = 0.591 inches, and temperature of the dew-point 62°.5.

When the temperature of the wet bulb is below 32° Fahrenheit, the factors in the first part of the Table must be used.

# XIII. FACTOR $\frac{d}{96} imes \frac{1}{80}$ , for computing the force of vapor by apjohn's formula.

Below 32° Fahrenheit; the Wet Bulb covered with a Film of Ice.

	Tenths of Degrees.												
of Wet and Dry Bulb Therm.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
0		2 1 X = 1			12/12								
0	0.00000	0.00003	0.00007	0.00010	0.00014	0.00017	0.00020	0.00024	0.00027	0.0003			
1	.00034	.00037	.00041	.00044	.00047	.00051	.00054	.00058	.00061	.0006			
2	.00068	.00071	.00075	.00078	.00081	.00085	.00088	.00092	.00095	.0009			
3	.00102	.00105	.00109	.00112	.00116	.00119	.00122	.00126	.00129	.0013			
4	.00136	.00139	.00143	.00146	.00150	.00153	.00156	.00160	.00163	.0016			
5	.00170	.00173	.00177	.00180	.00184	.00187	.00190	.00194	.00198	.0020			
6	.00204	.00207	.00211	.00214	.00218	.00221	.00224	.00228	.00231	.0023			
7	.00238	.00241	.00245	.00248	.00252	.00255	.00258	.00262	.00265	.0026			
8	.00272	.00275	.00279	.00282	.00285	.00289	.00292	.00296	.00299	.0030			
9	.00306	.00309	.00313	.00316	.00319	.00323	.00326	.00330	.00333	.0033			
10	.00340	.00343	.00347	.00350	.00354	.00357	.00360	.00364	.00367	.0037			

# FACTOR $\frac{d}{88} \times \frac{1}{30}$ .

#### Reading of Wet-Bulb Thermometer above 32° Fahrenheit.

d, or Difference	Salasin)	EMER	tall bis	n dia io	Tenths o	f Degrees.	1500	eng.		
of Wet and Dry Bulb Therm.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° °	0.00000	0.00004	0.00000	0.00017	0.00015	0.00000	0.00000		0.00000	
	.00038	.00042		.00049	0.00015	.00057	.00023	0.00027	0.00030	.000
1 2	.00038	.00042		.00049	.00091	.00057	.00098	.00064	.00068	.000
3	.00076	.00030		.00125	.00129	.00093	.00098	.00102	.00106	.001
.4	.00114	.00118	.00121	.00123	.00129	.00132	.00157		.00144	.001
5	.00189	.00193	.00197	.00201	.00205	.00209	.00212	.00216	.00220	.002
6	.00228	.00231	.00235	.00239	.00242	.00246	.00250	.00254	.00258	.002
7	.00265	.00269	.00273	.00277	.00280	.00284	.00288	.00292	.00295	.002
8	.00303	.00307	.00311	.00315	.00318	.00322	.00326	.00330	.00333	.003
9	.00341	.00345	.00349	.00352	.00356	.00360	.00364	.00368	.00371	.003
10	.00379	.00383	.00386	.00390	.00394	.00398	.00401	.00405	.00409	.004
11	.00416	.00420	.00424	.00428	.00432	.00436	.00439	.00443	.00447	.004
12	.00454	.00458	.00462	.00466	.00470	.00474	.00477	.00481	.00485	.004
13	.00493	.00496	.00500	.00504	.00508	.00511	.00515	.00519	.00522	.005
14	.00530	.00534	.00538	.00541	.00545	.00549	.00553	.00556	.00560	.005
15	.00568	.00572	.00576	.00580	.00584	.00587	.00591	.00595	.00598	.006
16	.00606	.00610	.00614	.00618	.00622	.00625	.00629	.00633	.00636	.006
17	.00644	.00648	.00652	.00655	.00659	.00663	.00666	.00670	.00674	.006
18	.00682	.00686	.00690	.00693	.00697	.00701	.00704	.00708	.00712	.007
19	.00720	.00724	.00728	.00731	.00735	.00739	.00742	.00746	.00750	.007
20	.00758	.00761	.00765	.00769	.00773	.00777	.00780	.00784	.00788	.007

In the Greenwich Magnetic and Meteorological Observations for 1842 and 1843, Mr. Glaisher discussed the relation between the temperature of evaporation given by the Wet-bulb Thermometer and the temperature of the Dew-Point as given by Daniell's Hygrometer. Comparing the observations taken simultaneously every six hours with the Psychrometer, and with Daniell's Dew-Point Hygrometer, and dividing the average difference between the temperatures of the Wet and Dry bulb by the average difference of the temperature of the Dew-Point and of the Air, he obtained the empirical factors given in the following Table.

The observations from which they are deduced are those taken at the Observatory in the years 1841 to 1845, for the temperatures below 35° F., and in the years 1841 to 1843, for the temperatures above 35° F.

The observations made at Toronto Observatory, Canada West, in similar circumstances, in the years 1840 to 1842, were also compared in the same manner, and the factors derived from them showed a very close accordance for temperatures above 30° F., but were found smaller at temperatures below 30° F.

The errors in the temperature of the Dew-Point, which may result by using the Greenwich factors, though frequently within half a degree, often amount, however, to  $\pm 2$  or 3 degrees, and, in extreme cases, to  $\pm 4$  or 5 degrees, as shown in the volume of the *Greenwich Observations* for 1842, p. 60 of the *Abstracts*.

#### Use of the Table.

Multiply the difference between the Wet-bulb and Dry-bulb Thermometers by the factor standing in the Table opposite the reading of the Dry-bulb, and subtract the product from the reading of the Dry-bulb; the remainder will be the temperature of the Dew-Point.

Example. — Dry-bulb =  $62^{\circ}$  F.; Wet-bulb =  $55^{\circ}$ ; Difference =  $7^{\circ}$ .

Opposite 62°, in the first column, stands the factor 1.7, which multiplied by 7°, the difference, gives  $11^{\circ}.9$ , to be subtracted from the Dry-bulb; or  $62^{\circ}-11^{\circ}.9=50^{\circ}.1$ , temperature of the Dew-Point.

XIV. FACTORS TO FIND OUT THE TEMPERATURE OF THE DEW-POINT FROM THE READINGS OF THE PSYCHROMETER. — GLAISHER.

Dry-Bulb Therm. Fahren.	Factors.								
21°	8.5	35°	2.6	49°	2.2	63°	1.7	77°	1.5
22	8.5	36	2.6	50	2.1	64	1.7	78	1.5
23	8.5	37	2.5	51	2.1	65	1.7	79	1.5
24	7.3	38	2.5	52	2.0	66	1.6	80	1.5
25	6.4	39	2.5	53	2.0	67	1.6	81	1.5
26	6.1	40	2.4	54	2.0	68	1.6	82	1.5
27	5.9	41	2.4	55	2.0	69	1.5	83	1.5
28	5.7	42	2.4	56	1.9	70	1.5	84	1.5
29	5.0	43	2.4	57	1.9	71	1.5	85	1.5
30	4.6	44	2.3	58	1.9	72	1.5	86	1.5
31	3.6	45	2.3	59	1.8	73	1.5	87	1.5
32	3.1	46	2.3	60	1.8	74	1.5	88	1.5
33	2.8	47	2.2	61	1.8	75	1.5	89	1.5
34	2.6	48	2.2	62	1.7	76	1.5	90	1.5

XV. WEIGHT OF VAPOR, IN GRAINS TROY, CONTAINED IN A CUBIC FOOT OF SATURATED AIR, AT TEMPERATURES BETWEEN 0° AND 94° FAHRENHEIT.

From the Greenwich Observations.

Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.						
0°	0.78	19°	1.52	38°	2.89	57°	5.34	76°	9.60
1	0.81	20	1.58	39	2.99	58	5.51	77	9.89
2	0.84	21	1.63	40	3.09	59	5.69	78	10.19
3	0.87	22	1.69	41	3.19	60	5.87	79	10.50
4	0.90	23	1.75	42	3.30	61	6.06	80	10.81
5	0.93	24	1.81	43	3.41	62	6.25	81	11.14
6	0.97	25	1.87	44	3.52	63	6.45	82	11.47
7	1.00	26	1.93	45	3.64	64	6.65	83	11.82
. 8	1.04	27	2.00	46	3.76	65	6.87	84	12.17
9	1.07	28	2.07	47	3.88	66	7.08	85	12.53
10	1.11	29	2.14	48	4.01	67	7.30	86	12.91
11	1.15	30	2.21	49	4.14	68	7.53	87	13.29
12	1.19	31	2.29	50	4.28	69	7.76	88	13.68
13	1.24	32	2.37	51	4.42	70	8.00	89	14.08
14	1.28	33	2.45	52	4.56	71	8.25	90	14.50
15	1.32	34	2.53	53	4.71	72	8.50	91	14.91
16	1.37	35	2.62	54	4.86	73	8.76	92	15.33
17	1.41	36	2.71	55	5.02	74	9.04	93	15.76
18	1.47	37	2.80	56	5.18	75	9.31	94	16.22

XVI. FACTORS TO DEDUCE THE WEIGHT OF VAPOR CONTAINED IN A CUBIC FOOT OF AIR, AT THE TIME OF A GIVEN OBSERVATION, FROM THE INDICATIONS OF DEW-POINT INSTRUMENTS. — GREENW. OBS.

t = Temperature of Air; t" = Temperature of Dew-Point.

Difference or t-t''.	Factors.	Difference or t-t".	Factors.	Difference or t-t".	Factors.	Difference or t — t".	Factors.	Difference or t-t".	Factors.
1	0.999	9	0.982	17	0.966	25	0.951	33	0.935
2	0.996	10	0.980	18	0.964	26	0.949	34	0.934
3	0.994	11	0.978	19	0.962	27	0.947	35	0.932
4	0.992	12	0.976	20	0.960	28	0.945	36	0.930
5	0.990	13	0.974	21	0.958	29	0.943	37	0.929
6	0.988	14	0.972	22	0.956	30	0.942	38	0.927
7	0.986	15	0.970	23	0.954	31	0.939	39	0.925
8	0.984	16	0.968	24	0.952	32	0.937	40	0.923

Use of Table XVI. — The difference between the temperatures of the air and of the Dew-Point being known, multiply the factor in the Table corresponding to that difference into the weight of a cubic foot of vapor at the temperature of the Dew-Point, as given in Table XV., and the product will be the weight of vapor in a cubic foot of air at the time of the observation.

Example. — Temperature of air = 60° F.; Dew-Point = 52°; Diff. = 8°.

Table gives for a difference of 8°, factor 0.984; Table XV. gives weight of a cubic foot of vapor at temperature  $52^{\circ} = 4.5^{\circ}.56$ .

Hence,  $0.984 \times 4.56 = 4^{gr}.49$ , the weight of vapor required.

#### TABLE XVII.

FOR COMPARING THE WEIGHT OF A CUBIC FOOT OF DRY AND OF SATURATED AIR.

This table is composed of two tables found in the Greenwich Meteorological Observations for 1842, pages xlvi. and li.; the first containing the weight of a cubic foot of dry air, under a barometric pressure of 30 inches, at temperatures between 0° and 90° F.; the other giving the weight of a cubic foot of saturated air under the same barometric pressure and temperature, together with the excess of the first above the last.

The weight of a cubic foot of dry air, on which the tables are based, is assumed to be 563 grains Troy, being a mean value, in round numbers, between the determinations of Shuckburgh, which is 557.7295 grains, and that of Biot and Arago, 568.7013. The true mean is 563.2154, but 563 is the number used in the calculations.

The coefficient of the expansion of the air is that of Gay-Lussac, viz. 0.00375 for 1° Centigrade, or 0.002083 of its bulk for 1° Fahrenheit.

### Use of the Table.

This table shows the amount of buoyancy imparted to the air by the addition of moisture; and from it, the temperature and the relative humidity of the air being known, the weight of a cubic foot of air, in the actual condition of the atmosphere at the time of an observation, can be deduced.

It suffices to take in the fourth column, headed "Excess," the quantity corresponding to the temperature of the air in the first, multiply it into the given Relative Humidity, and subtract the product from the number in the second column. The result will be the weight of a cubic foot of air at the existing temperature and moisture, under a barometric pressure of 30 inches.

This result will be reduced to its true value, under the barometric pressure given by the observation, by multiplying it by  $\frac{\text{Height of Barometer}}{30}$ .

# Example.

The temperature of the air is 60° F.; the relative humidity, 0.852; the barometer reads 29 inches.

The table gives, for temperature of air,  $60^{\circ}$ ; excess,  $3.35 \times 0.852 = 2.85$ , which, subtracted from 531.91 in the second column, = 529.12, weight of a cubic foot of air under 30 inches of pressure; and  $529.12 \times \frac{29 \text{ inch}}{30} = 511.48$ , the weight of a cubic foot of air in the given conditions of temperature, moisture, and barometric pressure.

# XVII. FOR COMPARING THE WEIGHT OF A CUBIC FOOT OF DRY AND OF SATURATED AIR,

### AT TEMPERATURES BETWEEN 0° AND 90° FAHRENHEIT.

### From the Greenwich Observations.

Temper- ature Fahren.	Weight of a cubic foot of Dry Air.	Weight of a cubic foot of Saturat- ed Air.	Excess of Dry Air.	Temper- ature Fahren.	Weight of a cubic foot of Dry Air.	Weight of a cubic foot of Saturat- ed Air.	Excess of Dry Air.	Temper- ature Fahren.	Weight of a cubic foot of Dry Air	Weight of a cubic foot of Saturat- ed Air.	Excess of Dry Air
E CO	10	The fact		4.770	CPA	Page 1	G de la	nizi Di k	ele tal e		SEPER
0	Grains.	Grains.	Grains	0	Grains.	Grains.	Grains.	0	Grains.	Grains.	Grains
0	603.21	602.77	0.44	30	565.35	564.08	1.27	60	531.97	528.62	3.35
1	601.87	601.40	0.47	31	564.17	562.86	1.31	61	530.93	527.48	3.45
2	600.52	600.03	0.49	32	563.00	561.64	1.36	62	529.88	526.32	3.56
3	599.20	598.69	0.51	33	561.84	560.42	1.42	63	528.84	525.17	3.67
4	597.87	597.34	0.53	34	560.67	559.20	1.47	64	527.81	524.03	3.78
5	596.55	596.01	0.54	35	559.51	558.01	1.50	65	526.88	522.90	3.88
6	595.24	594.69	0.55	36	558.35	556.79	1.56	66	525.76	521.75	4.01
7	593.94	593.36	0.58	37	557.21	555.61	1.60	67	524.75	520.61	4.14
8	592.63	592.04	0.59	38	556.05	554.40	1.65	68	523.72	519.46	4.26
9	591.33	590.72	0.61	39	554.91	553.20	1.71	69	522.70	518.29	4.41
10	590.04	589.40	0.64	40	553.77	552.00	1.77	70	521.70	517.17	4.53
11	588.75	588.07	0.68	41	552.65	550.80	1.84	71	520.70	516.02	4.68
12	587.48	586.78	0.70	42	551.52	549.63	1.89	72	519.69	514.87	4.82
13	586.21	585.49	0.72	43	550.39	548.44	1.95	73	518.70	513.75	4.95
14	584.94	584.18	0.75	44	549.27	547.26	2.01	74	517.70	512.61	5.09
15	583.67	582.89	0.78	45	548.16	546.06	2.10	75	516.71	511.46	5.25
16	582.41	581.61	0.80	46	547.05	544.88	2.17	76	515.73	510.32	5.41
17	581.15	580.33	0.82	47	545.97	543.75	2.22	77	514.74	509.18	5.56
18	579.91	579.06	0.85	48	544.85	542.55	2.30	78	513.77	508.04	5.73
19	578.67	577.79	0.88	49	543.75	541.36	2.39	79	512.80	506.91	5.89
20	577.44	576.54	0.90	50	542.65	540.21	2.44	80	511.82	505.74	6.08
21	576.21	575.27	0.94	51	541.55	539.04	2.51	81	510.87	504.61	6.26
22	574.98	574.01	0.97	52	540.48	537.87	2.61	82	509.89	503.45	6.44
23	573.76	572.76	1.00	53	539.41	536.71	2.70	83	508.93	502.32	6.61
24	572.55	571.50	1.05	54	538.33	535.55	2.78	84	507.97	501.16	6.81
25	571.33	570.26	1.07	55	537.27	534.39	2.88	85	507.03	500.05	6.98
26	570.13	569.01	1.12	56	536.19	533.22	2.97	86	506.07	498.87	7.20
27	568.92	567.77	1.15	57	535.12	532.06	3.06	87	505.11	497.71	7.40
28	567.73	566.53	1.20	58	534.07	530.92	3.15	88	504.19	496.58	7.61
29	566.54	565.31	1.23	59	533.03	529.77	3.26	89	503.25	495.44	7.81
30	565.35	564.08	1.27	60	531.97	528.62	3.35	90	502.32	494.28	8.04

#### TABLE XIV'.

Mr. Glaisher published in London, in 1856, another series of Hygrometrical Tables, which were unknown to the writer when the Second Edition of this volume was issued. They are based on Regnault's Table of Elastic Forces of Vapor, and on the coefficient of the expansion of the air as determined by the same physicist. Psychrometrical Table, however, is not computed from Regnault's formula, but by first finding out, in the manner described on page 140, the temperatures of the dewpoint from the readings of the Psychrometer, by means of the empirical factors given below, in Table XIV'., and then taking the corresponding values of the force of vapor from Regnault's table. These factors have been derived from the combination of all simultaneous observations of the dry and wet bulb thermometers with those of Daniell's hygrometer, taken at the Royal Observatory, Greenwich, from the year 1841 to 1854, with some observations taken at high temperatures in India, and others at low and medium temperatures at Toronto; they are, therefore, more correct than those given in Table XIV. page 140. The results in this new Psychrometrical Table, nevertheless, by no means entirely coincide with those given by the formula, as a comparison with those in Table VII. will show.

XIV'. FACTORS TO FIND OUT THE TEMPERATURE OF THE DEW-POINT FROM THE READINGS OF THE PSYCHROMETER. — GLAISHER.

Dry-Bulb Therm. Fahren.	Factors.								
° 10	8.78	° 28	5.12	o 46	2.14	64	1.83	o 82	1.67
11	8.78	29	4.63	47	2.12	65	1.82	83	1.67
12	8.78	30	4.15	48	2.10	66	1.81	84	1.66
13	8.77	31	3.70	49	2.08	67	1.80	85	1.65
14	8.76	32	3.32	50	2.06	68	1.79	86	1.65
15	8.75	33	3.01	51	2.04	69	1.78	87	1.64
16	8.70	34	2.77	52	2.02	70	1.77	88	1.64
17	8.62	35	2.60	53	2.00	71	1.76	89	1.63
18	8.50	36	2.50	54	1.98	72	1.75	90	1.63
19	8.34	37	2.42	55	1.96	73	1.74	91	1.62
20	8.14	38	2.36	56	1.94	74	1.73	92	1.62
21	7.88	39	2.32	57	1.92	75	1.72	93	1.61
22	7.60	40	2.29	58	1.90	76	1.71	94	1.60
23	7.28	41	2.26	59	1.89	77	1.70	95	1.60
24	6.92	42	2.23	60	1.88	78	1.69	96	1.59
25	6.53	43	2.20	61	1.87	79	1.69	97	1.59
26	6.08	44	2.18	62	1.86	80	1.68	98	1.58
27	5.61	45	2.16	63	1.85	81	1.68	99	1.58
28	5.12	46	2.14	64	1.83	82	1.67	100	1.57

# MISCELLANEOUS TABLES,

FOR

COMPARING THE HYGROMETRICAL RESULTS OBTAINED BY DIFFERENT AUTHORITIES.

### MISCELLANEOUS TABLES.

THE object of these Tables is to afford the means of comparing the different determinations of the hygrometrical elements which have been obtained, or adopted, by various physicists, especially the values of the elastic forces of vapor given in other tables than those contained in the preceding pages.

Table XVIII., giving the elastic forces of vapor, expressed in millimetres of mercury, for Centigrade temperatures, was calculated by August from Dalton's experiments, and reduced to French measures in the translation of Kaemtz's *Meteorology*, by Chas. Martins, page 70, from which it has been taken. On these values are based the first psychrometrical tables published by August, in Berlin, 1825.

Table XIX. is the table computed by Kaemtz from his own experiments. It is found, reduced to French measures, in the same volume, page 68.

Table XX. furnishes the results of the experiments made by Professor Magnus, in Berlin, and published in Poggendorf's *Annalen*, Tom. LXI. p. 226, and also in the *Annales de Chimie et de Physique*, 3<sup>me</sup> série, Tom. XII. p. 88, from which this table was copied.

Table XXI. has been published by the Committee of Physics and Meteorology of the Royal Society, in their Report on the Objects of Scientific Inquiry in these Sciences, London, 1840, p. 89. The values which it contains are not derived from new experiments, but are probably computed from those existing at that time.

Table XXII. furnishes a synoptic view of the differences in the values of the force of vapor adopted by various authorities, prepared with the view of facilitating their comparison. A reference to their respective origin will be found below, page 152.

Table XXIII., showing the weight, in grammes, of the vapor contained in a cubic metre of saturated air, at different temperatures, is taken from Pouillet's *Eléments de Physique*, Tom. II. p. 707.

Table XXIV. gives the weights as derived from August's experiments, in Kaemtz's Vorlesungen über Meteorologie. The table is copied from the French translation, by Martins, page 73. The tensions have been added, opposite the weights, and are extracted from August's table.

Table XXV. is found in Biot's Traité de Physique, Tom. I. p. 533.

## XVIII. ELASTIC FORCE OF AQUEOUS VAPOR,

# EXPRESSED IN MILLIMETRES OF MERCURY FOR EVERY TENTH OF A CENTIGRADE DEGREE.

CALCULATED BY AUGUST.

Centigrade	9.81	4	E E	M. France	Tenths o	f Degrees.				
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Miliim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin
-31	0.45	0.45	0.45	0.44	0.44	0.43	0.43	0.42	0.42	0.41
-30	0.50	0.49	0.49	0.48	0.48	0.47	0.47	0.46	0.46	0.45
-29	0.54	0.54	0.54	0.53	0.53	0.52	0.52	0.51	0.51	0.50
-28	0.59	0.58	0.58	0.57	0.57	0.56	0.56	0.55	0.55	0.54
-27	0.63	0.63	0.63	0.62	0.62	0.61	0.61	0.60	0.60	0.59
00	0.70	0.69	0.68	0.68	0.67	0.66	0.66	0.05	0.04	0.04
-26	0.70		0.68		0.67	0.66	0.66	0.65	0.64	0.64
-25	0.77	0.76	0.75	0.75	0.74	0.73	0.73	0.72	0.71	0.71
-24	0.83	0.83	0.82	0.82	0.81	0.86	0.86	0.79	0.78	0.78
-23 -22	0.99	0.89	0.88	0.96	0.87	0.95	0.94	0.83	0.94	0.84
-22	0.55	0.30	0.57	0.50	0.33	0.99	0.54	0.95	0.92	0.91
-21	1.06	1.05	1.04	1.04	1.03	1.02	1.02	1.01	1.00	1.00
-20	1.15	1.14	1.13	1.12	1.11	1.11	1.10	1.09	1.08	1.07
-19	1.26	1.25	1.24	1.23	1.22	1.21	1.20	1.18	1.17	1.16
-18	1.33	1.32	1.31	1.31	1.30	1.29	1.29	1.28	1.27	1.27
-17	1.44	1.43	1.42	1.41	1.40	1.39	1.38	1.36	1.35	1.34
-16	1.56	1.54	1.53	1.52	1.51	1.50	1.49	1.47	1.46	1.45
-10 -15	1.69	1.68	1.67	1.65	1.64	1.63	1.61	1.60	1.59	1.57
-14	1.80	1.79	1.78	1.77	1.76	1.75	1.74	1.72	1.71	1.70
-13	1.96	1.94	1.93	1.91	1.89	1.88	1.86	1.85	1.83	1.82
-12	2.12	2.10	2.09	2.07	2.05	2.04	2.02	2.01	1.99	1.98
i pulla	knist)	Marine.	se ligh	horses	my an		private.		Market 1	
-11	2.30	2.28	2.26	2.25	2.23	2.21	2.19	2.17	2.16	2.14
-10	2.48	2.46	2.44	2.43	2.41	2.39	2.37	2.35	2.34	2.32
- 9	2.66	2.64	2.62	2.61	2.59	2.57	2.55	2.53	2.52	2.50
-8 -7	2.86 3.09	2.84 3.06	3.04	2.80 3.02	3.00	2.76	2.74 2.95	2.72	2.70	2.68
Sin 8		hy.	Tania s	2 4 1 8	1	1			7.02	
- 6	3.32	3.29	3.27	3.25	3.23	3.20	3.18	3.16	3.14	3.11
- 5	3.56	3.56	3.54	3.51	3.48	3.46	3.43	3.40	3.37	3.33
-4	3.83	3.80	3.78	3.75	3.72	3.70	3.67	3.64	3.61	3.59
- 3	4.11	4.07	4.05	4.02	3.99	3.97	3.94	3.91	3.88	3.86
- 2	4.40	4.37	4.34	4.32	4.29	4.26	4.23	4.20	4.17	4.14
-1	4.71	4.68	4.65	4.62	4.59	4.56	4.53	4.49	4.46	4.43
-0	5.05	5.01	4.98	4.95	4.91	4.88	4.85	4.81	4.78	4.74
+.0	5.05	5.09	5.12	5.16	5.19	5.23	5.27	5.30	5.34	5.37
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centigrade					Tenths o	Degrees.				
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.								
1	5.41	5.45	5.49	5.52	5.56	5.60	5.64	5.68	5.72	5.75
2	5.80	5.84	5.88	5.92	5.96	6.00	6.04	6.08	6.13	6.17
3	6.20	6.24	6.29	6.33	6.37	6.41	6.46	6.50	6.54	6.59
4	6.63	6.68	6.72	6.77	6.81	6.86	6.90	6.95	6.99	7.04
5	7.08	7.13	7.18	7.23	7.28	7.33	7.38	7.43	7.48	7.53
6	7.58	7.63	7.68	7.74	7.79	7.84	7.89	7.94	7.99	8.05
7	8.10	8.15	8.21	8.26	8.32	8.37	8.43	8.48	8.53	8.59
8	8.64	8.70	8.76	8.82	8.87	8.93	8.99	9.05	9.11	9.17
9	9.23	9.30	9.36	9.43	9.50	9.57	9.63	9.70	9.77	9.84
10	9.90	9.96	10.02	10.08	10.14	10.20	10.25	10.31	10.37	10.43
11	10.49	10.56	10.63	10.69	10.76	10.83	10.90	10.96	11.03	11.10
12	11.17	11.24	11.31	11.38	11.45	11.52	11.59	11.66	11.73	11.80
13	11.86	11.94	12.02	12.10	12.18	12.26	12.34	12.42	12.50	12.58
14	12.66	12.74	12.82	12.90	12.98	13.05	13.13	13.21	13.29	13.37
15	13.44	13.52	13.61	13.69	13.77	13.86	13.94	14.02	14.11	14.19
16	14.28	14.37	14.47	14.56	14.65	14.74	14.84	14.93	15.02	15.11
17	15.20	15.29	15.38	15.46	15.55	15.64	15.73	15.82	15.90	15.99
18	16.08	16.17	16.27	16.36	16.45	16.54	16.64	16.73	16.82	16.91
19	17.01	17.13	17.25	17.37	17.49	17.61	17.73	17.85	17.97	18.09
20	18.20	18.31	18.43	18.54	18.65	18.76	18.88	18.99	19.10	19.21
21	19.33	19.45	19.56	19.68	19.80	19.92	20.03	20.15	20.27	20.39
22	20.51	20.63	20.76	20.88	21.01	21.13	21.25	21.38	21.50	21.63
23	21.75	21.88	22.00	22.13	22.26	22.38	22.51	22.63	22.76	22.89
24	23.01	23.13	23.24	23.36	23.48	23.60	23.71	23.83	23.95	24.07
25	24.18	24.34	24.50	24.67	24.83	24.99	25.15	25.32	25.48	25.64
Tolland.					# III F		T VE S			
26	25.81	25.97	26.13	26.28	26.44	26.60	26.76	26.92	27.07	27.23
27	27.39	27.55	27.71	27.86	28.02	28.18	28.34	28.50	28.65	28.81
28	28.96	29.13	29.29	29.46	29.63	29.79	29.96	30.13	30.30	30.46
29	30.63	30.81	30.98	31.16	31.33	31.51	31.69	31.86	32.04	32.21
30	32.39	32.57	32.76	32.94	33.13	33.31	33.50	33.68	33.87	34.05
21	24.04	24.40	94.09	24.00	95.00	95.03	25.40	07.00	05.50	0.5.00
31 32	34.24	34.43	34.63	34.82	35.02	35.21 37.20	35.40	35.60	35.79	35.99
33	36.18 38.21	36.38 38.43	36.59 38.64	36.79 38.86	36.99 39.08	39.29	37,40 39,51	37.60	37.80	38.01
34	40.38	40.60	40.82	41.04	41.26	41.49	41.71	39.73 41.93	39.94 42.15	40.16
35	42.59	42.82	43.05	43.28	43.51	43.74	43.97	44.20	44.43	44.66
eliga.	The part		100		A L	9 0	28 6	11.20	21.10	27.00
	0.	1.	2.	3.	4.	5.	6.	7	8	0
	0.	1.	2.	0,	4.	9.	0.	7.	8.	9.

### XIX. ELASTIC FORCE OF AQUEOUS VAPOR,

# EXPRESSED IN MILLIMETRES OF MERCURY, FOR CENTIGRADE TEMPERATURES. By KAEMTZ.

Temper- ature Centi- Grade.	Force of Vapor.								
0	Millim.								
-25	0.68	-12	1.92	0	4.58	12	10.24	24	21.43
-24	0.72	-11	2.05	1	4.92	13	10.91	25	22.74
-23	0.79	-10	2.21	2	5.26	14	11.62	26	24.16
-22	0.86	- 9	2.39	3	5.64	15	12.38	27	25.56
-21	0.92	- 8	2.57	4	6.01	16	13.17	28	27.07
-20	1.01	- 7	2.78	5	6.45	17	14.03	29	28.67
-19	1.10	- 6	2.98	6	6.90	18	14.93	30	30.36
-18	1.20	- 5	3.20	7	7.38	19	15.86	31	32.17
-17	1.29	- 4	3.45	8	7.89	20	16.87	32	33.95
-16	1.40	- 3	3.70	9	8.41	21	17.91	* 33	35.95
-15	1.51	- 2	3.97	10	9.00	22	19.04	34	37.99
-14	1.62	- 1	4.26	11	9.58	23	20.21	35	40.15
-13	1.76	0	4.58	12	10.24	24	21.43	36	42.40

### XX. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY, FOR CENTIGRADE TEMPERATURES.

By MAGNUS.

Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.
0	Millim.	0	Millim.	0	Millim.	0	Millim.	0	Millim.
-20	0.916	-7	2.671	6	6.939	19	16.345	32	35.419
-19	0.999	-6	2.886	7	7.436	20	17.396	33	37.473
-18	1.089	-5	3.115	8	7.964	21	18.505	34	39.630
-17	1.186	-4	3.361	9	8.525	22	19.675	35	41.893
-16	1.290	-3	3.624	10	9.126	23	20.909	36	44.268
-15	1.403	-2	3.905	11	9.751	24	22.211	37	46.758
-14	1.525	-1	4.205	12	10.421	25	23.582	38	49.368
-13	1.655	0	4.525	13	11.130	26	25.026	39	52.103
-12	1.796	+1	4.867	14	11.882	27	26.547	.40	54.964
-11	1.947	2	5.231	15	12.677	28	28.148	41	57.969
	L Think had		ta. 10	Shell H	to bear	To Killer		81.75	400
-10	2.109	3	5.619	16	13.519	29	29.832	42	61.109
- 9	2.284	4	6.032	17	14.409	30	31.602	43	64.396
-8	2.471	5	6.471	18	15.351	31	33.464	44	67.833

## XXI. ELASTIC FORCE OF AQUEOUS VAPOR,

### EXPRESSED IN ENGLISH INCHES OF MERCURY, FOR TEMPERATURES OF FAHRENHEIT.

From the Royal Society's Report.

Temperature of	Force of	Temperature of	Force of	Temperature of	Force	Temperature of	Force of
Air.	Vapor.	Air.	Vapor.	Air.	Vapor.	Air.	Vapor.
Fahrenheit.	Eng. Inches.	Fahrenheit.	Eng Inches.	Fahrenheit.	Eng. Inches.	Fahrenheit.	Eng. Inche
0°	0.051	31°	0.179	62°	0.551	93°	1.514
1 '	0.053	32	0.186	63	0.570	94	1.562
2	0.056	33	0.193	64	0.590	95	1 610
3	0.058	34	0.200	65	0.611	96	1.660
4	0.060	35	0.208	66	0.632	97	1.712
5	0.063	36	0.216	37	0.654	98	1.764
6	0.066	37	0.224	68	0.676	99	1.819
7	0.069	38	0.233	69	0.699	100	1.874
8	0.071	39	0.242	70	0.723	101	1.931
9	0.074	40	0.251	71	0.748	102	1.990
10	0.078	41	0.260	72	0.773	103	2.050
11	0.081	42	0.270	73	0.799	104	2.112
12	0.084	43	0.280	74	0.826	105	2.176
13	0.088	44	0.291	75	0.854	106	2.241
14	0.092	45	0.302	76	0.882	107	2.307
15	0.095	46	0.313	77	0.911	108	2.376
16	0.099	47	0.324	78	0.942	109	2.447
17	0.103	48	0.336	79	0.973	110	2.519
18	0.107	49	0.349	80	1.005	111	2.593
19	0.112	50	0.361	81	1.036	112	2.669
20	0.116	51	0.375	82	1.072	113	2.747
21	0.121	52	0.389	83	1.106	114	2.826
22	0.126	53	0.402	84	1.142	115	2.908
23	0.131	54	0.417	85	1.179	116	2.992
24	0.136	55	0.432	86	1.217	117	3.078
25	0.142	56	0.447	87	1.256	118	3.166
26	0.147	57	0.463	88	1.296	119	3.257
27	0.153	58	0.480	89	1.337	120	3.349
28	0.159	59	0.497	90	1.380	121	3.444
29	0.165	60	0.514	91	1.423	122	3.542
30	0.172	61	0.532	92	1.468	123	3.641
31	0.179	62	0.551	93	1.514	124	3.743

#### TABLE XXII.

FOR SHOWING THE DIFFERENCES IN THE VALUES OF THE ELASTIC FORCE OF AQUEOUS VAPOR ADOPTED BY DIFFERENT AUTHORITIES.

THE following synoptic view of the values of the elastic force of vapor adopted by various authorities, furnishes the means of readily comparing them, and of appreciating the amount of the differences which they exhibit. The values are given both in English and in French measures.

Dalton's values are copied from the Edinburgh Encyclopædia, Art. Hygrometry. Those adopted in the Greenwich Observations are found in the same article, and also in the volumes published annually by that Observatory. Biot's table of tensions is, in fact, the same, computed by Pouillet from Dalton's results, by Biot's formula, and published in Biot's Traité de Physique, Tom. I. p. 531. Dr. Ure's results are taken from his Memoir in the Philosophical Transactions for 1818, p. 347. In the column headed "Daniell" are given the forces of vapor as found in the table published in his Meteorological Essays, 2d edition, p. 596, a table computed by Galbraith, from Dr. Ure's experiments, by the formula of Ivory.

For the columns headed Royal Society, August, Kaemtz, Magnus, and Regnault, see above, p. 147.

# XXII. FOR SHOWING THE DIFFERENCES IN THE VALUES OF THE ELASTIC FORCE OF AQUEOUS VAPOR, ADOPTED BY DIFFERENT AUTHORITIES.

# FORCE OF VAPOR EXPRESSED IN ENGLISH INCHES FOR TEMPERATURES OF FAHRENHEIT.

Temper-				Force of	Vapor acc	ording to			10.2	Temper-
ature of Air, Fahren- heit.	Dalton.	Green- wich Observa- tions.	Ure.	Daniell.	Royal Society.	August.	Kaemtz.	Magnus.	Regnault.	ature of Air, Fahren- heit.
. 0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	0
0	0.064	0.061		0.068	0.051	0.053	0.048	0.044	0.043	0
10	0.090	0.089		0.098	0.078	0.082	0.074	0.070	0.068	10
20	0.129	0.129		0.140	0.116	0.124	0.112	0.108	0.108	20
30	0.186	0.186		0.200	0.172	0.184	0.166	0.164	0.167	30
32	0.200	0.199	0.200	0.216	0.186	0.199	0.180	0.178	0.181	32
40	0.263	0.264	0.250	0.280	0.251	0.269	0.244	0.245	0.248	40
50	0.375	0.373	0.360	0.400	0.361	0.390	0.354	0.359	0.361	50
60	0.524	0.523	0.516	0.560	0.516	0.547	0.505	0.517	0.518	60
70	0.721	0.727	0.726	0.770	0.723	0.766	0.710	0.733	0.733	70
80	1.000	1.001	1.010	1.060	1.005	1.058	0.988	1.025	1.023	80
90	1.360	1.368	1.360	1.430	1.380	1.442	1.354	1.412	1.410	90
95	1.580	1.594	1.640	1.636	1.562	1.677	1.581	1.649	1.647	95
100	1.860	1.852	1.860		1.874			1.921	1.918	100

# FORCE OF VAPOR EXPRESSED IN MILLIMETRES FOR CENTIGRADE TEMPERATURES.

Temper-				Force of	Vapor acc	ording to			1314 - F	Tempe
ature of Air, Centi- grade.	Dalton.	Green- wich Observa- tions.	Biot.	Daniell.	Royal Society.	August.	Kaemtz.	Magnus.	Regnault.	ature of Air Centi- grade
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	0
-20			1.33			1.15	1.01	0.91	0.91	-20
-15	1.93	1.88	1.88	2.11	1.60	1.69	1.51	1.40	1.38	-15
-10	2.64	2.62	2.63	2.92	2.34	2.48	2.21	2.11	2.08	-10
- 5	3.66	3.66	3.66	4.01	3.33	3.56	3.20	3.11	3.13	- 5
0	5.08	5.06	5.06	5.49	4.72	5.05	4.58	4.52	4.60	0
+ 5	6.93	6.95	6.95	7.42	6.60	7.08	6.45	6.47	6.53	+ 5
10	9.52	9.48	9.47	10.16	9.17	9.90	9.00	9.13	9.16	10
15	12.88	12.85	12.84	13.79	12.62	13.44	12.38	12.68	12.70	15
20	17.17	17.30	17.31	18.34	17.17	18.20	16.87	17.40	17.39	20
25	23.11	23.12	23.09	24.54	23.14	24.18	22.74	23.58	23.55	25
30	30.73	30.70	30.64	32.33	30.91	32.39	30.36	31.60	31.55	30
35	40.13	40.47	40.40	41.55	40.89	42.59	40.15	41.89	41.83	35
40			53.00		53.64			54.96	54.91	40

XXIII. WEIGHT OF VAPOR, IN GRAMMES, CONTAINED IN A CUBIC METRE OF SATURATED AIR, AT TEMPERATURES BETWEEN —20° AND +40° CENTIGRADE.—POUILLET.

Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.
Centigrade.	Millim.	Grammes.	Centigrade.	Millim.	Grammes.	Centigrade.	Millim	Grammes.
-20°	1.3	1.5	11°	10.1	10.3	26°	24.4	23.8
-15	1.9	2.1	12	10.7	10.9	27	25.9	25.1
-10	2.6	2.9	13	11.4	11.6	28	27.4	26.4
- 5	3.7	4.0	14	12.1	12.2	29	29.0	27.9
0	5.0	5.4	15	12.8	13.0	30	30.6	29.4
1800 A			0		A CONTRACTOR	100		1 100
+ 1	5.4	5.7	16	13.6	13.7	31	32.4	31.0
2	5.7	6.1	17	14.5	14.5	32	34.3	32.6
3	6.1	6.5	18	15.4	15.3	33	36.2	34.3
4	6.5	6.9	19	16.3	16.2	34	38.3	36.2
5	6.9	7.3	20	17.3	17.1	35	40.4	38.1
		<b>建作业</b>	0 674	EQT.01	1000			
6	7.4	7.7	21	18.3	18.1	36	42.7	40.2
7	7.9	8.2	22	19.4	19.1	37	45.0	42.2
8	8.4	8.7	23	20.6	20.2	38	47.6	44.4
9	8.9	9.2	24	21.8	21.3	39	50.1	46.7
10	9.5	9.7	25	23.1	22.5	40	53.0	49.2

XXIV. WEIGHT OF VAPOR, IN GRAMMES, CONTAINED IN A CUBIC METRE OF SATURATED AIR, AT TEMPERATURES BETWEEN  $-25^{\circ}$  AND  $+36^{\circ}$  CENTIGE. — KAEMTZ.

Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.
							1 172 110	
Centigrade.	Millim.	Grammes.	Centigrade.	Millim.	Grammes.	Centigrade.	· Millim.	Grammes.
-25°	0.77	0.93	-4°	3.83	4.37	16°	14.28	14.97
-24	0.83	1.01	-3	4.11	4.70	17	15.20	15.84
-23	0.90	1.10	-2	4.40	5.01	18	16.08	16.76
-22	0.99	1.19	-1	4.71	5.32	19	17.01	17.75
-21	1.06	1.26	0	5.05	5.66	20	18.20	18.77
BANK T			W. (1			0.10		S I TEAT
-20	1.15	1.38	+1	5.41	6.00	21	19.33	19.82
-19	1.26	1.47	2	5.80	6.42	22	20.51	20.91
-18	1.33	1.60	3	6.20	6.84	23	21.75	22.09
-17	1.44	1.74	4	6.63	7.32	24	23.01	23.36
-16	1.56	1.84	5	7.08	7.77	25	24.18	24.61
PAR H								
-15	1.69	2.00	6	7.58	8.25	26	25.81	25.96
-14	1.80	2.14	7	8.10	8.79	26	27.39	27.34
-13	1.96	2.33	8	8.64	9.30	28	28.96	28.81
-12	2.12	2.48	9	9.23	9.86	29	30.63	30,35
-11	2.30	2.63	10	9.90	10.57	30	32.39	31.93
		La Fri					02.00	
-10	2.48	2.87	11	10.49	11.18	31	34.24	33.65
- 9	2.66	3.08	12	11.17	11.53	32	36.18	35.45
- 8	2.86	3.30	13	11.86	12.57	33	38.21	37.20
- 7	3.09	3.53	14	12.66	13.33	34	40.38	39.12
- 6	3.32	3.80	15	13.44	14.17	35	42.59	41.13
- 5	3,56	4.08	16	14.28	14.97	36	44.96	43.17

#### XXV. FORCES OF VAPOR AND RELATIVE HUMIDITY,

CORRESPONDING TO THE DEGREES OF SAUSSURE'S HAIR-HYGROMETER, AT THE TEMPERATURE OF 10° CENTIGRADE.

From the Experiments of Gay-Lussac.

The force of vapor is expressed in hundredths, the tension at full saturation being represented by 100.

Degrees of Hair-Hy- grometer.	Force of Vapor.	Relative Humidity in Thou- sandths.	Degrees of Hur-Hy- grometer.	Force of Vapor.	Relative Humidity in Thou- sandths.	Degrees of Hair-Hy- grometer.	Force of Vapor.	Relative Humidity in Thou- sandths.
0			0			0		
0.	0.00	0.000	34	17.10	0.100	67	43.73	THE PARTY OF
1	0.45	PART THE	35	17.68	0.177	68	44.89	
2	0.90	N 17 5 19	36	18.30	S. Latin S. Co.	69	46.04	0 100
3	1.35		37	18.92		70	47.19	0.472
4	1.80		38	19.54		71	48.51	444
5	2.25	0.022	39	20.16		72	49.82	0.500
6	2.71		40	20.78	0.208	73	51.14	
7	3.18	<b>可以发示和</b>	41	21.45	Sept Diggs	74	52:45	and the second
8	3.64	natio s'iro	42	. 22.12	Enghalit 3	75	53.76	0.538
9	4.10	ro limate	43	22.79	anies ilea	76	55.25	1000
10	4.57	0.046	44	23.46	O CO 911	77	56.74	
11	5.05	Sale Ballet	45	24.13	0.241	78	58.24	+ The
12	5.52	1000000000	46	24.86	agy films	79	59.73	
13	6.00	I II that	47	25.59		80	61.22	0.612
14	6.48		48	26.32		81	62.89	
15	6.96	0.070	49	27.06	SAMMAN	82	64.57	
16	7.46	1 1/3	50	27.79	0.278	83	66.24	
17	7.95		51	28.58		84	67.92	100
18	8.45		52	29.38		85	69.59	0.696
19	8.95		53	30.17		86	71.49	
20	9.45	0.094	54	30.97	City State on	87	73.39	
21	9.97	0.004	55	31.76	0.318	88	75.29	
22	10.49		56	32.66	0.013	89	77.19	
23	11.01		57	33.57	THE REAL	90	79.09	0.791
24	11.53	at is	58	34.47	100	91	81.09	
25	-0.0-			TRANS.				13 348
25	12.05	0.120	59	35.37	0.000	92	83.08	
26	12.59		60	36.28	0.363	93	85.08	
27 28	13.14 13.69	FALL BY	61	37.31 38.34	( 中	94	87.07	0.00
28	13.69		62	39.36		95	89.06	0.891
29	14.23		63	39.30	3 30 45	96	91.25	
30	14.78	0.148	-64	40.39		97	93.44	-
31	15.36	THE REST	65	41.42	0.414	98	95.63	THO TO
- 32	15.94		66	42.58		99	97.81	in tab
33	16.52		67	43.73	CALLY TO	100	100.00	1.000

#### XXVI.

#### TABLE

FOR

DEDUCING THE RELATIVE HUMIDITY IN HUNDREDTHS, FROM THE INDICATIONS OF

SAUSSURE'S HAIR-HYGROMETER;

Calculated from the Experiments of Melloni.

By M. T. HAEGHENS.

The Hair-Hygrometer of Saussure having been formerly used for long series of observations, and being still employed by some meteorologists, notwithstanding the imperfection of this instrument, on account of its giving directly the relative humidity without calculation, it was desirable to ascertain the correspondence of the degrees of that hygrometer with the relative humidity expressed in hundredths, as in the preceding table. Though these instruments compared with each other, show very often great discrepancies in their indications, yet a large number of them agree sufficiently well with the experiments of Melloni, August, and others, to allow the following table of comparison to be constructed, which table may be considered as giving good approximations. For the calculation of it, Mr. Haeghens used the results of Melloni, which agree also satisfactorily with a series of observations very carefully made by M. Delcros. See Annuaire Météorologique de la France, pour 1850.

#### RELATIVE HUMIDITY IN HUNDREDTHS.

Degrees of Saussure's Hygrome-			]	Degrees	of Saussi Un		grometer.		DI T	
ter. Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity
0	0	0	1	1	2	3	3	4	4	5
1	5	6	6	7	8	8	. 9	10	11	11
2	12	12	13	14	15	16	17	18	· 18	19
3	19	20	21	22	23	24	24	25	26	26
4	- 27	27	28	28	29	30	31	32	33	34
5	35	36	37	37	38	39	40	41	42	43
6	44	45	46	47	49	50	51	52	53	55
7	56	57	58	59	61	62	63	65	66	68
8	69	70	72	73	75	77	78	79	81	82
9	83	85	87	88	90	91	93	95	97	98
10	100	1.					٧.		11.	201

### TABLE XXVII.

The following Table shows the Relative Humidity, in hundredths, corresponding to the degrees of Saussure's Hair-Hygrometer, as determined by various physicists. It is found in Kaemtz, Vorlesungen über Meteorologie, page 100; also in the French translation by Martins, Cours de Météorologie, page 80.

XXVI. RELATIVE HUMIDITY, CORRESPONDING TO THE DEGREES OF SAUSSURE'S HAIR-HYGROMETER.

Saturation = 100.

Degrees		Relative Humid	ity according to		Degrees
of Hair- Hygrometer.	Gay-Lussac.	Prinsep.	August.	Melloni.	Hair- Hygrometer
100°	100.0	100.0	100.0	100.0	100°
95	89.1	88.7	94.0	90.8	95
90	79.1	78.2	86.0	83.1	90 -
85	69.6	. 68.3	79.0	76.5	85
80	61.2	59.2	71.0	68.9	80
75	53.8	50.6	64.0	62.0	75
70	47.2	43.6	56.0	55.6	70
65	41.4	37.2	48.0	49.6	65
60	36.3	31.5	41.0	44.0	60
55	31.8	26.3	36.0	39.1	55
50	27.8	21.8	31.0	34.6	50
45	24.1	17.7	27.0	29.8	45
40	20.8	14.3	23.0	27.0	40
35	17.7	11.4	19.0	23.8	35
30	14.8	9.1	16.0	19.0	30
25	12.0	7.1	13.0	16.4	25
20	9.4	4.9	10.0	11.7	20
15	7.0	3.0	7.0	8.3	15
10	4.6	1.6	4.0	5.0	10
5	2.2	0.6	2.0	2.6	. 5
0	0.0	0.0	0.0	0.0	0

The following There are a first to the property of the control of the control of the tenth of the second of the se

A CONTRACTOR OF THE STREET OF

# APPENDIX

TO

THE HYGROMETRICAL TABLES.

WHITE WEEKER HE THE LITTERAND WHITE DEVENTED

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#### TABLES

FOR

### COMPARING THE QUANTITIES OF RAIN-WATER.

The three kinds of measures which are most in use for noting the quantities of rain and melted snow, are the Centimetres and Millimetres in France, the Paris or French inches and lines in Germany, and the English inches and decimals in England, America, and also in Russia, the Russian foot being the same as the English foot. The following tables will facilitate the comparison of these various measures with each other.

A glance at the tables will show that the first column on the left contains the numbers to be converted, and the heads of the following columns the fractions of these numbers, or units, each of which is one tenth of those in the first column. Shorter tables, at the bottom, give, when necessary, the value of proportional parts still smaller than those found in the larger tables.

#### Example.

Let 13 Centimetres be converted into French inches and lines.

Take, in Table II., the line beginning with 10 Centimetres in the first column, follow that line as far as the column headed 3 Centimetres, and there will be found the number of 4 inches 9.63 lines, which is the corresponding value in French inches of 10 + 3, or 13 Centimetres.

If the number is followed by a fraction, as for instance, 13.5 Centimetres, or 135 Millimetres, we find,—

In the larger table 13 Centimetres =  $\frac{4}{0.963}$  In the smaller table at the bottom  $\frac{5}{13.5}$  Centimetres =  $\frac{.2,216}{4.11,846}$ 

When the measures which are to be compared are both subdivided into decimal parts, the equivalents of the numbers greater than 9.9 may be found by moving the decimal point.

# Example.

Let 346.7 Centimetres be converted into English inches.

In Table I., in the column headed 4, on the fourth line,

we find 3.4 Centimetres = 1.3386 English inches.

Moving the decimal point by two places we have

340 Centimetres = 133.86 English inches.

Then, in the column headed 7, on the

line beginning with 6, we find 6.7 Centimetres = 2.64

Making together  $\overline{346.7}$  Centimetres =  $\overline{136.50}$  English inches.

1 Centimetre = 0.3937079 English Inch

1 Centimetre = 0.3937079 English Inch.  Millimetres.											
Centi-		1			Milli	1	i		1	I	
metres	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Eng.Inc		h. Eng.Inch			-	The second second		1	-	
0	0.000				0.1575		0.2362	0.2756	0.3150	0.354	
1	0.393	7 0.433			0.5512			0.6693	0.7087	0.748	
2	0.787	A DOMESTIC	100000000000000000000000000000000000000	THE REAL PROPERTY.	0.9449	A STATE OF THE PARTY OF THE PAR	1.0236	1.0630	1.1024	1.141	
3	1.181			1	1.3386	A CALL TO A SEC.	1.4173	1.4567	1.4961	1.535	
4	1.5748				1.7323		1.8111	1.8504	1.8898	1.929	
5	1.968				2.1260		2.2048	2.2441	2.2835	2.322	
6	2.362				2.5197	THE RESERVE	2.5985	2.6378	2.6772	2.716	
7	2.7560		The state of	2.8741	2.9134	The second second	2.9922	3.0316	3.0709	3.110	
8	3.149		1	3.2678	3.3071	3.3465	3.3859	3.4253	3.4646	3.504	
9	3.5434	1 3.5827	3.6221	3.6615	3.7009	3.7402	3.7796	3.8190	3.8583	3.897	
II. CONVERSION OF CENTIMETRES INTO FRENCH INCHES, LINES, AND DECIMALS.  1 Centimetre = 0. inches 4.43296 Paris lines.											
		1 50 M		and State	Uni	ts.	2000	final ree	-ACTOR/LIN	1217 1081	
Centi- netres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
1000	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin. I	r.In. Lin. F	r.In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Li	
0	0. 0,00	0. 4,43	0. 8,87	1. 1,30	1. 5,73	1.10,16	2. 2,60	2. 7,03	2.11,46	3. 3,9	
10	3. 8,33	4. 0,76	4. 5,20	4. 9,63	5. 2,06	5. 6,49	5.10,93	6. 3,36	6. 7,79	7. 0,2	
20	7. 4,66	7. 9,09	8. 1,53	8. 5,96	8.10,39	9. 2,82	9. 7,26	9.11,69	10. 4,12	10. 8,	
30	11. 0,99	11. 5,42	11. 9,85	2. 2,29 1	2. 6,72	12.11,15	13. 3,59	13. 8,02	14. 0,45	14. 4,8	
40	14. 9,32	15. 1,75	15. 6,18	5.10,62	6. 3,05	16. 7,48	16.11,92	17. 4,35	17. 8,78	18. 1,2	
50	18. 5,65	18.10,08	19. 2,51	9. 6,95 1	9.11,38	20. 3,81	20. 8,25	21. 0,68	21. 5,11	21. 9,	
60	22. 1,98	22. 6,41	22.10,84	23. 3,28 2	3. 7,71	24. 0,14	24. 4,58	24. 9,01	25. 1,44	25. 5,8	
70	25.10,31	26. 2,74	26. 7,17	26.11,61 2	7. 4,04	27. 8,17	28. 0,90	28. 5,34	28. 9,77	29. 2,2	
80	29. 6,64	29.11,07	30. 3,50	30. 7,93	1. 0,37	31. 4,80	31. 9,23	32. 1,67	32. 6,10	32.10,	
90	33. 2,97	33. 7,40	33.11,83	34. 4,26	4. 8,70	35. 1,13	35. 5,56	35.10,00	36. 2,43	36. 6,8	
1	Centim.	Fr.In. Lin.	Centim. F	r.In. Lin.	Centim.	Fr.In, Lin.	Centim.	Fr.In. Lin.	Centim.	Fr.In. Li	
	100	36.11,30	200 7	3.10.59	300	110.9,89	400	147.9,18	500	184.8,4	
	CONVE	RSION (	F CENT	METRES	INTO	FRENCH	LINES	AND DE	CINALS.		
Centi-				militare.	U	nits.			LC LG		
metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
JENNY.	Fr. Line	s. Fr. Lines	Fr. Lines.	Fr. Lines.	Fr. Lines.	Fr. Lines.	Fr. Lines.	Fr. Lines.	Fr. Lines.	Fr. Line	
0	0.00			13.30	17.73	22.16	26.60	31.03	35.46	39.9	
10	44.33	48.76	53.20	57.63	62.06	66.49	70.93	75.36	79.79	84.2	
20	88.66	93.09	97.53	101.96	106.39	110.82	115.26	119.69	124.12	128.5	
30	132.99	137.42	141.85	146.29	150.72	155.15	159.59	164.02	168.45	172.8	
40	177.32	181.75	186.18	190.62	195.05	199.48	203.92	208.35	212.78	217.2	
50	221.65		230.51	234.95	239.38	243.81	248.25	252.68	257.11	261.5	
60	265.98	270.41	274.84	279.28	283.71	288.14	292.58	297.01	301.44	305.8	
70	310.31		319.17	323.61	328.04	332.47		341.34	345.77	350.20	
80	354.64			367.93	372.37	376.80	381.23	385.67	390.10	394.58	
90	398.97	7   403.40	407.83	412.26	416.70	421.13	425.56	430.00	434.43	438.86	
	CONVE	RSION C	F MILLI	METRES	INTO I	FRENCH	LINES .	AND DE	CIMALS.	ar , to t	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Fr. Line	s. Fr. Lines 0.443	Fr. Lines. 0.887	Fr. Lines. 1.330	Fr. Lines 1.773	Fr. Lines. 2.216	Fr. Lines. 2.660	Fr. Lines. 3.103	Fr. Lines. 3.546	Fr. Lines 3.990	

		A STATE	11	English Inc	h = 2.5399	5 Centime	res.			
English		No.			U	nits.			,	
English Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
Hef?	Centim			Centim.			Centim.	Centim.	Centim.	Centim
0	0.00		100	7.62	1	111111111111111111111111111111111111111	15.24	17.78	20.32	22.8
10	25.40					A STATE OF	40.64	100000000000000000000000000000000000000	45.72	48.2
20	50.80					100000000000000000000000000000000000000	66.04		71.12	73.6
30	76.20		2000				91.44	- Mariana Contract	96.52	99.0
40	101.60			1	-		116.84	119.38	121.92	124.4
50	127.00			100-51-00-00-00-00-00-00-00-00-00-00-00-00-00	THE PERSON	A STREET, ST.	142.24	THE PARTY OF THE P	147.32	149.8
60	152.40	A STATE OF THE STA					167.64	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	172.72	175.2
70	177.80			185.42		A CONTRACTOR OF THE PARTY OF TH	193.04	195.58	198.12	200.6
80	203.20	1000000			190	THE PERSON NAMED IN	218.44	COMPLETE A	223.52	226.0
90	228.60			110000000000000000000000000000000000000	10000	A CALL DATE OF	243.84	246.38	248.92	251.4
100	254.00	256.54	259.08	261.62	264.16	266.70	269.24	271.78	274.32	276.8
110	279.39	281.93	284.47	287.01	289.55	292.09	294.63	297.17	299.71	302.2
120	304.79	307.33	309.87	312.41	314.95	317.49	320.03	322.57	325.11	327.6
130	330.19	332.73	335.27	337.81	340.35	342.89	345.43	347.97	350.51	353.0
140	355.59	358.13	360.67	363.21	365.75	368.29	370.83	373.37	375.91	378.4
150	380.99	383.53	386.07	388.61	391.15	393.69	396.23	398.77	401.31	403.8
160	406.39	408.93	411.47	414.01	416.55	419.09	421.63	424.17	426.71	429.2
170	431.79	434.33	436.87	439.41	441.95	444.49	447.03	449.57	452.11	454.6
180	457.19	No. of the last		464.81	THE PURPLE	CONTRACTOR OF THE PARTY OF	472.43	474.97	477.51	480.0
190	482.59			490.21		495.29	497.83	1	502.91	505.4
200	507.99	510.53	513.07	515.61	518.15	520.69	523.23	525.77	528.31	530.8
200	Tenths of an Inch.									
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	0		0	0		0	0	G .:	0	-
	Centim 0.000	. Centim. 0.254	Centim. 0.508	Centim. 0.762	1.016	Centim. 1.270	Centim. 1.524	Centim. 1.778	Centim. 2.032	Centim 2.286
O CLIPS	0.000	0.254	0.308	0.702	1.010	1.270	1.024	1.770	2.034	2.200
I	v. conv	ERSION	OF ENG		CHES I			NCHES A	ND LIN	ES.
Eng.					· Un	its.	集/工			9
nches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
,440			Fr.In. Lin. I							
0			1.10,52							
	0 4 50	10. 3,85	11. 3,11							
10					00 0 00	00 F 40		95 4 01	26, 3,27	
10 20	18. 9,19	19. 8,45								
10 20 30	18. 9,19 28. 1,78	19. 8,45 29. 1,04	30. 0,30	30.11,56	31.10,82	32.10,08	33. 9,34	34. 8,60	35. 7,86	
10 20 30 40	18. 9,19 28. 1,78 37. 6,38	19. 8,45 29. 1,04 38. 5,64	30. 0,30 3 39. 4,90 4	30.11,56 40. 4,16	31.10,82 41. 3,42	32.10,08 42. 2,68	33. 9,34 43. 1,94	34. 8,60 44. 1,20	35. 7,86 45. 0,46	45.11,7
10 20 30 40 50	18. 9,19 28. 1,78 37. 6,38 46.10,97	19. 8,45 29. 1,04 38. 5,64 47.10,23	30. 0,30 3 39. 4,90 4 48. 9,49 4	30.11,56 40. 4,16 49. 8,75	31.10,82 41. 3,42 50. 8,01	32.10,08 42. 2,68 51. 7,27	33. 9,34 43. 1,94 52. 6,53	34. 8,60 44. 1,20 53. 5,79	35. 7,86 45. 0,46 54. 5,05	45.11,7 55. 4,3
10 20 30 40 50 60	18. 9,19 28. 1,78 37. 6,38 46.10,97 56. 3,57	19. 8,45 29. 1,04 38. 5,64 47.10,23 57. 2,83	30. 0,30 3 39. 4,90 4 48. 9,49 4 58. 2,09 5	30.11,56 40. 4,16 49. 8,75 59. 1,35	31.10,82 41. 3,42 50. 8,01 60. 0,61	32.10,08 42. 2,68 51. 7,27 60.11,87	33. 9,34 43. 1,94 52. 6,53 61.11,13	34. 8,60 44. 1,20 53. 5,79 62.10,39	35. 7,86 45. 0,46 54. 5,05 63. 9,65	45.11,7 55. 4,3 64. 8,9
10 20 30 40 50 60 70	18. 9,19 28. 1,78 37. 6,38 46.10,97 56. 3,57 65. 8,16	19. 8,45 29. 1,04 38. 5,64 47.10,23 57. 2,83 66. 7,42	30. 0,30 3 39. 4,90 4 48. 9,49 4 58. 2,09 5 67. 6,68 6	30.11,56 40. 4,16 49. 8,75 59. 1,35 68. 5,94	31.10,82 41. 3,42 50. 8,01 60. 0,61 69. 5,20	32.10,08 42. 2,68 51. 7,27 60.11,87 70. 4,46	33. 9,34 43. 1,94 52. 6,53 61.11,13 71. 3,72	34. 8,60 44. 1,20 53. 5,79 62.10,39 72. 2,98	35. 7,86 45. 0,46 54. 5,05 63. 9,65 73. 2,24	45.11,7 55. 4,3 64. 8,9 74. 1,5
10 20 30 40 50 60 70 80	18. 9,19 28. 1,78 37. 6,38 46.10,97 56. 3,57 65. 8,16 75. 0,76	19. 8,45 29. 1,04 38. 5,64 47.10,23 57. 2,83 66. 7,42 76. 0,02	30. 0,30 3 39. 4,90 4 48. 9,49 4 58. 2,09 5 67. 6,68 6 76.11,28 7	30.11,56 40. 4,16 49. 8,75 59. 1,35 58. 5,94 77.10,54	31.10,82 41. 3,42 50. 8,01 60. 0,61 69. 5,20 78. 9,80	32.10,08 42. 2,68 51. 7,27 60.11,87 70. 4,46 79. 9,06	33. 9,34 43. 1,94 52. 6,53 61.11,13 71. 3,72 80. 8,32	34. 8,60 44. 1,20 53. 5,79 62.10,39 72. 2,98 81. 7,58	35. 7,86 45. 0,46 54. 5,05 63. 9,65 73. 2,24 82. 6,84	45.11,7 55. 4,3 64. 8,9 74. 1,5 83. 6,1
10 20 30 40 50 60 70 80 90	18. 9,19 28. 1,78 37. 6,38 46.10,97 56. 3,57 65. 8,16 75. 0,76 84. 5,35	19. 8,45 29. 1,04 38. 5,64 47.10,23 57. 2,83 66. 7,42 76. 0,02 85. 4,61	30. 0,30 3 39. 4,90 4 48. 9,49 4 58. 2,09 5 67. 6,68 6 76.11,28 7 86. 3,87 8	30.11,56 40. 4,16 49. 8,75 69. 1,35 68. 5,94 67.10,54	31.10,82 41. 3,42 50. 8,01 60. 0,61 69. 5,20 78. 9,80 88. 2,39	32.10,08 42. 2,68 51. 7,27 60.11,87 70. 4,46 79. 9,06 39. 1,65	33. 9,34 43. 1,94 52. 6,53 61.11,13 71. 3,72 80. 8,32 90. 0,91	34. 8,60 44. 1,20 53. 5,79 62.10,39 72. 2,98 81. 7,58 91. 0,17	35. 7,86 45. 0,46 54. 5,05 63. 9,65 73. 2,24 82. 6,84 91.11,43	45.11,7 55. 4,3 64. 8,9 74. 1,5 83. 6,1 92.10,6
10 20 30 40 50 60 70 80 90	18. 9,19 28. 1,78 37. 6,38 46.10,97 56. 3,57 65. 8,16 75. 0,76 84. 5,35	19. 8,45 29. 1,04 38. 5,64 47.10,23 57. 2,83 66. 7,42 76. 0,02 85. 4,61	30. 0,30 3 39. 4,90 4 48. 9,49 4 58. 2,09 5 67. 6,68 6 76.11,28 7 86. 3,87 8 Eng.Inch. F	30.11,56 40. 4,16 49. 8,75 69. 1,35 68. 5,94 67.10,54	31.10,82 41. 3,42 50. 8,01 60. 0,61 69. 5,20 78. 9,80 88. 2,39 Eng.Inch.	32.10,08 42. 2,68 51. 7,27 60.11,87 70. 4,46 79. 9,06 39. 1,65	33. 9,34 43. 1,94 52. 6,53 61.11,13 71. 3,72 80. 8,32 90. 0,91	34. 8,60 44. 1,20 53. 5,79 62.10,39 72. 2,98 81. 7,58 91. 0,17	35. 7,86 45. 0,46 54. 5,05 63. 9,65 73. 2,24 82. 6,84 91.11,43	45.11,7 55. 4,3 64. 8,9 74. 1,5 83. 6,1 92.10,6

0.

1.

0.0,00 | 0.1,13 | 0.2,25 | 0.3,38

2.

3.

Fr.In. Lin. Fr.In. Lin.

4.

5.

6.

7.

0.4,50 | 0.5,63 | 0.6,76 | 0.7,88 | 0.9,01 | 0.10,13

8.

### V. CONVERSION OF FRENCH INCHES INTO CENTIMETRES.

1 French Inch = 2.7070 Centimetres.

French		Units.											
Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim			
0	0.00	2.71	5.41	8.12	10.83	13.53	16.24	18.95	21.66	24.36			
10	27.07	29.78	32.48	35.19	37.90	40.60	43.31	46.02	48.73	51.48			
20	54.14	56.85	59.55	62.26	64.97	67.67	70.38	73.09	75.80	78.50			
30	81.21	83.92	86.62	89.33	92.04	94.74	97.45	100.16	102.87	105.57			
40	108.28	110.99	113.69	116.40	119.11	121.81	124.52	127.23	129.94	132.64			
50	135.35	138.06	140.76	143.47	146.18	148.88	151.59	154.30	157.01	159.71			
		Essex III	- IN THE ST	ni il erah	THE Y	MAN TO I	there you	Hall A					
60	162.42	165.13	167.83	170.54	172.25	175.95	178.66	181.37	184.08	186.78			
70	189.49	192.20	194.90	197.61	200.32	203.02	205.73	208.44	211.15	213.85			
80	216.56	219.27	221.97	224.68	227.39	230.09	232.80	235.51	238.22	240.92			
90	243.63	246.34	249.04	251.75	254.46	257.16	259.87	262.58	265.29	267.99			
100	270.70	273.41	276.11	278.82	281.53	284.23	286.94	289.65	292.36	295.06			
			Shill in	AL THE WAY		71.3	an Plant	9.00	647.	2 H N			
110	297.77	300.48	303.18	305.89	308.60	311.30	314.01	316.72	319.42	322.13			
120	324.84	327.55	330.25	332.96	335.67	338.37	341.08	343.79	346.49	349.20			
130	351.91	354.62	357.32	360.03	362.74	365.44	368.15	370.86	373.56	376.27			
140	378.98	381.69	384.39	387.10	389.81	392.51	395.22	397.93	400.63	403.34			
150	406.05	408.76	411.46	414.17	416.88	419.58	422.29	425.00	427.70	430.41			
			Part III			A COUNTY		STORY OF	146				
160	433.12	435.83	438.53	441.24	443.95	446.65	449.36	452.07	454.77	457.48			
170	460.19	462.90	465.60	468.31	471.02	473.72	476.43	479.14	481.84	484.55			
180	487.26	489.97	492.67	495.38	498.09	500.79	503.50	506.21	508.91	511.62			
190	514.33	517.04	519.74	522.45	525.16	527.86	530.57	533.28	535.98	538.69			
200	541.40	544.11	546.81	549.52	552.23	554.93	557.64	560.35	563.05	565.76			

#### CONVERSION OF FRENCH LINES INTO CENTIMETRES.

#### 1 French Line = 0.22558 Centimetre.

French		N3	Dille-	17.	Tenths o	f a Line.			WATE		
Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
4 100	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	
0	0.000	0.023	0.045	0.068	0.090	0.113	0.135	0.158	0.180	0.203	
1	0.226	0.248	0.271	0.293	0.316	0.338	0.361	0.383	0.406	0.429	
2	0.451	0.474	0.496	0.519	0.541	0.564	0.587	0.609	0.632	0.654	
3	0.677	0.699	0.722	0.744	0.767	0.790	0.812	0.835	0.857	0.880	
4	0.902	0.925	0.947	0.970	0.993	1.015	1.038	1.060	1.083	1.105	
5	1.128	1.150	1.173	1.196	1.218	1.241	1.263	1.286	1.308	1.331	
6	1.353	1.376	1.399	1.421	1.444	1.466	1.489	1.511	1.534	1.557	
. 7	1.579	1.602	1.624	1.647	1.669	1.692	1.714	1.737	1.760	1.782	
8	1.805	1.827	1.850	1.872	1.895	1.917	1.940	1.963	1.985	2.008	
9	2.030	2.053	2.075	2.098	2.120	2.143	2.166	2.188	2.211	2.233	
10	2.256	2.278	2.301	2.324	2.346	2.369	2.391	2.414	2.436	2.459	
11	2.481	2.504	2.527	2.549	2.572	2.594	2.617	2.639	2.662	2.684	
12	2.707	2.730	2.752	2.775	2.797	2.820	2.842	2.865	2.887	2.910	

1 French Inch = 1.065765 English Inch.

French Inches.	0.	ME I		Units.												
		1.	2.	3.	4.	5.	6.	7.	8.	9.						
E	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.						
0	0.000	1.066	2.132	3.197	4.263	5.329	6.395	7.460	8.526	9.592						
10	10.658	11.723	12.789	13.855	14.921	15.986	17.052	18.118	19.184	20.250						
20	21.315	22.381	23.447	24.513	25.578	26.644	27.710	28.776	29.841	30.907						
30	31.973	33.039	34.104	35.170	36.236	37.302	38.368	39.433	40.499	41.565						
40	42.631	43.696	44.762	45.828	46.894	47.959	49.025	50.091	51.157	52.222						
50	53.288	54.354	55.420	56.486	57.551	58.617	59.683	60.749	61.814	62.880						
10000	991		1					101 20								
60	63.946	65.012	66.077	67.143	68.209	69.275	70.340	71.407	72.472	73.538						
70	74.604	75.669	76.735	77.801	78.867	79.932	80.998	82.064	83.130	84.195						
80	85.261	86.327	87.393	88.458	89.524	90.590	91.656	92.722	93.787	94.853						
90	95.919	96.985	98.050	99.116	100.182	101.248	102.314	103.379	104.445	105.511						
100 1	106.576	107.642	108.708	109.774	110.840	111.905	112.971	114.037	115.103	116.168						
		1 010	FA	7.42 17:00	ara H		Programme Service									
110 1	17.234	118.300	119.366	120.431	121.497	122.563	123.629	124.695	125.760	126.826						
120 1	27.892	128.958	130.023	131.089	132.155	133.221	134.286	135.352	136.418	137.484						
130 1	38.549	139.615	140.681	141.747	142.813	143.878	144.944	146.010	147.076	148.141						
140 1	49.207	150.273	151.339	152.404	153.470	154.536	155.602	156.667	157.733	158.799						
150 1	59.865	160.931	161.996	163.062	164.128	165.194	166.259	167.325	168.391	169.457						
						81/ E I	H I			20 19						
160 1	70.522	171.588	172.654	173.720	174.785	175.851	176.917	177.983	179.049	180.114						
170 1	81.180	182.246	183.312	184.377	185.443	186.509	187.575	188.640	189.706	190.772						
180 1	91.838	192.903	193.969	195.035	196.101	197.167	198.232	199.298	200.364	201.430						
190 2	02.495	203.561	204.627	205.693	206.758	207.824	208.890	209.956	211.021	212.087						
200 2	13.153	214.219	215.285	216.350	217.416	218.482	219.548	220.613	221.679	222.745						

#### CONVERSION OF FRENCH LINES INTO ENGLISH INCHES.

1 French Line = 0.088814 English Inch.

E		Tenths of a Line.											
French Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng. Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inc			
0	0.0000	0.0089	0.0178	0.0266	0.0355	0.0444	0.0533	0.0622	0.0711	0.079			
1	0.0888	0.0977	0.1066	0.1155	0.1243	0.1332	0.1421	0.1510	0.1599	0.168			
2	0.1776	0.1865	0.1954	0.2043	0.2132	0.2220	0.2309	0.2398	0.2487	0.257			
3	0.2664	0.2753	0.2842	0.2931	0.3020	0.3108	0.3197	0.3286	0.3375	0.346			
4	0.3553	0.3641	0.3730	0.3819	0.3908	0.3997	0.4085	0.4174	0.4263	0.435			
5	0.4441	0.4530	0.4618	0.4707	0.4796	0.4885	0.4974	0.5062	0.5151	0.524			
6	0.5329	0.5418	0.5506	0.5595	0.5684	0.5773	0.5862	0.5951	0.6039	0.612			
7	0.6217	0.6306	0.6395	0.6483	0.6572	0.6661	0.6750	0.6839	0.6927	0.701			
8	0.7105	0.7194	0.7283	0.7372	0.7460	0.7549	0.7638	0.7727	0.7816	0.790			
9	0.7993	0.8082	0.8171	0.8260	0.8349	0.8437	0.8526	0.8615	0.8704	0.879			
10	0.8881	0.8970	0.9059	0.9148	0.9237	0.9325	0.9414	0.9503	0.9592	0.968			
11	0.9770	0.9858	0.9947	1.0036	1.0125	1.0214	1.0302	1.0391	1.0480	1.056			
12	1.0658	1.0746	1.0835	1.0924	1.1013	1.1102	1.1191	1.1279	1.1368	1.145			

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# METEOROLOGICAL TABLES.

III.

BAROMETRICAL TABLES.

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### COMPARISON

OF

# THE BAROMETRICAL SCALES,

OR

### TABLES

FOR CONVERTING THE INDICATIONS OF THE ENGLISH, METRICAL, OLD FRENCH,
AND RUSSIAN BAROMETERS INTO EACH OTHER.

COMPARISON ...

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#### COMPARISON

OF

### THE BAROMETRICAL SCALES.

The following tables are intended for converting into each other the four most important Barometrical Scales. They are sufficiently detailed to save the labor of any calculation or even of interpolation for the ordinary wants of Meteorology. But before making use of them, for comparing the observations taken with barometers of different scales, it is necessary to reduce the observed heights to the temperature of the freezing point, or to any other temperature, provided it be the same for all, by means of the tables calculated for this purpose, and which will be found below. The reason of it may be readily understood.

The length of the bars of metal, or of other substances, which represent the standard measures of length which obtain among different nations, varying with the temperature, it was necessary to determine a fixed point of temperature at which they really ought to have the length adopted as the standard unit of measure. This temperature is the *normal* temperature of the standard, and the length of the standard-bar, at this temperature, is the *true* length of it.

If the normal temperature of the various standards used for dividing Barometrical Scales were the same, the heights of the barometrical column, taken with these scales, could be compared directly, provided the scales be made of the same substance, brass, for instance, because their variations above or below this normal temperature would remain parallel with each other. But unfortunately it is not so. The English Yard is a standard at the temperature of 62° Fahrenheit; the Old French Toise, at 13° Reaumur; the Metre, at the freezing point, or zero Centigrade. Thus metallic rods intended to represent these various units of measure give the true or standard length only when at these respective temperatures; at any other temperature they are longer or shorter than the standard, and their subdivisions, inches, ines, or millimetres, partake of the error.

It is obvious, therefore, that the barometrical heights, taken with different scales, cannot be compared *directly* by means of the following tables, which give the reation between these scales at their respective *normal* temperatures. For suppose he temperature of the three barometers to be the freezing point, or 32° Fahrenheit,

the scale of the Metrical Barometer alone will actually represent the standard length, and the millimeters will have the true length; while the inches and lines of the Old French and of the English Barometers will be too short, causing thus the barometrical column to appear too high. If the temperature of the instruments be 62° Fahrenheit, the divisions of the English Barometer will have the true standard length, and those of the Old French Barometer nearly so; but the millimeters of the Metrical Barometer will be too long, causing the barometrical column to appear too low. It is to neutralize the effect of those inequalities arising from the expansion of the scale that it is necessary, before comparing the observations taken with the three barometers, to reduce them to the same temperature. This is done by means of the tables above mentioned, for reducing the barometer to the freezing point, which suppose the scales to be of brass from top to bottom, and which take into account the expansion or contraction they undergo by the variations of temperature.

But in doing so, we must be aware that the accuracy of the comparison depends in part upon the correctness of the indications of the attached thermometers, which determine the amount of the correction to be applied for reducing the barometers to the freezing point. If the thermometers do not agree, an error is introduced which will affect the height of the reduced columns, and the final comparison. Therefore the correction of the attached thermometers ought to be ascertained and applied to them before the reduction is made; or if this correction is unknown, it will be well to place the instruments to be compared in the most favorable conditions for taking the same temperature, and then to take the temperature given by one of the thermometers to reduce both barometers. If the correction of the attached thermometer has not been applied before the reduction, it will be contained, after the reduction, in the total correction of the instrument. If it be so, this circumstance must be indicated.

In computing the following tables, the value of the Metre, as determined by Capt. Kater, (Philosoph. Transact. for 1818, p. 109, and Baily's Astronomical Tables, p. 192,) has been adopted, viz. 1 Metre, at 0° Centigrade = 39.37079 English inches, at 62° Fahrenheit. The relation of the Metre (legal) to the Old French system of measures is known to be 1 Metre = 443.296 French or Paris lines. From these equations are derived the elements used in the computations, which are found at the head of each table.

Besides the larger Tables I. – VIII., a set of smaller ones, Tables IX. – XVI., has been added, which will be found useful for comparing Barometrical differences, such as ranges, amount of variation in a given time, &c., expressed in measures of different scales, in which only small quantities occur that are not found in the large tables.

I.-II.

#### COMPARISON

OF

## THE ENGLISH BAROMETER

WITH

THE METRICAL AND THE OLD FRENCH BAROMETERS,

OR

## TABLES

FOR CONVERTING ENGLISH INCHES INTO MILLIMETRES, AND INTO FRENCH OR PARIS LINES AND DECIMALS;

GIVING THE VALUES CORRESPONDING TO EVERY TENTH OF AN INCH, FROM 9

TO 19 INCHES; AND TO EVERY HUNDREDTH, FROM

19 TO 31.5 ENGLISH INCHES.

#### USE OF TABLE I.

#### Example.

THE English Barometer reads 20.657 inches. What would be the corresponding height in the Metrical Barometer?

In Table I., first column on the left, look out the line of 20 inches 6 tenths; or that line, in the sixth column, headed 5 hundredths, is found the value in millimetres for

$$20.65$$
 inches =  $524.50$  millimetres.

At the bottom of the page, for 
$$0.007$$
 " = 0.18 " Or for  $20.657$  " = 524.68 "

which would be the reading of the Metrical Barometer.

This example may serve for all tables, throughout the volume, which are constructed on the same plan.

1 English Inch = 25.39954 Millimetres.

Post					Tenths o	f an Inch.				16 3 10 10 3
English Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
Mark S	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
9	228.60	231.14	233.68	236.22	238.76	241.30	243.84	246.38	248.92	251.46
10	254.00	256.54	259.08	261.62	264.16	266.70	269.24	271.78	274.32	276.85
11	279.39	281.93	284.47	287.01	289.55	292.09	294.63	297.17	299.71	302.25
12	304.79	307.33	309.87	312.41	314.95	317.49	320.03	322.57	325.11	327.65
13	330.19	332.73	335.27	337.81	340.35	342.89	345.43	347.97	350.51	353.03
14	355.59	358.13	360.67	363.21	365.75	368.29	370.83	373.37	375.91	378.43
15	380.99	383.53	386.07	388.61	391.15	393.69	396.23	398.77	401.31	403.85
16	406.39	408.93	411.47	414.01	416.55	419.09	421.63	424.17	426.71	429.25
17	431.79	434.33	436.87	439.41	441.95	444.49	447.03	449.57	452.11	454.65
18	457.19	459.73	462.27	464.81	467.35	469.89	472.43	474.97	477.51	480.03
English				I	Hundredths	of an Inc	ch.		Calabara J	
Inches and tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	3.5.111	Dation	Millim.	70/7:121	Brilli	DECIN	TATUM.	0.000	251111	7.5000
19.0	Millim. 482.59	Millim. 482.85	Millim. 483.10	Millim. 483.35	Millim. 483.61	Millim. 483.86	Millim. 484.12	Millim 484.37	Millim.	Millim
1	485.13	485.39	485.64	100000000000000000000000000000000000000		100000000000000000000000000000000000000		MOROLE !	484.62	484.88
2		C 100 (00)	488.18	485.89	486.15	486.40	486.66	486.91	487.16	487.42
3	487.67	487.93	490.72	488.43	488.69	488.94	489.20	489.45	489.70	489.90
		490.47	the second second	490.97	491.23	491.48	491.74	491.99	492.24	492.50
4	492.75	493.01	493.26	493.51	493.77	494.02	494.28	494.53	494.78	495.04
5	495.29	495.55	495.80	496.05	496.31	496.56	496.81	497.07	497.32	497.58
6	497.83	498.08	498.34	498.59	498.85	499.10	499.35	499.61	499.86	500.12
7	500.37	500.62	500.88	501.13	501.39	501.64	501.89	502.15	502.40	502.66
8	502.91	503.16	503.42	503.67	503.93	504.18	504.43	504.69	504.94	505.20
9	505.45	505.70	505.96	506.21	506.47	506.72	506.97	507.23	507.48	507.74
20.0	507.99	508.24	508.50	508.75	509.01	509.26	509.51	509.77	510.02	510.28
1	510.53	510.78	511.04	511.29	511.55	511.80	512.05	512.31	512.56	512.82
2	513.07	513.32	513.58	513.83	514.09	514.34	514.59	514.85	515.10	515.36
3	515.61	515.86	516.12	516.37	516.63	516.88	517.13	517.39	517.64	517.90
4	518.15	518.40	518.66	518.91	519.17	519.42	519.67	519.93	520.18	520.44
		020120	020.00				020101	0 20 10 0	020.10	020111
5	520.69	520.94	521.20	521.45	521.71	521.96	522.21	522.47	522.72	522.98
6	523.23	523.48	523.74	523.99	524.25	524.50	524.75	525.01	525.26	525.52
7	525.77	526.02	526.28	526.53	526.79	527.04	527.29	527.55	527.80	528.06
8	528.31	528.56	528.82	529.07	529.33	529.58	529.83	530.09	530.34	530.60
9	530.85	531.10	531.36	531.61	531.87	532.12	532.37	532.63	532.88	533.14
				Thousan	dths of an	Inch.				
0.	1.	2.	3.	4		5.	6.	7.	8.	9.
0.0	0.03	0.05	0.08	3 0.	10 0	.13	0.15	0.18	0.20	0.23

English				en Hali V	Hundredth	s of an Inc	h.			
Inches and tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
21.0	533.39	533.64	533.90	534.15	534.41	534.66	534.91	535.17	535.42	535.68
1	535.93	536.18	536.44	536.69	536.95	537.20	537.45	537.71	537.96	538.22
2	538.47	538.72	538.98	539.23	539.49	539.74	539.99	540.25	540.50	540.76
3	541.01	541.26	541.52	541.77	542.03	542.28	542.53	542.79	543.04	543.30
4	543.55	543.80	544.06	544.31	544.57	544.82	545.07	545.33	545.58	545.84
5	546.09	546.34	546.60	546.85	547.11	547.36	547.61	547.87	548.12	548.38
6	548.63	548.88	549.14	549.39	549.65	549.90	550.15	550.41	550.66	550.92
7	551.17	551.42	551.68	551.93	552.19	552.44	552.69	552.95	553.20	553.46
8	553.71	553.96	554.22	554.47	554.73	554.98	555.23	555.49	555.74	556.00
9	556.25	556.50	556.76	557.01	557.27	557.52	557.77	558.03	558.28	558.54
22.0	558.79	559.04	559.30	559.55	559.81	560.06	560.31	560.57	560.82	561.08
1	561.33	561.58	561.84	562.09	562.35	562.60	562.85	563.11	563.36	563.62
2	563.87	564.12	564.38	564.63	564.89	565.14	565.39	565.65	565.90	566.16
3	566.41	566.66	566.92	567.17	567.43	567.68	567.93	568.19	568.44	568.70
4	568.95	569.20	569.46	569.71	569.97	570.22	570.47	570.73	570.98	571.24
5	571.49	571.74	572.00	572.25	572.51	572.76	573.01	573.27	573.52	573.78
6	574.03	574.28	574.54	574.79	575.05	575.30	575.55	575.81	576.06	576.32
7	576.57	576.82	577.08	577.33	577.59	577.84	578.09	578.35	578.60	578.86
8	579.11	579.36	579.62	579.87	580.13	580.38	580.63	580.89	581.14	581.40
9	581.65	581.90	582.16	582.41	582.67	582.92	583.17	583.43	583.68	583.94
23.0	584.19	584.44	584.70	584.95	585.21	585.46	585.71	585.97	586.22	586.48
1	586.73	586.98	587.24	587.49	587.75	588.00	588.25	588.51	588.76	589.02
2	589.27	589.52	589.78	590.03	590.29	590.54	590.79	591.05	591.30	591.56
3	591.81	592.06	592.32	592.57	592.83	593.08	593.33	593.59	593.84	594.10
4	594.35	594.60	594.86	595.11	595.37	595.62	595.87	596.13	596.38	596.64
5	596.89	597.14	597.40	597.65	597.91	598.16	598.41	598.67	598.92	599.18
6	599.43	599.68	599.94	600.19	600.45	600.70	600.95	601.21	601.46	601.72
7	601.97	602.22	602.48	602.73	602.99	603.24	603.49	603.75	604.00	604.26
8	604.51	604.76	605.02	605.27	605.53	605.78	606.03	606.29	606.54	606.79
9	607.05	607.30	607.56	607.81	608.06	608.32	608.57	608.83	609.08	609.33
24.0	609.59	609.84	610.10	610.35	610.60	610.86	611.11	611.37	611.62	611.87
1	612.13	612.38	612.64	612.89	613.14	613.40	613.65	613.91	614.16	614.41
2	614.67	614.92	615.18	615.43	615.68	615.94	616.19	616.45	616.70	616.95
3	617.21	617.46	617.72	617.97	618.22	618.48	618.73	618.99	619.24	619.49
4	619.75	620.00	620.26	620.51	620.76	621.02	621.27	621.53	621.78	622.03
				Thous	andths of	an Inch.				
0.	1.	2.	3.	4.	5		6.	7.	8.	9.
0.0	0.03	0.05	0.08	0.1	0 0.	13 (	0.15	0.18	0.20	0.23

English				I	Iundredths	of an Inc	h.			Ayraw.
Inches and tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
nearly C	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
24.5	622.29	622.54	622.80	623.05	623.30	623.56	623.81	624.07	624.32	624.57
6	624.83	625.08	625.34	625.59	625.84	626.10	626.35	626.61	626.86	627.11
7	627.37	627.62	627.88	628.13	628.38	628.64	628.89	629.15	629.40	629.65
8	629.91	630.16	630.42	630.67 633.21	630.92 633.46	631.18 633.72	631.43	631.69	631.94	632.19 634.73
25.0	634.99	635.24	635.50	637.75	636.00	636.26	636.51	636.77	637.02	637.27
1	637.53	637.78	638.04	638.29	638.54	638.80	639.05	639.31	639.56	639.81
2	640.07	640.32	640.58	640.83	641.08	641.34	641.59	641.85	642.10	642.35
3	642.61	642.86	643.12	643.37	643.62 646.16	643.88 646.42	644.13	644.39	644.64	644.89
			0 20100							
5	647.69	647.94	648.20	648.45	648.70	648.96	649.21	649.47	649.72	649.97
6	650.23	650.48	650.74	650.99	651.24	651.50	651.75	652.01	652.26	652.5
7	652.77	653.02	653.28	653.53	653.78	654.04	654.29	654.55	654.80	655.05
8	655.31	655.56	655.82	656.07	656.32	656.58	656.83	657.09	657.34	657.59
9	657.85	658.10	658.36	658.61	658.86	659.12	659.37	659.63	659.88	660.13
<b>26</b> .0	660.39	660.64	660.90	661.15	661.40	661.66	661.91	662.17	662.42	662.67
1	662.93	663.18	663.44	663.69	663.94	664.20	664.45	664.71	664.96	665.21
2	665.47	665.72	665.98	666.23	666.48	666.74	666.99	667.25	667.50	667.73
3	668.01	668.26	668.52	668.77	669.02	669.28	669.53	669.79	670.04	670.29
4	670.55	670.80	671.06	671.31	671.56	671.82	672.07	672.33	672.58	672.88
5	673.09	673.34	673.60	673.85	674.10	674.36	674.61	674.87	675-12	675.37
6	675.63	675.88	676.14	676.39	676.64	676.90	677.15	677.41	677.66	677.91
7	678.17	678.42	678.68	678.93	679.18	679.44	679.69	679.95	680.20	680.45
8	680.71	680.96	681.22	681.47	681.72	681.98	682.23	682.49	682.74	682.99
9	683.25	683.50	683.76	684.01	684.26	684.52	684.77	685.03	685.28	685.58
27.0	685.79	686.04	686.30	686.55	686.80	687.06	687.31	687.57	687.82	688.07
1	688.33	688.58	688.84	689.09	689.34	689.60	689.85	690.11	690.36	690.6
2	690.87	691.12	691.38	691.63	691.88	692.14	692.39	692.65	692.90	693.15
3	693.41	693.66	693.92	694.17	694.42	694.68	694.93	695.19	695.44	695.69
4	695.95	696.20	696.46	696.71	696.96	697.22	697.47	697.73	697.98	698.23
5	698.49	698.74	699.00	699.25	699.50	699.76	700.01	700.27	700.52	700.7
6	701.03	701.28	701.54	701.79	702.04	702.30	702.55	702.81	703.06	703.3
7	703.57	703.82	704.08	704.33	704.58	704.84	705.09	705.35	705.60	705.8
8	706.11	706.36	706.62	706.87	707.12	707.38	707.63	707.89	708.14	708.39
9	708.65	708.90	709.16	709.41	709.66	709.92	710.17	710.43	710.68	710.9
				Thou	sandths of	an Inch.				
0.	1.	2.	3.	4		5.	6.	7.	8.	9.
0.0	0.03	0.05	0.08	0.1	0 0	.13	0.15	0.18	0.20	0.23

Hundredths of an Inch.

English	Hundredths of an Inch.												
Inches and tenths.	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.			
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim			
28.0	711.19	711.44	711.70	711.95	712.20	712.46	712.71	712.97	713.22	713.4			
1	713.73	713.98	714.24	714.49	714.74	715.00	715.25	715 51	715.76	716.0			
2	716.27	716.52	716.78	717.03	717.28	717.54	717.79	718.04	718.30	718.5			
3	718.81	719.06	719.31	719.57	719.82	720.08	720.33	720.58	720.84	721.0			
4	721.35	721.60	721.85	722-11	722.36	722.62	722.87	723.12	723.38	723.6			
5	723.89	724.14	724.39	724.65	724.90	725.16	725.41	725.66	725.92	726.1			
6	726.43	726.68	726.93	727.19	727.44	727.70	727.95	728.20	728.46	728.7			
7	728.97	729.22	729.47	729.73	729.98	730.24	730.49	730.74	731.00	731.2			
8	731.51	731.76	732.01	732.27	732.52	732.78	733.03	733.28	733.54	732.7			
9	734.05	734.30	734.55	734.81	735.06	735.32	735.57	735.82	736.08	736.3			
29.0	736.59	736.84	737.09	737.35	737.60	737.86	738.11	738.36	738.62	738.8			
1	739.13	739.38	739.63	739.89	740.14	740.40	740.65	740.90	741.16	741.4			
2	741.67	741.92	742.17	742.43	742.68	742.94	743.19	743.44	743.70	743.9			
3	744.21	744.46	744.71	744.97	745.22	745.48	745.73	745.98	746.24	746.4			
4	746.75	747.00	747.25	747.51	747.76	748.02	748.27	748.52	748.78	749.0			
5	749.29	749.54	749 79	750.05	750.30	750.56	750.81	751.06	751.32	751.5			
6	751.83	752.08	752.33	752.59	752.84	753.10	753.35	753.60	753.86	754.1			
7	754.37	754.62	754.87	755.13	755.38	755.64	755.89	756.14	756.40	756.6			
8	756.91	757.16	757.41	757.67	757.92	758.18	758.43	758.68	758.94	759.1			
9	759.45	759.70	759.95	760.21	760.46	760.72	760.97	761.22	761.48	761.7			
30.0	761.99	762.24	762.49	762.75	763.00	763.26	763.51	763.76	764.02	764.2			
1	764.53	764.78	765.03	765.29	765.54	765.80	766.05	766.30	766.56	766.8			
2	767.07	767.32	767.57	767.83	768.08	768.34	768.59	768.84	769.10	769.3			
3	769.61	769.86	770.11	770.37	770.62	770.88	771.13	771.38	771.64	771.8			
4	772.15	772.40	772.65	772.91	773.16	773.42	773.67	773.92	774.18	774.4			
5	774.69	774.94	775.19	775.45	775.70	775.96	776.21	776.46	776.72	776.9			
6	777.23	777.48	777.73	777.99	778.24	778.50	778.75	779.00	779.26	779.5			
7	779.77	780.02	780.27	780.53	780.78	781.04	781.29	781.54	781.80	782.0			
8	782.31	782.56	782.81	783.07	783.32	783.58	783.83	784.08	784.34	784.5			
9	784.85	785.10	785.35	785.61	785.86	786.12	786.37	786.62	786.88	787.1			
1.0	787.39	787.64	787.89	788.15	788.40	788.66	788.91	789.16	789.42	789.6			
1	789.93	790.18	790.43	790.69	790.94	791.20	791.45	791.70	791.96	792.2			
2	792.47	792.72	792.97	793.23	793.48	793.74	793.99	794.24	794.50	794.7			
3	795.01	795.26	795.51	795.77	796.02	796.28	796.53	796.78	797.04	797.2			
4	797.55	797.80	798.05	798.31	798.56	798.82	799.07	799.32	799.58	799.8			
				Thous	sandths of	an Inch.		1					
0.	1.	2.	3.	4.		5.	6.	7.	8.	9.			
0.0	0.03	0.05	0.08	0.1	0 0.	13	0.15	0.18	0.20	0.23			

1 English Inch = 11.2595 French or Paris Lines.

			1 English	l lnch = 1	1.2595 Fre	nch or Par	is Lines.	A PORT		
English				Sec.	Tenths o	f an Inch.				7 7 31
Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	1000	1		Par lines	Par.lines.	Par.lines	Par.lines	. Par.lines
11	123.85	124.93	126.11	127.23	128.36	129.48	130.61	131.74	132.86	133.99
12	135.11	136.24	137.37	138.49	139.62	140.74	141.87	143.00	144.12	145.25
13	146.37	147.50	148.63	149.75	150.88	152.00	153.13	154.26	155.38	156.51
14	157.63	158.76	159.88	161.01	162.14	163.26	164.39	165.51	166.64	
15	168.89	170.02	171.14	172.27	173.40	174.52	175.65	176.77	177.90	0.00
16	180.15	181.28	182.40	183.53	184.66	185.78	186.91	188.03	189.16	190.29
				Hundre	edths of an	Inch.	Middle 1		LINE A	157
0.	1.	2.	3.	4.		5.	6.	7.	8.	9.
0.000	0.113	0.225	0.338	0.45	0 0.	563 0	.676	0.788	0.901	1.013
English				I	Hundredth	s of an Inc	h.			
Inches and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines	Par lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines
17.0	191.41	191.52	191.64	191.75	191.86	191.97	192.09	192.20	192.31	192.42
1	192.54	192.65	192.76	192.88	192.99	193.10	193.21	193.33	193.44	193.55
2	193.66	193.78	193.89	194.00	194.11	194.23	194.34	194.45	194.56	194.68
3	194.79	194.90	195.01	195.13	195.24	195.35	195.46	195.58	195.69	195.80
4	195.92	196.03	196.14	196.25	196.37	196.48	196.59	196.70	196.82	196.93
5	197.04	197.15	197.27	197.38	197.49	197.60	197.72	197.83	197.94	198.05
6	198.17	198.28	198.39	198.50	198.62	198.73	198.84	198.96	199.07	199.18
7	199.29	199.41	199.52	199.63	199.74	199.86	199.97	200.08	200.19	200.31
8	200.42	200.53	200.64	200.76	200.87	200.98	201.09	201.21	201.32	201.43
9	201.55	201.66	201.77	201.88	202.00	202.11	202.22	202.33	202.45	202.56
18.0	202.67	202.78	202.90	203.01	203.12	203.23	203.35	203.46	203.57	203.68
1	203.80	203.91	204.02	204.13	204.25	204.36	204.47	204.59	204.70	204.81
2	204.92	205.04	205.15	205.26	205.37	205.49	205.60	205.71	205.82	205.94
3	206.05	206.16	206.27	206.39	206.50	206.61	206.72	206.84	206.95	207.06
4	207.17	207.29	207.40	207.51	207.63	207.74	207.85	207.96	208.08	208.19
5	208.30	208.41	208.53	208.64	208.75	208.86	208.98	209.09	209.20	209.31
6	209.43	209.54	209.65	209.76	209.88	209.99	210.10	210.21	210.33	210.44
7	210.55	210.67	210.78	210.89	211.00	211.12	211.23	211.34	211.45	211.57
8	211.68	211.79	211.90	212.02	212.13	212.24	212.35	212.47	212.58	212.69
9	212.80	212.92	213.03	213.14	213.25	213.37	213.48	213.59	213.71	213.82
19.0	213.93	214.04	214.16	214.27	214.38	214.49	214.61	214.72	214.83	214.94
1	215.06	215.17	215.28	215.39	215.51	215.62	215.73	215.84	215.96	216.07
2	216.18	216.29	216.41	216.52	216.63	216.75	216.86	216.97	217.08	217.20
3	217.31		217.53	217.65	217.76	217.87	217.98	218.10	218.21	218.32
4	218.43	218.55	218.66	218.77	218.88	219.00	219.11	219.22	219.34	219.45
5	219.56	219.67	219.79	219.90	220.01	220.12	220.24	220.35	220.46	220.57
6	220.69		220.91	221.02	221.14	221.25	221.36	221.47	221.59	221.70
7	221.81	221.92	222.04	222.15	222.26	222.38	222.49	222.60	222.71	222.83
8	222.94		223.16	223.28	223.39	223.50	223.61	223.73	223.84	223.95
9	224.06	224.18	224.29	22112	224.51	- C C	100	221.85	224.96	225.08

1 English Inch = 11.2595 French or Paris Lines.

English Inches and				i en la	Iundredth	s of an Incl	h.			
Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
00	Par.lines.	Par.lines.	Par.lines.	Par.lines.		Par.lines.	Par.lines.		Par.lines.	Par.lines
20.0	225.19	225.30	225.42	225.53	225.64	225.75	225.87	225.98	226.09	226.20
1	226.32	226.43	226.54	226.65	226.77	226.88	226.99	227.10	227.22	227.33
2	227.44	227.55	227.67	227.78	227.89	228.00	228.12	228.23	228.34	228.46
3	228.57	228.68	228.79	228.91	229.02	229.13	229.24	229.36	229.47	229.58
4	229.69	229.81	229.92	230.03	230.14	230.26	230.37	230.48	230.59	230.71
5	230.82	230.93	231.04	231.16	231.27	231.38	231.50	231.61	231.72	231.83
6	231.95	232.06	232.17	232.28	232.40	232.51	232.62	232.73	232.85	232.96
7	233.07	233.18	233.30	233.41	233.52	233.63	233.75	233.86	233.97	234.09
8	234.20	234.31	234.42	234.54	234.65	234.76	234.87	234.99	235.10	235.21
9	235.32	235.44	235.55	235.66	235.77	235.89	236.00	236.11	236.22	236.3
21.0	236.45	236.56	236.67	236.79	236.90	237.01	237.13	237.24	237.35	237.46
1	237.58	237.69	237.80	237.91	238.03	238.14	238.25	238.36	238.48	238.59
2	238.70	238.81	238.93	239.04	239.15	239.26	239.38	239.49	239.60	239.7
3	239.83	239.94	240.05	240.17	240.28	240.39	240.50	240.62	240.73	240.8
4	240.95	241.07	241.18	241.29	241.40	241.52	241.63	241.74	241.85	241.9
5	242.08	242.19	242.30	242.42	242.53	242.64	242.75	242.87	242.98	243.0
6	243.21	243.32	243.43	243.54	243.66	243.77	243.88	243.99	244.11	244.2
7	244.33	244.44	244.56	244.67	244.78	244.89	245.01	245.12	245.23	245.3
8	245.46	245.57	245.68	245.79	245.91	246.02	246.13	246.25	246.36	246.4
9	246.58	246.70	246.81	246.92	247.03	247.15	247.26	247.37	247.48	247.6
22.0	247.71	247.82	247.93	248.05	248.16	248.27	248.38	248.50	248.61	248.75
1	248.83	248.95	249.06	249.17	249.29	249.40	249.51	249.62	249.74	249.8
2	249.96	250.07	250.19	250.30	250.41	250.52	250.64	250.75	250.86	250.9
3	251.09	251.20	251.31	251.42	251.54	251.65	251.76	251.88	251.99	252.1
4	252.21	252.33	252.44	252.55	252.66	252.78	252.89	253.00	253.11	253.2
5	253.34	253.45	253.56	253.68	253.79	253.90	254.01	254.13	254.24	254.3
6	254.46	254.58	254.69	254.80	254.92	255.03	255.14	255.25	255.37	255.48
7	255.59	255.70	255.82	255.93	256.04	256.15	256.27	256.38	256.49	256.60
8 9	256.72 257.84	256.83 257.96	256.94 258.07	257.05 258.18	257.17 258.29	257.28 258.41	257.39 258.52	257.50 258.63	257.62 258.74	257.73 258.80
23.0	258.97	259.08	259.19	259.31	259.42	259.53	259.64	259.76	259.87	259.98
1	260.09	260.21	260.32	260.43	260.54	260.66	260.77	260.88	261.00	261.11
2	261.22	261.33	261.45	261.56	261.67	261.78	261.90	262.01	262.12	262.23
3	262.35	262.46	262.57	262.68	262.80	262.91	263.02	263.13	263.25	263.36
4	263.47	263.58	263.70	263.81	263.92	264.04	264.15	264.26	264.37	264.49
5	264.60	264.71	264.82	264.94	265.05	265.16	265.27	265.39	265.50	265.61
6	265.72	265.84	265.95	266.06	266.17	266.29	266.40	266.51	266.62	266.74
7	266.85	266.96	267.08	267.19	267.30	267.41	267.53	267.64	267.75	267.86
8	267.98	268.09	268.20	268.31	268.43	268.54	268.65	268.76	268.88	268.99
9	269.10	269.21	269.33	269.44	269.55	269.67	269.78	269.89	270.00	270.12
Water 1	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 English Inch = 11.2595 French or Paris Lines.

English nches and					lunareaths	of an Inc	u.			PARSAS.
Tenths.	0.	1.	2.	3.	4.	. 5.	6.	7.	8.	9.
•	Par.lines.	Par.lines.		Par.lines.	Par.lines.	Par.lines.	Par.lines.		Par.lines.	Par.line
24.0	270.23	270.34	270.45	270.57	270.68	270.79	270.90	271.02	271.13	271.2
1	271.35	271.47	271.58	271.69	271.80	271.92	272.03	272.14	272.25	272.3
2	272.48	272.59	272.71	272.82	272.93	273.04	273.16	273.27	273.38	273.4
3	273.61	273.72	273.83	273.94	274.06	274.17	274.28	274.39	274.51	274.6
4	274.73	274.84	274.96	275.07	275.18	275.29	275.41	275.52	275.63	275.7
5	275.86	275.97	276.08	276.20	276.31	276.42	276.53	276.65	276.76	276.8
6	276.98	277.10	277.21	277.32	277.43	277.55	277.66	277.77	277.88	278.0
7	278.11	278.22	278.33	278.45	278.56	278.67	278.79	278.90	279.01	279.1
8	279.24	279.35	279.46	279.57	279.69	279.80	279.91	280.02	280.14	280.2
9	280.36	280.47	280.59	280.70	280.81	280.92	281.04	281.15	281.26	281.3
25.0	281.49	281.60	281.71	281.83	281.94	282.05	282.16	282.28	282.39	282.5
1	282.61	282.73	282.84	282.95	283.06	283.18	283.29	283.40	283.51	283.6
2	283.74	283.85	283.96	284.08	284.19	284.30	284.41	284.53	284.64	284.7
3	284.87	284.98	285.09	285.20	285.32	285.43	285.54	285.65	285.77	285.8
4	285.99	286.10	286.22	286.33	286.44	286.55	286.67	286.78	286.89	287.0
5	287.12	287.23	287.34	287.46	287.57	287.68	287.79	287.91	288.02	288.1
6	288.24	288.36	288.47	288.58	288.69	288.81	288.92	289.03	289.14	289.2
7	289.37	289.48	289.59	289.71	289.82	289.93	290.04	290.16	290.27	290.3
8	290.50-	290.61	290.72	290.83	290.95	291.06	291.17	291.28	291.40	291.5
9	291.62	291.73	291.85	291.96	292.07	292.18	292.30	292.41	292.52	292.6
26.0	292.75	292.86	292.97	293.08	293.20	293.31	293.42	293.54	293.65	293.7
1	293.87	293.99	294.10	294.21	294.32	294.44	294.55	294.66	294.77	294.8
2	295.00	295.11	295.22	295.34	295.45	295.56	295.67	295.79	295.90	296.0
3	296.12	296.24	296.35	296.46	296.58	296.69	296.80	296.91	297.03	297.1
4	297.25	297.36	297.48	297.59	297.70	297.81	297.93	298.04	298.15	298.2
5	298.38	298.49	298.60	298.71	298.83	298.94	299.05	299.17	299.28	299.3
6	299.50	299.62	299.73	299.84	299.95	300.07	300.18	300.29	300.40	300.5
7	300.63	300.74	300.85	300.97	301.08	301.19	301.30	301.42	301.53	301.6
8	301.75	301.87	301.98	302.09	302.20	302.32	302.43	302.54	302.66	302.7
9	302.88	302.99	303.11	303.22	303.33	303.44	303.56	303.67	303.78	303.8
27.0	304.01	304.12	304.23	304.34	304.46	304.57	304.68	304.79	304.91	305.0
1	305.13	305.25	305.36	305.47	305.58	305.70	305.81	305.92	306.03	306.1
2	306.26	306.37	306.48	306.60	306.71	306.82	306.93	307.05	307.16	307.27
3	307.38	307.50	307.61	307.72	307.83	307.95	308.06	308.17	308.29	308.40
4	308.51	308.62	308.74	308.85	308.96	309.07	309.19	309.30	309.41	309.5
5	309.64	309.75	309.86	309.97	310.09	310.20	310.31	310.42	310.54	310.68
6	310.76	310.87	310.99	311.10	311.21	311.33	311.44	311.55	311.66	311.78
7	311.89	312.00	312.11	312.23	312.34	312.45	312.56	312.68	312.79	312.90
8	313.01	313.13	313.24	313.35	313.46	313.58	313.69	313.80	313.91	314.03
9	314.14	314.25	314.37	314.48	314.59	314.70	314.82	314.93	315.04	315.15
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 English Inch = 11.2595 French or Paris Lines.

English nches and		1	1	1	1		1	1		
Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
Miles	Par.lines.	Par.lin								
28.0	315.27	315.38	315.49	315.60	315.72	315.83	315.94	316.05	316.17	316.2
1	316.39	316.50	316.62	316.73	316.84	316.95	317.07	317.18	317.29	317.4
2	317.52	317.63	317.74	317.86	317.97	318.08	318.19	318.31	318.42	318.5
3	318.64	318.76	318.87	318.98	319.09	319.21	319.32	319.43	319.54	319.6
4	319.77	319.88	319.99	320.11	320.22	320.33	320.45	320.56	320.67	320.7
5	320.90	321.01	321.12	321.23	321.35	321.46	321.57	321.68	321.80	321.9
6	322.02	322.13	322.25	322.36	322.47	322.58	322.70	322.81	322.92	323.0
7	323.15	323.26	323.37	323.49	323.60	323.71	323.82	323.94	324.05	324.
8	324.27	324.39	324.50	324.61	324.72	324.84	324.95	325.06	325.17	325.2
9	325.40	325.51	325.62	325.74	325.85	325.96	326.08	326.19	326.30	326.
29.0	326.53	326.64	326.75	326.86	326.98	327.09	327.20	327.31	327.43	327.
1	327.65	327.76	327.88	327.99	328.10	328.21	328.33	328.44	328.55	328.
2	328.78	328.89	329.00	329.12	329.23	329.34	329.45	329.57	329.68	329.
3	329.90	330.02	330.13	330.24	330.35	330.47	330.58	330.69	330.80	330.9
4	331.03	331.14	331.25	331.37	331.48	331.59	331.70	331.82	331.93	332.0
5	332.16	332.27	332.38	332.49	332.61	332.72	332.83	332.94	333.06	333.
6	333.28	333.39	333.51	333.62	333.73	333.84	333.96	334.07	334.18	334.5
7	334.41	334.52	334.63	334.74	334.86	334.97	335.08	335.20	335.31	335.4
8	335.53	335.65	335.76	335.87	335.98	336.10	336.21	336.32	336.43	336.3
9	336.66	336.77	336.88	337.00	337.11	337.22	337.33	337.45	337.56	337.6
30.0	337.78	337.90	338.01	338.12	338.24	338.35	338.46	338.57	338.69	338.8
1	338.91	339.02	339.14	339.25	339.36	339.47	339.59	339.70	339.81	339.9
2	340.04	340.15	340.26	340.37	340.49	340.60	340.71	340.83	340.94	341.0
3	341.16	341.28	341.39	341.50	341.61	341.73	341.84	341.95	342.06	342.
4	342.29	342.40	342.51	342.63	342.74	342.85	342.96	343.08	343.19	343.
5	343.41	343.53	343.64	343.75	343.87	343.98	344.09	344.20	344.32	344.4
6	344.54	344.65	344.77	341.88	344.99	345.10	345.22	345.33	345.44	345.
7	345.67	345.78	345.89	346.00	346.12	346.23	346.34	346.45	346.57	346.6
8	346.79	346.91	347.02	347.13	347.24	347.36	347.47	347.58	347.69	347.8
9	347.92	348.03	348.14	348.26	348.37	348.48	348.59	348.71	348.82	348.9
31.0	349.04	349.16	349.27	349.38	349.49	349.61	349.72	349.83	349.95	350.0
1	350.17	350.28	350.40	350.51	350.62	350.73	350.85	350.96	351.07	351.1
2	351.30	351.41	351.52	351.63	351.75	351.86	351.97	352.08	352.20	352.3
3	352.42	352.53	352.65	352.76	352.87	352.99	353.10	353.21	353.32	353.4
4	353.55	353.66	353.77	353.89	354.00	354.11	354.22	354.34	354.45	354.5
5	354.67	354.79	354.90	355.01	355.12	355.24	355.35	355.46	355.57	355.6
6	355.80	355.91	356.03	356.14	356.25	356.36	356.48	356.59	356.70	356.8
ALL SE				Thousan	dths of an	Inch.				
0.	1.	2.	3.	4.	1 8	.	6.	7.	8.	9.
0.000	0.011	0.023								

III. - IV.

### COMPARISON

OF

## THE METRICAL BAROMETER

WITH

THE ENGLISH AND THE OLD FRENCH BAROMETERS,

OR

## TABLES

FOR CONVERTING MILLIMETRES INTO ENGLISH INCHES AND DECIMALS,
AND INTO FRENCH OR PARIS LINES;

GIVING THE VALUES CORRESPONDING TO EVERY MILLIMETRE FROM 250 TO 600; AND TO EVERY TENTH OF A MILLIMETRE FROM 600 TO 800 MILLIMETRES.

the second section, as seems the second section of the second second 的现在分词,这个人也可以可以可以不是的。 第一章 The state of the s There is a second with home to be a true to be a facility or with the first of the state of the s paying the same of the same of the same of Berger (1964) and the state of the state of

1 Metre = 39.37079 English Inches.

Millime- tres.	Millimetres. Units.												
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In	Eng. In.	Eng. In.			
250	9.843	9.882	9.921	9.961	10.000	10.040	10.079	10.118	10.158	10.197			
260	10.236	10.276	10.315	10.355	10.394	10.433	10.473	10.512	10.551	10.591			
270	10.630	10.669	10.709	10.748	10.788	10.827	10.866	10.906	10.945	10.984			
280	11.024	11.063	11.103	11.142	11.181	11.221	11.260	11.299	11.339	11.378			
290	11.418	11.457	11.496	11.536	11.575	11.614	11.654	11.693	11.732	11.772			
300	11.811	11.851	11.890	11.929	11.969	12.008	12.047	12.087	12.126	12.166			
310	12.205	12.244	12.284	12.323	12.362	12.402	12.441	12.481	12.520	12.559			
320	12.599	12.638	12.677	12.717	12.756	12.795	12.835	12.874	12.914	12.953			
330	12.992	13.032	13.071	13.110	13.150	13.189	13.229	13.268	13.307	13.547			
340	13.386	13.425	13.465	13.504	13.544	13.583	13.622	13.662	13.701	13.740			
350	13.780	13.819	13.859	13.898	13.937	13.977	14.016	14.055	14.095	14.134			
360	14.173	14.213	14.252	14.292	14.331	14.370	14.410	14.449	14.488	14.528			
370	14.567	14.607	14.646	14.685	14.725	14.764	14.803	14.843	14.882	14.922			
380	14.961	15.000	15.040	15.079	15.118	15.158	15.197	15.236	15.276	15.315			
390	15.355	15.494	15.433	15.473	15.512	15.551	15.591	15.630	15.670	15.709			
400	15.748	15.788	15.827	15.866	15.906	15.945	15.985	16.024	16.063	16.103			
410	16.142	16.181	16.221	16.260	16.300	16.339	16.378	16.418	16.458	16.496			
420	16.536	16.575	16.614	16.654	16.693	16.733	16.772	16.811	16.851	16.890			
430	16.929	16.969	17.008	17.048	17.087	17.126	17.166	17.205	17.244	17.284			
440	17.323	17.362	17.402	17.441	17.481	17.520	17.559	17.599	17.638	17.677			
450	17.717	17.756	17.796	17.835	17.874	17.914	17.953	17.992	18.032	18.071			
460	18.111	18.150	18.189	18.229	18.268	18.307	18.347	18.386	18.426	18.465			
470	18.504	18.544	18.583	18.622	18.662	18.701	18.740	18.780	18.819	18.859			
480	18.898	18.937	18.977	19.016	19.055	19.095	19.134	19.174	19.213	19.252			
490	19.292	19.331	19.370	19.410	19.449	19.489	19.134	19.567	19.607	19.646			
500	19.685	19.725	19.764	19.804	19.843	19.882	19.922	19.961	20.000	20.040			
510	20.079	20.118	20.158	20.197	20.237	20.276	20.315	20.355	20.394	20.433			
520	20.079	20.118	20.158	20.197	20.237	20.276	20.709	20.333	20.394	20.433			
530	20.473	20.906	20.945	20.985	21.024	21.063	21.103	21.142	21.181	21.221			
540	21.260	21.300	21.339	21.378	21.418	21.457	21.496	21.536	21.575	21.615			
550	21.654	21.693	21.733	21.772	21.811	21.851	21.890	21.930	21.969	22.008			
560	22.048	22.087	22.126	22.166	22.205	22.244	22.284	22.323	22.363	22.402			
570	22.441	22.481	22.520	22.559	22.599	22.638	22.678	22.717	22.756	22.796			
580	22.835	22.874	22.914	22.953	22.993	23.032	23.071	23.111	23.150	23.189			
590	23.229	23.268	23.308	23.347	23.386	23.426	23.465	23.504	23.544	23.583			
				Tenths	of Millime	etres.							
0.	1.	2.	3.	4.	5	.	6.	7.	8.	9.			
0.000	0.004	0.008	0.012	0.010	6 0.0	20 0	024 0	.028	0.031	0.035			

1 Metre = 39.37079 English Inches.

tres.	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.			
13.4	Eng In.	Eng. I											
600	23.622	23.626	23.630	23.634	23.638	23.642	23.646	23.650	23.654	23.65			
601	23.662	23.666	23.670	23.674	23.678	23.682	23.685	23.689	23.693	23.69			
602	23.701	23.705	23.709	23.713	23.717	23.721	23.725	23.729	23.733	23.73			
603	23.741	23.745	23.748	23.752	23.756	23.760	23.764	23.768	23.772	23.77			
604.	23.780	23.784	23.788	23.792	23.796	23.800	23.804	23.808	23.811	23.81			
605	23.819	23.823	23.827	23.831	23.835	23.839	23.843	23.847	23.851	23.88			
606	23.859	23.863	23.867	23.871	23.874	23.878	23.882	23.886	23.890	23.89			
607	23.898	23,902	23.906	23.910	23.914	23.918	23.922	23.926	23.930	23.93			
608	23.937	23.941	23.945	23.949	23.953	23.957	23.961	23.965	23.969	23.97			
609	23.977	23.981	23.985	23.989	23.993	23.996	24.000	24.004	24.008	24.01			
610	24.016	24.020	24.024	24.028	24.032	24.036	24.040	24.044	24.048	24.05			
611	24.056	24.059	24.063	24.067	24.071	24.075	24.079	24.083	24.087	24.09			
612	24.095	24.099	24.103	24.107	24.111	24.115	24.119	24.122	24.126	24.18			
613	24.134	24.138	24.142	24.146	24.150	24.154	24.158	24.162	24.166	24.17			
614	24.174	24.178	24.182	24.185	24.189	24.193	24.197	24.201	24.205	24.20			
615	24.213	24.217	24.221	24.225	24.229	24.233	24.237	24.241	24.245	24.24			
616	24.252	24.256	24.260	24.264	24.268	24.272	24.276	24.280	24.284	24.28			
617	24.292	24.296	24,300	24.304	24.308	24.311	24.315	24.319	24.323	24.32			
618	24.331	24.335	24.339	24.343	24.347	24.351	24.355	24.359	24.363	24.36			
619	24.371	24.374	24.378	24.382	24.386	24.390	24.394	24.398	24.402	24.40			
620	24.410	24.414	24.418	24.422	24.426	24.430	24.434	24.437	24.441	24.44			
621	24.449	24.453	24.457	24.461	24.465	24.469	24.473	24.477	24.481	24.48			
622	24.489	24.493	24.497	24.500	24.504	24.508	24.512	24.516	24.520	24.52			
623	24.528	24.532	24.536	24.540	24.544	24.548	24.552	24.556	24.559	24.56			
624	24.567	24.571	24.575	24.579	24.583	24.587	24.591	24.595	24.599	24.60			
625	24.607	24.611	24.615	24.619	24.622	24.626	24.630	24.634	24.638	24.64			
626	24.646	24.650	24.654	24.658	24.662	24.666	24.670	24.674		24.68			
627	24.685	24.689	24.693	24.697	24.701	24.705	24.709	24.713	24.717	24.72			
628	24.725	24.729	24.733	24.737	24.741	24.745	24.748	24.752	24.756	24.76			
629	24.764	24.768	24.772	24.776	24.780	24.784	24.788	24.792	24.796	24.80			
630	24.804	24.808	24.811	24.815	24.819	24.823	24.827	24.831	24.835	24.83			
631	24.843	24.847	24.851	24.855	24.859	24.863	24.867	24.871	24.874	24.87			
632	24.882	24.886	24.890	24.894	24.898	24.902	24.906	24.910	24.914	24.91			
633	24.922	24.926	24.930	24.934	24.937	24.941	24.945	24.949	24.953	24.95			
634	24.961	24.965		24.973	24.977	24.981	24.985	24.989	24.993	24.99			
635	25.000	25.004	25.008	25.012	25.016	25.020	25.024	25.028	25.032	25.03			
636	25.040	25.044	25.048	25.052	25.056	25.060	25.063	25.067	25.071	25.07			
637	25.079	25.083	25.087	25.091	25.095	25.099	25.103	25.107	25.111	25.11			
638	25.119	25.123	25.126	25.130	25.134	25.138	25.142	25.146	25.150	25.15			
639	25.158	25.162	25.166	25.170	25.174	25.178	25.182	25.185	25.189	25.19			
	0.	1.	2.	3.			6.	7.	8.	9.			

1 Metre = 39.37079 English Inches.

Millime-					rentns or	Millimetres	•			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
640	Eng. ln. 25.197	Eng. In. 25.201	Eng. In. 25.205	Eng. In. 25.209	Eng. In. 25.213	Eng. In. 25.217	Eng. In. 25.221	Eng. In. 25.225	Eng. In. 25.229	Eng. Ir 25.23
641	25.197	25.241	25.245	25.248	25.252	25 256	25.260	25.264	25.268	25.27
642	25.276	25.280	25.284	25.288	25.292	25.296	25.300	25.304	25.308	25.31
643	25.315	25.319	25.323	25.327	25.331	25.335	25.339	25.343	25.347	25.35
644	25.355	25.359	25.363	25.367	25.371	25.374	25.378	25.382	25.386	25.39
645	25.394	25.398	25.402	25.406	25.410	25.414	25.418	25.422	25.426	25.43
646	25.434	25.437	25.441	25.445	25.449	25.453	25.457	25.461	25.465	25.46
647	25.473	25.477	25.481	25.485	25.489	25.493	25.497	25.500	25.504	25.50
648	25.512	25.516	25.520	25.524	25.528	25.532	25.536	25.540	25.544	25.54
649	25.552	25.556	25.560	25.563	25.567	25.571	25.575	25.579	25.583	25.58
650	25.591	25.595	25.599	25.603	25.607	25.611	25.615	25.619	25.623	25.62
651	25.630	25.634	25.638	25.642	25.646	25.650	25.654	25.658	25.662	25.66
652	25.670	25.674	25.678	25.682	25.686	25.689	25.693	25.697	25.701	25.70
653	25.709	25.713	25.717	25.721	25.725	25.729	25.733	25.737	25.741	25.74
654	25.748	25.752	25.756	25.760	25.764	25.768	25.772	25.776	25.780	25.78
655	25.788	25.792	25.796	25.800	25.804	25.808	25.811	25.815	25.819	25.82
656	25.827	25.831	25.835	25.839	25.843	25.847	25.851	25.855	25.859	25.86
657	25.867	25.871	25.874	25.878	25.882	25.886	25.890	25.894	25.898	25.90
658	25.906	25.910	25.914	25.918	25.922	25.926	25.930	25.934	25.937	25.94
659	25.945	25.949	25.953	25.957	25.961	25.965	25.969	25.973	25.977	25.98
660	25.985	25.989	25.993	25.997	26.000	26.004	26.008	26.012	26.016	26.02
661	26.024	26.028	26.032	26.036	26.040	26.044	26.048	26.052	26.056	26.06
662	26.063	26.067	26.071	26.075	26.079	26.083	26.087	26.091	26.095	26.09
663	26.103	26.107	26.111	26.115	26.119	26.123	26.126	26.130	26.134	26.13
664	26.142	26.146	26.150	26.154	26.158	26.162	26.166	26.170	26.174	26.17
665	26.182	26.186	26.189	26.193	26.197	26.201	26.205	26.209	26.213	26.21
666	26 221	26.225	26.229	26.233	26.237	26.241	26.245	26.249	26.252	26.25
667 668	26.260 26.300	26.264	26.268	26.272 26.311	26.276 26.315	26.280 26.319	26.284	26.288	26.292 26.331	26.29 26.33
669	26.339	26.343	26.347	26.351	26.355	26.359	26.363	26.367	26.371	26.37
670	26.378	26.382	26.386	26.390	26.394	26.398	26.402	26.406	26.410	26.41
671	26.418	26.422	26.426	26.430	26.434	26.437	26.441	26.445	26.449	26.45
672	26.457	26.461	26.465	26.469	26.473	26.477	26.481	26.485	26.489	26.49
673	26.497	26.500	26.504	26.508	26.512	26.516	26.520	26.524	26.528	26.53
674	26.536		26.544	26.548	26.552	26.556	26.560	26.563	26.567	26.57
675	26.575	26.579	26.583	26.587	26.591	26.595	26.599	26.603	26.607	26.61
676	26.615	26.619	26.623	26.626	26.630	26.634	26.638	26.642	26.646	26.65
677	26.654	26.658	26.662	26.666	26.670	26.674	26.678	26.682	26.686	26.68
678	26.693	26.697	26.701	26.705	26.709	26.713	26.717	26.721	26.725	26.72
679	26.733	26.737	26.741	26.745	26.749	26.752	26.756	26.760	26.764	26.76
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 39.37079 English Inches.

Millime-					Fenths of M	Illimetres.				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. Ir				
680	26.772	26.776	26.780	26.784	26.788	26.792	26.796	26.800	26.804	26.808
681	26.812	26.815	26.819	26.823	26.827	26.831	26.835	26.839	26.843	26.84
682	26.851	26.855	26.859	26.863	26.867	26.871	26.875	26.878	26.882	26.88
683	26.890	26.894	26.898	26.902	26.906	26.910	26.914	26.918	26.922	26.92
684	26.930	26.934	26.937	26.941	26.945	26.949	26.953	26.957	26.961	26.96
685	26.969	26.973	26.977	26.981	26.985	26.989	26.993	26.997	27.000	27.00
686	27.008	27.012	27.016	27.020	27.024	27.028	27.032	27.036	27.040	27.04
687	27.048	27.052	27.056	27.060	27.063	27.067	27.071	27.075	27.079	27.08
688	27.087	27.091	27.095	27.099	27.103	27.107	27.111	27.115	27.119	27.12
689	27.126	27.130	27.134	27.138	27.142	27.146	27.150	27.154	27.158	27.16
690	27.166	27.170	27.174	27.178	27.182	27.186	27.189	27.193	27.197	27.20
691	27.205	27.209	27.213	27.217	27.221	27.225	27.229	27.233	27.237	27.24
692	27.245	27.249	27.252	27.256	27.260	27.264	27.268	27.272	27.276	27.28
693	27.284	27.288	27.292	27.296	27.300	27.304	27.308	27.312	27.315	27.31
694	27.323	27.327	27.331	27.335	27.339	27.343	27.347	27.351	27.355	27.35
695	27.363	27.367	27.371	27.375	27.378	27.382	27.386	27.390	27.394	27.39
696	27.402	27.406	27.410	27.414	27.418	27.422	27.426	27.430	27.434	27.43
697	27.441	27.445	27.449	27.453	27.457	27.461	27.465	27.469	27.473	27.47
698	27.481	27.485	27.489	27.493	27.497	27.500	27.504	27.508	27.512	27.51
699	27.520	27.524	27.528	27.532	27.536	27.540	27.544	27.548	27.552	27.55
700	27.560	27.563	27.567	27.571	27.575	27.579	27.583	27.587	27.591	27.59
701	27.599	27.603	27.607	27.611	27.615	27.619	27.623	27.626	27.630	27.63
702	27.638	27.642	27.646	27.650	27.654	27.658	27.662	27.666	27.670	27.67
703	27.678	27.682	27.686	27.689	27.693	27.697	27.701	27.705	27.709	27.71
704	27.717	27.721	27.725	27.729	27.733	27.737	27.741	27.745	27.749	27.78
705	27.756	27.760	27.764	27.768	27.772	27.776	27.780	27.784	27.788	27.79
706	27.796	27.800	27.804	27.808	27.812	27.815	27.819	27.823	27.827	27.8
707	27.835	27.839	27.843	27.847	27.851	27.855	27.859	27.863	27.867	27.8
708	27.875	27.878	27.882	27.886	27.890	27.894	27.898	27.902	27.906	27.9
709	27.914	27.918	27.922	27.926	27.930	27.934	27.938	27.941	27.945	27.9
710	27.953	27.957	27.961	27.965	27.969	27.973	27.977	27.981	27.985	27.98
711	27.993	27.997	28.001	28.004	28.008	28.012	28.016	28.020	28.024	28.02
712	28.032	28.036	28.040	28.044	28.048	28.052	28.056	28.060	28.063	28.0
713	28.071	28.075	28.079	28.083	28.087	28.091	28.095	28.099	28.103	28.10
714	28.111	28.115	28.119	28.123	28.126	28.130	28.134	28.138	28.142	28.1
715	28.150	28.154	28.158	28.162	28.166	28.170	28.174	28.178	28.182	28.18
716	28.189	28.193	28.197	28.201	28.205	28.209	28.213	28.217	28.221	28.2
717	28.229	28.233	28.237	28.241	28.245	28.249	28.252	28.256	28.260	28.2
718	28.268	28.272	28.276	28.280	28.284	28.288	28.292	28.296	28.300	28.30
719	28.308	28.312	28.315	28.319	28.323	28.327	28.331	28.335	28.339	28.3
Libraria	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 39.37079 English Inches.

Millime-				augaj liita	Tenths of	Millimetres	3.			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
720	Eng. In. 28.347	Eng. In. 28.351	Eng. In. 28.355	Eng. In. 28.359	Eng. In. 28.363	Eng. In. 28.367	Eng. In. 28.371	Eng. In. 28.375	Eng. In. 28.378	Eng. In. 28.382
721	28.386	28.390	28.394	28.398	28.402	28.406	28.410	28.414	28.418	28.422
722	28.426	28.430	28.434	28.438	28.441	28.445	28.449	28.453	28.457	28.461
723	28.465	28.469	28.473	28.477	28.481	28.485	28.489	28.493	28.497	28.501
724	28.504	28.508	28.512	28.516	28.520	28.524	28.528	28.532	28.536	28.540
725	28.544	28.548	28.552	28.556	28.560	28.564	28.567	28.571	28.575	28.579
726	28.583	28.587	28.591	28.595	28.599	28.603	28.607	28.611	28.615	28.619
727	28.623	28.627	28.630	28.634	28.638	28.642	28.646	28.650	28.654	28.658
728	28.662	28.666	28.670	28.674	28.678	28.682	28.686	28.689	28.693	28.697
729	28.701	28.705	28.709	28.713	28.717	28.721	28.725	28.729	28.733	28.737
730	28.741	28.745	28.749	28.752	28.756	28.760	28.764	28.768	28.772	28.776
731	28.780	28.784	28.788	28.792	28.796	28.800	28.804	28.808	28.812	28.815
732	28.819	28.823	28.827	28.831	28.835	28.839	28.843	28.847	28.851	28.855
733	28.859	28.863	28.867	28.871	28.875	28.878	28.882	28.886	28.890	28.894
734	28.898	28.902	28.906	28.910	28.914	28.918	28.922	28.926	28.930	28.934
735	28.938	28.941	28.945	28.949	28.953	28.957	28.961	28.965	28.969	28.973
736	28.977	28.981	28.985	28.989	28.993	28.997	29.001	29.004	29.008	29.012
737	29.016	29.020	29.024	29.028	29.032	29.036	29.040	29.044	29.048	29.052
738	29.056	29.060	29.064	29.067	29.071	29.075	29.079	29.083	29.087	29.091
739	29.095	29.099	29.103	29.107	29.111	29.115	29.119	29.123	29.127	29.130
740	29.134	29.138	29.142	29.146	29.150	29.154	29.158	29.162	29.166	29.170
741	29.174	29.178	29.182	29.186	29.190	29.193	29.197	29.201	29.205	29.209
742	29.213	29.217	29.221	29.225	29.229	29.233	29.237	29.241	29.245	29.249
743	29.252	29.256	29.260	29.264	29.268	29.272	29.276	29.280	29.284	29.288
744	29.292	29.296	29.300	29.304	29.308	29.312	29.315	29.319	29.323	29.327
745	29.331	29.335	29.339	29.343	29.347	29.351	29.355	29.359	29.363	29.367
746	29.371	29.375	29.378	29.382	29.386	29.390	29.394	29.398	29.402	29.406
747	29.410	29.414	29.418	29.422	29.426	29.430	29.434	29.438	29.441	29.445
748	29.449	29.453	29.457	29.461	29.465	29.469	29.473	29.477	29.481	29.485
749	29.489	29.493	29.497	29.501	29.504	29.508	29.512	29.516	29.520	29.524
750	29.528	29.532	29.536	29.540	29.544	29.548	29.552	29.556	29.560	29.564
751	29.567	29.571	29.575	29.579	29.583	29.587	29.591	29.595	29.599	29.603
752	29.607	29.611	29.615	29.619	29.623	29.627	29.630	29.634	29.638	29.642
753	29.646	29.650	29.654	29.658	29.662	29.666	29.670	29.674	29.678	29.682
754	29.686	29.690	29.693	29.697	29.701	29.705	29.709	29.713	29.717	29.721
755	29.725	29.729	29.733	29.737	29.741	29.745	29.749	29.753	29.756	29.760
756	29.764	29.768	29.772	29.776	29.780	29.784	29.788	29.792	29.796	29.800
757	29.804	29.808	29.812	29.815	29.819	29.823	29.827	29.831	29.835	29.839
758	29.843	29.847	29.851	29.855	29.859	29.863	29.867	29.871	29.875	29.878
759	29.882	29.886	29.890	29.894	29.898	29.902	29.906	29.910	29.914	29.918
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 39.37079 English Inches.

Millime-					Tenths of	Millimetre	3.			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In	Eng. In.	Eng. I
760	29.922	29.926	29.930	29.934	29.938	29.941	29.945	29.949	29.953	29.95
761	29.961	29.965	29.969	29.973	29.977	29.981	29.985	29.989	29.993	29.99
762	30.001	30.004	30.008	30.012	30.016	30.020	30.024	30.028	30.032	30.03
763	30.040	30.044	30.048	30.052	30.056	30.060	30.064	30.067	30.071	30 07
764	30.079	30.083	30.087	30.091	30.095	30.099	30.103	30.107	30.111	30.11
765	30.119	30.123	30.127	30.130	30.134	30.138	30.142	30.146	30.150	30.15
766	30.158	30.162	30.166	30.170	30.174	30.178	30.182	30.186	30.190	30.19
767	30.197	30.201	30.205	30.209	30.213	30.217	30.221	30.225	30.229	30.23
768	30.237	30.241	30.245	30.249	30.253	30.256	30.260	30.264	30.268	30.27
769	30.276	30.280	30.284	30.288	30.292	30.296	30.300	30.304	30.308	30.3
770	30.316	30.319	30.323	30.327	30.331	30.335	30.339	30.343	30.347	30.3
771	30.355	30.359	30.363	30.367	30.371	30.375	30.379	30.382	30.386	30.3
772	30.394	30.398	30.402	30.406	30.410	30.414	30.418	30.422	30.426	30.4
773	30.434	30.438	30.441	30.445	30.449	30.453	30.457	30.461	30.465	20.46
774	30.473	30.477	30.481	30.485	30.489	30.493	30.497	30.501	30.504	30.50
775	30.512	30.516	30.520	30.524	30.528	30.532	30.536	30.540	30.544	30.5
776	30.552	30.556	30.560	30.564	30.567	30.571	30.575	30.579	30.583	30.58
777	30.591	30.595	30.599	30.603	30.607	30.611	30.615	30.619	30.623	30.63
778	30.630	30.634	30.638	30.642	30.646	30.650	30.654	30.658	30.662	30.66
779	30.670	30.674	30.678	30.682	30.686	30.690	30.693	30.697	30.701	30.70
780	30.709	30.713	30.717	30.721	30.725	30.729	30.733	30.737	30.741	30.74
781	30.749	30.753	30.756	30.760	30.764	30.768	30.772	30.776	30.780	30.78
782	30.788	30.792	30.796	30.800	30.804	30.808	30.812	30.816	30.819	30.82
783	30.827	30.831	30.835	30.839	30.843	30.847	30.851	30.855	30.859	30.86
784	30.867	30.871	30.875	30.879	30.882	30.886	30.890	30.894	30.898	30.90
785	30.906	30.910	30.914	30.918	30.922	30.926	30.930	30.934	30.938	30.9
786	30.945	30.949	30.953	30.957	30.961	30.965	30.969	30.973	30.977	30.98
787	30.985	30.989	30.993	30.997	31.001	31.004	31.008	31.012	31.016	31.02
788	31.024	31.028	31.032	31.036	31.040	31.044	31.048	31.052	31.056	31.06
789	31.064	31.067	31.071	31.075	31.079	31.083.	31.087	31.091	31.095	31.09
790	31.103	31.107	31.111	31.115	31.119	31.123	31.127	31.130	31.134	31.13
791	31.142	31.146	31.150	31.154	31.158	31.162	31.166	31.170	31.174	31.17
792	31.182	31.186	31.190	31.193	31.197	31.201	31.205	31.209	31.213	31.21
793	31.221	31.225	31.229	31.233	31.237	31.241	31.245	31.249	31.253	31.25
994	31.260	31.264	31.268	31.272	31.276	31.280	31.284	31.288	31.292	31.29
795	31.300	31.304	31.308	31.312	31.316	31.319	31.323	31.327	31.331	31.33
796	31.339	31.343	31.347	31.351	31.355	31.359	31.363	31.367	31.371	31.37
797	31.379	31.382	31.386	31.390	31.394	31.398	31.402	31.406	31.410	31.41
798	31.418	31.422	31.426	31.430	31.434	31.438	31.442	31.445	31.449	31.45
799	31.457	31.461	31.465	31.469	31.473	31.477	31.481	31.485	31.489	31.49
800	31.497	31.501	31.505	31.508	31.512	31.516	31.520	31.524	31.528	31.53
				Hundredth	s of Millir	netres.	rabbier (			
0.	1.	2.	3.	4.	5		6.	7.	8	9.
.0000	.0004	.0008		A SHARE STATE					11 42 10 11	19 11 15 11

1 Millimetre = 0.443296 French or Paris Line.

fillimetres			y in	military to	Millimetre	es. Unit	s.			
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines	Par.lines.	Par.lines.	Par.lines.	Par.line	s. Par.line	s. Par.lines	Par.lines.	Par.lines.
300	132.99	133.43	133.88	134.32	134.76	135.2	1 135.68	136.09	136.54	136.98
310	137.42	137.87	138.31	138.75	139.19	139.6	THE OWNER OF THE OWNER		The second second	141.41
320	141.85	142.30	142.74	143.18	143.63	144.0	1000000	Mary Comment		145.84
330	146.29	146.73	147.17	147.62	148.06	148.5		1 35 1 3 3 3		150.28
340	150.72	151.16	151.61	152.05	152.49	152.9	4 153.38	153.82	154.27	154.71
350	155.15	155.60	156.04	156.48	156.93	157.3	7 157.81	158.26	158.70	159.14
360	159.59	160.03	160.47	160.92	161.36	161.8	0 162.23	162.69	163.13	163.58
370	164.02	164.46	164.91	165.35	165.79	166.2	4 166.68	167.12		168.01
380	168.45	168.90	169.34	169.78	170.23	170.6	7 171.11	171.56	172.00	172.44
390	172.89	173.33	173.77	174.22	174.66	175.1	0 175.5	175.99	176.43	176.88
400	177.32	177.76	178.20	178.65	179.09	179.5	3 179.98	180.42	180.86	181.31
410	181.75	182.19	182.64	183.08	183.52	183.9	7 184.4	184.85	185.30	185.74
420	186.18	186.63	187.07	187.51	187.96	188.4	0 188.8	1 189.29	189.73	190.17
430	190.62	191.06	191.50	191.95	192.39	192.8	3 193.28	3 193.72	194.16	194.61
440	195.05	195.49	195.94	196.38	196.82	197.2	7 197.7	198.15	198.60	199.04
450	199.48	199.93	200.37	200.81	201.26	201.7	0 202.1	202.59	203.03	203.47
460	203.92	204.36	204.80	205.25	205.69	206.1	3 206.58	3 207.02	207.46	207.91
470	208.35	208.79	209.24	209.68	210.12	210.5	7 211.0	211.45	211.90	212.34
480	212.78	213.23	213.67	214.11	214.56	215.0	0 215.4	215.88	216.33	216.77
490	217.22	217.66	218.10	218.54	218.99	219.4	3 219.8	7 220.32	220.76	221.20
500	221.65	222.09	222.53	222.98	223.42	223.8	6 224.3	224.75	225.19	225.64
510	226.08	226.52	226.97	227.41	227.85	228.3	0 228.7	1 229.18	229.63	230.07
520	230.51	230.96	231.40	231.84	232.29	232.7	3 233.1	7 233.62	234.06	234.50
530	234.95	235.39	235.83	236.28	236.72	237.1				238.94
540	239.38	239.82	240.27	240.71	241.15	241.6	0 242.0	1 242.48	242.93	243.37
550	243.81	244.26	244.70	245.14	245.59	246.0	3 246.4	7 246.92		247.80
560	248.25	248.69	249.13	249.57	250.01	250.4	0101	THE REAL PROPERTY.		252.24
570	252.68	253.12	253.57	254.01	254.45	254.9		A STATE OF THE PARTY OF THE PAR	CONTRACTOR OF THE	256.67
580	257.11	257.55	258.00	258.44	258.88	259.3			1 1 1 1 1 1 1 1 1	261.10
590	261.54	261.99	262.43	262.87	263.32	263.7	6 264.2	0 264.65	265.09	265.53
				Tenths	of Millim	etres.			X E W	
0.	1.	2.	3.	4.	5		6.	7.	8.	9.
0.000	0.044	0.089	0.133	0.17	7 0.2	222	0.266	0.310	0.355	0.399
				Hundred	ths of Milli	metres.		130,180		
0.000	0.004	0.009	0.013	0.018	3 0.0	22	0.027	0.031	0.035	0.040

1 Millimetre = 0.443296 French Line.

Millime-				1	Cenths of I	Millimetres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
No. Tan	Par.lines.	Par.lines.	Par.lines.	Par.lines.		Par.lines.	Par.lines.	Par.lines.		Par.line
600	265.98	266.02	266.07.	266.11	266.15	266.20	266.24	266.29	266.33	266.38
601	266.42	266.47	266.51	266.55	266.60	266.64	266.69	266.73	266.78	266.8
602	266.86	266.91	266.95	267.00	267.04	267.09	267.13	267.17	267.22	267.2
603	267.31	267.35	267.40	267.44	267.48	267.53	267.57	267.62	267.66	267.7
604	267.75	267.80	267.84	267.88	267.93	267.97	268.02	268.06	268.11	268.1
605	268.19	268.24	268.28	268.33	268.37	268.42	268.46	268.50	268.55	268.5
606	268.64	268.68	268.73	268.77	268.81	268.86	268.90	268.95	268.99	269.0
607	269.08	269.13	269.17	269.21	269.26	269.30	269.35	269.39	269.44	269.4
608	269.52	269.57	269.61	269.66	269.70	269.75	269.79	269.83	269.88	269.9
609	269.97	270.01	270.06	270.10	270.14	270.19	270.23	270.28	270.32	270.3
610	270.41	270.45	270.50	270.54	270.59	270.63	270.68	270.72	270.77	270.8
611	270.85	270.90	270.94	270.99	271.03	271.08	271.12	271.16	271.21	271.2
612	271.30	271.34	271.39	271.43	271.47	271.52	271.56	271.61	271.65	271.7
613	271.74	271.78	271.83	271.87	271.92	271.96	272.01	272.05	272.10	272.1
614	272.18	272.23	272.27	272.32	272.36	272.41	272.45	272.49	272.54	272.5
615	272.63	272.67	272.72	272.76	272.80	272.85	272.89	272.94	272.98	273.0
616	273.07	273.11	273.16	273.20	273.25	273.29	273.34	273.38	273.42	273.4
617	273.51	273.56	273.60	273.65	273.69	273.74	273.78	273.82	273.87	273.9
618	273.96	274.00	274.05	274.09	274.13	274.18	274.22	274.27	274.31	274.3
619	274.40	274.44	274.49	274.53	274.58	274.62	274.67	274.71	274.75	274.8
620	274.84	274.89	274.93	274.98	275.02	275.07	275.11	275.15	275.20	275.2
621	275.29	275.33	275.38	275.42	275.46	275.51	275.55	275.60	275.64	275.6
622	275.73	275.77	275.82	275.86	275.91	275.95	276.00	276.04	276.08	276.1
623	276.17	276.22	276.26	276.31	276.35	276.38	276.44	276.48	276.53	276.5
624	276.62	276.66	276.71	276.75	276.79	276.84	276.88	276.93	276.97	277.0
625	277.06	277.10	277.15	277.19	277.24	277.28	277.33	277.37	277.41	277.4
626	277.50	277.55	277.59	277.64	277.58	277.72	277.77	277.81	277.86	277.9
627	277.95	277.99	278.04	278.08	278.12	278.17	278.21	278.26	278.30	278.3
628	278.39	278.43	278.48	278.52	278.57	278.61	278.66	278.70	278.74	278.7
629	278.83	278.88	278.92	278.97	279.01	279.05	279.10	279.14	279.19	279.2
630	279.28	279.32	279.37	279.41	279.45	279.50	279.54	279.59	279.63	279.6
631	279.72	279.76	279.81	279.85	279.90	279.94	279.99	280.03	280.07	280.1
632	280.16	280.21	280.25	280.30	280.34	280.38	280.43	280.47	280.52	280.5
633	280.61	280.65	280.70	280.74	280.78	280.83	280.87	280.92	280.96	281.0
634	281.05	281.09	281.14	281.18	281.23	281.27	281.32	281.36	281.40	281.4
635	281.49	281.54	281.58	281.63	281.67	281.71	281.76	281.80	281.85	281.8
636	281.94	281.98	282.02	282.07	282.11	282.16	282.20	282.25	282.29	282.3
637	282.38	282.42	282.47	282.51	282.56	282.60	282.65	282.69	282.73	282.7
638	282.82	282.87	282.91	282.96	283.00	283.04	283.09	283.13	283.18	283.2
639	283.27	283.31	283.35	283.40	283.44	283.49	283.53	283.58	283.62	283.6
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Millimetre = 0.443296 French Line.

Millime-				Samila Si	Tenths of	Millimetres	•			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.		A COLUMN TO A COLU	Par.lines.	Par.lines.	Par.lines.			Par.lin
640	283.71	283.75	283.80	283.84	283.89	283.93	283.98	284.02	284.06	284.1
641	284.15	284.20	284.24	284.29	284.33	284.37	284.42	284.46	284.51	284.5
642	284.60	284.64	284.68	284.73	284.77	284.82	284.86	284.91	284.95	284.9
643	285.04	285.08	285.13	285.17	285.22	285.26	285.31	285.35	285.39	285.4
644	285.48	285.53	285.57	285.62	285.66	285.70	285.75	285.79	285.84	285.8
645	285.93	285.97	286.01	286.06	286.10	286.15	286.19	286.24	286.28	286.
646	286.37	286.41	286.46	286.50	286.55	286.59	286.64	286.68	286.72	286.
647	286.81	286.86	286.90	286.95	286.99	287.03	287.08	287.12	287.17	287.5
648	287.26	287.30	287.34	287.39	287.43	287.48	287.52	287.57	287.61	287.0
649	287.70	287.74	287.79	287.83	287.88	287.92	287.96	288.01	288.05	288.
650	288.14	288.19	288.23	288.28	288.32	288.36	288.41	288.45	288.50	288.
651	288.59	288.63	288.67	288.72	288.76	288.81	288.85	288.90	288.94	288.9
652	289.03	289.07	289.12	289.16	289.21	289.25	289.29	289.34	289.38	289.
653	289.47	289.52	289.56	289.61	289.65	289.69	289.74	289.78	289.83	289.8
654	289.92	289.96	290.00	290.05	290.09	290.14	290.18	290.23	290.27	290.
655	290.36	290.40	290.45	290.49	290.54	290.58	290.62	290.67	290.71	290.
656	290.80	290.85	290.89	290.94	290.98	291.02	291.07	291.11	291.16	291.
657	291.25	291.29	291.33	291.38	291.42	291.47	291.51	291.56	291.60	291.6
658	291.69	291.73	291.78	291.82	291.87	291.91	291.95	292.00	292.04	292.0
659	292.13	292.18	292.22	292.26	292.31	292.35	292.40	292.44	292.49	292.
660	292.58	292.62	292.66	292.71	292.75	292.80	292.84	292.89	292.93	292.9
661	293.02	293.06	293.11	293.15	293.20	293.24	293.28	293.33	293.37	293.4
662	293.46	293.51	293.55	293.59	293.64	293.68	293.73	293.77	293.82	293.8
663	293.91	293.95	293.99	294.04	294.08	294.13	294.17	294.22	294.26	294.3
664	294.35	294.39	294.44	294.48	294.53	294.57	294.61	294.66	294.70	294.7
665	294.79	294.84	294.88	294.92	294.97	295.01	295.06	295.10	295.15	295.1
666	295.24	295.28	295.32	295.37	295.41	295.46	295.50	295.55	295.59	295.6
667	295.68	295.72	295.77	295.81	295.86	295.90	295.94	295.99	296.03	296.0
668	296.12	296.17	296.21	296.25	296.30	296.34	296.39	296.43	296.48	296.5
669	296.56	296.61	296.65	296.70	296.74	296.79	296.83	296.88	296.92	296.9
670	297.01	297.05	297.10	297.14	297.19	297.23	297.27	297.32	297.36	297.4
671	297.45	297.50	297.54	297.58	297.63	297.67	297.72	297.76	297.81	297.8
672	297.89	297.94	297.98	298.03	298.07	298.12	298.16	298.21	298.25	298.2
673	298.34	298.38	298.43	298.47	298.52	298.56	298.60	298.65	298.69	298.7
674	298.78	298.83	298.87	298.91	298.96	299.00	299.05	299.09	299.14	299.1
675	299.22	299.27	299.31	299.36	299.40	299.45	299.49	299.54	299.58	299.6
676	299.67	299.71	299.76	299.80	299.85	299.89	299.93	299.98	300.02	300.0
677	300.11	300.16	300.20	300.24	300.29	300.33	300.38	300.42	300.47	300.5
678	300.55	300.60	300.64	300.69	300.73	300.78	300.82	300.86	300.91	300.9
679	301.00	301.04	301.09	301.13	301.18	301.22	301.26	301.31	301.35	301.4
19	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Millimetre = 0.443296 French line.

Millime-	Matak				Tenths of	Millimetres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
(Right of	Par.lines.	Par.lines.	1	Par.lines.	C	Par.lines.				
680	301.44	301.49	301.53	301.57	301.62	301.66	301.71	301.75	301.80	301.84
681	301.88	301.93	301.97	302.02	302.06	302.11	302.15	302.19	302.24	302.28
682	302.33	302.37	302.42	302.46	302.51	302.55	302.59	302.64	302.68	302.73
683	302.77	302.82	302.86	302.90	302.95	302.99	303.04	303.08	303.13	303.17
684	303.21	303.26	303.30	303.35	303.39	303.44	303.48	303.52	303.57	303.61
685	303.66	303.70	303.75	303.79	303.83	303.88	303.92	303.97	304.01	304.06
686	304.10	304.15	304.19	304.23	304.28	304.32	304.37	304.41	304.46	304.50
687	304.54	304.59	304.63	304.68	304.72	304.77	304.81	304.85	304.90	304.94
688	304.99	305.03	305.08	305.12	305.16	305.21	305.25	305.30	305.34	305.39
689	305.43	305.48	305.52	305.56	305.61	305.65	305.70	305.74	305.79	305.83
690	305.87	305.92	305.96	306.01	306.05	306.10	306.14	306.18	306.23	306.27
691	306.32	306.36	306.41	306.45	306.49	306.54	306.58	306.63	306.67	306.72
692	306.76	306.81	306.85	306.89	306.94	306.98	307.03	307.07	307.12	307.16
693	307.20	307.25	307.29	307.34	307.38	307.43	307.47	307.51	307.56	307.60
694	307.65	307.69	307.74	307.78	307.82	307.87	307.91	307.96	308.00	308.05
695	308.09	308.13	308.18	308.22	308.27	308.31	308.36	308.40	308.45	308.49
696	308.53	308.58	308.62	308.67	308.71	308.76	308.80	308.84	308.89	308.93
697	308.98	309.02	309.07	309.11	309.15	309.20	309.24	309.29	309.33	309.38
698	309.42	309.46	309.51	309.55	309.60	309.64	309.69	309.73	309.78	309.82
699	309.86	309.91	309.95	310.00	310.04	310.09	310.13	310.17	310.22	310.26
700	310.31	310.35	310.40	310.44	310.48	310.53	310.57	310.62	310.66	310.71
701	310.75	310.79	310.84	310.88	310.93	310.97	311.02	311.06	311.11	311.15
702	311.19	311.24	311.28	311.33	311.37	311.42	311.46	311.50	311.55	311.59
703	311.64	311.68	311.73	311.77	311.81	311.86	311.90	311.95	311.99	312.04
704	312.08	312.12	312.17	312.21	312.26	312.30	312.35	312.39	312.43	312.48
705	312.52	312.57	312.61	312.66	312.70	312.75	312.79	312.83	312.88	312.92
706	312.97	313.01	313.06	313.10	313.14	313.19	313.23	313.28	313.32	313.37
707	313.41	313.45	313.50	313.54	313.59	313.63	313.68	313.72	313.76	313.81
708	313.85	313.90	313.94	313.99	314.03	314.08	314.12	314.16	314.21	314.25
709	314.30	314.34	314.39	314.43	314.47	314.52	314.56	314.61	314.65	314.70
710	314.74	314.78	314.83	314.87	314.92	314.96	315.01	315.05	315.09	315.14
711	315.18	315.23	315.27	315.32	315.36	315.41	315.45	315.49	315.54	315.58
712	315.63	315.67	315.72	315.76	315.80	315.85	315.89	315.94	315.98	316.03
713	316.07	316.11	316.16	316.20	316.25	316.29	316.34	316.38	316.42	316.47
714	316.51	316.56	316.60	316.65	316.69	316.73	316.78	316.82	316.87	316.91
715	316.96	317.00	317.05	317.09	317.13	317.18	317.22	317.27	317.31	317.36
716	317.40	317.44	317.49	317.53	317.58	317.62	317.67	317.71	317.75	317.80
717	317.84	317.89	317.93	317.98	318.02	318.06	318.11	318.15	318.20	318.24
718	318.29	318.33	318.38	318.42	318.46	318.51	318.55	318.60	318.64	318.69
719	318.73	318.77	318.82	318.86	318.91	318.95	319.00	319.04	319.08	319.13
.0	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Millimetre = 0.443296 French Line.

Millime-				autore v	Tenths of	Millimetres	3.			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
11150000	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.			Par.lines.	Par.lines
720	319.17	319.22	319.26	319.31	319.35	319.39	319.44	319.48	319.53	319.57
721	319.62	319.66	319.70	319.75	319.79	319.84	319.88	319.93	319.97	320.02
722	320.06	320.10	320.15	320.19	320.24	320.28	320.33	320.37	320.41	320.46
723	320.50	320.55	320.59	320.64	320.68	320.72	320.77	320.81	320.86	320.90
724	320.95	320.99	321.03	321.08	321.12	321.17	321.21	321.26	321.30	321.35
725	321.39	321.43	321.48	321.52	321.57	321.61	321.66	321.70	321.74	321.79
726	321.83	321.88	321.92	321.97	322.01	322.05	322.10	322.14	322.19	322.23
727	322.28	322.32	322.36	322.41	322.45	322.50	322.54	322.59	322.63	322.68
728	322.72	322.76	322.81	322.85	322.90	322.94	322.99	323.03	323.07	323.12
729	323.16	323.21	323,25	323.30	323.34	323.38	323.43	323.47	323.52	323.56
<b>F</b> 20	323.61	323.65	323.69	323.74	323.78	323.83	323.87	323.92	323.96	324.00
730 731	324.05	324.09	324.14	324.18	324.23	324.27	324.32	324.36	324.40	324.45
732	324.49	324.54	324.58	324.63	324.67	324.71	324.76	324.80	324.85	324.89
733	324.94	324.98	325.02	325.07	325.11	325.16	325.20	325.25	325.29	325.33
734	325.38	325.42	325.47	325.51	325.56	325.60	325.65	325.69	325.73	325.78
									ETE BY	
735	325.82	325.87	325.91	325.96	326.00	326.04	326.09	326.13	326.18	326.22
736	326.27	326.31	326.35	326.40	326.44	326.49	326.53	326.58	326.62	326.66
737	326.71	326.75	326.80	326.84	326.89	326.93	326.98	327.02	327.06	327.11
738	327.15	327.20	327.24	327.29	327.33	327.37	327.42	327.46	327.51	327.55
739	327.60	327.64	327.68	327.73	327.77	327.82	327.86	327.91	327.95	327.99
740	328.04	328.08	328.13	328.17	328.22	328.26	328.30	328.35	328.39	328.44
741	328.48	328.53	328.57	328.62	328.66	328.70	328.75	328.79	328.84	328.88
742	328.93	328.97	329.01	329.06	329.10	329.15	329.19	329.24	329.28	329.32
743	329.37	329.41	329.46	329.50	329.55	329.59	329.63	329.68	329.72	329.77
744	329.81	329.86	329.90	329.95	329.99	330.03	330.08	330.12	330.17	330.21
	990 96	990 90	220.04	200 20	000 40	000 40	200 50	200 55	200 61	000 0
745 746	330.26 330.70	330.30 330.74	330.34	330.39 330.83	330.43 330.88	330.48 330.92	330.52 330.96	330.57 331.01	330.61	330.65
747	331.14	331.19	331.23	331.28	331.32	331.36	331.41	331.45	331.50	331.54
748	331.59	331.63	331.67	331.72	331.76	331.81	331.85	331.90	331.94	331.98
749	332.03	332.07	332.12	332.16	332.21	332.25	332.29	332.34	332.38	332.43
Sacs :	Chie Ni	B88 138	610 0	052 8	Aria	and of	20 m	note p	100	
750	332.47	332.52	332.56	332.60	332.65	332.69	332.74	332.78	332.83	332.87
751	332.92	332.96	333.00	333.05	333.09	333.14	333.18	333.23	333.27	333.31
752	333.36	333.40	333.45	333.49	333.54	333.58	333.62	333.67	333.71	333.76
753	333.80	333.85	333.89	333.93	333.98	334.02	334.07	334.11	334.16	334.20
754	334.25	334.29	334.33	334.38	334.42	334.47	334.51	334.56	334.60	334.64
755	334.69	334.73	334.78	334.82	334.87	334.91	334.95	335.00	335.04	335.09
756	335.13	335.18	335.22	335.26	335.31	335.35	335.40	335.44	335.49	335.53
757	335.58	335.62	335.66	335.71	335.75	335.80	335.84	335.89	335.93	335.97
758	336.02	336.06	336.11	336.15	336.20	336.24	336.28	336.33	336.37	336.42
759	336.46	336.51	336.55	336.59	386.64	336.68	336.73	336.77	336.82	336.86
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Millimetre = 0.443296 French Line

Millime- tres.								1	1	1
aros.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lin								
760	336.90	336.95	336.99	337.48	337.53	337.57	337.61	337.66	337.70	337.
761	337.35	337.39	337.44	337.92	337.97	338.01	338.06	338.10	338.15	338.
762	337.79	337.84	337.88	338.37	338.41	338.46	338.50	338.55	338.59	338.
763	338.23	338.28	338.32	338.81	338.86	338.90	338.94	338.99	339.03	339.
764	338.68	338.72	990.11	330.01	990.00	300.30	000.04	000.55	005.00	000.
765	339.12	339.17	339.21	339.25	339.30	339.34	339.39	339.43	339.48	339.
766	339.56	339.61	339.65	339.70	339.74	339.79	339.83	339.87	339.92	339.
767	340.01	340.05	340.10	340.14	340.19	340.23	340.27	340.32	340.36	340.
768	340.45	340.50	340.54	340.58	340.63	340.67	340.72	340.76	340.81	340.
769	340.89	340.94	340.98	341.03	341.07	341.12	341.16	341.20	341.25	341.
770	341.34	341.38	341.43	341.47	341.52	341.56	341.60	341.65	341.69	341.
771	341.78	341.83	341.87	341.91	341.96	342.00	342.05	342.09	342.14	342.
772	3 12.22	342.27	342.31	342.36	342.40	342.45	342.49	342.53	342.58	342.
773	342.67	342.71	342.76	342.80	342.85	342.89	342.93	342.98	343.02	343.
774	343.11	343.16	343.20	343.24	343.29	343.33	343.38	343.42	343.47	343.
775	343.55	343.60	343.64	343.69	343.73	343.78	343.82	343.86	343.91	343.
776	344.00	344.04	344.09	344.13	344.17	344.22	344.26	344.31	344.35	344.
777	344.44	344.49	344.53	344.57	344.62	344.66	344.71	344.75	344.80	344.
778	344.88	344.93	344.97	345.02	345.06	345.11	345.15	345.19	345.24	345.
779	345.33	345.37	345.42	345.46	345.50	345.55	345.59	345.64	345.68	345.
780	345.77	345.82	345.86	345.90	345.95	345.99	346.04	346.08	346.13	346.
781	346.21	346.26	346.30	346.35	346.39	346.44	346.48	346.52	346.57	346.
782	346.66	346.70	346.75	346.79	346.83	346.88	346.92	346.97	347.01	347.
783	347.10	347.15	347.19	347.23	347.28	347.32	347.37	347.41	347.46	347.
784	347.54	347.59	347.63	347.68	347.72	347.77	347.81	347.85	347.90	347.
* 785	347.99	348.03	348.08	348.12	348.16	348.21	348.25	348.30	348.34	348.
786	348.43	348.47	348.52	348.56	348.61	348.65	348.70	348.74	348.79	348.
787	348.87	348.92	348.96	349.01	349.05	349.10	349.14	349.18	349.23	349.
788	349.32	349.36	349.41	349.45	349.49	349.54	349.58	349.63	349.67	349.
789	349.76	349.80	349.85	349.89	349.94	349.98	350.03	350.07	350.12	350.
790	350.20	350.25	350.29	350.34	350.38	350.43	350.47	350.51	350.56	350.
791	350.65	350.69	350.74	350.78	350.82	350.87	350.91	350.96	351.00	351.
792	351.09	351.13	351.18	351.22	351.27	351.31	351.36	351.40	351.44	351.
793	351.53	351.58	351.62	351.67	351.71	351.76	351.80	351.84	351.89	351.
794	351.98	352.02	352.07	352.11	352.15	352.20	352.24	352.29	352.33	352.
795	352.42	352.46	352.51	352.55	352.60	352.64	352.69	352.73	352.77	352.
796	352.86	352.91	352.95	353.00	353.04	353.09	353.13	353.17	353.22	353.
797	353.31	353.35	353.40	353.44	353.48	353.53	353.57	353.62	353.66	353.
798	353.75	353.79	353.84	353.88	353.93	353.97	354.02	354.06	354.10	354.
799	354.19	354.24	354.28	354.33	354.37	354.42	354.46	354.50	354.55	354.
800	354.64	354.68	354.73	354.77	354.81	354.86	354.90	354.95	354.99	355.

## V. - VI.

#### COMPARISON

OF

## THE OLD FRENCH BAROMETER

WITH

THE ENGLISH AND THE METRICAL BAROMETERS,

OR

## TABLES

FOR CONVERTING FRENCH OR PARIS LINES INTO ENGLISH INCHES AND DECIMALS, AND INTO MILLIMETRES;

GIVING THE VALUES CORRESPONDING TO EVERY PARIS LINE FROM 120 TO 216 LINES, OR FROM 10 TO 18 INCHES; AND TO EVERY TENTH OF A LINE FROM 216 TO 348 LINES, OR FROM 18 TO 29 FRENCH INCHES.

#### TABLE V.

MM. J. J. Pohl and J. Schabus have published, in the number for March, 1852, of the Proceedings of the Imperial Academy of Vienna, Class of Mathematics and Natural Philosophy, a set of short Thermometrical and Barometrical Reduction Tables, among which is found a table for the reduction of the Old French Barometrical Scale into the English. As this table shows slight discrepancies from the one given in the following pages, it may not be out of place to state that they arise from an accidental error in the equation used by MM. Pohl and Schabus in computing their table. Adopting, as they do, Bird's value of the metre, viz.

1 metre = 39.37062 English inches,

the value of the Paris line is

1 Paris line = 0.088813 English inches.

But the table seems to have been computed by using the equation

1 Paris line = 0.088823 English inches,

which gives, at the end of the table,

 $348 \text{ lines} \times .088823 = 30.9104 \text{ English inches},$ 

instead of

348 " × .088813 = 30.9069 " "

thus causing an error

= 0.0035 " "

which, of course, gradually diminishes in lower numbers.

1 Paris Line = 0.088814 English Inch.

French or Paris				and the	Ur	nits.				
Lines. Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
10 Inch.	Eng. In. 10.658	Eng In. 10.746	Eng. In. 10.835	Eng. In. 10.924	Eng. In 11.013	Eng. In. 11.102	Eng. In. 11.191	Eng. In	100 / 100 miles 100 miles	Eng. In. 11.457
120 130	11.546	11.635	11.723	11.812	11.901	11.102	12.079	12.168		12.345
140	12.434	12.523	12.612	12.700	12.789	12.878	12.967	13.056		13.233
150	13.322	13.411	13.500	13.589	13.677	13.766	13.855	13.94		14.121
160	14.210	14.299	14.388	14.477	14.565	14.654	14.743	14.832	100000000000000000000000000000000000000	15.010
TAUS.	10000	BUR		7.35.3 E. S		EST TO	22.457	36		LENE
170	15.098	15.187	15.276	15.365	15.454	15.542	15.631	15.720		15.898
180	15.987	16.075	16.164	16.253	16.342	16.431	16.519	16.608		16.786
190	16.875	16.963	17.052	17.141	17.230	17.319	17.408	17.496		17.674
200	17.763	17.852	17.940	18.029	18.118	18.207	18.296	18.384		18.562
210	18.651	18.740	18.829	18.917	19.006	19.095	19.184	19.273	3   19.361	19.450
Paris				THE A	Ter	ths.				
Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
18 Inch.	Eng. In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In.	Eng. In		Eng. In
216	19.184	19.193	19.202	19.210	19.219	19.228	19.237	19.246		19.264
217	19.273	19.282	19.290	19.299	19.308	19.317	19.326	19.335		19.353
218	19.361	19.370	19.379	19.388	19.397	19.406	19.415	19.424		19.441
219	19.450	19.459	19.468	19.477	19.486	19.495	19.504	19.512		19.530
220	19.539	19.548	19.557	19.566	19.575	19.583	19.592	19.601		19.619
221	19.628	19.637	19.040	19.655	19.663	19.672	19.681	19.690	19.699	19.708
222	19.717	19.726	19.734	19.743	19.752	19.761	19.770	19.779	19.788	19.797
223	19.806	19.814	19.823	19.832	19.840	19.850	19.859	19.868		19.885
224	19.894	19.903	19.912	19.921	19.930	19.939	19.948	19.957	19.965	19.974
225	19.983	19.992	20.001	20.010	20.019	20.028	20.036	20.045	20.054	20.063
226	20.072	20,081	20.090	20.099	20.107	20.116	20.125	20.134	20.143	20.152
227	20.161	20.170	20.179	20.187	20.196	20.205	20.214	20.223	20.232	20.241
19 Inch.		MINUTE S		HOR.	ANG TRUE		MAN ME	3		- XFET
228	20.250	20.258	20.267	20.276	20.285	20.294	20.303	20.312		20.330
229	20.338	20.347	20.356	20.365	20.374	20.383	20.392	20.401	The state of the state of	20.418
230	20.427	20.436	20.445	20.454	20.463	20.472	20.481	20.489		20.507
231	20.516	20.525	20.534	20.543	20.552	20.560	20.569	20.578		20.596
232	20.605	20.614 20.703	20.623	20.631 20.720	20.640	20.649 20.738	20.658	20.667	100	20.685
233	20.094	20.703	20.711	20.120	20.125	20.190	20.141	20.750	20.705	20.114
234	20.782	20.791	20.800	20.809	20.818	20.827	20.836	20.845	20.854	20.862
235	20.871	20.880	20.889	20.898	20.907	20.916	20.925	20.933		20.951
236	20.960	20.969	20.978	20.987	20.996	21.005	21.013	21.022		21.040
237	21.049	21.058	21.067	21.076	21.084	21.093	The state of the s	21.111		21.129
238	21.138	21.147	21.155	21.164	21.173	21.182	21.191	21.200	21.209	21.218
239	21.227	21.235	21.244	21.253	21.262	21.271	21.280	21.289	21.298	21.306
				Hundr	edths of a	Line.				
0.	1.	2.	3.	4.	5		6.	7.	8.	9.
-			-							

1 Paris Line = 0.088814 English Inch.

			1		Tenths	of a Line.				
French or ParisLines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
20 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eug. In.	Eng. In.	Eng. In.	Eng. In
240	21.315	21.324	21.333	21.342	21.351	21.360	21.369	21.378	21.386	21.395
241	21.404	21.413	21.422	21.431	21.440	21.449	21.457	21.466	21.475	21.484
242	21.493	21.502	21.511	21.520	21.529	21.537	21.546	21.555		21.573
243	21.582	21.591	21.600	21.608	21.617	21.626	21.635	21.644	1.3.43	21.662
244	21.671	21.679	21.688	21.697	21.706	21.715	21.724	21.733	21.742	21.751
245	21.759	21.768	21.777	21.786	21.795	21.804	21.813	21.822	21.830	21.839
246	21.848	21.857	21.866	21.875	21.884	21.893	21.902	21.910	21.919	21.928
247	21.937	21.946	21.955	21.964	21.973	21.981	21.990	21.999	22.008	22.017
248	22.026	22.035	22.044	22.053	22.061	22.070	22.079	22.088	22.097	22.106
249	22.115	22.124	22.132	22.141	22.150	22.159	22.168	22.177	22 186	22.195
250	22.203	22.212	22.221	22.230	22.239	22.248	22.257	22.266	22.275	22.283
251	22.292	22.301	22.310	22.319	22.328	22.337	22.346	22.354	22.363	22.372
21 In. =	100		1000		100		-	1	OF I	1.445
252	22.381	22.390	22.399	22.408	22.417	22.426	22.434	22.443	22.452	22.461
253 .	22.470	22.479	22.488	22.497	22.505	22.514	22.523	22.532	22.541	22.550
254	22.559	22.568	22.577	22.585	22.594	22.603	22.612	22.621	22.630	22.639
255	22.648	22.656	22.665	22.674	22.683	22.692	22.701	22.710	22.719	22.728
256	22.736	22.745	22.754	22.763	22.772	22.781	22.790	22.799	22.807	22.816
257	22.825	22.834	22.843	22.852	22.861	22.870	22.878	22.887	22.896	22.905
258	22.914	22.923	22.932	22.941	22.950	22.958	22.967	22.976	22.985	22.994
259	23.003	23.012	23.021	23.029	23.038	23.047	23.056	23.065	23.074	23.083
260	23.092	23.101	23.109	23.118	23.127	23.136	23.145	23.154	23.163	23.172
261	23.180	23.189	23.198	23.207	23.216	23.225	23.234	23.243	23.252	23.260
262	23.269	23.278	23.287	23.296	23.305	23.314	23.323	23.331	23.340	23.349
263	23.358	23.367	23.376	23.385	23.394	23.402	23.411	23.420	23.429	23.438
22 In. =	20 115				SHEET IN		Charles 1		1185.05	tel
264	23.447	23.456	23.465	23.474	23.482	23,491	23.500	23.509	23.518	23.527
265 266	23.536 23.625	23.545	23.553	23.562	23.571	23.580	23.589	23.598	23.607	23.616
267	23.713	23.633	23.642 23.731	23.651	23.660	23.669	23.678	23.687	23.696	23.704
268	23.802	23.811	23.820	23.740	23.749 23.838	23.758	23.767	23.776 23.864	23.784 23.873	23.793 23.882
269	23.891	23.900	23.909	23.918	23.926	23.935	23.944	23.953	23.962	23.971
Towns.	EW. IN.	NACE V			100000	20.000	201011	20.000	20.002	20.011
270	23.980	23.989	23.998	24,006	24.015	24.024	24.033	24.042	24.051	24.060
271	24.069	24.077	24.086	24.095	24.104	24.113	24.122	24.131	24.140	24.149
272	24.157	24.166	24.175	24.184	24.193	24.202	24.211	24.220	24.228	24.237
273	24.246	24.255	24.264	24.273	24.282	24.291	24.300	24.308	24.317	24.326
274	24.335	24.344	24.353	24.362	24.371	24.379	24.388	24.397	24.406	24.415
275	24.424	24.433	24.442	24.450	24.459	24.468	24.477	24.486	24.495	24.504
				Hundre	dths of a	Line.	1412	10.42		
0.	1.	2.	3.	1				Py 1	e 1	
		-		4.	_ 5		-	7.	8.	9.
.0000	.0009	.0018	.0027	.0036	.00	14 .00	53 .0	0062	.0071	.0080

1 Paris Line = 0.088814 English Inch.

French or	Tenths of a Line.										
ParisLines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
23 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.		Eng. In.	Eng. In.	Eng. In	
276	24.513	24.522	24.530	24.539	24.548	24.557	24.566	24.575	24.584	24.593	
277	24.601	24.610	24.619	24.628	24.637	24.646	100 miles	24.664	24.673	24.681	
278	24.690	24.699	24.708	24.717	24.726	24.735	The state of the s	24.752	24.761	24.770	
279	24.779	24.788	24.797	24.806	24.815	24.824	29.00	24.841	24.850	24.859	
280	24.868	24.877	24.886	24.895	24.903	24.912	24.921	24.930	24.939	24.948	
281	24.957	24.966	24.974	24.983	24.992	25.001	25.010	25.019	25.028	25.03	
282	25.046	25.054	25.063	25.072	25.081	25.090	25.099	25.108	25.117	25.125	
283	25.134	25.143	25.152	25.161	25.170	25.179	25.188	25.197	25.205	25.214	
284	25.223	25.232	25.241	25.250	25.259	25.268	25.276	25.285	25.294	25.303	
285	25.312	25.321	25.330	25.339	25.348	25.356	25.365	25.374	25.383	25.392	
286	25.401	25.410	25.419	25.427	25.436	25.445	25.454	25.463	25.472	25.481	
287	25.490	25.498	25.507	25.516	25.525	25.534	25.543	25.552	25.561	25.570	
24 In. =			07.400			1000			07 010	0	
288	25.578	25.587	25.596	25.605	25.614	25.623	25.632	25.641	25.649	25.658	
289	25.667	25.676	25.685	25.694	25.703	25.712	25.721	25.729	25.738	25.747	
290	25.756	25.765	25.774	25.783	25.792	25.800	25.809	25.818	25.827	25.836	
291	25.845	25.854	25.863	25.872	25.880	25.889	25.898	25.907	25.916	25.92	
292	25.934	25.943	25.951	25.960	25.969	25.978	25.987	25.996	26.005	26.014	
293	26.023	26.031	26.040	26.049	26.058	26.067	26.076	26.085	26.094	26.102	
294	26.111	26.120	26.129	26.138	26.147	26.156	26.165	26.173	26.182	26.191	
295	26.200	26.209	26.218	26.227	26.236	26.245	26.253	26.262	26.271	26.280	
296	26.289	26.298	26.307	26.316	26.324	26.333	26.342	26.351	26.360	26.369	
297	26.378	26.387	26.396	26.404	26.413	26.422	26.431	26.440	26.449	26.458	
298	26.467	26.475	26.484	26.493	26.502	26.511	26.520	26.529	26.538	26.547	
299	26.555	26.564	26.573	26.582	26.591	26.600	26.609	26.618	26.626	26.635	
25 In. =	B. Bank ;	12.50	No. of Lot	mile of the	read a	was 'r	and the	- 9 - 7 - 4	STATE OF		
300	26.644	26.653	26.662	26.671	26.680	26.689	26.697	26.706	26.715	26.724	
301	26.733	26.742	26.751	26.760	26.769	26.777	26.786	26.795	26.804	26.813	
302	26.822	26.831	26.840	26.848	26.857	26.866	26.875	26.884	26.893	26.902	
303	26.911	26.920	26.928	26.937	26.946	26.955	26.964	26.973	26.982	26.991	
304	26.999	27.008	27.017	27.026	27.035	27.044	27.053	27.062	27.071	27.079	
305	27.088	27.097	27.106	27.115	27.124	27.133	27.142	27.150	27.159	27.168	
306	27.177	27.186	27.195	27.204	27.213	27.221	27.230	27.239	27.248	27.257	
307	27.266	27.275	27.284	27.293	27.301	27.310	27.319	27.328	27.337	27.346	
308	27.355	27.364	27.372	27.381	27.390	27.399	27.408	27.417	27.426	27.435	
309	27.444	27.452	27.461	27.470	27.479	27.488	27.497	27.506	27.515	27.523	
310	27.532	27.541	27.550	27.559	27.568	27.577	27.586	27.595	27.603	27.612	
311	27.621	27.630	27.639	27.648	27.657	27.666	27.674	27.683	27.692	27.701	
Hundredths of a Line.											
0.	1.	2.	3.	1 4.	5	.	6.	7.	8.	9.	

.0009

.0018

.0027

.0044

.0053

.0062

.0071

.0080

.0036

1 Paris Line = 0.088814 English Inch.

French or	Tenths of a Line.										
ParisLines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
26 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In	
312	27.710	27.719	27.728	27.737	27.745	27.754	27.763	27.772	27.781	27.790	
313	27.799	27.808	27.817	27.825	27.834	27.843	27.852	27.861	27.870	27.879	
314	27.888	27.896	27.905	27.914	27.923	27.932	27.941	27.950	27.959	27.968	
315	27.976	27.985	27.994	28.003	28.012	28.021	28.030	28.039	28.047	28.056	
316	28.065	28.074	28.083	28.092	28.101	28.110	28.119	28.127	28.136	28.145	
317	28.154	28.163	28.172	28.181	28.190	28.198	28.207	28.216	28.225	28.234	
318	28.243	28.252	28.261	28.269	28.278	28.287	28.296	28.305	28.314	28.323	
319	28.332	28.341	28.349	28.358	28.367	28.376	28.385	28.394	28.403	28.412	
320	28.420	28.429	28.438	28.447	28.456	28.465	28.474	28.483	28.492	28.500	
321	28.509	28.518	28.527	28.536	28.545	28.554	28.563	28.571	28.580	28.589	
322	28.598	28.607	28.616	28.625	28.634	28.643	28.651	28.660	28.669	28.678	
323	28.687	28.696	28.705	28.714	28.722	28.731	28.740	28.749	28.758	28.767	
27 In. =									Un ente	Land	
324	28.776	28.785	28.793	28.802	28.811	28.820	28.829	28.838	28.847	28.856	
325	28.865	28.873	28.882	28.891	28.900	28.909	28.918	28.927	28.936	28.944	
326	28.953	28.962	28.971	28.980	28.989	28.998	29.007	29.016	29.024	29.033	
327	29.042	29.051	29.060	29.069	29.078	29.087	29.095	29.104	29.113	29.122	
328	29.131	29.140	29.149	29.158	29.167	29.175	29.184	29.193	29.202	29.211	
329	29.220	29.229	29.238	29.246	29.255	29.264	29.273	29.282	29.291	29.300	
330	29.309	29.318	29.326	29.335	29.344	29.353	29.362	29.371	29.380	29.389	
331	29.397	29.406	29.415	29.424	29.433	29.442	29.451	29.460	29.468	29.477	
332	29.486	29.495	29.504	29.513	29.522	29.531	29.540	29.548	29.557	29.566	
333	29.575	29.584	29.593	29.602	29.611	29.619	29.628	29.637	29.646	29.655	
334	29.664	29.673	29.682	29.691	29.699	29.708	29.717	29.726	29.735	29.744	
335	29.753	29.762	29.770	29.779	29.788	29.797	29.806	29.815	29.824	29.833	
28 In. =											
336	29.842	29.850	29.859	29.868	29.877	29.886	29.895	29.904	29.913	29.921	
337	29.930	29.939	29.948	29.957	29.966	29.975	29.984	29.992	30.001	30.010	
338	30.019	30.028	30.037	30.046	30.055	30.064	30.072	30.081	30.090	30.099	
339	30.108	30.117	30.126	30.135	30.143	30.152	30.161	30.170	30.179	30.188	
340	30.197	30.206	30.215	30.223	30.232	30.241	30.250	30.259	30.268	30.277	
341	30.286	30.294	30.303	30.312	30.321	30.330	30.339	30.348	30.357	30.366	
342	30.374	30.383	30.392	30.401	30.410	30.419	30.428	30.437	30.445	30.454	
343	30.463	30.472	30.481	30.490	30.499	30.508	30.516	30.525	30.534	30.543	
344	30.552	30.561	30.570	30.579	30.588	30.596	30.605	30.614	30.623	30.632	
345	30.641	30.650	30.659	30.667	30.676	30.685	30.694	30.703	30.712	30.721	
346	30.730	30.739	30.747	30.756	30.765	30.774	30.783	30.792	30.801	39.810	
347 29 In. =	30.818	30.827	30.836	30.845	30.854	30.863	30.872	30.881	30.990	30.898	
348	30.907	30.916	30.925	30.934	30.943	30.952	30.961	30.969	30.978	30.987	

Hundredths of a Line.

0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
.0000	.0009	.0018	.0027	.0036	.0044	.0053	.0062	.0071	.0080

1 Paris Line = 2.255829 Millimetres.

120         270.70         272.96         275.21         277.47         279.72         281.98         284.23         286.49         288.75         291.0           130         293.26         295.51         297.77         300.03         302.28         304.54         306.79         309.05         311.30         313.5           140         315.82         318.07         320.33         322.58         324.84         327.10         329.35         331.61         333.86         336.11           150         338.37         340.63         342.89         345.14         347.40         349.65         351.91         354.17         356.42         358.6           160         360.93         363.19         365.44         367.70         369.96         372.21         374.47         376.72         378.98         381.2           170         383.49         385.75         388.00         390.26         392.51         394.77         397.03         399.28         401.54         403.7           180         406.05         408.30         410.56         412.82         415.07         417.33         419.58         421.84         424.10         426.3           190         423.61         430.86	French or ParisLines.					Un	its.				E
120	Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
130											Millim.
140   315.82   318.07   320.33   322.58   324.84   327.10   329.35   331.61   333.86   336.11   360.62   312.89   315.14   317.40   319.65   351.91   354.17   356.42   358.6   360.93   363.19   365.44   367.70   369.96   372.21   374.47   376.72   378.98   381.2   381.30   383.49   385.75   388.00   399.26   392.51   394.77   397.03   399.28   401.54   426.3   190   428.61   430.86   433.12   435.37   437.63   439.89   442.14   444.40   446.65   448.9   200   451.17   453.42   455.68   457.93   460.19   462.44   464.70   466.96   469.21   471.4   471.40				The year			ACTOR DESCRIPTION	8000			
150	Market St. In	Marine Think	ACCOUNT OF THE PARTY OF THE PAR	7.00		The state of the s	Charles and a second	ALC: NO.			
160   360.93   363.19   365.44   367.70   369.96   372.21   374.47   376.72   378.98   381.2   170   383.49   355.75   388.00   390.26   392.51   394.77   397.03   399.28   401.54   403.7   180   406.05   408.30   410.56   412.82   415.07   417.33   419.58   421.84   424.10   426.3   190   428.61   430.86   433.12   435.37   437.63   439.59   442.14   444.40   446.65   448.9   200   451.17   453.42   455.68   457.93   460.19   462.44   464.70   466.96   469.21   471.4   210   473.72   475.98   478.24   480.49   482.75   485.00   487.26   489.51   491.77   494.0	Maria Contract					- 01-0019	CONTRACTOR OF THE PARTY OF THE		A CONTRACTOR OF THE PARTY OF TH	-373	
170	V										
180	100	500.55	505.19	909.44	307.70	309.90	314.41	914.41	310.12	310.30	901.2
180	170	383.49	385 75	388 00	390.26	392 51	301 77	307 03	300.28	401.54	403.79
190				17000000			The same of the same of				
200						120000			The second second		
Paris   Lines.   Pari	7			1 19943					49.50		
Paris Lines.  O. 1. 2. 3. 4. 5. 6. 7. 8. 9.  18 Inch. Millim.	37	0-04-0		The state of the s	1111	4 E 2 2/2 N			WALL COLOR		The state of the s
Paris Lines.   O.		110112	1 410.00	, 110:21	1 400.40			401.20	400.01	101.11	10110
Lines.   O.   1.   2.   3.   4.   5.   6.   7.   8.   9.				2486		Tenths o	f a Line.				
216		0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
217	18 Inch.			Millim.	Millim.	Millim.					Millim.
218    491.77   492.00   492.22   492.45   492.67   492.90   493.12   493.35   493.58   493.86   219   494.03   494.25   494.48   494.70   494.93   495.15   495.38   495.61   495.83   496.00   498.32   498.54   498.76   498.99   499.21   499.44   499.67   499.89   500.12   500.34   500.55   500.79   501.02   501.25   501.47   501.70   501.92   502.15   502.37   502.60   502.85   503.05   503.28   503.50   503.73   503.95   504.18   504.40   504.63   504.55   505.05	216	487.26	487.48	487.71	487.94	488.16	488.39	488.61	488.84	489.06	489.2
219    494.03    494.25    494.48    494.70    494.93    495.15    495.88    495.61    495.83    496.00    496.28    496.51    496.73    496.96    497.18    497.41    497.64    497.86    498.09    498.3    221    498.54    498.76    498.99    499.21    499.44    499.67    499.89    500.12    500.34    500.5	217	The second section is a second	489.74	489.97	Comments.	490.42	490.64	490.87	491.09	491.32	-1870
220	218	491.77	492.00	492.22	492.45	492.67	492.90	493.12	493.35	493.58	493.8
221 498.54 498.76 498.99 499.21 499.44 499.67 499.89 500.12 500.34 500.5  222 500.79 501.02 501.25 501.47 501.70 501.92 502.15 502.37 502.60 502.82  223 503.05 503.28 503.50 503.73 503.95 504.18 504.40 504.63 504.85 505.08  224 505.31 505.53 505.76 505.98 506.21 506.43 506.66 506.88 507.11 507.3  225 507.56 507.79 508.01 508.24 508.46 508.69 508.91 509.14 509.37 509.58  226 509.82 510.04 510.27 510.49 510.72 510.95 511.17 511.40 511.62 511.86  227 512.07 512.30 512.52 512.75 512.98 513.20 513.43 513.65 513.88 514.10  228 514.33 514.55 514.78 515.01 515.23 515.46 515.68 515.91 516.13 516.36  229 516.58 516.81 517.04 517.26 517.49 517.71 517.94 518.16 518.39 518.61  230 518.84 519.07 519.29 519.52 519.74 519.97 520.19 520.42 520.65 520.87  231 521.10 521.32 521.55 521.77 522.00 522.22 522.45 522.68 522.90 523.13  232 523.35 523.58 523.80 524.03 524.25 524.48 524.71 524.93 525.16 525.38  233 525.61 525.83 526.06 526.28 526.51 526.74 526.96 527.19 527.41 527.64  234 527.86 528.09 528.32 528.54 528.77 528.99 529.22 529.44 529.67 529.89  235 530.12 530.35 530.57 530.80 531.02 531.25 531.47 531.70 531.92 532.15  236 532.38 532.60 532.83 533.05 533.28 533.50 533.73 533.95 534.18 534.41  237 534.63 534.86 535.08 535.31 535.53 535.76 535.98 536.21 536.44 536.64  238 536.89 537.11 537.34 537.56 537.79 538.02 538.24 538.47 538.69 538.29  239 539.14 539.37 539.59 539.82 540.05 540.27 540.50 540.72 540.95 541.17  Tenths of a Line.	219	494.03	494.25	494.48	494.70	494.93	495.15	495.38	495.61	495.83	496.0
222   500.79   501.02   501.25   501.47   501.70   501.92   502.15   502.37   502.60   502.83   223   503.05   503.28   503.50   503.73   503.95   504.18   504.40   504.63   504.85   505.08   224   505.31   505.53   505.76   505.98   506.21   506.43   506.66   506.88   507.11   507.3   225   507.56   507.79   508.01   508.24   508.46   508.69   508.91   509.14   509.37   509.58   226   509.82   510.04   510.27   510.49   510.72   510.95   511.17   511.40   511.62   227   512.07   512.30   512.52   512.75   512.98   513.20   513.43   513.65   513.88   228   514.33   514.55   514.78   515.01   515.23   515.46   515.68   515.91   516.13   229   516.58   516.81   517.04   517.26   517.49   517.71   517.94   518.16   518.39   518.61   230   518.84   519.07   519.29   519.52   519.74   519.97   520.19   520.42   520.65   520.87   231   521.10   521.32   521.55   521.77   522.00   522.22   522.45   522.68   522.90   523.13   232   523.35   523.58   523.80   524.03   524.25   524.48   524.71   524.93   525.16   525.38   233   525.61   525.83   526.06   526.28   526.51   526.74   526.96   527.19   527.41   527.64   234   527.86   528.09   528.32   528.54   528.77   528.99   529.22   529.44   529.67   529.89   235   530.12   530.35   530.57   530.80   531.02   531.25   531.47   531.70   531.92   532.15   236   532.38   532.60   532.83   535.08   535.31   535.53   535.76   535.73   533.95   534.63   534.64   536.66   238   536.89   537.11   537.34   537.56   537.79   538.02   538.24   538.47   538.69   538.92   239   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17    Tenths of a Line.	220	496.28	496.51	496.73	496.96	497.18	497.41	497.64	497.86	498.09	498.3
223   503.05   503.28   503.50   503.73   503.95   504.18   504.40   504.63   504.85   505.06   224   505.31   505.53   505.76   505.98   506.21   506.43   506.66   506.88   507.11   507.34   225   507.56   507.79   508.01   508.24   508.46   508.69   508.91   509.14   509.37   509.58   226   509.82   510.04   510.27   510.49   510.72   510.95   511.17   511.40   511.62   227   512.07   512.30   512.52   512.75   512.98   513.20   513.43   513.65   513.88   19 Inch.  228   514.33   514.55   514.78   515.01   515.23   515.46   515.68   515.91   516.13   516.36   229   516.58   516.81   517.04   517.26   517.49   517.71   517.94   518.16   518.39   518.61   230   518.84   519.07   519.29   519.52   519.74   519.97   520.19   520.42   520.65   231   521.10   521.32   521.55   521.77   522.00   522.22   522.45   522.68   522.90   523.13   232   523.33   523.58   523.80   524.03   524.25   524.48   524.71   524.93   525.16   525.38   233   525.61   525.83   526.06   526.28   526.51   526.74   526.96   527.19   527.41   527.64   234   527.86   528.09   528.32   528.54   528.77   528.99   529.22   529.44   529.67   529.88   235   530.12   530.35   530.57   530.80   531.02   531.25   531.47   531.70   531.92   532.15   236   532.38   532.60   532.83   533.05   533.28   533.50   533.73   533.95   534.18   534.41   237   534.63   534.86   535.08   535.31   535.53   535.76   535.98   536.21   536.44   536.66   238   536.89   537.11   537.34   537.56   537.79   538.02   538.24   538.47   538.69   538.92   239   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17    Tenths of a Line.	221	498.54	498.76	498.99	499.21	499.44	499.67	499.89	500.12	500.34	500.5
223   503.05   503.28   503.50   503.73   503.95   504.18   504.40   504.63   504.85   505.06   224   505.31   505.53   505.76   505.98   506.21   506.43   506.66   506.88   507.11   507.3- 225   507.56   507.79   508.01   508.24   508.46   508.69   508.91   509.14   509.37   509.55   226   509.82   510.04   510.27   510.49   510.72   510.95   511.17   511.40   511.62   227   512.07   512.30   512.52   512.75   512.98   513.20   513.43   513.65   513.88   19 Inch.  228   514.33   514.55   514.78   515.01   515.23   515.46   515.68   515.91   516.13   516.36   229   516.58   516.81   517.04   517.26   517.49   517.71   517.94   518.16   518.39   518.61   230   518.84   519.07   519.29   519.52   519.74   519.97   520.19   520.42   520.65   520.87   231   521.10   521.32   521.55   521.77   522.00   522.22   522.45   522.68   522.90   523.13   232   523.33   523.58   523.80   524.03   524.25   524.48   524.71   524.93   525.16   525.38   233   525.61   525.83   526.06   526.28   526.51   526.74   526.96   527.19   527.41   527.64   234   527.86   528.09   528.32   528.54   528.77   528.99   529.22   529.44   529.67   529.88   235   530.12   530.35   530.57   530.80   531.02   531.25   531.47   531.70   531.92   532.15   236   532.38   532.60   532.83   533.05   533.28   533.50   533.73   533.95   534.18   534.41   237   534.63   534.86   535.08   535.31   535.53   535.76   535.98   536.21   536.44   536.66   238   536.89   537.11   537.34   537.56   537.79   538.02   538.24   538.47   538.69   538.92   239   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17    Tenths of a Line.	222	500.79	501.02	501.25	501.47	501.70	501.92	502.15	502.37	502.60	502.82
224   505.31   505.53   505.76   505.98   506.21   506.43   506.66   506.88   507.11   507.3-255   507.56   507.79   508.01   508.24   508.46   508.69   508.91   509.14   509.37   509.58   226   509.82   510.04   510.27   510.49   510.72   510.95   511.17   511.40   511.62   511.84   512.77   512.30   512.52   512.75   512.98   513.20   513.43   513.65   513.88   514.10   516.88   514.10   516.88   514.10   516.88   514.10   516.88   515.91   516.13   516.36   516.88   516.81   517.04   517.26   517.49   517.71   517.94   518.16   518.39   518.61   520   518.84   519.07   519.29   519.52   519.74   519.97   520.19   520.42   520.65   520.87   231   521.10   521.32   521.55   521.77   522.00   522.22   522.45   522.68   522.90   523.13   523.33   523.58   523.80   524.03   524.25   524.48   524.71   524.93   525.16   525.38   526.66   526.28   526.51   526.74   526.96   527.19   527.41   527.64   527.86   528.09   528.32   528.54   528.87   528.99   529.22   529.44   529.67   529.88   523.80   534.86   535.38   533.05   533.28   533.50   533.73   533.95   534.18   534.41   537.84   537.56   537.79   538.02   538.24   538.47   538.69   538.92   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17   540.95   541.17   540.95   541.17   540.95   541.17   540.95   541.17   540.95   541.17   540.95   540.72   540.95   541.17   540.95   541.17   540.95   540.72   540.95   540.72   540.95   541.17   540.95   540.72   540.95   541.17   540.95   540.72   540.95   541.17   540.95   540.72   540.95   541.17   540.95   541.17   540.95   540.72   540.95   540.95   540.95   540.72   540.95   541.17   540.95   540	Black Street	C. S. S. L. L.	1 1 10 10 10 10 10 10	E SHALL CHA	5.78 (S. S. S. S. S. S.	1.1116.5.111	TANK DE		A plant of		
225   507.56   507.79   508.01   508.24   508.46   508.69   508.91   509.14   509.37   509.58   226   509.82   510.04   510.27   510.49   510.72   510.95   511.17   511.40   511.62   511.86   512.77   512.30   512.52   512.75   512.98   513.20   513.43   513.65   513.88   514.10   511.62   511.86   513.88   514.10   516.83   514.55   514.78   515.01   515.23   515.46   515.68   515.91   516.13   516.36   518.84   519.07   519.29   519.52   519.74   519.97   520.19   520.42   520.65   520.83   231   521.10   521.32   521.55   521.77   522.00   522.22   522.45   522.68   522.90   523.15   523.35   523.88   524.03   524.25   524.48   524.71   524.93   525.16   525.38   525.61   525.83   526.06   526.28   526.51   526.74   526.96   527.19   527.41   527.64   523.8   523.80   533.35   533.28   533.50   533.37   533.95   534.18   534.41   537.84   537.84   537.84   537.84   537.84   537.85   538.02   538.24   538.47   538.69   538.92   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17   540.95   541.17   540.95   541.17   540.95   541.17   540.95   540.72   540.95   540.72   540.95   541.17   540.95   540.72   540.95   541.17   540.95   541.17   540.95   540.72   540.95   540.72   540.95   541.17   540.95   541.17   540.95   540.72   540.95   541.17   540.95   541.17   540.95   540.72   540.95   541.17   540.95   541.17   540.95   540.72   540.95   541.17   540.95   541.17   540.95   540.72   540.95   541.17   540.95   541.17   540.95   540.72   540.95   541.17   540.95   540.72   540.95   541.17   540.95   541.17   540.95   540.72   540.95   540.95   541.17   540.95   540.	200	COLD STORY		1.1.00000 /	DEFAULT AND A STREET		LEGISTER STATE	C330000 C	1000	The second second	
226   509.82   510.04   510.27   510.49   510.72   510.95   511.17   511.40   511.62   511.86   227   512.07   512.30   512.52   512.75   512.98   513.20   513.43   513.65   513.88   514.16   19 Inch.  228   514.33   514.55   514.78   515.01   515.23   515.46   515.68   515.91   516.13   516.36   229   516.58   516.81   517.04   517.26   517.49   517.71   517.94   518.16   518.39   518.61   230   518.84   519.07   519.29   519.52   519.74   519.97   520.19   520.42   520.65   520.87   231   521.10   521.32   521.55   521.77   522.00   522.22   522.45   522.68   522.90   523.15   232   523.35   523.58   523.80   524.03   524.25   524.48   524.71   524.93   525.16   525.38   233   525.61   525.83   526.06   526.28   526.51   526.74   526.96   527.19   527.41   527.64   234   527.86   528.09   528.32   528.54   528.77   528.99   529.22   529.44   529.67   529.88   235   530.12   530.35   530.57   530.80   531.02   531.25   531.47   531.70   531.92   532.18   236   532.38   532.60   532.83   533.05   533.28   533.50   533.73   533.95   534.18   534.41   237   534.63   534.86   535.08   535.31   535.53   535.76   535.98   536.21   536.44   536.66   238   536.89   537.11   537.34   537.56   537.79   538.02   538.24   538.47   538.69   538.92   239   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17    Tenths of a Line.   0.   1.   2.   3.   4.   5.   6.   7.   8.   9.	A CONTRACTOR OF THE PARTY OF TH	100			TOTAL SECTION						
227   512.07   512.30   512.52   512.75   512.98   513.20   513.43   513.65   513.88   514.16   228   514.33   514.55   514.78   515.01   515.23   515.46   515.68   515.91   516.13   516.36   229   516.58   516.81   517.04   517.26   517.49   517.71   517.94   518.16   518.39   518.61   230   518.84   519.07   519.29   519.52   519.74   519.97   520.19   520.42   520.65   520.87   231   521.10   521.32   521.55   521.77   522.00   522.22   522.45   522.68   522.90   523.15   232   523.35   523.58   523.80   524.03   524.25   524.48   524.71   524.93   525.16   525.38   233   525.61   525.83   526.06   526.28   526.51   526.74   526.96   527.19   527.41   527.64   234   527.86   528.09   528.32   528.54   528.77   528.99   529.22   529.44   529.67   529.89   235   530.12   530.35   530.57   530.80   531.02   531.25   531.47   531.70   531.92   532.18   236   532.38   532.60   532.83   533.05   533.28   533.50   533.73   533.95   534.18   534.41   237   534.63   534.86   535.08   535.31   535.53   535.76   535.98   536.21   536.44   536.66   238   536.89   537.11   537.34   537.56   537.79   538.02   538.24   538.47   538.69   538.92   239   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17    Tenths of a Line.	VIOLET	Section Land	ALC: NO SERVICE	2.3-2.7	Constant of the	1. JUNE 1945	ESTATE YOUR	10 Table 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		State of the same	
19 Inch.  228		150000000000000000000000000000000000000		C. U.C. 11 C	Transfer of the last	1,1000,1.0	S200 11 1 2 /	JUNE DE LA CONTRACTION DE LA C			
229   516.58   516.81   517.04   517.26   517.49   517.71   517.94   518.16   518.39   518.60   518.84   519.07   519.29   519.52   519.74   519.97   520.19   520.42   520.65   520.83   521.10   521.32   521.55   521.77   522.00   522.22   522.45   522.68   522.90   523.13   523.35   523.58   523.80   524.03   524.25   524.48   524.71   524.93   525.16   525.38   525.61   525.83   526.06   526.28   526.51   526.74   526.96   527.19   527.41   527.64   523.35   530.12   530.35   530.57   530.80   531.02   531.25   531.47   531.70   531.92   532.18   532.38   532.60   532.38   532.60   532.38   533.05   533.28   533.50   533.73   533.95   534.18   534.41   536.66   536.89   537.11   537.34   537.56   537.79   538.02   538.24   538.47   538.69   538.92   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17    Tenths of a Line.   7	Charles Table 1		012.00	120	012.10	012.00	010.20		alley or		
229         516.58         516.81         517.04         517.26         517.49         517.71         517.94         518.16         518.39         518.60           230         518.84         519.07         519.29         519.52         519.74         519.97         520.19         520.42         520.65         520.83           231         521.10         521.32         521.55         521.77         522.00         522.22         522.45         522.68         522.90         523.12           232         523.35         523.58         523.80         524.03         524.25         524.48         524.71         524.93         525.16         525.38           233         525.61         525.83         526.06         526.28         526.51         526.74         526.96         527.19         527.41         527.64           234         527.86         528.09         528.32         528.54         528.77         528.99         529.22         529.44         529.67         529.89           235         530.12         530.35         530.57         530.80         531.02         531.47         531.70         531.92         532.18           236         532.38         532.60         532.83	228	514.33	514.55	514.78	515.01	515.23	515.46	515.68	515.91	516.13	516.36
230         518.84         519.07         519.29         519.52         519.74         519.97         520.19         520.42         520.65         520.87           231         521.10         521.32         521.55         521.77         522.00         522.22         522.45         522.68         522.90         523.13           232         523.35         523.58         523.80         524.03         524.25         524.48         524.71         524.93         525.16         525.38           233         525.61         525.83         526.06         526.28         526.51         526.74         526.96         527.19         527.41         527.61           234         527.86         528.09         528.32         528.54         528.77         528.99         529.22         529.44         529.67         529.89           235         530.12         530.35         530.57         530.80         531.02         531.25         531.47         531.70         531.92         532.18           236         532.38         532.60         532.83         533.05         533.28         533.50         533.73         533.95         534.41         534.41         534.41         536.44         536.46         535.08 <td>THE RESERVE AND ADDRESS OF THE PARTY OF THE</td> <td>ACCURATION STATE</td> <td>College L. 7</td> <td>ALCOHOL: N</td> <td>STATE OF THE STATE OF THE STATE</td> <td>The second second second</td> <td></td> <td></td> <td>1000000</td> <td>A STATE OF THE PARTY OF</td> <td></td>	THE RESERVE AND ADDRESS OF THE PARTY OF THE	ACCURATION STATE	College L. 7	ALCOHOL: N	STATE OF THE STATE	The second second second			1000000	A STATE OF THE PARTY OF	
231    521.10    521.32    521.55    521.77    522.00    522.22    522.45    522.68    522.90    523.15    232    523.35    523.58    523.80    524.03    524.25    524.48    524.71    524.93    525.16    525.38    233    525.61    525.83    526.06    526.28    526.51    526.74    526.96    527.19    527.41    527.64    234    527.86    528.09    528.32    528.54    528.77    528.99    529.22    529.44    529.67    529.85    235    530.12    530.35    530.57    530.80    531.02    531.25    531.47    531.70    531.92    532.18    236    532.38    532.60    532.83    533.05    533.28    533.50    533.73    533.95    534.18    534.41    237    534.63    534.86    535.08    535.31    535.53    535.76    535.98    536.21    536.44    536.66    238    536.89    537.11    537.34    537.56    537.79    538.02    538.24    538.47    538.69    538.92    239    539.14    539.37    539.59    539.82    540.05    540.27    540.50    540.72    540.95    541.17     Tenths of a Line.   Tenths of a Line.	A CONTRACTOR OF THE PARTY OF TH	PERSONAL PROPERTY.	Market Street Street	Carrie Land	A COLUMN	0.0000000000000000000000000000000000000			7.53	20020180	
232         523.35         523.58         523.80         524.03         524.25         524.48         524.71         524.93         525.16         525.38           233         525.61         525.83         526.06         526.28         526.51         526.74         526.96         527.19         527.41         527.64           234         527.86         528.09         528.32         528.54         528.77         528.99         529.22         529.44         529.67         529.89           235         530.12         530.35         530.57         530.80         531.02         531.25         531.47         531.70         531.92         532.18           236         532.38         532.60         532.83         533.05         533.28         533.50         533.28         533.50         533.73         533.95         534.41         534.41         534.41         536.44         536.64           238         536.89         537.11         537.34         537.56         537.79         538.02         538.24         538.47         538.69         538.92           239         539.14         539.37         539.59         539.82         540.05         540.27         540.50         540.72         540.95 <td></td> <td></td> <td>1 1000</td> <td></td> <td>100</td> <td></td> <td></td> <td>100000</td> <td></td> <td></td> <td></td>			1 1000		100			100000			
233   525.61   525.83   526.06   526.28   526.51   526.74   526.96   527.19   527.41   527.64   234	0200000	医三角 医脂肪	CONFRAIR	Page 18 14 1 15	5253530303	116.45/10.	100000000000000000000000000000000000000		Session Va		
235   530.12   530.35   530.57   530.80   531.02   531.25   531.47   531.70   531.92   532.15   236   532.38   532.60   532.83   533.05   533.28   533.50   533.73   533.95   534.18   534.41   237   534.63   534.86   535.08   535.31   535.53   535.76   535.98   536.21   536.44   536.66   238   536.89   537.11   537.34   537.56   537.79   538.02   538.24   538.47   538.69   538.92   239   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17    Tenths of a Line.   1.   2.   3.   4.   5.   6.   7.   8.   9.	PRODUCTOR - 1	1.1000000000000000000000000000000000000	67-127-14-E-0	100000000000000000000000000000000000000	B-0415 B-757	5470101111	Call State of the		340 454	A Commission of	
235   530.12   530.35   530.57   530.80   531.02   531.25   531.47   531.70   531.92   532.15   236   532.38   532.60   532.83   533.05   533.28   533.50   533.73   533.95   534.18   534.41   237   534.63   534.86   535.08   535.31   535.53   535.76   535.98   536.21   536.44   536.66   238   536.89   537.11   537.34   537.56   537.79   538.02   538.24   538.47   538.69   538.92   239   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17    Tenths of a Line.   1.   2.   3.   4.   5.   6.   7.   8.   9.	204	FOR 00	*00.00	F00.00	F00 F1	W00 W5	<b>**********</b>	<b>*00.00</b>	<b>**20.4</b>	#00.0F	<b>200 CC</b>
236    532.38    532.60    532.83    533.05    533.28    533.50    533.73    533.95    534.18    534.41    237	DECEMBER OF STREET	CALL TO S	CONTRACT OF THE	10015		10.27 5.22 1 7			33357		
237   534.63   534.86   535.08   535.31   535.53   535.76   535.98   536.21   536.44   536.66   238   536.89   537.11   537.34   537.56   537.79   538.02   538.24   538.47   538.69   538.92   239   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17    Tenths of a Line.  0.   1.   2.   3.   4.   5.   6.   7.   8.   9.	BRIDGE IN CO.	2007/2007/2017	ACT OF STREET,	100000	MARKET TO		NAME OF TAXABLE PARTY.	1000	Carlot Land	- B12771 - 134 - 1	
238		Maria Laboratoria	A Charles Land			San					
239   539.14   539.37   539.59   539.82   540.05   540.27   540.50   540.72   540.95   541.17  Tenths of a Line.  0.   1.   2.   3.   4.   5.   6.   7.   8.   9.	11		1.0				Other Control of the Control		- LOC X-51		
Tenths of a Line.  0. 1. 2. 3. 4. 5. 6. 7. 8. 9.										X 22	
	2,5	300.14	300.01	300.00				040.00	040.72	010.00	041.11
0.00 0.22 0.45 0.69 0.00 1.12 1.25 1.50 1.00 0.00	0.	1.	2.	3.	4.	5	.   6	.	7.	8.	9.
	0.00	0.22	0.45	0.60	0.00		9 7	25 1	=0	1.00	2.02

1 Paris Line = 2.255829 Millimetres.

Paris or					Tenths o	f a Line.				
French Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
20 Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
240	541.40	541.62	541.85	542.08	542.30	542.53	542.75	542.98	543.20	543.4
241	543.65	543.88	544.11	544.33	544.56	544.78	545.01	545.23	545.46	545.6
242	545.91	546.14	546.36	546.59	546.81	547.04	547.26	547.49	547.72	547.9
243	548.17	548.39	548.62	548.54	549.07	549.29	549.52	549.75	549.97	550.2
244	550.42	550.65	550.87	551.10	551.32	551.55	551.78	552.00	552.23	552.4
245	552.68	552.90	553.13	553.35	553.58	553.81	554.03	554.26	554.48	554.7
246	554.93	555.16	555.39	555.61	555.84	556.06	556.29	556.51	556.74	556.9
247	557.19	557.42	557.64	557.87	558.09	558.32	558.54	558.77	558.99	559.5
248	559.45	559.67	559.90	560.12	560.35	560.57	560.80	561.02	561.25	561.4
249	561.70	561.93	562.15	562.38	562.60	562.83	563.05	563.28	563.51	563.
250	563.96	564.18	564.41	564.63	564.86	565.09	565.31	565.54	565.76	565.9
251	566.21	566.44	566.66	566.89	567.12	567.34	567.57	567.79	568.02	568.
21 Inches.							PASSEL I			
252	568.47	568.69	568.92	569.15	569.37	569.60	569.82	570.05	570.27	570.
253	570.72	570.95	571.18	571.40	571.63	571.85	572.08	572.30	572.53	572.
254	572.98	573.21	573.43	573.66	573.88	574.11	574.33	574.56	574.79	575.
255	575.24	575.46	575.69	575.91	576.14	576.36	576.59	576.82	577.04	577.
256	577.49	577.72	577.94	578.17	578.39	578.62	578.85	579.07	579.30	579.
257	579.75	579.97	580.20	580.42	580.65	580.88	581.10	581.33	581.55	581.
258	582.00	582.23	582.46	582.68	582.91	583.13	583.36	583.58	583.81	584.
259	584.26	584.49	584.71	584.94	585.16	585.39	585.61	585.84	586.06	586.
260	586.52	586.74	586.97	587.19	587.42	587.64	587.87	588.09	588.32	588.
261	588.77	589.00	589.22	589.45	589.67	589.90	590.12	590.35	590.58	590.
262	591.03	591.25	591.48	591.70	591.93	592.16	592.38	592.61	592.83	593.
263	593.28	593.51	593.73	593.96	594.19	594.41	594.64	594.86	595.09	595.
22 Inches.			400	1.00			1		1	1000
264	595.54	595.76	595.99	596.22	596.44	596.67	596.89	597.12	597.34	597.
265	597.79	598.02	598.25	598.47	598.70	598.92	599.15	599.37	599.60	599.
266	600.05	600.28	600.50	600.73	600.95	601.18	601.40	601.63	601.86	602.
267	602.31	602.53	602.76	602.98	603.21	603.43	603.66	603.89	604.11	604.
268	604.56	604.79	605.01	605.24	605.46	605.69	605.92	606.14	606.37	606.
269	606.82	607.04	607.27	607.49	607.72	607.95	608.17	608.40	608.62	608.
270	609.07	609.30	609.52	609.75	609.98	610.20	610.43	610.65	610.88	611.
271	611.33	611.56	611.78	612.01	612.23	612.46	612.68	612.91	613.13	613.
272	613.59	613.81	614.04	614.26	614.49	614.71	614.94	615.16	615.39	615.
273	615.84	616.07	616.29	616.52	616.74	616.97	617.19	617.42	617.65	617.
274	618.10	618.32	618.55	618.77	619.00	619.23	619.45	619.68	619.90	620.
275	620.35	620.58	620.80	621.03	621.26	621.48	621.71	621.93	622.16	622.
				Hundre	edths of a	Line.		realers (Estates		
0.	1.	2.	3.	4		5.	6.	7.	8.	9.
0.000	0.023	0.045	0.06	3 0.0	90 0.	113	0.135	0.158	0.180	0.20

1 Paris Line = 2.255829 Millimetres.

Paris or				N 1 1 1 1	Tenth	of a Line.				H CHIEF
French Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
23 Inches.	Millim.	Millim.	Millim.	Millim.	Millim	Millim.	Millim.	Millim.	Millim.	Millim.
276	622.61	622.83	623.06	623.29	623.5	623.74	623.96	624.19	624.41	624.64
277	624.86	625.09	625.32	625.54	625.7	625.99	626.22	626.44	626.67	626.89
278	627.12	627.35	627.57	627.80	628.0	2 628.25	628.47	628.70	628.93	629.15
279	629.38	629.60	629.83	630.05	630.2	630.50	630.73	630.96	631.18	631.41
280	631.63	631.86	632.08	632.31	632.5	632.76	632.99	633.21	633.44	633.66
281	633.89	634.11	634.34	634.56	634.7	635.02	635.24	635.47	635.69	635.92
282	636.14	636.37	636.59	636.82	637.0	637.27	637.50	637.72	637.95	638.17
283	638.40	638.63	638.85	639.08	639.3	639.53	639.75	639.98	640.20	640.43
284	640.66	640.88	641.11	641.33	641.5	6 641.78	642.01	642.23	643.46	642.69
285	642.91	643.14	643.36	643.59	643.8	1 644.04	644.26	644.49	644.72	644.94
286	645.17	645.39	645.62	645.84	646.0	7 646.30	646.52	646.75	646.97	647.20
287	647.42	647.65	647.87	648.10	648.3	3 648.55	648.78	649.00	649.23	649.45
4 Inches.	2475 3	balling i		9.507 \$ 9	a let	1 111	THE RES	E MISSI	1.5	7
288	649.68	649.90	650.13	650.36	650.5	8 650.81	651.03	651.26	651.48	651.71
289	651.93	652.16	652.39	652.61	652.8	4 653.06	653.29	653.51	653.74	653.96
290	654.19	654.42	654.64	654.87	655.0	9 655.32	655.54	655.77	656.00	656.22
291	656.45	656.67	656.90	657.12	657.3	5 657.57	657.80	658.03	658.25	658.48
292	658.70	658.93	659.15	659.38	659.6	0 659.83	660.06	660.28	660.51	660.73
293	660.96	661.18	661.41	661.63	661.8	6 662.09	662.31	662.54	662.76	662.99
294	663.21	663.44	663.66	663.89	664.1	2 664.34	664.57	664.79	665.02	665.24
295	665.47	665.70	665.92	666.15	666.3	7 666.60	666.82	667.05	667.27	667.50
296	667.73	667.95	668.18	668.40	668.6	3 668.83	669.08	669.30	669.53	669.76
297	669.98	670.21	670.43	670.66	670.5	8 671.11	671.33	671.56	671.79	672.01
298	672.24	672.46	672.69	672.91	673.1	4 673.36	673.59	673.82	674.04	674.27
299	674.49	674.72	674.94	675.17	675.4	0 675.65	675.85	676.07	676.30	676.52
25 Inches.				DISTRICT PART		A DESCRIPTION OF THE PERSON OF				- Series
300	676.75	676.97	677.20	677.43	677.6	5 677.89	678.10	678.33	678.55	678.78
301	679.00	679.23	679.46	679.68	679.9	1 680.13	680.36	680.58	680.81	681.08
302	681.26	681.49	681.71	681.94	682.1	6 682.39	682.61	682.84	683.07	683.29
303	683.52	683.74	683.97	684.19	684.4	2 684.6	684.87	685.10	685.32	685.58
304	685.77	686.00	686.22	686.45	686.6	7 686.9	687.13	687.35	687.58	687.80
305	688.03	688.25	688.48	688.70	688.9	3 689.1	689.38	689.61	689.83	690.06
306	690.28	690.51	690.73	690.96	691.1	9 691.4	691.64	691.86	692.09	692.3
307	692.54	692.77	692.99	693.22	693.4	4 693.6	693.89	694.12	694.34	694.57
308	694.80	695.02	695.25	695.47	695.7	0 695.9	696.15	696.37	696.60	696.8
309	697.05	697.28	697.50	697.73	697.9	5 698.18	698.40	698.63	698.86	699.08
310	699.31	699.53	699.76	699.98	700.2			700.89	701.11	701.34
311	701.56	701.79	702.01	702.24	702.4	7 702.6	702.92	703.14	703.37	703.59
				Hundr	edths of	a Line.				
0.	1.	2.	3.	4		5.	6.	7.	8.	9.
0.000	0.023	0.045	0.06	8 0.0	90	0.113	0.135	0.158	0.180	0.203

1 Paris Line = 2.255829 Millimetres.

Paris or				eira l	Tenths o	f a Line.	V			
French Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
26 Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
312	703.82	704.04	704.27	704.50	704.72	704.95	705.17	705.40	705.62	705.8
313	706.07	706.30	706.53	706.75	706.98	707.20	707.43	707.65	707.88	708.1
314	708.33	708.56	708.78	709.01	709.23	709.46	709.68	709.91	710.13	710.3
315	710.59	710.81	711.04	711.26	711.49	711.71	711.94	712.17	712.39	712.6
316	712.84	713.07	713.29	713.52	713.74	713.97	714.20	714.42	714.65	714.8
317	715.10	715.32	715.55	715.77	716.00	716.23	716.45	716.68	716.90	717.1
318	717.35	717.58	717.80	718.03	718.26	718.48	718.71	718.93	719.16	719.3
319	719.61	719.84	720.06	720.29	720.51	720.74	720.96	721.19	721.41	721.6
320	721.87	722.09	722.32	722.54	722.77	722.99	723.22	723.44	723.67	723.9
321	724.12	724.35	724.57	724.80	725.02	725.25	725.47	725.70	725.93	726.1
322	726.38	726.60	726.83	727.05	727.28	727.50	727.73	727.96	728.18	728.4
323	728.63	728.86	729.08	729.31	729.54	729.76	729.99	730.21	730.44	730.6
7 Inches.	120.00	120.00	.20.00	,				271000	1120	Yes
324	730.89	731.11	731.34	731.57	731.79	732.02	732.24	732.47	732.69	732.9
325	733.14	733.37	733.60	733.82	734.05	734.27	734.50	734.72	734.95	735.1
326	735.40	735.63	735.85	736.08	736.30	736.53	736.75	736.98	737.20	737.4
327	737.66	737.88	738.11	738.33	738.56	738.78	739.01	739.24	739.46	739.6
328	739.91	740.14	740.36	740.59	740.81	741.04	741.27	741.49	741.72	741.9
329	742.17	742.39	742.62	742.84	743.07	743.30	743.52	743.75	743.97	744.2
330	744.42	744.65	744.87	745.10	745.33	745.55	745.78	746.00	746.23	746.4
331	746.68	746.90	747.13	747.36	747.58	747.81	748.03	748.26	748.48	748.7
332	748.94	749.16	749.39	749.61	749.84	750.06	750.29	750.51	750.74	750.9
333	751.19	751.42	751.64	751.87	752.09	752.32	752.54	752.77	753.00	753.2
334	753.45	753.67	753.90	754.12	754.35	754.57	754.80	755.03	755.25	755.4
335	755.70	755.93		756.38	756.61	756.83	757.06	757.28	757.51	757.
Inches.	199.10	755.95	756.15	150.50	750.01	190.00	157.00	101.20	101.01	101.1
336	757.96	758.18	758.41	758.64	758.86	759.09	759.31	759.54	759.76	759.9
337	760.21	760.44	760.67	760.89	761.12	761.34	761.57	761.79	762.02	762.2
338	762.47	762.70	762.92	763.15	763.37	763.60	763.82	764.05	764.27	764.
339	764.73	764.95	765.18	765.40	765.63	765.85	766.08	766.31	766.53	766.
340	766.98	767.21	767.43	767.66	767.88	768.11	768.34	768.56	768.79	769.0
341	769.24	769.46	769.69	769.91	770.14	770.37	770.59	770.82	771.04	771.5
342	771.49	771.72	771.94	772.17	772.40	772.62	772.85	773.07	773.30	773.
343	773.75	773.97	774.20	774.43	774.65	774.88	775.10	775.33	775.55	775.
344	776.01	776.23	776.46	776.68	776.91	777.13	777.36	777.58	777.81	778.0
345	778.26	778.49	778.71	778.94	779.16	779.39	779.61	779.84	780.07	780.:
346	780.52	780.74	780.97	781.19	781.42	781.64	781.87	782.10	782.32	782.
347	782.77	783.00	783.22	783.45	783.67	783.90	784.13	784.35	784.58	784.8
348	785.03	785.25	785.48	785.71	785.93	786.16	786.38	786.61	786.83	787.
		•		Hundr	edths of a	Line.	15000100			
0.	1.	2.	3.	4		5.	6.	7.	8.	9.
0.000	0.023	0.045	0.06	8 0.0	90 0.	113	0.135	0.158	0.180	0.20

# VII. - VIII.

## COMPARISON

OF

# THE RUSSIAN BAROMETER

WITH

THE METRICAL AND THE OLD FRENCH BAROMETERS,

OR

## TABLES

FOR CONVERTING RUSSIAN HALF-LINES INTO MILLIMETRES, AND INTO FRENCH OR PARIS LINES;

GIVING THE VALUES CORRESPONDING TO EVERY HALF-LINE FROM 440 TO 540, OR FROM 22 TO 27 INCHES; AND TO EVERY TENTH, FROM 540 TO 610 HALF-LINES, OR FROM 27 TO 30.5 ENGLISH INCHES.

The second secon

#### RUSSIAN BAROMETER.

A LEGULAR system of Meteorological Observations has been established by order of the Russian government throughout the extensive regions placed under its sway, and a vast amount of observations made in Europe, in Asia, and in North America have already been published. The scale of the barometer employed in this system is divided in units, each of which is equal to one half of a Russian, or English decimal line, that is, 1 = 0.05 of an inch, 600 half-lines of the Russian Barometer being = 30 inches of the English Barometer.

The conversion of this scale, which is the English scale, slightly modified in its form, is easy. It suffices to divide the Russian heights by two, and to put back, by one figure, the decimal point, in order to have them converted into English inches and decimals. This transformation is so easy to effect, that a peculiar table for it would seem superfluous.

The normal temperature of the standard being the same as that of the English, that is, 13° Reaumur, or 62° Fahrenheit, the reduction of the Russian Barometer to the freezing point can be made by means of the table for reducing the English Barometers. But the attached thermometer being that of Reaumur, its indications must be first converted into degrees of Fahrenheit.

Tables VII. and VIII., which follow, have been computed in order to render more easy the comparison and the use of the Barometrical Observations recorded in the large collection, published annually by order of the Emperor of Russia, under the name of Annuaire Météorologique et Magnétique du Corps des Ingénieurs des Mines.

1 Russian Half-Line = 1.269977 Millimetres.

						977 Millim				
Russian				Uni	ts or Russi	an Half-Li	nes.			
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
22 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
440	558.79	560.06	561.33	562.60	563.87	565.14	566.41	567.68	568.95	570.2
450	571.49	572.76	574.03	575.30	576.57	577.84	579.11	580.38	581.65	582.9
460	584.19	585.46	586.73	588.00	589.27	590.54	591.81	593.08	594.35	595.6
470	596.89	598.16	599.43	600.70	601.97	603.24	604.51	605.78	607.05	608.3
480	609.59	610.86	612.13	613.40	614.67	615.94	617.21	618.48	619.75	621.0
24.5 In. 490	622.29	623.56	624.83	626.10	627.37	628.64	629.91	631.18	632.45	633.7
500	634.99	636.26	637.53	638.80	640.07	641.34	642.61	643.88	645.15	646.4
510	647,69	648.96	650.23	651.50	652.77	654.04	655.31	656.58	657.85	659.1
520	660.39	661.66	662.93	664.20	665.47	666.74	668.01	669.28	670.55	671.8
530	673.09	674.36	675.63		678.17			681.98	683.25	684.5
000	010.05	0,100	0.0.00	0.0.00	0.0.11		000111	002100	000.20	1 00 110
Russian					Ten	ths.		The same		
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
27 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
540	685.79	685.91	686.04	686.17	686.30	686.42	686.55	686.68	686.80	686.9
541	687.06	687.18	687.31	687.44	687.57	687.69	687.82	687.95	688.07	688.2
542	688.33	688.45	688.58	688.71	688.84	688.96	689.09	689.22	689.34	689.4
543	689.60	689.72	689.85	689.98	690.11	690.23	690.36	690.49	690.61	690.7
544	690.87	690.99	691.12	691.25	691.38	691.50	691.63	691.76	691.88	692.0
545	692.14	692.26	692.39	692.52	692.65	692.77	692.90	693.03	693.15	693.2
546	693.41	693.53	693.66	693.79	693.91	694.04	694.17	694.30	694:42	694.5
547	694.68	694.80	694.93	695.06	695.19	695.31	695.44	695.57	695.69	695.8
548	695.95	696.07	696.20	696.33	696.46	696.58	696.71	696.84	696.96	697.0
549	697.22	697.34	697.47	697.60	697.73	697.85	697.98	698.11	698.23	698.3
27.5 In.	600 10	C00 C1	C00 F1	600 0m	con 00	600 10	600.05	699.38	699.50	699.6
550	698.49	698.61	698.74	698.87	699.00	699.12	699.25			700.9
551	699.76	699.88	700.01	700.14	700.27	700.39	700.52	700.65	700.77	Control of
552	701.03	701.15	701.28	701.41	701.54	701.66	701.79	701.92	702.04	702.1
553 554	702.30	702.42	702.55	702.68 703.95	702.81	702.93	703.06	703.19	704.58	704.7
004			100.02		100	ers another	101.00	I warmen	and Late	A CONTRACT
555	704.84	704.96	705.09	705.22	705.35	705.47	705.60	705.73	705.85	705.9
556	706.11	706.23	706.36	706.49	706.62	706.74	706.87	707.00	707.12	707.2
557	707.38	707.50	707.63	707.76	707.89	708.01	708.14	708.27	708.39	708.5
558	708.65	708.77	708.90	709.03	709.16	709.28	709.41	709.54	709.66	709.7
559 28 Inch.	709.92	710.14	710.27	710.40	710.53	710.65	710.78	710.81	710.93	711.0
560	711.19	711.31	711.44	711.57	711.70	711.82	711.95	712.08	712.20	712.3
561	712.46	712.58	712.71	712.84	712.97	713.09	713.22	713.35	713.47	713.6
562	713.73	713.85	713.98	714.11	714.24	714.36	714.49	714.62	714.74	714.8
563	715.00	715.12	715.25	715.38	715.51	715.63	715.76	715.89	716.01	716.1
564	716.27	716.39	716.52	716.65	716.78	716.90	717.03	717.16	717.28	717.4
565	717.54	717.66	717.79	717.92	718.04	718.17	718.30	718.43	718.55	718.6
566	718.81	718.93	719.06	719.19	719.31	719.44	719.57	719.70	719.82	719.9
567	720.08	720.20	720.33	720.46	720.58	720.71	720.84	720.97	721.09	721.2
568	721.35	721.47	721.60	721.73	721.85	721.98	722.11	722.24	722.36	722.4

1 Russian Half-Line = 1.269977 Millimetre.

Russian			Winds		Ten	ths.				<b>W</b>
Half-Lines.	0.	1.	2.	3.	.4.	5.	6.	7.	8.	9.
28.5 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
570	723.89	724.01	724.14	724.27	724.39	724.52	724.65	724.78	724.90	725.03
571	725.16	725.28	725.41	725.54	725.66	725.79	725.92	726.05	726.17	726.30
572	726.43	726.55	726.68	726.81	726.93	727.06	727.19	727.32	727.44	727.57
573	727.70	727.82	7.27.95	728.08	728.20	728.33	728.46	728.59	728.71	728.84
574	728.97	729.08	729.21	729.34	729.46	729.59	729.73	729.85	729.97	730.11
575	730.24	730.36	730.49	730.62	730.74	730.87	731.00	731.13	731.25	731.38
576	731.51	731.63	731.76	731.89	732.01	732.14	732.27	732.40	732.52	732.65
577	732.78	732.90	733.03	733.16	733.28	733.41	733.54	733.67	733.79	733.92
578	734.05	734.17	734.30	734.43	734.55	734.68	734.81	734.94	735.06	735.19
579 29 Inch.	735.32	735.44	735.57	735.70	735.82	735.95	736.08	736.21	736.33	736.46
580	736.59	736.71	736.84	736.97	737.09	737.22	737.35	737.48	737.60	737.73
581	737.86	737.98	738.11	738.24	738.36	738.49	738.62	738.75	738.87	739.00
582	739.13	739.25	739.38	739.51	739.63	739.76	739.89	740.02	740.14	740.27
583	740.40	740.52	740.65	740.78	740.90	741.03	741.16	741.29	741.41	741.54
584	741.67	741.79	741.92	742.05	742.17	742.30	742.43	742.56	742.68	742.81
585	742.94	743.06	743.19	743.32	743.44	743.57	743.70	743.83	743.95	744.08
586	744.21	744.33	744.46	744.59	744.71	744.84	744.97	745.10	745.22	745.35
587	745.48	745.60	745.73	745.86	745.98	746.11	746.24	746.37	746.49	746.62
588	746.75	746.87	747.00	747.13	747.25	747.38	747.51	747.64	747.76	747.89
589	748.02	748.14	748.27	748.40	748.52	748.65	748.78	748.91	749.03	749.16
29.5 In.	140.02	140.14	140.21	140.40	140.02	140.00	1 40.10	740.01	145.00	145.10
590	749.29	749.41	749.54	749.67	749.79	749.92	750.05	750.18	750.30	750.43
591	750.56	750.68	750.81	750.94	751.06	751.19	751.32	751.45	751.57	751.70
592	751.83	751.95	752.08	752.21	752.33	752.46	752.59	752.72	752.84	752.97
593	753.10	753.22	753.35	753.48	753.60	753.73	753.86	753.99	754.11	754.24
594	754.37	754.49	754.62	754.75	754.87	755.00	755.13	755.26	755.38	755.51
595	755.64	755.76	755.89	756.02	756.14	756.27	756.40	756.53	756.65	756.78
596	756.91	757.03	757.16	757.29	757.41	757.54	757.67	757.80	757.92	758.05
597	758.18	758.30	758.43	758.56	758.68	758.81	758.94	759.07	759.19	759.32
598	759.45	759.57	759.70	759.84	759.96	760.09	760.21	760.34	760.46	760.59
599 30 Inch.	760.72	760.84	760.97	761.10	761.22	761.35	761.48	761.61	761.73	761.86
600	761.99	762.11	762.24	762.37	762.49	762.62	762.75	762.88	763.00	763.13
601	763.26	763.38	763.51	763.64	763.76	763.89	764.02	764.15	764.27	764.40
602	764.53	764.65	764.78	764.91	765.03	765.16	765.29	765.42	765.54	765.67
603	765.80	765.92	766.05	766.18	766.30	766.43	766.56	766.69	766.81	766.95
604	767.07	767.19	767.32	767.45	767.57	767.70	767.83	767.96	768.08	768.21
605	768.34	768.46	768.59	768.72	768.84	768.97	769.10	769.23	769.35	769.48
606	769.61	769.73	769.85	769.99	770.11	770.24	770.37	770.50	770.62	770.75
607	770.88	771.00	771.13	771.26	771.38	771.51	771.64	771.77	771.89	772.02
608	772.15	772.27	772.40	772.53	772.65	772.78	772.91	773.03	773.16	773.29
609	773.42	773.54	773.67	773.80	773.92	774.05	774.18	774.30	774.43	774.56
MAREL	San San	reither :		Н	indredths.	page 1	TOTAL S	Evoy II		
0.000	0.013	0.025	0.038	0.05	1 0.0	63 0.	076	.089	0.102	0.114

1 Russian Half-Line = 0.562976 Paris Line.

Russian					Units or R	ussian Half	-Lines.			
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
22 Inch.	Par. line.	Par. line.	Par. line.	Par. line.	Par line.	Par line.	Par. line.	Par. line	Par line.	Par. line.
440	247.71	248.27	248.84	249.40	249.96	250.52	251.09	251.65	252.21	252.78
450	253.34	253.90	254.47	255.03	255.59	256.15	256.72	257.28	257.84	258.41
460	258.97	259.53	260.09	260.66	261.22	261.78	262.35	262.91	263.47	264.04
470	264.60	265.16	265.72	266.29	266.85	267.41	267.98	268.54	269.10	269.67
480	270.23	270.79	271.35	271.92	272.48	273.04	273.61	274.17	274.73	275.30
24.5 In.		242 12	020 00	000 55	000 11	000 00	070 04	0=0.00	900 90	000.00
490	275.86	276.42	276.98	277.55	278.11	278.67 284.30	279.24	279.80 285.43	280.36	280.93 286.55
500	281.49	282.05	282.61	283.18 288.81	283.74	289.93	284.87		285.99	- 77 July 200
510	287.12	287.68	288.24	294.44	295.00	L'ENGLIS DE	The second second	291.06 296.69	291.62	292.18 297.81
520	292.75	293.31	293.87	300.07	0	295.56	296.13 301.76		297.25	303.44
530	298.38	298.94	299.50	300.07	300.03	301.19	301.70	302.32	302.88	303.44
Russian			arita j		Ten	iths.	-	1.00	15,077	T. Wale
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
27 Inch.	Par. line.	Par. line.	Par. line.	Par. line.						
540	304.01	304.06	304.12	304.18	304.23	304.29	304.34	304.40	304.46	304.51
541	304.57	304.63	304.68	304.74	304.80	304.85	304.91	304.96	305.02	305.08
542	305.13	305.19	305.25	305.30	305.36	305.41	305.47	305.53	305.58	305.64
543	305.70	305.75	305.81	305.86	305.92	305.98	306.03	306.09	306.15	306.20
544	306.26	306.32	306.37	306.43	306.48	306.54	306.60	306.65	306.71	306.77
545	306.82	306.88	306.93	306.99	307.05	307.10	307.16	307.22	307.27	307.33
546	307.38	307.44	307.50	307.55	307.61	307.67	307.72	307.78	307.84	307.89
547	307.95	308.00	308.06	308.12	308.17	308.23	308.29	308.34	308.40	308.45
548	308.51	308.57	308.62	308.68	308.74	308.79	308.85	308.90	308.96	309.02
549 27.5 In.	309.07	309.13	309.19	309.24	309.30	309.36	309.41	309.47	309.52	309.58
550	309.64	309.69	309.75	309.81	309.86	309.92	309.97	310.03	310.09	310.14
551	310.20	310.26	310.31	310.37	310.42	310.48	310.54	310.59	310.65	310.71
552	310.76	310.82	310.88	310.93	310.99	311.04	311.10	311.16	311.21	311.27
553	311.33	311.38	311.44	311.49	311.55	311.61	311.66	311.72	311.78	311.83
554	311.89	311.95	312.00	312.06	312.11	312.17	312.23	312.28	312.34	312.40
555	312.45	312.51	312.56	312.62	312.68	312.73	312.79	312.85	312.90	312.96
556	313.01	313.07	313.13	313.18	313.24	313.30	313.35	313.41	313.47	313.52
557	313.56	313.63	313.69	313.75	313.80	313.86	313.92	313.97	314.03	314.08
558	314.14	314.20	314.25	314.31	314.37	314.42	314.48	314.53	314.59	314.65
559	314.70	314.76	314.82	314.87	314.93	314.99	315.04	315.10	315.15	315.21
28 Inch.	215.05	015 00	915 90	275 4	915 40	015 55	915 60	215 66	315.72	315.77
560	315.27	315.32	315.38	315.44	315.49	315.55	315.60	315.66 316.22	316.28	316.34
561	315.83	315.89	315.94	316.00	316.05	316.11	316.17	316.22	316.28	316.90
562 563	316.39	316.45	316.51	316.56	316.62	316.67	316.73	317.35	317.41	317.46
564	316.96 317.52	317.01 317.57	317.07 317.63	317.12 317.69	317.18 317.74	317.24 317.80	317.29 317.86	317.91	317.41	318.03
565	318.08	318.14	318.19	318.25	318.31	318.36	318.42	318.48	318.53	318.59
566	318.64	318.70	318.76	318.81	318.87	318.93	318.98	319.04	319.09	319.15
567	319.21	319.26	319.32	319.38	319.43	319.49	319.55	319.60	319.66	319.71
568	319.77	319.83	319.88	319.94	320.00	320.05	320.11	320.16	320.22	320.28
569	320.33	320.39	320.45	320.50	320.56	320.61	320.67	320.73	320.78	320.84

#### COMPARISON OF THE RUSSIAN AND OLD FRENCH BAROMETERS.

1 Russian Half-Line = 0.562976 Paris Line.

Russian					Ten	ths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
28.5 Inch.	Par. line.									
570	320.90	320.95	321.01	321.07	321.12	321.18	321.23	321.29	321.35	321.40
571	321.46	321.52	321.57	321.63	321.68	321.74	321.80	321.85	321.91	321.97
572	322.02	322.08	322.13	322.19	322.25	322.30	322.36	322.42	322.47	322.53
573	322.59	322.64	322.70	322.75	322.81	322.87	322.92	322.98	323.04	323.09
574	323.15	323.20	323.26	323.32	323.37	323.43	323.49	323.54	323.60	323.65
575	323.71	323.77	323.82	323.88	323.94	323.99	324.05	324.11	324.16	324.22
576	324.27	324.33	324.39	324.44	324.50	324.56	324.61	324.67	324.72	324.78
577	324.84	324.89	324.95	325.01	325.06	325.12	325.17	325.23	325.29	325.34
578	325.40	325.46	325.51	325.57	325.63	325.68	325.74	325.79	325.85	325.91
579 29 Inch.	325.96	326.02	326.08	326.13	326.19	326.24	326.30	326.36	326.41	326.47
580	326.53	326.58	326.64	326.69	326.75	326.81	326.86	326.92	326.98	327.03
581	327.09	327.15	327.20	327.26	327.31	327.37	327.43	327.48	327.54	327.60
582	327.65	327.71	327.76	327.82	327.88	327.93	327.99	328.05	328.10	328.16
583	328.22	328.27	328.33	328.38	328.44	328.50	328.55	328.61	328.67	328.72
584	328.78	328.83	328.89	328.95	329.00	329.06	329.12	329.17	329.23	329.28
585	329.34	329.40	329.45	329.51	329.57	329.62	329.68	329.74	329.79	329.85
586	329.90	329.96	330.02	330.07	330.13	330.19	330.24	330.30	330.35	330.41
587	330.47	330.52	330.58	330.64	330.69	330.75	330.80	330.86	330.92	330.97
588	331.03	331.09	331.14	331.20	331.26	331.31	331.37	331.42	331.48	331.54
589	331.59	331.65	331.71	331.76	331.82	331.87	331.93	331.99	332.04	332.10
29.5 In.					100					
590	332.16	332.21	332.27	332.32	332.38	332.44	332.49	332.55	332.61	332.66
591	332.72	332.78	332.83	332.89	332.94	333.00	333.06	333.11	333.17	333.23
592	333.28	333.34	333.39	333.45	333.51	333.56	333.62	333.68	333.73	333.79
593	333.84	333.90	333.96	334.01	334.07	334.13	334.18	334.24	334.30	334.35
594	334.41	334.46	334.52	334.58	334.63	334.69	334.75	334.80	334.86	334.91
595	334.97	335.03	335.08	335.14	335.20	335.25	335.31	335.36	335.42	335.48
596	335.53	335.59	335.65	335.70	335.76	335.82	335.87	335.93	335.98	336.04
597	336.10	336.15	336.21	336.27	336.32	336.38	336.43	336.49	336.55	336.60
598	336.66	336.72	336.77	336.83	336.88	336.94	337.00	337.05	337.11	337.17
599	337.22	337.28	337.34	337.39	337.45	337.50	337.56	337.62	337.67	337.73
30 Inch.										,
600	337.79	337.84	337.90	337.95	338.01	338.07	338.12	338.18	338.24	338.29
601	338.35	338.40	338.46	338.52	338.57	338.63	338.69	338.74	338.80	338.86
602	338.91	338.97	339.02	339.08	339.14	339.19	339.25	339.31	339.36	339.42
603	339.47	339.53	339.59	339.64	339.70	339.76	339.81	339.87	339.92	339.98
604	340.04	340.09	340.15	340.21	340.26	340.32	340.38	340.43	340.49	340.54
605	340.60	340.66	340.71	340.77	340.83	340.88	340.94	340.99	341.05	341.11
606	341.16	341.22	341.28	341.33	341.39	341.44	341.50	341.56	341.61	341.67
607	341.73	341.78	341.84	341.90	341.95	342.01	342.06	342.12	342.18	342.23
608	342.29	342.35	342.40	342.46	342.51	342.57	342.63	342.68	342.74	342.80
609	342.85	342.91	342.96	343.02	343.08	343.13	343.19	343.25	343.30	343.36
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IX.-XVI.

## COMPARISON

OF

# BAROMETRICAL DIFFERENCES

EXPRESSED IN MEASURES OF DIFFERENT SCALES,

OR

## TABLES

FOR CONVERTING ENGLIST/ INCHES, MILLIMETRES, PARIS LINES, AND RUSSIAN HALF-LINES INTO EACH OTHER.

Control of the second of the s 117.90 100 10 AND AND THE PROPERTY OF THE PR

#### IX. CONVERSION OF ENGLISH INCHES INTO MILLIMETRES.

1 English Inch = 25.39954 Millimetres.

English				В	undredths	of an Inc	h.			
Inches and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0.0	0.000	0.254	0.508	0.762	1.016	1.270	1.524	1.778	2.032	2.286
0.1	2.540	2.794	3.048	3.302	3.556	3.810	4.064	4.318	4.572	4.826
0.2	5.080	5.334	5.588	5.842	6.096	6.350	6.604	6.858	7.112	7,366
0.3	7.620	7.874	8.128	8.382	8.636	8.890	9.144	9.398	9.652	9.906
0.4	10.160	10.414	10.668	10.922	11.176	11.430	11.684	11.938	12.192	12.446
0.5	12.700	12.954	13.208	13.462	13.716	13.970	14.224	14.478	14.732	14.980
0.6	15.240	15.494	15.748	16.002	16.256	16.510	16.764	17.018	17.272	17.520
0.7	17.780	18.034	18.288	18.542	18.796	19.050	19.304	19.558	19.812	20.06
0.8	20.320	20.574	20.828	21.082	21.336	21.590	21.844	22.098	22.352	22.60
0.9	22.860	23.114	23.368	23.622	23.876	24.130	24.384	24.638	24.892	25.14
1.0	25.400	25.654	25.908	26.162	26.416	26.670	26.924	27.178	27.432	27.68
1.1	27.939	28.193	28.447	28.701	28.955	29.209	29.463	29.717	29.971	30.22
1.2	30.479	30.733	30.987	31.241	31.495	31.749	32.003	32.257	32.511	32.76
1.3	33.019	33.273	33.527	33.781	34.035	34.289	34.543	34.797	35.051	35.30
1.4	35.559	35.813	36.067	36.321	36.575	36.829	37.083	37.337	37.591	37.84
1.5	38.099	38.353	38.607	38.861	39.115	39.369	39.623	39.877	40.131	40.38
1.6	40.639	40.893	41.147	41.401	41.655	41.909	42.163	42.417	42.671	42.92
1.7	43.179	43.433	43.687	43.941	44.195	44.449	44.703	44.957	45.211	45.46
1.8	45.719	45.973	46.227	46.481	46.735	46.989	47.243	47.497	47.751	48.00

#### K. CONVERSION OF ENGLISH INCHES INTO FRENCH OR PARIS LINES. 1 English Inch = 11.259515 Paris Lines.

English		13-10		I	Iundredths	of an Inc	h.			
Inches and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
THE TELL	Par. line.									
0.0	0.000	0.113	0.225	0.338	0.450	0.563	0.676	0.788	0.901	1.013
0.1	1.126	1.239	1.351	1.464	1.576	1.689	1.802	1.914	2.027	2.139
0.2	2.252	2.364	2.477	2.590	2.702	2.815	2.927	3.040	3.153	3.265
0.3	3.378	3.490	3.603	3.716	3.828	3.941	4.053	4.166	4.279	4.391
0.4	4.504	4.616	4.729	4.842	4.954	5.067	5.179	5.292	5.405	5.517
0.5	5.630	5.742	5.855	5.968	6.080	6.193	6.305	6.418	6.531	6.643
0.6	6.756	6.868	6.981	7.093	7.206	7.319	7.431	7.544	7.656	7.769
0.7	7.882	7.994	8.107	8.219	8.332	8.445	8.557	8.670	8.782	8.895
0.8	9.008	9.120	9.233	9.345	9.458	9.571	9.683	9.796	9.908	10.021
0.9	10.134	10.246	10.359	10.471	10.584	10.697	10.809	10.922	.11.034	11.147
1.0	11.260	11.372	11.485	11.597	11.710	11.822	11.935	12.048	12.160	12.273
1.1	12.385	12.498	12.611	12.723	12.836	12.948	13.061	13.174	13.286	13.399
1.2	13.511	13.624	13.737	13.849	13.962	14.074	14.187	14.300	14.412	14.525
1.3	14.637	14.750	14.863	14.975	15.088	15.200	15.313	15.426	15.538	15.651
1.4	15.763	15.876	15.988	16.101	16.214	16.326	16.439	16.551	16.664	16.777
1.5	16.889	17.002	17.114	17.227	17.340	17.452	17.565	17.677	17.790	17.903
1.6	18.015	18.128	18.240	18.353	18.466	18.578	18.691	18.803	18.916	19.029
1.7	19.141	19.254	19.366	19.479	19.592	19.704	19.817	19.929	20.042	20.155
1.8	20.267	20.380	20.492	20.605	20.717	20.830	20.943	21.055	21.168	21.280

## XI. CONVERSION OF MILLIMETRES INTO ENGLISH INCHES.

1 Metre = 39.37079 English Inches.

Millime-					CHUIS OF S	Millimetr				MARIE
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In. 0.0000	Eng. In. 0.0039	Eng. In. 0.0079	Eng. In. 0.0118	Eng. In. 0.0157	Eng. In. 0.0197	Eng. In. 0.0236	Eng. In. 0.0276	Eng. In. 0.0315	Eng. I
0	0.0394	0.0033	0.0472	0.0512	0.0551	0.0591	0.0630	0.0669	0.0709	0.074
1 2	0.0334	0.0433	0.0366	0.0906	0.0945	0.0984	0.1024	0.1063	0.1102	0.114
3	0.1181	0.0827	0.1260	0.1299	0.1339	0.1378	0.1417	0.1457	0.1496	0.153
4	0.1151	0.1220	0.1200	0.1693	0.1732	0.1772	0.1811	0.1850	0.1890	0.192
5	0.1969	0.2008	0.2047	0.2087	0.2126	0.2165	0.2205	0.2244	0.2283	0.232
6	0.2362	0.2402	0.2441	0.2480	0.2520	0.2559	0.2598	0.2638	0.2677	0,271
7	0.2756	0.2795	0.2835	0.2874	0.2913	0.2953	0.2992	0.3032	0.3071	0.311
8	0.3150	0.3189	0.3228	0.3268	0.3307	0.3347	0,3386	0.3425	0.3465	0.350
9	0.3543	0.3583	0.3622	0.3661	0.3701	0.3740	0.3780	0.3819	0.3858	0.389
10	0.3937	0.3976	0.4016	0.4055	0.4095	0.4134	0.4173	0.4213	0.4252	0.429
11	0.4331	0.4370	0.4410	0.4449 0.4843	0.4488	0.4528	0.4567	0.4606	0.4646	0.468
12	0.4724	0.4764		0.4045	0.4882	0.4921 0.5315	0.4961 0.5354	0.5394	0.5039	0.507
13 14	0.5118 0.5512	0.5551	0.5197 0.5591	0.5630	0.5669	0.5709	0.5748	0.5788	0.5433	0.586
15	0.5906	0.5945	0.5984	0.6024	0.6063	0.6102	0.6142	0.6181	0.6221	0.626
16	0.6299	0.6339	0.6378	0.6417	0.6457	0.6496	0.6536	0.6575	0.6614	0.665
17	0.6693	0.6732	0.6772	0.6811	0.6851	0.6890	0.6929	0.6969	0.7008	0.704
18	0.7087	0.7126	0.7165	0.7205	0.7244	0.7284	0.7323	0.7362	0.7402	0.744
19	0.7480	0.7520	0.7559	0.7599	0.7638	0.7677	0.7717	0.7756	0.7795	0.783
20	0.7874	0.7914	0.7953	0.7992	0.8032	0.8071	0.8110	0.8150	0.8189	0.822
21	0.8268	0.8307	0.8347	0.8386	0.8425	0.8465	0.8504	0.8543	0.8583	0.862
22	0.8662	0.8701	0.8740	0.8780	0.8819	0.8858	0.8898	0.8937	0.8977	0.901
23 24	0.9055	0.9095	0.9134 0.9528	0.9173	0.9213	0.9252	0.9292 0.9685	0.9331	0.9370	0.941
		The state of the			3150		William !	15.0	elu, in	4.0
25	0.9843	0.9882	0.9921	0.9961	1.0000	1.0040	1.0079	1.0118	1.0158	1.019
26	1.0236	1.0276	1.0315	1.0355	1.0394	1.0433	1.0473	1.0512	1.0551	1.059
27 28	1.0630	1.0669	1.0709	1.0748 1.1142	1.0788	1.0827	1.0866 1.1260	1.0906 1.1299	1.0945	1.098
29	1.1024	1.1063 1.1457	1.1103 1.1496	1.1142	1.1181	1.1614	1.1250	1.1693	1.1339 1.1732	1.13
30	1.1811	1.1851	1.1890	1.1929	1.1969	1.2008	1.2047	1.2087	1.2126	1.216
31	1.2205	1.2244	1.2284	1.2323	1.2362	1.2402	1.2441	1.2481	1.2520	1.255
32	1.2599	1.2638	1.2677	1.2717	1.2756	1.2796	1.2835	1.2874	1.2914	1.29
33	1.2992	1.3032	1.3071	1.3110	1.3150	1.3189	1.3229	1.3268	1.3307	1.334
34	1.3386	1.3425	1.3465	1.3504	1.3544	1.3583	1.3622	1.3662	1.3701	1.37
35	1.3780	1.3819	1.3859	1.3898	1.3937	1.3977	1.4016	1.4055	1.4095	1.413
36	1.4173	1.4213	1.4252	1.4292	1.4331	1.4370	1.4410	1.4449	1.4488	1.452
37	1.4567	1.4607	1.4646	1.4685	1.4725	1.4764	1.4803	1.4843	1.4882	1.492
38	1.4961	1.5000	1.5040	1.5079	1.5118	1.5158	1.5197	1.5236	1.5276	1.531
39 40	1.5355 1.5748	1.5394 1.5788	1.5433	1.5473 1.5866	1.5512	1.5551	1.5591	1.5630 1.6024	1.5670 1.6063	1.570
2000					Prince.	MANAGE TO SE	Control of the	SERVICE PARTY	ASTABLE ST	133017

#### XII. CONVERSION OF MILLIMETRES INTO FRENCH OR PARIS LINES.

1 Millimetre = 0.443296 Paris Line.

Millime-	34/	Tenths of a Millimetre.												
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
	Par. line.	Par. line.		Par. line.	The second second	Par. line.	Par. line.	Par. line.	1	Par. lin				
0	0.000	0.044	0.089	0.133	0.177	0.222	0.266	0.310	0.355	0.39				
1	0.443	0.488	0.532	0.576	0.621	0.665	0.709	0.754	0.798	0.84				
2	0.887	0.931	0.975	1.020	1.061	1.108	1.153		1.241	1.28				
3	1.330	1.374	1.419 1.862	1.463 1.906	1.507 1.950	1.552 1.995	1.596 2.039	1.640 2.083	1.685 2.128	1.72 2.17				
	2.216	2.261	2.305	2.349	2.394	2.438	2.482	2.527	2.571	2.61				
5	2.660	2.704	2.748	2.793	2.837	2.881	2.926	2.970	3.014	3.05				
7	3.103	3.147	3.192	3.236	3.280	3.325	3.369	3.413	3.458	3.50				
8	3.546	3.591	3.635	3.679	3.724	3.768	3.812	3.857	3.901	3.94				
9	3.990	4.034	4.078	4.123	4.167	4.211	4.256	4.300	4.344	4.38				
10	4.433	4.477	4.522	4.566	4.610	4.655	4.699	4.743	4.788	4.83				
11	4.876	4.921	4.965	5.009	5.054	5.098	5.142	5.187	5.231	5.27				
12	5.320	5.364	5.408	5.453	5.497	5.541	5.586	5.630	5.674	5.71				
13	5.763	5.807	5.851	5.896	5.940	5.984	6.029	6.073	6.117	6.16				
14	6.206	6.250	6.295	6.339	6.383	6.428	6.472	6.516	6.561	6.60				
15	6.649	6.694	6.738	6.782	6.827	6.871	6.915	6.960	7.004	7.04				
16	7.093	7.137	7.181	7.226	7.270	7.314	7.359	7.403	7.447	7.49				
17	7.536	7.580	7.625	7.669	7.713	7.758	7.802	7.846	7.891	7.93				
18	7.979	8.024	8.068	8.112	8.157	8.201	8.245	8.290	8.334	8.37				
19	8.423	8.467	8.511	8.556	8.600	8.644	8.689	8.733	8.777	8.82				
20	8.866	8.910	8.955	8.999	9.043	9.088	9.132	9.176	9.221	9.26				
21	9.309	9.354	9.398	9.442	9.487	9.531	9.575	9.620	9.664	9.70				
22	9.753	9.797	9.841	9.886	9.930	9.974	10.018	10.063	10.107	10.15				
23	10.196	10.240	10.284	10.329	10.373	10.417	10.462	10.506	10.550	10.59				
24	10.639	10.683	10.728	10.772	10.816	10.861	10.905	10.949	10.994	11.03				
25	11.082	11.127	11.171	11.215	11.260	11.304	11.348	11.393	11.437	11.48				
26	11.526	11.570	11.614	11.659	11.703	11.747	11.792	11.836	11.880	11.92				
27	11.969	12.013	12.058	12.102	12.146	12.191	12.235	12.279	12.324	12.36				
28	12.412	12.457	12.501	12.545	12.590	12.634	12.678	12.723	12.767	12.81				
29	12.856	12.900	12.944	12.989	13.033	13.077	13.122	13.166	13.210	13.25				
30	13.299	13.343	13.388	13.432	13.476	13.521	13.565	13.609	13.654	13.69				
31	13.742	13.786	13.831	13.875	13.919	13.964	14.008	14.052	14.097	14.14				
32	14.185	14.230	14.274	14.318	14.363	14.407	14.451	14.496	14.540	14.58				
33	14.629	14.673	14.717	14.762	14.806	14.850	14.895	14.939	14.983	15.02				
34	15.072	15.116	15.161	15.205	15.249	15.294	15.338	15.382	15.427	15.47				
35	15.515	15.560	15.604	15.648	15.693	15.737	15.781	15.826	15.870	15.91				
36	15.959	16.003	16.047	16.092	16.136	16.180	16.225	16.269	16.313	16.35				
37	16.402	16.446	16.491	16.535	16.579	16.624	16.668	16.712	16.757	16.80				
38	16.845	16.890	16.934	16.978	17.023	17.067	17.111	17.156	17.200	17.24				
39	17.289	17.333	17.377	17.422	17.466	17.510	17.555	17.599	17.643	17.688				
40	17.732	17.776	17.820	17.865	17.909	17.953	17.998	18.042	18.086	18.13				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

1 Paris Line = 2.255829 Millimetres.

Paris					Tenths o	f a Line.				
Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.000	0.226	0.451	0.677	0.902	1.128	1.353	1.579	1.805	2.030
1	2.256	2.481	2.707	2.933	3.158	3.384	3.609	3.835	4.060	4.286
2	4.512	4.737	4.963	5.188	5.414	5.640	5.865	6.091	6.316	6.542
3	6.767	6.993	7.219	7.444	7.670	7.895	8.121	8.347	8.572	8.798
4	9.023	9.249	9.474	9.700	9.926	10.151	10.377	10.602	10.828	11.054
5	11.279	11.505	11.730	11.956	12.181	12.407	12.633	12.858	13.084	13.309
						1914				
6	13.535	13.761	13.98€	14.212	14.437	14.663	14.888	15.114	15.340	15.565
7	15.791	16.016	16.242	16.468	16.693	16.919	17.144	17.370	17.595	17.821
8	18.047	18.272	18.498	18.723	18.949	19.175	19.400	19.626	19.851	20.077
9	20.302	20.528	20.754	20.979	21.205	21.430	21.656	21.882	22.107	22.333
10	22.558	22.784	23.009	23.235	23.461	23.686	23.912	24.137	24.363	24.589
11	24.814	25.040	25.265	25.491	25.716	25.942	26.168	26.393	26.619	26.844
		- 1		er 0					D. 10	
12	27.070	27.296	27.521	27.747	27.972	28.198	28.423	28.649	28.875	29.100
13	29.326	29.551	29.777	30.003	30.228	30.454	30.679	30.905	31.130	31.356
- 14	31.582	31.807	32.033	32.258	32.485	32.711	32.936	33.162	33.387	33.613
15	33.837	34.063	34.289	34.514	34.740	34.965	35.191	35.417	35.642	35.868
16	36.093	36.319	36.544	36.770	36.996	37.221	37.447	37.672	37.898	38.124
17	38.349	38.575	38.800	39.026	39.251	39.477	39.703	39.928	40.154	40.379
18 '	40.605	40.831	41.056	41.282	41.507	41.733	41.958	42.184	42.410	42.635

XIV. CONVERSION OF FRENCH OR PARIS LINES INTO ENGLISH INCHES.  $1 \ {\rm Paris \ Line} = 0.088814 \ {\rm English \ Inch}.$ 

Paris					Tenths o	f a Line.				
Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
RUN	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.
0	0.0000	0.0089	0.0178	0.0266	0.0355	0.0444	0.0533	0.0622	0.0711	0.0799
1	0.0888	0.0977	0.1066	0.1155	0.1243	0.1332	0.1421	0.1510	0.1599	0.1687
2	0.1776	0.1865	0.1954	0.2043	0.2132	0.2220	0.2309	0.2398	0.2487	0.2576
3	0.2664	0.2753	0.2842	0.2931	0.3020	0.3108	0.3197	0.3286	0.3375	0.3464
4	0.3553	0.3641	0.3730	0.3819	0.3908	0.3997	0.4085	0.4174	0.4263	0.4352
5	0.4441	0.4530	0.4618	0.4707	0.4796	0.4885	0.4974	0.5062	0.5151	0.5240
6	0.5329	0.5418	0.5506	0.5595	0.5684	0.5773	0.5862	0.5951	0.6039	0.6128
7	0.6217	0.6306	0.6395	0.6483	0.6572	0.6661	0.6750	0.6839	0.6927	0.7016
8	0.7105	0.7194	0.7283	0.7372	0.7460	0.7549	0.7638	0.7727	0.7816	0.7904
9	0.7993	0.8082	0.8171	0.8260	0.8349	0.8437	0.8526	0.8615	0.8704	0.8793
10	0.8881	0.8970	0.9059	0.9148	0.9237	0.9325	0.9414	0.9503	0.9592	0.9681
1.1	0.9770	0.9858	0.9947	1.0036	1.0125	1.0214	1.0302	1.0391	1.0480	1.0569
12	1.0658	1.0746	1.0835	1.0924	1.1013	1.1102	1.1191	1.1279	1.1368	1.1457
13	1.1546	1.1635	1.1723	1.1812	1.1901	1.1990	1.2079	1.2168	1.2256	1.2345
14	1.2434	1.2523	1.2612	1.2700	1.2789	1.2878	1.2967	1.3056	1.3144	1.3233
15	1.3322	1.3411	1.3500	1.3589	1.3677	1.3766	1.3855	1.3944	1.4033	1.4121
16	1.4210	1.4299	1.4388	1.4477	1.4565	1.4654	1.4743	1.4832	1.4921	1.5010
17	1.5098	1.5187	1.5276	1.5365	1.5454	1.5542	1.5631	1.5720	1.5809	1.5898
18	1.5987	1.6075	1.6164	1.6253	1.6342	1.6431	1.6519	1.6608	1.6697	1,6786

#### XV. CONVERSION OF RUSSIAN HALF-LINES INTO MILLIMETRES.

1 Russian Half-Line = 1.269977 Millimetres.

Russian					Ten	ths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.									
0	0.000	0.127	0.254	0.381	0.508	0.635	0.762	0.889	1.016	1.143
1	1.270	1.397	1.524	1.651	1.778	1.905	2.032	2.159	2.286	2.413
. 2	2.540	2.667	2.794	2.921	3.048	3.175	3.302	3.429	3.556	3.683
3	3.810	3.937	4.064	4.191	4.318	4.445	4.572	4.699	4.826	4.958
4	5.080	5.207	5.334	5.461	5.588	5.715	5.842	5.969	6.096	6.228
5	6.350	6.477	6.604	6.731	6.858	6.985	7.112	7.239	7.366	7.498
The Park	200			Out of				45 1		
6	7.620	7.747	7.874	8.001	8.128	8.255	8.382	8.509	8.636	8.768
7	8.890	9.017	9.144	9.271	9.398	9.525	9.652	9.779	9.906	10.038
8	10.160	10.287	10.414	10.541	10.668	10.795	10.922	11.049	11.176	11.303
9	11.430	11.557	11.684	11.811	11.938	12.065	12.192	12.319	12.446	12.573
10	12.700	12.827	12.954	13.081	13.208	13.335	13.462	13.589	13.716	13.843
11	13.970	14.097	14.224	14.351	14.478	14.605	14.732	14.859	14.986	15.118
TO .									Will be	
12	15.240	15.367	15.494	15.621	15.748	15.875	16.002	16.129	16.256	16.383
13	16.510	16.637	16.764	16.891	17.018	17.145	17.272	17.399	17.526	17.653
14	17.780	17.907	18.034	18.161	18.288	18.415	18.542	18.669	18.796	18.923
15	19.050	19.177	19.304	19.431	19.558	19.685	19.812	19.939	20.066	20.193
16	20.320	20.447	20.574	20.701	20.828	20.955	21.082	21.209	21.336	21.463
17	21.590	21.717	21.844	21.971	22.098	22.225	22.352	22.479	22.606	22.733
18	22.860	22.987	23.114	23.241	23.368	23.495	23.622	23.749	23.876	24.003

XVI. CONVERSION OF RUSSIAN HALF-LINES INTO PARIS LINES.

1 Russian Half-Line = 0.562976 Paris Line.

Russian					Ter	iths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
W. S.L.	Par. line	Par. line.	Par. line							
0	0.000	0.056	0.113	0.169	0.225	0.281	0.338	0.394	0.450	0.507
1	0.563	0.619	0.676	0.732	0.788	0.844	0.901	0.957	1.013	1.070
2	1.126	1.182	1.239	1.295	1.351	1.407	1.464	1.520	1.576	1.633
3	1.689	1.745	1.802	1.858	1.914	1.970	2.027	2.083	2.139	2.196
4	2.252	2.308	2.364	2.421	2.477	2.533	2.590	2.646	2.702	2.759
5	2.815	2.871	2.927	2.984	3.040	3.096	3.153	3.209	3.265	3.322
6	3.378	3.434	3.490	3.547	3.603	3.659	3.716	3.772	3.828	3.885
7	3.941	3.997	4.053	4.110	4.166	4.222	4.279	4.335	4.391	4.448
8	4.504	4.560	4.616	4.673	4.729	4.785	4.842	4.898	4.954	5.010
9	5.067	5.123	5.179	5.236	5.292	5.348	5.405	5.461	5.517	5.573
10	5.630	5.686	5.742	5.799	5.855	5.911	5.968	6.024	6.080	6.136
11	6.193	6.249	6.305	6.362	6.418	6.474	6.531	6.587	6.643	6.699
12	6.756	6.812	6.868	6.925	6.981	7.037	7.093	7.150	7.206	7.262
13	7.319	7.375	7.431	7.488	7.544	7.600	7.656	7.713	7.769	7.825
14	7.882	7.938	7.994	8.051	8.107	8.163	8.219	8.276	8.332	8.388
15	8.445	8.501	8.557	8.614	8.670	8.726	8.782	8.839	8.895	8.951
16	9.008	9.064	9.120	9.177	9.233	9.289	9.345	9.402	9.458	9.514
17	9.571	9.627	9.683	9.739	9.796	9.852	9.908	9.965	10.021	10.077
18	10.134	10.190	10.246	10.302	10.359	10.415	10.471	10.528	10.584	10.640

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# TABLES

FOR

# REDUCING BAROMETRICAL OBSERVATIONS,

TAKEN AT ANY TEMPERATURE,

TO THE TEMPERATURE OF THE FREEZING POINT.

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#### TABLES

FOR

REDUCING THE BAROMETRICAL OBSERVATIONS TAKEN AT ANY TEMPERATURE TO THE TEMPERATURE OF THE FREEZING POINT.

THE variations of the mercurial column in a stationary barometer are due to two causes, the changes of atmospheric pressure and the variations of temperature of the mercury, which affect the length of the column by changing its density. The variations of atmospheric pressure, which alone the barometer is destined to ascertain, are therefore hidden, and their observation falsified by the expansion or contraction of the mercury due to changes of temperature. For, supposing that, while the atmospheric pressure remains the same, the temperature of the instrument becomes lower, the mercurial column will become shorter, and the barometer will appear to fall; if the pressure becomes less, but the temperature increases, the expansion of the mercury will tend to compensate the diminution of pressure, and the barometer may remain stationary, or even may rise, while it ought to be falling; in other cases the action of temperature will tend to increase the amount of the changes of the barometrical height. It is therefore evident that successive observations, with the same barometer, do not give directly the actual changes of atmospheric pressure, unless they have been taken exactly at the same temperature, a case which, in practice, seldom occurs. Likewise simultaneous observations, taken with various barometers, do not give directly the actual differences of the absolute pressure of the atmosphere above the instruments. To obtain the true barometrical heights, that is, the action of the atmospheric pressure alone, the influence of the temperature must first be eliminated from the observed heights. This is done by reducing, by means of the following Tables, the various barometrical columns to the length they would have at a given temperature, which is the same for all. For the sake of convenient comparison, the freezing point has been almost universally adopted as the standard temperature to which all observations are to be reduced.

#### CONSTRUCTION OF THE TABLES.

In all the following Tables the barometers are supposed to be furnished with brass scales, extending from the surface of the mercury in the cistern to the top of the mercurial column. The correction to be applied is therefore composed of two elements: the correction for the expansion of the mercury, and that for the expansion of the scale; both of which ought to be, and have been, taken into account.

Indeed, the correction for the expansion of mercury is not sufficient to reduce the readings to the height which the barometer would indicate, under the same pressure, at the temperature of the freezing point. For when the temperature rises the mercurial column expands; but then the scale also grows longer, and this will tend to lower the reading of the height. The correction for the expansion of the mercury

must thus be diminished by the amount of that of the scale, that is, by nearly 100, this being the proportion between the expansion of brass and that of mercury.

It is also the expansion of the scale which causes an apparent anomaly in the Tables for the Reduction of the English and Old French Barometers. It can be seen, that, though the observations are to be reduced to the freezing point, or to 32° Fahrenheit and zero Reaumur, the Tables give still a correction for observations taken at that temperature. The reason of it is, that the normal length of the English and Old French standards has not been determined at the temperature of the freezing point, as is the case with the metre, but respectively at the temperatures of 62° Fahrenheit and 13° Reaumur. It is thus only at these temperatures that the scales graduated with these standards have their true length. Above and below, the inches of the scales are longer or shorter than the inches of the standards. At the freezing point, therefore, the correction for the expansion of the mercury is null, but that for the expansion of the scale is not. The scale being too short, the reading will be too high, and a subtractive correction must still be applied, which will be gradually compensated at lower temperatures by the now additive correction of the mercurial column. Thus the point of no correction will occur at 28°.5 Fahrenheit, instead of 32°, in the English Barometer, and at -1°.5 Reaumur, instead of zero, in the Old French.

Schumacher has calculated and published in his Collection of Tables, &c., and in his Jahrbuch for 1836, 1837, and 1838, extensive tables for the reduction of the English, Old French, and Metrical Barometers, using the following general formula:—

Let h =observed height.

" t = temperature of the attached thermometer.

" T = temperature to which the observed height is to be reduced.

" m = expansion, in volume, of mercury.

" l = linear expansion of brass.

" & = normal temperature of the standard scale.

The reduction to the freezing point will be given by the formula, -

$$h \cdot \frac{m(t-T)-l(t-\theta)}{1+m(t-T)}$$

The following tables, which may be found more convenient for ordinary use, have been calculated from the same formula. Table XVII., published in the Instructions of the Royal Society of London, is mostly abstracted from the table of Schumacher. It gives the reduction of the English Barometer, adopting the following values:—

Let h = observed height in English inches.

" t = temperature of attached thermometer in degrees of Fahrenheit.

" m = expansion, in volume, of mercury for one degree Fahrenheit = 0.0001001.

" l = linear expansion of brass for one degree Fahrenheit = 0.0000104344.

The normal temperature of standard being = 62°.

The reduction to 32° Fahrenheit will be given then by the formula,

$$-h \cdot \frac{m(t-32)-l(t-62)}{1+m(t-32)}$$
.

The elements for the other tables are found at the head of each.

## XVII.

### ENGLISH BAROMETER.

# TABLE

# GIVING THE CORRECTION TO BE APPLIED TO ENGLISH BAROMETERS,

WITH BRASS SCALES EXTENDING FROM THE CISTERN TO THE TOP OF
THE MERCURIAL COLUMN, FOR REDUCING THE OBSERVATIONS
TO THIRTY-TWO DEGREES FAHRENHEIT.

A CERMONA OF HIGHER E

# TIMEAT

CIVING THE CORRECTION TO SEE APPLICATION OF THE CONTROL OF THE CON

The control of the control of the second sec

#### TABLE XVII.

The following Table, calculated after that of Schumacher, has been adopted by the Committee of Physics and Meteorology of the Royal Society of London. It gives immediately the correction for every degree of Fahrenheit, and for every half-inch from 20 up to 31 inches. The scale of the barometer is supposed to be of brass, extending from the cistern to the top of the mercurial column. The difference of expansion of brass and mercury is taken into account. The standard temperature of the yard being 62° Fahr., and not 32° Fahr., the difference of expansion of the scale and of the mercurial column carries the point of no correction down to 29° Fahr. Therefore, from 29° up the correction must be subtracted from, from 29° down it must be added to, the observed height.

#### Examples of Calculation.

Barometer, observed height, . . . . . . 30.231
Attached thermometer 82° Fahr.

See in the last page the column of 30 inches; go down as far as the horizontal line corresponding with 82° in the first vertical column, which contains the temperatures; you will find there the correction —.143. We have thus:—

Barometer, observed height,	DIN	30.231
Subtractive correction for 82° Fahr.,		-0.143
Barometer at 32° Fahr.,		30.088
Barometer, observed height,	- 13 6130H	29.743
The column of 29.5 inches opposite to 25° Fahr. gives	an	
additive correction of,	100	+0.009
Barometer at 32° Fahr		29.752

It will be easy to apply also the correction for fractions of a degree Fahrenheit; for example:—

Barometer, observed height,	101			28.358	
Attached thermometer 71.3			4 4.		

In the column of 28.5 inches, we find that the difference between the correction for 71° and that for 72° is .003; dividing this difference proportionally to the fraction, we have for three tenths of a degree a correction of —.001, which added to —.108, the correction for 71°, makes a total correction of,

And barometer at 32° Fahr.,	 28.249

Degrees of Fah-				English	Inches.				Degree of Fal
of Fah- renheit.	20	20.5	21	21.5	22	22.5	23	23.5	of Fairenhei
°	0.051	. 050	1.054	+.055	1.050	1.050	. 050	. 000	°
1	+.051	+.053	+.054	.053	+.056	+.058	+.059	+.060	1
2	.049	.051			.054			.058	1
3	.048	.049	:050	.051	.052	.054	.055	.056	2 3
4	.046	.047	.048	.049	.050	.052	.053	.054	
5	.044	.045	.046	.045	.048	.050	.049	.052	5
6	+.040	+.042	+.042	+.044	+.044	+.046	+.047	+.048	6
7	.039	.040	.041	.042	.042	.044	.044	.046	7
8	.037	.038	.039	.040	.041	.041	.042	.043	8
9	.035	.036	.037	.038	.039	.039	.040	.041	9
10	.033	.034	.035	.036	.037	.037	.038	.039	10
11	+.031	+.032	+.033	+.034	+.035	+.035	+.036	+.037	11
12	.030	.030	.031	.032	.033	.033	.034	.035	12
13	.028	.029	.029	.030	.031	.031	.032	.033	13
14	.026	.027	.027	.028	.029	.029	.030	.031	14
15	.024	.025	.026	.026	.027	.027	.028	.029	15
16	+.022	+.023	+.024	+.024	+.025	+.025	+.026	+.026	16
17	.021	.021	.022	.022	.023	.023	.024	.024	17
18	.019	.019	.020	.020	.021	.021	.022	.022	18
19	.017	.018	.018	.018	.019	.019	.020	.020	19
20	.015	.016	.016	.016	.017	.017	.018	.018	20
21	+.014	+.014	+.014	+.015	+.015	+.015	+.015	+.016	21
22	.012	.012	.012	.013	.013	.013	.013	.014	22
23	.010	.010	.010	.011	.011	.011	.011	.012	23
24	.008	.008	.009	.009	.009	.009	.009	.010	24
25	.006	.007	.007	.007	.007	.007	.007	.007	25
26	+.005	+.005	+.005	+.005	+.005	+.005	+.005	+.005	26
27	.003	.003	.003	.003	.003	.003	.003	.003	27
28	.001	.001	.001	.001	.001	.001	.001	.001	28
29	001	001 •	001	001	001	001	001	001	29
30	.003	.003	.003	.003	.003	.003	.003	.003	30
31	005	005	005	005	005	005	005	005	31
32	.006	.006	.007	.007	.007	.007	.007	.007	32
33	.008	.008	.008	.009	.009	.009	.009	.010	33
34 35	.010 .012	.010 .012	.010 .012	.011	.011	.011	.011	.012	34 35
36	-010	Males 1	-014	-034	-015	-075	-010	-070	96
37	013	014	014	014	015	015	016	016	36
	.015	.016	.016	.016	.017	.017	.018	.018	37
38	.017	.017	.018	.018	.019	.019	.020	.020	38
40	.019	.019 .021	.020	.020	.021	.021	.022	.022	40
41	022	023	- 094	- 004	025	025	026	026	41
42	.022	.025	024	024	.025	.025	.028	.028	41
43	.024	.023	.025	.028	.027	.027	.030	.031	43
44	.028	.027	.027	.030	.031	.031	.032	.033	44
45	.030	.030	.031	.032	.033	.033	.034	.035	45
46	031	032	033	<b>∠.034</b>	035	035	036	037	46
47	.033	.034	.035	.036	.036	.037	.038	.039	47
48	.035	.036	.037	.038	.038	.039	.040	.041	48
49	.037	.038	.039	.040	.040	.041	.042	.043	49
50	.038	.039	.040	.041	.042	.043	.044	.045	50

Degrees				English	Inches.				Degrees
of Fah- renheit.	20	20.5	21	21.5	22	22.5	23	23.5	of Fah- renheit.
51	040	041	042	043	044	045	046	047	51
52	.042	.043	.044	.045	.046	.047	.048	.049	52
53	.044	.045	.046	.047	.048	.049	.050	.052	53
54 55	.046	.047	.048	.049	.050	.051	.052	.054	54 55
-	EARLY .	TON CO.	ELOUIN	A CONTRACTOR		249	TEAST.	Male.	
56 57	049 .051	050 .052	052 .054	053 .055	054	055 .057	057	058 .060	56 57
58	.053	.054	.055	.057	.058	.059	.061	.062	58
59	.055	.056	.057	.059	.060	.061	.063	.064	59
60	.056	.058	.059	.061	.062	.063	.065	.066	60
61	058	060	061	062	064	065	067	068	61
62	.060	.061	.063	.064	.066	.067	.069	.070	62
63	.062	.063	.065	.066	.068	.069	.071	.072	63
64	.063	.065	.067	.068	.070	.071	.073	.075	64
65	.065	.067	.068	.070	.072	.073	.075	.077	65
66	067	069	070	072	074	075	077	079	66
67	.069	.071	.072	.074	.076	.077	.079	.081	67
68	.071	.072	.074	.076	.078	.079	.081	.083	68
69 70	.072	.074	.076	.078	.080	.081	.083	.085	69
10	.074	.076	.078	.080	.082	.083	.085	.087	70
71	076	078	080	082	083	085	087	089	71
72	.078	.080	.082	.084	.085	.087	.089	.091	72
73 74	.079	.081	.083	.085	.087	.089	.091	.093	73
75	.083	.083	.085	.087	.089	.091	.093	.095	74 75
76	085	087	089	091	093	095	097	100	76
77	.087	.089	.091	.093	.095	.097	.100	.102	77
78	.088	.091	.093	.095	.097	.099	.102	.104	78
79	.090	.092	.095	.097	.099	.101	.104	.106	79
80	.092	.094	-096	.099	.101	.103	• .106	.108	80
81	094	096	098	101	103	105	108	110	81
82	.095	.098	.100	.103	.105	.107	.110	.112	82
83	.097	.100	.102	.104	.107	.109	.112	.114	83
84	.099	.101	.104	.106	.109	.111	.114	.116	84
85	.101	.103	.106	.108	.111	.113	116	.118	85
86	103	105	108	110	113	115	118	120	86
87	.104	.107	.109	.112	.115	.117	.120	.123	87
88	.106	.109	.111 .113	.114	.117	.119	.122	.125	88
90	.110	.112	.115	.118	.121	.123	.124	.127	89 90
91	_ 111	-114	_ 117	120	_ 100	105	100	101	0.7
91	111 .113	114 .116	117 .119	120	122 .124	125 .127	128 .130	131 .133	91 92
93	.115	.118	.121	.124	.126	.129	.132	.135	93
94 95	.117	.120 .121	.122	.125 .127	.128	.131	.134	.137	94
00	.110	1121	.122	.127	.100	100	.100	.105	95
96	120	123	126	129	132	135	138	141	96
97 98	.122	.125 .127	.128	.131 .133	.134	.137	.140	.143	97
99	.124	.127	.130	.135	.136 .138	.139	.142 .144	.145	98
100	.127	.130	.134	.137	140	.143	.146	.150	100
100	DEST. AT	1977 Th. 3.		GIB - SV	Marie Contract	CARE TITLE	SWEET THE	31102	BB 18

Degrees				English	Inches.				Degrees of Fah
of Fah- renheit.	24	24.5	25	25.5	26	26.5	27	27.5	of Fah renheit
°	+.061	+.063	+.064	+.065	+.067	+.068	+.069	+.071	°
1	.059	.061	.062	.063	.064	.065	.067	.068	1
2	.057	.058	.060	.061	.062	.063	.064	.066	2
3	.055	.056	.057	.059	.060	.061	.062	.063	3
4	.053	.054	.055	.056	.057	.058	.059	.061	4
5	.051	.052	.053	.054	.055	.056	.057	.058	5
6	+.049	+.050	+.051	+.052	+.053	+.054	+.055	+.056	6
7	.046	.047	.048	.049	.050	.051	.052	.053	7
8	044	.045	.046	.047	.048	.049	.050	.051	8
9	.042	.043	.044	.045	.046	.046	.047	.048	9
10	.040	.041	.042	.042	.043	.044	.045	.046	10
11	+.038	+.039	+.039	+.040	+.041	+.042	+.042	+.043	11
12	.036	.036	.037	.038	.039	.039	.040	.041	12
13	.033	.034	.035	.036	.036	.037	.038	.038	13
15	.031	.032	.033	.033	.034	.035	.035	.036	14
13	.029	.030	.030	.031	.032	.032	.033	.033	15
16	+.027	+.028	+.028	+.029	+.029	+.030	+.030	+.031	16
17	.025	.025	.026	.026	.027	.027	.028	.028	17
18	.023	.023	.024	.024	.025	.025	.025	.026	18
19	.021	.021	.021	.022	.022	.023	.023	.024	19
20	.018	.019	.019	.020	.020	.020	.021	.021	20
21	+.016	+.017	+.017	+.017	+.018	+.018	+.018	+.019	21
22	.014	.014	.015	.015	.015	.016	.016	.016	22
23	.012	.012	.012	.013	.013	.013	.013	.014	23
24 25	.010	.010	.010	.010	.011	.011	.011	.011	24
20	.008	.008	.008	.008	.008	.008	.009	•009	25
26	+.005	+.006	+.006	+.006	+.006	+.006	+.006	+.006	26
27	.003	.003	.003	.003	.004	.004	.004	.004	27
28	.001	.001	.001	.001	.001	.001	.001	.001	28
29	001	001	001	001	001	001	001	001	29
30	.003	.003	.003	.004	.004	.004	.004	.004	30
31 32	005	006	006	006	006	006	006	006	31
33	.008	.008	.008	.008	.008	.008	.008	.009	32
34	.012	.012	.010	.010	.011	.011	.011	.011	33 34
35	.014	.014	.015	.015	.015	.015	.016	.016	35
36	016	017	017	017	017	018	018	019	36
37	.018	.019	.019	.019	.020	.020	.021	.021	37
38	.020	.021	.021	.022	.022	.023	.023	.023	38
39	.023	.023	.024	.024	.024	.025	.025	.026	39
40	.025	.025	.026	.026	.027	.027	.028	.028	40
41	027	027	028	029	029	030	030	031	41
42	.029	.030	.030	.031	.031	.032	.033	.033	42
43	.031	.032	.032	.033	.034	.034	.035	.036	43
44 45	.033	.034	.035	.035	.036	.037	.037	.038	44 45
16	Inter a	atto.	2014	page and	and a	1000	men and	OKU-	
46	038	038	039	040	041	042	042	043	46
48	.040	.041	.041	.042	.043	.044	.045	.046	47
49	.042	.043	.044	.045	.045	.046	.047	.048	48
50	.046	.043	.048	.047	.048	.049	.050	.050	49 50

Degrees	English Inches.												
of Fah- renheit.	24	24.5	25	25.5	26	26.5	27	27.5	Degree of Fa renhe				
° 51		The series	N. Carlo		746 646		(68.8K)	004.00	51				
	048	049	050	051	052	053	054	055					
52	.050	.052	.053	.054	.055	.056	.057	.058	52				
53	.053	.054	.055	.056	.057	.058	.059	.060	53				
54 55	.055	.056	.057	.058	.059	.060	.062	.063	54 55				
		.000	.000		.002	.000	.001	1000	00				
56	059	060	061	063	064	065	066	068	56				
57	.061	.062	.064	.065	.066	.068	.069	.070	57				
58	.063	.065	.066	.067	.069	.070	071	.073	58				
59 60	.065	.067	.068	.070	.071	.072	.074	.075	59 60				
11	DY	1000		1012	.0.0	.0.0	10.00		00				
61	070	071	073	074	075	077	078	080	61				
62	.072	.073	.075	.076	.078	.079	.081	.082	62				
63	.074	.076	.077	.079	.080	.082	.083	.085	63				
64	.076	.078	.079	.081	.082	.084	.086	.087	64				
65	.078	.080	.082	.083	.085	.086	.088	.090	65				
66	080	082	084	085	087	089	090	092	66				
67	.083	.084	.086	.088	.089	.091	.093	.095	67				
68	.085	.086	.088	.090	.092	.094	.095	.097	68				
69	.087	.089	.090	.092	.094	.096	.098	.100	69				
70	.089	.091	.093	.095	.096	.098	.100	.102	70				
71	001	000	000	007	200	0.	10 01						
71	091	093	095	097	099	101	102	104	71				
72	.093	.095	.097	.099	.101	.103	.105	.107	72				
73 74	.095	.097	.099	.101	.103	.105	.107	.109	73				
75	.097	.102	.102	.104	.106	.108	.110 .112	.112	74 75				
	15/8					W 3-1	10.	Carlo III					
76	102	104	106	108	110	112	114	117	76				
77	.104	.106	.108	.110	.112	.115	117	.119	77				
78	.106	.108	.110	.113	.115	.117	.119	.122	78				
79	.108	.110	.113	.115	.117	.119	.122	.124	79				
80	.110	.113	.115	.117	.119	.122	.124	.126	80				
81	112	115	117	119	122	124	126	129	81				
82	.114	.117	.119	.122	.124	.126	.129	.131	82				
83	.117	.119	.121	.124	.126	.129	.131	.134	83				
84	.119	.121	.124	.126	.129	.131	.134	.136	84				
85	.121	.123	.126	.128	.131	.133	.136	.139	85				
96	100	100	100	101	100	100	100	314					
86 87	123 .125	126 .128	128 .130	131 .133	133 .136	136 .138	138 .141	141	86				
88	.125	.128	.130	.135	.138	.138	.141	.143	87				
89	.129	.132	.135	.137	.140	.143	.146	.148	88 89				
90	.131	.134	.137	.140	.142	.145	.148	.151	90				
0.	104	100	100	110	145	140			TAKE .				
91 92	134	136 .139	139 .141	142	145 .147	148 .150	150 .153	153 .156	91 92				
93	.138	.141	.144	.147	.149	.152	.155	.158	93				
94	.140	.143	.146	.149	.152	.155	.157	.161	94				
95	.142	.145	.148	.151	.154	.157	.160	.163	95				
0.0	144	147	150	150	120	150	100	100					
96 97	144	147 .149	150 .152	153 .156	156 .159	159 .162	162	165	96				
98	.148	.152	.152	.158	.161	.162	.165 .167	.168	97				
99	.151	.154	.157	.160	.163	.166	.169	.170	98				
100	.153	.156	.159	.162	.165	.169	.172	.175	99				
					-200		*414	.110	100				

Degrees of	English Inches.											
Fahren- heit.	28	28.5	29	29.5	30	30.5	31	Fahren heit.				
°	+.072	+.073	+.074	+.076	+.077	+.078	+.080	°o				
1	.069	.071	.072	.073	.074	.076	.077	li				
2		.068	.069	.070	.072	.073	.074	2				
3	.067	.065	.067	.068	.069	.070	.071	3				
4	.064	.063	.064	.065	.066	.067	.068	4				
5	.062	.060	.061	.062	.063	.065	.066	5				
6	+.057	+.058	+.059	+.060	+.061	+.062	+.063	6				
7	.054	.055	.056	.057	.058	.059	.060	7				
8	.052	.053	.054	.054	.055	.056	.057	8				
9	.049	.050	.051	.052	.053	.054	.054	9				
10	.047	.047	.048	.049	.050	.051	.052	10				
11	+.044	+.045	+.046	+.046	+.047	+.048	+.049	11				
12	.042	.042	.043	.044	.045	.045	.046	12				
13	.039	.040	.040	.041	.042	.043	.043	13				
14	.037	.037	.038	.038	.039	.040	.040	14				
15	.034	.035	.035	.036	.036	.037	.038	15				
16	+.032	+.032	+.033	+.033	+.034	+.034	+.035	16				
17	.029	.030	.030	.031	.031	.032	.032	17				
18	.026	.027	.027	.028	.028	.029	.029	18				
19	.024	.024	.025	.025	.026	.026	.027	19				
20	.021	.022	.022	.023	.023	.023	.024	20				
21	+.019	+.019	+.020	+.020	+.020	+.021	+.021	21				
22	.016	.017	.017	.017	.018	.018	.018	22				
23	.014	.014	.014	.015	.015	.015	.015	23				
24	.011	.012	.012	.012	.012	.012	.013	24				
25	.009	.009	.009	.009	.009	.010	.010	25				
26	+.006	+.006	+.007	+.007	+.007	+.007	+.007	26				
27	.004	.004	.004	.004	.004	.004	.004	27				
28	.001	.001	.001	.001	.001	.001	.001	28				
29	001	001	001	001	001	001	001	29				
30	.004	.004	.004	.004	.004	.004	.004	30				
31	006	006	007	007	007	007	007	31				
32	.009	.009	.009	.009	.009	.010	.010	32				
33	.011	.012	.012	.012	.012	.012	.012	33				
34	.014	.014	.014	.015	.015	.015	.015	34				
35	.016	.017	.017	.017	.018	.018	.018	35				
36	019	019	020	020	020	021	021	36				
37	.021	.022	.022	.022	.023	.023	.024	37				
48	.024	.024	.025	.025	.026	.026	.026	38				
39	.026	.027	.027	.028	.028	.029	.029	39				
40	.029	.029	.030	.030	.031	.031	.032	40				
41	031	032	033	033	034	034	035	41				
42	.034	.034	.035	.036	.036	.037	.037	42				
43	.036	.037	.038	.038	.039	.040	.040	43				
44 45	.039	.040	.040 .043	.041	.042	.042 .045	.043	44 45				
							111,00					
46	044	045	045	046	047	048	049	46				
47	.046	.047	.048	.049	.050	.051	.051	47				
48	.049	.050	.051	.052	.052	.053	.054	48				
	.051	.052	.053	.054	.055	.056	.057	49				

egrees of			1	English Inche	s.			Degrees
Fahren- heit.	28	28.5	29	29.5	30	30.5	31	Fahren heit.
51	056	057	058	059	060	061	062	51
52	.059	.060	.061	.062	.063	.064	.065	52
53	.061	.063	.064	.065	.066	.067	.068	53
54	.064	.065	.066	.067	.068	.070	.071	54
55	.066	.068	.069	.070	.071	.072	.073	55
56	069	070	071	073	074	075	076	56
57	.071	.073	.074	.075	.076	.078	.079	57
58	.074	.075	.077	.078	.079	.081	.082	58
59	.076	.078	.079	.080	.082	.083	.085	59
60	.079	.080	.082	.083	.085	.086	.087	60
61	081	083	084	086	087	089	090	61
62	.084	.085	.087	.088	.090	.091	.093	62
63	.086	.088	.089	.091	.093	.094	.096	63
64 65	.089	.090	.092	.094	.095	.097	.098	64
65	.091	.093	.095	.096	.098	.100	.101	03
66	094	096	097	099	101	102	104	66
67	.096	.098	.100	.102	.103	.105	.107	67
68	.099	.101	.102	.104	.106	.108	.109	68
69 70	.101	.103	.105	.107	.109	.110	.112	69
10	.104	.100	.100	.103	.111	.115	.110	1
71	106	108	110	112	114	116	118	71
72	.109	.111	.113	.115	.117	.119	.120	72
73	.111	.113	.115	.117	.119	.121	.123	73 74
74 75	.114	.116	.118	.120	.122	.124	.126	75
76	110	101	100	125	127	129	131	76
77	119 .121	121 .123	123 .126	.128	.130	.132	.134	77
78	.124	.126	.128	.130	.133	.135	.137	78
79	.126	.128	.131	.133	.135	.137	.140	79
80	.129	.131	.133	.136	.138	.140	.143	80
81	131	134	136	138	141	143	145	81
82	.134	.136	.138	.141	.143	.146	.148	82
83	.136	.139	.141	.143	.146	.148	.151	83
84	.139	.141	.144	.146	.149	.151	.154	84
85	.141	.144	.146	.149	.151	.154	.156	85
86	144	146	149	151	154	156	159	86
87	.146	.149	.151	.154	.157	.159	.162	87
88	.149	.151	.154	.157	.159	.162	.165	88
89	.151	.154	.156	.159	.162	.165	.167	89
90	.153	.156	.159	.162	.164	.167	.170	90
91	156	159	162	165	167	170	-173	91
92	.158	.161	.164	.167	.170	.172	.175	92
93	.161	.164	.167	.170	.172	.175	.178	93
94 95	.163	.166	.169 .172	.172 .175	.175 .178	.177	.180	94 95
1472	11 Ma.	Little 1	3-190	538 F	110.5-170	A TANK	(A8.4-1	
96	168	171	174	178	181	183	186	96
97	.171	.174	.177	.180	.183	.186	.189	97
98 99	.173 .176	.176 .179	.179	.183	.186 .188	.188	.191	98
100	.178	.181	.184	.188	.191	.194	.197	100
	AND RESERVED TO SERVED STATE OF THE PARTY OF							11

#### TABLE XVIII.

FOR REDUCING THE INDICATIONS OF ENGLISH BAROMETERS, WITH WOODEN OR GLASS SCALES, TO THE FREEZING POINT.

In most of the common barometers the scale is engraved upon a short plate of brass, or of ivory, fixed upon the wooden frame of the instrument. In such a case, the compound expansion of the two substances can only be guessed at, and the correction to be applied to the observations for reducing them to the freezing point cannot be determined with precision. As a near approximation for such imperfect instruments, the following table may be used. In computing this table, the expansion of glass, which is less than that of brass and greater than that of wood, has been substituted for that of brass, as an approximate value for a scale composed of these last two substances. The table thus gives the true correction, in English inches, for the barometers, the graduation of which is engraved on the glass tube itself. It answers equally for any English barometer with wooden scale, whatever be the substance of which the short plate bearing the graduation is made.

CORRECTIONS TO BE APPLIED TO ENGLISH BAROMETERS, WITH WOODEN OR GLASS SCALES, TO REDUCE THE OBSERVATIONS TO THE FREEZING POINT.

Expansion of Mercury for  $1^{\circ}$  Fahr. = 0.0001001; of Glass for  $1^{\circ}$  Fahr. = 0.00000444.

ttached nermom-		Barometer in English Inches.												
eter, ahren- heit.	26	26.5	27	27.5	28	28.5	29	29.5	30	30.5	31			
°	+.076	+.077	+.079	+.080	+.082	+.083	+.085	+.086	+.088	+.089	+.090			
1	+.073	+.075	+.076	+.078	+.079	+.080	+.082	+.083	+.085	+.086	+.088			
2	+.071	+.072	+.074	+.075	+.076	+.078	+.079	+.080	+.082	+.083	+.085			
	+.068	+.070	+.071	+.072	+.074	+.075	+.076	+.078	+.079	+.080	+.082			
1	+.066	+.067	+.069	+.070	+.071	+.072	+.074	+.075	+.076	+.077	+.079			
5	+.064	+.065	+.066	+.067	+.068	+.070	+.071	+.072	+.073	+.074	+.076			
6	+.061	+.062	+.063	+.065	+.066	+.067	+.068	+.069	+.070	+.072	+.073			
	+.059	+.060	+.061	+.062	+.063	+.064	+.065	+.067	+.068	+.069	+.070			
	+.056	+.057	+.058	+.059	+.060	+.061	+.063	+.064	+.065	+.066	+.067			
	+.054	+.055	+.056	+.057	+.058	+.059	+.060	+.061	+.062	+.063	+.064			
	+.051	+.052	+.053	+.054	+.055	+.056	+.057	+.058	+.059	+.060	+.061			
M	+.049	+.050	+.051	+.051	+.052	+.053	+.054	+.055	+.056	+.057	+.058			
	+.046	+.047	+.048	+.049	+.050	+.051	+.052	+.052	+.053	+.054	+.055			
	+.044	+.045	+.045	+.046	+.047	+.048	+.049	+.050	+.050	+.051	+.052			
	+.041	+.042	+.043	+.044	+.044	+.045	+.046	+.047	+.048	+.048	+.049			
5	+.039	+.039	+.040	+.041	+.042	+.042	+.043	+.044	+.045	+.045	+.046			
	+.036	+.037	+.038	+.038	+.039	+.040	+.040	+.041	+.042	+.043	+.043			
7	+.034	+.034	+.035	+.036	+.036	+.037	+.038	+.038	+.039	+.040	+.040			
1195	+.031	+.032	+.032	+.033	+.034	+.034	+.035	+.036	+.036	+.037	+.037			
	+.029	+.029	+.030	+.030	+.031	+.032	+.032	+.033	+.033	+.034	+.034			
	+.026	+.027	+.027	+.028	+.028	+.029	+.029	+.030	+.030	+.031	+.031			

Barometer with Glass or Wooden Scale.

A	ttached nermom-	Barometer in English Inches.										
	eter, 'ahren- heit.	26	26.5	27	27.5	28	28.5	29	29.5	30	30.5	31
											7772	
	0	9 3/4	7-3100				4 1	504/19	1		Single.	
	21	+.024	+.024	+.025	+.025	+.026	+.026	+.027	+.027	+.028	+.028	+.028
	22	+.021	+.022	+.022	+.023	+.022	+.023	+.024	+.024	+.025	+.025	+.025
	23	+.019	+.019	+.020	+.020	+.020	+.021	+.021	+.021	+.022	+.022	+.023
	24	+.016	+.017	+.017	+.017	+.018	+.018	+.018	+.019	+.019	+.019	+.020
	25	+.014	+.014	+.014	+.015	+.015	+.015	+.016	+.016	+.016	+.016	+.017
	26	+.011	+.012	+.012	+.012	+.012	+.013	+.013	+.013	+.013	+.013	+.014
	27	+.009	+.009	+.009	+.009	+.010	+.010	+.010	+.010	+.010	+.011	+.011
	28	+.006	+.007	+.007	+.007	+.007	+.007	+.007	+.007	+.007	+.008	+.008
	29	+.004	+.004	+.004	+.004	+.004	+.004	+.004	+.005	+.005	+.005	+.002
	30	+.002	₩.002	+.002	T.002	T.002	7.002	T.002	T.002	7.002	7.002	T.002
6	0.1	001	001	001	001	001	001	001	001	001	001	001
	31 32	003	001	001	004	001	004	004	004	004	004	004
	33	006	004	004	006	006	007	007	007	007	007	007
	34	008	009	009	009	009	009	009	010	010	010	010
	35	011	011	011	012	012	012	012	012	013	013	013
6	30											5.04
	36	013	014	014	014	014	015	015	015	C15	016	016
	37	016	016	017	017	017	017	018	018	018	019	019
	38	018	019	019	019	020	020	020	021	021	022	022
	39	021	021	022	022	022	023	023	024	034	024	025
	40	023	024	024	025	025	026	026	026	027	027	028
					115.		1000				31.7	<b>HEAR 19</b>
	41	026	026	027	027	028	028	029	029	030	030	031
	42	028	029	029	030	030	031	032	032	033	033	034
	43	031	031	032	033	033	034	033	035	036	036	037
100	44	033	034	035	035	→036	036	036	038	038	039	040
	45	036	036	037	038	038	039	039	041	041	042	043
	46	038	039	040	040	041	042	042	043	044	045	046
	47	041	041	042	043	044	045	044	046	047	048	049
	48	043	044	045	046	047	047	047	049	050	051	051
	49	046	046	047	048	-049	050	050	052	053	054	054
	50	048	049	050	051	052	053	054	055	056	056	057
	WOLVE OF										15	
	51	051	052	053	054	055	055	056	057	058	059	060
	52	053	054	055	056	057	058	059	060	061	062	063
	53	056	057	058	059	060	061	062	063	064	065	066
	54	058	059	060	061	063	064	065	066	067	068	069
	55	061	062	063	064	065	066	068	069	070	071	072
	Ke	063	_064	_ 065	_ 067	-068	_ 060	-070	- 071	_ 079	- 074	- 075
	56		064 067	065 068	067 069		-069 -072		071	073	074	075
	57 58	065 068	069	071	072	071 073	074	073 076	074	076 078	077 080	078 081
	59	070	072	073	074	076	077	079	080	081	083	084
	60	073	074	076	077	079	080	-081		084	085	087
_	00	013	1 .014	1-1010	.011	.013	000	-001	000	004	000	.001

Barometer with Glass or Wooden Scale.

	DETUILEGET WITH CLASS OF 14 OCCUR SCORES										
Attached Thermom- eter,	mom-										
Fahren- heit.	26	26.5	27	27.5	28	28.5	29	29.5	30	30.5	31
61	075	077	078	080	081	083	084	086	087	088	090
62	078	079	081	082	084	085	087	088	090	091	093
63	080	082	083	085	086	088	090	091	093	094	096
64	083	084	086	088	089	091	092	094	096	097	099
65	085	087	089	090	092	093	095	097	098	100	102
66	088	089	091	093	094	096	098	100	101	103	104
67	090	092	094	095	097	099	101	102	104	106	108
68	093	094	096	098	100	102	103	105	107	109	110
69	095	097	099	101	102	104	106	108	110	112	113
70	098	099	101	103	105	107	109	111	113	114	116
71	100	102	104	106	108	110	112	114	115	117	119
72	103	105	106	108	110	112	114	116	118	120	122
73	105	107	109	111	113	115	117	119	121	123	125
74	107	110	112	114	116	118	120	122	124	126	128
75	110	112	114	116	118	121	123	125	127	129	131
76	112	115	117	119	121	123	125	128	130	132	134
77	115	117	119	121	124	126	128	130	133	135	137
78	117	120	122	124	126	129	131	133	135	138	140
79	120	122	124	127	129	131	134	136	138	141	143
80	122	125	127	129	132	134	136	139	141	143	146
01	_ 195	197	190	100	104	700	100	140	144	140	7.40
81 82	125 127	127 130	130 132	132 135	134 137	137 139	139	142 144	144 147	146	149
83	130	132	135	137	140	142	142 145	147	150	149 152	152 155
84	132	135	137	140	142	145	147	150	152	155	158
85	135	137	140	142	145	147	150	153	155	158	160
86	137	140	142	145	148	150	153	155	158	161	163
87	139	142	145	148	150	153	156	158	161	164	166
88	142	145	147	150	153	156	158	161	164	167	169
89	144	147	150	153	156	158	161	164	167	169	172
90	147	150	153	155	158	161	164	167	169	172	175
91	149	152	155	158	161	164	167	169	172	175	178
92	152	155	158	161	163	166	169	172	175	178	181
93	154	157	160	163	166	169		175		181	184
94	157	160	163	166	169	172		178	181	184	187
95	159	162	165	168	171	174	178	181	184	187	190
96	162	165	168	171	174	177	180	183	186	190	193
97	164	167	170	174	177	180	183	186	189	192	196
98	167	170	173	176	179	183	186	189	192	195	199
99	169	172	175	179	182	185	188	192	195	198	201
100	171	175	178	181	185	188	191	194	198	201	204

### XIX.

METRICAL BAROMETER.

## TABLE

FOR

# REDUCING TO THE FREEZING POINT THE BAROMETRICAL COLUMN,

MEASURED BY BRASS SCALES, EXTENDING FROM THE CISTERN TO
THE TOP; CALCULATED FROM 260 TO 865 MILLIMETRES,
AND FOR EACH DEGREE CENTIGRADE.
By M. T. Delcros.

THE RESERVE OF THE PARTY OF THE 一体上使在另

#### TABLE XIX.

This table has been calculated by using the following coefficients of dilatation:—
Brass, linear dilatation, from Laplace and Lavoisier for 100° C. = 0.0018782.

Mercury, dilatation in volume, from Dulong and Petit for 100° C. = 0.0180180.

Dilatation of the mercurial column for 100° C. . . . = 0.0161398.

Dilatation of the mercurial column for 1° C. . . . = 0.0001614.

Observed height reduced to freezing point,

 $H = h - h \ (0.0001614). \quad T = h - h \left(\frac{T}{6196}\right).$ 

The second term of this last formula is given by the table, when the temperature and the height h of the barometer are known; this correction must be *subtracted* om the observed height h, when the temperature is above freezing point; it is to be ided when the temperature is below zero, or freezing point.

This table allows the barometrical heights taken at the highest summits, and in the sepest mines, to be corrected.

Examples of Calculation.	
Barometer, observed height,	567.49
Temperature of the barometer, +12°.7.	
Second page, $\begin{cases} \text{for } 10.0 = 0.912 \\ \text{for } 2.0 = 0.182 \\ \text{for } 0.7 = 0.064 \end{cases}$	
Second page, $\begin{cases} \text{for } 2.0 = 0.182 \end{cases}$	
for $0.7 = 0.064$	
Total, $= \overline{1.158}$	
에 등 ::(B. C. C. )   [1] [2] [2] [2] [2] [2] [2] [2] [2] [2] [2	1.10
Subtractive correction,	<b>— 1.16</b>
Barometer at zero,	566.33
Barometer, observed height,	454.17
Temperature of the barometer, —7°.8.	
First page, $\begin{cases} \text{for } 7.0 = 0.514 \\ \text{for } 0.8 = 0.059 \end{cases}$	
Total — 0.572	1,550.9
Total, $= 0.573$	
Additive correction,	+0.57
Barometer at zero,	454.74

Height of the			like the	TEMPERA	ATURE CE	NTIGRADE			
Barome- ter.	10	2°	3°	4°	5°	6°	70	80	90
Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin
260	0.042	0.084	0.126	0.168	0.210	0.252	0.294	0.336	0.378
265	0.043	0.086	0.128	0.171	0.214	0.257	0.299	0.342	0.38
270	0.044	0.087	0.131	0.174	0.218	0.261	0.305	0.349	0.399
275	0.044	0.089	0.133	0.178	0.222	0.266	0.311	0.355	0.399
280	0.045	0.090	0.136	0.181	0.226	0.271	0.316	0.362	0.40
285	0.046	0.092	0.138	0.184	0.230	0.276	0.322	0.368	0.41
290	0.047	0.094	0.140	0.187	0.234	0.281	0.328	0.374	0.42
295	0.048	0.095	0.143	0.190	0.238	0.286	0.333	0.381	0.428
300	0.048	0.097	0.145	0.194	0.242	0.291	0.339	0.387	0.43
305	0.049	0.098	0.148	0.197	0.246	0.295	0.345	0.394	0.44
310	0.050	0.100	0.150	0.200	0.250	0.300	0.350	0.400	0.45
315	0.051	0.102	0.152	0.203	0.254	0.305	0.356	0.407	0.458
320	0.052	0.103	0.155	0.207	0.258	0.310	0.361	0.413	0.46
325	0.052	0.105	0.157	0.210	0.262	0.315	0.367	0.420	0.47
330	0.053	0.106	0.160	0.213	0.266	0.320	0.374	0.426	0.479
335	0.054	0.108	0.162	0.216	0.270	0.324	0.379	0.432	0.48
340	0.055	0.110	0.165	0.219	0.274	0.329	0.384	0.439	0.49
345	0.056	0.111	0.167	0.223	0.278	0.334	0.390	0.445	0.50
350	0.056	0.113	0.169	0.226	0.282	0.339	0.395	0.452	0.508
355	0.057	0.115	0.172	0.229	0.286	0.344	0.401	0.458	0.51
360	0.058	0.116	0.174	0.232	0.290	0.349	0.407	0.465	0.523
365	0.059	0.118	0.177	0.236	0.294	0.353	0.412	0.471	0.530
370	0.060	0.119	0.179	0.239	0.299	0.358	0.418	0.478	0.537
375	0.060	0.121	0.182	0.242	0.303	0.363	0.424	0.484	0.545
380	0.061	0.123	0.184	0.245	0.307	0.368	0.429	0.491	0.552
385	0.062	0.124	0.186	0.249	0.311	0.373	0.435	0.497	0.559
390	0.063	0.126	0.189	0.252	0.315	0.378	0.441	0.504	0.566
395	0.064	0.127	0.191	0.255	0.319	0.382	0.446	0.510	0.574
400	0.065	0.129	0.194	0.258	0.323	0.387	0.452	0.516	0.581
405	0.065	0.131	0.196	0.261	0.327	0.392	0.457	0.523	0.588
410	0.066	0.132	0.198	0.265	0.331	0.397	0.463	0.529	0.596
415	0.067	0.134	0.201	0.268	0.335	0.402	0.469	0.536	0.603
420	0.068	0.136	0.203	0.271	0.339	0.407	0.474	0.542	0.610
425	0.068	0.137	0.206	0.274	0.343	0.411	0.480	0.549	0.617
430	0.069	0.139	0.208	0.278	0.347	0.416	0.486	0.555	0.625
435	0.070	0.140	0.211	0.281	0.351	0.421	0.491	0.562	0.632
440	0.071	0.142	0.213	0.284	0.355	0.426	0.497	0.568	0.639
445	0.072	0.144	0.215	0.287	0.359	0.431	0.503	0.574	0.646
450	0.073	0.145	0.218	0.290	0.363	0.436	0.508	0.581	0.654
455	0.073	0 147	0.220	0.294	0.367	0.441	0.514	0.587	0.661
110	10	2°	'3°	40	50	6,	70	80	90

Height of the				I Bivit Bitch	101111 011	NTIGRADE.			
Barome- ter.	10	20	3°	40	50	60	70	80	9°
Millim.	Millim.	Millim.	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	Millir
460	0.0742	0.1485	0.2227	0.2970	0.371	0.445	0.520	0.594	0.66
465	0.0750	0.1501	0.2251	0.3002	0.375	0.450	0.525	0.600	0.67
470	0.0759	0.1517	0.2276	0.3034	0.379	0.455	0.531	0.607	0.68
475	0.0767	0.1533	0.2300	0.3066	0.383	0.460	0.537	0.613	0.69
480	0.0775	0.1549	0.2324	0.3099	0.387	0.465	0.542	0.620	0.69
485	0.0783	0.1565	0.2348	0.3131	0.391	0.470	0.548	0.626	0.70
490	0.0791	0.1582	0.2373	0.3163	0.395	0.474	0.554	0.633	0.71
495	0.0800	0.1598	0.2397	0.3195	0.399	0.479	0.559	0.639	0.71
500	0.0807	0.1614	0.2421	0.3228	0.403	0.484	0.565	0.646	0.72
505 ·	0.0815	0.1630	0.2445	0.3260	0.407	0.489	0.570	0.652	0.73
510	0.0823	0.1646	0.2469	0.3293	0.412	0.494	0.576	0.658	0.74
515	0.0831	0.1662	0.2493	0.3325	0.416	0.499	0.582	0.665	0.74
520	0.0839	0.1679	0.2518	0.3357	0.420	0.504	0.587	0.671	0.75
525	0.0847	0.1695	0.2542	0.3389	0.424	0.508	0.593	0.678	0.76
530	0.0855	0.1711	0.2566	0.3422	0.428	0.513	0.599	0.684	0.77
535	0.0863	0.1727	0.2590	0.3454	0.432	0.518	0.604	0.691	0.77
540	0.0872	0.1743	0.2615	0.3486	0.436	0.523	0.610	0.697	0.78
545	0.0879	0.1759	0.2639	0.3518	0.440	0.528	0.616	0.704	0.79
550	0.0888	0.1775	0.2663	0.3551	0.444	0.533	0.621	0.710	0.79
555	0.0896	0.1791	0.2687	0.3583	0.448	0.537	0.627	0.717	0.80
560	0.0904	0.1808	0.2712	0.3615	0.452	0.542	0.633	0.723	0.813
565	0.0912	0.1824	0.2736	0.3647	0.456	0.547	0.638	0.730	0.82
570	0.0920	0.1840	0.2760	0.3680	0.460	0.552	0.644	0.736	0.828
575	0.0928	0.1856	0.2784	0.3712	0.464	0.557	0.650	0.742	0.83
580	0.0936	0.1872	0.2808	0.3744	0.468	0.562	0.655	0.749	0.84
585	0.0944	0.1888	0.2833	0.3777	0.472	0.566	0.661	0.755	0.850
590	0.0952	0.1904	0.2857	0.3809	0.476	0.571	0.667	0.762	0.857
595	0.0960	0.1921	0.2881	0.3841	0.480	0.576	0.672	0.768	0.864
600	0.0968	0.1937	0.2905	0.3874	0.484	0.581	0.678	0.775	0.872
605	0.0976	0.1953	0.2929	0.3906	0.488	0.586	0.683	0.781	0.879
610	0.0985	0.1969	0.2954	0.3938	0.492	0.591	0.689	0.788	0.886
615	0.0993	0.1985	0.2978	0.3970	0.496	0.595	0.695	0.794	0.893
620	0.1001	0.2001	0.3002	0.4003	0.500	0.600	0.700	0.800	0.901
625	0.1009	0.2017	0.3026	0.4035	0.504	0.605	0.706	0.807	0.908
630	0.1017	0.2034	0.3050	0.4067	0.508	0.610	0.712	0.813	0.915
335	0.1025	0.2050	0.3074	0.4099	0.512	0.615	0.717	0.820	0.922
640	0.1033	0.2066	0.3099	0.4132	0.516	0.620	0.723	0.826	0.930
645	0.1041	0.2082	0.3123	0.4164	0.520	0.625	0.729	0.833	0.937
650	0.1049	0.2098	0.3147	0.4196	0.524	0.629	0.734	0.839	0.944
655	0.1057	0.2114	0.3172	0.4229	0.529	0.634	0.740	0.846	0.951
660	0.1065	0.2130	0.3196	0.4261	0.533	0.639	0.746	0.852	0.959
	10	2º	3°	40	<b>5</b> °	6°	70	80	90

Height				TEMPERA	TURE CEI	NTIGRADE.			J. steries
Height of the Barome- ter.	10	2°	3°	40	5°	<b>6</b> °	70	80	90
Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
665	0.1073	0.2146	0.3220	0.4293	0.537	0.644	0.751	0.859	0.966
670	0.1081	0.2163	0.3244	0.4326	0.541	0.649	0.757	0.865	0.973
675	0.1089	0.2179	0.3268	0.4358	0.545	0.654	0.763	0.871	0.980
680	0.1097	0.2195	0.3292	0.4390	0.549	0.658	0.768	0.878	0.988
685	0.1106	0.2211	0.3317	0.4423	0.553	0.663	0.774	0.884	0.995
690	0.1114	0.2227	0.3341	0.4455	0.557	0.668	0.780	0.891	1.002
695	0.1122	0.2233	0.3365	0.4487	0.561	0.673	0.785	0.897	1.010
700	0.1130	0.2260	0.3389	0.4520	0.565	0.678	0.791	0.904	1.017
705	0.1138	0.2276	0.3414	0.4552	0.569	0.683	0.797	0.910	1.024
710	0.1146	0.2292	0.3438	0.4584	0.573	0.688	0.802	0.917	1.031
715	0.1154	0.2308	0.3462	0.4616	0.577	0.691	0.808	0.923	1.039
720	0.1162	0.2324	0.3486	0.4648	0.581	0.697	0.813	0.930	1.046
725	0.1170	0.2340	0.3510	0.4680	0.585	0.702	0.819	0.936	1.053
730	0.1178	0.2356	0.3535	0.4713	0.589	0.707	0.825	0.943	1.060
735	0.1186	0.2372	0.3559	0.4745	0.593	0.712	0.830	0.949	1.068
740	0.1104	0.2389	0.3583	0.4777	0.597	0.717	0.836	0.955	1.075
745	0.1202	0.2405	0.3607	0.4809	0.601	0.721	0.842	0.962	1.082
750	0.1210	0.2421	0.3631	0.4842	0.605	0.726	0.847	0.968	1.089
755	0.1218	0.2437	0.3655	0.4874	0.609	0.731	0.853	0.975	1.097
760	0.1227	0.2453	0.3680	0.4906	0.613	0.736	0.859	0.981	1.104
765	0.1235	0.2469	0.3704	0.4939	0.617	0.741	0.864	0.988	1.111
770	0.1243	0.2486	0.3728	0.4971	0.621	0.746	0.870	0.994	1.118
775	0.1251	0.2502	0.3752	0.5003	0.625	0.750	0.876	1.001	1.126
780	0.1259	0.2518	0.3777	0.5036	0.629	0.755	0.881	1.007	1.133
785	0.1267	0.2534	0.3801	0.5068	0.633	0.760	0.888	1.014	1.140
790	0.1275	0.2550	0.3825	0.5100	0.637	0.765	0.893	1.020	1.148
795	0.1283	0.2566	0.3849	0.5132	0.641	0.770	0.898	1.026	1.155
800	0.1291	0.2582	0.3874	0.5165	0.646	0.775	0.904	1.033	1.162
805	0.1299	0.2598	0.3898	0.5197	0.650	0.780	0.909	1.039	1.169
810	0.1307	0.2615	0.3922	0.5230	0.654	0.784	0.915	1.046	1.177
815	0.1315	0.2621	0.3946	0.5262	0.658	0.789	0.921	1.052	1.184
820	0.1323	0.2647	0.3970	0.5294	0.662	0.794	0.926	1.059	1.191
825	0.1331	0.2653	0.3994	0.5326	0.666	0.799	0.932	1.065	1.198
830	0.1340	0.2679	0.4019	0.5358	0.670	0.804	0.938	1.072	1.206
835	0.1348	0.2695	0.4043	0.5391	0.674	0.809	0.943	1.078	1.213
840	0.1356	0.2712	0.4067	0.5423	0.678	0.813	0.949	1.085	1.220
845	0.1364	0.2728	0.4091	0.5455	0.682	0.818	0.955	1.091	1.227
850	0.1372	0.2744	0.4116	0.5488	0.686	0.823	0.960	1.097	1.235
855 860	0.1380	0.2760 0.2776	0.4140 0.4164	0.5520 0.5552	0.690	0.828 0.833	0.966	1.104	1.242 1.249
865	0.1396	0.2792	0.4188	0.5584	0.698	0.838	0.977	1.117	1.256
	10	20	3°						
		2	3	40	<b>5</b> °	6°	70	8°	90

### XX.

#### METRICAL BAROMETER.

## TABLE

FOR

# REDUCING TO THE FREEZING POINT THE BAROMETRICAL COLUMN,

MEASURED BY BRASS SCALES, EXTENDING FROM THE CISTERN TO THE TOP; CAL-CULATED FOR THE HEIGHTS BETWEEN 605 AND 800 MILLIMETRES, AND FOR EVERY TENTH OF A DEGREE, FROM 0° TO + AND - 35° CENTIGRADE. By M. T. Haeghens. A THAT SEE SEE SEE \* 10

#### TABLE XX.

This table has been calculated by using the same coefficients of dilatation as in the preceding table, viz.:—

Brass, linear dilatation, from Laplace and Lavoisier for 100°C. = 0.0018782. Mercury, dilatation in volume, from Dulong and Petit for 100°C. = 0.0180180.

Dilatation of the mercurial column for 100° C. . . . = 0.0161398.

Dilatation of the mercurial column for 1°C. . . . = 0.0001614.

This table, calculated for the reduction of long series of meteorological observations, gives immediately the value of the correction for each tenth of a degree up to 35° C. above, and down to 35° C. below, the freezing point, and for mercurial columns extending from 605 to 800 millimetres.

#### Examples of Calculation.

For finding the correction, seek in the horizontal column, headed barometer, at the head of the pages, the corresponding height of the barometer; it will be found, p. 31, barometer 755<sup>mm</sup>. (from 752.50 to 757.50); next seek in the first vertical column, containing the temperatures, 17°, follow then horizontally this line as far as the column of 8 tenths, and you find there 2.17 millimetres, which is the correction, or the quantity to be subtracted for reducing the observed height to zero. We have thus:—

If the temperature is below zero, the correction will be additive.

Centi- grade	ı			. 2 3	Tenths o	f Degrees.				
Degrees.	1		1	1	1		1		1	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19
2	0.20	0.21	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28
3	0.29	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38
4	0.39	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48
5	0.49	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58
6	0.59	0.60	0.61	0.62	0.63	0.63	0.64	0.65	0.66	0.67
7	0.68	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77
8	0.78	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87
9	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97
10	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.05	1.06
11	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16
12	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26
13	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36
14	1.37	1.38	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46
15	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55
16	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63	1.64	1.65
17	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75
18	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85
19	1.86	1.87	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94
20	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.04
21	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14
22	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24
23	2.25	2.26	2.27	2.28	2.29	2.29	2.30	2.31	2.32	2.33
24	2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43
25	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53
26	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63
27	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.71	2.72
28	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82
29	2.83	2.84	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.92
30	2.93	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02
31	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.12
32	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.19	3.20	3.21
33	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.30	3.31
34	3.32	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.40	3.41
35	3.42	3.43	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.51
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

	BAROMETER: 610 <sup>mm</sup> (from 607.51 to 612.50).										
Centigrade Degrees.					Tenths o	f Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim.	Millim.	Millím.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09	
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	
3	0.30	0.31	0.32	0.32	0.33	0.34	0.35	0.36	0.37	0.38	
4	0.39	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	
5	0.49	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	
	0.50	0.00	0.01	0.00	0.00	0.01					
6	0.59	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	
7	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78	
8	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	
9	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.96	0.97	
10	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	
11	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	
12	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	
13	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	
14	1.38	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	
15	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56	1.57	
10	1.58	1 50	1.50	1.00	1.01	1 00	1 00	100	1.05	1.00	
16	1.67	1.59	1.59 1.69	1.60	1.61	1.62	1.63	1.64	1.65	1.66	
17	1.77	1.68	1.79	1.70	1.71	1.72	1.73	1.74	1.75	1.76	
18	1.87			1.80	1.81	1.82	1.83	1.84	1.85	1.86	
19 20	1.97	1.88	1.89	1.90 2.00	1.91 2.01	1.92 2.02	1.93	1.94	1.95 2.05	1.96 2.06	
20	2.0	1.00	1.00	2.00	2.01	2.02	2.00	2.04	2.00	2.00	
21	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16	
22	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.23	2.24	2.25	
23	2.26	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35	
24	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45	
25	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.55	
26	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65	
27	2.66	2.67	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75	
28	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.75	
29	2.86	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94	
30	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.04	
31	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.12	3.13	3.14	
32	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23	3.24	
33	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32	3.33	3.34	
34	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.42	3.43	3.44	
35	3.45	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.53	3.54	
N/ St	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

		В	AROMI	ETER:	615 <sup>mm</sup>	(from	612.51	to 617.5	60).	
Centigrade Degrees.				- Water	Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29
3	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39
4	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49
5	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59
6	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.68
7	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78
8	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88
9	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98
10	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08
11	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18
12	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28
13	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38
14	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48
15	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.58
16	1.59	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68
17	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.78
18	1.79	1.80	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88
19	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98
20	1.99	2.00	2.01	2.01	2.02	2.03	2.04	2.05	2.06	2.07
21	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17
22	2.18	2.19	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27
23	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.37
24	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47
25	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57
26	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67
27	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77
28	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87
29	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97
30	2.98	2.99	3.00	3.01	3.02	3.03	3.04	3.05	3.06	3.07
31	3.08	3.09	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17
32	3.18	3.19	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27
33	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.36
34 35	3.37	3.38 3.48	3.39	3.40	3.41	3.42 3.52	3.43	3.44	3.45	3.46
	0.					100			III E E	
	<b>V.</b>	1.	2.	3.	4.	5.	6.	7.	8.	9.

	BAROMETER: 620 <sup>mm</sup> . (from 617.51 to 622.50)													
Centi- grade Degrees.		Tenths of Degrees.												
42	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim	Millim				
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09				
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19				
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29				
3	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39				
4	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49				
5	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59				
6	0.60	0:61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69				
7	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79				
8	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89				
9	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99				
10	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09				
11	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19				
12	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29				
13	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39				
14	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49				
15	1.50	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.58	1.59				
16	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.69				
17	1.70	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.78	1.79				
18	1.80	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.89				
19	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99				
20	2.00	2.01	2.02	2.03	2.04	2.05	2.06	2.07	2.08	2.09				
21	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19				
22	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29				
23	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.37	2.38	2.39				
24	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49				
25	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59				
26	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67	2.68	2.69				
27	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78	2.79				
28	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87	2.88	2.89				
29	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	2.99				
30	3.00	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09				
31	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.19				
32	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29				
33	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.37	3.38	3.39				
34	3.40	3.41	3.42	3.43	3.44	3.45	3.46	3.47	3.48	3.49				
35	3.50	3.51	3.52	3.53	3.54	3.55	3.56	3.57	3.58	3.59				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

Centigrade Degrees.  O. Millim. 0.000  1 0.10 2 0.20 3 0.30 4 0.40 5 0.50  6 0.61 7 0.71 8 0.81 9 0.91 10 1.01  11 1.11 12 1.21 13 1.31 14 1.41 15 1.51  16 1.61 17 1.71 18 1.82 19 1.92 20 2.02  21 2.12 2.22 2.32 2.32 2.4 2.42 2.5 2.52  26 2.62 27 2.72 28 2.82 2.93 30 3.03  31 3.13 32 3.23	В		AROME	TER:	625 <sup>mm</sup> ·	(from	622.51	to 627.5	50).	
Millim.   0.00		grade		- Various	Tenths o	f Degrees.				Alama's Santain Santain
0 0.00  1 0.10 2 0.20 3 0.30 4 0.40 5 0.50  6 0.61 7 0.71 8 0.81 9 0.91 10 1.01  11 1.11 12 1.21 13 1.31 14 1.41 15 1.51  16 1.61 17 1.71 18 1.82 19 1.92 20 2.02  21 2.12 22 2.22 23 2.32 24 2.42 25 2.52  26 2.62 27 2.72 28 2.82 29 2.93 30 3.03  31 3.13 32 3.23	1.	V.	2.	3.	4.	5.	6.	7.	8.	9.
2 0.20 3 0.30 4 0.40 5 0.50 6 0.61 7 0.71 8 0.81 9 0.91 10 1.01 11 1.11 12 1.21 13 1.31 14 1.41 15 1.51 16 1.61 17 1.71 18 1.82 19 1.92 20 2.02 21 2.12 22 2.22 23 2.32 24 2.42 25 2.52 26 2.62 27 2.72 28 2.82 29 2.93 30 3.03 31 3.13 32 3.23	Millim. 0.01	0	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim, 0.05	Millim. 0.06	Millim. 0.07	Millim 0.08	Millim. 0.09
2 0.20 3 0.30 4 0.40 5 0.50 6 0.61 7 0.71 8 0.81 9 0.91 10 1.01 11 1.11 12 1.21 13 1.31 14 1.41 15 1.51 16 1.61 17 1.71 18 1.82 19 1.92 20 2.02 21 2.12 22 2.22 23 2.32 24 2.42 25 2.52 26 2.62 27 2.72 28 2.82 29 2.93 30 3.03 31 3.13 32 3.23	0.11	1	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19
3   0.30 4   0.40 5   0.50 6   0.61 7   0.71 8   0.81 9   0.91 10   1.01 11   1.11 12   1.21 13   1.31 14   1.41 15   1.51 16   1.61 17   1.71 18   1.82 19   1.92 20   2.02 21   2.12 22   2.22 23   2.32 24   2.42 25   2.52 26   2.62 27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	0.21		0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29
4 0.40 5 0.50 6 0.61 7 0.71 8 0.81 9 0.91 10 1.01 11 1.11 12 1.21 13 1.31 14 1.41 15 1.51 16 1.61 17 1.71 18 1.82 19 1.92 20 2.02 21 2.12 22 2.22 23 2.32 24 2.42 25 2.52 26 2.62 27 2.72 28 2.82 29 2.93 30 3.03 31 3.13 32 3.23	0.31	11	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39
5   0.50 6   0.61 7   0.71 8   0.81 9   0.91 10   1.01 11   1.11 12   1.21 13   1.31 14   1.41 15   1.51 16   1.61 17   1.71 18   1.82 19   1.92 20   2.02 21   2.12 22   2.22 23   2.32 24   2.42 25   2.52 26   2.62 27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	0.41		0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49
7   0.71 8   0.81 9   0.91 10   1.01 11   1.11 12   1.21 13   1.31 14   1.41 15   1.51 16   1.61 17   1.71 18   1.82 19   1.92 20   2.02 21   2.12 22   2.22 23   2.32 24   2.42 25   2.52 26   2.62 27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	0.51	14	0.52	0.53	0.54	0.55	0.56	0.58	0.59	0.60
7   0.71 8   0.81 9   0.91 10   1.01 11   1.11 12   1.21 13   1.31 14   1.41 15   1.51 16   1.61 17   1.71 18   1.82 19   1.92 20   2.02 21   2.12 22   2.22 23   2.32 24   2.42 25   2.52 26   2.62 27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	0.62	6	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70
8   0.81 9   0.91 10   1.01 11   1.11 12   1.21 13   1.31 14   1.41 15   1.51 16   1.61 17   1.71 18   1.82 19   1.92 20   2.02 21   2.12 22   2.22 23   2.32 24   2.42 25   2.52 26   2.62 27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	0.72	- 11	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80
10	0.82		0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90
11	0.92	9	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00
12     1.21       13     1.31       14     1.41       15     1.51       16     1.61       17     1.71       18     1.82       19     1.92       20     2.02       21     2.12       22     2.22       23     2.32       24     2.42       25     2.52       26     2.62       27     2.72       28     2.82       29     2.93       30     3.03       31     3.13       32     3.23	1.02	10	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.10
13     1.31       14     1.41       15     1.61       17     1.71       18     1.82       19     1.92       20     2.02       21     2.12       22     2.22       23     2.32       24     2.42       25     2.52       26     2.62       27     2.72       28     2.82       29     2.93       30     3.03       31     3.13       32     3.23	1.12	11	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.20
14     1.41       15     1.51       16     1.61       17     1.71       18     1.82       19     1.92       20     2.02       21     2.12       22     2.22       23     2.32       24     2.42       25     2.52       26     2.62       27     2.72       28     2.82       29     2.93       30     3.03       31     3.13       32     3.23	1.22	12	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30
15   1.51 16   1.61 17   1.71 18   1.82 19   1.92 20   2.02 21   2.12 22   2.22 23   2.32 24   2.42 25   2.52 26   2.62 27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	1.32	13	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40
16	1.42	14	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50
17   1.71 18   1.82 19   1.92 20   2.02 21   2.12 22   2.22 23   2.32 24   2.42 25   2.52 26   2.62 27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	1.52	15	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60
18     1.82       19     1.92       20     2.02       21     2.12       22     2.32       24     2.42       25     2.52       26     2.62       27     2.72       28     2.82       29     2.93       30     3.03       31     3.13       32     3.23	1.62	16	1.63	1.64	1.65	1.66	1.67	1.68	1.69	1.70
19   1.92 20   2.02 21   2.12 22   2.22 23   2.32 24   2.42 25   2.52 26   2.62 27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	1.73	17	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81
20   2.02   2.12   2.12   2.22   2.32   2.42   2.52   2.52   2.62   2.72   2.72   2.82   2.93   3.03   3.03   3.13   3.13   3.2   3.23	1.83		1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91
21 2.12 22 2.22 23 2.32 24 2.42 25 2.52 26 2.62 27 2.72 28 2.82 29 2.93 30 3.03 31 3.13 32 3.23	1.93	11	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01
22   2.22 23   2.32 24   2.42 25   2.52 26   2.62 27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	2.03	20	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11
23   2.32 24   2.42 25   2.52 26   2.62 27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	2.13		2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21
24   2.42 25   2.52   2.52   26   2.62 27   2.72 28   2.82 29   2.93 30   3.03   3.13 32   3.23	2.23		2.24	2.25	2.26	2.27	2.28	2.29	2.30	2.31
25   2.52   262   27   2.72   28   2.82   29   2.93   30   3.03   31   3.13   32   3.23	2.33		2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41
26 2.62 27 2.72 28 2.82 29 2.93 30 3.03 31 3.13 32 3.23	2.43		2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51
27   2.72 28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	2.53	25	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61
28   2.82 29   2.93 30   3.03 31   3.13 32   3.23	2.63	11	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71
29 2.93 30 3.03 31 3.13 32 3.23	2.73	11	2.74	2.75	2.76	2.77	2.78	2.79	2.80	2.81
30 3.03 31 3.13 32 3.23	2.83	- 11	2.84	2.85	2.87	2.88	2.89	2.90	2.91	2.92
32 3.23	2.94 3.04		2.95 3.05	2.96 3.06	2.97 3.07	2.98 3.08	2.99 3.09	3.00 3.10	3.01	3.02
32 3.23	0.11	91						Family 1		
The state of the s	3.14		3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22
22 1 2 22	3.24	33	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32
33 3.33 34 3.43	3.44		3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.42
35 3.53	3.54		3.55	3.46 3.56	3.47 3.57	3.48 3.58	3.49 3.59	3.50 3.60	3.51 3.61	3.52 3.62
0.	1.	0.00	2.	3.	4.	5.	6.	7.	8.	9.

BAROMETER: 630<sup>mm.</sup> (from 627.51 to 632.50).

Centigrade

Degrees.					Tenths of Degrees.						
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim	
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09	
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40	
4	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	
5	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	
6	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	
7	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80	
8	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90	
9	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01	
10	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11	
11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21	
12	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31	
13	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.41	
14	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.52	
15	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62	
16	1.63	1.64	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	
17	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81	1.82	
18	1.83	1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91	1.92	
19	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02	
20	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.13	
21	2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	
22	2.24	2.25	2.26	2.27	2.28	2.29	2.30	2.31	2.32	2.33	
23	2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43	
24	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53	
25	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	
26	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.73	2.74	
27	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	
28	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94	
29	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.04	
30	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.12	3.13	3.14	
31	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23	3.24	
32	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32	3.34	3.35	
33	3.36	3.37	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45	
34	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.53	3.54	3.55	
35	3.56	3.57	3.58	3.59	3.60	3.61	3.62	3.63	3.64	3.65	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

		В.	AROMI	ETER:	635 <sup>mm</sup> .	(from	632.51	to 637.5	50).	
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim.	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim.
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19
2	0.20	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40
4	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50
5	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60
6	0.61	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71
7	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81
8	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91
9	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01
10	1.02	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12
11	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22
12	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32
13	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.41	1.42
14	1.43	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53
15	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63
16	1.64	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73
17	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83
18	1.84	1.86	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94
19	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.04
20	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14
21	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24
22	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35
23	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45
24	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.55
25	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65
26	2.66	2.67	2.69	2.70	2.71	2.72	2.73	2.74	2.75	2.76
27	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86
28	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96
29	2.97 3.07	2.98 3.08	2.99 3.10	3.00	3.01	3.02	3.03	3.04	3.05	3.06
	0.01	9.00	9.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17
31	3.18	3.19	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27
32	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.37
33	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45	3.46	3.47
34 35	3.48 3.59	3.49	3.51 3.61	3.52 3.62	3.53	3.54	3.55 3.65	3.56	3.57	3.58 3.68
	0.	1.	2.	3.	4.	5.	ME I			
			2.	0.	4.	0.	6.	7.	8.	9.

BAROMETER: 640<sup>mm</sup> (from 637.51 to 642.50). Centigrade Degrees. Tenths of Degrees. 0. 1. 2. 3. 4. 5. 6. 7. 9. 8. Millim. Millim. Millim. Millim. Millim. Millim. Millim, Millim, Millim. Millim. 0.00 0.02 0.03 0.01 0 0.04 0.05 0.06 0.07 0.08 0.09 1 0.10 0.11 0.12 0.13 0.14 0.15 0.17 0.19 0.20 0.18 2 0.21 0.22 0.23 0.24 0.25 0.26 0.27 0.28 0.29 0.30 0.38 3 0.31 0.32 0.33 0.34 0.35 0.36 0.37 0.39 0.40 4 0.41 0.42 0.43 0.44 0.45 0.46 0.48 0.50 0.49 0.51 0.52 0.53 0.54 0.55 0.56 0.57 0.58 5 0.59 0.60 0.61 0.62 0.63 0.64 6 0.65 0.66 0.67 0.68 0.69 0.70 0.71 0.72 0.73 0.74 0.75 0.76 7 0.77 0.78 0.80 0.81 0.82 0.83 0.84 0.85 0.86 0.87 0.88 8 0.89 0.90 0.91 0.92 0.93 0.94 0.95 9 0.96 0.97 0.98 0.99 1.00 1.01 1.02 1.03 1.05 1.08 10 1.04 1.06 1.07 1.09 1.11 1.12 1.13 11 1.14 1.15 1.16 1.17 1.18 1.19 1.20 1.21 1.22 1.23 12 1.24 1.25 1.26 1.27 1.28 1.29 1.30 1.31 1.32 1.33 13 1.34 1.35 1.36 1.37 1.38 1.39 1.40 1.42 1.43 1.44 1.45 1.46 1.47 14 1.48 1.49 1.50 1.51 1.52 1.53 1.54 15 1.55 1.56 1.57 1.58 1.60 1.59 1.61 1.62 1.63 1.64 1.65 1.66 1.67 1.68 16 1.69 1.70 1.71 1.72 1.74 1.75 1.76 1.81 17 1.77 1.78 1.79 1.80 1.82 1.83 1.84 1.85 18 1.86 1.87 1.88 1.89 1.90 1.91 1.92 1.93 1.94 1.95 1.96 1.97 1.98 19 1.99 2.00 2.01 2.02 2.03 2.05 2.06 20 2.07 2.08 2.09 2.10 2.11 2.12 2.16 2.13 2.14 2.15 21 2.17 2.18 2.19 2.20 2.21 2.22 2.23 2.24 2.25 2.26 22 2.27 2.28 2.29 2.30 2.31 2.32 2.33 2.34 2.36 2.37 23 2.38 2.39 2.40 2.41 2.42 2.43 2.44 2.45 2.46 2.47 2.50 24 2.48 2.49 2.51 2.52 2.53 2.54 2.55 2.56 2.57 2.64 25 2.58 2.59 2.60 2.61 2.62 2.63 2.65 2.66 2.68 26 2.69 2.70 2.71 2.72 2.73 2.74 2.75 2.76 2.77 2.78 27 2.79 2.80 2.81 2.82 2.83 2.84 2.85 2.86 2.87 2.88 28 2.89 2.90 2.91 2.92 2.93 2.94 2.95 2.96 2.97 2.99 29 3.00 3.01 3.02 3.03 3.04 3.05 3.06 3.07 3.08 3.09 30 3.10 3.11 3.12 3.13 3.14 3.15 3.16 3.17 3.18 3.19 3.22 31 3.20 3.21 3.23 3.24 3.25 3.26 3.27 3.28 3.30 3.32 3.33 3.34 32 3.31 3.35 3.36 3.37 3.38 3.39 3.40 33 3.41 3.42 3.43 3.44 3.45 3.46 3.47 3.48 3.49 3.50 34 3.51 3.52 3.53 3.54 3.55 3.56 3.58 3.57 3.59 3.60 3.62 3.63 3.64 3.65 3.66 35 3.67 3.68 3.69 3.70 3.71 1. 2. 3. 0. 4. 5. 6. 7. 8. 9.

BAROMETER: 645<sup>mm</sup>. (from 642.51 to 647.50).

Centigrade Degrees

Tenths of Degrees

grade Degrees.	Tenths of Degrees.											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim,	Millim.	Millim		
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09		
1	0.10	0.11	0.12	0.14	0.15	0.16	0.17	0.18	0.19	0.20		
2	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30		
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.39	0.40	0.41		
4	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51		
5	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61		
6	0.62	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72		
7	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82		
8	0.83	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93		
9	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03		
10	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13		
11	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24		
12	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34		
13	1.35	1.36	1.37	1.38	1.39	1.41	1.42	1.43	1.44	1.45		
14	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55		
15	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63	1.64	1.66		
16	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76		
17	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85	1.86		
18	1.87	1.88	1.89	1.91	1.92	1.93	1.94	1.95	1.96	1.97		
19	1.98	1.99	2.00	2.01	2.02	2.03	2.04	2.05	2.06	2.07		
20	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.17	2.18		
21	2.19	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28		
22	2.29	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.37	2.38		
23	2.39	2.40	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49		
24	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59		
25	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67	2.69	2.70		
26	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.80		
27	2.51	2.82	2.83	2.84	2.85	2.86	2.87	2.88	2.89	2.90		
28	2.9:	2.93	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01		
29	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10	3.11		
30	3.12	3.13	3.14	3.15	3.16	3.18	3.19	3.20	3.21	3.22		
31	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32		
32	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.42		
33	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.53		
34	3.54	3.55	3.56	3.57	3.58	3.59	3.60	3.61	3.62	3.63		
35	3.64	3.65	3.66	3.67	3.68	3.69	3.70	3.71	3.72	3.73		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

		В	AROMI	ETER:	650 <sup>mm</sup> .	(from	647.51	to 652.5	0).	
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° 0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim 0.09
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30
3	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.41
4	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51
5	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62
6	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72
7	0.73	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82	0.83
8	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93
9	0.94	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04
10	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14
11	1.15	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25
12	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35
13	1.36	1.37	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46
14	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56
15	1.57	1.58	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67
16	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76	1.77
17	1.78	1.79	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88
18	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98
19	1.99	2.00	2.01	2.03	2.04	2.05	2.06	2.07	2.08	2.09
20	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19
21	2.20	2.21	2.22	2.24	2.25	2.26	2.27	2.28	2.29	2.30
22	2.31	2.32	2.33	2.34	2.35	2.36	2.37	2.38	2.39	2.40
23	2.41	2.42	2.43	2.44	2.46	2.47	2.48	2.49	2.50	2.51
24	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61
25	2.62	2.63	2.64	2.65	2.67	2.68	2.69	2.70	2.71	2.72
26	2.73	2.84	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82
27	2.83	2.84	2.85	2.86	2.88	2.89	2.90	2.91	2.92	2.93
28	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3.03
29	3.04	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.13	3.14
30	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23	3.24
31	3.25	3.26	3.27	3.28	3.29	3.31	3.32	3.33	3.34	3.35
32	3.36	3.37	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45
33	3.46	3.47	3.48	3.49	3.50	3.52	3.53	3.54	3.55	3.56
34	3.57	3.58	3.59	3.60	3.61	3.62	3.63	3.64	3.65	3.66
35	3.67	3.68	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.77
NAME OF THE PERSON NAME OF THE P	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

BAROMETER: 655<sup>mm</sup>. (from 652.51 to 657.50).

Centigrade Degrees.										
8	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.									
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.09	0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.28	0.29	0.30	0.31
3	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.41
4	0.42	0.43	0.44	0.46	0.47	0.48	0.49	0.50	0.51	0.52
5	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62
6	0.63	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.73
7	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.83	0.84
8	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.94
9	0.95	0.96	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05
10	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15
11	1.16	1.17	1.18	1.20	1.21	1.22	1.23	1.24	1.25	1.26
12	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36
13	1.37	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47
14	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.57	1.58
15	1.59	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1,67	1.68
16	1.69	1.70	1.71	1.72	1.73	1.74	1.76	1.77	1.78	1.79
17	1.80	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.89
18	1.90	1.91	1.92	1.94	1.95	1.96	1.97	1.98	1.99	2.00
19	2.01	2.02	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10
20	2.11	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21
21	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29	2.31	2.32
22	2.33	2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41	2.42
23	2.43	2.44	2.45	2.46	2.47	2.48	2.50	2.51	2.52	2.53
24	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63
25	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.73	2.74
26	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84
27	2.85	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95
28	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.05	3.06
29	3.07	3.08	3.09	3.10	3.11	3.12	3.13	3.14	3.15	3.16
30	3.17	3.18	3.19	3.20	3.21	3.22	3.24	3.25	3.26	3.27
.31	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.37
32	3.38	3.39	3.40	3.42	3.43	3.44	3.45	3.46	3.47	3.48
33	3.49	3.50	3.51	3.52	3.53	3.54	3.55	3.56	3.57	3.58
34	3.59	3.61	3.62	3.63	3.64	3.65	3.66	3.67	3.68	3.69
35	3.70	3.71	3.72	3.73	3.74	3.75	3.76	3.77	3.79	3.80
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

	BAROMETER: 660 <sup>mm</sup> . (from 657.51 to 662.50).												
Centi- grade Degrees.		Tenths of Degrees.											
d	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
° 0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim.	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim 0.10			
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20			
2	0.21	0.22	0.23	0.25	0.26	0.27	0.28	0.29	0.30	0.31			
3	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.41	0.42			
4	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52			
5	0.53	0.54	0.55	0.57	0.58	. 0.59	0.60	0.61	0.62	0.63			
6	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.74			
7	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82	0.83	0.84			
8	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94	0.95			
9	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.06			
10	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16			
11	1.17	1.18	1.19	1.20	1.21	1.23	1.24	1.25	1.26	1.27			
12	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37			
13	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48			
14	1.49	1.50	1.51	1.52	1.53	1.55	1.56	1.57	1.58	1.59			
15	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.69			
16	1.70	1.72	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80			
17	1.81	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91			
18	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01			
19	2.02	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12			
20	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.21	2.22	2.23			
21	2.24	2.25	2.26	2.27	2.28	2.29	2.30	2.31	2.32	2.33			
22	2.34	2.35	2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.44			
23	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.53	2.54	2.55			
24	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65			
25	2.66	2.67	2.68	2.70	2.71	2.72	2.73	2.74	2.75	2.76			
26	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.86	2.87			
27	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97			
28	2.98	2.99	3.00	3.02	3.03	3.04	3.05	3.06	3.07	3.08			
29	3.09	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.19			
30	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29			
31	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40			
32	3.41	3.42	3.43	3.44	3.45	3.46	3.47	3.48	3.49	3.51			
33	3.52	3.53	3.54	3.55	3.56	3.57	3.58	3.59	3.60	3.61			
34	3.62 3.73	3.63 3.74	3.64	3.65 3.76	3.66 3.77	3.68	3.69	3.70	3.71	3.72 3.82			
		d-name						400					
MELL	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

	BAROMETER: 665 <sup>mm</sup> . (from 662.51 to 667.50).									
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim, 0.00	Millim. 0.01	Millim. 0.02	Millim.	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim.	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.31
3	0.32	0.33	0.34	0.35	0.37	0.38	0.39	0.40	0.41	0.42
4	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.51	0.52	0.53
5	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63
6	0.64	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.73	0.74
7	0.75	0.76	0.77	0.78	0.79	0.81	0.82	0.83	0.84	0.85
8	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.95	0.96
9	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06
10	1.07	1.08	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17
11	1.18	1.19	1.20	1.21	1.22	1.23	1.25	1.26	1.27	1.28
12	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.39
13	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49
14	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58	1.59	1.60
15	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.69	1.70	1.71
16	1.72	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81
17	1.83	1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91	1.92
18	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.02	2.03
19	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.13	2.14
20	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24
21	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35
22	2.36	2.37	2.38	2.39	2.40	2.42	2.43	2.44	2.45	2.46
23	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.56	2.57
24	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67
25	2.68	2.69	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78
26	2.79	2.80	2.81	2.82	2.83	2.84	2.86	2.87	2.88	2.89
27	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	3.00
28	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10
29	3.11	3.12	3.13	3.15	3.16	3.17	3.18	3.19	3.20	3.21
30	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.30	3.31	3.32
31	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.42
32	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.53
33 34	3.54	3.55	3.56	3.57	3.59	3.60	3.61	3.62	3.63	3.64
35	3.76	3.66 3.77	3.67 3.78	3.68 3.79	3.69 3.80	3.70 3.81	3.71	3.72	3.74	3.75 3.85
- 6	0.	1.	2.	3.						
	0.		20	9.	4.	5.	6.	7.	8.	9.

Centi-					Tentha	f Degrees.				Trans
grade Degrees.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millin								
0	0.00	0.01	0.02	0.03	0.04	0.05	0.07	0.08	0.09	0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.20	0.21
2	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.31
3	0.32	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.41	0.42
4	0.43	0.44	0.45	0.47	0.48	0.49	0.50	0.51	0.52	0.53
5	0.54	0.55	0.56	0.57	0.58	0.60	0.61	0.62	0.63	0.64
6	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.73	0.74	0.75
7	0.76	0.77	0.78	0.79	0.80	0.70	0.71	0.73	0.74	0.75
8	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96
9	0.97	0.98	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07
10	1.08	1.09	1.10	1.11	1.13	1.14	1.15	1.16	1.17	1.18
	A Video	L. Davis	1001	1000	The same	100	6304		1	1 15
11	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.27	1.28	1.29
12	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.40
13	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50
14 15	1.62	1.53 1.63	1.54 1.64	1.55 1.66	1.56 1.67	1.57 1.68	1.58 1.69	1.59 1.70	1.60	1.61
10	1.02	1.03	1.04	1.00	1.07	1.00	1.05	1.10	1.71	1.72
16	1.73	1.74	1.75	1.76	1.77	1.78	1.80	1.81	1.82	1.83
17	1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91	1.92	1.94
18	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.04
19	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15
20	2.16	2.17	2.18	2.20	2.21	2.22	2.23	2.24	2.25	2.26
21	2.27	2.28	2.29	2.30	2.31	2.33	2.34	2.35	2.36	2.37
22	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.46	2.47	2.48
23	2.49	2.50	2.51	2.52	2.53	2,54	2.55	2.56	2.57	2.59
24	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67	2.68	2.69
25	2.70	2.71	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.80
00	207	0.00	0.00	000	2.00	0.00	0.00	0.00	0.00	2.04
26 27	2.81	2.82	2.83	2.84	2.86 2.96	2.87	2.88 2.99	2.89 3.00	2.90 3.01	2.91
28	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.02 3.13
29	3.14	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23
30	3.24	3.26	3.27	3.28	3.29	3.30	3.31	3.32	3.33	3.34
7	1	The same	1 3500	01.00	1	T Mary	S ASSESSED	S. Barrell	1	
31	3.35	3.36	3.37	3.39	3.40	3.41	3.42	3.43	3.44	3.45
32	3.46	3.47	3.48	3.49	3.50	3.52	3.53	3.54	3.55	3.56
33	3.57	3.58	3.59	3.60	3.61	3.62	3.63	3.64	3.66	3.67
34	3.68 3.79	3.69 3.80	3.70 3.81	3.71 3.82	3.72	3.73	3.74	3.75	3.76	3 77
99	0.19	3.00	3.01	3.02	3.83	3.84	3.85	3.86	3.87	3.88
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

BAROMETER:	675mm.	(from	672.51 to	677.50).

		В.	AROME	TER:	675 <sup>mm</sup> ·	(from 6	572.51 t	o 677.50	0).	The t
Centigrade Degrees.				in section of	Tenths o	f Degrees.				Service of the servic
1	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.03	0.04	0.05	0.07	0.08	0.09	0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.31	0.32
3	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.41	0.42
4	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53
5	0.54	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63	0.64
6	0.65	0.66	0.68	0.69	0.70	0.71	0.72	0.73	0.74	0.75
7	0.76	0.77	0.78	0.80	0.81	0.82	0.83	0.84	0.85	0.86
8	0.87	0.88	0.89	0.90	0.92	0.93	0.94	0.95	0.96	0.97
9	0.98	0.99	1.00	1.01	1.02	1.03	1.05	1.06	1.07	1.08
10	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.17	1.18	1.19
11	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.29	1.30
12	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.41
13	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51
14	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62
15	1.63	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73
16	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.82	1.83	1.84
17	1.85	1.86	1.87	1.88	1.90	1.91	1.92	1.93	1.94	1.95
18	1.96	1.97	1.98	1.99	2.00	2.02	2.03	2.04	2.05	2.06
19	2.07	2.08	2.09	2.10	2.11	2.12	2.14	2.15	2.16	2.17
20	2.18	2.19	2.20	2.21	2.22	2.23	2.24	2.26	2.27	2.28
21	2.29	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.38	2.39
22	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49
23	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59	2.60
24	2.61	2.63	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71
25	2.72	2.73	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82
26	2.83	2.84	2.85	2.87	2.88	2.89	2.90	2.91	2.92	2.93
27	2.94	2.95	2.96	2.97	2.99	3.00	3.01	3.02	3.03	3.04
28	3.05	3.06	3.07	3.08	3.09	3.10	3.12	3.13	3.14	3.15
29	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.24	3.25	3.26
30	3.27	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.36	3.37
31	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45	3.46	3.48
32	3.49	3.50	3.51	3.52	3.53	3.54	3.55	3.56	3.57	3.58
33	3.60	3.61	3.62	3.63	3.64	3.65	3.66	3.67	3.68	3.69
34	3.70	3.72	3.73	3.74	3.75	3.76	3.77	3.78	3.79	3.80
35	3.81	3.82	3.83	3.85	3.86	3.87	3.88	3.89	3.90	3.91
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER:	680 <sup>mm</sup> .	(from 6	677.51 t	o 682.50	0).	
Centigrade Degrees.				44 mal	Tenths of	Degrees.				The second
18	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
0	0.00	0.01	0.02	0.03	0.04	0.05	0.07	0.08	0.09	0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.26	0.27	0.29	0.30	0.31	0.32
3	0.33	0.34	0.35	0.36	0.37	0.38	0.40	0.41	0.42	0.43
4	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.52	0.53	0.54
5	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.63	0.64	0.65
6	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.74	0.75	0.76
7	0.00	0.78	0.79	0.80	0.81	0.82	0.72	0.85	0.86	0.87
8	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.97	0.98
9	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.08	1.09
10	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.19	1.20
L.	7 07	7.00	1.00	104	1.05	1.00	1 00	1.00	1.00	1 01
11	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.30	1.31
12	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.42
13	1.43	1.44	1.45 1.56	1.46	1.47	1.48	1.49	1.50	1.51	1.53
14 15	1.54	1.55 1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.75
16	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85
17	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96
18	1.98	1.99	2.00	2.01	2.02	2.03	2.04	2.05	2.06	2.07
19	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17	2.18
20	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29
21	2.30	2.32	2.33	2.34	2.35	2.36	2.37	2.38	2.39	2.40
22	2.41	2.43	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51
23	2.52	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62
24	2.63	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.72	2.73
25	2.74	2.75	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84
26	2.85	2.86	2.88	2.89	2,90	2.91	2.92	2.93	2.94	2.95
27	2.96	2.97	2.99	3.00	3.01	3.02	3.03	3.04	3.05	3.06
28	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17
29	3.18	3.19	3.20	3.22	3.23	3.24	3.25	3.26	3.27	3.28
30	3.29	3.30	3.31	3.33	3.34	3.35	3.36	3.37	3.38	3.39
21	3.40	3.41	3.42	3.44	3.45	3.46	3.47	3.48	3.49	3.50
31 32	3.40	3.41	3.53	3.54	3.56	3.57	3.58	3.59	3.60	3.61
33	3.62	3.63	3.64	3.65	3.67	3.68	3.69	3.70	3.71	3.72
34	3.73	3.74	3.75	3.76	3.78	3.79	3.80	3.81	3.82	3.83
35	3.84	3.85	3.86	3.87	3.89	3.90	3.91	3.92	3.93	3.94
301	0		0	9	-		-	- Py	-	-
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER:	685 <sup>mm</sup> .	(from	682.51 t	o 687.5	0).	
Centigrade Degrees.				See and	Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim. 0.10
			4,							
1	0.11	0.12	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.27	0.28	0.29	0.30	0.31	0.32
3	0.33	0.34	0.35	0.36	0.38	0.39	0.40	0.41	0.42	0.43
4	0.44	0.45	0.46	0.48	0.49	0.50	0.51	0.52	0.53	0.54
5	0.55	0.56	0.57	0.59	0.60	0.61	0.62	0.63	0.64	0.65
6	0.66	0.67	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76
7	0.77	0.78	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87
8	0.88	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98
9	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09
10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.21
11	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.32
12	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.42	1.43
13	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.53	1.54
14	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65
15	1.66	1.67	1.68	1.69	. 1.70	1.71	1.72	1.74	1.75	1.76
16	1.77	1.78	1.79	1.80	1.81	1.82	1.84	1.85	1.86	1.87
17	1.88	1.89	1.90	1.91	1.92	1.93	1.95	1.96	1.97	1.98
18	1.99	2.00	2.01	2.02	2.03	2.05	2.06	2.07	2.08	2.09
19	2.10	2.11	2.12	2.13	2.14	2.16	2.17	2.18	2.19	2.20
20	2.21	2.22	2.23	2.24	2.26	2.27	2.28	2.29	2.30	2.31
21	2.32	2.33	2.34	2.35	2.37	2.38	2.39	2.40	2.41	2.42
22	2.43	2.44	2.45	2.47	2.48	2.49	2.50	2.51	2.52	2.53
23	2.54	2.55	2.56	2.58	2.59	2.60	2.61	2.62	2.63	2.64
24	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75
25	2.76	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86
26	2.87	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2,96	2.97
27	2.99	3.00	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08
28	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.20
29	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.31
30	3.32	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.41	3.42
31	3.43	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.52	3.53
32	3.54	3.55	3.56	3.57	3.58	3.59	3.60	3.62	3.63	3.64
33	3.65	3.66	3.67	3.68	3.69	3.70	3.71	3.73	3.74	3.75
34	3.76	3.77	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86
35	3.87	3.88	3.89	3.90	3.91	3.92	3.94	3.95	3.96	3.97
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

	BAROMETER: 690 <sup>mm</sup> (from 687.51 to 692.50).										
Centigrade Degrees.					Tenths o	f Degrees.					
100	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim, 0.00	Millim. 0.01	Millim.	Millim, 0.03	Millim. 0.04	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10	
1	0.11	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.21	
2	0.22	0.23	0.25	0.26	0.27	0.28	0.29	0.30	0.31	0.32	
3	0.33	0.35	0.36	0.37	0.38	0.39	0.40	0.41	0.42	0.43	
4	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53	0.55	
5	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63	0.65	0.66	
May	0.00	0.00	0.00	0.70	0	0.50	0.71	0	0.70	0	
6	0.67	0.68	0.69	0.70	0.71	0.72	0.74	0.75	0.76	0.77	
8	0.78	0.79	0.80	0.81	0.82	0.84	0.85	0.97	0.98	0.88	
9	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.08	1.09	1.10	
10	1.11	1.12	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21	
10						-					
11	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.33	
12	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.41	1.43	1.44	
13	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.53	1.54	1.55	
14	1.56	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65	1.66	
15	1.67	1.68	1.69	1.70	1.72	1.73	1.74	1.75	1.76	1.77	
		Samuel	Miles I			100					
16	1.78	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.87	1.88	
17	1.89	1.90	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99	
18	2.00	2.02	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10	
19	2.12 2.23	2.13	2.14	2.15	2.16	2.17 2.28	2.18	2.19	2.21 2.32	2.22	
20	2.20	2.24	2.20	2.20	2.21	2.20	2.23	2.01	2.02	2.00	
21	2.34	2.35	2.36	2.37	2.38	2.39	2.41	2.42	2.43	2.44	
22	2.45	2.46	2.47	2.48	2.49	2.51	2.52	2.53	2.54	2.55	
23	2.56	2.57	2.58	2.59	2.61	2.62	2.63	2.64	2.65	2.66	
24	2.67	2.68	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77	
25	2.78	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87	2.88	
1000	N.S. W			V. Marie	U L					5 1	
26	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	3.00	
27	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.10	3.11	
28	3.12	3.13	3.14	3.15	3.16	3.17	3.19	3.20	3.21	3.22	
29 30	3.23	3.24	3.25 3.36	3.26	3.39	3.29 3.40	3.41	3.42	3.32	3.33	
30	0.04	0.00	0.00	0.01	0.00	0.40	0.11	0.12	0.10	0.11	
31	3.45	3.46	3.47	3,49	3.50	3.51	3.52	3.53	3.54	3.55	
32	3.56	3.57	3.59	3.60	3.61	3.62	3.63	3.64	3.65	3.66	
33	3.68	3.69	3.70	3.71	3.72	3.73	3.74	3.75	3.76	3.78	
34	3.79	3.80	3.81	3.82	3.83	3.84	3.85	3.86	3.88	3.89	
35	3.90	3.91	3.92	3.93	3.94	3.95	3.96	3.98	3.99	4.00	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

		В.	AROMI	ETER:	695 <sup>mm</sup> .	(from 6	592.51 t	o 697.50	0).	
Centigrade Degrees.				(1012)	Tenths of	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.03	0.04	0.06	0.07	0.08	0.09	0.10
1	0.11	0.12	0.13	0.15	0.16	0.17	0.18	0.19	0.20	0.21
2	0.22	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.31	0.33
3	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.42	0.43	0.44
4	0.45	0.46	0.47	0.48	0.49	0.50	0.52	0.53	0.54	0.55
5	0.56	0.57	0.58	0.59	0.61	0.62	0.63	0.64	0.65	0.66
					THE STATE OF	the last		diversity.		
6	0.67	0.68	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77
7	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.89
8	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.98	0.99	1.00
9	1.01	1.02	1.03	1.04	1.05	1.07	1.08	1.09	1.10	1.11
10	1.12	1.15	1.14	1.10	1.17	1.18	1.19	1.20	1.21	1.22
11	1.23	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33
12	1.35	1.36	1.37	1.38	1.39	1.40	1.41	1.42	1.44	1.45
13	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.54	1.55	1.56
14	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65	1.66	1.67
15	1.68	1.69	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.78
		. 6		1		100				
16	1.79	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.90
17	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.99	2.00	2.01
18	2.02	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.12
19	2.13	2.14	2.15	2.16	2.18	2.19	2.20	2.21	2.22	2.23
20	2.24	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34
21	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2,43	2.45	2.46
22	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.55	2.56	2.57
23	2.58	2.59	2.60	2.61	2.62	2.64	2.65	2.66	2.67	2.68
24	2.69	2.70	2.71	2.73	2.74	2.75	2.76	2.77	2.78	2.79
25	2.80	2.82	2.83	2.84	2.85	2.86	2.87	2.88	2.89	2.91
20	/ TIL	1	1			Local			1	
26	2.92	2.93	2.94	2.95	2.96	2.97	2.98	3.00	3.01	3.02
27	3.03	3.04	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.13
28 29	3.14	3.15	3.16	3.17	3.19	3.20	3.21	3.22	3.23	3.24
30	3.25	3.26 3.38	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35
00	0.01	9.90	3.39	3.40	3.41	3.42	3.43	3.44	3.45	3.47
31	3.48	3.49	3.50	3.51	3.52	3.53	3.54	3.56	3.57	3.58
32	3.59	3.60	3.61	3.62	3.63	3.65	3.66	3.67	3.68	3.69
33	3.70	3.71	3.72	3.74	3.75	3.76	3.77	3.78	3.79	3.80
34	3.81	3.83	3.84	3.85	3.86	3.87	3.88	3.89	3.90	3.91
35	3.93	3.94	3.95	3.96	3.97	3.98	3.99	4.00	4.02	4.03
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER:	700 <sup>mm</sup> .	(from	69 <b>7</b> .51 t	o 702.5	0).	
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim. 0.07	Millim.	Millim.	Millim. 0.10
		0.12	0.74	0.15	0.70	0.10	0.10	0.70	0.00	0.02
1	0.11	0.12	0.14	0.15	0.16	0.17	0.18	0.19	0.20	0.21
2 3	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.31	0.32	0.33
4	0.45	0.46	0.47	0.49	0.50	0.51	0.52	0.53	0.54	0.55
5	0.56	0.58	0.59	0.60	0.61	0.62	0.63	0.64	0.66	0.67
		0.00				1				
6	0.68	0.69	0.70	0.71	0.72	0.73	0.75	0.76	0.77	0.78
7	0.79	0.80	0.81	0.82	0.84	0.85	0.86	0.87	0.88	0.89
8	0.90	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.01
9	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.10	1.11	1.12
10	1.13	1.14	1.15	1.16	1.17	1.19	1.20	1.21	1.22	1.23
	1.24	1.25	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34
11 12	1.36	1.37	1.38	1.39	1.40	1.41	1.42	1.43	1.45	1.46
13	1.47	1.48	1.49	1.50	1.51	1.53	1.54	1.55	1.56	1.57
14	1.58	1.59	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68
15	1.69	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.79	1.80
A STATE		Name of the	e Life				CYLINE I			
16	1.81	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91
17	1.92	1.93	1.94	1.95	1.97	1.98	1.99	2.00	2.01	2.02
18	2.03	2.04	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.14
19	2.15	2.16	2.17 2.28	2.18 2.29	2.19	2.20	2.21 2.33	2.23	2.24	2.25
20	2.20	2.21	2.20	2.29	2.50	2.52	2.00	2.04	2.50	2.36
21	2.37	2.38	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47
22	2.49	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.58	2.59
23	2.60	2.61	2.62	2.63	2.64	2.66	2.67	2.68	2.69	2.70
24	2.71	2.72	2.73	2.75	2.76	2.77	2.78	2.79	2.80	2.81
25	2.82	2.84	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.93
26	2.94	2.95	2.96	2.97	2.98	2.99	3.01	3.02	3.03	3.04
27	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15
28	3.16	3.17	3.19	3.20	3.21	3.22	3.23	3.24	3.25	3.27
29	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.36	3.37	3.38
30	3.39	3.40	3.41	3.42	3.43	3.45	3.46	3.47	3.48	3.49
31	3.50	3.51	3.52	3.54	3.55	3.56	3.57	3.58	3.59	3.60
32	3.62	3.63	3.64	3.65	3.66	3.67	3.68	3.69	3.71	3.72
33	3.73	3.74	3.75	3.76	3.77	3.78	3.80	3.81	3.82	3.83
34	3.84	3.85	3.86	3.88	3.89	3.90	3.91	3.92	3.93	3.94
35	3.95	3.97	3.98	3.99	4.00	4.01	4.02	4.03	4.04	4.06
N. (19. )	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
					101					
C					101					

	BAROMETER: 705 <sup>mm.</sup> (from 702.51 to 707.50).											
Centigrade Degrees.				********	Tenths o	ns of Degrees.						
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.		
0	0.00	0.01	0.02	0.03	0.05	0.06	0.07	0.08	0.09	0.10		
1	0.11	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20	0.22		
2	0.23	0.24	0.25	0.26	0.27	0.28	0.30	0.31	0.32	0 33		
3	0.34	0.35	0.36	0.38	0.39	0.40	0.41	0.42	0.43	0.44		
4	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53	0.55	0.56		
5	0.57	0.58	0.59	0.60	0.61	0.63	0.64	0.65	0.66	0.67		
TO STATE	0.00			0.00	100							
6	0.68	0.69	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.79		
7	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.88	0.89	0.90		
8 9	0.91	0.92	0.93 1.05	0.94	0.96 1.07	0.97	0.98	0.99	1.00	1.01		
10	1.14	1.15	1.16	1.17	1.18	1.19	1.21	1.22	1.12	1.13		
10	2,27	1.10	1.10		1.10	1.10	1.21	1.22	1.20	1.24		
11	1.25	1.26	1.27	1.29	1.30	1.31	1.32	1.33	1.34	1.35		
12	1.37	1.38	1.39	1.40	1.41	1.42	1.43	1.45	1.46	1.47		
13	1.48	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58		
14	1.59	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.70		
15	1.71	1.72	1.73	1.74	1.75	1.76	1.78	1.79	1.80	1.81		
			38 48			Server a						
16	1.82	1.83	1.84	1.85	1.87	1.88	1.89	1.90	1.91	1.92		
17	1.93 2.05	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.03	2.04		
18	2.16	2.06	2.07	2.08	2.09	2.11	2.12	2.13	2.14	2.15		
19 20	2.28	2.29	2.30	2.31	2.21 2.32	2.33	2.34	2.36	2.25	2.26 2.38		
20		2.23	2.00	2.01	2.02	2.00	2.07	2.00	2.01	2.00		
21	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47	2.48	2.49		
22	2.50	2.51	2.53	2.54	2.55	2.56	2.57	2.58	2.59	2.61		
23	2.62	2.63	2.64	2.65	2.66	2.67	2.69	2.70	2.71	2.72		
24	2.73	2.74	2.75	2.77	2.78	2.79	2.80	2.81	2.82	2.83		
25	2.84	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.94	2.95		
-	9.00	0.07	9.60	0.00		0.00	0.00					
26	2.96	2.97	2.98	2.99	3.00	3.02	3.03	3.04	3.05	3.06		
27 28	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17		
29	3.30	3.31	3.21 3.32	3.22	3.23 3.35	3.24	3.25 3.37	3.27 3.38	3.28 3.39	3.29		
30	3.41	3.42	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.52		
					0.10		0.40		0.50	0.02		
31	3.53	3.54	3.55	3.56	3.57	3.58	3.60	3.61	3.62	3.63		
32	3.64	3.65	3.66	3.68	3.69	3.70	3.71	3.72	3.73	3.74		
33	3.75	3.77	3.78	3.79	3.80	3.81	3.82	3.83	3.85	3.86		
34	3.87	3.88	3.89	3.90	3.91	3.93	3.94	3.95	3.96	3.97		
35	3.98	3.99	4.01	4.02	4.03	4.04	4.05	4.06	4.07	4.08		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

	BAROMETER: 710 <sup>mm</sup> (from 707.51 to 712.50).												
Centigrade Degrees.	Tenths of Degrees.												
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
0	Millim.	Millim.	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim			
0	0.00	0.01	0.02	0.03	0.05	0.06	0.07	0.08	0.09	0.10			
1	0.11	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.21	0.22			
2	0.23	0.24	0.25	0.26	0.28	0.29	0.30	0.31	0.32	0.33			
3	0.34	0.36	0.37	0.38	0.39	0.40	0.41	0.42	0.44	0.45			
4	0.46	0.47	0.48	0.49	0.50	0.52	0.53	0.54	0.55	0.56			
5	0.57	0.58	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.68			
6	0.69	0.70	0.71	0.72	0.73	0.74	0.76	0.77	0.78	0.79			
7	0.80	0.81	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.91			
8	0.92	0.93	0.94	0.95	0.96	0.97	0.99	1.00	1.01	1.02			
9	1.03	1.04	1.05	1.07	1.08	1.09	1.10	1.11	1.12	1.13			
10	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.23	1.24	1.25			
11	1.26	1.27	1.28	1.29	1.31	1.32	1.33	1.34	1.35	1.36			
12	1.38	1.39	1.40	1.41	1.42	1.43	1.44	1.46	1.47	1.48			
13	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58	1.59			
14	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.70	1.71			
15	1.72	1.73	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.82			
16	1.83	1.84	1.86	1.87	1.88	1.89	1.90	1.91	1.93	1.94			
17	1.95	1.96	1.97	1.98	1.99	2.01	2.02	2.03	2.04	2.05			
18	2.06	2.07	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.17			
19	2.18	2.19	2.20	2.21	2.22	2.23	2.25	2.26	2.27	2.28			
20	2.29	2.30	2.31	2.33	2.34	2.35	2.36	2.37	2.38	2.40			
21	2.41	2.42	2.43	2.44	2.45	2.46	2.48	2.49	2.50	2.51			
22	2.52	2.53	2.54	2.56	2.57	2.58	2.59	2.60	2.61	2.62			
23	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.72	2.73	2.74			
24	2.75	2.76	2.77	2.78	2.80	2.81	2.82	2.83	2.84	2.85			
25	2.86	2.88	2.89	2.90	2.91	2.92	2.93	2.95	2.96	2.97			
26	2.98	2.99	3.00	3.01	3.03	3.04	3.05	3,06	3.07	3.08			
27	3.09	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.19	3.20			
28	3.21	3.22	3.23	3.24	3.25	3.27	3.28	3.29	3.30	3.31			
29	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.43			
30	3.44	3.45	3.46	3.47	3.48	3.50	3.51	3.52	3.53	3.54			
31	3.55	3.56	3.58	3.59	3.60	3.61	3.62	3.63	3.64	3.66			
32	3.67	3.68	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.77			
33	3.78	3.79	3.80	3.82	3.83	3.84	3.85	3.86	3.87	3.88			
34	3.90	3.91	3.92	3.93	3.94	3.95	3.96	3.98	3.99	4.00			
35	4.01	4.02	4.03	4.05	4.06	4.07	4.08	4.09	4.10	4.11			

2.

3.

BAROMETER: 715mm. (from 712.51 to 717.50). Centi-Tenths of Degrees. grade Degrees 2. 3. 4. 5. 6. 7. 8. 9. 0. 1. Millim. Millim Millim. Millim. Millim. Millim. Millim. Millim. Millim. Millim. 0.06 0 0.00 0.01 0.02 0.04 0.05 0.07 0.08 0.09 0.10 0.12 0.13 0.14 0.15 0.16 0.17 0.18 0.20 0.21 0.22 1 0.27 0.28 0.29 0.23 0.24 0.25 0.30 0.31 0.32 0.33 2 0.35 0.36 0.37 0.38 0.39 0.40 0.42 0.43 0.44 0.45 3 0.52 0.50 0.51 0.53 4 0.46 0.47 0.48 0.54 0.55 0.57 0.59 0.60 0.61 0.62 0.63 0.65 0.66 5 0.58 0.67 0.68 0.72 0.73 0.74 0.75 0.76 0.78 6 0.69 0.70 0.77 0.80 0.82 0.83 0.84 0.85 0.87 0.88 0.89 0.90 0.91 7 0.81 0.95 0.96 0.97 0.98 0.99 8 0.92 0.93 1.00 1.02 1.03 1.06 1.07 1.08 1.10 1.11 1.12 1.13 9 1.04 1.05 1.14 1.18 1.19 1.20 1.21 1.22 1.23 1.25 1.17 1.26 10 1.15 1.33 1.32 11 1.27 1.28 1.29 1.30 1.34 1.35 1.36 1.37 12 1.38 1.40 1.41 1.42 1.43 1.44 1.45 1.47 1.48 1.49 13 1.50 1.51 1.52 1.53 1.55 1.56 1.57 1.58 1.59 1.60 14 1.62 1.63 1.64 1.65 1.66 1.67 1.68 1.70 1.71 1.72 1.78 1.79 1.80 15 1.73 1.74 1.75 1.77 1.81 1.82 1.83 1.88 1.89 1.90 1.85 1.86 1.87 1.92 1.93 1.94 1.95 16 1.96 1.97 1.98 2.00 2.01 2.02 2.03 2.04 2.05 2.07 17 2.08 2.09 2.10 2.11 2.12 2.13 2.15 2.16 2.17 2.18 18 2.19 2.20 2.22 2.23 2.24 2.25 2.26 2.27 2.28 2.30 19 20 2.32 2.33 2.34 2.35 2.37 2.38 2.39 2.31 2.40 2.41 21 2.42 2.43 2.45 2.46 2.47 2.48 2.49 2.50 2.52 2.53 22 2.54 2.55 2.56 2.57 2.58 2.60 2.61 2.62 2.63 2.64 23 2.65 2.67 2.68 2.69 2.70 2.71 2.72 2.74 2.75 2.76 2.78 2.80 2.82 2.83 24 2.77 2.79 2.84 2.85 2.86 2.87 25 2.89 2.90 2.91 2.92 2.93 2.94 2.95 2.97 2.98 2.99 26 3.00 3.01 3.02 3.04 3.05 3.06 3.07 3.08 3.09 3.10 27 3.16 3.12 3.13 3.14 3.15 3.17 3.19 3.20 3.21 3.22 28 3.23 3.24 3.25 3.28 3.29 3.27 3.30 3.31 3.32 3.34 29 3.35 3.36 3.37 3.38 3.39 3.40 3.42 3.43 3.44 3.45 30 3.46 3.47 3.49 3.50 3.51 3.52 3.53 3.54 3.55 3.57 31 3.58 3.59 3.60 3.61 3.62 3.64 3.65 3.66 3.67 3.68 32 3.69 3.70 3.72 3.73 3.74 3.75 3.76 3.77 3.79 3.80 33 3.81 3.82 3.83 3.84 3.85 3.87 3.90 3.91 3.88 3.89 34 3.92 3.94 3.95 3.96 3.97 3.98 3.99 4.00 4.02 4.03 35 4.04 4.05 4.06 4.07 4.09 4.10 4.11 4.12 4.13 4.14 0. 1. 2. 3. 5. 6. 7. 8. 9.

BAROMETER: 720<sup>mm.</sup> (from 717.51 to 722.50).

Centigrade Degrees

Tenths of Degrees.

Degrees.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim								
0	0.00	0.01	0.02	0.03	0.05	0.06	0.07	0.08	0.09	0.10
1	0.12	0.13	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22
2	0.23	0.24	0.26	0.27	0.28	0.29	0.30	0.31	0.33	0.34
3	0.35	0.36	0.37	0.38	0.40	0.41	0.42	0.43	0.44	0.45
4	0.46	0.48	0.49	0.50	0.51	0.52	0.53	0.55	0.56	0.57
5	0.58	0.59	0.60	0.62	0.63	0.64	0.65	0.66	0.67	0.69
6	0.70	0.71	0.72	0.73	0.74	0.76	0.77	0.78	0.79	0.80
7	0.81	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.91	0.92
8	0.93	0.94	0.95	0.96	0.98	0.99	1.00	1.01	1.02	1.03
9	1.05	1.06	1.07	1.08	1.09	1.10	1.12	1.13	1.14	1.15
10	1.16	1.17.	1.19	1,20	1.21	1.22	1.23	1.24	1.26	1.27
11	1.28	1.29	1.30	1.31	1.32	1.34	1.35	1.36	1.37	1.38
12	1.39	1.41	1.42	1.43	1.44	1.45	1.46	1.48	1.49	1.50
13	1.51	1.52	1.53	1.55	1.56	1.57	1.58	1.59	1.60	1.62
14	1.63	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.73
15	1.74	1.75	1.77	1.78	1.79	1.80	1.81	1.82	1.84	1.85
16	1.86	1.87	1.88	1.89	1.91	1.92	1.93	1.94	1.95	1.96
17	1.98	1.99	2.00	2.01	2.02	2.03	2.05	2.06	2.07	2.08
18	2.09	2.10	2.11	2.13	2.14	2.15	2.16	2.17	2.18	2.20
19	2.21	2.22	2.23	2.24	2.25	2.27	2.28	2.29	2.30	2.31
20	2.32	2.34	2.35	2.36	2.37	2.38	2.39	2.41	2.42	2.43
21	2.44	2.45	2.46	2.48	2.49	2.50	2.51	2.52	2.53	2.54
22	2.56	2.57	2.58	2.59	2.60	2.61	2.63	2.64	2.65	2.66
23	2.67	2.68	2.70	2.71	2.72	2.73	2.74	2.75	2.77	2.78
24	2.79	2.80	2.81	2.82	2.84	2.85	2.86	2.87	2.88	2.89
25	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.99	3.00	3.01
26	3.02	3.03	3.04	3.06	3.07	3.08	3.09	3.10	3.11	3.13
27	3.14	3.15	3.16	3.17	3.18	3.20	3.21	3.22	3.23	3.24
28	3.25	3.27	3.28	3.29	3.30	3.31	3.32	3.34	3.35	3.36
29	3.37	3.38	3.39	3.40	3.42	3.43	3.44	3.45	3.46	3.47
30	3.49	3.50	3.51	3.52	3.53	3.54	3.56	3.57	3.58	3.59
31	3.60	3.61	3.63	3.64	3.65	3.66	3.67	3.68	3.70	3.71
32	3.72	3.73	3.74	3.75	3.77	3.78	3.79	3.80	3.81	3.82
33	3.83	3.85	3.86	3.87	3.88	3.89	3.90	3.92	3.93	3.94
34	3.95	3.96	3.97	3.99	4.00	4.01	4.02	4.03	4.04	4.06
35	4.07	4.08	4.09	4.10	4.11	4.13	4.14	4.15	4.16	4.17
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centi- grade egrees.	Tenths of Degrees,											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Milli		
°	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	, 0.09	0.1		
1	0.12	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.2		
2	0.23	0.25	0.26	0.27	0.28	0.29	0.30	0.32	0.33	0.8		
3	0.35	0.36	0.37	0.39	0.40	0.41	0.42	0.43	0.44	0.4		
4	0.47	0.48	0.49	0.50	0.51	0.53	0.54	0.55	0.56	0.8		
5	0.59	0.60	0.61	0.62	0.63	0.64	0.66	0.67	0.68	0.6		
6	0.70	0.71	0.73	0.74	0.75	0.76	0.77	0.78	0.80	0.8		
7	0.82	0.83	0.84	0.85	0.87	0.88	0.89	0.90	0.91	0.9		
8	0.94	0.95	0.96	0.97	0.98	0.99	1.01	1.02	1.03	1.0		
9	1.05	1.06	1.08	1.09	1.10	1.11	1.12	1.14	1.15	1.1		
10	1.17	1.18	1.19	1.21	1.22	1.23	1.24	1.25	1.26	1.2		
11	1.29	1.30	1.31	1.32	1.33	1.35	1.36	1.37	1.38	1.3		
12	1.40	1.42	1.43	1.44	1.45	1.46	1.47	1.49	1.50	1.5		
13	1.52	1.53	1.54	1.56	1.57	1.58	1.59	1.60	1.61	1.6		
14	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.73	1.7		
15	1.76	1.77	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.8		
16	1.87	1.88	1.90	1.91	1.92	1.93	1.94	1.95	1.97	1.9		
17	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07	2.08	2.0		
18	2.11	2.12	2.13	2.14	2.15	2.16	2.18	2.19	2.20	2.2		
19 20	2.22 2.34	2.23	2.25	2.26 2.38	2.27	2.28	2.29	2.31 2.42	2.32 2.43	2.3		
	9.40	0.48	0.40	0.40	0.00	1	0.50	0.53				
21	2.46	2.47	2.48	2.49	2.50	2.52	2.53	2.54	2.55	2.5		
22 23	2.69	2.70	2.71	2.61 2.73	2.62	2.63	2.64	2.66	2.67 2.78	2.6		
24	2.81	2.82	2.83	2.73	2.74	2.75	2.88	2.89	2.78	2.9		
25	2.93	2.94	2.95	2.96	2.97	2.98	3.00	3.01	3.02	3.0		
26	3.04	3.05	3.07	3.08	3.09	3.10	3.11	3.12	3.14	3.1		
27	3.16	3.17	3.18	3.19	3.21	3.22	3.23	3.24	3.25	3.2		
28	3.28	3.29	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.3		
29	3.39	3.41	3.42	3.43	3.44	3.45	3.46	3.49	3.49	3.5		
30	3.51	3.52	3.53	3.55	3.56	3.57	3.58	3.59	3.60	3.6		
31	3.63	3.64	3.65	3.66	3.67	3.69	3.70	3.71	3.72	3.7		
32	3.74	3.76	3.77	3.78	3.79	3.80	3.81	3.83	3.84	3.8		
33	3.86	3.87	3.88	3.90	3.91	3.92	3.93	3.94	3.96	3.9		
34	3.98	3.99	4.00	4.01	4.03	4.04	4.05	4.06	4.07	4.0		
35	4.10	4.11	4.12	4.13	4.14	4.15	4.17	4.18	4.19	4.2		
166	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

		(partire				Sayer:				
		В.	AROMI	ETER:	730 <sup>mm</sup> .	(from	727.51 t	o 732.5	0).	
				#40 VE						
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.09	0.11
200	0.10	0.10	074	0.15	0.10	0.10	0.10	0.00	0.01	0.00
1 2	0.12	0.13 0.25	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.22
3	0.35	0.37	0.38	0.39	0.40	0.41	0.42	0.44	0.45	0.46
4	0.47	0.48	0.49	0.51	0.52	0.53	0.54	0.55	0.57	0.58
5	0.59	0.60	0.61	0.62	0.64	0.65	0.66	0.67	0.68	0.70
			The same			Miles			15	1
6	0.71	0.72	0.73	0.74	0.75	0.77	0.78	0.79	0.80	0.81
7	0.82	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93
8	0.94	0.95	0.97	0.98	0.99	1.00	1.01	1.03	1.04	1.05
9	1.06	1.07	1.08	1.10	1.11	1.12	1.13	1.14	1.15	1.17
10	1.18	1.19	1.20	1.21	1.23	1.24	1.25	1.26	1.27	1.28
11	1.30	1.31	1.32	1.33	1.34	1.35	1.37	1.38	1.39	1.40
12	1.41	1.43	1.44	1.45	1.46	1.47	1.48	1.50	1.51	1.52
13	1.53	1.54	1.56	1.57	1.58	1.59	1.60	1.61	1.63	1.64
14	1.65	1.66	1.67	1.68	1.70	1.71	1.72	1.73	1.74	1.76
15	1.77	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.86	1.87
U PAR				1 - 70		100			2 17	1989/19
16	1.89	1.90	1.91	1.92	1.93	1.94	1.96	1.97	1.98	1.99
17	2.00	2.01	2.03	2.04	2.05	2.06	2.07	2.09	2.10	2.11
18	2.12	2.13	2.14	2.16	2.17	2.18	2.19	2.20	2.22	2.23
19	2.24	2.25	2.26	2.27	2.29	2.30	2.31	2.32	2.33	2.34
20	2.36	2.37	2.38	2.39	2.40	2.42	2.43	2.44	2.45	2.46
91	2.47	9 40	9 50	9 51	0 50	0 50	954	9 50	0 57	0.50
21 22	2.59	2.49	2.50 2.62	2.51 2.63	2.52	2.53 2.65	2.54 2.66	2.56	2.57	2.58
23	2.71	2.72	2.73	2.75	2.76	2.77	2.78	2.79	2.80	2.82
24	2.83	2.84	2.85	2.86	2.87	2.89	2.90	2.91	2.92	2.93
25	2.95	2.96	2.97	2.98	2.99	3.01	3.02	3.03	3.04	3.05
W. S.					Fig. 1	12 15 1		Name and		TO THE
26	3.06	3.08	3.09	3.10	3.11	3.12	3.13	3.15	3.16	3.17
27	3.18	3.19	3.20	3.22	3.23	3.24	3.25	3.26	3.28	3.29
28	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.41
29	3.42	3.43	3.44	3.45	3.46	3.48	3.49	3.50	3.51	3.52
30	3.53	3.55	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64
31	3.65	3.66	3.68	3.69	3.70	3.71	3 72	9 79	0 84	0.50
32	3.77	3.78	3.79	3.81	3.82	3.83	3.84	3.73	3.75 3.86	3.76
33	3.89	3.90	3.91	3.92	3.94	3.95	3.96	3.97	3.98	3.88
34	4.01	4.02	4.03	4.04	4.05	4.06	4.07	4.09	4.10	4.11
35	4.12	4.14	4.15	4.16	4.17	4.18	4.19	4.21	4.22	4.23
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	BAROMETER: 735 <sup>mm.</sup> (from 732.51 to 757.50).									
Centigrade Degrees.	Tenths of Degrees.											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.		
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.09	0.11		
1	0.12	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.21	0.23		
2	0.24	0.25	0.26	0.27	0.28	0.30	0.31	0.32	0.33	0.34		
3	0.36	0.37	0.38	0.39	0.40	0.42	0.43	0.44	0.45	0.46		
4	0.47	0.49	0.50	0.51	0.52	0.53	0.55	0.56	0.57	0.58		
5	0.59	0.61	0.62	0.63	0.64	0.65	0.66	0.68	0.69	0.70		
		line.			0 70	0	0.00	0 =0	0.00	0.00		
6	0.71	0.72	0.74	0.75	0.76	0.77	0.78	0.79	0.81	0.82		
7	0.83	0.84	0.85	0.87	1.00	0.89	1.02	0.91	1.04	0.94		
8	1.07	0.96 1.08	1.09	1.10	1.12	1.13	1.14	1.15	1.16	1.17		
9	1.19	1.20	1.21	1.22	1.23	1.25	1.26	1.27	1.28	1.29		
10	1.15	1.20	1.21		1.20	1.20	1.20		1.20			
11	1.30	1.32	1.33	1.34	1.35	1.36	1.37	1.39	1.40	1.41		
12	1.42	1.44	1.45	1.46	1.47	1.48	1.49	1.51	1.52	1.53		
13	1.54	1.55	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65		
14	1.66	1.67	1.69	1.70	1.71	1.72	1.73	1.74	1.76	1.77		
15	1.78	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.87	1.89		
				18		7	al P			1 - 15 8		
16	1.90	1.91	1.92	1.93	1.95	1.96	1.97	1.98	1.99	2.00		
17	2.02	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.12		
18	2.14	2.15	2.16	2.17	2.18	2.19	2.21	2.22	2.23	2.24		
19	2.25	2.27	2.28	2.29	2.30	2.31	2.33	2.34	2.35	2.36		
20	2.37	2.38	2.40	2.41	2.42	2.43	4.44	2.40	2.41	4.40		
21	2.49	2.50	2.51	2.53	2.54	2.55	2.56	2.57	2.59	2.60		
22	2.61	2.62	2.63	2.65	2.66	2.67	2.68	2.69	2.70	2.72		
23	2.73	2.74	2.75	2.76	2.78	2.79	2.80	2.81	2.82	2.84		
24	2.85	2.86	2.87	2.88	2.89	2.91	2.92	2.93	2.94	2.95		
25	2.97	2.98	2.99	3.00	3.01	3.03	3.04	3.05	3.06	3.07		
26	3.08	3.10	3.11	3.12	3.13	3.14	3.16	3.17	3.18	3.19		
27	3.20	3.21	3.23	3.24	3.25	3.26	3.27	3.29	3.30	3.31		
28	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40	3.42	3.43		
29	3.44	3.45	3.46	3.48	3.49	3.50	3.51	3.52	3.54	3.55		
30	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64	3.65	3.67		
31	3.68	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.77	3.78		
32	3.80	3.81	3.82	3.83	3.84	3.86	3.87	3.88	3.89	3.90		
33	3.91	3.93	3.94	3.95	3.96	3.97	3.99	4.00	4.01	4.02		
34	4.03	3.05	4.06	4.07	4.08	4.09	4.10	4.12	4.13	4.14		
35	4.15	4.16	4.18	4.19	4.20	4.21	4.22	4.24	4.25	4.26		
1000	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

### BAROMETER: 740<sup>mm</sup> (from 737.51 to 742.50).

Centigrade Degrees

#### Tenths of Degrees.

Degrees.			1200	_71,=154	Tentile 0	i Degrees.				
	0.	L	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
° 0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.09	0.11
1	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.21	0.23
2	0.24	0.25	0.26	0.27	0.29	0.30	0.31	0.32	0.33	0.35
3	0.36	0.37	0.38	0.39	0.41	0.42	0.43	0.44	0.45	0.47
4	0.48	0.49	0.50	0.51	0.53	0.54	0.55	0.56	0.57	0.59
5	0.60	0.61	0.62	0.63	0.64	0.66	0.67	0.68	0.69	0.70
6	0.72	0.73	0.74	0.75	0.76	0.78	0.79	0.80	0.81	0.82
7	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94
8	0.96	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05	1.06
9	1.07	1.09	1.10	1.11	1.12	1.13	1.15	1.16	1.17	1.18
10	1.19	1.21	1.22	1.23	1.24	1.25	1.27	1.28	1.29	1.30
11	1.31	1.33	1.34	1.35	1.36	1.37	1.39	1.40	1.41	1.42
12	1.43	1.45	1.46	1.47	1.48	1.49	1.50	1.52	1.53	1.54
13	1.55	1.56	1.58	1.59	1.60	1.61	1.62	1.64	1.65	1.66
14	1.67	1.68	1.70	1.71	1.72	1.73	1.74	1.76	1.77	1.78
15	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90
16	1.91	1.92	1.93	1.95	1.96	1.97	1.98	1.99	2.01	2.02
17	2.03	2.04	2.05	2.07	2.08	2.09	2.10	2.11	2.13	2.14
18	2.15	2.16	2.17	2.19	2.20	2.21	2.22	2.23	2.25	2.26
19	2.27	2.28	2.29	2.31	2.32	2.33	2.34	2.35	2.36	2.38
20	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47	2.48	2.50
21	2.51	2.52	2.53	2.54	2.56	2.57	2.58	2.59	2.60	2.62
22	2.63	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.74
23	2.75	2.76	2.77	2.78	2.79	2.81	2.82	2.83	2.84	2.85
24	2.87	2.88	2.89	2.90	2.91	2.93	2.94	2.95	2.96	2.97
25	2.99	3.00	3.01	3.02	3.03	3.05	3.06	3.07	3.08	3.09
26	3.11	3.12	3.13	3.14	3.15	3.17	3.18	3.19	3.20	3.21
27	3.22	3.24	3.25	3.26	3.27	3.28	3.30	3.31	3.32	3.33
28	3.34	3.36	3.37	3.38	3.39	3.40	3.42	3.43	3.44	3.45
29	3.46	3.48	3.49	3.50	3.51	3.52	3.54	3.55	3.56	3.57
30	3.58	3.60	3.61	3.62	3.63	3.64	3.65	3.67	3.68	3.69
31	3.70	3.71	3.73	3.74	3.75	3.76	3.77	3.79	3.80	3.81
32	3.82	3.83	3.85	3.86	3.87	3.88	3.89	3.91	3.92	3.93
33	3.94	3.95	3.97	3.98	3.99	4.00	4.01	4.02	4.04	4.05
34	4.06	4.07	4.08	4.10	4.11	4.12	4.13	4.14	4.16	4.17
35	4.18	4.19	4.20	4.22	4.23	4.24	4.25	4.26	4.28	4.29
- High	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER:	745 <sup>mm</sup> .	(from 7	42.51 t	o 747.50	0).	
Centigrade Degrees.					Tenths of	Degrees.				
	0.	1	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.10	0.11
1	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.22	0.23
2	0.24	0.25	0.26	0.28	0.29	0.30	0.31	0.32	0.34	0.35
3	0.36	0.37	0.38	0.40	0.41	0.42	0.43	0.44	0.46	0.47
4	0.48	0.49	0.51	0.52	0.53	0.54	0.55	0.57	0.58	0.59
5	0.60	0.61	0.63	0.64	0.65	0.66	0.67	0.69	0.70	0.71
	0 70	0 70	0 ===	0.70	0.55	0.70	0.70	0.01	0.00	0.00
6	0.72	0.73	0.75	0.76	0.77	0.78	0.79	0.81	0.82	0.83
7	0.84	0.85	0.99	1.00	1.01	1.02	1.03	1.05	1.06	1.07
8 9	1.08	1.09	1.11	1.12	1.13	1.14	1.15	1.17	1.18	1.19
10	1.20	1.03	1.23	1.24	1.25	1.26	1.27	1.29	1.30	1.31
10	1.20	1.21	1.20	1.24	1.20	1.20	1.27	1.25	1.00	1.01
11	1.32	1.33	1.35	1.36	1.37	1.38	1.39	1.41	1.42	1.43
12	1.44	1.45	1.47	1.48	1.49	1.50	1.52	1.53	1.54	1.55
13	1.56	1.58	1.59	1.60	1.61	1.62	1.64	1.65	1.66	1.67
14	1.68	1.70	1.71	1.72	1.73	1.74	1.76	1.77	1.78	1.79
15	1.80	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91
- 55	A mari	- 01					- 00			
16	1.92	1.94	1.95	1.96	1.97	1.98	2.00	2.01	2.02	2.03
17	2.04	2.06	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.15
18	2.16	2.18	2.19	2.20	2.21	2.22	2.24	2.25	2.26	2.27
19 20	2.28	2.30	2.31	2.32	2.33 2.45	2.34	2.36	2.37	2.38	2.39
20	2.40	2.42	2.43	2.44	2.45	2.46	2.48	2.49	2.50	2.51
21	2.53	2.54	2.55	2.56	2.57	2.59	2.60	2.61	2.62	2.63
22	2.65	2.66	2.67	2.68	2.69	2.71	2.72	2.73	2.74	2.75
23	2.77	2.78	2.79	2.80	2.81	2.83	2.84	2.85	2.86	2.87
24	2.89	2.90	2.91	2.92	2.93	2.95	2.96	2.97	2.98	2.99
25	3.01	3.02	3.03	3.04	3.05	3.07	3.08	3.09	3.10	3.11
26	3.13	3.14	3.15	3.16	3.17	3.19	3.20	3.21	3.22	3.23
27	3.25	3.26	3.27	3.28	3.29	3.31	3.32	3.33	3.34	3.35
28	3.37	3.38	3.39	3.40	3.41	3.43	3.44	3.45	3.46	3.48
29	3.49	3.50	3.51	3.52	3.54	3.55	3.56	3.57	3.58	3.60
30	3.61	3.62	3.63	3.64	3.66	3.67	3.68	3.69	3.70	3.72
		1	diam'r.		12/3/	lakeri				
31	3.73	3.74	3.75	3.76	3.78	3.79	3.80	3.81	3.82	3.84
32	3.85	-3.86	3.87	3.88	3.90	3.91	3.92	3.93	3.94	3.96
33	3.97	3.98	3.99	4.00	4.02	4.03	4.04	4.05	4.06	4.08
34	4.09	4.10	4.11	4.12	4.14	4.15	4.16	4.17	4.18	4.20
39	4.21	4.22	4.23	4.24	4.26	4.27	4.28	4.29	4.30	4.32
1000		100	-		S (32)	110000		The state of the		1100

С

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3.

BAROMETER: 750<sup>mm</sup> (from 747.51 to 752.50).

Centigrade Degrees

Tenths of Degrees.

Degrees.			Manager 1				kanist.			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.10	0.11
1	0.12	0.13	0.15	0.16	0.17	0.18	0.19	0.21	0.22	0.23
2	0.24	0.25	0.27	0.28	0.29	0.30	0.31	0.33	0.34	0.35
3	0.36	0.38	0.39	0.40	0.41	0.42	0.44	0.45	0.46	0.47
4	0.48	0.50	0.51	0.52	0.53	0.55	0.56	0.57	0.58	0.59
5	0.61	0.62	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.71
	0.73	0.74	0.75	0.76	0.77	0.79	0.80	0.81	0.82	0.84
6 7	0.75	0.74	0.73	0.88	0.90	0.79	0.92	0.93	0.94	0.96
8	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05	1.07	1.08
9	1.09	1.10	1.11	1.13	1.14	1.15	ST. T. SECTION CO.	the same time to		17
10	1.03	1.10	1.23	1.15	1.14	1.13	1.16 1.28	1.17	1.19 1.31	1.20 1.32
			3.42.20					a Miles		No.
11	1.33	1.34	1.36	1.37	1.38	1.39	1.40	1.42	1.43	1.44
12	1.45	1.46	1.48	1.49	1.50	1.51	1.53	1.54	1.55	1.56
13	1.57	1.59	1.60	1.61	1.62	1.63	1.65	1.66	1.67	1.68
14	1.69	1.71	1.72	1.73	1.74	1.76	1.77	1.78	1.79	1.80
15	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.92
16	1.94	1.95	1.96	1.97	1.99	2.00	2.01	2.02	2.03	2.05
17	2.06	2.07	2.08	2.09	2.11	2.12	2.13	2.14	2.15	2.17
18	2.18	2.19	2.20	2.21	2.23	2.24	2.25	2.26	2.28	2.29
19	2.30	2.31	2.32	2.34	2.35	2.36	2.37	2.38	2.40	2.41
20	2.42	2.43	2.45	2.46	2.47	2.48	2.49	2.51	2.52	2.53
21	2.54	2.55	2.57	2.58	2.59	2.60	0.07	2.63		0.0=
22	2.66	2.68	2.69	2.70	2.71	2.72	2.61		2.64	2.65
23	2.78	2.80	2.81	2.82	2.83	2.72	2.73	2.75	2.76	2.77
24	2.91	2.92	2.93	2.94	2.95	2.97	2.86	2.99	2.88	2.89
25	3.03	3.04	3.05	3.06	3.07	3.09	2.98 3.10	3.11	3.00	3.01
	-0.00	I have been			100					
26	3.15	3.16	3.17	3.18	3.20	3.21	3.22	3.23	3.24	3.26
27	3.27	3.28	3.29	3.30	3.32	3.33	3.34	3.35	3.37	3.38
28	3.39	3.40	3.41	3.43	3.44	3.45	3.46	3.47	3.49	3.50
29	3.51	3.52	3.54	3.55	3.56	3.57	3.58	3.60	3.61	3.62
30	3.63	3.64	3.66	3.67	3.68	3.69	3.70	3.72	3.73	3.74
31	3.75	3.76	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86
32	3.87	3.89	3.90	3.91	3.92	3.93	3.95	3.96	3.97	3.98
33	3.99	4.01	4.02	4.03	4.04	4.06	4.07	4.08	4.09	4.10
34	4.12	4.13	4.14	4.15	4.16	4.18	4.19	4.20	4.21	4.22
35	4.24	4.25	4.26	4.27	4.29	4.30	4.31	4.32	4.33	4.35
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centi- grade Degrees.				2-00	Tenths o	f Degrees.				
F.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Milli
o	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.09	0.10	0.1
1	0.12	0.13	0.15	0.16	0.17	0.18	0.19	0.21	0.22	0.2
2	0.24	0.26	0.27	0.28	0.29	0.30	0.32	0.33	0.34	0.3
3	0.37	0.38	0.39	0.40	0.41	0.43	0.44	0.45	0.46	0.4
4	0.49	0.50	0.51	0.52	0.54	0.55	0.56	0.57	0.58	0.6
5	0.61	0.62	0.63	0.65	0.66	0.67	0.68	0.69	0.71	0.7
6	0.73	0.74	0.76	0.77	0.78	0.79	0.80	0.82	0.83	0.8
7	0.85	0.87	0.88	0.89	0.90	0.91	0.93	0.94	0.95	0.9
8	0.97	0.99	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.0
9	1.10	1.11	1.12	1.13	1.15	1.16	1.17	1.18	1.19	1.2
10	1.22	1.23	1.24	1.26	1.27	1.28	1.29	1.30	1.32	1.3
11	1.34	1.35	1.36	1.38	1.39	1.40	1.41	1.43	1.44	1.4
12	1.46	1.47	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.5
13	1.58	1.60	1.61	1.62	1.63	1.65	1.66	1.67	1.68	1.6
14	1.71	1.72	1.73	1.74	1.75	1.77	1.78	1.79	1.80	1.8
15	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.9
16	1.95	1.96	1.97	1.99	2.00	2.01	2.02	2.04	2.05	2.0
17	2.07	2.08	2.10	2.11	2.12	2.13	2.14	2.16	2.17	2.1
18	2.19	2.21	2.22	2.23	2.24	2.25	2.27	2.28	2.29	2.3
19	2.32	2.33	2.34	2.35	2.36	2.38	2.39	2.40	2.41	2.4
20	2.44	2.45	2.46	2.47	2.49	2.50	2.51	2.52	2.53	2.5
21	2.56	2.57	2.58	2.60	2.61	2.62	2.63	2.64	2.66	2.6
22	2.68	2.69	2.71	2.72	2.73	2.74	2.75	2.77	2.78	2.7
23	2.80	2.81	2.83	2.84	2.85	2.86	2.88	2.89	2.90	2.9
24 25	2.92 3.05	3.06	2.95 3.07	2.96 3.08	2.97 3.10	2.99 3.11	3.00	3.01	3.02	3.0 3.1
					100/6	- College	11000	Allega (St.	EL CO	
26	3.17	3.18	3.19	3.20	3.22	3.23	3.24	3.25	3.27	3.2
27 28	3.29	3.30	3.31	3.33	3.34	3.35	3.36	3.38	3.39	3.4
28	3.41	3.42	3.44	3.45	3.46	3.47	3.49	3.50	3.51 3.63	3.5
30	3.66	3.67	3.68	3.69	3.70	3.72	3.73	3.74	3.75	3.7
31	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.8
32	3.90	3.91	3.92	3.94	3.95	3.96	3.97	3.98	4.00	4.0
33	4.02	4.03	4.05	4.06	4.07	4.08	4.09	4.11	4.12	4.1
34	4.14	4.16	4.17	4.18	4.19	4.20	4.22	4.23	4.24	4.2
35	4.26	4.28	4.29	4.30	4.31	4.33	4.34	4.35	4.36	4.3
STEEL STEEL	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER:	760 <sup>mm</sup> .	(from	757.51 t	o 762.5	0).	
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.09	Millim. 0.10	Millim. 0.11
1	0.12	0.13	0.15	0.16	0.17	0.18	0.20	0.21	0.22	0.23
2	0.25	0.26	0.27	0.28	0.29	0.31	0.32	0.33	0.34	0.36
3	0.37	0.38	0.39	0.40	0.42	0.43	0.44	0.45	0.47	0.48
4	0.49	0.50	0.52	0.53	0.54	0.55	0.56	0.58	0.59	0.60
5	0.61	0.63	0.64	0.65	0.66	0.67	0.69	0.70	0.71	0.72
6	0.74	0.75	0.76	0.77	0.79	0.80	0.81	0.82	0.83	0.85
7	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94	0.96	0.97
8	0.98	0.99	1.01	1.02	1.03	1.04	1.05	1.07	1.08	1.09
9	1.10	1.12	1.13	1.14	1.15	1.17	1.18	1.19	1.20	1.21
10	1.23	1.24	1.25	1.26	1.28	1.29	1.30	1.31	1.32	1.34
11	1.35	1.36	1.57	1.39	1.40	1.41	1.42	1.44	1.45	1.46
12	1.47	1.48	1.50	1.51	1.52	1.53	1.55	1.56	1.57	1.58
13	1.59	1.61	1.62	1.63	1.64	1.66	1.67	1.68	1.69	1.71
14	1.72	1.73	1.74	1.75	1.77	1.78	1.79	1.80	1.82	1.83
15	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.94	1.95
16	1.96	1.97	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07
17	2.09	2.10	2.11	2.12	2.13	2.15	2.16	2.17	2.18	2.20
18	2.21	2.22	2.23	2.24	2.26	2.27	2.28	2.29	2.31	2.32
19	2.33	2.34	2.36	2.37	2.38	2.39	2.40	2.42	2.43	2.44
20	2.45	2.47	2.48	2.49	2.50	2.51	2.53	2.54	2.55	2.56
21	2.58	2.59	2.60	2.61	2.63	2.64	2.65	2.66	2.67	2.69
22	2.70	2.71	2.72	2.74	2.75	2.76	2.77	2.78	2.80	2.81
23	2.82	2.83	2.85	2.86	2.87	2.88	2.89	2.91	2.92	2.93
24	2.94	2.96	2.97	2.98	2.99	3.01	3.02	3.03	3.04	3.05
25	3.07	3.08	3.09	3.10	3.12	3.13	3.14	3.15	3.16	3.18
26	3.19	3.20	3.21	3.23	3.24	3.25	3.26	3.28	3.29	3.30
27	3.31	3.32	3.34	3.35	3.36	3.37	3.39	3.40	3.41	3.42
28	3.43	3.45	3.46	3.47	3.48	3.50	3.51	3.52	3.53	3.54
29	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64	3.66	3.67
30	3.68	3.69	3.70	3.72	3.73	3.74	3.75	3.77	3.78	3.79
31	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91
32	3.93	3.94	3.95	3.96	3.97	3.99	4.00	4.01	4.02	4.04
33	4.05	4.06	4.07	4.08	4.10	4.11	4.12	4.13	4.15	4.16
34	4.17	4.18	4.20	4.21	4.22	4.23	4.24	4.26	4.27	4.28
35	4.29	4.31	4.32	4.33	4.34	4.35	4.37	4.38	4.39	4.40
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER:	765 <sup>mm</sup>	(from	762.51	to <b>767.5</b>	0).	
Centigrade Degrees.					Tenths o	f Degrees.				1000
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim, 0.02	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.09	Millim. 0.10	Millim. 0.11
1	0.12	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22	0.23
2	0.25	0.26	0.27	0.28	0.30	0.31	0.32	0.33	0.35	0.36
3	0.37	0.38	0.40	0.41	0.42	0.43	0.44	0.46	0.47	0.48
4	0.49	0.51	0.52	0.53	0.54	0.56	0.57	0.58	0.59	0.61
5	0.62	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.72	0.73
6	0.74	0.75	0.77	0.78	0.79	0.80	0.82	0.83	0.84	0.85
7	0.86	0.88	0.89	0.90	0.91	0.93	0.94	0.95	0.96	0.98
8	0.99	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.09	1.10
9	1.11	1.12	1.14	1.15	1.16	1.17	1.19	1.20	1.21	1.22
10	1.23	1.25	1.26	1.27	1.28	1.30	1.31	1.32	1.33	1.35
11	1.36	1.37	1.38	1.40	1.41	1.42	1.43	1.44	1.46	1.47
12	1.48	1.49	1.51	1.52	1.53	1.54	1.56	1.57	1.58	1.59
13	1.61	1.62	1.63	1.64	1.65	1.67	1.68	1.69	1.70	1.72
14	1.73	1.74	1.75	1.77	1.78	1.79	1.80	1.82	1.83	1.84
15	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96
16	1.98	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07	2.09
17	2.10	2.11	2.12	2.14	2.15	2.16	2.17	2.19	2.20	2.21
18	2.22	2.23	2.25	2.26	2.27	2.28	2.30	2.31	2.32	2.33
19	2.35	2.36	2.37	2.38	2.40	2.41	2.42	2.43	2.44	2.46
20	2.47	2.48	2.49	2.51	2.52	2.53	2.54	2.56	2.57	2.58
21	2.59	2.61	2.62	2.63	2.64	2.65	2.67	2.68	2.69	2.70
22	2.72	2.73	2.74	2.75	2.77	2.78	2.79	2.80	2.82	2.83
23	2.84	2.85	2.86	2.88	2.89	2.90	2.91	2.93	2.94	2.95
24	2.96	2.98	2.99	3.00	3.01	3.03	3.04	3.05	3.06	3.07
25	3.09	3.10	3.11	3.12	3.14	3.15	3.16	3.17	3.19	3.20
26	3.21	3.22	3.23	3.25	3.26	3.27	3.28	3.30	3.31	3.32
27	3.33	3.35	3.36	3.37	3.38	3.40	3.41	3.42	3.43	3.44
28	3.46	3.47	3.48	3.49	3.51	3.52	3.53	3.54	3.56	3.57
29	3.58	3.59	3.61	3.62	3.63	3.64	3.65	3.67	3.68	3.69
30	3.70	3.72	3.73	3.74	3.75	3.77	3.78	3.79	3.80	3.82
31	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91	3.93	3.94
32	3.95	3.96	3.98	3.99	4.00	4.01	4.03	4.04	4.05	4.06
33	4.07	4.09	4.10	4.11	4.12	4.14	4.15	4.16	4.17	4.19
34	4.20	4.21	4.22	4.24	4.25	4.26	4.27	4.28	4.30	4.31
35	4.32	4.33	4.35	4.36	4.37	4.38	4.40	4.41	4.42	4.43
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER:	770 <sup>mm</sup> ·	(from	76 <b>7</b> .51 t	o 772.5	0).	
Centigrade Degrees.					Tenths of	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.04	0.05	0.00	0.07	0.09	0.10	0.11
1	0.12	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22	0.24
2	0.25	0.26	0.27	0.29	0.30	0.31	0.32	0.34	0.35	0.36
3	0.37	0.39	0.40	0.41	0.42	0.43	0.45	0.46	0.47	0.48
4	0.50	0.51	0.52	0.53	0.55	0.56	0.57	0.58	0.60	0.61
5	0.62	0.63	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.73
0	0.75	0.76	0 77	0.70	0.00	0.01	0.00	0.00	0.05	0.00
6 7	0.75	0.76	0.77	0.78	0.80	0.81	0.82	0.83	0.85	0.86
8	0.99	1.01	1.02	1.03	1.04	1.06	1.07	1.08	1.09	1.11
9	1.12	1.13	1.14	1.16	1.17	1.18	1.19	1.21	1.22	1.23
10	1.24	1.26	1.27	1.28	1.29	1.30	1.32	1.33	1.34	1.35
11	1.37	1.38	1.39	1.40	1.42	1.43	1.44	1.45	1.47	1.48
12	1.49	1.50	1.52	1.53	1.54	1.55	1.57	1.58	1.59	1.60
13	1.62	1.63	1.64	1.65	1.67	1.68	1.69	1.70	1.72	1.73
14	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.83	1.84	1.85
15	1.86	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96	1.98
1	- 00		0.00	2.05				THE STATE OF		Time
16	1.99	2.00	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10
17	2.11	2.13	2.14	2.15	2.16	2.17	2.19	2.20	2.21	2.22
18	2.36	2.25	2.26	2.27	2.29	2.30	2.31	2.32	2.34	2.35
20	2.49	2.50	2.51	2.52	2.54	2.42	2.44	2.45 2.57	2.46 2.58	2.47
20	2.40	2.30	2.01	2.02	2.04	2.00	2.00	2.01	2.00	2.00
21	2.61	2.62	2.63	2.65	2.66	2.67	2.68	2.70	2.71	2.72
22	2.73	2.75	2.76	2.77	2.78	2.80	2.81	2.82	2.83	2.85
23	2.86	2.87	2.88	2.90	2.91	2.92	2.93	2.95	2.96	2.97
24	2.98	3.00	3.01	3.02	3.03	3.04	3.06	3.07	3.08	3.09
25	3.11	3.12	3.13	3.14	3.16	3.17	3.18	3.19	3.21	3.22
				P CO			Market 1			
26	3.23	3.24	3.26	3.27	3.28	3.29	3.31	3.32	3.33	3.34
27	3.36	3.37	3.38	3.39	3.41	3.42	3.43	3.44	3.45	3.47
28	3.48	3.49	3.50	3.52	3.53	3.54	3.55	3.57	3.58	3.59
29	3.60	3.62	3.63 3.75	3.64	3.65	3.67	3.68	3.69	3.70	3.72
90	3.73	3.74	3.75	5.11	3.78	3.79	3.80	3.82	3.83	3.84
31	3.85	3.87	3.88	3.89	3.90	3.91	3.93	3.94	3.95	3.96
32	3.98	3.99	4.00	4.01	4.03	4.04	4.05	4.06	4.08	4.09
33	4.10	4.11	4.13	4.14	4.15	4.16	4.18	4.19	4.20	4.21
34	4.23	4.24	4.25	4.26	4.28	4.29	4.30	4.31	4.32	4.34
35	4.35	4.36	4.37	4.39	4.40	4.41	4.42	4.44	4.45	4.46
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROMI	ETER:	775 <sup>mm</sup> .	(from	772.51 to	o <b>77</b> 7.50	0).	
Centigrade Degrees.				2011921	Tenths of	f Degrees.				- HOLY
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.03	0.04	0.05	0.06	0.08	0.09	0.10	0.11
1	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.23	0.24
2	0.25	0.26	0.28	0.29	0.30	0.31	0.33	0.34	0.35	0.36
3	0.38	0.39	0.40	0.41	0.43	0.44	0.45	0.46	0.48	0.49
4	0.50	0.51	0.53	0.54	0.55	0.56	0.58	0.59	0.60	0.61
5	0.63	0.64	0.65	0.66	0.68	0.69	0.70	0.71	0.73	0.74
6	0.75	0.76	0.78	0.79	0.80	0.81	0.83	0.84	0.85	0.86
7	0.88	0.89	0.90	0.91	0.93	0.94	0.95	0.96	0.98	0.99
8	1.00	1.01	1.03	1.04	1.05	1.06	1.08	1.09	1.10	1.11
9	1.13	1.14	1.15	1.16	1.18	1.19	1.20	1.21	1.23	1.24
10	1.25	1.26	1.28	1.29	1.30	1.31	1.33	1.34	1.35	1.36
11	1.38	1.39	1.40	1.41	1.43	1.44	1.45	1.46	1.48	1.49
12	1.50	1.51	1.53	1.54	1.55	1.56	1.58	1.59	1.60	1.61
13	1.63	1.64	1.65	1.66	1.68	1.69	1.70	1.71	1.73	1.74
14	1.75	1.76	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.86
15	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99
	0.00	0.00	0.00	0.01	0.05	0.00	0.00	0.00		
16	2.00	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11
17	2.13	2.14 2.26	2.15	2.16 2.29	2.18	2.19	2.20	2.21 2.34	2.23 2.35	2.24
18	2.38	2.39	2.40	2.41	2.43	2.44	2.45	2.46	2.48	2.49
20	2.50	2.51	2.53	2.54	2.55	2.56	2.58	2.59	2.60	2.61
				1-11-27						
21	2.63	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.73	2.74
22	2.75	2.76	2.78	2.79	2.80	2.81	2.83	2.84	2.85	2.86
23	2.88	2.89	2.90	2.91	2.93	2.94	2.95	2.96	2.98	2.99
24	3.00	3.01	3.03	3.04	3.05	3.06	3.08	3.09	3.10	3.11
25	3.13	3.14	3.15	3.16	3.18	3.19	3.20	3.21	3.23	3.24
26	3.25	3.26	3.28	3.29	3.30	3.31	3.33	3.34	3.35	3.36
27	3.38	3.39	3.40	3.41	3.43	3.44	3.45	3.46	3.48	3.49
28	3.50	3.51	3.53	3.54	3.55	3.56	3.58	3.59	3.60	3.61
29	3.63	3.64	3.65	3.66	3.68	3.69	3.70	3.72	3.73	3.74
30	3.75	3.77	3.78	3.79	3.80	3.82	3.83	3.84	3.85	3.87
31	3.88	3.89	3.90	3.92	3.93	3.94	3.95	3.97	3.98	3.99
32	4.00	4.02	4.03	4.04	4.05	4.07	4.08	4.09	4.10	4.12
33	4.13	4.14	4.15	4.17	4.18	4.19	4.20	4.22	4.23	4.24
34	4.25	4.27	4.28	4.29	4.30	4.32	4.33	4.34	4.35	4.37
35	4.38	4.39	4.40	4.42	4.43	4.44	4.45	4.47	4.48	4.49
-	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
		1	MINISTER OF	MA HE					A Property	

		В	AROMI	ETER :	780 <sup>mm</sup> ·	(from	777.51	to 782.5	0).	
Centigrade Degrees.					Tenths o	f Degrees.		1		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim.	Millim. 0.04	Millim. 0.05	Millim.	Millim. 0.08	Millim. 0.09	Millim. 0.10	Millim. 0.11
1	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.23	0.24
2	0.25	0.26	0.28	0.29	0.30	0.31	0.33	0.34	0.35	0.37
3	0.38	0.39	0.40	0.42	0.43	0.44	0.45	0.47	0.48	0.49
4	0.50	0.52	0.53	0.54	0.55	0.57	0.58	0.59	0.60	0.62
5	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.72	0.73	0.74
6	0.76	0.77	0.78	0.79	0.81	0.82	0.83	0.84	0.86	0.87
7	0.88	0.89	0.91	0.92	0.93	0.94	0.96	0.97	0.98	0.99
8	1.01	1.02	1.03	1.04	1.06	1.07	1.08	1.10	1.11	1.12
9	1.13	1.15	1.16	1.17	1.18	1.20	1.21	1.22	1.23	1.25
10	1.26	1.27	1.28	1.30	1.31	1.32	1.33	1.35	1.36	1.37
11	1.38	1.40	1.41	1.42	1.44	1.45	1.46	1.47	1.49	1.50
12	1.51	1.52	1.54	1.55	1.56	1.57	1.59	1.60	1.61	1.62
13	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.74	1.75
14	1.76	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.86	1.88
15	1.89	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99	2.00
16	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.13
17	2.14	2.15	2.17	2.18	2.19	2.20	2.22	2.23	2.24	2.25
18	2.27	2.28	2.29	2.30	2.32	2.33	2.34	2.35	2.37	2.38
19	2.39	2.40	2.42	2.43	2.44	2.45	2.47	2.48	2.49	2.51
20	2.52	2.53	2.54	2.56	2.57	2.58	2.59	2.61	2.62	2.63
21	2.64	2.66	2.67	2.68	2.69	2.71	2.72	2.73	2.74	2.76
22	2.77	2.78	2.79	2.81	2.82	2.83	2.85	2.86	2.87	2.88
23	2.90	2.91	2.92	2.93	2.95	2.96	2.97	2.98	3.00	3.01
24	3.02	3.03	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.14
25	3.15	3.16	3.17	3.19	3.20	3.21	3.22	3.24	3.25	3.26
26	3.27	3.29	3.30	3.31	3.32	3.34	3.35	3.36	3.37	3.39
27	3.40	3.41	3.42	3.44	3.45	3.46	3.47	3.49	3.50	3.51
28	3.52	3.54	3.55	3.56	3.58	3.59	3.60	3.61	3.63	3.64
29	3.65	3.66	3.68	3.69	3.70	3.71	3.73	3.74	3.75	3.76
30	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.89
31	3.90	3.92	3.93	3.94	3.95	3.97	3.98	3.99	4.00	4.02
32	4.03	4.04	4.05	4.07	4.08	4.09	4.10	4.12	4.13	4.14
33	4.15	4.17	4.18	4.19	4.20	4.22	4.23	4.24	4.26	4.27
34	4.28	4.29	4.31	4.32	4.33	4.34	4.36	4.37	4.38	4.39
35	4.41	4.42	4.43	4.44	4.46	4.47	4.48	4.49	4.51	4.52
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centigrade Degrees.										
	•			* Addition of	Tenths o	f Degrees.			N. U.S.	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim.	Millim.	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim. 0.10	Millim. 0.11
1	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.22	0.23	0.24
2	0.25	0.27	0.28	0.29	0.30	0.32	0.33	0.34	0.35	0.37
3	0.38	0.39	0.41	0.42	0.43	0.44	0.46	0.47	0.48	0.49
4	0.51	0.52	0.53	0.54	0.56	0.57	0.58	0.60	0.61	0.62
5	0.63	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.73	0.75
6	0.76	0.77	0.79	0.80	0.81	0.82	0.84	0.85	0.86	0.87
7	0.89	0.90	0.91	0.92	0.94	0.95	0.96	0.98	0.99	1.00
8	1.01	1.03	1.04	1.05	1.06	1.08	1.09	1.10	1.11	1.13
9	1.14	1.15	1.17	1.18	1.19	1.20	1.22	1.23	1.24	1.25
10	1.27	1.28	1.29	1.30	1.32	1.33	1.34	1.36	1.37	1.38
11	1.39	1.41	1.42	1.43	1.44	1.46	1.47	1.48	1.50	1.51
12	1.52	1.53	1.55	1.56	1.57	1.58	1.60	1.61	1.62	1.63
13	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.74	1.75	1.76
14	1.77	1.79	1.80	1.81	1.82	1.84	1.85	1.86	1.88	1.89
15	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01
16	2.03	2.04	2.05	2.07	2.08	2.09	2.10	2.12	2.13	2.14
17	2.15	2.17	2.18	2.19	2.20	2.22	2.23	2.24	2.26	2.27
18	2.28	2.29	2.31	2.32	2.33	2.34	2.36	2.37	2.38	2.39
19	2.41	2.42	2.43	2.45	2.46	2.47	2.48	2.50	2.51	2.52
20	2.53	2.55	2.56	2.57	2.58	2.60	2.61	2.62	2.64	2.65
21	2.66	2.67	2.69	2.70	2.71	2.72	2.74	2.75	2.76	2.77
22	2.79	2.80	2.81	2.83	2.84	2.85	2.86	2.88	2.89	2.90
23	2.91	2.93	2.94	2.95	2.96	2.98	2.99	3.00	3.02	3.03
24	3.04	3.05	3.07	3.08	3.09	3.10	3.12	3.13	3.14	3.15
25	3.17	3.18	3.19	3.21	3.22	3.23	3.24	3.26	3.27	3.28
26	3.29	3.31	3.32	3.33	3.34	3.36	3.37	3.38	3.40	3.41
27	3.42	3.43	3.45	3.46	3.47	3.48	3.50	3.51	3.52	3.53
28	3.55	3.56	3.57	3.59	3.60	3.61	3.62	3.64	3.65	3.66
29	3.67	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.78	3.79
30	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91
31	3.93	3.94	3.95	3.97	3.98	3.99	4.00	4.02	4.03	4.04
32	4.05	4.07	4.08	4.09	4.11	4.12	4.13	4.14	4.16	4.17
33	4.18	4.19	4.21	4.22	4.23	4.24	4.26	4.27	4.28	4.30
34 35	4.31	4.32	4.33	4.35	4.36	4.37	4.38 4.51	4.40	4.41	4.42 4.55
	0.	1.	2.	3.			-	7.		9.
			4.	٥.	4.	5.	6.		8.	9.

		D.		ETER:	100	(11011)	07.01	0 100.0	٠,٠	
Centi- grade Jegrees.					Tenths o	Degrees.				等 (以)
e.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin
0	0.00	0.01	0.03	0.04	0.05	0.06	0.08	0.09	0.10	0.11
1	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.22	0.23	0.24
2	0.26	0.27	0.28	0.29	0.31	0.32	0.33	0.34	0.36	0.37
3	0.38	0.40	0.41	0.42	0.43	0.45	0.46	0.47	0.48	0.50
4	0.51	0.52	0.54	0.55	0.56	0.57	0.59	0.60	0.61	0.62
5	0.64	0.65	0.66	0.68	0.69	0.70	0.71	0.73	0.74	0.75
6	0.77	0.78	0.79	0.80	0.82	0.83	0.84	0.85	0.87	0.88
7	0.89	0.91	0.13	0.93	0.94	0.96	0.97	0.98	0.99	1.0
8	1.02	1.03	1.05	1.06	1.07	1.08	1.10	1.11	1.12	1.13
9	1.15	1.16	1.17	1.19	1.20	1.21	1.22	1.24	1.25	1.26
10	1.13	1.10	1.30	1.31	1.33	1.34	1.35	1.36	1.38	1.39
10	1.20	1.29	1.50	1.51	1.00	1.04	1.00	1.00	1.00	1.03
11	1.40	1.42	1.43	1.44	1.45	1.47	1.48	1.49	1.50	1.52
12	1.53	1.54	1.56	1.57	1.58	1.59	1.61	1.62	1.63	1.64
13	1.66	1.67	1.68	1.70	1.71	1.72	1.73	1.75	1.76	1.77
14	1.79	1.80	1.81	1.82	1.84	1.85	1.86	1.87	1.89	1.90
15	1.91	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.03
16	2.04	2.05	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.15
17	2.17	2.18	2.19	2.21	2.22	2.23	2.24	2.26	2.27	2.28
18	2.30	2.31	2.32	2.33	2.35	2.36	2.37	2.38	2.40	2.41
19	2.42	2.44	2.45	2.46	2.47	2.49	2.50	2.51	2.52	2.54
20	2.55	2.56	2.58	2.59	2.60	2.61	2.63	2.64	2.65	2.66
07	2.68	2.69	2.70	2.72	2.73	2.74	2.75	2.77	2.78	2.79
21	2.81	- 10 - 11 m	2.83	2.84	2.86	2.74	2.88	2.89	2.91	2.92
22	2.81	2.82	2.83	2.84	2.80	3.00	3.01	3.02	3.03	3.05
23 24	3.06	3.07	3.09	3.10	3.11	3.12	3.14	3.15	3.16	3.17
25	3.19	3.20	3.21	3.23	3.24	3.25	3.26	3.13	3.29	3.30
H-03 m	Tuesda.						0.00	0.10	0.10	
26	3.32	3.33	3.34	3.35	3.37	3.38	3.39	3.40	3.42	3.43
27	3.44	3.46	3.47	3.48	3.49	3.51	3.52	3.53	3.54	3.56
28	3.57	3.58	3.60	3.61	3.62	3.63	3.65	3.66	3.67	3.68
29	3.70	3.71	3.72	3.74	3.75	3.76	3.77	3.79	3.80	3.81
30	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91	3.93	3.94
31	3.95	3.97	3.98	3.99	4.00	4.02	4.03	4.04	4.05	4.07
32	4.08	4.09	4.11	4.12	4.13	4.14	4.16	4.17	4.18	4.19
33	4.21	4.22	4.23	4.25	4.26	4.27	4.28	4.30	4.31	4.32
34	4.34	4.35	4.36	4.37	4.39	4.40	4.41	4.42	4.44	4.45
35	4.46	4.48	4.49	4.50	4.51	4.53	4.54	4.55	4.56	4.58
1	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

BAROMETER: 795mm. (from 792.51 to 797.50). Centigrade Degrees Tenths of Degrees. 2. 3. 4. 5. 6. 7. 9. 0. 1. 8. Millim, Millim. Millim. Millim. Millim, Millim. Millim. Millim. Millim. Millim. 0 0.00 0.01 0.03 0.04 0.05 0.06 0.08 0.09 0.10 0.12 0.13 0.14 0.15 0.17 0.18 0.19 0.21 0.22 0.23 0.24 1 0.30 0.27 0.28 0.31 0.32 0.33 0.36 0.37 2 0.26 0.35 0.38 0.40 0.41 0.42 0.44 0.45 0.46 0.47 0.49 0.50 3 4 0.51 0.53 0.54 0.55 0.56 0.58 0.59 0.60 0.62 0.63 0.67 0.68 5 0.64 0.65 0.69 0.71 0.72 0.73 0.74 0.76 0.78 0.80 0.81 0.82 6 0.77 0.83 0.85 0.86 0.87 0.89 0.90 0.91 0.92 0.94 0.95 0.96 0.98 1.00 1.01 7 0.99 1.04 1.05 1.06 1.08 8 1.03 1.09 1.10 1.12 1.13 1.14 1.15 1.17 1.18 1.19 1.21 1.22 1.23 1.26 9 1.24 1.27 10 1.28 1.30 1.31 1.32 1.33 1.35 1.36 1.39 1.37 1.40 11 1.41 1.42 1.44 1.45 1.46 1.48 1.49 1.50 1.51 1.53 12 1.54 1.55 1.57 1.58 1.59 1.60 1.62 1.63 1.64 1.66 13 1.67 1.68 1.69 1.71 1.72 1.73 1.75 1.76 1.77 1.78 1.80 14 1.81 1.82 1.83 1.85 1.86 1.87 1.89 1.90 1.91 15 1.92 1.94 1.95 1.96 1.98 2.00 2.03 1.99 2.01 2.04 16 2.05 2.07 2.08 2.09 2.10 2.13 2.16 2.17 2.12 2.14 17 2.18 2.19 2.21 2.22 2.23 2.25 2.26 2.27 2.28 2.30 18 2.31 2.32 2.34 2.35 2.36 2.37 2.39 2.41 2.43 2.40 19 2.44 2.45 2.46 2.48 2.49 2.50 2.51 2.53 2.54 2.55 20 2.57 2.58 2.59 2.60 2.62 2.63 2.64 2.67 2.68 2.66 21 2.69 2.71 2.72 2.73 2.75 2.76 2.77 2.78 2.80 2.81 22 2.82 2.84 2.85 2.86 2.89 2.90 2.87 2.91 2.93 2.94 23 2.95 2.96 2.98 2.99 3.00 3.02 3.03 3.04 3.05 3.07 24 3.08 3.09 3.11 3.13 3.18 3.12 3.14 3.16 3.17 3.19 25 3.21 3.22 3.23 3.25 3.26 3.27 3.28 3.30 3.31 3.32 26 3.34 3.35 3.36 3.37 3.39 3.40 3.41 3.43 3.44 3.45 27 3.46 3.48 3.49 3.50 3.52 3.53 3.58 3.54 3.55 3.57 28 3.59 3.61 3.62 3.63 3.64 3.66 3.67 3.70 3.71 3.68 29 3.72 3.73 3.75 3.76 3.77 3.79 3.80 3.81 3.82 3.84 30 3.85 3.86 3.88 3.89 3.90 3.91 3.93 3.94 3.95 3.96 31 3.98 3.99 4.00 4.02 4.05 4.08 4.09 4.03 4.04 4.07 32 4.11 4.12 4.13 4.14 4.21 4.22 4.16 4.17 4.18 4.20 33 4.23 4.25 4.30 4.26 4.27 4.29 4.31 4.32 4.34 4.35 34 4.36 4.38 4.39 4.40 4.41 4.47 4.48 4.43 4.44 4.45 35 4.49 4.50 4.52 4.53 4.54 4.59 4.61 4.56 4.57 4.58 2. 0. 1. 3. 9. 5. 6. 7. 8.

C

BAROMETER: 800<sup>mm.</sup> (from 797.51 to 802.50).

Centigrade

Tenths of Degrees.

grade Degrees.					Tentns o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.03	0.04	0.05	0.06	0.08	0.09	0.10	0.12
1	0.13	0.14	0.15	0.17	0.18	0.19	0.21	0.22	0.23	0.25
2	0.26	0.27	0.28	0.30	0.31	0.32	0.34	0.35	0.36	0.37
3	0.39	0.40	0.41	0.43	0.44	0.45	0.46	0.48	0.49	0.50
4	0.52	0.53	0.54	0.56	0.57	0.58	0.59	0.61	0.62	0.63
5	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.74	0.75	0.76
6	0.77	0.79	0.80	0.81	0.83	0.84	0.85	0.87	0.88	0.89
7	0.90	0.92	0.93	0.94	0.96	0.97	0.98	0.99	1.01	1.02
8	1.03	1.05	1.06	1.07	1.08	1.10	1.11	1.12	1.14	1.15
9	1.16	1.17	1.19	1.20	1.21	1.23	1.24	1.25	1.27	1.28
10	1.29	1.30	1.32	1.33	1.34	1.36	1.37	1.38	1.39	1.41
11	1.42	1.43	1.45	1.46	1.47	1.48	1.50	1.51	1.52	1.54
12	1.55	1.56	1.58	1.59	1.60	1.61	1.63	1.64	1.65	1.67
13	1.68	1.69	1.70	1.72	1.73	1.74	1.76	1.77	1.78	1.79
14	1.81	1.82	1.83	1.85	1.86	1.87	1.89	1.90	1.91	1.92
15	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.03	2.04	2.05
16	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.16	2.17	2.18
17	2.20	2.21	2.22	2.23	2.25	2.26	2.27	2.29	2.30	2.31
18	2.32	2.34	2.35	2.36	2.38	2.39	2.40	2.41	2.43	2.44
19	2.45	2.47	2.48	2.49	2.50	2.52	2.53	2.54	2.56	2.57
20	2.58	2.60	2.61	2.62	2.63	2.65	2.66	2.67	2.69	2.70
21	2.71	2.72	2.74	2.75	2.76	2.78	2.79	2.80	2.81	2.83
22	2.84	2.85	2.87	2.88	2.89	2.91	2.92	2.93	2.94	2.96
23	2.97	2.98	3.00	3.01	3.02	3.03	3.05	3.06	3.07	3.09
24	3.10	3.11	3.12	3.14	3.15	3.16	3.18	3.19	3.20	3.22
25	3.23	3.24	3.25	3.27	3.28	3.29	3.31	3.32	3.33	3.34
26	3.36	3.37	3.38	3.40	3.41	3.42	3.43	3.45	3.46	3.47
27	3.49	3.50	3.51	3.52	3.54	3.55	3.56	3.58	3.59	3.60
28	3.62	3.63	3.64	3.65	3.67	3.68	3.69	3.71	3.72	3.73
29	3.74	3.76	3.77	3.78	3.80	3.81	3.82	3.83	3.85	3.86
30	3.87	3.89	3.90	3.91	3.93	3.94	3.95	3.96	3.98	3.99
31	4.00	4.02	4.03	4.04	4.05	4.07	4.08	4.09	4.11	4.12
32	4.13	4.14	4.16	4.17	4.18	4.20	4.21	4.22	4.24	4.25
33	4.26	4.27	4.29	4.30	4.31	4.33	4.34	4.35	4.36	4.38
34	4.39	4.40	4.42	4.43	4.44	4.45	4.47	4.48	4.49	4.51
35	4.52	4.53	4.55	4.56	4.57	4.58	4.60	4.61	4.62	4.64
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# XXI.

#### OLD FRENCH BAROMETER.

### TABLE

FOR

# REDUCING TO THE FREEZING POINT THE OBSERVATIONS TAKEN WITH OLD FRENCH BAROMETERS,

PROVIDED WITH BRASS SCALES, EXTENDING FROM THE CISTERN TO THE

TOP OF THE MERCURIAL COLUMN; CALCULATED FROM 240 TO 345

LINES, OR FROM 23 INCHES 4 LINES TO 28 INCHES 9 LINES.

By Kaemtz.

#### TABLE XXI.

This table is taken from Kaemtz's Lehrbuch der Meteorologie, Vol. II. p. 2: To render it more useful, the first page, giving the corrections for Barometri Heights between 240 and 280 Paris lines, has been added.

The values adopted by Kaemtz for reducing the Old French Barometer are following: —

Let h = observed height in French lines.

- " t = temperature of attached thermometer in degrees of Reaumur.
- "  $m = \text{expansion of mercury between 0 and 80}^{\circ}$  Reaumur = 0.018018.
- "  $l = \text{linear expansion of brass between 0 and 80}^{\circ}$  Reaumur = 0.0018782.

The normal temperature of standard being = 13° Reaumur.

And the formula becomes, -

$$-h \cdot \frac{m \times t - l \cdot (t - 13)}{1 + m \times t}$$

The Table gives the corrections only for full degrees and for every fifth line; the intermediate values can easily be found by an interpolation at sight.

### Example of Reduction.

Observed height			100	= :	325.32 lin	ies.
Attached thermom	éter	1		=	12.5 Rea	aumur.
In the line beginning w	rith 12°, and in the	e vertic	al colu	imn he	aded 325	lines,
we find,	Correction for	12°	=-	-0.89 li	ines.	
	Interpolation for	0°.5	=-	-0.03	66	
	C	700 5	Att 1	0.00	Situ epi	
	Correction for	12.5	=-	0.92	**	

And we have,

Observed height, 325.32 "Correction for 12°.5, —0.92 "

Height at the freezing point = 324.40 lines.

Normal Temperature of the Scale = 130 Reaumur.

Attached Thermom- eter.			,II	Barometer in	ı Paris Line	8.			Attached Thermon eter.
Degrees of Reaumur.	240	245	250	255	260	265	270	275	Degrees o Reaumur
0	Par. Lines.	Par Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	0
-15	+0.65	+0.66	+0.68	+0.69	+0.70	+0.72	+0.73	+0.75	-15
-14	0.60	0.61	0.63	0.64	0.65	0.67	0.68	0.69	-14
-13	0.55	0.57	0.58	0.59	0.60	0.61	0.62	0.64	-13
-12	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	-12
-11	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.52	-11
-10	0.41	0.42	0.43	0.44	0.44	0.45	0.46	0.47	-10
- 9	+0.36	+0.37	+0.38	+0.38	+0.39	+0.40	+0.41	+0.41	- 9
- 8	0.31	0.32	0.33	0.33	0.34	0.35	0.35	0.36	- 8
- 7	0.27	0.27	0.28	0.28	0.29	0.29	0.30	0.30	- 7
- 6	0.22	0.22	0.23	0.23	0.24	0.24	0.24	0.25	- 6
- 5	0.17	0.17	0.18	0.18	0.18	0.19	0.19	0.19	- 5
- 4	+0.12	+0.12	+0.13	+0.13	+0.13	+0.13	+0.14	+0.14	- 4
- 3	0.07	0.07	0.08	0.08	0.08	0.08	0.08	0.08	- 3
- 2	+0.02	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	- 2
- 1	-0.02	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	- 1
0	-0.07	-0.07	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	0
+ 1	-0.12	-0.12	-0.13	-0.13	-0.13	-0.13	-0.14	-0.14	+ 1
2	0.17	0.17	0.18	0.18	0.18	0.19	0.19	0.19	2
3	0.22	0.22	0.23	0.23	0.24	0.24	0.24	0.25	3
4	0.27	0.27	0.28	0.28	0.29	0.29	0.30	0.30	4
5	0.31	0.32	0.33	0.33	0.34	0.35	0.35	0.36	5
+ 6	-0.36	-0.37	-0.38	-0.38	-0.39	-0.40	-0.41	-0.41	+ 6
7	0.41	0.42	0.43	0.44	0.44	0.45	0.46	0.47	7
8	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.52	8
9	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	9
10	0.55	0.57	0.58	0.59	0.60	0.61	0.62	0.64	10
+11	-0.60	-0.61	-0.63	-0.64	-0.65	-0.67	-0.68	-0.69	+11
12	0.65	0.66	0.68	0.69	0.70	0.72	0.73	0.75	12
13	0.70	0.71	0.73	0.74	0.76	0.77	0.79	0.80	13
14	0.75	0.76	0.78	0.79	0.81	0.82	0.84	0.86	14
15	0.80	0.81	0.83	0.84	0.86	0.88	0.89	0.91	15
+16	-0.84	-0.86	-0.88	-0.90	-0.91	-0.93	-0.95	-0.97	+16
17	0.89	0.91	0.93	0.95	0.97	0.98	1.00	1.02	17
18	0.94	0.96	0.98	1.00	1.02	1.04	1.06	1.08	18
19	0.99	1.01	1.03	1.05	1.07	1.09	1.11	1.13	19
20	1.04	1.06	1.08	1.10	1.12	1.14	1.17	1.19	20
+21	-1.08	-1.11	-1.13	-1.15	-1.17	-1.20	-1.22	-1.24	+21
22	1.13	1.16	1.18	1.20	1.23	1.25	1.27	1.30	22
23	1.18	1.20	1.23	1.25	1.28	1.30	1.33	1.35	23
24	1.23	1.25	1.28	1.31	1.33	1.36	1.38	1.41	24
25	1.28	1.30	1.33	1.36	1.38	1.41	1.44	1.46	25

Normal Temperature of the Scale = 13° Reaumur.

eter. Degrees of								Thermon eter.
Reaumur.	280	285	290	295	300	305	310	Degrees of Reaumur
0	Par. Lines.	0						
-15	+0.77	+0.78	+0.79	+0.81	+0.82	+0.84	+0.85	-15
-14	0.71	0.73	0.74	0.75	0.76	0.77	0.79	-14
-13	0.65	0.67	0.68	0.69	0.70	0.71	0.72	-13
-12	0.60	0.61	0.62	0.63	0.64	0.65	0.66	-12
-11 -10	0.54 0.48	0.55 0.49	0.56 0.50	0.57 0.51	0.58 0.52	0.59 0.53	0.60 0.54	-11 -10
- 9	+0.43	+0.44	+0.44	+0.45	+0.46	+0.46	+0.47	- 9
- 8	0.37	0.38	0.38	0.39	0.40	0.40	0.41	-8
-7	0.31	0.32	0.32	0.33	0.34	0.34	0.35	- 7
- 6	0.26	0.26	0.26	0.27	0.27	0.28	0.28	- 6
- 5	0.20	0.20	0.21	0.21	0.21	0.22	0.22	- 5
- 4	+0.14	+0.15	+0.15	+0.15	+0.15	+0.16	+0.16	- 4
- 3	0.09	0.09	0.09	0.09	0.09	0.09	0.09	- 3
- 2	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	- 2
- 1	-0.03 -0.08	-0.03 -0.09	-0.03 -0.09	-0.03 -0.09	-0.03 -0.09	-0.03 -0.09	-0.03 -0.09	- 1
+1	-0.14	-0.14	-0.15	-0.15	-0.15	-0.15	-0.16	+ 1
2	0.20	0.20	0.21	0.21	0.21	0.22	0.22	2
3	0.26	0.26	0.27	0.27	0.27	0.28	0.28	3
4	0.31	0.32	0.32	0.33	0.33	0.34	0.35	4
5	0.37	0.37	0.38	0.39	0.40	0.40	0.41	5
+ 6	-0.43	-0.43	-0.44	-0.45	-0.46	-0.46	0.47	+ 6
7	0.48	0.49	0.50	0.51	0.52	0.53	0.53	7
8	0.54	0.55	0.56	0.57	0.58	0.59	0.60	8
9	0.60	0.61	0.62	0.63	0.64	0.65	0.66	9
10	0.65	0.66	0.68	0.69	0.70	0.71	0.72	10
+11	-0.71	-0.72	-0.74	-0.75	-0.76	-0.77	-0.79	+11
13	0.77	0.78	0.80	0.81	0.82	0.84	0.85	12
14	0.82	0.84	0.85	0.87	0.88	0.90	0.91	13
15	0.94	0.95	0.97	0.93	0.94 1.00	0.96 1.02	0.98 1.04	14 15
+16	-0.99	-1.01	-1.03	-1.05	-1.07	-1.08	-1.10	+16
17	1.05	1.07	1.09	1.11	1.13	1.15	1.16	17
18	1.11	1.13	1.15	1.17	1.19	1.21	1.23	18
19	1.16	1.18	1.21	1.23	1.25	1.27	1.29	19
20	1.22	1.24	1.27	1.29	1.31	1.33	1.35	20
+21	-1.28	-1.30	-1.33	-1.35	-1.37	-1.39	-1.42	+21
23	1.34	1.36	1.38	1.41	1.43	1.45	1.48	22
24	1.39	1.41	1.44	1.47	1.49	1.52	1.54	23
25	1.50	1.47	1.50	1.53 1.59	1.55 1.61	1.58 1.64	1.60	24 25

Normal Temperature of the Scale = 13° Reaumur.

Attached Thermom- eter.			Barom	eter in Paris	Lines.			Attached Thermometer.
Degrees of Reaumur.	315	320	325	330	335	340	345	Degrees of Reaumur.
0	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	0
-15	+0.86	+0.88	+0.89	+0.90	+0.92	+0.93	+0.95	-15 -14
-14 -13	0.80	0.75	0.76	0.84	0.78	0.79	0.81	-13
-13 -12	0.74	0.68	0.69	0.70	0.71	0.73	0.74	-12
-11	0.61	0.62	0.63	0.64	0.65	0.66	0.67	-11
-10	0.54	0.55	0.56	0.57	0.58	0.59	0.60	-10
- 9	+0.48	+0.49	+0.50	+0.50	+0.51	+0.52	+0.53	- 9
-8	0.42	0.42	0.43	0.44	0.44	0.45	0.46	-8
-7	0.35	0.36	0.36	0.37	0.37	0.38	0.39	- 7
- 6	0.29	0.29	0.30	0.30	0.31	0.31	0.32	- 6
- 5	0.22	0.23	0.23	0.24	0.24	0.24	0.25	- 5
- 4	+0.16	+0.16	+0.17	+0.17	+0.17	+0.17	+0.18	- 4
- 3	0.10	0.10	0.10	0.10	0.10	0.10	0.11	- 3
- 2	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.04	- 2
- 1	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	- 1
0	-0.10	-0.10	-0.10	-0.10	-0.10	-0.10	-0.10	0
+ 1	-0.16	-0.16	-0.16	-0.17	-0.17	-0.17	-0.17	+ 1
2	0.22	0.23	0.23	0.23	0.24	0.24	0.24	2
3	0.29	0.29	0.30	0.30	0.31	0.31	0.31	3
4	0.35	0.36	0.36	0.37	0.37	0.38	0.38	4
5	0.42	0.42	0.43	0.44	0.44	0.45	0.45	5
+ 6	-0.48	-0.49	-0.49	-0.50	-0.51	-0.52	-0.53	+ 6
7	0.54	0.55	0.56	0.57	0.58	0.59	0.60	7
8	0.61	0.62	0.63	0.64	0.65	0.66	0.67	8
9	0.67	0.68	0.69	0.70	0.71	0.72	0.74	9
10	0.74	0.75	0.76	0.77	0.78	0.79	0.81	10
+11	-0.80	-0.81	-0.82	-0.84	-0.85	-0.86	-0.88	+11
12	0.86	0.88	0.89	0.90	0.92	0.93	0.95	12
13	0.93	0.94	0.96	0.97	0.99	1.00	1.02	13
14	0.99	1.01	1.02	1.04	1.05	1.07	1.09	14
15	1.05	1.07	1.09	1.10	1.12	1.14	1.16	15
+16	-1.12	-1.14	-1.15	-1.17	-1.19	-1.21	-1.23	+16
17	1.18	1.20	1.22	1.24	1.26	1.28	1.30	17
18	1.25	1.27	1.29	1.31	1.33	1.35	1.37	18
19 20	1.31	1.33	1.35	1.37	1.39 1.46	1.41 1.48	1.44	19 20
		The Francisco				31.	E NISE	
+21	-1.44	-1.46	-1.48	-1.51	-1.53	-1.55	-1.58	+21
22	1.50	1.53	1.55	1.57	1.60	1.62	1.65	22
23	1.57	1.59	1.62	1.64	1.67	1.69	1.72	23
24 25	1.63	1.66	1.68	1.71	1.73	1.76	1.79	24
40	1.69	1.72	1.75	1.78	1.80	1.83	1.86	25

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### TABLES

FOR CORRECTING THE

DEPRESSION OF THE BAROMETRICAL COLUMN

DUE TO CAPILLARY ACTION.

C

### CORRECTION FOR CAPILLARY ACTION.

It is known that the effects of capillary action are not the same in different liquids. In a tube plunged in water, the liquid in the tube rises higher than the level of the water in the vessel, and terminates by a concave surface, which is called a concave meniscus. In a tube plunged in mercury the liquid in the tube stands lower than the mercury in the vessel, and terminates by a convex surface, or a convex meniscus. It is thus evident that the mercurial column in the tube of a Barometer does not rise to its true height, and that it needs to be corrected for the depression due to capillarity, before it indicates the real pressure of the atmosphere.

La Place, in the Mécanique Céleste, Tom. IV., has shown that the value of that cor rection depends upon the form of the meniscus, and gave a formula to compute it As this form varies in tubes of different bores, so does the depression, which diminishes as the diameter of the tube increases. The form of the meniscus, however was supposed to be the same in tubes of the same diameter, and constant in the same tube; and on this supposition the tables generally used for correcting the capillary action have been computed. But more accurate observations have proved that owing to various causes not yet all well understood, the form of the meniscus is often different in tubes of the same diameter, and that it is even variable in the tube of the same instrument.

It thus became necessary to construct new tables, taking into consideration, in a given case, both the diameter of the tube and the form of the meniscus. Such tables, with a double entry, have been given by Schleiermacher, in the Bibliothèque Universelle de Genève, Tom. VIII.; by Bravais, in the Annales de Physique et de Chimie, Tom. V. p. 508; and by Delcros. The numbers in these tables agree very closely; but as Delcros's table is more extended than that of Schleiermacher, and in a more convenient form than that of Bravais, it is given below, together with a reduction of it to English measures, for the ordinary use.

The other tables may serve for comparison.

Table XXII., from the Report of the Committee of Physics and Meteorology of the Royal Society of London, 1840, gives the correction to be applied to English barometers for capillary action in boiled and unboiled tubes. It takes into account the diameter of the tube, but not the variations of the height of the meniscus, or of the convexity which terminates the barometrical column. This last element is supposed to be in its normal state, and constant.

Tables XXIII. and XXIV., by Delcros, in the Annuaire Météorologique de France, for 1849, give the means of finding the true correction to be applied to metrical barometers for capillary action.

C

The first shows the normal height of the meniscus when in contact with the air (as is the case in the inferior branch of a siphon barometer), and in the barometric vacuum at the top of the column, in tubes of different bores. It enables the observer to judge better of its variations.

Table XXIV. has been calculated by Delcros after the formulas of Schleiermacher, making the constant x equal to  $6^{\text{mm}}.5278$ , being the mean value between that of Gay-Lussac =  $6^{\text{mm}}.5262$ , and that of Schleiermacher =  $6^{\text{mm}}.5295$ . It gives the amount of the capillary action in millimetres of mercury, taking into account both the size of the bore, or the internal radius of the tube, which will be found in the vertical argument, and the height of the meniscus, given in the horizontal argument. The internal radius of the tube is supposed to be known; the height of the meniscus, or the vertical distance from the base, that is, from the sharp line where the mercury ceases to be in contact with the walls of the tube, to the very top of the convexity, can be ascertained by measuring it several times by means of the vernier.

Example: — Suppose the internal radius of the tube to be  $3^{mm}.2$ , and the height of the meniscus to be  $0^{mm}.8$ ; seek in the first vertical column the number  $3^{mm}.2$ ; follow then the horizontal line as far as the vertical column headed  $0^{mm}.8$ , you find there the number  $0^{mm}.776$ , which is the amount of the depression due to capillary action, or the value of the correction to be added to the observation.

Table XXV. is taken from Pouillet's Eléments de Physique, Vol. II. p. 698 (1853). Table XXVI. is found in Gehler's Physicalisches Wörterbuch, and in Schubarth, Physicalische Tabellen, p. 21.

Table XXVII., which is Delcros's table reduced into English measures, gives the means of correcting with more accuracy the indications of the English barometers. For its use, see, above, the explanation to Table XXIV.

Table XXVIII. is from Baily's Astronomical Tables.

XXII. TABLE FOR THE CORRECTION TO BE ADDED TO ENGLISH BAROMETERS FOR CAPILLARY ACTION.

Diameter	Correct	ion for
of Tube.	Unboiled Tubes.	Boiled Tubes.
Inch.	Inch.	Inch.
0.60	0.004	0.002
0.50	0.007	0.003
0.45	0.010	0.005
0.40	0.014	0.007
0.35	0.020	0.010
0.30	0.028	0.014
0.25	0.040	0.020
0.20	0.060	0.029
0.15	0.088	0.044
0.10	0.142	0.070

XXIII. TABLE OF THE HEIGHT OF THE MENISCUS OF THE BAROMETRICAL COLUMN.

Internal Radius of the Tube in	Normal Heig niscus in M	ht of the Me- Iillimetres.
Millimetres.	In the Air.	In the Vacuum.
1	0.427	0.34
2	0.795	0.64
3	1.079	0.86
4	1.287	1.03
5	1.413	1.13
6	1.488	1.19
7	1.524	1.22
	3 3 g g/	

VERTICAL ARGUMENT = INTERNAL RADIUS OF TUBE. HORIZONTAL ARGUMENT = HEIGHT OF MENISCUS IN MILLIMETRES.

Radius of			10.				10 8	Height of	the Men	iscus in I	Height of the Meniscus in Millimetres								Radius of
the Tube in Milli- metres.	0.1	0.5	0.3	0.4	0.5	9.0	2.0	0.8	6.0	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	the Tube in Milli- metres.
1.0	Millim. 1.268		Millim.	Millim. 4.396	Millim. 5.085	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	1.0
1.2	0.876			3.162	3.728	4.190	3	3	3		3	3	3	3	3	3	3	3	1.2
1.4	0.638	-		2.363	2.825	3.218	3.542	2 0	3 3	3 8	3 3	3 3	2 3	3 3	3 3	3 3	3 3	3 3	1.4
0.89	0.378	0.747	1.103	1.437	1.746	2.024	2.270	2.483	2.662	3	2	3	3	3	3	3	3	3	. o
	1	_		46			7	14		14.0									
20.0	0.302	0.598	0.885	1.158	1.413	1.648	1.859	2.046	2.209	2.348	9004	3 3	3 3	3 3	3 3	3 3	3 3	3 3	2.0
2 6	0.203		0.599	0.787	0.966	1.135	1.292	1.436	1.565	1.680	1.780	1.866	3	3	3	3	3	3	2.6
2.6	0.170		0.502	0.661	0.813	0.958	1.093	1.218	1.332	1.436	1.528	1.608	1.676	1 511	3 3	3 3	3 3	3 3	2.6
7.0	0.140	0.200	0.440	00000	160.0	0.010	0.305	1.0.1	1.142	1.200	1.010	1.032	004-1	110.1		**			6.9
3.0	0.122	0.243	0.362	0.478	0.591	0.698	0.800	0.896	0.985	1.068	1.143	1.210	1.270	1.322	1.368	1 938	3 3	2 3	3.0
3.4	0.091	0.181	0.269	0.356	0.441	0.523	0.601	0.675	0.745	0.810	0.871	0.926	0.976	1.021	1.061	1.095	3	3	3.4
9.8	0.079	0.157	0.234	0.310	0.384	0.455	0.524	0.590	0.652	0.710	0.764	0.814	0.860	0.901	0.938	0.970	2000	3 3	3.6
	0.069	0.137	0.505	0.271	0.336	0.339	0.459	0.517	0.572	0.624	0.6/3	0.718	097.0	0.797	0.831	0.861	0.887		n n
4.0	090.0	0.120	0.180	0.238	0.295	0.350	0.404	0.455	0.504	0.551	0.594	0.635	0.673	0.707	0.738	0.766	0.790	* 5	4.0
4 4	0.053	0.094	0.140	0.210	0.250	0.273	0.356	0.356	0.395	0.432	0.526	0.500	0.531	0.559	0.585	0.609	0.630	33	4 4
4.6	0.045	0.083	0.124	0.164	0.504	0.242	0.280	0.316	0.351	0.384	0.416	0.445	0.473	0.499	0.522	0.544	0.563	3	4.6
4.8	0.037	0.074	0.110	0.146	0.181	0.215	0.249	0.281	0.312	0.342	0.370	0.397	0.422	0.445	0.467	0.486	0.504	3	4.8
5.0	0.033	0.065	860.0	0.130	0.161	0.192	0.221	0.250	0.278	0.305	0.330	0.354	0.377	0.398	0.418	0.436	0.452	8	5.0
5.2	0.029	0.058	0.087	0.116	0.144	0.171	0.198	0.224	0.248	0.272	0.295	0.317	0.337	0.356	0.374	0.390	0.405	0.418	27.2
4. 6.	0.020	0.052	0.070	0.092	0.128	0.137	0.158	0.200	0.199	0.218	0.204	0.255	0.302	0.287	0.301	0.315	0.327	0.338	4. 6.
5.8	0.021	0.042	0.062	0.083	0.103	0.122	0.142	091.0	0.178	0.196	0.213	0.228	0.243	0.257	0.271	0.283	0.294	0.304	5.8
6.0	0.019	0.037	0.056	0.074	0.092	0.110	0.127	0.144	0.160	0.176	0.191	0.205	0.219	0.231	0.243	0.254	0.264	0.273	6.0
6.2	0.017	0.034	0.050	190.0	0.083	0.099	0.114	0.129	0 144	0.158	0.172	0.185	0.197	0.508	0.219	0.229	0.238	0.246	6.2
6.4	0.015	0.030	0.045	0.060	0.074	0.089	0.103	0.116	0.130	0.142	0.154	0.166	0.177	0.187	0.197	0.206	0.214	0.221	6.4
6.8	0.012	0.024	0.037	0.034	0.061	0.020	0.084	0.095	0.105	0.116	0.126	0.135	0.144	0.153	0.160	0.168	0.174	0.180	6.8
7.0	0.011	0.022	0.033	0.044	0.055	0.065	0.075	0.085	0.095	0.105	0.114	0.122	0.130	0.138	0.145	0.152	0.158	0.163	7.0
A STATE OF THE PARTY OF THE PAR		ACCOUNT OF THE PERSON				Carried Section	The state of the s			-						-			

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FROM POULLET.

Internal Diameter of Tube.  Millimetres. 2.00 2.50 3.00 3.50 4.00	Millimetres. 4.579 3.595 2.902 2.415 2.053	Differences.  Millimet.  0.985  0.692  0.487  0.362  0.301	Internal Diameter of Tube.  Millimetres. 8.50 9.00 9.50 10.00 10.50	Depression.  Millimetres. 0.604 0.534 0.473 0.419 0.372	Differences.  Millimet.  0.070 0.061 0.054 0.047 0.042	Internal Diameter of Tube.  Millimetres. 15.00 15.50 16.00 16.50 17.00	Millimetres. 0.127 0.112 0.099 0.087 0.077	Millimet.  0.015 0.013 0.012 0.010 0.009
4.50	1.752	0.245	11.00	0.330	0.037	17.50	0.068	0.008
5.00	1.507	0.201	11.50	0.293	0.033	18.00	0.060	0.007
5.50	1.306	0.170	12.00	0.260	0.030	18.50	0.053	0.006
6.00	1.136	0.141	12.50	0.230	0.026	19.00	0.047	0.006
6.50	0.995	0.118	13.00	0.204	0.023	19.50	0.041	0.005
7.00	0.877	0.102	13.50	0.181	0.020	20.00	0.036	0.004
7.50	0.775	0.091	14.00	0.161	0.018	20.50	0.032	
8.00	0.684	0.080	14.50	0.143	0.016	21.00	0.028	

#### XXVI. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION.

Internal		Depression	according t	0	Internal		Depression	according	to
Diameter of Tube.	La Place.	Young.	Ivory.	Cavendish.	Diameter of Tube.	La Place.	Young.	Ivory.	Cavendish.
Millimetres.	Millim.	Millim.	Millim.	Millim.	Millimetres.	Millim.	Millim.	Millim.	Millim.
2.00	4.454	4.887	4.888	4.472	11.50	0.315		Selection of	0.00
2.50	3.568				12.00	0.281	0.242	0.253	0.200
3.00	2.918	2.986	2.988	3.054	12.50	0.250			
3.50	2.442			200	13.00	0.223	0.188	0.196	0.170
4.00	2.068	2.063	2.066	2.187	13.50	0.198		1 2	
4.50	1.774				14.00	0.176	0.144	0.152	0.150
5.00	1.534	1.510	1.513	1.735	14.50	0.156		The state of	
5.50	1.337		The street		15.00	0.137	0.111	0.118	0.131
6.00	1.171	1.139	1.134	1.377	15.50	0.121			
6.50	1.030				16.00	0.107	0.088	0.087	200
7.00	0.909	0.869	0.868	1.073	16.50	0.094			
7.50	0.803	- 1	- 9		17.00	0.083	0.068	0.071	
8.00	0.712	0.669	0.673	0.820	17.50	0.073			
8.50	0.632			100	18.00	0.064	0.053	0.054	- 10 E
9.00	0.562	0.517	0.521	0.608	18.50	0.056		Charles	
9.50	0.500			th.do.	19.00	0.049	0.041	0.042	92,0
10.00	0.445	0.402	0.406	0.406	19.50	0.043			
10.50	0.397			- 60a	20.00	0.038	0.031	0.031	nico.
11.00	0.354	0.311	0.316	0.270	20.50	0.034	4		1200
11.50	0.315	100	OF P	0519	21.00	0.030	0.024	0.024	SUPPLY S

XXVII. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION, REDUCED INTO ENGLISH INCHES FROM DELCROS'S TABLE.

Internal Diam- eter				Heigh	nt of Me	niscus i	in Thou	sandths	of an I	English	Inch.			7
of Tube.	5	10	15	20	25	30	35	40	45	50	55	60	65	70
Eng. In.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch
0.10	0.040			-	0.155		NEW P	170				1154		
0.12	.027	.053	.076	.097	.114		50	- 000		and S		TO THE		
0.14	.019	.038	.056	.071		0.097	THE STATE OF	o line	31			DOM:		
0.16	.015	.029	.042	.055	.066		0.084	(=12	100			1000		
0.18	.011	.022	.033	.043	.052	.060	.067	0.073				RIPAL		
0.20	.009	.018	.026	.034	.042	.049	.055	.060	0.064			TE.	t ko	
0.22	.007	.014	.021	.028	.034	.040	.045	.049	.053	0.057		Till the last		
0.24	.006	.012	.017	.023	.028	.033	.037	.041	.045	.048	0.050	ata h		
0.26	.005	.010	.014	.019	.023	.027	.031	.035	.038	.040	.043	0.045		
0.28	.004	.008	.012	.016	.019	.023	.026	.029	.032	.034	.036	.038		
0.30	.003	.007	.010	.013	.016	.019	.022	.025	.027	.029	.031	.033	0.034	-
		AV.		= 11			10.9		7			1180	FRA	255
0.32	.003	.006	.009	.011	.014	.016	.019	.021	.023	.025	.027	.028	.030	3.5
0.34	.002	.005	.007	.010	.012	.014	.016	.018	.020	.022	.023	.024	.026	63
0.36	.002	.004	.006	.008	.010	.012	.014	.016	.017	.019	.020	.021	.022	
0.38	.002	.004	.005	.007	.009	.010	.012	.013	.015	.016	.017	.018	.019	
0.40	.002	.003	.005	.006	.008	.009	.010	.012	.013	.014	.015	.016	.017	2 10
0.42	.001	.003	.004	.005	.007	.008	.009	.010	.011	.012	.013	.014	.015	0.01
0.11	.001	.002	.004	.005	.006	.007	.008	.009	.010	.011	.011	.012	.013	.01
0.44	.001	.002	.003	.003	.005	.006	.007	.008	.008	.009	.010	.012	.013	.01
0.48	.001	.002	.003	.004	.003	.005	.006	.007	.007	.008	.009	.009	.010	.01
0.48	.001	.002	.003	.004	.004	.003	.005	.006	.006	.003	.008	.009	.008	.00
0.50	.001	.002	.002	.003	.004	.004	.005	.005	.006	.006	.007	.003	.007	.00
0.54	.001	.001	.002	.003	.003	.003	.003	.004	.005	.005	.006	.006	.006	.00
Her.	5	10	15	20	25	30	35	40	45	50	55	60	65	70

EXVIII. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION, EXPRESSED IN ENGLISH INCHES. — BAILY.

Diameter of Tube.	Depression according to			Diameter	Depression according to		
	Ivory.	Young.	La Place.	of Tube.	Ivory.	Young.	La Place.
Eng. Inch.	Eng. Inch.	Eng. Inch.	Eng. Inch.	Eng. Inch.	Eng. Inch.	Eng. Inch.	Eng. Inch
0.05	0.2949	0.2964	0	0.35	0.0212	0.0196	0.0216
0.10	.1404	.1424	.1394	0.40	.0154	.0139	.0159
0.15	.0865	.0880	.0854	0.45	.0112	.0100	.0117
0.20	.0583	.0589	.0580	0.50	.0082	.0074	.0087
0.25	•0409	.0404	.0412	0.60	.0043	.0045	.0046
0.30	-0293	.0280	.0296	0.70	.0023		.0024
0.35	0.0212	0.0196	0.0216	0.80	0.0012	0	0.0013



# METEOROLOGICAL TABLES

IV.

HYPSOMETRICAL TABLES.

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### BAROMETRICAL

# MEASUREMENT OF HEIGHTS,

OR

### TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

D

#### HYPSOMETRICAL TABLES

FOR

# COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

Numerous determinations of altitude are one of the great desiderata of physical sience, and no more ready means for obtaining them is at the disposal of the scienfic man than the Barometer. A traveller, furnished with the improved and consinent instruments we can now command, and with some experience in using them, in take a large number of barometric observations for determining heights, at the est of little trouble or time. It is, however, quite otherwise with the computations y which the results are obtained. The prospect of that tedious and time-robbing bor not only too often cools the zeal of the observer, but a vast amount of data stually collected remain of no avail from the want of having been computed.

The object of this much enlarged set of Hypsometrical Tables is to facilitate the sk of the computer. It contains practical tables adapted to the three usual baroetrical scales, and, among them, No. I., II., and V. are so disposed as to dispense ith the use of logarithms, and to reduce the computation to the simplest arithmetical operations. The others suppose the use of logarithms, a method which may still preferred by some observers.

As these various tables represent the development of the principal formulæ which are been proposed, the computer is enabled to compare the results obtained by uch of them, and to select that which he most approves.

These formulæ may be referred to two classes, the respective types of which are aplace's and Bessel's formulæ.

Laplace, in the Mécanique Céleste, Tom. IV. p. 292, gave a complete solution of e problem, and proposed a formula which soon superseded the older and less accute formulæ of De Luc, Shuckburgh, and others. The coefficients which enter in it ere derived from the best determinations of the needed physical constants which sience could then furnish, the most important of which are the relative weight of e air and of the mercury, and the rate of expansion of air by heat. The first was sumed to be 10157, according to the experiments of Biot and Arago; and the bametrical coefficient deduced from it, 18317 metres. This coefficient was, hower, empirically increased to 18336 metres, in order to adjust the results of the rmula to those furnished by the careful trigonometrical measurements made by amond for the purpose of testing its correctness. It becomes 18393 metres when cluding the correction due to the effect of the decrease of gravity with the height the density of the mercurial column and of the air. The coefficient expressing e expansion of the air by heat, as determined by Gay-Lussac, viz. 0.00375 of its alk for one Centigrade degree, was adopted, but Laplace increased it to 0.004, in der to take into the account the effect of the greater expansive power of the vapors ontained in the atmosphere.

D

These values have been retained in the different formulæ proposed later by Gauss in Schumacher's Jahrbuch for 1840, by Schmidt, Mathem. und Physische Geographie II. p. 205, and by Baily, Astronomical Tables, p. 183, which, therefore, only change the form without changing the results. D'Aubuisson, in his formula and tables, Trait de Géognosie, p. 488, only reduced the barometrical coefficient to its theoretica value, which he determined to be 18365 metres, leaving unchanged the other coefficients of Laplace's formula.

Bessel first introduced, in his formula, Astronomische Nachrichten, No. 356, a sep arate correction for the effect of moisture. The correction for the temperature of the air is computed in his tables for two values of the coefficient, that of Gay-Lussac 0.00375, and that of Rudberg, 0.00365. Laplace's barometrical coefficient is retained, but the correction for the decrease of gravity is considerably modified.

In Elie Ritter's formula, in the Mémoires de la Societé de Physique de Genève Tom. XIII. p. 343, the corrections for temperature and moisture are also separated but other values of the barometrical and thermometrical coefficients, derived from Regnault's determinations, are used, and a new method is proposed for applying the correction due to the expansion of air, which is made proportional to the square of the difference between the observed temperatures at each station.

Baeyer's formula, recently published in Poggendorf's Annalen der Physik une Chemie, Tom. XCVIII. p. 371, does not belong to either of the two classes just men tioned; for while it keeps Laplace's barometrical and thermometrical coefficients, i corrects the effect of temperature by a method analogous to that of Ritter, and it en tirely neglects the effect of aqueous vapor.

In the following set the tables of Delcros, Guyot, and Loomis develop the formulof Laplace. The much larger tables of Delcros render unnecessary those of Olt manns, which are yearly reprinted in the Annuaire du Bureau des Longitudes. In stead of Gauss's tables will be found the tables of Dippe, which are computed fron the same formula, but are more extended. Baily's tables close the first series. The tables of Plantamour, computed from Bessel's formula, are given here in preference to Bessel's tables, because Plantamour substituted for Laplace's barometrical coefficient that derived from the probably more accurate determination of the relative weigh of the air and mercury by Regnault, viz. 18404.8 metres. E. Ritter's tables, computed from his own formula, give perhaps, in extreme cases, better results; bu as, in ordinary circumstances, the altitudes obtained do not much differ from those furnished by the less complicated tables of Plantamour, they were not reprinted here.

The miscellaneous tables which follow furnish useful materials for solving severa questions connected with the barometrical measurements.

Regnault's table of Barometric Pressures corresponding to Temperatures of the Boiling Point of Water, revised by Moritz, and its reduction to English measures, will be found a valuable addition for thermometrical measurements of heights.

The Appendix to the Hypsometrical Tables now offers, in a new form, a complete series of tables for the comparison of the different measures of length generally used for indicating altitudes, the convenience of which will be fully appreciated by those who have attempted to collect and to use the abundant contributions furnished by all civilized nations to that branch of geographical science.

D

#### TABLES

FOR

# DETERMINING DIFFERENCES OF LEVEL BY MEANS OF BAROMETRICAL OBSERVATIONS,

COMPUTED FROM THE COMPLETE FORMULA OF LAPLACE,

By M. T. DELCROS.

#### Construction of the Tables.

If we take z = difference of level of the two barometers, a = earth's mean radius = 6366200 metres, L = mean latitude between the two stations,

and further: -

At Station. 
$$\begin{cases} h = \text{observed height of the barometer,} \\ T = \text{temperature of the barometer,} \\ t = \text{temperature of the air,} \\ h' = \text{observed height of the barometer,} \\ T' = \text{temperature of the barometer,} \\ t' = \text{temperature of the air,} \end{cases}$$

and if we make finally H = h + h'.  $(\frac{T-T'}{6196})$ ,

we shall have, according to Laplace, the following general and complete equation: -

$$z=18336 ext{ metres} imes \left\{ egin{array}{ll} (1+rac{2.(t+t')}{1000}) \\ (1+0.0028371 ext{ cos. 2. L}) \\ (1+rac{z}{a}). & ext{Log. } (rac{\hbar}{H})+rac{z}{a} ext{ 0.868589}) \end{array} 
ight\}$$

after the proper transformations this equation becomes: -

$$z = \text{Log.} \left(\frac{h}{H}\right) \text{ 18336 metres} \times \left\{ \begin{array}{l} \left(1 + \frac{2. \ (t + t')}{1000}\right) \\ \left(1 + 0.0028371 \text{ cos. 2. L}\right) \\ \left(1 + \frac{\left(\log. \left(\frac{h}{H}\right) + 0.868589\right). \frac{z}{a}}{\text{Log.} \left(\frac{h}{H}\right)} \right) \end{array} \right\}$$

introducing into this expression the value in metres of a, the earth's mean radius, making  $z = \text{Log.}\left(\frac{h}{H}\right)$  18336 and Log.  $\left(\frac{h}{H}\right) = \left(\frac{z}{18336}\right)$ , which can be done without sensible error, the above formula takes the following form, sufficiently accurate for practical purposes:—

$$z = \text{Log.}\left(\frac{h}{H}\right)$$
. 18336 metres  $\times \left\{ \begin{array}{l} \left(1 + \frac{c_2 \cdot (t + t')}{1000}\right) \\ \left(1 + 0.0028371 \text{ cos. 2. L}\right) \\ \left(1 + \frac{z + 15926}{6366200}\right) \end{array} \right\}$ 

the four factors of which can easily be developed in tables, as has been done by Mr. Oltmanns. But though this savant chose to develop also the second factor, I found it better not to do so, partly because the calculation of it is very easy, and also on account of the great extent it would have been necessary to give to this table, in order to avoid troublesome interpolations.

In the calculation of h'.  $\left(\frac{T-T'}{6196}\right)$ , Mr. Oltmanns used the constant coefficient of the absolute expansion of the mercurial column; I took that of the relative expansion of the mercury and of the brass scale. It is obvious, therefore, that if the scale of the barometer employed was of wood, glass, iron, or of another substance, it would be necessary to make use of as many different coefficients, and the Table II. could not be used. Moreover, Oltmanns combined the last two factors of the general formula in one single table with double entry. This table I have calculated, extending it sufficiently to avoid a double interpolation; but as it seemed to me much too extensive, I substituted for it Tables III. and IV., which are more condensed, without rendering any troublesome interpolation necessary.

I carried the calculation of these tables beyond the limits at which Oltmanns chose to stop, in order that they may answer for the most extreme cases.

At the head of each table will be found the factor of which it is the development; this makes any other explanation superfluous.

All these tables give, at sight, the numbers wanted; only when very great precision is desired, a slight interpolation, at sight, and very easy to apply, may be required. My principal object was to relieve the computer of the troublesome and annoying labor of interpolations.

l added to these four tables the small Table V., taken from the Annuaire du Bureau des Longitudes of Paris. It will be seldom used.

When calculating differences of level, in the same order, with the tables, and by the complete formula of Laplace, the results thus obtained never differ by more than one decimetre in the most extreme cases. The following example will illustrate this statement. I take the observation made in a balloon, by Gay-Lussac, at Paris, as an extreme case, which is very well adapted to manifest the errors of the tables, if there were any, by comparing the results obtained by means of them with those of the direct calculation according to the complete formula of Laplace, from which they are derived.

Example of Calculation by the complete Formula of Laplace and by the Tables

Height of the Balloon of Gay-Lussac.

The observation gave: -

Balloon 
$$h' = 328.80$$
  $T' = -9.5$   $t' = -9.5$   
Paris  $h = 765.68$   $T = +30.8$   $t = +30.8$ 

$$T - T' = +40.3$$
  $(t+t') = +21.3$  et  $2(t+t') = 42^{\circ}.6$ 

With these data the formula of Laplace gives the following calculation: -

Log. 
$$h'$$
. = 328.80 = 2.5169318  
Log.  $(T - T') = +40.3$  = 1.6053050  
Log. dilat. coefficient = 0.0001614 = 6.2079035

Corr. 
$$a = +$$
 $h' =$ 

$$\begin{array}{c}
Milli. \\
2.14 \log. = 0.3301403 \\
328.80
\end{array}$$

$$H = 330.94 \text{ log.} = 2.5197480$$
 $\log h = 765.68 = 2.8840473$ 

(Log. 
$$h$$
 — Log. H) = Difference of Log. =  $0.3642993$ 

Log. of (Log. 
$$h$$
 — log. H) = 9.5614583  
Log. general coefficient =  $18336$  = 4.2633046

Log. 
$$\left(\frac{h}{H}\right)$$
 18336  $= (A + a) = 3.8247629$   
Corresponding number  $= 6679.79 = (A + a)$ 

Log. cos. 2 L = 
$$97^{\circ}$$
 40' = - 9.1251872

Log. constant = 
$$0.0028371 = +$$
 7.4528746  
Log. (A + a) = 6679.79. = + 3.8247629

Log. ( 
$$(0.0028371. \text{ Cos. } 2 \text{ L}) \times (A + a)$$
 ) =  $-0.4028247$ 

Corresponding number =-2.53

$$(A + a + \beta) = 6677.26$$

For temp. air = 
$$v = 284.45$$
 =  $(6.677 \times 42.6)$ 

$$(A + \alpha + \beta + \nu) = 6961.71$$

$$Constan = + 15926$$

Compt. log. 
$$a = 6366200 \dots \text{Log.} \dots = 3.1961197$$

$$(A + a + \beta + 1) = 6961.71 \dots \text{Log.} \dots = 3.8427153$$

$$\delta = +$$
 25.03 Log. =  $+$  1.3984372

$$(A + a + \beta + v + \delta) = 6986.74$$

Altitude of balloon = 7035.44 by the formula of Laplace.

Now let us calculate by the tables, placing side by side the corresponding results given by the formula of Laplace.

Balloon 
$$h' = 328.80$$
  $T' = -9.5$   $t' = -9.5$   $Paris h = 765.68$   $T = +30.8$   $t = +30.8$   $t = +30.8$  with  $\begin{cases} h' = 328.80 \\ h = 765.68 \end{cases}$  Table I. gives  $\begin{cases} 1478.4 \\ 8209.8 \end{cases}$  By the formula of Laplace we found: 
$$A = 6731.4$$
 with  $(T' - T) = -40^{\circ}.3$ , Table II. gives  $a = -52.0$  
$$(A + a) = 6679.4$$
 
$$(A + a + \beta) = 6679.1$$
 
$$(A + a + \beta) = 6677.1$$
 
$$(A + a + \beta) = 6677.1$$
 
$$(A + a + \beta) = 6677.1$$
 with  $2(t + t')$  direct calculation gives  $v = +284.5$  
$$+284.45$$
 
$$(A + a + \beta + v) = 6961.6$$
 
$$(A + a + \beta + v) = 6961.6$$
 
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$$(A + a + \beta + v) = 6961.6$$
 
$$(A + a + \beta + v) = 6961.6$$
 
$$(A + a + \beta + v) = 6961$$

Two results which are sensibly identical. This ought not to astonish us; the tables being the exact development of the formula, they ought to give the same results, provided in both cases nothing has been neglected, and the four factors have been calculated in the same relative order.

DELCROS.

## Disposition and Use of the Tables.

The disposition of the tables is the following: -

In Table I., the first column on the left contains the height of the barometer in millimetres, corrected for the error of the instrument.

The second column headed N (number), gives in metres the first two figures of the number corresponding to each height of the barometer in the first column; the third column, headed 0.0, gives the remaining figures for the full number of millimetres; the following columns give the remaining figures for the same number of millimetres and each decimal fraction of a millimetre which may follow it. The value of the hundredths is to be found in the last column.

Example: - Height of Barometer = 761.00.

We look out in the first column for the number 761, and we find on the same line in the second column, 81; in the third column, headed 0.0, or full number, 61.1. The corresponding number is thus 8161.1 metres.

Height of barometer = 761.35.

The second column gives 81; the column headed 0.3 gives, on the same line, 64.2. The corresponding number is then 8164.2. Adding the value of five hundredths of millim., being 0°.5, as indicated in the last column, we have 8164.7 metres, corresponding to 761.35 millim.

The other four tables need no further explanation.

To calculate, by means of the tables, a difference of level from two barometrical observations, proceed in the following manner:—

- 1. Take the height of the barometer at the lower station, or h, and seek in Table I. the number corresponding to this height. Seek likewise the number corresponding to the height of the barometer at the upper station. Subtract the second from the first. The remainder is the approximate difference of level between the two stations. Then apply the following corrections.
  - 2. Correction to be applied for the temperature of the barometers.

If T' be the temperature of the attached thermometer at the upper station, and T that of the attached thermometer at the lower station, take the difference, or T' - T, and seek in Table II. the number corresponding to this difference.

When T' is smaller than T, that is, when the temperature of the attached thermometer of the upper station is lower than that of the lower station, the correction is to be *subtracted* from the approximate height; when T' is greater than T, it is to be *added*.

3. Correction for the temperature of the air.

The first correction having been applied, multiply the number obtained, or N, by the double sum of the temperatures of the air at both stations, and divide the product by 1000; the number thus found, or the quantity expressed by  $\frac{N}{1000}$ . 2 (t + t') is the correction in metres which is to be *added* to the preceding number N.

- 4. Tables III. and IV. give two corrections; the first due to the decrease of gravitation in latitude, which is to be added when the mean latitude of the places of observation is between the 45th parallel and the equator; and to be subtracted when it is between the same parallel and the poles, as indicated at the head of the columns. The second correction, due to the decrease of gravitation on the vertical line, is always additive.
- 5. Table V. gives another small correction to be added in the case of the lower station being very elevated above the level of the ocean.

#### Examples of Calculation.

Measurement of the Height of Guanaxuato. By M. de Humboldt.

Barometer at the upper station, Barometer at the level of the sea,

$$h' = 600.95$$
  $T' = 21.3$   $t' = 21.3$   
 $h = 763.15$   $T = 25.3$   $t = 25.3$ 

### BAROMETRICAL MEASUREMENT OF HEIGHTS.

Table I. gives the corresponding numbers,		$\begin{cases} h = 8183.5 \\ h' = 6280.8 \end{cases}$
a company of the party of the first of the f	Difference,	1902.7
Table II. gives for T' — T,		<b>—</b> 5.2
	Difference,	1897.5 = N
$\frac{N}{1000}$ . 2 $(t+t')=1.897\times 93.2$ ,		+ 176.8
	Sum,	2074.3
Table III. gives for mean latitude of 21°,		+ 4.3
Table IV. gives for decrease of gravitation	in the vertical line	e, + 6.0
Hence altitude of Guanaxuato above the c	cean,	2084.6

Measurement of the height of Mont Blanc, August 29, 1844. By MM. Bravais and Martins.

Barometer at one metre below the summit, $h' = 424.05$ T' = -	-4.2 t' = -	- <sup>°</sup> .6
Barometer of the Observatory of Geneva, $h = 729.65 \text{ T} =$		
the left barrel contract carry many letting attended to	7 20000	
Table I. gives for numbers corresponding to	h = 7826.0 $h' = 3504.4$	
west to the restriction for the same and the second second	an in <del>terestor</del>	
Difference,	4321.6	
Table II. gives for T' — T,	- 29.3	
Difference,	4292.3	= N
$\frac{N}{1000}$ 2 $(t+t') = 4292 \times 23.4 =$	+ 100.4	
Sum,	4392.7	
Table III. gives for the mean latitude of 46°,	- 0.4	
Difference,	4392.3	TO THE
Table IV. for decrease of gravitation in the vertical line	+ 13.7	
Table V. for the elevation of the lower station,	+ 0.5	
Sum,	4406.5	
Elevation of the lower barometer above the ocean,	407.0	
above the ocean,	407.0	
Hence elevation of upper barometer above the ocean,	4813.5	
Finally, height of the summit of Mont Blanc above the ocean,	4814.5	

TABLE I. — Giving  $A = 18336 \times \log$ . H or h..., argument H or h in Millimetres.

					1							
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
288	4	23.4	26.2	28.9	31.7	34.4	37.2	40.0	42.7	45.5	48.2	1 0.3
289	4	51.0	53.8	56.5	59.3	62.0	64.8	67.5	70.3	73.0	75.8	2 0.5
290	4	78.5	81.3	84.0	86.7	89.5	92.2	95.0	97.7	1 600		3 0.8
290	5		T'S	1.76		100	7 - 8	4		00.4	03.2	4 1.1
291	5	05.9	08.7	11.4	14.1	16.8	19.6	22.3	25.0	27.8	30.5	5 1.4
292	5	33.2	36.0	38.7	41.4	44.1	46.8	49.6	52.3	55.0	57.7	6 1.6
293	5	60.5	63.2	65.9	68.6	71.3	74.0	76.7	79.5	82.2	84.9	7 1.9
294	5	87.6	90.3	93.0	95.7	98.4		15 414		200	E 1	8 2.2
294	6		100-2				01.1	03.8	06.5	09.2	11.9	9 2.4
295	6	14.6	17.3	20.0	22.7	25.4	28.1	30.8	33.5	36.2	38.9	
296	6	41.6	44.3	47.0	49.6	52.3	55.0	57.7	60.4	63.1	65.8	1
297	6	68.4	71.1	73.8	76.5	79.1	81.8	84.5	87.2	89.9	92.5	N. ASEL
298	6	95.2	97.9	00.7	000	05.0	00.0		100	10.0	70.0	- P#= -
298	7	07.0	0	00.5	03.2	05.9	08.6	11.2	13.9	16.6	19.2	11 1 1 1
299	7	21.9	24.5	27.2	29.9	32.5	35.2	37.8	40.5	43.2	45.8	1
		40 =		×0.0			07.5		0	00 m	<b>**</b> 0.0	COMM.
300	7	48.5	51.1	53.8	56.4	59.1	61.7	64.4	67.0	69.7	72.3	Niet W
301	7	75.0	77.6	80.3	82.9	85.5	88.2	90.8	93.5	96.1	98.7	100
302	8	01.4	04.0	06.6	09.3	11.9	14.5	17.2	19.8	22.4	25.1	ŦX I
303	8	27.7	30.3	33.0	35.6	38.2	40.8	43.5	46.1	48.6	51.3	
304	8	54.0	56.6	59.2	61.8	64.4	67.0	69.6	72.3	74.9	77.5	
305	8	80.1	82.7	85.3	87.9	90.5	93.1	95.7	98.3	01.0	00.0	
305	9	000	00.0		7.0	100	100	01.0	24.4	01.0	03.6	No let
306	9	06.2	08.8	11.4	14.0	16.6	19.2	21.8	24.4	27.0	29.6	1 0.3
307	9	32.1 58.0	34.7 60.6	37.3 63.2	39.9 65.8	42.5 68.4	45.1 70.9	47.7	50.3	52.9	55.5	2 0.5
308	9	83.9	86.4	89.0	91.6	94.1	96.7	73.5	76.1	78.7	81.3	3 0.8
309	10	00.0	00.4	83.0	31.0	34.1	30.4	33.3	01.9	04.4	07.0	4 1.0
310	10	09.6	12.1	14.7	17.3	19.8	22.4	25.0	27.5	30.1	32.7	5 1.3
311	10	35.2	37.8	40.3	42.9	45.5	48.0	50.6	53.1	55.7	58.2	6 1.5
312	10	60.8	63.3	65.9	68.4	71.0	73.5	76.1	78.6	81.2	83.7	7 1.8 8 2.1
313	10	86.3	88.8	91.4	93.9	96.4	99.0		.0.0	01.1	00.,	9 2.3
313	11	00.0	00.0	L I WALL	00.0	00.1	00.0	01.5	04.1	06.6	09.1	9 12.0
314	11	11.7	14.2	16.7	19.3	21.8	24.3	26.9	29.4	31.9	34.5	
315	11	37.0	39.5	42.0	44.6	47.1	49.6	52.1	54.7	57.2	59.7	0 1
316	11	62.2	64.8	67.3	69.8	72.3	74.8	77.3	79.9	82.4	84.9	4
317	11	87.4	89.9	92.4	94.9	97.4	99.9	W par	1 4.34	- Ships	TAY WES	o Salah
317	12	in top	1 1 100	1 32	Heist	A Company	15.4	02.4	05.0	07.5	10.0	1213
318	12	12.5	15.0	17.5	20.0	22.5	25.0	27.5	30.0	32.5	35.0	THE PARTY
319	12	37.5	40.0	42.5	45.0	47.5	50.0	52.4	54.9	57.4	59.9	12-1
320	12	62.4	64.9	67.4	69.9	72.3	74.8	77.3	79.8	82.3	84.8	
321	12	87.2	89.7	92.2	94.7	92.1	99.6	TEXA	1 1 100	1 214	5.4	AR PERS
321	13	1100	- 5	19139	1.75	- Paris	THAT	02.1	04.6	07.1	09.5	WE OR S
322	13	12.0	14.5	17.0	19.4	21.9	24.4	26.8	29.3	31.8	34.2	1100
323	13	36.7	39.2	41.6	44.1	46.6	49.0	51.5	53.9	56.4	58.9	
324	13	61.3	63.8	66.2	68.7	71.1	73.6	76.1	78.5	81.0	83.4	and a
325	13	85.9	88.3	90.8	93.2	95.7	98.1	3.50	18.40	NAME OF THE PERSON OF THE PERS		
325	14		1 SEAL	1 3 3 3		133		00.5	03.0	05.4	07.9	HIS
Par			7			1					ALC: N	
Barom- eter Hor h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.

326 to 364mm.

		Contract of the last			320	6 to 3	364 <sup>mn</sup> .					
Barometer Horh.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Met
326	14	10.3	12.8	15.2	17.6	20.1	22.5	25.0	27.4	29.8	32.3	1 10.2
327	14	34.7	37.2	39.6	42.0	44.5	46.9	49.3	51.7	54.2	56.6	2 0.5
328	14	59.0	61.5	63.9	66.3	68.7	71.2	73.6	76.0	78.4	80.9	3 0.7
329	14	83.3	85.7	88.1	90.5	92.9	95.4	97.8			8.55	4 1.0
329	15	t. I HIS	e flun, si	1	18 9	THE STATE	115	F8.8	00.2	02.6	05.0	5 1.2
330	15	07.4	09.9	12.3	14.7	17.1	19.5	21.9	24.3	26.7	29.1	6 1.5
331	15	31.5	33.9	36.3	38.7	41.2	43.6	46.0	48.4	50.8	53.2	7 1.7
332	15	55.6	58.0	60.4	62.8	65.1	67.5	69.9	72.3	74.7	77.1	8 2.0
333	15	79.5	81.9	84.3	86.7	89.1	91.4	93.8	96.2	98.6	Ba.	9 2.2
333	16	1 516	1,52	2 1 8.0	- 11	19,1.0	9.0	430	The state of	100	01.0	0.03
334	16	03.4	05.8	08.1	10.5	12.9	15.3	17.7	20.0	22.4	24.8	Ladge
335	16	27.2	29.6	31.9	34.3	36.7	39.1	41.4	43.8	46.2	48.8	749
336	16	50.9	53.3	55.7	58.0	60.4	62.8	65.1	67.5	69.9	72.2	1   0.2
337	16	74.6	77.0	79.3	81.7	84.0	86.4	88.8	91.1	93.5	95.8	2 0.4
338	16	98.2	F-dri	17.5	1 23	3 318	- COLAN	227	T LU	LE LOUIS		3 0.7
338	17		00.5	02.9	05.2	07.6	10.0	12.3	14.7	17.0	19.4	4 1.0
339	17	21.7	24.1	26.4	28.8	31.1	33.4	35.8	38.1	40.5	42.8	5 1.2
340	17	45.2	47.5	49.8	52.2	54.5	56.9	59.2	61.5	63.9	66.2	6 1.5
341	17	68.6	70.9	73.2	75.6	77.9	80.2	82.6	84.9	87.2	89.5	7 1.7
342	17	91.9	94.2	96.5	98.9	1.88	1 16 1	100	tion .	1 13		8 1.9
342	18	T. P. F	C LE	1	10.0	01.2	03.5	05.8	08.2	10.5	12.8	9 2.2
343	18	15.1	17.4	19.8	22.1	24.4	26.7	29.0	31.4	33.7	36.0	- 100
344	18	38.3	40.6	42.9	45.2	47.6	49.9	52.2	54.5	56.8	59.1	2000
345	18	61.4	63.7	66.0	68.3	70.6	73.0	75.3	77.6	79.9	82.2	-20 m
346	18	84.5	86.8	89.1	91.4	93.7	96.0	98.3	100	100	100	TRE
346	19	Septime.	1.1:20	9,00	0.00	3.0	子 医虫	0.4.	00.6	02.9	05.2	E-24151
347	19	07.5	09.6	12.0	14.3	16.6	18.9	21.2	23.5	25.8	28.1	
348	19	30.4	32.7	34.9	37.2	39.5	41.8	44.1	46.4	48.6	50.9	
349	19	53.2	55.5	57.8	60.1	62.3	64.6	66.9	69.2	71.5	73.7	610
		Total	Trib.U	E 16 (18	11 (0/5)	1,000	100	1 11.50	TEST	4.5	Op.	
350	19	76.0	78.3	80.6	82.8	85.1	87.4	89.6	91.9	94.2	96.5	1   0.2
351	19	98.7		1 8	1-1-10	1.0	11, 11, 11	1.0	11,5	1.24	d nas	2 0.4
351	20	8.14	01.0	03.3	05.5	07.8	10.1	12.3	14.6	16.8	19.1	3 0.7
352	20	21.4	23.6	25.9	28.2	30.4	32.7	34.9	37.2	39.5	41.7	4 0.9
353	20	44.0	46.2	48.5	50.7	53.0	55.2	57.5	59.7	62.0	64.2	5 1.1
354	20	66.5	68.7	71.0	73.2	75.5	77.7	80.0	82.2	84.5	86.7	6 1.3
355	20	89.0	91.2	93.4	95.7	97.9	E 4.31	100		3 6.0	1 100	7 1.6
355	21	7 7.57	1 15-61	F 1 35	TY-VA	14 12 3	00.2	02.4	04.6	06.9	09.1	8 1.8
356	21	11.4	13.6	15.8	18.1	20.3	22.5	24.8	27.0	29.2	31.5	9 2.1
357	21	33.7	35.9	38.2	40.4	42.6	44.8	47.1	49.3	51.5	53.7	1010
358	21	56.0	58.2	60.4	62.6	64.9	67.1	69.3	71.5	73.7	76.0	TURO
359	21	78.2	80.4	82.6	84.8	87.0	89.3	91.5	93.7	95.9	98.1	
360	22	00.3	02.5	04.8	07.0	09.2	11.4	13.6	15.8	18.0	20.2	
361	22	22.4	24.6	26.8	29.0	31.2	33.4	35.6	37.9	40.1	42.3	
362	22	44.5	46.7	48.9	51.0	53.2	55.4	57.6	59.8	62.0	64.2	
363	22	66.4	68.6	70.8	73.0	75.2	77.4	79.6	81.8	83.9	86.1	
364	22	88.3	90.5	92.7	94.9	97.1	99.3	1 200	1 200	100	e l'age	
364	23	TECH-60	1000	1 5.76	172		A LEE	01.4	03.6	05.8	08.0	
Barom-		2 2 2				O VA						
eter Hor h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm.

365 to 403mm.

Barom-			A S. C.		Hegg	97/61					SA. C	Parts
eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for eac 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Met
365	23	10.2	12.4	14.5	16.7	18.9	21.1	23.2	25.4	27.6	29.8	1 0.
366	23	32.0	34.1	36.3	38.5	40.7	42.8	45.0	47.2	49.3	51.5	2 0.
367	23	53.7	55.9	58.0	60.2	62.4	64.5	66.7	68.9	71.0	73.2	3 0.
368	23	75.4	77.5	79.7	81.8	84.0	86.2	88.3	90.5	92.6	94.8	4 0.
369	23	97.0	99.1	5 14	- 1144.5	The late		A FAIR	1		134	5 1.
369	24			01.3	03.4	05.6	07.7	09.9	12.1	14.2	16.4	6 1.
370	24	18.5	20.6	22.8	24.9	27.1	29.2	31.4	33.5	35.7	37.8	7 1.
371	24	40.0	42.1	44.3	46.4	48.6	50.7	52.9	55.0	57.2	59.3	8 1.
372	24	61.5	63.6	65.8	67.9	70.1	72.2	74.3	76.5	78.6	80.8	9 1.
373	24	82.9	85.0	87.2	89.3	91.4	93.6	95.7	97.8	99.9	100	
373	25	To the	1 200	450	P. T. ASS	E Supe	in her	1 100	100		02.1	7111
374	25	04.2	06.3	08.4	10.6	12.7	14.8	16.9	19.0	21.2	23.3	
	12.1	A REP	100	MILES	to Tyle	tolk field	E V 3/15				3 6 7	1 34
375	25	25.4	27.5	29.6	31.8	33.9	36.0	38.1	40.2	42.4	44.5	
376	25	46.6	48.7	50.8	53.0	55.1	57.2	59.3	61.4	63.6	65.7	13791
377	25	67.8	69.9	72.0	74.1	76.2	78.3	80.5	82.6	84.7	86.8	102
378	25	88.9	91.0	93.1	95.2	97.3	99.4	2.42.4		1-60	E to Take	7 300
378	26	511111111111111111111111111111111111111	4 5 5	St.	Lab	25.5	10.0	01.5	03.6	05.7	07.8	
379	26	09.9	12.0	14.1	16.2	18.3	20.4	22.5	24.6	26.7	28.8	1
380	26	30.9	33.0	35.1	37.2	39.3	41.3	43.4	45.5	47.6	49.7	1
381	26	51.8	53.9	56.0	58.1	60.2	62.2	64.3	66.4	68.5	70.6	
382	26	72.7	74.8	76.9	78.9	81.0	83.1	85.2	87.3	89.3	91.4	
383	26	93.5	95.6	97.7	99.7	1.88	1.5	1.8	0.5	1 20		
383	27	2.8	67	r als	6.39	01.8	03.9	06.0	08.1	10.1	12.2	1   0.
384	27	14.3	16.4	18.4	20.5	22.6	24.6	26.7	28.8	30.9	32.9	2 0.
385	27	35.0	37.1	39.1	41.2	43.2	45.3	47.4	49.4	51.5	53.5	3 0.0
386	27	55.6	57.7	59.7	61.8	63.8	65.9	68.0	70.0	72.1	74.1	4 0.9
387	27	76.2	78.3	80.3	82.4	84.4	86.5	88.6	90.6	92.7	94.7	5 1.
388	27	96.8	98.8	10.5	Lindau	1 Card	1.0	and the		5.0		6 1.
388	28	13	N.E	00.9	02.9	05.0	07.0	09.1	11.1	13.2	15.2	7 1.
389	28	17.3	19.3	21.4	23.4	25.5	27.5	29.6	31.6	33.7	35.7	8 1.
390	28	37.8	39.8	41.9	43.9	46.0	48.0	50.0	52.1	54.1	56.2	9 1.
391	28	58.2	60.2	62.3	64.3	66.3	68.3	70.4	72.4	74.4	76.5	
392	28	78.5	80.5	82.6	84.6	86.6	88.6	90.7	92.7	94.7	96.8	1000
393	28	98.8	5.0	S AN	- 60	9 60	1.00	h-ked	1 1			Property.
393	29	A. A. SH	00.8	02.8	04.9	06.9	08.9	10.9	12.9	15.0	17.0	
394	29	19.0	21.0	23.0	25.1	27.1	29.1	31.1	33.1	35.2	37.2	
395	29	39.2	41.2	43.2	45.2	47.2	49.2	51.3	53.3	55.3	57.3	
396	29	59.3	61.3	63.3	65.3	67.3	69.3	71.4	73.4	75.4	77.4	
397	29	79.4	81.4	83.4	85.4	87.4	89.4	91.5	93.5	95.5	97.5	
398	29	99.5	1.0	nii bo		36.60	D 303	1 . 1. 13				
398	30	JASS A	01.5	03.5	05.5	07.5	09.5	11.5	13.5	15.5	17.5	
399	30	19.5	21.5	23.5	25.5	27.5	29.4	31.4	33.4	35.4	37.4	
HE	SALE	100	E I think	e tal	1 to how	MA BUS	ST GOOD	1000		66.83	100	826
400	30	39.4	41.4	43.4	45.4	47.4	49.4	51.3	53.3	55.3	57.3	I dita
401	30	59.3	61.3	63.3	65.2	67.2	69.2	71.2	73.2	75.1	77.1	
402	30	79.1	81.1	83.1	85.0	87.0	89.0	91.0	93.0	94.9	96.9	
403	30	98.9	190,0	INTER!	1.8,6	14 5.3	1 8.4			14 70 1	1200	1
			1	1		11111		-		391293	7	
Barom-	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac
or h.	1				The same	9.1 3.4		1	-	N CONTRACTOR	1 70	0.01mn

403 to 442mm.

Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Part for ea 0.01m
		-	70	70	Material	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Me
Milli.	Metr.	Metres.	Metres.	Metres. 02.8	Metres.	06.8	08.7	10.7	12.7	14.7	16.6	1   0.
404	31	18.6	20.6	22.5	24.5	26.5	28.4	30.4	32.4	34.4	36.3	2 0.
404	The Control of the Co	38.3	40.3	42.2	44.2	46.1	48.1	50.1	52.0	54.0	55.9	3 0.
	31	1 1 1 1	59.9	61.8	63.8	65.7	67.7	69.7	71.6	73.6	75.5	4 0
406	31	57.9		81.4	83.4	85.3	87.3	89.3	91.2	93.2	95.1	5 1
407	31	77.5	79.5	01.4	00.4	00.0	01.0	09.0	31.2	30.4	33.1	
408	31	97.1	99.0	01.0	02.9	04.9	06.8	08.8	10.7	12.7	14.6	6 1
408	32	100	10 "	01.0		100	26.3	28.2	30.2	32.1	34.1	7 1
409	32	16.6	18.5	20.5	22.4	24.4	The Part of the party	The second				8 1
410	32	36.0	37.9	39.9	41.8	43.8	45.7	47.6	49.6	51.5	53.5	9 1
411	32	55.4	57.3	59.3	61.2	63.2	65.1	67.0	69.0	70.9	72.9	2.0
412	32	74.8	76.7	78.7	80.6	82.5	84.4	86.4	88.3	90.2	92.2	16.6
413	32	94.1	96.0	97.9	99.9	THE STATE OF	0,0	4	10-14-57-0		110	133
413	33			ante de	MAH	01.8	03.7	05.6	07.5	09.5	11.4	
414	33	13.3	15.2	17.1	19.1	21.0	22.9	24.8	26.7	28.7	30.6	1.61
415	33	32.5	34.4	36.3	38.3	40.2	42.1	44.0	45.9	47.9	49.8	100
416	33	51.7	53.6	55.5	57.4	59.3	61.2	63.2	65.1	67.0	68.9	TYX
417	33	70.8	72.7	74.6	76.5	78.4	80.3	82.3	84.2	86.1	88.0	1 20
418	33	89.9	91.8	93.7	95.6	97.5	99.4	30111 30	34		14 100	Salt
418	34			5 L M B	100	1 2 2 6	4.24	01.3	03.2	05.1	07.0	Bay
419	34	08.9	10.8	12.7	14.6	16.5	18.4	20.3	22.2	24.1	26.0	Lane
420	34	27.9	29.8	31.7	33.6	35.5	37.3	39.2	41.1	43.0	44.9	60
421	34	46.8	48.7	50.6	52.5	54.4	56.2	58.1	60.0	61.9	63.8	
422	34	65.7	67.6	69.5	71.4	73.3	75.1	77.0	78.9	80.8	82.7	1 0
423	34	84.6	86.5	88.4	90.2	92.1	94.0	95.9	97.8	99.6	020	2 0
423	35	04.0	00.0	00.4	30.2	32.1	34.0	30.0	31.0	33.0	01.5	100
424	35	03.4	05.3	07.2	09.0	10.9	12.8	14.7	16.6	18.4	20.3	3 0 4 0
*44	99	05.4	03.0	01.2	03.0	10.5	12.0	14.7	10.0	10.4	20.0	
425	94	22.2	24.1	25.9	27.8	29.6	01 5	33.4	95 9	37.1	38.9	
	35		103			200	31.5	- P. 117	35.2			6 1
426	35	40.8	42.7	44.5	46.4	48.3	50.1	52.0	53.9	55.8	57.6	7 1
427	35	59.5	61.4	63.2	65.1	67.0	68.8	70.7	72.6	74.5	76.3	8 1
428	35	78.2	80.1	81.9	83.8	85.6	87.5	89.4	91.2	93.1	94.9	9 1
429	35	96.8	98.6	9.3	9.5	1 9-9	FIG. TO	Thefat	0 1 6-9			100
429	36	By by		00.5	02.3	04.2	06.0	07.9	09.7	11.6	13.4	1
430	36	15.3	17.1	19.0	20.8	22.7	24.6	26.4	28.2	30.1	31.9	1.55
431	36	33.8	35.6	37.5	39.3	41.2	43.0	44.8	46.7	48.5	50.4	100
432	36	52.2	54.0	55.9	57.7	59.6	61.4	63.2	65.1	66.9	68.8	100
433	36	70.6	72.4	74.3	76.1	78.0	79.8	81.6	83.5	85.3	87.2	1.58
434	36	89.0	90.8	92.7	94.5	96.3	98.1	1000	40	F IP FALL	1700	J. gd
434	37	- 1 1	1 18	Fort Ask	C 1 2.8	A. 1840	E Town	00.0	01.8	03.6	05.5	-78
435	37	07.3	09.1	11.0	12.8	14.6	16.4	18.3	20.1	21.9	23.8	20
436	37	25.6	27.4	29.2	31.1	32.9	34.7	36.5	38.3	40.2	42.0	190
437	37	43.8	45.6	47.5	49.3	51.1	52.9	54.8	56.6	58.4	60.3	. 80
438	37	62.1	63.9	65.7	67.6	69.4	71.2	73.0	74.8	76.7	78.5	100
439	37	80.3	82.1	83.9	85.7	87.5	89.3	91.2	93.0	94.8	96.6	
440	37	98.4	1 6 40	S. B. E. C	e l'ain		1000	i defin	1000	C. III II II	6.00	100
440	38	1 1 5	00.2	02.0	03.8	05.6	07.5	09.3	11.1	12.9	14.7	
441	38	16.5	18.3	20.1	21.9	23.7	25.5	27.3	29.1	30.9	32.7	
442	38	34.5	36.3	38.1	39.9	41.7	43.5	45.3	47.1	48.9	50.7	
Barom-	_	CA N					-10.0					
eter I or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Part for ea

443 to 482mm.

Barom-			SISTER	Post 1	Т	enth of	Millimet	re.				Parts
eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for each
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Meta
443	38	52.5	54.3	56.1	57.9	59.7	61.4	63.2	65.0	66.8	68.6	
444	38	70.4	72.2	74.0	75.8	77.6	79,3	81.1	82.9	84.7	86.5	
445	38	88.3	90.1	91.9	93.7	95.5	97.2	99.0		9	415	1
445	39	24 (1)				- V 25	911-90		00.8	02.6	04.4	
446	39	06.2	08.0	09.8	11.5	13.3	15.1	16.9	18.7	20.4	22.2	
447	39	24.0	25.8	27.6	29.3	31.1	32.9	34.7	36.5	38.2	40.0	
448	39	41.8	43.6	45.4	47.1	48.9	50.7	52.5	54.3	56.0	57.8	11-31
449	39	59.6	61.4	63.1	64.9	66.7	68.4	70.2	72.0	73.8	75.5	54.00
JAL .	1 04	W I I	1 1	Winds		93729	2 1 1	n la	8 6	ZII.	E 1 90	
450	39	77.3	79.1	80.8	82.6	84.3	86.1	87.9	89.6	91.4	93.1	1
451	39	94.9	96.7	98.4	95000	1 100	0 1	100		20 10	A. I	A M
451	40		A LEW		00.2	02.0	03.7	05.5	07.3	09.1	10.8	E M
452	40	12.6	14.4	16.1	17.9	19.6	21.4	23.2	24.9	26.7	28.4	· Plan
453	40	30.2	32.0	33.7	35.5	37.2	39.0	40.8	42.5	44.3	46.0	100
454	40	47.8	49.5	51.3	53.0	54.8	56.5	58.3	60.0	61.8	63.5	
455	40	65.3	67.0	68.8	70.5	72.3	74.0	75.8	77.5	79.3	81.0	1   0.2
456	40	82.8	84.5	86.3	88.0	89.8	91.5	93.2	95.0	96.7	98.5	2 0.3
457	41	00.2	01.9	03.7	05.4	07.2	08.9	10.6	12.4	14.1	15.9	3 0.5
458	41	17.6	19.3	21.1	22.8	24.6	26.3	28.0	29.8	31.5	33.3	4 0.7
459	41	35.0	36.7	38.5	40.2	41.9	43.6	45.4	47.1	48.8	50.6	5 0.9
460	41	52.3	54.0	55.8	57.5	59.2	60.9	62.7	64.4	66.1	67.9	6 1.0
461	41	69.6	71.3	73.1	74.8	76.5	78.2	80.0	81.7	83.4	85.2	7 1.2
462	41	86.9	88.6	90.3	92.1	93.8	95.5	97.2	98.9			8 1.4
462	42	7 60	19 60	41 B	0		1011 279			00.7	02.3	9 1.6
463	42	04.1	05.8	07.5	09.3	11.0	12.7	14.4	16.1	17.9	19.6	
464	42	21.3	23.0	24.7	26.4	28.1	29.8	31.6	33.3	35.0	36.7	
465	42	38.4	40.1	41.8	43.5	45.2	46.9	48.7	50.4	52.1	53.8	
466	42	55.5	57.2	58.9	60.6	62.3	64.0	65.8	67.5	69.2	70.9	
467	42	72.6	74.3	76.0	77.7	79.4	81.1	82.8	84.5	86.2	87.9	
468	42	89.6	91.3	93.0	94.7	96.4	98.1	99.8	4.1			
468	43		arit and	29	24.87	8 T- 100	11 33		01.5	03.2	04.9	
469	43	06.6	08.3	10.0	11.7	13.4	15.1	16.8	18.5	20.2	21.9	
470	43	23.6	25.3	27.0	28.7	30.4	32.0	33.7	35.4	37.1	38.8	
471	43	40.5	42.2	43.9	45.6	47.3	48.9	50.6	52.3	54.0	55.7	
472	43	57.4	59.1	60.8	62.5	64.2	65.8	67.5	69.2	70.9	72.6	
473	43	74.3	76.0	77.7	79.3	81.0	82.7	84.4	86-1	87.7	89.4	
474	43	91.1	92.8	94.5	96.1	97.8	99.5					
474	44		0 = 80		1 60	6.1 9.3	1-1-1	01.2	02.9	04.5	06.2	
475	44	07.9	09.6	11.2	12.9	14.6	16.2	17.9	19.6	21.3	22.9	
476	44	24.6	26.3	27.9	29.6	31.3	33.9	35.6	37.3	39.0	40.6	
477	44	41.3	43.0	44.6	46.3	48.0	49.6	51.3	53.0	54.7	56.3	
478	44	58.0	59.7	61.3	63.0	64.7	66.3	68.0	69.7	71.4	73.0	Na P
479	44	74.7	76.4	78.0	79.7	81.3	83.0	84.7	86.3	88.0	89.6	
480	44	91.3	93.0	94.6	96.3	97.9	99.6	0.2.4	00.0	00.0	03.0	
480	45	01.0	00.0	0 1.0	00.0	0	00.0	01.3	02.9	04.6	06.2	
481	45	07.9	09.5	11.2	12.8	14.5	16.1	17.7	19.4	21.0	22.7	1 Phone 1
482	45	24.3	25.9	27.6	29.2	30.9	32.5	34.2	35.8	37.5	39.1	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each

483 to 524mm.

							100			,			
Baro			0.0	0.1	0.2	0.0	0.4	0 -	0.0	0 =	0.0	0.0	Parts for each
H or	h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for each 0.01mm.
Mi		Metr.	Metres.	Metres,	Metres.	Metres,	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
48	3.5	Metr. 45	40.8	42.4	44.1	45.7	47.4	49.0	50.7	52.3	54.0	55.6	1   0.2
48	- 1	45	57.3	58.9	60.6	62.2	63.9	65 5	67.1	68.8	70.4	72.1	2 0.3
48	11	45	73.7	75.3	77.0	78.6	80.3	81.9	83.6	85.2	86.9	88.5	3 0.5
48	6	45	90.2	91.8	93.5	95.1	96.8	98.4			2 4 0		4 0.6
48	6	46	Mary Mil	1 60	E 7 560		Ag Ro	6 T 104	00.0	01.7	03.3	05.0	5 0.8
48	- 11	46	06.6	08.2	09.9	11.5	13.1	14.7	16.4	18.0	19.6	21.3	6 1.0
48	- 11	46	22.9	24.5	26.2	27.8	29.4	31.0	32.7	34.3	35.9	37.6	7 1.1
48		46	39.2	40.8	42.4	44.1	45.7	47.3	48.9	50.5	52.2	53.8	8 1.3
49	- 11	46	55.4	57.0	58.6	60.3	61.9	63.5	65.1	66.7	68.4	70.0	9 1.4
49		46	71.6	73.2	74.9	76.5	78.1	79.7	81.4	83.0	84.6	86.3	A SER
49	- 11	46	87.9	89.5	91.1	92.8	94.4	96.0	97.6	99.2	00.9	02.5	
49	- 11	47	04.1	05.7	07.3	08.9	10.5	12.1	13.8	15.4	17.0	18.6	1 196
49	- 31	47	20.2	21.8	23.4	25.0	26.6	28.2	29.9	31.5	33.1	34.7	1 1
49		47	36.3	37.9	39.5	41.1	42.7	44.3	45.9	47.5	49.1	50.7	REAL PROPERTY.
49	- 11	47	52.3	53.9	55.5	57.1	58.7	60.3	61.9	63.5	65.1	66.7	
49	- 11	47	68.3	69.9	71.5	73.1	74.7	76.3	78.0	79.6	81.2	82.8	DES.
49	- 1	47	84.4	86.0	87.6	89.2	90.8	92.4	94.0	95.6	97.2	98.8	132
49	- 11	48	00.4	02.0	03.6	05.2	06.8	08.3	09.9	11.5	13.1	14.7	Ladi-
		140	March	th of 15a	W. Whi	100		Directly)	01	1	4 3	Halland.	1
50	0	48	16.3	17.9	19.5	21.1	22.7	24.2	25.8	27.4	89.0	30.6	(B)
50	- 11	48	32.2	33.8	35.4	37.0	38.6	40.1	41.7	43.3	44.9	46.5	WES-
50	- 11	48	48.1	49.7	51.3	52.9	54.5	56.0	57.6	59.2	60.8	62.4	La H
50	- 11	48	64.0	65.6	67.2	68.7	70.3	71.9	73.5	75.1	76.6	78.2	1130
50	- 11	48	79.8	81.4	83.0	84.5	86.1	87.7	89.3	90.9	92.4	94.0	V.307
50	- 11	48	95.6	97.2	98.7	00.0	0.0	00	0.50	00.0	00.0	00 =	N. A. P.
50	- 11	49	11.0	10.0	14.	00.3	01.9	03.4	05.0	06.6	08.2	09.7	
50	- 11	49	11.3	12.9	14.4	16.0	17.6	19.1	20.7	22.3	23.9	25.4	
50	- 11	49	27.0 42.7	28.6 44.3	30.1 45.8	31.7 47.4	33.3	34.8	36.4	38.0	39.6 55.3	41.1 56.8	1 4 12
50	- 11	49	58.4	60.0	61.5	63.1	49.0 64.6	50.5 66.2	52.1 67.8	53.7 69.3	70.9	72.4	TO THE
51		49	74.0	75.6	77.1	78.7	80.2	81.8	83.4	84.9	86.5	88.0	
51	- 11	49	89.6	91.2	92.7	94.3	95.8	97.4	99.0		30.0	00.0	124
51	1	50	a Hal		a Pito					00.5	02.1	03.6	
51		50	05.2	06.7	08.3	09.8	11.4	12.9	14.5	16.0	17.6	19.1	
51	3	50	20.7	22.2	23.8	25.3	26.9	28.4	30.0	31.5	33.1	34.6	144
51	4	50	36.2	37.7	39.3	40.8	42.4	43.9	45.5	46.0	48.6	50.1	A SAFE
51	- 11	50	51.7	53.2	54.8	56.3	57.9	59.4	61.0	62.5	64.1	65.6	STATE OF
51	H	50	67.2	68.7	70.3	71.8	73.4	74.9	76.4	78.0	79.5	81.1	
51	- 11	50	82.6	84.1	85.7	87.2	88.7	90.2	91.8	93.3	94.8	96.4	FIET F
51	- 11	50	97.9	99.4	0	00.7	1			00 =	-0.	1.48	PRI EVE
51	- 11	51	10.0	740	01.0	02.5	04.1	05.6	07.1	08.7	10.2	11.8	HART .
51 52	11	51	13.3	14.8	16.4	17.9	19.4	20.9	22.5	24.0	25.5	27.1	The Mark
52	- 11	51 51	28.6	30.1	31.7	33.2	34.7	36.2	37.8	39.3	40.8	42.4	1 4074
52	11	51	43.9 59.2	45.4 60.7	47.0 62.2	48.5 63.8	50.0	51.5	53.1	54.6 69.8	56.1 71.4	57.7 72.9	
52	- 11	51	74.4	75.9	77.5	79.0	65.3 80.5	66.8 82.0	68.3 83.6	85.1	86.6	88.2	1 100
52	- 11	51	89.7	91.2	92.7	94.3	95.8	97.3	98.8	00.1	00.0	00.2	4
1													
Bar		N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac
Ho				7.1	0.20	0.0	0.4	0.0	0.0	0.7	0.0	0.0	0.01mm
						1			ī		and the second		

524 to 565mm.

Barom- eter	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac
H or h.					*			24.5		110	17.7	0.01 mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres	Metres.	Metres.	Metres.	Metres, 01.9	Metres.	Met
524	52	0.0	00.4	000	00.4	700	10.4	140	15.5	17.0	18.5	The state of
526	52	04.9	06.4	07.9	09.4	10.9	12.4	14.0	30.6	32.1	33.6	
STATE OF THE PARTY	52	20.0	21.5	23.0	24.5	26.0	27.5	29.1		47.2	48.7	No.
527	52	35.1	36.6	38.1	39.6	41.1	42.6	44.2	45.7		63.8	
528	52	50.2	51.7	53.2	54.7	56.2	57.7	59.3	60.8	62.3	7.50	1   0.1
529	52	65.3	66.8	68.3	69.8	71.3	72.8	74.3	75.8	77.3	78.8	2 0.3
530	52	80.3	81.8	83.3	84.8	86.3	87.8	89.3	90.8	92.3	93.8	3 0.4
531	52	95.3	96.8	98.3	99.8	07.0	00.0	04.0	0-0	000	000	4 0.6
531	53	700	110	10.0		01.3	02.8	04.3	05.8	07.3	08.8	5 0.7
532	53	10.3	11.8	13.3	14.8	16.3	17.8	19.3	20.8	22.3	23.8	6 0.9
533	53	25.3	26.8	28.3	29.8	31.3	32.7	34.2	35.7	37.2	38.7	7 1.0
534	53	40.2	41.7	43.2	44.7	46.2	47.6	49.1	50.6	52.1	53.6	21
535	53	55.1	56.5	58.1	59.6	61.1	62.5	64.0	65.5	67.0	68.5	8 1.2
536	53	70.0	71.5	73.0	74.4	75.9	77.4	78.9	80.4	81.8	83.3	9 1.3
537	53	84.8	86.3	87.8	89.2	90.7	92.2	93.7	95.2	96.6	98.1	
538	53	99.6					S N MA					
538	54	6	01.1	02.6	04.0	05.5	07.0	08.5	10.0	11.4	12.9	
539	54	14.4	15.9	17.4	18.8	20.3	21.8	23.3	24.8	26.2	27.7	1100
540	54	29.2	30.7	32.1	33.6	35.1	36.5	38.0	39.5	41.0	42.4	
541	54	43.9	45.4	46.8	48.3	49.8	51.2	52.7	54.2	55.7	57.1	E PH
542	54	58.6	60.1	61.5	63.0	64.5	66.0	67.4	68.9	70.4	71.8	1274
543	54	73.3	74.8	76.2	77.7	79.1	80.6	82.1	83.5	85.0	86.4	
544	54	87.9	89.4	90.8	92.3	93.7	95.2	96.7	98.1	99.6	E 11.348	
544	55	2-11-50		P. C. C.				E TO		and the same	01.0	CLEME
545	55	02.5	04.0	05.4	06.9	08.4	09.8	11.3	12.8	14.3	15.7	
546	55	17.2	18.7	20.1	21.6	23.0	24.5	26.0	27.4	28.9	30.3	
547	55	31.8	33.3	34.7	36.1	37.6	39.0	40.5	41.9	43.4	44.8	
548	55	46.3	47.7	49.2	50.6	52.1	53.5	55.0	56.4	57.9	59.3	1
549	55	60.8	62.2	63.7	65.1	66.6	68.0	69.5	70.9	72.4	73.8	S. 45
. 3		The Street	1	1		1						The second
550	55	75.3	76.7	78.2	79.6	81.1	82.5	84.0	85.4	86.9	88.3	Satisfaction of the same
551	55	89.8	91.2	92.7	94.1	95.6	97.0	98.4	99.9			
551	56									01.3	02.8	1 0.1
552	56	04.2	05.6	07.1	08.5	10.0	11.4	12.8	14.3	15.7	17.2	2 0.3
553	56	18.6	20.0	21.5	22.9	24.4	25.8	27.2	28.7	30.1	31.6	3 0.4
554	56	33.0	34.4	35.9	37.3	38.8	40.2	41.6	43.1	44.5	46.0	4 0.6
555	56	47.4	48.8	50.3	51.7	53.1	54.5	56.0	57.4	58.8	60.3	5 0.7
556	56	61.7	63.1	64.6	66.0	67.4	68.8	70.3	71.7	73.1	74.6	6 0.9
557	56	76.0	77.4	78.9	80.3	81.7	83.1	84.6	86.0	87.4	88.9	7 1.0
558	57	90.3	91.7	93.2	94.6	96.0	97.4	98.9		S. S. Land	100	8 1.2
558	57	The same	1	E E					00.3	01.7	03.2	9 1.3
559	57	04.6	06.0	07.4	08.9	10.3	11.7	13.1	14.5	16.0	17.4	TO COL
560	57	18.8	20.2	21.6	23.1	24.5	25.9	27.3	28.7	30.2	31.6	1.05
561	57	33.0	34.4	35.8	37.3	38.7	40.1	41.5	42.9	44.4	45.8	11-1250
562	57	47.2	48.6	50.0	51.4	52.8	54.2	55.7	57.1	58.5	59.9	N. MON
563	57	61.3	62.7	64.1	65.5	66.9	68.3	69.8	71.2	72.6	74.0	33th
564	57	75.4	76.8	78.2	79.6	81.0	82.4	83.9	85.3	86.7	88.1	1970
565	57	89.5	90.9	92.4	93.8	95.2	96.6	98.0	99.4	The Table	Sell Es	100
Barom- eter H or h	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each

565 to 605mm.

				N. Carlo	900	to 6	05 <sup>mm</sup> .					
Birom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr
565	58									00.8	02.2	11.1100
566	58	03.6	05.0	06.4	07.8	09.2	10.6	12.1	13.5	14.9	16.3	500
567	58	17.7	19.1	20.5	21.9	23.3	24.7	26.1	27.5	28.9	30.3	17 990
568	58	31.7	33.1	34.5	35.9	37.3	38.7	40.1	41.5	42.9	44.3	1 320
569	58	45.7	47.1	48.5	49.9	51.3	52.7	54.1	55.5	56.9	58.3	
570	58	59.7	61.1 75.1	62.5 76.5	63.9	65.3 79.3	80.6	68.1 82.0	69.5	70.9	72.3	
571	58 58	73.7 87.6	89.0	90.4	91.8	93.2	94.5	95.9	83.4	84.8 98.7	86.2	
572 572	59	07.0	03.0	30.4	91.0	33.2	94.0	30.3	97.3	90.1	00.1	
573	59	01.5	02.9	04.3	05.7	07.1	08.4	09.8	11.2	12.6	14.0	
574	59	15.4	16.8	18.2	19.6	21.0	22.3	23.7	25.1	26.5	1000	
574	99	19.4	10.0	10.2	13.0	21.0	22.0	20.1	25.1	20.5	27.9	
575	59	29.3	30.7	32.1	33.4	34.8	36.2	37.6	39.0	40.3	41 7	1 1 20
576	59	43.1	44.5	45.9	47.2	48.6	50.2	51.4	52.8	54.1	41.7 55.5	1   0.1
577	59	56.9	58.3	59.7	61.0	62.4	63.8	65.2	66.6	67.9	69.3	2 0.3
578	59	70.7	72.1	73.5	74.8	76.2	77.6	79.0	80.4	81.7	83.1	3 0.4
579	59	84.5	85.9	87.2	88.6	90.0	91.3	92.7	94.1	95.5	96.8	4 0.5
580	59	98.2	99.6	01.2	00.0	50.0	01.0	52.1	34.1	35.5	30.0	5 0.7
580	60	00.2	00.0	00.9	02.3	03.7	05.0	06.4	07.8	09.2	10.5	6 0.8
581	60	11.9	13.3	14.6	16.0	17.4	18.7	20.1	21.5	22.9	24.2	7 1.0
582	60	25.6	27.0	28.3	29.7	31.1	32.4	33.8	35.2	36.6	37.9	8 1.1
583	60	39.3	40.7	42.0	43.4	44.7	46.1	47.5	48.8	50.2	51.5	9 1.2
584	60	52.9	54.3	55.6	57.0	58.4	59.7	61.1	62.5	63.9	65.2	3   1.2
585	60	66.6	68.0	69.3	70.7	72.0	73.4	74.8	76.1	77.5	78.8	
596	60	80.2	81.6	82.9	84.3	85.6	87.0	88.4	89.7	91.1	92.4	
587	60	93.8	95.1	96.5	97.8	99.2	0	00.4	03.1	31.1	34.4	
587	61		0011	00.0	31.0	33.2	00.5	01.9	03.2	04.6	05.9	
588	61	07.3	08.6	10.0	11.3	12.7	14.0	15.4	16.7	18.1	19.4	
589	61	20.8	22.1	23.5	24.8	26.2	27.5	28.9	30.2	31.6	32.9	
590	61	34.3	35.6	37.0	38.3	39.7	41.0	42.4	43.7	45.1	46.4	
591	61	47.8	49.1	50.5	51.8	53.2	54.5	55.9	57.2	58.6	59.9	
592	61	61.3	62.6	64.0	65.3	66.7	68.0	69.3	70.7	72.0	73.4	
593	61	74.7	76.0	77.4	78.7	80.1	81.4	82.7	84.1	85.4	86.8	
594	61	88.1	89.4	90.8	92.1	93.5	94.8	96.1	97.5	98.8	00.0	
594	62	10	0.0	200	t Home		16				00.2	
595	62	01.5	02.8	04.2	05.5	06.9	08.2	09.5	10.9	12.2	13.6	
596	62	14.9	16.2	17.6	18.9	20.2	21.5	22.9	24.2	25.5	26.9	
597	62	28.2	29.5	30.9	32.2	33.6	34.9	36.2	37.6	38.9	40.3	
598	62	41.6	42.9	44.3	45.6	46.9	48.2	49.6	50.9	52.2	53.6	
599	62	54.9	56.2	57.6	58.9	60.2	61.5	62.9	64.2	65.5	66.9	
600	62	68.2	69.5	70.8	72.2	73.5	74.8	76.1	77.4	78.8	80.1	
601	62	81.4	82.7	84.1	85.4	86.7	88.0	89.4	90.7	92.0	93.4	B Alka
602	62	94.7	96.0	97.3	98.7	R Pros	7083	No.	t Pres	200		FIRE.
602	63		1.0	1 7 7 4	1.1	00.0	01.3	02.6	03.9	05.3	06.6	2 280
C)3	63	07.9	09.2	10.5	11.9	13.2	14.5	15.8	17.1	18.5	19.8	
604	63	21.1	22.4	23.7	25.1	26.4	27.7	29.0	30.3	31.7	33.0	
605	63	34.3	35.6	36.9	38.2	39.5	40.8	42.2	43.5	44.8	46.1	523
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.

606 to 647mm.

										613	-	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres,	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Met
606	63	47.4	48.7	50.0	51.3	52.6	53.9	55.3	56.6	57.9	59.2	TO DISTO
607	63	60.5	61.8	63.1	64.5	65.8	67.1	68.4	69.7	71.1	72.1	0.80
608	63	73.7	75.0	76.3	77.6	78.9	80.2	81.5	82.8	84.1	85.4	1, 190
609	63	86.7	88.0	89.3	90.6	91.9	93.2	94.6	95.9	97.2	98.5	1000
610	63	99.8						1	33-70	1 495		406
610	64		01.1	02.4	03.7	05.0	06 3	07.6	08.9	10.2	11.5	E Au
611	64	12.8	14.1	15.4	16.7	18.0	19.3	20.7	22.0	23.3	24.6	1
612	64	25.9	27.2	28.5	29.8	31.1	32.4	33.7	35.0	36.3	37.6	1
613	64	38.9	40.2	41.5	42.8	44.1	45.4	46.7	48.0	49.3	50.6	1 0000
614	64	51.9	53.2	54.5	55.8	57.1	58.3	59.6	60.9	62.2	63.5	1
615	64	64.8	66.1	67.4	68.7	70.0	71.2	72.5	73.8	75.1	76.4	100
616	64	77.7	79.0	80.3	81.6	82.9	84.2	85.5	86.8	88.1	89.4	1-16
-617	64	90.7	92.0	93.3	94.6	95.9	97.1	98.4	99.7		TVE'S	200
617	65		417份与			2 205		al shad		01.0	02.3	1000
618	65	03.6	04.9	06.2	07.4	08.7	10.0	11.3	12.6	13.8	15.1	6.6
619	65	16.4	17.7	19.0	20.3	21.6	22.8	24.1	25.4	26.7	28.0	7.8564
620	65	29.3	30.6	31.9	33.1	34.4	35.7	37.0	38.3	39.5	40.8	TA THE
621	65	42.1	43.4	44.7	45.9	47.2	48.5	49.8	51.1	52.3	53.6	1   0.1
622	65	54.9	56.2	57.5	58.7	60.0	61.3	62.6	63.9	65.1	66.4	2 0.2
623	65	67.7	69.0	70.3	71.5	72.8	74.1	75.4	76.7	77.9	79.2	3 0.4
624	65	80.5	81.8	83.0	84.3	85.6	86.8	88.1	89.4	90.7	91.9	4 0.5
	* 11		15 m				00.0	00.1			3 100	5 0.6
625	65	93.2	94.5	95.8	97.0	98.3	99.6		1			6 0.8
625	66			1.0	Lili	00.0	00.0	00.9	02.2	03.4	04.7	7 0.9
626	66	06.0	07.3	08.5	09.8	11.1	12.3	13.6	14.9	16.2	17.4	8 1.0
627	66	18.7	20.0	21.2	22.5	23.8	25.0	26.3	27.6	28.9	30.1	9 1.1
628	66	31.4	32.7	33.9	36.2	56.4	37.7	39.0	40.2	41.5	42.7	
629	66	44.0	45.3	46.5	47.8	49.1	50.3	51.6	52.9	54.2	55.4	
630	66	56.7	58.0	59.2	60.5	61.7	63.0	64.3	65.5	66.8	68.0	
631	66	69.3	70.6	71.8	73.1	74.4	75.6	76.9	78.2	79.5	80.7	
632	66	82.0	83.2	84.5	85.7	87.0	88.2	89.5	90.7	92.0	93.2	476
633	66	94.5	95.8	97.0	98.3	99.5	00.2	00.0				
- 633	67				Was a second	00.0	00.8	02.1	03.3	04.6	05.8	K III
634	67	07.1	08.4	09.6	10.9	12.1	13.4	14.7	15.9	17.2	18.4	
635	67	19.7	20.9	22.2	23.4	24.7	25.9	27.2	28.4	29.7	30.9	A STATE OF
636	67	32.2	33.4	34.7	35.9	37.2	38.4	39.7	40.9	42.2	43.4	
637	67	44.7	45.9	47.2	48.4	49.7	50.9	52.2	53.4	54.7	55.9	
638	67	57.2	58.4	59.7	60.9	62.2	63.4	64.7	65.9	67.2	68.4	
639	67	69.7	70.9	72.2	73.4	74.7	75.9	77.1	78.4	79.6	80.9	
640	67	82.1	83.3	84.6	85.8	87.1	88.3	89.6	90.8	92.1	93.3	
641	67	94.6	95.8	97.1	98.3	99.6	00.0	50.0			00.0	
641	68	7-8	EUT BE	1116	TOTAL SERVICE		.00.8	02.0	03.3	04.5	05.8	
642	68	07.0	08.2	09.5	10.7	12.0	13.2	14.4	15.7	16.9	18.2	
643	68	19.4	20.6	21.9	23.1	24.3	25.5	26.8	28.0	29.2	30.5	
644	68	31.7	32.9	34.2	35.4	36.7	37.9	39.1	40.4	41.6	42.9	
645	68	44.1	45.3	46.6	47.8	49.0	50.2	51.5	52.7	53.9	55.2	
646	68	56.4	57.6	58.9	60.1	61.3	62.5	63.8	65.0	66.2	67.5	
647	68	68.7	69.9	71.2	72.4	73.6	74.8	76.1	77.3	78.5	79.8	N. N. A.
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm

648 to 689mm.

	1154				040	10 0	89"	A. A.				4161
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Met
648	68	81.0	82.2	83.5	84.7	85.9	87.1	88.4	89.6	90.8	92.1	
649	68	93.3	94.5	95.8	97.0	98.2	99.4	or Line	180	100	1,1286	1
649	69	11.34		1			1	00.7	01.9	03.1	04.4	199
	100	1 2 2 2	1490	1999		141	91374		11 3.8	E FR		119
650	69	05.6	06.8	08.0	09.3	10.5	11.7	12.9	14.1	15.4	16.6	1970
651	69	17.8	19.0	20.2	21.5	22.7	23.9	25.1	26.3	27.6	28.8	- Niga
652	69	30.0	31.2	32.4	33.7	34.9	36.1	37.3	38.5	39.8	41.0	1.116
653	69	42.2	43.4	44.6	45.9	47.1	48.3	49.5	50.7	52.0	53.2	179
654	69	54.4	55.6	56.8	58.1	59.3	60.5	61.7	62.9	64.2	65.4	100
655	69	66.6	67.8	69.0	70.2	71.4	72.6	73.9	75.1	76.3	77.5	
656	69	78.7	79.9	81.1	82.4	83.6	84.8	86.0	87.2	88.5	89.7	THE
657	69	90.9	92.1	93.3	94.5	95.7	96.9	98.2	99.4	111	- H	100
657	70		1 3 3	10.4		1 54	11.518		5 1 0 0	00.6	01.8	THE
658	70	03.0	04.2	05.4	06.6	07.8	09.0	10.3	11.5	12.7	13.9	710
659	70	15.1	16.3	17.5	18.7	19.9	21.1	22.4	23.6	24.8	26.0	F-16.
660	70	27.2	28.4	29.6	30.8	32.0	33.2	34.4	35.6	36.8	38.0	1   0.1
661	70	39.2	40.4	41.6	42.8	44.0	45.2	46.4	47.6	48.8	50.0	2 0.5
662	70	51.2	52.4	53.6	54.8	56.0	57.2	58.5	59.7	60.9	62.1	3 0.
663	70	63.3	64.5	65.7	66.9	68.1	69.3	70.5	71.7	72.9	74.1	4 0.3
664	70	75.3	76.5	77.7	78.9	80.1	81.2	82.4	83.6	84.8	86.0	5 0.6
665	70	87.2	88.4	89.6	90.8	92.0	93.2	94.4	95.6	96.8	98.0	6 0.
666	70	99.2	417	uPich		111					9 43 11	7 0.8
666	71		00.4	01.6	02.8	04.0	05.2	06.4	07.6	08.8	10.0	8 1.0
667	71	11.2	12.4	13.6	14.8	16.0	17.1	18.3	19.5	20.7	21.9	9 1.1
668	71	23.1	24.3	25.5	26.7	27.9	29.0	30.2	31.4	32.6	33.8	SALS
669	71	35.0	36.2	37.4	38.6	39.8	40.9	42.1	43.3	44.5	45.7	145
670	71	46.9	48.1	49.3	50.5	51.7	52.8	54.0	55.2	56.4	57.6	1950
671	71	58.8	60.0	61.2	62.3	63.5	64.7	65.9	67.1	68.2	69.4	60.0
672	71	70.6	71.8	73.0	74.2	75.4	76.5	77.7	78.9	80.1	81.3	PARK
673	71	82.5	83.7	84.9	86.0	87.2	88.4	89.6	90.8	91.9	93.1	1110
674	71	94.3	95.5	96.7	97.8	99.0	207.8	100	K 8 5 5	0.6		1 29.9
674	72				The state of		00.2	01.4	02.6	03.7	04.9	7/01
675	72	06.1	07.3	08.5	09.6	10.8	12.0	13.2	14.4	15.5	16.7	
676	72	17.9	19.1	20.3	21.4	22.6	23.8	25.0	26.2	27.3	28.5	BALL
677	72	29.7	30.9	32.0	33.2	34.4	35.5	36.7	37.9	39.1	40.2	
678	72	41.4	42.6	43.8	44.9	46.1	47.3	48.5	49.7	50.8	52.0	
679	72	53.2	54.4	55.5	56.7	57.9	59.0	60.2	61.4	62.6	63.7	
680	72	64.9	66.1	67.2	68.4	69.6	70.7	71.9	73.1	74.3	75.4	
681	72	76.6	77.8	78.9	80.1	81.3	82.4	83.6	84.8	86.0	87.1	1   0.1
682	72	88.3	89.5	90.6	91.8	93.0	94.1	95.3	96.5	97.7	98.8	2 0.2
683	73	00.0	01.2	02.3	03.5	04.6	05.8	07.0	08.1	09.3	10.4	3 0.3
684	73	11.6	12.8	13.9	15.1	16.2	17.4	18.6	19.7	20.9	22.0	4 0.5
685	73	23.2	24.4	25.5	26.7	27.8	29.0	30.2	31.3	32.5	33.6	5 0.6
636	73	34.8	36.0	37.1	38.3	39.4	40.6	41.8	42.9	44.1	45.2	6 0.7
687	73	46.4	47.6	48.7	49.9	51.0	52.2	53.4	54.5	55.7	56.8	7 0.8
688	73	58.0	59.2	60.3	61.5	62.6	63.8	65.0	66.1	67.3	68.4	8 0.9
689	73	69.6	70.7	71.9	73.0	74.2	75.3	76.5	77.6	78.8	79.9	9 1.1
Barom- eter	N.	0.0	0.1	0.2	0.3							Parts
f or h.		0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for eac 0.01mm

690 to 730mm.

					690	10	30"	(ATE 3 (I)				
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres,	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
690	73	81.1	82.3	83.4	84.6	85.7	86.9	88.1	89.2	90.4	91.5	
691	73	92.7	93.8	95.0	96.1	97.3	98.4	99.6		- 500	10000	E MALEN
691	74	1000	1 8 20	E/G	1 641	The said		1 3 4	00.7	01.9	03.0	
692	74	04.2	05.3	06.5	07.6	08.8	09.9	11.1	12.2	13.4	14.5	
693	74	15.7	16.8	18.0	19.1	20.3	21.4	22.6	23.7	24.9	26.0	The state of
694	74	27.2	28.3	29.5	30.6	31.8	32.9	34.1	35.2	36.4	37.5	
695	74	38.7	39.8	41.0	42.1	43.3	44.4	45.5	46.7	47.8	49.0	
696	74	50.1	51.2	52.4	53.5	54.7	55.8	56.9	58.1	59.2	60.4	
697	74	61.5	62.6	63.8	64.9	66.1	67.2	68.3	69.5	70.6	71.8	-
698	74	72.9	74.0	75.2	76.3	77.5	78.6	79.7	80.9	82.0	83.2	
699	74	84.3	85.4	86.6	87.7	88.9	90.0	91.1	92.3	93.4	94.6	1
		8.40	6.13	1 232	44	1000	112411		100		10000	
700	74	95.7	96.8	98.0	99.1	THE RE	10.50			LUNA	Train !	
700	75	1.16.48	100	1.00	2.30	00.3	01.4	02.5	03.7	04.8	06.0	
701	75	07.1	08.2	09.4	10.5	11.6	12.7	13.9	15.0	16.1	17.3	
702	75	18.4	19.5	20.7	21.8	23.0	24.1	25.2	26.4	27.5	28.7	
703	75	29.8	30.9	32.1	33.2	34.3	35.4	36.6	37.7	38.8	40.0	The state of
704	75	41.1	42.2	43.4	44.5	45.6	46.7	47.9	49.0	50.1	51.3	2270
705	75	52.4	53.5	54.7	55.8	56.9	58.0	59.2	60.3	61.4	62.6	1850
706	75	63.7	64.8	66.0	67.1	68.2	69.3	70.5	71.6	72.7	73.9	200
707	75	75.0	76.1	77.2	78.4	79.5	80.6	81.7	82.8	84.0	85.1	
708	75	86.2	87.3	88.5	89.6	90.7	91.8	93.0	94.1	95.2	96.4	1
709	75	97.5	98.6	99.7	00.0	00	0110	00.0	0 1.1	00.2	00.1	
709	76	4	0010		00.9	02.0	03.1	04.2	05.3	06.5	07.6	100
710	76	08.7	09.8	10.9	12.1	13.2	14.3	15.4	16.5	17.7	18.8	100
711	76	19.9	21.0	22.1	23.3	24.4	25.5	26.6	27.7	28.9	30.0	
712	76	31.1	32.2	33.3	34.4	35.5	36.6	37.8	38.9	40.0	41.1	1:0.1
713	76	42.2	43.3	44.4	45.6	46.7	47.8	48.9	50.0	51.2	52.3	2 0.2
714	76	53.4	54.5	55.6	56.8	57.9	59.0	60.1	61.2	62.4	63.5	3 0.3
715	76	64.6	65.7	66.8	67.9	69.0	70.1	71.3	72.4	73.5	74.6	4 0.4
716	76	75.7	76.8	77.9	79.0	80.1	81.2	82.4	83.5	84.6	85.7	5 0.5
717	76	86.8	87.9	89.0	90.1	91.2	92.3	93.5	94.6	95.7	96.8	6 0.7
718	76	97.9	99.0	00.0	0012	02.2	52.0	03.0	0 1.0		00.0	7 0.8
718	77		Margaria.	00.1	01.2	02.3	03.4	04.6	05.7	06.8	07.9	8 0.9
719	77	09.0	10.1	11.2	12.3	13.4	14.5	15.7	16.8	17.9	19.0	9 1.0
720	77	20.1	21.2	22.3	23.4	24.5	25.6	26.7	27.8	28.9	30.0	3   1.0
721	77	31.1	32.2	33.3	34.4	35.5	36.6	37.7	38.8	39.9	41.0	
722	77	42.1	43.2	44.3	45.4	46.5	47.6	48.7	49.8	50.9	52.0	0/5/8
723	77	53.1	54.2	55.3	56.4	57.5	58.6	59.8	60.9	62.0	63.1	
724	77	64.2	65.3	66.4	67.5	68.6	69.6	70.7	71.8	72.9	74.0	Joseph 1
725	77	75.1	76.2	77.3	78.4	79.5	80.6	81.7	82.8	83.9	85.0	A MATE OF
726	77	86.1	87.2	88.3	89.4	90.5	91.6	92.7	93.8	94.9	96.0	
727	77	97.1	98.2	99.3	1 50.00	I JE AU	Po die		000	No. of Street		
727	78	Date	1 2 11	2.01	00.4	01.5	02.5	03.6	04.7	05.8	06.9	STATE OF
728	78	08.0	09.1	10.2	11.3	12.4	13.5	14.6	15.7	16.8	17.9	-
729	78	19.0	20.1	21.2	22.3	23.4	24.4	25.5	26.6	27.7	28.8	STE ST
730	78	29.9	31.0	32.1	33.3	34.3	35.3	36.4	37.5	38.6	39.7	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0 01 mm.

731 to 770mm.

				and the same	731	to 7	70mm.			N. C.		
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
731	78	40.8	41.9	43.0	44.1	45.2	46.2	47.3	48.4	49.5	50.6	100
732	78	51.7	52.8	53.9	54.9	56.0	57.0	58.2	59.3	60.3	61.4	2018
733	78	62.5	63.6	64.7	65.8	66.9	67.9	69.0	70.1	71.2	72.3	45
734	78	73.4	74.5	75.6	76.6	77.7	78.8	79.9	81.0	82.0	83.1	
735	78	84.2	85.3	86.4	87.5	88.6	89.6	90.7	91.8	92.9	.94.0	
736	78	95.1	96.2	97.3	98.3	99.4	00.5	01.6	02.7	03.7	04.8	
736	79	05.9	07.0	08.1	09.1	10.2	11.3	12.4	13.5	14.5	15.6	
737	79	16.7	17.8	18.9	19.9	21.0	22.1	23.2	24.3	25.3	26.4	
739	79	27.5	28.6	29.6	30.7	31.8	32.8	33.9	35.0	36.1	37.1	THE REAL PROPERTY.
100	10	2110	20.0	20.0	0011	01.0	0210	1	00.0	00.1		1960
740	79	38.2	39.3	40.4	41.4	42.5	43.6	44.7	45.8	46.8	47.9	
741	79	49.0	50.1	51.1	52.2	53.3	54.3	55.4	56.5	57.6	58.6	GOY Y
742	79	59.7	60.8	61.8	62.9	64.0	65.0	66.1	67.2	68.3	69.3	
743	79	70.4	71.5	72.6	73.6	74.7	75.8	76.9	78.0	79.0	80.1	11105
744	79	81.2	82.3	83.3	84.4	85.5	86.5	87.6	88.7	89.8	90.8	Last 1
745	79	91.9	93.0	94.0	95.1	96.1	97.2	98.3	99.3			2445
745	80	174310	A. A.	4.00	1 700	1,315	SOF	3,000	1.000	00.4	01.4	Add .
746	80	02.5	03.6	04.6	05.7	06.8	07.8	08.9	10.0	11.1	12.3	445
747	80	13.2	14.3	15.3	16.4	17.4	18.5	19.6	20.6	21.7	22.7	not i
748	80	23.8	24.9	25.9	27.0	28.0	29.1	30.2	31.2	32.3	33.3	BIT
749	80	34.4	35.5	36.5	37.6	38.7	39.7	40.8	41.9	43.0	44.0	BSSS T
	1	1				1.4	Roy .	ALC: U	540	0.11	S 45	A TOTAL
750	80	45.1	46.2	47.3	48.4	49.4	50.5	51.6	52.6	53.7	54.7	-1005
751	80	55.7	56.8	57.8	58.9	59.9	61.0	62.1	63.1	64.2	65.2	GET S
752	80	66.3	67.4	68.4	69.5	70.5	71.6	72.7	73.7	74.8	75.8	Direc S
753	80	76.9	78.0	79.0	80.1	81.1	82.2	83.3	84.3	85.4	86.4	-240
754	80	87.5	88.5	89.6	90.6	91.7	92.7	93.8	94.8	95.9	96.9	1 0.1
755	80	98.0	99.1	00.1	07.0	00.0	00.0		05.1	00 =		2 0.2
755	81	08.6	09.6	10.7	01.2	02.2	03.3	04.4	05.4	06.5	07.5	3 0.3
756 757	81 81	19.1	20.1	21.2	11.7	12.8 23.3	13.8	14.9	15.9 26.4	17.0 27.5	18.0 28.5	4 0.4
758	81	29.6	30.6	31.7	32.7	33.8	34.8	35.9	36.9	38.0	39.0	5 0.5
759	81	40.1	41.1	42.2	43.2	44.3	45.3	46.4	47.4	48.5	49.5	6 0.6 7 0.7
.00					10.2	22.0	20.0	20.2	2112	20.0	40.0	7 0.7 8 0.8
760	81	50.6	51.6	52.7	53.7	54.8	55.8	56.9	57.9	59.0	60.0	9 0.9
761	81	61.1	62.1	63.2	64.2	65.3	66.3	67.3	68.4	69.4	70.5	010.0
762	81	71.5	72.5	73.6	74.6	75.7	76.7	77.8	78.8	79.9	80.9	
763	81	82.0	83.0	84.1	85.1	86.2	87.2	88.2	89.3	90.3	91.4	1000 B
764	81	92.4	93.4	94.5	95.5	96.6	97.6	98.6	99.7	150	COT	Had I
764	82		J.Fr	74 50	- LAIL	1434	1211	1	100	00.7	01.8	
765	82	02.8	03.8	04.9	05.9	07.0	08.0	09.0	10.1	11.1	12.2	1855
766	82	13.2	14.2	15.3	16.3	17.4	18.4	19.4	20.5	21.5	22.6	145.25
767	82	23.6	24.6	25.7	26.7	27.8	28.8	29.8	30.9	31.9	33.0	CHE !
768	82	34.0	35.0	36.1	37.1	38.2	39.2	40.2	41.3	42.3	43.4	543
769	82	44.4	45.4	46.5	47.5	48.5	49.5	50.6	51.6	52.6	53.7	265
770	82	54.7	55.7	56.8	57.8	58.8	59.8	60.9	61.9	62.9	64.0	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.

771 to 810mm.

				70.70	100000	1 10 8					P	7/
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr
771	82	65.0	66.0	67.1	68.1	69.2	70.2	71.2	72.3	73.3	74.4	-
772	82	75.4	76.4	77.5	78.5	79.5	80.5	81.6	82.6	83.6	84.7	NAME OF TAXABLE PARTY.
773	82	85.7	86.7	87.8	88.8	89.8	90.8	91.9	92.9	93.9	95.0	4000
774	82	96.0	97.0	98.0	99.1	00.0			210		3010	The N
774	83	A Training				00.1	01.1	02.1	03.1	04.2	05.2	
775	83	06.2	07.2	08.3	09.3	10.3	11.3	12.4	13.4	14.4	15.5	
776	83	16.5	17.5	18.5	19.6	20.6	21.6	22.6	23.6	24.7	25.7	
777	83	26.7	27.7	28.8	29.8	30.8	31.8	32.9	33.9	34.9	36.0	948
778	83	37.0	38.0	39.0	40.1	41.1	42.1	43.1	44.1	45.2	46.2	933
779	83	47.2	48.2	49.2	50.3	51.3	52.3	53.3	54.3	55.4	56.4	
		10			00.0	02.0	02.0		0 1.0			
780	83	57.4	58.4	59.4	60.5	61.5	62.5	63.5	64.5	65.6	66.6	
781	83	67.6	68.6	69.6	70.7	71.7	72.7	73.7	74.7	75.8	76.8	100.5
782	83	77.8	78.8	79.8	80.9	81.9	82.9	83.9	84.9	86.0	87.0	478
783	83	88.0	89.0	90.0	91.1	92.1	93.1	94.1	95.1	96.2	97.2	300
784	83	98.2	99.2	12.00	A THE					-1,-1-1		1000
784	84			00.2	01.2	02.2	03.2	04.3	05.3	06.3	07.3	
785	84	08.3	09.3	10.3	11.4	12.4	13.4	14.4	15.4	16.5	17.5	29E
786	84	18.5	19.5	20.5	21.5	22.5	23.5	24.6	25.6	26.6	27.6	
787	84	28.6	29.6	30.6	31.6	32.6	33.6	34.7	35.7	36.7	37.7	BED
788	84	38.7	39.7	40.7	41.7	42.7	43.7	44.8	45.8	46.8	47.8	
789	84	48.8	49.8	50.8	51.8	52.8	53.8	54.9	55.9	56.9	57.9	1000
.03	0.4	20.0	2010	00.0	01.0	02.0	00.0	01.0	00.0	00.0	0	148 Km
790	84	58.9	59.9	60.9	61.9	62.9	63.9	65.0	66.0	67.0	68.0	
791	84	68.9	69.9	70.9	71.9	72.9	73.9	75.0	76.0	77.0	78.0	1   0.1
792	84	79.0	80.0	81.0	82.0	83.0	84.0	85.0	86.0	87.0	88.0	2 0.2
793	84	89.0	90.0	91.0	92.0	93.0	94.0	95.1	96.1	97.1	98.1	3 0.3
794	84	99.1		02.0	0210	00.0	0 100		00.2			4 0.4
794	85	00.2	00.1	01.1	02.1	03.1	04.1	05.1	06.1	07.1	08.1	5 0.5
795	85	09.1	10.1	11.1	12.1	13.1	14.1	15.1	16.1	17.1	18.1	6 0.6
796	85	19.1	20.1	21.1	22.1	23.1	24.1	25.1	26.1	27.1	28.1	7 0.7
797	85	29.1	30.1	31.1	32.1	33.1	34.1	35.1	36.1	37.1	38.1	8 0.8
798	85	39.1	40.1	41.1	42.1	43.1	44.1	45.1	46.1	47.1	48.1	9 0.9
799	85	49.1	50.1	51.1	52.0	53.0	54.1	55.0	56.0	57.0	58.0	0.00
	00		0012	02.12	02.0	00.0	01.1		00.0		00.0	
800	85	59.0	60.0	61.0	62.0	63.0	64.0	65.0	66.0	67.0	68.0	
801	85	69.0	70.0	70.9	71.9	72.9	73.9	74.9	75.9	76.9	77.9	18-010
802	85	78.9	79.9	80.9	81.9	82.9	83.9	84.9	85.8	86.8	87.8	San San San
803	85	88.8	89.8	90.8	91.8	92.8	93.8	94.8	95.8	96.7	97.7	1
804	85	98.7	99.7			02.0	00.0					-X45
804	86			00.7	01.7	02.7	03.7	04.7	05.7	06.6	07.6	He E I
805	86	08.6	09.6	10.6	11.6	12.6	13.6	14.6	15.5	16.5	17.5	500 S   1
806	86	18.5	19.5	20.5	21.5	22.5	23.4	24.4	25.4	26.4	27.4	All I
807	86	28.4	29.4	30.4	31.3	32.3	33.3	34.3	35.3	36.3	37.3	
808	86	38.3	39.2	40.2	41.2	42.2	43.2	44.2	45.1	46.1	47.1	SEE L
809	86	48.1	49.1	50.1	51.1	52.0	53.0	54.0	55.0	56.0	57.0	THE PERSON NAMED IN
000	00	The said	11.6.1	-		01/07:7		1000			00	THE P
810	86	57.9	58.9	59.9	60.9	61.9	62.8	63.8	64.8	65.8	66.8	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each

TABLE II. Correction for Difference of Temperature of Attached Thermometers.

Temperature of Barometers at Station  $\left\{ egin{aligned} & \text{Upper} = \mathbf{T}' \\ & \text{Lower} = \mathbf{T}. \end{aligned} \right.$ 

,						( Lower =			
T'-T	Correct.	T' - T	Correct.	T' - T	Correct.	T'-T	Correct.	T'-T	Correct.
Centig.	Metres.	Centigrade.	Metres.	Centigrade.	Metres.	Centigrade,	Metres.	Centigrade.	Metres.
0.0	0.0	8.0	10.3	16.0	20.6	24.0	30.9	32.0	41.3
0.2	0.3	8.2	10.6	16.2	20.9	24.2	31.2	32.2	41.5
0.4	0.5	8.4	10.8	16.4	21.1	24.4	31.5	32.4	41.8
0.6	0.8	8.6	11.1	16.6	21.4	24.6	31.7	32.6	42.0
0.8	1.0	8.8	11.3	16.8	21.7	24.8	32.0	32.8	42.3
1.0	1.3	9.0	11.6	17.0	21.9	25.0	32.2	33.0	42.5
1.2	1.5	9.2	11.9	17.2	22.2	25.2	32.5	33.2	42.8
1.4	1.8	9.4	12.1	17.4	22.4	25.4	32.7	33.4	43.1
1.6	2.1	9.6	12.4	17.6	22.7	25.6	33.0	33.6	43.3
1.8	2.3	9.8	12.6	17.8	22.9	25.8	33.3	33.8	43.6
2.0	2.6	10.0	12.9	18.0	23.2	26.0	33.5	34.0	43.8
2.2	2.8	10.2	13.1	18.2	23.5	26.2	33.8	34.2	44.1
2.4	3.1	10.4	13.4	18.4	23.7	26.4	34.0	34.4	44.3
2.6	3.4	10.6	13.7	18.6	24.0	26.6	34.3	34.6	44.6
2.8	3.6	10.8	13.9	18.8	24.2	26.8	34.6	34.8	44.9
3.0	3.9	11.0	14.2	19.0	24.5	27.0	34.8	35.0	45.1
3.2	4.1	11.2	14.5	19.2	24.8	27.2	35.1	35.2	45.4
3.4	4.4	11.4	14.7	19.4	25.0	27.4	35.3	35.4	45.6
3.6	4.6	11.6	15.0	19.6	25.3	27.6	35.6	35.6	45.9
3.8	4.9	11.8	15.2	19.8	25.5	27.8	35.8	35.8	46.2
4.0	5.2	12.0	15.5	20.0	25.8	28.0	36.1	36.0	46.4
4.2	5.4	12.2	15.8	20.2	26.0	28.2	36.4	36.2	46.7
4.4	5.7	12.4	16.0	20.4	26.3	28.4	36.6	36.4	46.9
4.6	5.9	12.6	16.3	20.6	26.6	28.6	36.9	36.6	47.2
4.8	6.2	12.8	16.5	20.8	26.8	28.8	37.1	36.8	47.4
5.0	6.4	13.0	16.8	21.0	27.1	29.0	37.4	37.0	47.7
5.2	6.7	13.2	17.0	21.2	27.3	29.2	37.6	37.2	48.0
5.4	7.0	13.4	17.3	21.4	27.6	29.4	37.9	37.4	48.2
5.6	7.2	13.6	17.5	21.6	27.8	29.6	38.2	37.6	48.5
58	7.5	13.8	17.8	21.8	28.1	29.8	38.4	37.8	48.7
6.0	7.7	14.0	18.0	22.0	28.4	30.0	38.7	38.0	49.0
6.2	8.0	14.2	18.3	22.2	28.6	30.2	38.9	38.2	49.2
6.4	8.3	14.4	18.5	22.4	28.9	30.4	39.2	38.4	49.5
6.6	8.5	14.6	18.8	22.6	29.1	30.6	39.5	38.6	49.8
6.8	8.8	14.8	19.0	22.8	29.4	30.8	39.7	38.8	50.0
7.0	9.0	15.0	19.3	23.0	29.7	31.0	40.0	39.0	50.3
7.2	9.3	15.2	19.6	23.2	29.9	31.2	40.2	39.2	50.5
7.4	9.5	15.4	198	23.4	30.2	31.4	40.5	39.4	50.8
7.6	9.8	15.6	20.1	23.6	30.4	31.6	40.7	39.6	51.1
7.8	10.1	15.8	20.3	23.8	30.7	31.8	41.0	39.8	51.3
8.0	10.3	16.0	20.6	24.0	30.9	32.0	41.3	40.0	51.6

This Table supposes the scale to be of brass from the top to the cistern. If it were of glass or of wood, the argument T'—T ought to be diminished at the ratio of 54 to 62.

In computing by the formula of Laplace, we begin by reducing the barometers to the same temperature by means of the following formula:  $H = h' + h' \left(\frac{T' - T}{6196}\right)$ . Table II. saves this trouble, and gives, in metres, the correction due to the difference of temperature of the barometers.

#### BAROMETRICAL MEASUREMENT OF HEIGHTS. - DELCROS.

TABLE III. CORRECTION FOR DECREASE OF GRAVITATION IN LATITUDE.

 $\beta = (0.0028371 \text{ cosin. 2 L}). (A + \alpha + \beta).$ 

The Argument is the Mean Latitude between the two Stations.

	<u></u>		1	The Alg			attitude between				
Added   Subtret   1000   2000   3000   4000   5000   6000   7000   8000   900   0   2.8   5.7   8.5   11.3   14.2   17.0   19.9   22.7   25.   2   88   2.8   5.7   8.5   11.3   14.2   17.0   19.8   22.7   25.   2   88   2.8   5.7   8.5   11.3   14.1   17.0   19.8   22.6   22.5   2   2   88   2.8   5.6   8.5   11.3   14.1   17.0   19.8   22.6   25.   4   86   2.8   5.6   8.4   11.2   14.0   16.9   19.7   22.6   25.   5   85   2.8   5.6   8.4   11.2   14.0   16.9   19.7   22.5   25.   2   2   2   2   2   2   2   2   2	LATI	TUDE.				Co	rrection, in	metres, for			
0         90         2.8         5.7         8.5         11.3         14.2         17.0         19.9         22.7         25.           1         89         2.8         5.7         8.5         11.3         14.2         17.0         19.8         22.7         25.           3         87         2.8         5.6         8.5         11.3         14.1         16.9         19.7         22.6         25.           4         86         2.8         5.6         8.4         11.2         14.0         16.9         19.7         22.6         25.           5         85         2.8         5.5         8.4         11.2         14.0         16.9         19.7         22.6         25.           6         84         2.8         5.5         8.3         11.1         13.9         16.6         19.4         22.2         25.           7         83         2.7         5.5         8.2         11.0         13.8         16.5         19.3         22.0         24.           8         82         2.7         5.4         8.1         10.8         13.5         16.2         18.9         21.6         24.           10			1000	2000	3000	4000	5000	6000	7000	8000	9000
1         89         2.8         5.7         8.5         11.3         14.2         17.0         19.8         22.7         25.2           2         88         2.8         5.7         8.5         11.3         14.1         17.0         19.5         22.6         25.           3         87         2.8         5.6         8.5         11.3         14.1         16.9         19.7         22.5         25.           4         86         2.8         5.6         8.4         11.2         14.0         16.8         19.6         22.3         25.           6         84         2.8         5.5         8.3         11.1         13.9         16.6         19.4         22.2         22.           8         82         2.7         5.4         8.2         10.9         13.6         16.4         19.1         21.8         24.           9         81         2.7         5.4         8.2         10.9         13.6         16.4         19.1         21.8         22.0         22.0         24.           10         80         2.7         5.3         8.0         10.7         13.3         16.2         18.9         21.6         2	0		28	5.7	8.5	11.3	14.2	17.0	19.9	22.7	25.7
2         88         2.8         5.7         8.5         11.3         14.1         17.0         19.8         22.6         25.           3         87         2.8         5.6         8.5         11.3         14.1         16.9         19.7         22.6         25.           4         86         2.8         5.6         8.4         11.2         14.0         16.9         19.7         22.5         25.           5         85         2.8         5.5         8.3         11.1         13.9         16.6         19.4         22.2         25.           7         83         2.7         5.5         8.2         11.0         13.8         16.5         19.3         22.0         24.           8         82         2.7         5.4         8.2         10.9         13.6         16.4         19.1         21.8         22.0         24.           9         81         2.7         5.4         8.1         10.8         13.5         16.2         18.9         21.6         24.           10         80         2.7         5.3         8.0         10.7         13.3         16.0         18.7         21.3         24.      <		- Care 1	100000000000000000000000000000000000000	0000		THE RESERVE THE PARTY OF THE PA	De la contrata del contrata de la contrata del contrata de la contrata del la contrata de la contrata della contrata della contrata de la contrata de la contrata della contrata de la contrata della con		THE LANGE CO. LANGE CO.		25.6
3         87         2.8         5.6         8.5         11.3         14.1         16.9         19.7         22.6         25.           4         86         2.8         5.6         8.4         11.2         14.0         16.9         19.7         22.5         25.5           5         85         2.8         5.6         8.4         11.2         14.0         16.8         19.6         22.3         25.5           6         84         2.8         5.5         8.3         11.1         13.9         16.6         19.4         22.2         25.           7         83         2.7         5.5         8.2         11.0         13.8         16.5         19.3         22.0         24.           8         82         2.7         5.4         8.1         10.8         16.4         19.1         21.3         24.           10         80         2.7         5.3         8.0         10.7         13.3         16.0         18.7         21.3         24.           11         79         2.6         5.2         7.9         10.5         13.1         15.8         18.4         21.0         21.6         24.2         11.2 <td< td=""><td>11</td><td></td><td>100</td><td></td><td>100000</td><td></td><td>Committee of the Committee of the Commit</td><td></td><td></td><td>Lateral Parks and</td><td>25.5</td></td<>	11		100		100000		Committee of the Commit			Lateral Parks and	25.5
4         86         2.8         5.6         8.4         11.2         14.0         16.9         19.7         22.5         25.           5         85         2.8         5.6         8.4         11.2         14.0         16.8         19.6         22.3         25.           6         84         2.8         5.5         8.3         11.1         13.9         16.6         19.4         22.2         25.           7         83         2.7         5.4         8.2         10.9         13.6         16.4         19.1         21.8         24.           9         81         2.7         5.4         8.1         10.8         13.5         16.2         18.9         21.6         24.           10         80         2.7         5.3         8.0         10.7         13.3         16.0         18.7         21.3         24.           11         79         2.6         5.2         7.8         10.4         13.0         15.5         18.1         20.7         23.           12         78         2.6         5.2         7.8         10.4         13.0         15.5         18.1         20.7         23.           13 </td <td></td> <td></td> <td>1.73</td> <td></td> <td></td> <td>THE PROPERTY OF</td> <td>almost a part of the</td> <td></td> <td>12200</td> <td></td> <td>25.4</td>			1.73			THE PROPERTY OF	almost a part of the		12200		25.4
5         85         2.8         5.6         8.4         11.2         14.0         16.8         19.6         22.3         25.         6         84         2.8         5.5         8.3         11.1         13.9         16.6         19.4         22.2         22.7         7         83         2.7         5.4         8.2         11.0         13.8         16.5         19.3         22.0         24.         8         82         2.7         5.4         8.1         10.8         16.5         19.3         22.0         24.         9         81         2.7         5.4         8.1         10.8         13.5         16.2         18.9         21.6         24.         10         80         2.7         5.3         8.0         10.7         13.3         16.0         18.7         21.3         24.         11         79         2.6         5.2         7.9         10.5         13.1         15.8         18.4         21.0         23.         13         77         2.5         5.1         7.6         10.2         12.7         15.3         17.8         20.4         22.         14.4         76         2.5         5.0         7.5         10.8         12.5         15.0         17.5 </td <td></td> <td></td> <td></td> <td>35.70</td> <td></td> <td></td> <td>SC C#130</td> <td>1 1 1 - 6 - 7 1</td> <td></td> <td>1000</td> <td>25.3</td>				35.70			SC C#130	1 1 1 - 6 - 7 1		1000	25.3
6         84         2.8         5.5         8.3         11.1         13.9         16.6         19.4         22.2         25.7           7         83         2.7         5.5         8.2         11.0         13.8         16.5         19.3         22.0         24.           8         82         2.7         5.4         8.2         10.9         13.6         16.4         19.1         21.8         24.           9         81         2.7         5.4         8.1         10.8         13.5         16.2         18.9         21.6         24.           10         80         2.7         5.3         8.0         10.7         13.3         16.0         18.7         21.3         24.           11         79         2.6         5.2         7.9         10.5         13.1         15.8         18.4         21.0         23.           12         78         2.6         5.2         7.8         10.4         13.0         15.5         18.1         21.0         23.           13         77         2.5         5.1         7.6         10.2         12.7         15.3         17.8         20.0         22.           14	1	The second		Control of the		100000000000000000000000000000000000000	THE AREA STORY			27772	25.1
7         83         2.7         5.5         8.2         11.0         13.8         16.5         19.3         22.0         24.           8         82         2.7         5.4         8.2         10.9         13.6         16.4         19.1         21.8         24.           9         81         2.7         5.4         8.1         10.8         13.5         16.2         18.9         21.6         24.           10         80         2.7         5.3         8.0         10.7         13.3         16.0         18.7         21.3         24.           11         79         2.6         5.2         7.9         10.5         13.1         15.8         18.4         21.0         23.           12         78         2.6         5.2         7.8         10.4         13.0         15.5         18.1         20.7         23.           13         77         2.5         5.1         7.6         10.2         12.7         15.3         17.8         20.4         22.         21.           14         76         2.5         5.0         7.5         10.0         12.5         15.0         17.5         20.0         22.	-			Charles Co.							25.0
8         82         2.7         5.4         8.2         10.9         13.6         16.4         19.1         21.8         24.9           9         81         2.7         5.4         8.1         10.8         13.5         16.2         18.9         21.6         24.           10         80         2.7         5.3         8.0         10.7         13.3         16.0         18.7         21.3         24.           11         79         2.6         5.2         7.9         10.5         13.1         15.8         18.4         21.0         23.           12         78         2.6         5.2         7.8         10.4         13.0         15.5         18.1         20.7         23.           13         77         2.5         5.1         7.6         10.2         12.7         15.3         17.8         20.4         22.           14         76         2.5         5.0         7.5         10.0         12.5         15.0         17.5         20.0         22.           16         74         2.4         4.8         7.2         9.6         12.0         14.4         16.8         19.2         21.1	i		I I Could be a little	1			The second second		A Part of the Control		24.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1		1.25 C 18 7 18 7						100 mm 1		24.5
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		81	The second of		100		13.5		18.9	21.6	24.3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			The state of the s		10 C 10 C 10 C 10 C	The state of the s	Chierry Street		W. T. E. a. G.	and the second	24.0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		79	LA BOLD A BU	March Colonia			11 Car (2) 36			21.0	23.7
14         76         2.5         5.0         7.5         10.0         12.5         15.0         17.5         20.0         22.           15         75         2.5         4.9         7.4         9.8         12.3         14.7         17.2         19.7         22.           16         74         2.4         4.8         7.2         9.6         12.0         14.4         16.8         19.2         21.           17         73         2.4         4.7         7.0         9.4         11.8         14.1         16.5         18.8         21.           18         72         2.3         4.6         6.9         9.2         11.5         13.8         16.1         18.4         20.           19         71         2.2         4.5         6.7         8.9         11.2         13.4         15.6         17.9         20.           20         70         2.2         4.3         6.5         8.7         10.9         13.0         15.2         17.4         19.           21         69         2.1         4.2         6.3         8.4         10.5         12.6         14.7         16.9         19.           21 <td>12</td> <td>78</td> <td></td> <td></td> <td></td> <td>10.4</td> <td>The state of the s</td> <td>15.5</td> <td></td> <td>20.7</td> <td>23.3</td>	12	78				10.4	The state of the s	15.5		20.7	23.3
15         75         2.5         4.9         7.4         9.8         12.3         14.7         17.2         19.7         22.           16         74         2.4         4.8         7.2         9.6         12.0         14.4         16.8         19.2         21.           17         73         2.4         4.7         7.0         9.4         11.8         14.1         16.5         18.8         21.           18         72         2.3         4.6         6.9         9.2         11.5         13.8         16.1         18.4         20.           19         71         2.2         4.5         6.7         8.9         11.2         13.4         15.6         17.9         20.           20         70         2.2         4.3         6.5         8.7         10.9         13.0         15.2         17.4         19.           21         69         2.1         4.2         6.3         8.4         10.5         12.6         14.7         16.9         19.           21         69         2.1         4.2         6.3         8.4         10.5         12.2         14.3         16.3         18.           23	13	77	2.5	5.1	7.6	10.2	12.7	15.3	17.8	20.4	22.9
16         74         2.4         4.8         7.2         9.6         12.0         14.4         16.8         19.2         21.           17         73         2.4         4.7         7.0         9.4         11.8         14.1         16.5         18.8         21.           18         72         2.3         4.6         6.9         9.2         11.5         13.8         16.1         18.4         20.           19         71         2.2         4.5         6.7         8.9         11.2         13.4         15.6         17.9         20.           20         70         2.2         4.3         6.5         8.7         10.9         13.0         15.2         17.4         19.           21         69         2.1         4.2         6.3         8.4         10.5         12.6         14.7         16.9         19.           22         68         2.0         4.1         6.1         8.2         10.2         12.2         14.3         16.3         18.           23         67         2.0         3.9         5.9         7.9         9.8         11.4         13.3         15.2         17.           24	14	76	2.5	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5
17         73         2.4         4.7         7.0         9.4         11.8         14.1         16.5         18.8         21.8           18         72         2.3         4.6         6.9         9.2         11.5         13.8         16.1         18.4         20.           19         71         2.2         4.5         6.7         8.9         11.2         13.4         15.6         17.9         20.           20         70         2.2         4.3         6.5         8.7         10.9         13.0         15.2         17.4         19.           21         69         2.1         4.2         6.3         8.4         10.5         12.6         14.7         16.9         19.           22         68         2.0         4.1         6.1         8.2         10.2         12.2         14.3         16.3         18.           23         67         2.0         3.9         5.9         7.9         9.8         11.8         13.8         15.8         17.           24         66         1.9         3.8         5.7         7.6         9.5         11.4         13.3         15.2         17.           25	15	75	2.5	4.9	7.4	9.8	12.3	14.7	17.2	19.7	22.1
18         72         2.3         4.6         6.9         9.2         11.5         13.8         16.1         18.4         20.           19         71         2.2         4.5         6.7         8.9         11.2         13.4         15.6         17.9         20.           20         70         2.2         4.3         6.5         8.7         10.9         13.0         15.2         17.4         19.           21         69         2.1         4.2         6.3         8.4         10.5         12.6         14.7         16.9         19.           22         68         2.0         4.1         6.1         8.2         10.2         12.2         14.3         16.3         18.           23         67         2.0         3.9         5.9         7.9         9.8         11.8         13.8         15.8         17.           24         66         1.9         3.8         5.7         7.6         9.5         11.4         13.3         15.2         17.           25         65         1.8         3.6         5.5         7.3         9.1         10.9         12.8         14.6         16.           26	16	74	2.4	4.8	7.2	9.6	12.0	14.4	16.8	19.2	21.6
19         71         2.2         4.5         6.7         8.9         11.2         13.4         15.6         17.9         20           20         70         2.2         4.3         6.5         8.7         10.9         13.0         15.2         17.4         19.           21         69         2.1         4.2         6.3         8.4         10.5         12.6         14.7         16.9         19.           22         68         2.0         4.1         6.1         8.2         10.2         12.2         14.3         16.3         18.           23         67         2.0         3.9         5.9         7.9         9.8         11.8         13.8         15.8         17.           24         66         1.9         3.8         5.7         7.6         9.5         11.4         13.3         15.2         17.           25         65         1.8         3.6         5.5         7.3         9.1         10.9         12.8         14.6         16.           26         64         1.7         3.3         5.0         6.7         8.3         10.5         11.7         13.3         15.           27	17	73	2.4	4.7	7.0	9.4	11.8	14.1	16.5	18.8	21.2
20         70         2.2         4.3         6.5         8.7         10.9         13.0         15.2         17.4         19.2           21         69         2.1         4.2         6.3         8.4         10.5         12.6         14.7         16.9         19.           22         68         2.0         4.1         6.1         8.2         10.2         12.2         14.3         16.3         18.           23         67         2.0         3.9         5.9         7.9         9.8         11.8         13.8         15.8         17.           24         66         1.9         3.8         5.7         7.6         9.5         11.4         13.3         15.2         17.           25         65         1.8         3.6         5.5         7.3         9.1         10.9         12.8         14.6         16.           26         64         1.7         3.5         5.2         7.0         8.7         10.5         12.2         14.0         15.           27         63         1.7         3.3         5.0         6.7         8.3         10.0         11.7         13.3         15.           28	18	72	2.3	4.6	6.9	9.2	11.5	13.8	16.1	18.4	20.7
21         69         2.1         4.2         6.3         8.4         10.5         12.6         14.7         16.9         19.           22         68         2.0         4.1         6.1         8.2         10.2         12.2         14.3         16.3         18.           23         67         2.0         3.9         5.9         7.9         9.8         11.8         13.8         15.8         17.           24         66         1.9         3.8         5.7         7.6         9.5         11.4         13.3         15.2         17.           25         65         1.8         3.6         5.5         7.3         9.1         10.9         12.8         14.6         16.           26         64         1.7         3.5         5.2         7.0         8.7         10.5         12.2         14.0         15.           27         63         1.7         3.3         5.0         6.7         8.3         10.0         11.7         13.3         15.           28         62         1.6         3.2         4.8         6.3         7.9         9.5         11.1         12.7         14.           29	19	71	2.2	4.5	6.7	8.9	11.2	13.4	15.6	17.9	20.1
22         68         2.0         4.1         6.1         8.2         10.2         12.2         14.3         16.3         18.           23         67         2.0         3.9         5.9         7.9         9.8         11.8         13.8         15.8         17.           24         66         1.9         3.8         5.7         7.6         9.5         11.4         13.3         15.2         17.           25         65         1.8         3.6         5.5         7.3         9.1         10.9         12.8         14.6         16.           26         64         1.7         3.5         5.2         7.0         8.7         10.5         12.2         14.0         15.           27         63         1.7         3.3         5.0         6.7         8.3         10.0         11.7         13.3         15.           28         62         1.6         3.2         4.8         6.3         7.9         9.5         11.1         12.7         14.           29         61         1.5         3.0         4.5         6.0         7.5         9.0         10.5         12.0         13.           30	20	70	2.2	4.3	6.5	8.7	10.9	13.0	15.2	17.4	19.6
23         67         2.0         3.9         5.9         7.9         9.8         11.8         13.8         15.8         17.           24         66         1.9         3.8         5.7         7.6         9.5         11.4         13.3         15.2         17.           25         65         1.8         3.6         5.5         7.3         9.1         10.9         12.8         14.6         16.           26         64         1.7         3.5         5.2         7.0         8.7         10.5         12.2         14.0         15.           27         63         1.7         3.3         5.0         6.7         8.3         10.0         11.7         13.3         15.           28         62         1.6         3.2         4.8         6.3         7.9         9.5         11.1         12.7         14.           29         61         1.5         3.0         4.5         6.0         7.5         9.0         10.5         12.0         13.           30         60         1.4         2.8         4.3         5.7         7.1         8.5         9.9         11.3         12.           31 <td< td=""><td>21</td><td>69</td><td>2.1</td><td>4.2</td><td>6.3</td><td></td><td>THE RESERVE THE PARTY OF THE PA</td><td></td><td></td><td>16.9</td><td>19.0</td></td<>	21	69	2.1	4.2	6.3		THE RESERVE THE PARTY OF THE PA			16.9	19.0
24         66         1.9         3.8         5.7         7.6         9.5         11.4         13.3         15.2         17.           25         65         1.8         3.6         5.5         7.3         9.1         10.9         12.8         14.6         16.           26         64         1.7         3.5         5.2         7.0         8.7         10.5         12.2         14.0         15.           27         63         1.7         3.3         5.0         6.7         8.3         10.0         11.7         13.3         15.           28         62         1.6         3.2         4.8         6.3         7.9         9.5         11.1         12.7         14.           29         61         1.5         3.0         4.5         6.0         7.5         9.0         10.5         12.0         13.           30         60         1.4         2.8         4.3         5.7         7.1         8.5         9.9         11.3         12.0         13.           31         59         1.3         2.7         4.0         5.3         6.6         8.0         9.3         10.6         12. <td< td=""><td>11</td><td></td><td>The second second</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>18.4</td></td<>	11		The second second								18.4
25         65         1.8         3.6         5.5         7.3         9.1         10.9         12.8         14.6         16.           26         64         1.7         3.5         5.2         7.0         8.7         10.5         12.2         14.0         15.           27         63         1.7         3.3         5.0         6.7         8.3         10.0         11.7         13.3         15.           28         62         1.6         3.2         4.8         6.3         7.9         9.5         11.1         12.7         14.           29         61         1.5         3.0         4.5         6.0         7.5         9.0         10.5         12.0         13.           30         60         1.4         2.8         4.3         5.7         7.1         8.5         9.9         11.3         12.0           31         59         1.3         2.7         4.0         5.3         6.6         8.0         9.3         10.6         12.           32         58         1.2         2.5         3.7         5.0         6.2         7.5         8.7         9.9         11.           33         57<	11				100						17.7
26         64         1.7         3.5         5.2         7.0         8.7         10.5         12.2         14.0         15.27         63         1.7         3.3         5.0         6.7         8.3         10.0         11.7         13.3         15.28         62         1.6         3.2         4.8         6.3         7.9         9.5         11.1         12.7         14.22         14.2         12.0         13.3         13.0         10.5         12.0         13.3         13.0         13.0         4.5         6.0         7.5         9.0         10.5         12.0         13.3         13.0         13		779-20					111111111111111111111111111111111111111		The second second second		17.1
27         63         1.7         3.3         5.0         6.7         8.3         10.0         11.7         13.3         15.           28         62         1.6         3.2         4.8         6.3         7.9         9.5         11.1         12.7         14.           29         61         1.5         3.0         4.5         6.0         7.5         9.0         10.5         12.0         13.           30         60         1.4         2.8         4.3         5.7         7.1         8.5         9.9         11.3         12.           31         59         1.3         2.7         4.0         5.3         6.6         8.0         9.3         10.6         12.           32         58         1.2         2.5         3.7         5.0         6.2         7.5         8.7         9.9         11.           33         57         1.1         2.3         3.5         4.6         5.8         6.9         8.1         9.2         10.           34         56         1.1         2.1         3.2         4.2         5.3         6.4         7.4         8.5         9.           35         55					CONTRACTOR OF THE PARTY OF THE	A CONTRACTOR OF THE PARTY OF TH	and the first of the first				16.4
28         62         1.6         3.2         4.8         6.3         7.9         9.5         11.1         12.7         14.           29         61         1.5         3.0         4.5         6.0         7.5         9.0         10.5         12.0         13.           30         60         1.4         2.8         4.3         5.7         7.1         8.5         9.9         11.3         12.           31         59         1.3         2.7         4.0         5.3         6.6         8.0         9.3         10.6         12.           32         58         1.2         2.5         3.7         5.0         6.2         7.5         8.7         9.9         11.           33         57         1.1         2.3         3.5         4.6         5.8         6.9         8.1         9.2         10.           34         56         1.1         2.1         3.2         4.2         5.3         6.4         7.4         8.5         9.           35         55         1.0         1.9         2.9         3.9         4.8         5.8         6.8         7.8         8.           36         54	I BOTH TO THE REAL PROPERTY OF THE PARTY OF		1		1	STATE OF THE REAL PROPERTY.	THE RESERVE THE SERVE	L 55/17 645.7	Company of the last of the last	DOLLOW THE REAL PROPERTY.	15.7
29         61         1.5         3.0         4.5         6.0         7.5         9.0         10.5         12.0         13.           30         60         1.4         2.8         4.3         5.7         7.1         8.5         9.9         11.3         12.           31         59         1.3         2.7         4.0         5.3         6.6         8.0         9.3         10.6         12.           32         58         1.2         2.5         3.7         5.0         6.2         7.5         8.7         9.9         11.           33         57         1.1         2.3         3.5         4.6         5.8         6.9         8.1         9.2         10.           34         56         1.1         2.1         3.2         4.2         5.3         6.4         7.4         8.5         9.           35         55         1.0         1.9         2.9         3.9         4.8         5.8         6.8         7.8         8.           36         54         0.9         1.7         2.6         3.5         4.4         5.3         6.1         7.0         7.           37         53 <t< td=""><td>11</td><td>175</td><td></td><td></td><td>100000000000000000000000000000000000000</td><td></td><td>THE RESERVE OF THE PARTY OF THE</td><td>COLUMN TO THE REPORT OF THE PARTY OF THE PAR</td><td>The second second</td><td></td><td>15.0</td></t<>	11	175			100000000000000000000000000000000000000		THE RESERVE OF THE PARTY OF THE	COLUMN TO THE REPORT OF THE PARTY OF THE PAR	The second second		15.0
30         60         1.4         2.8         4.3         5.7         7.1         8.5         9.9         11.3         12.           31         59         1.3         2.7         4.0         5.3         6.6         8.0         9.3         10.6         12.           32         58         1.2         2.5         3.7         5.0         6.2         7.5         8.7         9.9         11.           33         57         1.1         2.3         3.5         4.6         5.8         6.9         8.1         9.2         10.           34         56         1.1         2.1         3.2         4.2         5.3         6.4         7.4         8.5         9.           35         55         1.0         1.9         2.9         3.9         4.8         5.8         6.8         7.8         8.           36         54         0.9         1.7         2.6         3.5         4.4         5.3         6.1         7.0         7.           37         53         0.8         1.6         2.3         3.1         3.9         4.7         4.8         5.5         6.2         7.           38									The second second second		
31         59         1.3         2.7         4.0         5.3         6.6         8.0         9.3         10.6         12.           32         58         1.2         2.5         3.7         5.0         6.2         7.5         8.7         9.9         11.           33         57         1.1         2.3         3.5         4.6         5.8         6.9         8.1         9.2         10.           34         56         1.1         2.1         3.2         4.2         5.3         6.4         7.4         8.5         9.           35         55         1.0         1.9         2.9         3.9         4.8         5.8         6.8         7.8         8.           36         54         0.9         1.7         2.6         3.5         4.4         5.3         6.1         7.0         7.           37         53         0.8         1.6         2.3         3.1         3.9         4.7         5.5         6.2         7.           38         52         0.7         1.4         2.1         2.7         3.4         4.1         4.8         5.5         6.           39         51         0.6	1				120000000000000000000000000000000000000			THE PERSON NAMED IN COLUMN 1	5 100 671		13.5
32         58         1.2         2.5         3.7         5.0         6.2         7.5         8.7         9.9         11.           33         57         1.1         2.3         3.5         4.6         5.8         6.9         8.1         9.2         10.           34         56         1.1         2.1         3.2         4.2         5.3         6.4         7.4         8.5         9.           35         55         1.0         1.9         2.9         3.9         4.8         5.8         6.8         7.8         8.           36         54         0.9         1.7         2.6         3.5         4.4         5.3         6.1         7.0         7.           37         53         0.8         1.6         2.3         3.1         3.9         4.7         5.5         6.2         7.           38         52         0.7         1.4         2.1         2.7         3.4         4.1         4.8         5.5         6.           39         51         0.6         1.2         1.8         2.4         2.9         3.5         4.1         4.7         5.           40         50         0.5 </td <td>11</td> <td></td> <td>CONTRACT OF THE</td> <td></td> <td></td> <td></td> <td></td> <td>0.0000000000000000000000000000000000000</td> <td></td> <td>100</td> <td>THE RESERVE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN C</td>	11		CONTRACT OF THE					0.0000000000000000000000000000000000000		100	THE RESERVE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN C
33     57     1.1     2.3     3.5     4.6     5.8     6.9     8.1     9.2     10.       34     56     1.1     2.1     3.2     4.2     5.3     6.4     7.4     8.5     9.       35     55     1.0     1.9     2.9     3.9     4.8     5.8     6.8     7.8     8.       36     54     0.9     1.7     2.6     3.5     4.4     5.3     6.1     7.0     7.       37     53     0.8     1.6     2.3     3.1     3.9     4.7     5.5     6.2     7.       38     52     0.7     1.4     2.1     2.7     3.4     4.1     4.8     5.5     6.       39     51     0.6     1.2     1.8     2.4     2.9     3.5     4.1     4.7     5.       40     50     0.5     1.0     1.5     2.0     2.5     3.0     3.4     3.9     4.       41     49     0.4     0.8     1.2     1.6     2.0     2.4     2.8     3.2     3.       42     48     0.3     0.6     0.9     1.2     1.5     1.8     2.1     2.4     2.8	11	22 - 20	The same of the same				U11700-000-2110		Section 1 to 1 to 1	and the contract of	ALCOHOLD BY
34     56     1.1     2.1     3.2     4.2     5.3     6.4     7.4     8.5     9.       35     55     1.0     1.9     2.9     3.9     4.8     5.8     6.8     7.8     8.       36     54     0.9     1.7     2.6     3.5     4.4     5.3     6.1     7.0     7.       37     53     0.8     1.6     2.3     3.1     3.9     4.7     5.5     6.2     7.       38     52     0.7     1.4     2.1     2.7     3.4     4.1     4.8     5.5     6.       39     51     0.6     1.2     1.8     2.4     2.9     3.5     4.1     4.7     5.       40     50     0.5     1.0     1.5     2.0     2.5     3.0     3.4     3.9     4.       41     49     0.4     0.8     1.2     1.6     2.0     2.4     2.8     3.2     3.       42     48     0.3     0.6     0.9     1.2     1.5     1.8     2.1     2.4     2.8		13.				11111 4 1 1 1 1 1 1 1 1					10.4
35         55         1.0         1.9         2.9         3.9         4.8         5.8         6.8         7.8         8.           36         54         0.9         1.7         2.6         3.5         4.4         5.3         6.1         7.0         7.           37         53         0.8         1.6         2.3         3.1         3.9         4.7         5.5         6.2         7.           38         52         0.7         1.4         2.1         2.7         3.4         4.1         4.8         5.5         6.2         7.           39         51         0.6         1.2         1.8         2.4         2.9         3.5         4.1         4.7         5.           40         50         0.5         1.0         1.5         2.0         2.5         3.0         3.4         3.9         4.           41         49         0.4         0.8         1.2         1.6         2.0         2.4         2.8         3.2         3.           42         48         0.3         0.6         0.9         1.2         1.5         1.8         2.1         2.4         2.	H			-	The second second second			The second second			9.6
36         54         0.9         1.7         2.6         3.5         4.4         5.3         6.1         7.0         7.           37         53         0.8         1.6         2.3         3.1         3.9         4.7         5.5         6.2         7.           38         52         0.7         1.4         2.1         2.7         3.4         4.1         4.8         5.5         6.           39         51         0.6         1.2         1.8         2.4         2.9         3.5         4.1         4.7         5.           40         50         0.5         1.0         1.5         2.0         2.5         3.0         3.4         3.9         4.           41         49         0.4         0.8         1.2         1.6         2.0         2.4         2.8         3.2         3.           42         48         0.3         0.6         0.9         1.2         1.5         1.8         2.1         2.4         2.	11	1910.0		a like one	C. C. L. C. L.		BUT PULL IN MARKET BE			The state of the s	8.7
37         53         0.8         1.6         2.3         3.1         3.9         4.7         5.5         6.2         7.           38         52         0.7         1.4         2.1         2.7         3.4         4.1         4.8         5.5         6.           39         51         0.6         1.2         1.8         2.4         2.9         3.5         4.1         4.7         5.           40         50         0.5         1.0         1.5         2.0         2.5         3.0         3.4         3.9         4.           41         49         0.4         0.8         1.2         1.6         2.0         2.4         2.8         3.2         3.           42         48         0.3         0.6         0.9         1.2         1.5         1.8         2.1         2.4         2.	11		A CONTRACTOR OF THE PARTY OF TH	AND DESCRIPTION		and the second second	100000000000000000000000000000000000000	THE RESERVE TO SHEET		THE RESERVE OF THE PARTY OF THE	7.9
38     52     0.7     1.4     2.1     2.7     3.4     4.1     4.8     5.5     6.       39     51     0.6     1.2     1.8     2.4     2.9     3.5     4.1     4.7     5.       40     50     0.5     1.0     1.5     2.0     2.5     3.0     3.4     3.9     4.       41     49     0.4     0.8     1.2     1.6     2.0     2.4     2.8     3.2     3.       42     48     0.3     0.6     0.9     1.2     1.5     1.8     2.1     2.4     2.	11			1	1	177 STATE TO STATE OF THE STATE	Description of the second second	The state of the s		The Control of	7.0
39     51     0.6     1.2     1.8     2.4     2.9     3.5     4.1     4.7     5.       40     50     0.5     1.0     1.5     2.0     2.5     3.0     3.4     3.9     4.       41     49     0.4     0.8     1.2     1.6     2.0     2.4     2.8     3.2     3.       42     48     0.3     0.6     0.9     1.2     1.5     1.8     2.1     2.4     2.	1	DATE BY				The second second	1001-003-00	1200 1000	The second second	A COLUMN TO A STATE OF	6.2
40     50     0.5     1.0     1.5     2.0     2.5     3.0     3.4     3.9     4.       41     49     0.4     0.8     1.2     1.6     2.0     2.4     2.8     3.2     3.       42     48     0.3     0.6     0.9     1.2     1.5     1.8     2.1     2.4     2.					1	CONTRACTOR OF THE PARTY OF THE	CONTRACTOR STATES	THE R. P. LEWIS CO., LANSING	The second second	2011/2012	5.3
41     49     0.4     0.8     1.2     1.6     2.0     2.4     2.8     3.2     3.4       42     48     0.3     0.6     0.9     1.2     1.5     1.8     2.1     2.4     2.2						in the same of the same	CAMP COLUMN	ALC: THE RESERVE OF THE PARTY O			4.4
42 48 0.3 0.6 0.9 1.2 1.5 1.8 2.1 2.4 2.		Conc.		No. of Contract of	1	CONTRACTOR OF STREET				THE CONTRACTOR	3.5
				188-55U-05-73	La Laborita I	C. C. ST A-W 1423 R	LILLIE LITERATE	Committee of the Commit	the second second second	A STATE OF THE PARTY OF THE PAR	2.7
	11			The second second	1 1 1 1 1 1 1 1 1			Control of the contro		The state of the s	1.8
44 46 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.	44	46		0.2	0.3	0.4		0.6	0.7	CONTRACTOR OF THE PARTY OF THE	0.9
45   45   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	45	45	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

TABLE IV. Correction for Decrease of Gravitation on a Vertical Line.

$$\delta = \left(\frac{A + \alpha + \beta + \nu + 15296}{6366200}\right) \times A \left(+\alpha + \beta + \nu\right).$$

Argument =  $(A + \alpha + \beta + \nu)$ .

Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond. Correction Positive.
Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
100	0.2	2100	6.0	4100	12.9	6100	21.1
200	0.5	2200	6.3	4200	13.3	6200	21.6
300	0.8	2300	6.6	4300	13.7	6300	22.0
400	1.0	2400	6.9	4400	14.1	6400	22.5
500	1.3	2500	7.3	4500	14.5	6500	22.9
600	1.6	2600	7.6	4600	14.9	6600	23.4
700	1.8	2700	7.9	4700	15.3	6700	23.9
800	2.1	2800	8.3	4800	15.7	6800	24.3
900	2.4	2900	8.6	4900	16.1	6900	. 24.8
1000	2.7	3000	8.9	5000	16.5	7000	25.3
1100	2.9	3100	9.3	5100	16.9	7100	25.7
1200	3.2	3200	9.6	5200	17.3	7200	26.2
1300	3.5	3300	10.0	5300	17.7	7300	26.7
1400	3.8	3400	10.3	5400	18.1	7400	27.2
1500	4.1	3500	10.7	5500	18.5	7500	27.7
1600	4.4	3600	11.1	5600	19.0	7600	28.1
1700	4.7	3700	11.4	5700	19.4	7700	28.6
1800	5.0	3800	11.8	5800	19.8	7800	29.1
1900	5.3	3900	12.2	5900	20.3	7900	29.6
2000	5.6	4000	12.5	6000	20.7	8000	30.1

TABLE V. CORRECTION FOR THE ELEVATION OF THE LOWER STATION ABOVE OCEAN.

Argument = Height of Barometer at Lower Station.

Metres. 1000 2000 3000 4000		He	ight of Baron	neter at Lowe	er Station in	Millimetres.		
Difference	400	450	500	550	600	650	700	750
Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
1000	1.7	1.4	1.1	0.9	0.6	0.4	0.2	0.0
2000	3.4	2.8	2.2	1.7	1.3	0.8	0.4	0.1
3000	5.1	4.2	3.3	2.6	1.9	1.3	0.7	0.1
4000	6.8	5.6	4.4	3.4	2.5	1.7	0.9	0.1
5000	8.5	6.9	5.5	4.3	3.1	2.1	1.1	0.1
6000	10.3	8.3	6.7	5.2	3.8	2.5	1.3	0.2
7000	12.0	9.7	7.8	6.0	4.4	2.9	1.5	0.2
8000	13.7	11.1	8.9	6.9	5.0	3.4	1.8	0.2
9000	15.4	12.5	10.0	7.7	5.7	3.8	2.0	0.3

#### II.





FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

BY A. GUYOT.

Tables which, like the preceding ones by Delcros, in metrical measures, are sufficiently extensive to save the necessity of interpolations, relieve the computer of most of his trouble, and considerably reduce the chances of error in the computations. They thus render to science itself a real service, by inducing observers to determine a larger number of points, and to secure the accuracy of the results by repeating their observations at the same point in various atmospheric circumstances, both of which they can do without fear of being overwhelmed by the labor of the computation.

Similar tables are here offered to the observers who use instruments graduated to English measures. Like those of Delcros, the new tables are based on Laplace's formula, with a slight modification of only one constant. They dispense with the use of logarithms, and give the differences of level corresponding to every thousandth of an inch from 12 to 31 inches by means of the simplest arithmetical operations, so that the data being prepared and corrected, the computation of an elevation takes but a few minutes, and is done with scarcely any chance of error.

Laplace's formula and constants were adopted for the computation of the tables in preference to others found in the following sets for reasons which a few words will explain.

It has been remarked, page 9, that, in consequence of Laplace's constants having been retained in Gauss's, Schmidt's, and Baily's formulæ, they all give similar results; but that Bessel's formula differs in separating the correction due to the moisture of the air from that due to its temperature, while in Laplace's, and in the formulæ just mentioned, both are united. To introduce a separate correction for the expansion of aqueous vapor is, in the writer's view, a doubtful improvement. The laws of the distribution and transmission of moisture through the atmosphere are too little known, and its amount, especially in mountain regions, is too variable, and depends too much upon local winds and local condensation, to allow a reasonable hope of obtaining the mean humidity of the layer of air between the two stations by means of hygrometrical observations taken at each of them. These doubts are confirmed by the experience of the author and of many other observers, which shows that, on an average, Laplace's method works not only as well as the other, but more uniformly well. At any rate, the gain, if there is any, is not clear enough to compensate for the undesirable complication of the formula.

Though the several co-efficients of Laplace's formula need perhaps to be modified according to more recent and probably more accurate determinations of the physical constants on which they depend, as has been proposed by Plantamour, E. Ritter, and lately by the writer himself in a paper read before the American Association for the Advancement of Science at their meeting in Montreal, they have been retained in preparing the following tables, partly because it was found that the errors due to

the various co-efficients nearly compensate each other; partly on the ground that, until a severe test, by means of actual comparative measurements made for the purpose, has shown the expediency of these modifications, it seemed desirable to adhere to the old constants, and thus to preserve a uniformity in the results with the tables of Oltmans, Delcros, Gauss, Baily, and others, which have already been extensively used. The substitution of the co-efficient 0.00260, expressing, according to Schmidt's computation (Mathem. und Physic. Geogr., II. p. 202), the variation of gravity in latitude, for the value 0.002837, does not sensibly alter the altitudes obtained.

The close agreement of the determinations furnished by Laplace's formula, in barometrical measurements carefully conducted, made in favorable circumstances, and during the warm season, with those obtained from repeated trigonometrical observations, or by the spirit-level, strongly testifies in favor of its general correctness. A few striking examples will suffice to show it.

The altitude of Mont Blanc, measured by the barometer, by MM. Bravais and Martins, on the 29th of August, 1844, and computed by Delcros, by means of nine corresponding stations situated on all sides of the mountain (see *Annuaire Météorologique de France*, for 1851, p. 274), was found to be 4810 metres. The altitude of the same point, being the mean of seven of the most elaborate and reliable geodetic measurements, which cost nearly twenty years of labor, is 4809.6 metres.

For smaller elevations the formula seems to answer equally well.

The barometrical measurement of Mount Washington, in New Hampshire, by the author, on the 8th and 9th of August, 1851, gave, by Delcros's Tables, for the mean of eight observations, taken at different hours of the day, 5466.7 English feet above Gorham, N. H., 6285.7 above high tide, and 6291.7 feet above the mean level of the ocean in Portland harbor. In August, 1852, W. A. Goodwin, Civil Engineer, starting from Gorham Railroad Station, found, by the spirit-level, Mount Washington to be 6285.5 feet above mean tide. In September, 1853, Captain T. J. Cram, of the Topographical Engineers, executed, in behalf of the Coast Survey, a careful measurement with the spirit-level, on the same line, for the purpose of testing the various methods of measuring altitudes, and found Mount Washington to be 6293 English feet above the mean level of the ocean.

In lower latitudes the formula showed equally good results. By a barometrical measurement in July, 1856, the altitude of the highest peak of the Black Mountain, North Carolina, about Lat. 36°, was found by the author to be 6701 English feet; and that of the highest Mountain House 5248 feet. In September, 1857, Major T. C. Turner, Chief Engineer of the Morganton Railroad, ran a line of levels from the same point which was used as the lower station for the barometrical measurement, to the top of the highest peak, and found its altitude to be 6711 English feet, and that of the Mountain House 5246 feet. Other points on the line agreed equally well.

Such an agreement, in so considerable elevations, is all that can be desired.

These figures show conclusively, that, when the errors which may arise from the great variability of the data furnished by the instruments have been removed by a repetition, in various states of the atmosphere, and by a proper combination of simultaneous observations at stations not too distant from each other, those which remain and may be attributed to the formula cannot be considerable. But, on the other

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hand, we have no right to expect such results from single observations, taken, perhaps, in unsettled weather, without paying any regard to the time of the day at which they were made, to the distance or the non-simultaneity of the corresponding observations, or to other unfavorable circumstances. It is too well known that in such cases large errors may and do actually occur; but for these the formula ought not to be held responsible.

#### ARRANGEMENT OF THE TABLES.

If we call

h = the observed height of the barometer  $\tau =$  the temperature of the barometer t at the lower station;

t =the temperature of the air

h' = the observed height of the barometer

 $\tau'$  = the temperature of the barometer

t' = the temperature of the air

at the upper station.

If we make, further,

Z = the difference of level between the two barometers;

L = the mean latitude between the two stations;

H= the height of the barometer at the upper station reduced to the temperature of the barometer at the lower station; or,

 $H = h' \{1 + 0.00008967 (\tau - \tau')\};$ 

The expansion of the mercurial column, measured by a brass scale, for 1° Fahrenheit = 0.00008967;

The increase of gravity from the equator to the poles = 0.00520048, or 0.00260 to the 45th degree of latitude;

The earth's mean radius = 20,886,860 English feet;

Then, Laplace's formula, reduced to English measures, reads as follows:

$$Z = \log \frac{h}{H} \times 60158.6 \text{ English feet} \left\{ egin{align*} \left(1 + rac{t + t' - 64}{900}
ight). \\ \left(1 + 0.00260\cos 2 L
ight). \\ \left(1 + rac{z + 52252}{20886860} + rac{h}{10443430}
ight). \end{aligned} 
ight.$$

Table I. gives, in English feet, the value of  $\log H$  or  $h \times 60158.6$  for every hundredth of an inch, from 12 to 31 inches in the barometer, together with the value of the additional thousandths, in a separate column. These values have been diminished by a constant, which does not alter the difference required.

Table II. gives the correction 2.343 feet  $\times$   $(\tau - \tau')$  for the difference of the temperatures of the barometers at the two stations, or  $\tau - \tau'$ . As the temperature at the upper station is generally lower,  $\tau - \tau'$  is usually positive, and the correction negative. It becomes positive when the temperature of the upper barometer is higher, and  $\tau - \tau'$  negative. When the heights of the barometers have been reduced to the same temperature, or to the freezing point, this table will not be used.

Table IV. shows the correction  $D' \frac{z + 52252}{20886860}$  to be applied to the approximate altitude for the decrease of gravity on a vertical acting on the density of the mercurial column. It is always additive.

Table V. furnishes the small correction  $\frac{h}{10443430}$  for the decrease of gravity on a vertical acting on the density of the air; the height of the barometer h at the lower station representing its approximate altitude. Like the preceding correction, it is always additive.

#### USE OF THE TABLES.

In Table I. find first the numbers corresponding to the observed heights of the barometer h and h'. Suppose, for instance, h=29.345 in.; find in the first column on the left the number 29.3; on the same horizontal line, in the column headed .04, is given the number corresponding to 29.34=28121.7; in the last column but one on the right, we find for .005=4.5, or for 29.345=28126.2. Take likewise the value of h', and find the difference.

If the barometrical heights have not been previously reduced to the same temperature, or to the freezing point, apply to the difference the correction found in Table II. opposite the number representing  $\tau - \tau'$ ; we thus obtain the approximate difference of level, D.

For computing the correction due to the expansion of the air according to its temperature, or  $D \times \left(\frac{t+t'-64}{900}\right)$ , make the sum of the temperatures, subtract from that sum 64; multiply the rest into the approximate difference D, and divide the product by 900. This correction is of the same sign as (t+t'-64). By applying it, we obtain a second approximate difference of level, D'.

In Table III., with D' and the mean latitude of the stations, find the correction for variation of gravity in latitude, and add it to D', paying due attention to the sign.

In Table IV. with D', and in Table V. with D' and the height of the barometer at the lower station, take the corrections for the decrease of gravity on a vertical, and add them to the approximate difference of level.

The sum thus found is the true difference of level between the two stations, or Z; by adding the elevation of the lower station above the level of the sea, when known, we obtain the *altitude* of the upper station.

The use of the small table, VI., by means of which approximate differences of level can be obtained by a single multiplication, is explained below, page 90.

# Example 1.

Measurement of Mount Washington, New Hampshire, by A. Guyot, August 8th, 1851, 4 p. M.; the barometer at the lower station being at 825 English feet above the mean level of the sea; at the upper station at one foot below the summit.

The observation gave,

Gorham, 
$$h=29.272$$
 in.  $\tau=70^{\circ}.70$  F.  $t=72^{\circ}.05$  F. Mount Washington,  $h'=24.030$  "  $t=72^{\circ}.52$  F.  $t'=50^{\circ}.54$  F.  $t'=50^{\circ}.54$  F.  $t'=64^{\circ}.52$  F.

#### BAROMETRICAL MEASUREMENT

Table I. gives for $h = 29.272$ inches, for $h' = 24.030$ "	28,061.00 22,905.60
Difference,	5,155.40
Table II. gives for $\tau - \tau' = 16^{\circ}.38$	- 37.64
Approximate difference of level, D =	5,117.76
$\frac{D \times (t + t' - 64)}{900} = \frac{5118 \times 58.6}{900} =$	333.19
Second approximate difference, $D'=$	5,450.95
Table III. gives for $D'=5450$ and Lat. $44^{\circ}$	0.50
Table IV. gives for $D'=5450$	14.94
Table V. gives for $h = 29.27$	0.00
Barometer below summit,	+ 1.00
Mount Washington above Gorham, or $Z=$	5,465.39
Barometer at Gorham above sea level	825.00
Mount Washington above the sea, or altitude,	6,290.39 Eng. ft.

# Example 2.

Measurement of the highest peak of the Black Mountain, in North Carolina, July 11th, 1856, by A. Guyot.

By observation we have at,

	Barometer.	Attached Thermometer	r. Tempe	rature of Air.
Mountain House,	h = 24.934  in.	$\tau = 64^{\circ}.58 \text{ F}.$	t = 0	61°.34 F.
Highest Peak,	h' = 23.662 "	$\tau' = 61^{\circ}.88 \text{ F.}$	t'=	59°.36 F.
	7-	$-\tau' = 2^{\circ}.70 \text{ F}.$	19	20°.70 F.
			(	64°
		t+t'	-64 = 3	56°.7 F.
Table I. gives	for $h = 24.934$ .		. 23,87	0.4
	for $h' = 23.662$			
en recent or control of the real of	Difference	e,	. 1.36	8.0
Table II. gives	for $\tau - \tau' = 2.7$			
		nate difference, L		THE RESERVE TO SERVE
		$\frac{4)}{900} = \frac{1362 \times 56.7}{900}$		5.8
	Second approxim	nate difference, D	' = 1,44	7.5
Table III. give	s for $D'=1448$ ar	nd Lat. 36° .		1.2
Table IV. give	es for $D'=1448$			3.8
Table V. give	s for $D'=1448$ ar	nd h = 25 .		0.7
Highest peak	above Mountain Hou	use, or	$Z = \overline{1,45}$	3.2
	se above the sea			
Black Mountai	in, highest peak abo	ve the sea, or altit	tude, 6,70	)1.6 Eng. ft.

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# TABLES

FOR COMPUTING THE DIFFERENCE IN THE HEIGHT OF TWO PLACES FROM BAROMETRICAL OBSERVATIONS.

I. D = 60158.58 X log H or h. Argument, the observed Height of the Barometer at either Station.

Barometer	Eng. Inch.	19.0	12.1	12.2	12.3	12.4		12.5	12.6	12.7	12.8	12.9	1	13.0	13.1	13.2	13.3	13.4
Thousandths	Inch.	and the		Feet.	1 2.1	2 4.2		3 6.2	4 8.3	5 10.4	6 12.5	7 14.6	11	8 16.6	9 18.7	N		
	60.	Eng. Feet.	4990.0	5387.2	5599.0	0.6089		6017.4	6224.0	6429.2	6632.7	6834.5		7034.9	7233.8	7431.1	7627.0	7821.4
	80.	Eng. Feet.	5159 4	5367.0	5578.9	5788.1		5996.6	6203.5	6408.8	6612.4	6814.4		7014.9	7213.9	7411,4	1.7097	7802.0
	.00	Eng. Feet.	4910.4	5344.7	5556.8	5767.2		5975.8	6182.8	6388.3	6592.1	6794.3		6995.0	7194.1	7391.8	7587.9	7782.6
en and	90°	Eng. Feet.	4593.7	5323.4	5535.7	5746.2		5955.0	6162.2	6367.8	8:11:9	6774.1		6975.0	7174.3	7372.1	7568.4	7763.2
of an Inch.	.05	Eng. Feet.	4872.1	5302.1	5514.5	5725.3		5934.2	6141.6	6347.3	6551.5	6754.0		6955.0	7154.4	7352.3	7548.8	7743.8
Hundredths of an Inch.	.04	Eng. Feet.	4850.4	5280.7	5493.4	5704.3		5913.4	6120.9	6326.8	6531.1	6733.8		6934.9	7134.5	7332.6	7529.2	7724.4
	.03	Eng. Feet.	4828.7	5259.4	5472.2	5683.2		5892.6	6100.2	6306.3	6510.8	6713.6	Total Control	6914.9	7114.6	7312.9	7509.6	7704.9
-	.02	Eng. Feet.	4806.9	5238.0	5452.0	5662.2		5871.7	9.6209	6285.8	6490.4	6693.4		6894.8	7.094.7	7293.1	7490.0	7685.4
vein svin	10.	Eng. Feet.	4785.2	5216.6	5429.8	5641.2	X	5850.8	6058.8	6265.2	6470.0	6673.2		6874.7	7074.8	7273.3	7470.4	0.9994
	00.	Eng. Feet.	4763.4	4980.2	5408.5	5620.1	The state of the s	5829.9	6038.1	6244.6	6449.6	6652.9		6854.7	7054.9	7253.6	7450.8	7646.5
Barometer	in Eng. Inch.		12.0	12.1	12.3	12.4		12.5	12.6	12.7	12.8	12.9		13.0	13.1	13.2	13.3	13.4

		1 4			1/4												6			1	10	A.	5	4	3	
	Eng. Inch.	16 C	13.6	13.7	13.8	13.9	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	15.0	15.1	15.2	15.3	15.4	12.00	15.6	15.7	15.8	15.9
Thousandths of an	nen.		Feet.	1.9	8.8	9.9	7.5	9.4	11.3	13.2	15.0	17.0		244	1.7	3.4	5.1	8.9	8.5	10.2	11.9	13.6	15.3			
Thou				-	03	က	4	10	9	7	œ	6			-	Ø	က	4	10	9	2	œ	6			
	60.	Eng. Feet.	8205.9	8396.0	8584.8	8772.2	8958.3	9143.0	9326.5	9508.7	9.6896	8.6986	10047.8	10225.1	10401.2	10576.0	10749.6	10922.1	11093.5	11263.8	11433.0	11601.1	11768.2	11934.3	12099.2	12263.1
	80.	Eng. Feet.	8186.8	8377.1	8565.9	8753.5	8939.7	9124.6	9308.2	9490.5	9671.6	9851.4	10030.0	10207.4	10383.6	10558.6	10732.3	10904.9	11076.4	11246.8	11416.2	11584.4	11751.6	11917.7	12082.7	12246.7
	20.	Eng. Feet.	8167.7	8358.1	8547.1	8734.8	8921.2	9106.2	9289.9	9472.3	9653.5	9833.5	10012.2	10189.7	10366.1	10541.2	10715.0	10887.7	11059.3	11229.8	11399.3	11567.6	11734.9	11901.1	12066.3	12230.4
	90.	Eng. Feet.	8148.6	8339.1	8528.3	8716.1	8902.6	9087.8	9271.6	9454.2	9635.5	9815.6	9994.4	10172.0	10348.5	10523.7	9.26901	10870.5	11042.2	11212.8	11382.4	11550 8	11718.2	11884.6	12049.8	12214.0
Hundredths of an Inch.	.05	Eng. Feet.	8199.4	8320.1	8509.4	8697.4	8884.0	8.6906	9253.3	9436.0	9617.4	9.797.6	9976.5	10154.3	10330.9	10506.3	10680.3	10853.2	11025.1	11195.8	11365.5	115340	11701.5	11868.0	12033.3	12197.6
Hundredth	.04	Eng. Feet.	81103	8301.1	8490.6	9.8198	8865.4	9020.8	9234.9	9417.7	9599.3	9.6226	9958.7	10136.6	10313.3	10488.8	10662.9	10836.0	11008.0	11178.8	11348.6	11517.9	11684.8	11851.4	12016.9	12181.2
	.03	Eng. Feet.	8091 1	8282.1	8471.7	8659.9	8846.8	9032.4	9216.6	9399.5	9581.2	9761.7	9940.9	10118.8	10295.7	10471.3	10645.6	10818.7	8.06601	11161.8	11331.6	11500 4	11668.1	11834.8	12000.4	12164.8
	.02	Eng. Feet.	8071.9	8263.1	8452.8	8641.1	8828.2	9013.9	9198.2	9381.3	9563.1	9743.7	9923.0	10101.1	10278.0	10453.8	10628.2	10801.5	10973.6	11144.7	11314.7	11483.6	11651.4	11818.2	11983.8	12148.4
	10.	Eng. Feet.	8059 8	8244.0	8433.9	8622.3	8809.5	8995.4	9179.8	9363.0	9545.0	9725.7	9905.1	10083.3	10260.4	10436.3	10610.8	10784.1	10956.5	11127.7	11297.8	11466.7	11634.6	11801.5	11967.3	12132.0
	00.	Eng. Feet.	0.0401	8225.0	8415.0	8603.6	8790.8	89768	9161.4	9344.7	9526.8	9.707.6	9887.2	10065.5	10242.7	10418.7	10593.4	10766.9	10939.3	11110.6	11280.8	11449.9	11617.9	11784.9	11950.8	12115.6
Barometer	Eng. Inch.	1 6	19.6	13.7	13.8	13.9	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	15.0	15.1	15.2	15.3	15.4	70	15.6	15.7	15.8	15.9

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Barometer	Eng. Inch.		16.0	1.91	16.2	16.3	16.4	9	10.0	9.91	16.7	16.8	16.9		17.0	17.1	17.2	17.3	17.4		6.71	17.6	17.7	17.8	17.9	0	18.0	18.1	18.2	18.3	18.4
Thousandths	Inch.		Poot	reer.	1.6	3.1	4.7	6	6.9	7.8	9.4	11.0	12.5		14.1				1.5		2.9	4.4	80.00	7.3	8.8		10.2	11.7	13.1		
Thous	4 H			3	_	67	က		4	20	9	7	00		6.			130	Н	(	N	es	4	10	9		-	00	6		-
	60.	Eng. Feet.	12426.1	12588.0	12748.9	12908.8	13067.7	70001	1.62251	13382.7	13538.7	13693.9	13848.1		14001.5	14153.9	14305.5	14456.2	14605.9		.14754.9	14903.0	15050.3	15196.7	15342.4	1	15487.1	15631.2	15774.4	15916.8	16058 5
	80.	Eng. Feet.	12409.9	12571.9	12732.9	12892.9	13051.9	0 01061	13210.0	13367.1	13523.2	13678.4	13832.7		13986.2	14138.7	14290.3	14441.1	14591.0		14740.1	14888.2	15035.6	15182.1	15327.8		15472.7	15616.8	15760.1	15902.6	16044 4
	. 20.	Eng. Feet.	12393.6	12555.7	12716.8	12876.9	13036.0	0 10101	15194.2	13351.4	13507.6	13662.9	13817.3		13970.9	14123.5	14275.2	14426.1	14576.1	1	14725.2	14873.5	15020.9	15167.5	15313.3	, 1	15458.2	15602.4	15745.8	15888.4	10000
	90.	Eng. Feet.	12377.4	12539.6	12700.8	12861.0	13020.2	02161	13178.4	13335.7	13492.0	13647.4	13801.9		13955.6	14108.3	14260.1	14411.0	14561.1		14710.3	14858.7	15006.2	15152.9	15298.7		15443.7	15588.0	15731.5	15874.2	100101
Hundredths of an Inch.	.05	Eng. Feet.	12361.1	12523.4	12684.7	12845.0	13004.3	0 60161	13162.6	13320.0	13476.4	13631.9	13786.5		13940.2	14093.0	14244.9	14396.0	14546.1	1 4	14695.4	14843.9	14991.5	15138.2	15284.2		15429.3	15573.6	15717.2	15859.9	10001
Hundredth	.04	Eng. Feet.	12344.8	12507.2	12668.6	12829.0	12988.4	0 07 101	13146.8	13304.3	13460.8	13616.4	13771.1		13924.9	14077.8	14229.8	14380.9	14531.2		14680.5	14829.1	14976.8	15123.6	15269.6	The state of the s	15414.8	15559.2	15702.9	15845.7	0 4004
	.03	Eng. Feet.	12328.5	12491.0	12652.5	12813.0	12972.5	0.0.0.	13131.0	13288.6	13445.2	13600.9	13755.7		13909.6	14062.6	14214.6	14365.8	14516.2		14665.6	14814.3	14962.0	15109.0	15255.0		15400.3	15544.8	15688.5	15831.4	0 0000
	.02	Eng. Feet.	12312.2	12474.8	12636.4	12797.0	12956.6	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	13115.2	13272.9	13429.6	13585.4	13740.3		13894.2	14047.3	14199.4	14350.8	14501.2	a distance	14650.7	14799.4	14947.3	15094.3	15240.5	No. of Contract of	15385.8	15530.4	15674.2	15817.2	, 02020
all selection of the se	10.	Eng. Feet.	12295.9	12458.6	12620.3	12781.0	12940.7	. 0000	13099.4	13257.2	13414.0	13569.8	13724.8		13878.8	14032.0	14184.3	14335.7	14486.2	No position of	14635.8	14784.6	14932.5	15079.6	15225.9		15371.3	15516.0	15659.9	15802.9	0 170 12
The state of the s	00.	Eng. Feet.	12279.6	12442.4	12604.2	12765.0	12924.8	0 0000	13083.6	13241.5	13398.4	13554.3	13709.4	No. of Street,	13863.5	14016.8	14169.1	14320.6	14471.2	8 76 4	14620.9	14769.8	14917.8	15065.0	15211.3	The state of the s	15356.8	15501.5	15645.5	15788.6	120010
Barometer	in Eng. Inch.		16.0	1.91	16.2	16.3	16.4	1	16.5	9.91	16.7	16.8	16.9		17.0	17.1	17.2	17.3	17.4		17.5	9.71	17.7	17.8	17.9		18.0	18.1	18.2	18.3	101

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4			В	AR	OM.	ET	RIC	CAL	M	EA:	SUI	REI	IEI	NT	0	F 1	HE	IGH	TS.		GU	YO	T.						100
Barometer	Eng. Inch.		18.5	18.6	18.7	18.8	18.9	19.0	19.1	19.2	19.3	19.4		19.5	19.6	19.7	8.61	19.9	20.0	20.1	20.2	20.3	20.4	6	c.02	50.6	20.7	20.8	20.9
Thousandths	Inch.		,	reet.	1 1.4	2 2.7	3 4.1	70.4	179	6 8.1	7 9.5	8 10.9		9 12.2				1 1.3	2 2.6	3 3.9	4 5.1	5 6.4	7.7		_	8 10.3	9 11.6		
T	60.	Eng. Feet.	16199.5	16339.6	16479.0	16617.8	16755.7	16809.8		-	-	-		17568.4	17701.4	17833.7	17965.4	18096.4	18226.8	18356.6	18485.7	18614.1	18741.9	KI P		18995.7	19121.7	19247.0	19371.8
	80.	Eng. Feet.	16185.4	16325.7	16465.1	16603.9	16741.9	16879.9	17015.8	17151.6	17286.8	17421.2		17555.0	1.889.1	17820.5	17952.2	18083.4	18213.8	18343.6	18472.8	18601.3	18729.1	, 04000	18856.4	18983.1	19109.1	19234.5	19359.3
	20.	Eng. Feet.	16171.3	16311.7	16451.2	16590.0	16728.1	16865.5	17002.1	17138.1	17273.3	17407.8		17541.7	17674.8	17807.3	17939.1	18070.3	18200.8	18330.7	18459.9	18588.5	18716.4		18843.7	18970.5	19096.5	19222.0	19346.9
	90°	Eng. Feet.	16157.3	16297.7	16437.2	16576.2	16714.4	16851.8	16988.5	17124.5	17259.8	17394.4		17528.3	17661.5	17794.1	17926.0	18057.2	18187.8	18317.7	18447.0	18575.7	18703.6	0.000	18831.0	18957.8	19083.9	19209.5	19334.4
of an Inch.	.05	Eng. Feet.	16143.2	16283.7	16423.3	16562.3	9.00291	16838 1	16974.9	17110.9	17246.3	17380.9		17515.0	17648.2	17780.8	17912.8	18044.1	18174.8	18304.8	18434.1	18562.8	18690.9	0,000	18818.3	18945.2	19071.4	19196.9	19322.0
Hundredths of an Inch.	.04	Eng. Feet.	16129.1	16269.7	16409.4	16548.5	16686.8	16994.9	16961.2	17097.4	17232.8	17367.5		17501.6	17635.0	17767.6	17899.6	18031.0	18161.7	18291.8	18421.2	18550.0	18678.1		18805.6	18932.5	19058.8	19184.4	19309.5
	.03	Eng. Feet.	16115.0	16255.6	16395.4	16534.6	16673.0	16910 6	16947.5	17083.8	17219.3	17354.1		17488.2	17621.7	17754.4	17886.5	18017.9	18148.7	18278.8	18408.3	18537.1	18665.3		18792.9	18919.9	19046.2	19171.9	1,79997
	.03	Eng. Feet.	16100.9	16241.6	16381.5	16520.7	16659.2	0 20421	16933.9	17070.9	17205.8	17340.6		17474.8	17608.3	17741.1	17873.3	18004.8	18135.6	18265.8	18395.4	18524.3	18652.5	100	18780.1	18907.2	19033.6	19159.3	19984.5
	10.	Eng. Feet.	16086.8	16227.6	16367.5	16506.8	16645.4	0 0000	16090 9	1.026.6	17192.2	17327.2		17461.4	17595.0	17727.9	17860.1	9.16671	18122.6	18252.8	18382.5	18511.4	18639.7		18767.4	18894.5	19021.0	19146.8	19979.0
	00.	Eno Foot	16072.6	16213.5	16353.5	16492.9	16631.5	. 00.00	16006 5	17019 0	17178.7	17313.7		17448.0	17581.7	17714.6	17846.9	17978.5	18109.5	18239.8	18369.5	18498.5	18626.9		18754.6	18881.8	19008.3	19134.2	19959.5
Barometer	in Eng. Inch.		18.5	18.6	18.7	18.8	18.9	00.	10.1	10.01	19.3	19.4		19.5	9.61	19.7	19.8	19.9	0.09	20.1	20.2	20.3	20.4		20.5	20.6	20.7	20.8	20.9

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Barometer	Eng. Inch.	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	23.0	23.1	23.2	23.3	23.4
Thousandths	Inch.	Feet.	1.2	2.4	3.6	4.8	0.9	7.2	8.4	9.7	10.9				1.1	2.3	3.4	4.6	5.7	8.9	8.0	9.1	10.2			
Thous	E E		-	2	က	4	70	9	1	00	6		18	NOW THE	1	67	භ	4	20	9	1	00	6			
	60.	Eng. Feet. 19496.0	9.61961	19742.6	19865.0	19986.9	20108.2	20228.9	20349.1	20468.7	20587.8	20706.3	20824.4	20941.9	21058-8	21175.3	21291.1	21406.5	21521.4	21635.8	21749.7	21863.0	21976.0	22088.4	22200.4	22311.8
	80.	Eng. Feet.	19607.3	19730.3	19852.8	19974.7	20096.1	20216.9	20337.1	20456.8	20575.9	20694.5	20812.6	20930.1	21047.1	21163.6	21279.5	21395.0	21509.9	21624.4	21738.3	21851.7	21964.7	22077.2	22189.2	22300.7
	20.	Eng. Feet.	19594.9	19718.0	9.04861	19962.6	20083.9	20204.8	20325.1	20444.8	20564.0	20682.7	20801.8	20918.4	21035.4	21152.0	21268.0	21383.5	21498.5	21613.0	21727.0	21840.4	21953.4	22066.0	22178.0	22289.6
	90.	Eng. Feet. 19458.S	19582.6	19705.8	19828.4	19950.4	20071.8	20192.7	20313.1	20432.9	20552.1	20670.8	20789.0	20906.7	21023.8	21140.4	21256.4	21371.9	21487.0	21601.6	21715.6	21829.1	21942.1	22054.7	22166.8	22278.4
Hundredths of an Inch.	.05	Eng. Feet.	19570.2	19693.5	19816.1	19938.2	20059.7	20180.7	20301.1	20420.9	20540.2	20659.0	20777.2	20894.9	21012.1	21128.7	21244.8	21360.4	21475.5	21590.1	21704.2	21817.7	21930.8	22043.5	22155.6	22267.3
Hundredth	.04	Eng. Feet.	19557.9	19681.2	19803.9	19926.0	20047.6	20168.6	20289.1	20409.0	20528.3	20647.1	20765.4	20883.2	21000.4	21117.1	21233.2	21348.9	21464.0	21578.7	21692.8	21806.4	21919.6	22032.3	22144.5	22256.2
	.03	Eng. Feet.	19545.5	19668.9	19791.6	19913.9	20035.5	20156.5	20277.0	20397.0	20516.4	90635.3	20753.6	20871.4	20988.7	21105.4	91921.6	21337.3	21452.5	21567.2	21681.4	21795.1	21908.3	22021.0	22133.3	22245.0
	.02	Eng. Feet.	19533.1	19656.6	19779.4	1.10961	20023.3	20144.4	20265.0	20385.0	20504.5	90693.4	20741.8	20859.7	20977.0	21093.8	21210.1	21325.8	21441.1	21555.8	21670.1	21783.7	21897.0	22009.8	22122.1	22233.9
	10.	Eng. Feet.	19520.8	19644.3	19767.1	19889.5	20011.2	20132.3	20253.0	20373.0	20192.6	90611.5	90739.0	20847.9	20965.3	21082.1	21198.5	21314.2	21429.6	21544.3	21658.7	21772.4	21885.6	21998.5	22110.8	22222.7
	00.	Eng. Feet.	19508.4	19632.0	19754.9	19877.3	1.99991	20120.3	20241.0	20361.1	20480.7	90599.7	20718.2	20836.2	20953.6	21070.5	21186.9	21302.6	21418.1	21532.9	21647.3	21761.0	21874.3	21987.2	22099.6	22211.5
Barometer	in Eng. Inch.	91.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	99.0	99.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	23.0	23.1	23.2	23.3	23.4

Barometer	Eng. Inch.	23.5	23.6	23.7	23.8	23.9	24.0	24.1	24.2	24.3	24.4	3	C-+7	24.6	24.7	24.8	24.9	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9
Thousandths	Inch.			Feet	1.1	2.2	3.2	4.3	5.4	6.5	7.5	90	0.0	9.7			1.0	2.1	3.1	4.1	5.1	6.2	7.2	8.2	9.2		
Tho					-	67	ေ	4	20	9	-	0	0	0			-	es.	က	4	70	9	1-	00	6		
	60°	Eng. Feet 22422.8	22533.3	22643.4	22752.9	22862.0	22970.8	23079.1	23186.8	23294.2	23401.0	00204	4.10062	23613.5	23719.1	23824.3	23929.1	24033.4	24137.2	24240.8	24343.9	24446.6	24548.9	24650.7	24752.3	24853.4	24954.1
	80.	Eng Feet 22411.7	22522.3	22632.4	22742.0	22851.2	22960.0	23068.3	23176.1	23283.4	23390.3	094060	23490.5	23602.9	23708.6	23813.8	23918.6	24023.0	24126.9	24230.4	24333.6	24436.3	24538.7	24640.6	24742.1	24843.3	24944.1
	.07	Eng Feet. 22400.6	22511.2	22621.4	22731.0	22840.3	22949.1	23057.5	23165.3	23272.7	23379.7	0 00100	23450.2	23592.3	23698.0	23803.3	23908.2	24012.5	24116.5	24220.1	24323.3	24426.1	21528.4	24630.4	24732.0	24833.2	21931.0
	90°	Eng Feet. 22389.5	22500.2	22610.4	22720.1	22829.4	22938.2	23046.6	23154.5	23262.0	23369.0	0 22100	23475.0	23581.7	23687.5	23792.8	23897.7	24002.1	24106.1	24209.7	24313.0	24115.8	24518.2	24620.2	24721.8	24823.1	24924.0
of an Inch.	.05	Eng. Feet. 22378.4	22489.1	22599.4	22709.1	22818.4	22927.4	23035.8	23143.8	23251.3	23358.3	0 10100	23404.9	23571.1	23676.9	23782.3	23887.2	23991.7	24095.7	24199.4	24302.7	24405.5	24508.0	24610.0	24711.7	24813.0	24913.9
Hundredths of an Inch.	.04	Eng. Feet. 22367.4	22478.1	22588.4	22698.2	22807.5	22916.5	23025.0	23133.0	23240.5	23347.6	0072700	23404.3	23560.5	23666.3	23771.7	23876.7	23981.3	24085.4	24189.0	24292.4	24395.3	24497.8	24599.9	24701.5	24802.9	24903.8
	.03	Eng. Feet.	22467.0	22577.4	22687.2	22796.6	22905.6	23014.2	23122.2	23229.8	23337.0		23443.7	23549.9	23655.8	23761.2	23866.2	93970.8	24075.0	24178.7	24282.1	24385.0	24487.5	24589.7	24691.4	24792.8	24893.7
	.03	Eng. Feet.	22456.0	22566.4	22676.3	22785.7	22894.7	23003.3	23111.4	23219.1	23326.3	0 00.00	23433.0	23539.3	23645.2	23750.7	23855.7	93960.4	24064.6	24168.3	24271.8	24374.7	24477.3	24579.5	24681.2	24782.6	24883.7
	10.	Eng. Feet.	22444.9	22555.4	22665.3	22774.8	22883.9	22992.5	23100.7	23208.3	23315.6	00000	23422.3	23528.7	23634.6	23740.2	23845.3	93049.9	24054.2	24158.0	24261.4	24364.5	24467.0	24569.3	24671.1	24772.5	24873.6
	00.	Eng. Feet.	22433.8	22544.3	22654.3	22763.8	22873.0	22981.7	23089.9	23197.6	23304.9		23411.7	23518.1	23624.1	23729.7	23834.8	93030.5	24043.8	24147.6	24251.1	24354.2	24456.8	24559.1	24660.9	24762.4	24863.5
Barometer	in Eng. Inch.	93.5	23.6	23.7	23.8	23.9	24.0	24.1	24.2	24.3	24.4		24.5	24.6	24.7	24.8	24.9	95.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9

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Barometer	Eng. Inch.	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	56.9	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	28.0	28.1	28.2	28.3	28.4
Thousandths of an	T	Feet.		1.0	2.0	2.9	3.9	4.9	5.9	6.9	7.8	00		100		6.0	1.9	2.8	3.7	4.7	5.6	6.5	7.5	8.4		
Thouse	Inc			-	67	ත	4	10	9	7	00	6		BM9	1	H	64	က	4	10	9	1	00	6		
	60.	Eng. Feet. 25054.5	25154.4	25254.0	25353.1	25451.9	25550.4	25648.5	25746.2	25843.5	25940.5	26037.2	26133.4	26229.3	26324.9	26420.1	26514.9	26609.5	26703.7	26797.6	26891.0	26984.3	27077.1	27169.6	27261.8	27353.7
	80.	Eng. Feet. 25044.5	25144.4	25244.0	25343.2	25442.1	25540.5	25638.7	25736.4	25833.8	25930.8	26027.5	26123.8	26219.8	26315.3	26410.6	26505.5	26600.0	26694.3	26788.2	26881.7	26975.0	27067.8	27160.4	27252.6	27344.5
	20.	Eng. Feet. 25034.4	25134.5	25234.1	25333.3	25432.2	25530.7	25628.9	25726.7	25824.0	25921.1	26017.9	26114.2	26210.2	26305.8	26401.1	26496.0	26590.6	26684.9	26778.8	26872.3	26965.6	27058.6	27151.2	27243.4	27335.3
	90.	Eng. Feet. 25024.4	25124.5	25224.1	25323.4	25422.3	25520.9	25619.1	25716.9	25814.3	25911.4	26008.2	26104.6	26200.6	26296.3	26391.6	26486.5	26581.2	26675.5	26769.5	26863.0	26956.3	27049.3	27141.9	27234.2	27326.2
Hundredths of an Inch.	.05	Eng. Feet. 25014.4	25114.5	25214.2	25313.5	25412.4	25511.0	25609.3	25707.1	25804.6	25901.7	25998.6	26095.0	26191.0	26286.7	26382.1	26477.1	26571.7	26666.1	26760.1	26853.7	26947.0	27040.0	27132.7	27225.0	27317.0
Hundredth	.04	Eng. Feet. 25004.4	25104.5	25204.2	25303.6	25402.6	25501.2	25599.5	25697.4	25794.8	25892.0	25988.9	26085.3	26181.4	26277.2	26372.5	26467.6	26562.3	26656.7	26750.7	26844.3	26937.7	27030.7	27123.4	27215.7	27307.8
	.03	Eng. Feet. 24994.3	25094.5	25194.3	25293.7	25392.7	25491.4	25589.7	25687.6	25785.1	25882.3	25979.2	26075.7	26171.8	26267.6	26363.0	26458.1	26552.8	26647.2	26741.3	26835.0	26928.4	27021.5	27114.2	27206.5	27298.6
	.03	Eng. Feet. 24984.3	25084.5	25184.3	25283.8	25382.8	25481.5	25579.8	25677.8	25775.4	25872.6	25969.6	26066.1	26162.2	26258.0	26353.5	26118.6	26543.3	26637.8	26731.9	26825.6	26919.0	27012.2	27104.9	27197.3	27289.4
	10.	Eng. Feet. 24974.2	25074.5	25174.4	25273.8	25372.9	25471.7	25570.0	25668.1	25765.6	25862.9	25959.9	26056.5	26152.6	26248.5	26344.0	26439.1	26533.9	26628.4	26722.5	26816.3	26909.7	27002.9	27095.6	27188.1	27280.2
	00.	Eng. Feet. 24964.2	25064.5	25164.4	25263.9	25363.0	25461.8	25560.2	25658.3	25755.9	25853.2	25950.2	26046.8	26143.0	26238.9	26334.4	26429.6	26524.4	26618.9	26713.1	26806.9	26900.4	26993.6	27086.4	27178.9	27271.0
Barometer	Eng. Inch.	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	28.0	28.1	28.2	28.3	28.4

Thousandths Barometer of an in	. Eng. Inch.	000	Feet. 80.0	28.6		1.8 28.8	28.9	3.6 29.0		1		7.2 29.4	8.1 29.5	29.6	29.7	29.8	8.6 29.9	1.7 30.0	2.6 30.1	3.4 30.2	4.3 30.3	5.2 30.4	6.0 30.5		7.7 30.7	30.8	30.9
Chousan	Inch		Fe			7 6					7 6		6				3		60		Y	9		8			
	60.	Eng. Feet.	2.044.12	6.05612	4.12012	97077.9	27808.3	27898.1	27987.7	28077.1	28166.2	28254.9	28343.4	28431.5	28519.3	28606.9	28694.2	28781.1	28867.9	28954.3	29040.3	29126.2	29211.8	29297.0	29382.0	29466.8	90881 9
	80.	Eng. Feet.	1.004.12	6.12612	27010.3	27708.9	27799.2	27889.1	27978.8	28068.2	28157.3	28246.1	28334.5	28422.7	28510.6	28598.2	28685.5	28772.5	28859.2	28945.7	29031.7	29117.6	29203.2	29288.5	29373.5	29458.3	0 07 700
	.07	Eng. Feet.	0.12412	2.81672	27009.3	27699.9	27790.2	27880.2	27969.8	28059.2	28148.4	28237.2	28325.7	28413.9	28501.8	28589.4	28676.8	28763.8	28850.5	28937.0	29023.2	29109.0	7.10109	29280.0	29365.1	29449.8	00000
	90.	Eng. Feet.	0.11417	27509.1	2,000.2	27690.8	2.181.2	27871.2	27960.9	28050.3	28139.5	28228.4	28316.9	28405.1	28493.0	28580.7	28668.1	28755.1	28841.9	28928.4	29014.6	29100.4	1.98186.1	29271.5	29356.6	29441.4	0 10100
Hundredths of an Inch.	.05	Eng. Feet.	27405.1	975011	27091.1	27681.8	27772.2	27862.2	27951.9	28041.4	28130.6	28219.5	28308.0	28396.3	28484.2	28571.9	28659.3	28746.4	28833.2	28919.8	29006.0	29091.8	9,77166	29262.9	29348.1	29432.9	
Hundredth	.04	Eng. Feet.	27399.0	27490.9	27582.0	27672.7	27763.1	27853.2	27943.0	28032.4	28121.7	28210.6	28299.2	28387.5	28475.4	28563.2	28650.6	28737.7	28824.5	28911.1	28997.4	29083.3	0 09166	29254.4	29339.6	29424.4	0 00200
	.03	Eng. Feet.	27390.4	27481.8	27572.9	27663.7	27754.1	27844.2	27934.0	28023.5	28112.8	28201.7	28290.3	28378.7	28466.7	28554.4	28641.9	28729.0	28815.9	28902.5	28988.8	29074.7	99160.4	29215.9	29331.1	29416.0	0 00100
	.03	Eng. Feet.	27381.2	27472.6	27563.8	27654.6	27745.1	27835.2	27925.0	28014.6	28103.8	28192.9	28281.5	28369.8	28457.9	28545.6	28633.2	28720.3	28807.2	28893.8	28980.1	29066.1	90151 9	29237.4	29322.5	29407.5	- 00:00
	10.	Eng. Feet.	27372.0	27463.5	27554.7	27645.5	27736.0	27826.2	27916.1	28005.6	28094.9	28184.0	28272.6	28361.0	28449.1	28536.9	28624.4	28711.6	28798.5	28885.2	28971.5	29057.5	90143 3	29228.9	29314.0	29399.0	- 00,00
	.00	Eng. Feet.	27362.9	27454.4	27545.6	27636.5	27727.0	27817.2	27907.1	27996.7	28086.0	28175.1	28263.8	28352.2	28440.3	28528.1	28615.7	28702.9	28789.8	28876.5	28962.9	29048.9	90124 7	29220.3	29305.5	29390.5	000000
Barometer	Eng. Inch.		28.5	28.6	28.7	28.8	28.9	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	30.0	30.1	30.2	30.3	30.4	20 G	30.6	30.7	30.8	000

II. CORRECTION FOR 7-7', OR DIFFERENCE OF THE TEMPERATURE OF THE BAROMETERS AT THE TWO STATIONS.

This Correction is negative when the attached Thermometer at the Upper Station is lowest; positive, when the attached Thermometer at the Upper Station is highest.

Te													-								_	_		
	Correction in Eng.	0 0 0 0	210.7	915.5	216.7	217.9	20,000	219.0	220.2	221.4	222.5	223.7		224.9	226.1	227.2	228.4	229.6		230.7	931.9	933.1	234.3	235.4
	r — r' Fahren- heit.	0	91.0	0.00	99.5	93.0		93.5	0.16	94.5	95.0	95.5		96.0	96.5	97.0	97.5	98.0		98.5	0.00	900 8	100.0	100.5
	Correction in Eng.	1001	190.9	199.1	193.3	194.4		195.6	196.8	197.9	199.1	200.3		201.5	202.6	203.8	205.0	206.1		207.3	208.5	2 606	210.8	212.0
	r — r' Fabren- beit.	010	81.5	82.0	82.5	83.0		83.5	84.0	84.5	85.0	85.5		86.0	86.5	87.0	87.5	88.0		88.5	0.68	20.08	90.0	90.5
	Correction in Eng.	166.2	167.5	168.7	169.8	171.0	1.5	172.2	173.4	174.5	175.7	176.9		178.0	179.2	180.4	181.6	182.7	No. of Street, or other Persons and Street, o	183.9	185.1	186.2	187.4	188.6
	τ — τ' Fahren- beit.	001	71.5	72.0	72.5	73.0		73.5	74.0	74.5	75.0	75.5		0.94	2.94	0.77	77.5	78.0		78.5	79.0	79.5	80.0	80.5
	Correc- tion in Eng. Feet.	149.9	144.1	145.2	146.4	147.6	1000	148.8	149.9	151.1	152.3	153.4		154.6	155.8	157.0	158.1	159.3	100	160.5	161.6	162.8	164.0	165.2
	τ — τ' Fahren- heit.	019	61.5	62.0	62.5	63.0		63.5	64.0	64.5	65.0	65.5		0.99	66.5	0.79	67.5	68.0		68.5	0.69	69.5	0.07	70.5
	Correction in Eng.	119.5	120.6	121.8	123.0	124.2	The same	125.3	126.5	127.7	128.8	130.0		131.2	132.4	133.5	134.7	135.9	Same and	187.0	138.2	139.4	140.6	141.7
	r — r' Fahren- heit.	51.0	51.5	52.0	52.5	53.0	Series Series	53.5	54.0	54.5	92.0	55.5		0.99	56.5	67.0	57.5	58.0	Service Servic	58.5	59.0	59.5	0.09	60.5
	Correction in Eng. Feet.	0.96	97.2	98.4	9.66	1001		6.101	103.1	104.2	105.4	9.901		107.8	108.9	110.1	111.3	112.4	ACCOUNT OF THE	113.6	114.8	0.911	117.1	118.3
	τ — τ' Fahren- heit.	41.0	41.5	45.0	42.5	43.0	25000	43.5	44.0	44.5	45.0	45.5		46.0	46.5	47.0	47.5	48.0	200	48.5	49.0	49.5	20.0	-
	Correction in Eng.	72.6	73.8	75.0	76.1	77.3	10.85	78.5	9.64	80.8	82.0	83.2		84.3	85.5	86.7	87.8	89.0	7 5 6	90.2	91.4	92.5	93.7	94.9
	T — T' Fahren- heit.	31.0	31.5	32.0	32.5	33.0	10000	33.5	34.6	34.5	35.0	35.5		36.0	36.5	37.0	37.5	38.0		38.5	39.0	39.5	40.0	40.5
	Correction in Eng.	49.2	50.4	51.5	52.7	53.9		55.1	56.5	57.4	58.6	59.7		6.09	62.1	63.2	64.4	9.29	Sec. 19	8.99	6.79	69.1	70.3	71.4
	r — r' Fahren- heit.	21.0.	21.5	22.0	22.5	23.0		23.5	24.0	24.5	25.0	25.5		26.0	26.5	27.0	27.5	28.0	A COLUMN	28.5	29.0	29.5	30.0	30.5
	Correction in Eng. Feet.	25.8	26.9	28.1	29.3	30.5		31.6	32.8	34.0	35.1	36.3		37.5	38.7	39.8	41.0	42.2		43.3	44.5	45.7	46.9	48.0
	Fahren- heit.	0.11	11.5	12.0	12.5	13.0		13.5	14.0	14.5	15.0	15.5		16.0	16.5	17.0	17.5	18.0	- 100 km	18.5	19.0	19.5	20.0	20.5
	Correction in Eng. Feet.	2.3	3.5	4.7	6.9	7.0		8.2	9.4	10.5	11.7	12.9		14.1	15.2	16.4	17.6	18.7	1	19.9	21.1	22.3	23.4	24.6
	Fahren- heit.	1.0	1.5	2.0	2.5	3.0	-	3.5	4.0	4.5	0.9	5.5		0.9	6.5	7.0	7.5	8.0		8.5	0.6	9.5	10.0	10.5
100		7,44	1	100		100	11	-					-					-		-	-	-	==	

III. CARRESTON FOR THE PROPERTY OF LEAST

Approxi- mate	ence of Level.	Eng. Feet 1000 2000 3000 4000 5000 6000 6000 10000 10000 11000 115000 115000 115000 115000 115000 115000 115000 115000 115000 115000 200000 20000 20000 20000 20000 20000 20000 20000 20000 20000 2000	24000
	450	Pect.	00
	440	Feet. 0.02 0.03 0.04 0.05 0.05 0.09 0.09 1.15 1.15 1.15 1.15 1.15 1.15 1.15 1.1	2.2
	480 4		6.5
	400	Feet. 0.55 (	11.3
	380		15.1
#5 A	360 3		19.3
	-		-
	340		
	8 69 8 80		27.
	000	1.3 2.6 5.2 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5	32.5
	620	1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	34.9
	260	1.66 1.66 1.66 1.66 1.66 1.66 1.66 1.66	38.4
Latitude.	240	Feet. 1.7. 2.5. 2.5. 2.5. 2.5. 2.5. 2.5. 2.5. 2	41.8
La	680		44.9
	200		47.8
	300		50.5
	16° ]		55.1
	140		57.4
	780		59.4
	100 1		58.6
	800		62.5
	6° 8	Feet. 110.2 1	61.0 6
	• <b>86</b> °	m	2 61.8 8 64.4
	ê 80 80 80 80 80 80 80 80 80 80 80 80 80 8	2.6 5 15.	64.8
	000		65.0
Approxi- mate	Differ- ence of Level.	Eng. Feet. 1000 2000 3000 4000 6000 7000 8000 9000 11000 12000 14000 15000 17000 17000 18000 19000 20000 220000 23000	25000

		September 1							_				,											_		_	
NTH		820	Feet.	158.8	150.6	146.9	143.3	139.8	136.5	133.5	130.5	127.7	124.9	122.3	119.8	117.4	115.1	112.8	110.8	108.7	106.7	104.8	103.0	101.2	99.5	97.8	1.96
NE TE		08	Feet.	157.2	149.1	145.4	141.8	138.4	135.1	132.2	129.2	126.4	123.7	121.1	118.6	116.3	113.9	1111.7	109.7	9.701	105.6	103.8	101.9	100.2	98.5	8.96	95.2
TO OT	80	120	Feet.	155.7	147.6	143.9	140.4	137.0	133.8	130.8	127.9	125.1	122.5	6.611	117.3	112.1	112.8	9.011	9.801	9,901	104.6	102.8	6.001	8.66	97.5	95.9	94.2
NDING ETER.	neit, bein	200	1	154.0		142.5	139.0	135.7	132.4	129.5	126.6	123.8	121.2	9.811		113.9	-	109.5	107.5	105.5	103.5	101.7	6.66	98.2	96.5	6.46	93.3
OCLUMN OF AIR, CORRESPONDING TO ONE TENTH OF AN INCH IN THE BAROMETER.	Temperature of the Air, Fahrenheit, being	<b>65</b> °		152.5		141.0 1	137.6	134.3	131.1	128.5	125.3	122.6	120.0	117.4		112.8 1		108.4	106.4	104.4	102.5 1	100.7	6.86	97.2	95.5	93.9	92.3
t, cor	the Air,	009		1 6 0 1		139.6	136.1 1	132.9 1	129.7	126.8 1	124.0 1	121.3 1	118.7 1	116.2 1	113.8 1	111.6 1		1	105.3 1	103.3 1	101.4	9.66	6.76	96.2	94.5	92.9	91.4
	ture of	55° 6		149.3 15		138.1 13	134.7 13	131.5 13	128.4 15	125.5 12	122.7 12	120.0 12	117.5	115.0 11		110.4 11		106.1		102.3 10	100.3	98.6	6.96	95.1 6	93.6	92.0	90.4
INCH	mpera											1										A.C.					
COLUI	Te	200	Feet.	147.7		136.6	133.3	130.1	127.0	124.2	121.4	118.8	116.2	113.8		109.3		105.0	103.1	101.2	99.3	97.5	95.8	94.1	92.6	91.0	89.5
OF A COLUMN OF OF AN INCH		450	Feet.	146.1	138.6	135.2	131.9	128.7	125.7	122.9	120.1	117.5	115.0	112.6	110.3	108.1	105.9	103.9	102.0	1001	98.2	96.5	94.8	93.1	91.6	0.06	88.5
Неіснт		400	Feet.	144.6	137.1	133.7	130.5	127.3	124.3	121.5	118.8	116.2	113.7	111.3	100.1	106.9	104.8	102.7	100.9	0.66	97.2	95.4	93.8	92.1	9.06	89.1	87.6
VI. Hı	Barometer Reading	Inches.	1	18.5	19.5	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.5	25.0	25.5	26.0	26.5	27.0	27.5	28.0	28.5	29.0	29.5	30.0	30.5
тнв		34.00	43 6	N 0	2 10	7	8.0	1.0	1.2	1.3	1.5	1.7	1.8	2.0	2.2	2.3	2.5	7	00	0	3.2	က	10	-	00	0	=
	at	65	Feet.	0.0	0.5	0.7	Y					M.	1	-				2.7		3.0		3.3	3.5	3.7	80.	4.0	4.1
HEIGHT OF Positive.	I Inches	56	Feet.	4.0	1.1	1.4	1.8	2.1	2.5	2.8	3.2	3.5	3.9	4.2	4.6	4.9		5.6	6.0	6.3	6.7	7.0	7.4	7.7	8.1	8.4	8.8
1	English on.	24	Feet.	9.0	1.7	2.2	2.8	60	3.9	4.4	5.0	5.5	6.1	9.9	7.2	7.7	8.3	8.8	9.4	6.6	10.5	11.0	11.6	12.1	12.7	13.2	13.8
F. N.	neter, în rer Stati	22	Feet.	ى ئى س	2.3	3.1	80.00	4.6	5.4	6.2	6.9	7.7	8.5	9.5	10.0	10.8	11.5	12.3	13.1	13.8	14.6	15.4	1.91	16.9	17.7	18.5	19.2
CORRECTION FOR THE LOWER STATION.	Height of the Barometer, in English Inches, at Lower Station.	50	Feet.	0.0	0.0	4.0	0.9	0.9	7.1	8.1	9.1	10.1	11.11	12.1	13.1	14.1	12.1	1.91	17.1	18.1	19.5	20.2	21.2	22.2	23.2	24.2	25.2
RRECT	ight of t	<b>20</b>	Feet.	ا ا ا	9 69	5.1	6.4	7.6	8.9	10.2	11.4	12.7	14.0	15.3	16.5	17.8	1.61	20.3	21.6	22.9	24.1	25.4	26.7	28.0	29.5	30.5	31.8
V. Co		91	Feet.	9.1	4.7	6.3	7.8	9.4	11.0	12.5	14.1	15.7	17.2	18.8	20.4	21.9	23.5	25.1	26.6	28.2	8.62	31.3	82.9	34.5	36.0	37.6	39.1
	1	+200		6. 0 6. 0	9.3	12.2	15.2	18.3	21.5	24.7	28.1	31.5	35.1	38.7	42.5	46.3	50.3	54.3	58.4	62.6	67.0	71.4	15.9	80.5	85.2	0.06	94.9
Correction	Decrease of Gravity on a Vertical.  Positive.	2+ 0	1 1	,	7.9	10.8	13.7 1	16.7	19.9 2	23.1 2	26.4 2	29.8 3	33.3 3	36.9 3	40.6 4	44.4 4	48.3 5	52.3 5	56.4 5	60.5 6	64.8 6	69.2 7	73.6 7	78.2 8	82.9 8	87.6	92.5 9
	Approxi- mate Dif-		-	5983	3000	Terror C	5000	0009	7000	8000 2	-							-	-			- 11			-		
IV	App	ference of Level	Eng Feet.	10	30 80	40	200	09	70	80	06	10000	11000	12000	13000	14000	15000	16000	17000	18000	19000	20000	21000	22000	23000	24000	25000

## III.

#### TABLE

FOR

COMPUTING THE DIFFERENCE IN THE HEIGHTS OF TWO PLACES BY MEANS OF THE BAROMETER.

By PROF. ELIAS LOOMIS.

This table was computed from the formula of Laplace, modified in accordance with the results of more recent determinations.

Suppose that we have observed

At the lower station.

{ H, the height of the barometer, T, the temperature of the barometer, t, the temperature of the air, the height of the barometer, T', the temperature of the barometer, t', the temperature of the air.

Represent by s the height of the lower station above the level of the sea, by L the lantude of the place, and by h the observed height h' reduced to the temperature T. The difference of level x between the two stations is given by the formula,

$$x = 60158. \ 6 \ \mathrm{ft.} imes \log. rac{\mathrm{H}}{\hbar} imes \left\{ egin{array}{l} (1 + rac{t + t' - 64}{900}) \\ (1 + 0.00265 \ \mathrm{cos.} \ 2 \ \mathrm{L}) \\ (1 + rac{x + 52251}{20888629} + rac{s}{10444315}) \end{array} 
ight\}$$

But h represents the height h' reduced from the temperature T' to the temperature T. The expansion of mercury for 1° Fahr. is 0.0001000; that of the brass which forms the scale of the barometer is 0.0000104; the difference is 0.0000896. Hence we have h = h' {1 + 0.0000896 (T - T')}.

Therefore,

60158. 6 ft. log. 
$$\frac{H}{h} = 60158.6$$
 ft. log.  $\frac{H}{h'} = 2.3409$  ft. (T  $-$  T').

Part I. of the accompanying Table furnishes in English feet the value of the expression 60158.6 log. H for heights of the barometer from 11 to 31 inches; only they have all been diminished by the constant 27541.5 feet which does not change the difference

Part II. furnishes the correction —  $2.3409 \, (T - T')$  depending upon the difference T - T' of the temperatures of the barometers at the two stations. This cor-

rection is generally negative. It would be positive if T - T' were negative; that is, if the temperature T' of the barometer at the upper station exceeded the temperature T at the lower station.

Part III. gives the correction  $A \times 0.00265$  cos. 2 L, to be applied to the approximate altitude A, and which arises from the variation of gravity from the latitude of 45 degrees, to the latitude L of the place of observation. This correction has the same sign as cos. 2 L; that is, it is positive from the equator to 45 degrees, and negative from 45 degrees to the pole.

Part IV. gives the correction  $A \times \frac{A + 52251}{20889629}$ , which is always to be added to the approximate height A, and which is due to the diminution of gravity on the vertical.

Part V. furnishes for the approximate difference of level A the small correction  $A \times \frac{s}{10444315}$  corresponding to several values of the height s of the lower station. But in place of s there has been substituted as the argument of the table, the height H of the barometer at this station.

## Method of Computation.

Take from Part I. the two numbers corresponding to the observed barometric heights H and h'. From their difference subtract the correction 2.3409 (T — T') found in Part II. with the difference T — T' of the thermometers attached to the barometers. We thus obtain an approximate altitude a.

We then calculate the correction  $a^{\frac{t+t'-64}{900}}$  for the temperature of the air, by multiplying the nine-hundredth part of a by the sum of the temperatures t and t' diminished by 64. This correction is of the same sign as t+t'-64. We thus obtain a second approximate altitude A.

With A and the latitude of the place L, we seek in Part III. the correction  $A \times 0.00265$  cos. 2 L arising from the variation of gravity with the latitude.

For the approximate height A, Part IV. gives the correction A  $\times \frac{A + 52251}{20389629}$  arising from the diminution of gravity on a vertical. This correction is always additive.

Finally, when the height s of the lower station is considerable, the small correction  $A \times \frac{s}{10444315}$  may be found in Part V. This correction is always additive.

# Example 1.

M. Humboldt made the following observations on the mountain of Guanaxuato, in Mexico, in Latitude 21°, viz.

PARTY THE TANK OF A PARTY A	Upper station.	Lower station near the sea.
Thermometer in open air,	$t' = 70^{\circ}.3$	$t = 77^{\circ}.5$
Thermometer to barometer,	$T' = 70^{\circ}.3$	$T = 77^{\circ}.5$
Barometer,	h' = 23.660	H = 30.046

Required the difference in the height of the two stations.

50

#### OF TWO PLACES BY MEANS OF THE BAROMETER.

P . I . ( for H = 30.046 inches	27649.7
Part I. gives { for $H = 30.046$ inches for $h = 23.66$ inches	21406.9
Difference	6242.8
Part II. gives for $T - T' = 7^{\circ}.2$ ,	16.9
Approximate altitude a,	6225.9
$\frac{a}{900}(t+t'-64)=6.918\times83.8,$	+579.7
Second approximate altitude A,	6805.6
Part III. gives for $A = 6806$ , and $L = 21^{\circ}$ ,	+13.3
Part IV. gives for 6806,	+19.3
Height above the sea,	6838.2 feet.

## Example 2.

M. Gay Lussac in his celebrated balloon ascent in 1805, found his barometer to icate 12.945 English inches, the temperature being 14°.9 Fahrenheit. The baneter at Paris at the same time indicated 30.145 English inches with a temperature of 87°.44 Fahrenheit. Required the elevation of the balloon above Paris.

Port I gives ( for H = 30.145 inches,	27735.6
Part I. gives $\begin{cases} \text{for H} = 30.145 \text{ inches,} \\ \text{for } h' = 12.945 \text{ inches,} \end{cases}$	5650.4
Difference,	22085.2
Part II. gives for $T - T' = 72^{\circ}.54$ ,	-169.9
	The state of the s
Approximate altitude a,	21915.3
$\frac{a}{900}(t+t'-64)=24.35\times38.34,$	+933.6
Second approximate altitude A,	22848.9
Part III. gives for $A=22848$ , and $L=48^{\circ}$ 50'	-8.2
Part IV. gives for 22848,	+82.1
Height of balloon above Paris,	22922.8 feet.

PART I.

Argument, the observed Height of the Barometer at either Station

		Arg	ument, t	he observed	Height o	f the Bar	ometer at el	ther Stat	ion.		
Inches.	Feet.	Diff.	Inches.	Feet.	Diff.	Inches.	Feet.	Diff.	Inches.	Feet.	Diff.
11.0	1396.9	996.4	16.0	11186.3	162.8	21.0	18291.0	124.1	26.0	23971.0	100.:
11.1	1633.3	236.4	16.1	11349.1	The state of	21.1	18415.1	124.1	26.1	23971.3	99.
11.2	1867.6	234.3	16.2	11510.9	161.8	21.2	18538.7	123.0	26.2	24071.2	99.
11.3	2099.9	230.2	16.3	11671.7	159.8	21.3	18661.6	122.4	26.3	24170.7	99.
11.4	2330.1	230.2	16.4	11831.5	158.8	21.4	18784.0	121.8	26.4	24269.8	98.
11.5	2558.3	226.2	16.5	11990.3	157.9	21.5	18905.8	121.2	26.5	24368.6	98.
11:6	2784.5	224.2	16.6	12148.2	156.9	21.6	19027.0	120.7	26.6	24467.0	98.
11.7	3008.7	222.4	16.7	12305.1	155.9	21.7	19147.7	120.1	26.7	24565.1	97.
11.8	3231.1	220.5	16.8	12461.0	155.1	21.8	19267.8	119.6	26.8	24662.7	97.
11.9	3451.6	218.6	16.9	12616.1	154.1	21.9	19387.4	119.0	26.9	24760.0	97.
12.0	3670.2	216.8	17.0	12770.2	153.3	22.0	19506.4	118.5	27.0	24857.0	96.
12.1	3887.0	215.0	17.1	12923.5	152.3	22.1	19624.9	118.0	27.1	24953.6	96.
12.2	4102.0	213.3	17.2	13075.8	151.5	22.2	19742.9	117.4	27.2	25049.8	95.
12.3	5315.3	211.6	17.3	13227.3	150.6	22.3	19860.3	116.9	27.3	25145.7	95.
12.4	4526.9	209.8	17.4	13377.9	149.7	22.4	19977.2	116.4	27.4	25241.2	95.
12.5	4736.7	208.2	17.5	13527.6	148.9	22.5	20093.6	115.8	27.5	25336.4	94.
12.6	4944.9	206.5	17.6	13676.5	148.0	22.6	20209.4	115.4	27.6	25431.2	94.
12.7	5151.4	205.0	17.7	13824.5	147.2	22.7	20324.8	114.8	27.7	25525.7	94.
12.8	5356.4	203.3	17.8	13971.7	146.3	22.8	20439.6	114.4	27.8	25619.9	93.
12.9	5559.7	201.7	17.9	14118.0	145.6	22.9	20554.0	113.8	27.9	25713.7	93.
13.0	5761.4	200.2	18.0	14263.6	144.7	23.0	20667.8	113.3	28.0	25807.1	93.
13.1	5961.6	198.7	18.1	14408.3	144.0	23.1	20781.1	112.9	28.1	25900.3	92.
13.2	6160.3	197.2	18.2	14552.3	143.1	23.2	20894.0	112.4	28.2	25993.1	92.
13.4	6357.5	195.7	18.3	14695.4	142.4	23.3	21006.4	111.9	28.3	26085.6	92.
13.5	6553.2	194.3	18.4	14837.8	141.6	23.4	21118.3	111.4	28.4	26177.7	91.
13.6	6747.5	192.8	18.5	14979.4	140.9	23.5	21229.7	110.9	28.5	26269.6	91.
13.7	7131.7	191.4	18.6	15120.3 15260.3	140.0	23.6	21340.6	110.5	28.6	26361.1	91.
13.8	7321.7	190.0	18.8	15399.7	139.4	23.7	21451.1	110.0	28.7	26452.3 26543.2	90.
13.9	7510.3	188.6	18.9	15538.3	138.6	23.9	21670.6	109.5	28.9	26633.7	90.
14.0	7697.6	187.3	19.0	15676.2	137.9	24.0	21779.7	109.1	29.0	26724.0	90.
14.1	7883.6	186.0	19.1	15813.3	137.1	24.1	21888.4	108.7	29.1	26813.9	89.
14.2	8068.2	184.6	19.2	15949.8	136.5	24.2	21996.6	108.2	29.2	26903.5	89.
14.3	8251.5	183.3	19.3	16085.5	135.7	24.3	22104.3	107.7	29.3	26992.8	89.
14.4	8433.6	182.1	19.4	16220.5	135.0	24.4	22211.6	107.3	29.4	27081.9	89.
14.5	8614.4	180.8	19.5	16354-8	134.3	24.5	22318.4	106.8	29.5	27170.6	88.
14.6	8794.0	179.6	19.6	16488.5	133.7	24.6	22424.8	106.4	29.6	27259.0	88.
14.7	8972.3	178.3	19.7	16621-4	132.9	24.7	22530.8	106.0	29.7	27347.1	88.
14.8	9149.5	177.2	19.8	16753-7	132.3	24.8	22636.4	105.6	29.8	27434.9	87.
14.9	9325.5	176.0	19.9	16885.3	131.6	24.9	22741.5	105.1	29.9	27522.5	87.
15.0	9500.3	174.8	20.0	17016-3	131.0	25-0	22846.3	104.8	30.0	27609.7	87.
15.1	9673.8	173.5	20.1	17146-6	130.3	25.1	22950.6	104.3	30.1	27696.6	86.
15.2	9846.2	172.4	20.2	17276-3	129.7	25.2	23054.4	103.8	30.2	27783.3	86.
15.3	10017.5	171.3 170.2	20.3	17405-3	129.0	25.3	23157.9	103.5	30.3	27869.7	86. 86.
15.4	10187.7	169.1	20.4	17533.7	128.4	25.4	23261.0	103.1	30.4	27955.7	85.
15.5	10356.8	168.0	20.5	17661-4	127.7	25.5	23363.6	102.6	30.5	28041.5	85.
15.6	10524.8	167.0	20.6	17788-6	127.2 126.5	25.6	23465.9	102.3	30.6	28127.1	85.
15.7	10691.8	165.9	20.7	17915-1	125.9	25.7	23567.7	101.5	30.7	28212.3	85.
15.8	10857.7	164.8	20.8	18041.0	125.3	25.8	23669.2	101.3	30.8	28297.3	84.
15.9	11022.5	163.8	20.9	18166-3	124.7	25.9	23770.3	100.7	30.9	28382.0	84.
16.0	11186.3		21.0	18291.0	E9 - 7-1	26.0	23871.0		31.0	28466.4	198

PART II.

Correction due to T — T', or the Difference of the Temperatures of the Barometers at the two Stations.

This Correction is Negative when the Temperature at the Upper Station is lowest, and vice versa.

r — T'.	Correc-	T-T'.	Correc-	T — T'.	Correc-	T-T'.	Correction.	T-T'.	Correction.	T T'.	Correc-
Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.
0		0		0		0		0		0	
1	2.3	14	32.8	27	63.2	40	93.6	53	124.1	66	154.5
2	4.7	15	35.1	28	65.5	41	96.0	54	126.4	67	156.8
3	7.0	16	37.5	29	67.9	42	98.3	55	128.7	, 68	159.2
4	9.4	17	39.8	30	70.2	43	100.7	56	131.1	69	161.5
5	11.7	18	42.1	31	72.6	44	103.0	57	133.4	70	163.9
6	14.0	19	44.5	32	74.9	45	105.3	58	135.8	71	166.2
7	16.4	20	46.8	33	77.3	46	107.7	59	138.1	72	168.6
8	18.7	21	49.2	34	79.6	47	110.0	60	140.4	73	170.9
9	21.1	22	51.5	35	81.9	48	112.4	61	142.8	74	173.5
10	23.4	23	53.8	36	84.3	49	114.7	62	145.1	75	175.6
11	25.8	24	56.2	37	86.6	50	117.0	63	147.5	76	177.9
12	28.1	25	58.5	38	89.0	51	119.4	64	149.8	77	180.5
13	30.4	26	60.9	39	91.3	52	121.7	65	152.2	78	182.6
	ity fro	n due to m the La	T III. the Chang titude of 4	50 to the	9		orrection d	PAR'	Γ V. Height of	the Lower	

Mark SCHOOL STREET, ST		ity La P	from titude ositive	due to the Lat of the I from 1	the Charlet of Place of Lat. 45	ange of of 450 Observe to 450	to the ration.	PART IV. Correction for Decrease of Gravity	Corr	ection	due to	the Hestation	eight o	f the L	ower		
Chatter 201		1,5920	19.	Lati	tude.	3	(dr	on a Vertical.	He	ight of	Baron	eter a	Lower	Statio	nn.		
Commercia	App.	00	100	200	300	400	450	Always		1		1111			100 100	App.	
Total Control	Alt.	900	800	700	600	500		Positive.	16 in.	18 in.	20 in.	22 in.	24 in.	26 in.	28 in.	Alt.	-
1	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	
l	1000	2.6	2.5	2.0	1.3	0.5	0	2.5	1.6	1.3	1.0	0.8	0.6	0.4	0.2	1000	1
i	2000	5.3	5.0	4.1	2.6	0.9	0	5.2	3.1	2.5	2.0	1.5	1.1	0.7	0.3	2000	-
	3000	7.9	7.5	6.1	4.0	1.4	0	7.9	4.7	3.8	3.0	2.3	1.7	1.1	0.5	3000	-
I	4000	10.6	10.0	8.1	5.3	1.8	0	10.8	6.3	5.1	4.0	3.1	2.2	1.4	0.7	4000	1
	5000	13.2	12.4	10.1	6.6	2.3	0	13.7	7.8	6.4	5.0	3.8	2.8	1.8	0.8	5000	ı
	6000	15.9	14.9	12.2	7.9	2.8	0	16.7	9.4	7.6	6.0	4.6	3.3	2.1	1.0	6000	ı
	7000	18.5	17.4	14.2	9.3	3.2	0	19.9	11.0	8.9	7.1	5.4	3.9	2.5	1.2	7000	ı
Total Section	8000	21.2	19.9	16.2	10.6	3.7	0	23.1	12.5	10.2	8.1	6.2	4.4	2.8	1.3	8000	ı
	9000	23.8	22.4	18.3	11.9	4.1	0	26.4	14.1	11.4	9.1	6.9	5.0	3.2	1.5	9000	ı
	10000	26.5	24.9	20.3	13.2	4.6	0	29.8	15.7	12.7	10.1	7.7	5.5	3.5	1.7	10000	ı
	11000	29.1	27.4	22.3	14.6	5.1	0	33.3	17.2	14.0	11.1	8.5	6.1	3.9	1.8	11000	1
	12000	31.8	29.9	24.4	15.9	5.5	0	36.9	18.8	15.3	12.1	9.2	6.6	4.2	2.0	12000	1
	13000	34.4	32.4	26.4	17.2	6.0	0	40.6	20.4	16.5	13.1	10.0	7.2	4.6	2.2	13000	1
1	14000	37.1	34.9	28.4	18.5	6.4	0	44.4	21.9	17.8	14.1	10.8	7.7	4.9	2.3	14000	-
ì	15000	39.7	37.3	30.4	19.9	6.9	0	48.3	23.5	19.1	15.1	11.5	8.3	5.3	2.5	15000	1
	16000	42.4	39.8	32.5	21.2	7.4	0	52.3	25.1	20.3	16.1	12.3	8.8	5.6	2.7	16000	1
ı	17000	45.0	42.3	34.5	22.5	7.8	0	56.4	26.6	21.6	17.1	13.1	9.4	6.0	2.8	17000	
	18000	47.7	44.8	36.5	23.8	8.3	0	60.5	28.2	22.9	18.1	13.8	9.9	6.3	3.0	18000	
	19000	50.3	47.3	38.6	25.2	8.7	0	64.8	29.8	24.1	19.2	14.6	10.5	6.7	3.2	19000	1
į	20000	53.0	49.8	40.6	26.5	9.2	0	69.2	31.3	25.4	20.2	15.4	11.0	7.0	3.3	20000	1
	21000	55.6	52.3	42.6	27.8	9.7	0	73.6	32.9	26.7	21.2	16.1	11.6	7.4	3.5	21000	1
	22000	58.3	54.8	44.7	29.1	10.1	0	78.2	34.5	28.0	22.2	16.9	12.1	7.7	3.7	22000	-
	23000	60.9	57.3	46.7	30.5	10.6	0	82.9	36.0	29.2	23.2	17.7	12.7	8.1	3.8	23000	-
H	24000	63.6	59.8	48.7	31.8	11.0	0	87.6	37.6	30.5	24.2	18.5	13.2	8.4	4.0	24000	1
i	25000	66.2	62.2	50.7	33.1	11.5	0	92.5	39.1	31.8	25.2	19.2	13.8	8.8	4.1	25000	1

#### TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO THE LEVEL OF THE SEA, OR TO ANY OTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION MEASURED BY THE BAROMETER, BY M. C. DIPPE.

The following tables, published by M. C. Dippe, in the Astronomische Nachrichten No. 1056, November, 1856, are a modification and extension of Gauss's tables published in Schumacher's Jahrbuch, for 1836 and the following years; which are based on the formula of Laplace. In this new form they answer a double purpose. They give the means of solving a problem which often occurs in Meteorology, viz. The difference of elevation between two stations, and the temperature of the air a both, being known, to reduce the height of the barometer at one of the stations to the height it would have at the other. They are likewise adapted to the computation of heights from barometrical observations.

The formula of Laplace, which has been used, the Metres being reduced to Toises

and the Centigrade degrees to degrees of Reaumur, reads as follows:

$$h = 9407.73 \left(1 + \frac{t+t'}{400}\right) \left(1 + a\cos 2\phi\right) \left(1 + \frac{h}{r}\right) \left\{\log \frac{b}{b'} + 2\log\left(1 + \frac{h}{r}\right)\right\}.$$

Where t and t' = the temperatures of the air, in degrees of Reaumur, at the lower and upper station,

b and b' = the height of the barometer, in any scale, reduced to the freezing point, at the lower and upper station,

h = the difference of level, in toises, between the two stations,

r = the distance, in toises, of the lower station to the centre of the Earth,

 $\phi$  = the latitude of the place of observation,

a = the increase of gravity from the equator to the poles.

Making, besides, m = the modulus of the common logarithms, the formula becomes, with sufficient accuracy,

$$\log b - \log b' = h \left\{ \frac{1}{9407.73} \cdot \frac{1}{1 + \frac{t + t'}{400}} - \frac{2m}{r} \right\} \cdot \frac{1}{1 + a \cos 2\phi} \cdot \frac{1}{1 + \frac{h}{r}}.$$

Assuming r, or the radius of the Earth, at 45° latitude = 3266631 toises, and a = 0.002595, instead of 0.002845 adopted in Gauss's tables, and making

$$u = \log b - \log b',$$

$$a = \log \left(\frac{1}{9407.73} \cdot \frac{1}{1 + \frac{t+t'}{400}} - \frac{2m}{r}\right),$$

$$c = -m a \cos 2 \phi,$$

$$c' = -\frac{mh}{r},$$

then the reduction of the height of the barometer to another level is given by the formula,

#### BAROMETRICAL MEASUREMENT OF HEIGHTS.

1. 
$$\log u = \log h + a + c + c';$$

$$2. \log b = \log b' + u.$$

Table I. contains the values of a for the argument t + t'; 10 units are to be subtracted from the characteristic.

Table II. gives the values of c for the argument  $\phi$ , or the correction for the change of gravity in latitude, which is negative from  $0^{\circ}$  to  $45^{\circ}$ , positive from  $45^{\circ}$  to  $90^{\circ}$ .

Table III. furnishes the values of c' for the argument h in toises, or the correction for the decrease of gravity on the vertical. Both in Tables II. and III. the values of c and c' are given in units of the fifth decimal place.

The difference of elevation of the two stations is given by the formula,

$$1. \qquad u = \log b - \log b',$$

$$2. \log h = \log u + \Lambda + c + c',$$

in which A is the arithmetical complement of a, and the corrections c and c' receive contrary signs. For the sake of convenience, the values of A have been placed in Table II, and in Table III. the correction for A is found in another column, with the more convenient argument  $v = \log u + A$ .

If the heights of the barometers have not been reduced to the freezing point, then, B and B' being the unreduced heights of the barometers, and T and T' the temperature of the attached thermometer in degrees of Reaumur,

$$b:b'=rac{\mathrm{B}}{1+rac{\mathrm{T}}{4440}}:rac{\mathrm{B}'}{1+rac{\mathrm{T}'}{4440}},$$

and making  $\frac{m}{4440} = \beta$ ,

$$u = \log b - \log b' = (\log B - \beta T) - (\log B' - \beta T').$$

Instead of  $\beta = 0.000098$ , we can write with sufficient accuracy 0.00010.

## Use of the Tables.

These tables can be used in any latitude, and for any barometrical scale; but the indications of the barometers must be reduced to the freezing point; and the temperatures of the air must be given in degrees of Reaumur. The tables suppose the use of logarithms with 5 decimals, such as those of Lalande, and give the results in toises.

## I. For Reducing Barometrical Observations to another Level.

Given h in toises, t, t',  $\phi$ , and b or b'. To find b or b'.

In Table I. with the argument t + t', take a, In Table II. with the argument  $\phi$ , take c, In Table III. with the argument h, take c',

the last two corrections being given in units of the fifth decimal, making

$$\log h + a + c + c' - 10$$
 (whole units) =  $\log u$ .

Then we have

for a level lower by 
$$h$$
 toises,  $\log b = \log b' + u$ ; for a level higher by  $h$  toises,  $\log b' = \log b - u$ .

If h, or the difference of elevation, is given in metres, take c', which is always negative, from Table III. (for A) with the argument  $v = \log h + 9.71$ , and write

$$\log u = 9.71018 + \log h + a + c + c' - 10$$
 (whole units).

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Then again is  $\log b = \log b' + u$ .

## Example 1.

Suppose the height of the barometer, reduced to the freezing point, to be b'=295.39 Paris lines; the temperature of the air  $t'=11^{\circ}.8$  Reaumur, and the latitude  $\phi=51^{\circ}.48'$ ; the increase of heat downwards being 1° Reaumur for 100 toises. What is the height of the barometer, reduced to the freezing point, at a station lower by h=498.2 toises?

Then

 $\log b = 2.51971$ Barometer at the lower station b = 330.90 Paris lines.

## Example 2.

Suppose the reduced barometer b'=598.6 millimetres; the temperature of the air  $t'=18^{\circ}.0$  Centigrade = 14°.4 Reaumur; the difference of elevation h=2217 metres;  $\phi=3^{\circ}$ . The temperature of the air at the lower station  $t=27^{\circ}.5$  Centigrade = 22°.0 Reaumur, and  $t+t'=36^{\circ}.4$  Reaumur.

Then 
$$\log h = \begin{cases} \log 2217 = 3.34577 \\ + 9.71018 \\ \hline 3.05595 \end{cases} v = 3.06$$

$$a = 5.98750$$

$$c = -0.00112$$

$$c' = -0.00015$$

$$\log u = 9.04218 - 10$$

$$u = 0.11020$$

$$\log b' = 9.77714$$

$$\log b = 9.88734$$
Barometer at the lower station  $b = 771.5$  millimetres.

# 2. For Computing Differences of Elevation from Barometrical Observations.

Given the unreduced height of the barometer at the lower and upper station, B and B'; the temperatures of the attached thermometers, T and T'; the temperatures of the air, t and t'; and the latitude,  $\phi$ .

To find h, or the difference of elevation between the two stations.

Subtract (log B' — 10 T') from (log B — 10 T), paying due attention to the nature of the signs of T and T', and taking the numbers 10 T and 10 T' as units of the fifth decimal. Calling then (log B — 10 T) — (log B' — 10 T') = u, or if the heights of the Barometers are reduced to the freezing point, log b — log b' = u, take,

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In Table I., A with the argument t+t', and make  $v=\log u+A$ . In Table II., with the argument  $\phi$ , take c reversing the sign.

In Table III., for A, with the argument v, take c', which, in this case, is always positive; then, remembering that the values of c and c' are given in units of the fifth decimal, we have,

$$v + c + c'$$
 = log  $h$  in toises,  
 $v + c + c' + 0.28982 = \log h$  in metres,  
 $v + c + c' + 0.80584 = \log h$  in English feet.

#### Example 1.

L. station B = 329.013 Paris lines; T = 
$$+15.88$$
 R.;  $t = +15.96$  R.;  $\phi = 45.32$ . U. station B' =  $268.215$  Paris lines; T' =  $+8.40$  R.;  $t = +\frac{7.92}{23.88}$  R. 
$$t + t' = 23.88$$
 R. 
$$log B = 2.51722 - 10 \times 15.88 = 2.51563$$
 
$$log B' = 2.42848 - 10 \times 8.4 = 2.42764$$
 
$$u = 0.08799$$
 
$$log u = 8.94443$$
 
$$A = 3.99982$$
 
$$v = 2.94425$$
 
$$c = -0.00002$$
 
$$c' = +0.00012$$
 
$$log h = 2.94435$$
 
$$h = 879.74 \text{ toises.}$$

## Example 2.

L. station B = 
$$763.15$$
 millimetres; T =  $t$  =  $25.3$  Cent. =  $20.24$  R.;  $\phi$  =  $21.5$  U. station B' =  $600.95$  millimetres; T' =  $t'$  =  $21.3$  Cent. =  $17.04$  R.  $t + t' = 37.28$  R.  $t$ 

h = 1069.3 toises = 2084.0 metres = 6837.9 English feet.

I. ARGUMENT: SUM OF THE TEMPERATURES OF THE AIR IN DEGREES OF REAUMUR.

t+t'		Correction fo	r	t+t'		Correction for	
Reaumur.	а	Difference.	<b>A</b>	Reaumur.	а	Difference.	A
-60°	6.09617	7=1=-1	3.90383	-20°	6.04776		3.95224
-59	6.09489	128	3.90511	-19	6.04661	115	3.95339
-58	6.09362	127	3.90638	-18	6.04547	114	3.95453
-57	6.09235	127	3.90765	-17	6.04434	113	3.95566
-56	6.09108	127	3.90892	-16	6.04320	114	3.95680
-96	0.03103	126	0.00032	-10	0.01020	113	0.00000
-55	6.08982		3.91018	-15	6.04207		3.95793
-54	6.08856	126	3.91144	-14	6.04094	113	3.95906
-53	6.08730	126	3.91270	-13	6.03981	113	3.96019
-52	6.08605	125	3.91395	-12	6.03869	112	3.96131
-51	6.08480	125	3.91520	-11	6.03757	112	3.96243
31	0.00100	124		Transition of the state of the		112	
-50	6.08356	125	3.91644	-10	6.03645	112	3.96355
-49	6.08231		3.91769	- 9	6.03533	The second second	3.96467
-48	6.08108	123	3.91892	- 8	6.03422	. 111	3.96578
-47	6.07984	124	3.92016	-7	6.03311	111	3.96689
-46	6.07861	123	3.92139	- 6	6.03201	110	3.96799
Sales of		120				111	
-45	6.07738	122	3.92262	- 5	6.03090	110	3.96910
-44	6.07616	122	3.92384	- 4	6.02980	109	3.97020
-43	6.07494	122	3.92506	- 3	6.02871	110	3.97129
-42	6.07372	122	3.92628	- 2	6.02761	109	3.97239
-41	6.07250	121	3.92750	- 1	6.02652	109	3.97348
-40	6.07129		3.92871	0	6.02543		3.97457
-39	6.07009	120	3.92991	+ 1	6.02434	109	3.97566
-38	6.06888	121	3.93112	127 (24)	6.02326	108	3.97674
		120	THE R. P. LEWIS CO., LANSING, MICH.	2	AND THE RESERVE AS A SECOND	109	
-37	6.06768	120	3.93232	3	6.02217	108	3.97783
-36	6.06648	119	3.93352	4	6.02109	107	3.97891
-35	6.06529	berin	3.93471	5	6.02002		3.97998
-34	6.06410	119	3.93590	6	6.01895	107	3.98103
-33	6.06291	119	3.93709	7	6.01787	108	3.98213
-32	6.06173	118	3.93827	8	6.01680	107	3 98320
-31	6.06055	118	3.93945	9	6.01574	106	3.98426
	0,0000	118	0.00040	9	0.01074	106	0.00420
-30	6.05937		3.94063	10	6.01468		3.98532
-29	6.05819	118	3.94181	11	6.01362	106	3.98638
-28	6.05702	117	3.94298	12	6.01256	106	3.98744
-27	6.05585	117	3.94415	13	6.01150	106	3.98850
-26	6.05469	116	3.94531	14	6.01045	105	3.98955
14		117	and they are	1 1 E		105	
-25	6.05352	116	3.94648	15	6.00940	105	3.99060
-24	6.05236	115	3.94764	16	6.00835	105	3.99165
-23	6.05121	The second second	3.94879	17	6.00731	104	3.99269
-22	6.05005	116	3.94995	18	6.00626	105	3.99374
-21	6.04890	115	3.95110	19	6.00522	104	3.99478
-20	6.04776	114	3.95224	+20	6.00418	104	3.99582

(Continued.)

t+t'		Correction fo	r	$  _{t+t'} $	Correction for					
Reaumur.	a	Difference.	A	Reaumur.	а	Difference.	A			
+20° 21 22 23 24	6.00418 6.00315 6.00212 6.00108 6.00006	103 103 104 102 103	3.99582 3.99685 3.99788 3.99892 3.99994	+40° 41 42 43 44	5.98393 5.98294 5.98195 5.98097 5.97998	99 99 98 99 98	4.01607 4.01706 4.01805 4.01903 4.02002			
25 26 27 28 29	5.99903 5.99801 5.99699 5.99597 5.99495	102 102 102 102 104	4.00097 4.00199 4.00301 4.00403 4.00505	45 46 47 48 49	5.97900 5.97803 5.97705 5.97608 5.97511	97 98 97 97	4.02100 4.02197 4.02295 4.02392 4.02489			
30 31 32 33 34	5.99394 5.99293 5.99192 5.99091 5.98991	101 101 101 100 101	4.00606 4.00707 4.00808 4.00909 4.01009	50 51 52 53 54	5.97414 5.97317 5.97221 5.97124 5.97028	97 96 97 96 95	4.02586 4.02683 4.02779 4.02876 4.02972			
35 36 37 38 39	5.98890 5.98790 5.98691 5.98591 5.98492	100 99 100 99	4.01110 4.01210 4.01309 4.01409 4.01508	55 56 57 58 59	5.96933 5.96837 5.96742 5.96646 5.96551	96 95 96 95	4.03067 4.03163 4.03258 4.03354 4.03449			

# H. LATITUDE. — CORRECTION FOR a.

# III. DECREASE OF GRAVITY ON THE VERTICAL. — CORRECTION

		For .	A reve	erse the S	igns o	f c.	noite:				nt h, in To Negative.	oises,		arg. v, Positive.
φ	c	φ	φ	C	φ	φ	c	φ	h	c'	h	c'	v	c'
0	110	0	0	001	0	0	50.	0	700		1000	01	10	
	-113+	90	15	-98+	75	30	-56+	60	100	1 3	1600	21 23	1.8	1
1 2	113	89	16	96	74	31	53	59	200	2.44	1700		1.9	1
10000	112	88	17	93	73	32	49	58	300	4	1800	24	2.0	1
3	112	87	18	91	72	33	46	57	400	5	1900	25	2.1	2
4	112	86	19	89	71	34	42	56	500	7	2000	27	2.2	2
6.0			751	1 Audie	7.70	To the	3 certs	300	2 Terrupus	1	W 1881	HISTORY	2.3	3
5	111	85	20	86	70	35	39	55	600	8	2100	28	2.4	3
6	110	84	21	84	69	36	35	54	700	9	2200	29	2.5	4
7	109	83	22	81	68	37	31	53	800	11	2300	31	2.6	5
8	103	82	23	78	67	38	27	52	900	12	2400	32	2.7	7
9	107	81	24	75	66	39	23	51	1000	13	2500	33	2.8	8
	1000		Sept 1			A S	100		a geolite				2.9	11
10	106	80	25	72	65	. 40	20	50	1100	15	2600	35	3.0	13
11	104	79	26	69	64	41	16	49	1200	16	2700	36	3.1	17
12	103	78	27	66	63	42	12	48	1300	17	2800	37	3.2	21
13	101	77	28	63	62	43	8	47	1400	19	2900	39	3.3	27
14	100	76	29	60	61	44	4	46	1500	20	3000	40	3.4	33
					A CO	191	AT .		SURT	Edg S	DEN HE	Morning	3.5	42
15	-98+	75	30	-56+	60	45	-0+	45	1600	21	3500	47	3.6	53

#### TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO ANOTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION MEASURED BY THE BAROMETER, BY M. C. DIPPE.

In No. 1088 of the Astronomische Nachrichten, published in June, 1857, Dr. DIPPE gives the following set of Tables for reducing barometrical observations to another level, and for computing heights. These tables, being based, as the preceding ones (IV.), on the formula of Laplace, and computed with the same constants, give results nearly identical, but dispense with the use of logarithms.

#### USE OF THE TABLES.

The tables suppose the height of the barometer to be expressed in French inches or Paris lines, and the temperature in degrees of Reaumur; they give the differences of level in French toises.

The signs used have the following signification: -

At Lower Station.  $\begin{cases} B = \text{Observed Height of Barometer in Paris lines.} \\ T = \text{Attached Thermometer in degrees of Reaumur.} \\ b = \text{Barometer reduced to the freezing point.} \\ t = \text{Temperature of the air, detached Thermometer.} \end{cases}$ 

B' = Observed Height of Barometer.

 $\phi =$  Latitude of the place.

h = Difference of elevation between the two stations.

I. For Reducing Barometrical Observations to another Level.

Given, h in toises, t, t',  $\phi$ , and b or b'. To find b or b'.

Make first  $2\tau = \frac{t+t}{2}$  and  $\tau$ , and

#### BAROMETRICAL MEASUREMENT OF HEIGHTS.

In Table I., with the argument  $2\tau$ , take  $\tau'$ ; In Table III., with the arguments h and  $\tau$ , take C; In Table IV., with the arguments h and  $\phi$ , take C';

Make, further,

$$u = h + C + C'$$
 and  $\frac{u}{100} \tau'$ ;

And if b' be given, and b required,

In Table II., with the argument b, take H;

then is

$$H = H' + (u - \frac{u}{100} \tau'),$$

and the height of the barometer, in Table II., due to H, is b required.

If b be given, and b' required for a level higher by h toises, then,

In Table II., with the argument b, take H'.

Make, further,

$$H' = H - (u - \frac{u}{100} \tau'),$$

and b' is the height of the barometer in Table II., corresponding to H'.

## Example 1.

Suppose the height of the barometer reduced to the freezing point to be b'=295.39 Paris lines; the temperature of the air  $t'=11^{\circ}.8$  Reaumur; and the latitude  $b=51^{\circ}.48$ ; the increase of heat downwards being 1° Reaumur for 100 toises. What is the height of the barometer reduced to the freezing point, at a station lower by h=498.2 toises?

In this case, 
$$t'=11^{\circ}.8$$
;  $t=11^{\circ}.8+4^{\circ}.98$ ;  $t+t'=28^{\circ}.58$ ;  $2\tau=\frac{t+t}{2}=14^{\circ}.29$ ;  $\tau=7^{\circ}.15$ ;

and according to Table I.

$$\tau' = +6.67.$$

With h and  $\tau$ , in Table III., we find C = -1.4With h and  $\phi$ , in Table IV., we find C' = +0.3

We add 
$$h = 498.2$$
  
and we have  $u = 497.1$ ;  $\frac{u}{100} = 4.97$   
 $-\frac{u}{100}\tau' = -33.15$   $\frac{u}{463.95}$   $\frac{34}{463.95}$   $\frac{u}{100}\tau' = +33.15$ 

With b', in Table II., we find H' =

H = 831.81

Finally, with H, in Table II., we find b = 330.91 Paris lines, which is the required neight of the barometer at the lower station. Gauss's tables (IV.) would give b = 330.90 lines.

## Example 2.

Suppose b'=330.46 Paris lines;  $t'=-12^{\circ}.3$  Reaumur; h'=92.7 toises;  $\phi=62^{\circ}.$ 

In this case, assuming t = t',

$$2\tau = \frac{t+t'}{2} = -12^{\circ}.3; \ \tau = -6.15;$$

and according to Table I.

$$\tau' = -6.55$$
.

With h and  $\tau$ , in Table III., take C = -0.2

With h and  $\phi$ , in Table IV., take C' = + 0.1

Add h = 92.7

We have 
$$u = \frac{6.07}{92.6}$$

$$-\frac{u}{100} \tau' = + \frac{6.07}{98.67}$$

With b', in Table II., take H' = 826.22H = 924.89

$$\frac{u}{100}\tau' = -6.07$$

With H, in Table II., we find b=338.53 Paris lines. Gauss's tables (IV.) would give b=338.54 lines.

II. For Computing Differences of Elevation from Barometrical Observations.

Suppose to be given B, B', T, T', t, t',  $\phi$ ; required h.

Make first 
$$\tau = \frac{t+t'}{4}$$
 and  $T - T'$ .

Then in Table II., with the argument { B take H, B' take H',

and make

$$u = (H - H') + \frac{H - H'}{100} \tau - (T - T'),$$

in which each full degree of T - T' corresponds to a toise.

Further, in Table III., with u and  $\tau$ , take C reversing the sign;

in Table IV., with u and  $\phi$ , take C' reversing the sign;

in Table V., with T — T' and \( \tau\_1 \) take C'' with the signs of T — T'.

Then the difference of elevation required is

$$h = u + C + C' + C''.$$

If the heights of the barometer, reduced to the freezing point, or b and b', are given

then in Table II., with the argument,  $\begin{cases} b \text{ take H} \\ b' \text{ take H}' \end{cases}$ 

and make

$$u = H - H' + \frac{H - H'}{100} \tau$$
.

Further, in Table III., take C reversing the sign; in Table IV., take C' reversing the sign;

and

$$h = u + C + C'.$$

## Example 1.

Suppose to be given,

B = 333.6 Paris lines; T = 
$$+$$
 17°.0 Reaumur;  $t = +$  19°.0 R.;  $\phi = 48^\circ$ .

$$B' = 289.9$$
 Paris lines;  $T' = +16^{\circ}.3$  Reaumur;  $t' = +15^{\circ}.2$  R.

$$T - T' = 0^{\circ}.7$$
  $t + t' = +34^{\circ}.2$   
 $\tau = +8.55$ 

In Table II. with B take H = 864.9  
with B' take H' = 291.2  
H - H' = 573.7  

$$\frac{H-H'}{100} \tau = 49.06$$
  
 $\frac{H-H'}{100} \tau = 49.06$   
 $\frac{H-H'}{100} \tau = 49.06$   
 $\frac{H-H'}{100} \tau = 49.06$   
 $\frac{H-H'}{100} \tau = 49.06$ 

In Table III., with u and  $\tau$ , take C = +1.8

In Table IV., with u and  $\phi$ , take C' = -0.2In Table V., with T - T' and  $\tau$  take C'' = 0.0

Difference of elevation, or h = 623.66 to ses. Gauss's Tables give 623.64 to ses.

## Example 2.

Suppose to be given,

$$b = 342.68 \text{ Paris lines}; t = -10^{\circ}.38 \text{ Reaumur}; \phi = 65^{\circ}.$$

$$b' = 285.47$$
 Paris lines;  $t' = -14^{\circ}.94$  Reaumur;  $T - T' = 0^{\circ}$ . R.

$$t + t' = -\frac{25^{\circ}.32}{6.33}$$

In Table II. with 
$$b$$
 take  $H = 974.58$ 

" with 
$$b'$$
 take  $H' = 228.28$ 

$$H - H' = 746.30$$
 $\frac{H - H'}{100} \tau = -47.24$ 

$$\tau = \frac{-6.33}{44.78}$$

$$\frac{2.24}{22}$$

$$u = 699.06$$
  
In Table III., with  $u$  and  $\tau$ , take  $C = +1.8$ 

In Table IV., with 
$$u$$
 and  $\phi$ , take  $C' = -1.2$ 

$$h = 699.66$$

Gauss's Tables give h = 699.72 toises.

# TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO ANOTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION, BY M. C. DIPPE.

Table I. — Argument, the observed Height of the Barometer at either Station.

Barom-		FR U	-		Tenths	of a Line.		1 89		7.1
eter in Paris	0	1	2	3	4	5	6	7	8	9
Lines.	. HILLER I	25	48 8			Villa in		N. C.		
B or B'		EMP.			H or H' in	n Toises =				
270	0.7	2.2	3.7	5.2	6.7	8.2	9.7	11.2	12.8	14.
271	15.8	17.3	18.8	20.3	21.8	23.3	24.8	26.3	27.8	29.
272	30.8	32.3	33.8	35.3	36.8	38.3	39.8	41.3	42.8	44.
273	45.8	47.3	48.8	50.3	51.8	53.3	54.8	56.3	57.8	59.
274	60.8	62.2	63.7	65.2	66.7	68.2	69.7	71.2	72.7	74
275	75.6	77.1	78.6	80.1	81.6	83.1	84.5	86.0	87.5	89.
23 Inch.	STEEL ST					MI CONTRACTOR				
276	90.5	91.9	93.4	94.9	96.4	97.9	99.3	100.8	102.3	103
277	105.2	106.7	108.2	109.7	111.1	112.6	114.1	115.6	117.0	118.
278	120.0	121.4	122.9	124.4	125.8	127.3	128.8	130.2	131.7	133.
279	134.6	136.1	137.6	139.0	140.5	142.0	143.4	144.9	146.3	147.
280	149.3	150.7	152.2	153.6	155.1	156.5	158.0	159.5	160.9	162.
281	163.8	165.3	166.7	168.2	169.6	171.1	172.5	174.0	175.4	176.
282	178.3	179.8	181.2	182.7	184.1	185.6	187.0	188.5	189.9	191
283	192.8	194.2	195.7	197.1	198.6	200.0	201.4	202.9	204.3	205
284	207.2	208.6	210.1	211.5	213.0	214.4	215.8	217.3	218.7	220
285	221.6	223.0	224.4	225.9	227.3	228.7	230.2	231.6	233.0	234
286	235.9	237.3	238.7	240.2	241.6	243.0	244.4	245.9	247.3	248.
287	250.1	251.6	253.0	254.4	255.8	257.3	258.7	260.1	261.5	262
4 Inch.							2. (1)			
288	264.4	265.8	267.2	268.6	270.0	271.4	272.9	274.3	275.7	277
289	278.5	279.9	281.3	282.8	284.2	285.6	287.0	288.4	289.8	291.
290	292.6	294.0	295.4	296.8	298.3	299.7	301.1	302.5	303.9	305.
291	306.7	308.1	309.5	310.9	312.3	313.7	315.1	316.5	317.9	319.
292	320.7	322.1	323.5	324.9	326.3	327.7	329.1	330.5	331.9	. 333.
293	334.7	336.1	337.5	338.9	340.2	341.6	343.0	344.4	345.8	347
294	348.6	350.0	351.4	352.8	354.2	355.5	356.9	358.3	359.7	361.
295	362.5	363.9	365.2	366.6	368.0	369.4	370.8	372.2	373.5	374.
296	376.3	377.7	379.1	380.4	381.8	383.2	384.6	385.9	387.3	388.
297	390.1	391.5	392.8	394.2	395.6	397.0	398.3	399.7	401.1	402.
298	403.8	405.2	406.5	407.9	409.3	410.7	412.0	413.4	414.8	416.
299	417.5	418.9	420.2	421.6	423.0	424.3	425.7	427.1	428.4	429
5 Inch.			STATE S	14 1 A	TAU BY	p #2/2/24				
300	431.1	432.5	433.9	435.2	436.6	437.9	439.3	440.7	442.0	443.
301	444.7	446.1	447.5	448.8	450.2	451.5	452.9	454.2	455.6	456.
302	458.3	459.6	461.0	462.3	463.7	465.0	466.4	467.8	469.1	470.
303	471.8	473.1	474.5	475.8	477.2	478.5	479.9	481.2	482.6	483.
304	485.3	486.6	487.9	489.3	490.6	492.0	493.3	494.7	496.0	497
305	498.7	500.0	501.4	502.7	504.0	505.4	506.7	508.0	509.4	510.
6675	512.0	District.	ALLE BY			B-1111				8

TABLE I. Continued.

Barom- eter in	rin											
Paris Lines.	0	1	2	3	4	5	6	7	8	9		
306	512.0	513.4	514.7	516.0	517.4	518.7	520.1	521.4	522.7	524.0		
307	525.4	526.7	528.0	529.4	530.7	532.0	533.4	534.7	536.0	537.4		
308	538.7	540.0	541.3	542.6	544.0	545.3	546.6	547.9	549.3	550.6		
309	551.9	553.2	554.6	555.9	557.2	558.5	559.8	561.2	562.5	563.8		
310	565.1	566.4	567.8	569.1	570.4	571.7	573.0	574.3	575.6	576.9		
311	578.3	579.6	580.9	582.2	583.5	584.8	586.1	587.5	588.8	590.1		
26 Inch.			in the			174 174			THE REAL PROPERTY.			
312	591.4	592.7	594.0	595.3	596.6	597.9	599.2	600.6	601.9	603.2		
313	604.5	605.8	607.1	608.4	609.7	611.0	612.3	613.6	614.9	616.2		
314	617.5	618.8	620.1	621.4	622.7	624.0	625.3	626.6	627.9	629.2		
315	630.5	631.8	633.1	634.4	635.7	637.0	638.3	639.5	640.8	642.1		
316	643.4	644.7	646.0	647.3	648.6	649.9	651.2	652.5	653.8	655.1		
317	656.3	657.6	658.9	660.2	661.5	662.8	664.1	665.4	666.6	667.9		
319	669.2	670.5	671.8	673.1	674.3	675.6	676.9	678.2	679.5	680.8		
319	682.0	683.3	684.6	685.9	687.2	688.4	689.7	691.0	692.3	693.6		
320	694.8	696.1	697.4	698.7	699.9	701.2	702.5	703.8	705.0	706.3		
321	707.6	708.9	710.1	711.4	712.7	713.9	715.2	716.5	717.7	719.0		
322	720.3	721.6	722.8	724.1	725.4	726.6	727.9	729.2	730.4	731.7		
323	733.0	734.2	735.5	736.7	738.0	739.3	740.5	741.8	743.1	744.3		
7 Inch.	H IN THE	7 8 1		M Ag		OF ALL						
324	745.6	746.8	748.1	749.4	750.6	751.9	753.2	754.4	755.7	756.9		
325	758.2	759.4	760.7	761.9	763.2	764.5	765.7	767.0	768.2	769.5		
326	770.7	772.0	773.2	774.5	775.7	777.0	778.2	779.5	780.7	782.0		
327	783.2	784.5	785.7	787.0	788.2	789.5	790.7	792.0	793.2	794.5		
328	795.7	797.0	798.2	799.4	800.7	801.9	803.2	804.4	805.7	806.9		
329	808.2	809.4	810.6	811.9	813.1	814.4	815.6	816.8	818.1	819.3		
000	000 0	001.0	000 0	0040	005 5	000 =	000 0	000.0	000 4	001 -		
330	820.6	821.8	823.0	824.3	825.5	826.7	828.0	829.2	830.4	831.7		
331	832.9	834.2	835.4	836.6	837.9	839.1	840.3	841.6	842.8	844.0		
332	845.2	846.5	847.7	848.9	850.2	851.4	852.6	853.9	855.1	856.3		
333	857.5	858.8	860.0	\$61.2	862.4	863.7	864.9	866.1	867.3	868.6		
334	869.8	871.0	872.2	873.4	874.7	875.9	877.1	878.3	879.6	880.8		
335	882.0	883.2	884.4	885.7	886.9	888.1	889.3	890.5	891.7	893.0		
336	894.2	895.4	896.6	897.8	899.0	900.3	901.5	902.7	903.9	905.1		
337	906.3	907.5	908.7	909.9	911.2	912.4	913.6	914.8	916.0	917.2		
338	918.4	919.6	920.8	922.0	923.3	924.5	925.7	926.9	928.1	929.3		
339	930.5	931.7	932.9	934.1	935.3	936.5	937.7	938.9	940.1	941.3		
340	942.5	943.7	944.9	946.1	947.3	948.5	949.7	950.9	952.1	953.3		
341	954.5	955.7	956.9	958.1	959.3	960.5	961.7	962.9	964.1	965.3		
249	066 5	967.7	968.9	970.1	971.3	972 5	072 7	0746	070.0	0000		
342	966.5	The second second	- 17 - 17 - 17 - 17 - 17 - 17 - 17 - 17	40.1		A COLUMN TO SERVICE AND ADDRESS OF THE PARTY	973.7	974.8	976.0	977.2		
343	978.4	979.6	980.8	982.0	983.2	984.4	985.6	986.8	987.9	989.1		
344	990.3	991.5	992.7	993.9	995.1	996.2	997.4	998.6	999.8	1001.0		
345	1002.2	1003.4		1005.7	1006.9	1008.1	1009.3	1010.5	1011.6	1012.8		
346	The second second	1015.2	1016.4	1017.5	1018.7	1019.9	1021.1	1022.3	1023.4	1024.6		
347 29 Inch	1025.8	1027.0	1028.1	1029.3	1030.5	1031.7	1032.8	1034.0	1035.2	1036.4		
	1037.5	1038.7	1039.9	1041 1	10199	1049 4	1044.6	1010	1046 9	1048.1		

Table II.

CORRECTION FOR THE TEMPERATURE OF THE AIR.

Argument,  $2\tau = \frac{t+t'}{2}$ .

2 τ	τ'	Diff.	2 τ	τ'	Diff.	2 τ	τ'	Diff.	2 τ	τ'	Diff.
-25 -24 -23 -22 -21 -20 -19 -18 -17 -16	-14.29 -13.64 -13.00 -12.36 -11.73 -11.11 -10.50 - 9.89 - 9.29 - 8.70	0.65 0.64 0.63 0.62 0.61 0.61 0.60 0.59	-12 -11 -10 - 9 - 8 - 7 - 6 - 5 - 4 - 3	-6.38 -5.82 -5.26 -4.71 -4.17 -3.63 -3.09 -2.56 -2.04 -1.52	0.56 0.56 0.55 0.54 0.54 0.53 0.52 0.52	+ 1 2 3 4 5 6 7 8 9	+0.50 0.99 1.48 1.96 2.44 2.91 3.38 3.85 4.31 4.76	0.49 0.49 0.48 0.47 0.47 0.47 0.46 0.45	+14 15 16 17 18 19 20 21 22 23	+ 6.54 6.98 7.41 7.83 8.26 8.68 9.09 9.50 9.91	0.44 0.43 0.42 0.43 0.42 0.41 0.41 0.41 0.40
-15 -14 -13 -12	- 8.11 - 7.53 - 6.95 - 6.38	0.58 0.58 0.57	- 2 - 1 0 + 1	-1.01 -0.50 0.00 +0.50	0.51 0.50 0.50	11 12 13 +14	5.21 5.66 6.10 +6.54	0.45 0.44 0.44	24 25 26 +27	10.71 11.11 11.50 +11.89	0.40 0.39 0.39

TABLE III. FOR C.

#### ARGUMENTS, h and T.

In computing Heights reverse the signs of C. - Arguments, \u03c4 and u.

h, (u)	18 10	win 1		τ, in Deg	grees of Re	aumur =			
Toises.	<b>-16</b> °	-12°	_80	<b>-4°</b>	00	+40	+80	+12°	+16°
50	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
100	0.2	0.2	0.2	0.2	0.3	0.3	0.3	0.3	0.3
150	0.3	0.3	0.4	0.4	0.4	0.4	0.4	0.4	0.4
200	0.4	0.5	0.5	0.5	0.5	0.5	0.6	0.6	0.6
250	0.5	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.7
300	0.7	0.7	0.7	0.7	0.8	0.8	0.8	0.9	0.9
350	0.8	0.8	0.8	0.9	0.9	0.9	1.0	1.0	1.1
400	0.9	0.9	1.0	1.0	1.0	1.1	1.1	1.2	1.2
450	1.0	1.1	1.1	1.1	1.2	1.2	1.3	1.3	1.4
500	1.1	1.2	1.2	1.3	1.3	1.4	1.4	1.5	1.5
550	1.2	1.3	1.4	1.4	1.5	1.5	1.6	1.6	1.7
600	1.4	1.4	1.5	1.6	1.6	1.7	1.7	1.8	1.9
650	1.5	1.6	1.6	1.7	1.8	1.8	1.9	1.9	2.0
700	1.6	1.7	1.8	1.8	1.9	2.0	2.0	2.1	2.2
750	1.7	1.8	1.9	2.0	2.0	2.1	2.2	2.3	2.3
800	1.9	2.0	2.0	2.1	2.2	2.3	2.4	2.4	2.5
850	2.0	2.1	2.2	2.3	2.3	2.4	2.5	2.6	2.7
900	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9
950	2.3	2.4	2.5	2.6	2.7	2.7	2.9	3.0	3.1
1000	2.4	2.5	2.6	2.7	2.8	2.9	3.1	3.2	3.3

Table IV. for C'. correction in toises for the change of gravity in latitude.

In computing Heights, reverse the signs of C'. Arguments  $\varphi$  and u.

Latit	tude.		WID JUST	Aı	proximat	e Differen	ce of Leve	el, in Tois	es.		STAR STAR
	+	100	200	300	400	500	600	700	800	900	1000
0	90	0.3	0.5	0.8	1.0	1.3	1.6	1.8	2.1	2.3	2.6
5	85	0.3	0.5	0.8	1.0	1.3	1.5	1.8	2.0	2.3	2.6
10	80	0.2	0.5	0.7	1.0	1.2	1.5	1.7	2.0	2.2	2.4
15	75	0.2	0.4	0.7	0.9	1.1	1.3	1.6	1.8	2.0	2.3
20	70	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0
25	65	0.2	0.3	0.5	0.7	0.8	1.0	1.2	1.3	1.5	1.7
30	60	0.1	0.3	0.4	0.5	0.6	0.8	0.9	1.0	1.2	1.3
35	55	0.1	0.2	0.3	0.4	0.4	0.5	0.6	0.7	0.8	0.9
36	54	0.1	0.2	0.2	0.3	0.4	0.5	0.6	0.6	0.7	0.8
37	53	0.1	0.1	0.2	0.3	0.4	0.5	0.5	0.6	0.6	0.7
38	52	0.1	0.1	0.2	0.3	0.3	0.4	0.4	0.5	0.6	0.6
39	51	0.1	0.1	0.2	0.2	0.3	0.3	0.4	0.4	0.5	0.5
40	50	0.1	0.1	0.1	0.2	0.2	0.3	0.3	0.4	0.4	0.5
41	49	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.3	0.3	0.4
42	48	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.3
43	47	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.2	0.2
44	46	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1
45	45	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

TABLE V. FOR C".

Arguments  $\tau$  and T — T'. To be used only in computing Heights.

T — T	Correction for T — T', in Toises, with the same sign; $\tau =$												
Reaumur.	-12°	<b>-10</b> °	-80	<b>-6</b> °	-4°	_2°	00	+20	+40	+6°			
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0			
1	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0			
2	0.4	0.3	0.3	0.3	0.2	0.2	0.2	0.1	0.1	0.0			
3	0.6	0.5	0.5	0.4	0.4	0.3	0.2	0.2	0.1	0.1			
4	0.8	0.7	0.6	0.5	0.5	0.4	0.3	0.2	0.2	0.1			
5	1.0	09	0.8	0.7	0.6	0.5	04	0.3	0.2	0.1			
6	1.1	1.0	0.9	0.8	0.7	0.6	0.5	0.4	0.3	0.1			
7	1.3	1.2	1.1	0.9	0.8	0.7	0.6	0.4	0.3	0.2			
8	1.5	1.4	1.2	1.1	0.9	0.8	0.6	0.5	0.3	0.2			
9	1.7	1.6	1.4	1.2	1.1	0.9	0.7	0.6	0.4	0.2			
10	1.9	1.7	1.5	1.4	1.2	1.0	0.8	0.6	0.4	0.2			

Correction	for	T - T	with	contrary	y sign	a : -	T =	
------------	-----	-------	------	----------	--------	-------	-----	--

T — T'	+80	+10°	+12°	+140	T — T'	+80	+100	+120	+14°
1	0.0	0.0	0.0	0.0	6	0.0	0.1	0.2	0.3
2	0.0	0.0	0.1	0.1	7	0.0	0.1	0.2	0.3
3	0.0	0.0	0.1	0.1	8	0.0	0.1	0.2	0.4
4	0.0	0.0	0.1	0.2	9	0.0	0.1	0.2	0.4
5	0.0	0.1	0.2	0.2	10	0.0	0.1	0.3	0.4

LAPLACE'S FORMULA FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS, MODIFIED BY BABINET.

In the Comptes Rendus de l'Académie des Sciences for March, 1851, M. Babinet proposes the following modification of Laplace's formula, the object of which is to dispense both with the use of logarithms and with tables of any kind.

Laplace's formula is,

$$z = 18393$$
 metres (log H  $-\log h$ )  $\left[1 + \frac{2(T+t)}{1000}\right]$ ,

z being the difference of level between the two stations,

H, the height of barometer at the lower station,

h, the height of barometer at the upper station,

T, temperature of air at the lower station,

t, temperature of air at the upper station.

The two barometers are supposed to be reduced to the same temperature. small correction for the latitude is omitted.

For elevations less than 1000 metres, and even for much greater elevations, if approximate results only are needed, the formula may be transformed into the following:

 $z = 16000 \text{ metres } \frac{H - h}{H + h} \left[ 1 + \frac{2 (T + t)}{1000} \right]$ 

# Example 1.

Suppose,

at lower station, barometer at zero Cent. = 755mm; temperature of air 15° Cent. at upper station, barometer at zero Cent. = 745mm; temperature of air 10° Cent.

$$H - h = 10^{mm}$$
.  $T + t = 25^{\circ}$  Cent.  $H + h = 1500^{mm}$ .  $2 (T + t) = \frac{5}{1000} = .05$ .

Then

 $z = 16000_{1500} \times (1.05) = 112$  metres. Laplace's formula, by Delcros's tables, would give 111.6 metres.

# Example 2.

Suppose,

at lower station, barometer at zero Cent. = 730mm; temperature of air 20° Cent. at upper station, barometer at zero Cent. = 635mm; temperature of air 15° Cent.

$$H - h = 95^{mm}$$
.  $T + t = 35^{\circ}$  Cent.  $H + h = 1365^{mm}$ .  $2 (T + t) = \frac{7500}{17000} = .07$ .

Then

 $z = 16000_{\frac{95}{365}} \times (1.07) = 1191.5$  metres.

Laplace's formula, by Delcros's tables, would give 1191.1 metres.

For greater elevations an intermediate station may be supposed.

Babinet's formula reduced to English measures becomes,

$$z = 52494$$
 English feet  $\frac{H-h}{H+h} \left[ 1 + \frac{(T+t-64)}{900} \right];$ 

but as, in this form, it loses the simplicity of its coefficient, it will be found, on trial, that its use requires rather more computing than the author's tables (II.), p. 38, which give more accurate results.

## VII.

#### TABLES

FOR COMPUTING THE DIFFERENCE IN THE HEIGHTS OF TWO PLACES BY MEANS OF THE BAROMETER. - BAILY.

BAILY, in his Astronomical Tables and Formulæ, page 111, gives the following final formula:

$$\begin{split} x &= 60345.51 \left\{ 1 + .0011111 \left( t + t' - 64^{\circ} \right) \right\} \\ &\times \log \text{ of } \left\{ \frac{\beta}{\beta'} \times \frac{1}{1 + .0001 \left( \tau - \tau' \right)} \right\} \times \left\{ 1 + .002695 \cos 2 \phi \right\}. \end{split}$$

Where  $\phi$  = the latitude of the place,

 $\beta$  = the height of the barometer,

 $\tau$  = the temperature, Fahrenheit, of the mercury,

t = the temperature, Fahrenheit, of the air,

 $\beta'$  = the height of the barometer,

eta'= the height of the barometer, au'= the temperature, Fahrenheit, of the mercury, at the upper station.

t' = the temperature, Fahrenheit, of the air.

The numerical values assumed are as follows: -

The constant barometrical coefficient = 60158.53 English feet.

The expansion of moist air for 1° Fahrenheit = .0022222.The expansion of mercury for 1° Fahrenheit = .0001001.

The increase of gravitation from Equator to Poles = .00539.

The radius of the Earth at  $\phi$ = 20898240 English feet.

The height of lower station assumed = 4000 English feet.

Make A = the log of the first term, in English feet.

 $B = \text{the log of } 1 + .0001 (\tau - \tau').$ 

C = the log of the last term.

 $D = \log \beta - (\log \beta' + B).$ 

Then, by the tables which follow, the logarithm of the difference of altitude in English feet

 $= A + C + \log D$ .

Baily's Tables have been recomputed and extended by Downes, for Lee's Collection of Tables and Formulæ (2d edit. pp. 84, 85). These new tables are given here as revised by Mr. Downes for this volume.

I. THERMOMETERS IN THE OPEN AIR.

t+t'	A	t+t'	A	t+t'	A	t+t'	A	t+t'	A
P 1	4.74913	37	4.76742	73	4.78497	109	4.80183	0 145	4.8180
2	4.74965	38	4.76791	74	4.78544	110	4.80229	146	4.8185
3	4.75016	39	4.76841	75	4.78592	111	4.80275	147	4.8189
4	4.75068	40	4.76891	76	4.78640	112	4.80321	148	4.81940
5	4.75120	41	4.76940	77	4.78687	113	4.80367	149	4.81984
		, 11							410100
6	4.75171	42	4.76990	78	4.78735	114	4.80413	150	4.8202
7	4.75223	43	4.77039	79	4.78782	115	4.80458	151	4.8207
8	4.75274	44	4 77089	80	4.78830	116	4.80504	152	4.82110
9	4.75326	45	4.77138	81	4.78877	117	4.80550	153	4.82160
10	4.75377	46	4.77187	82	4.78925	118	4.80595	154	4.8220
11	4.75429	47	4.77236	83	4.78972	119	4.80641	155	4.82248
12	4.75480	48	4.77285	84	4.79019	120	4.80686	156	4.8229
13	4.75531	49	4.77335	85	4.79066	121	4.80731	157	4.8233
14	4 75582	50	4.77384	86	4.79113	122	4.80777	158	4.8237
15	4.75633	51	4.77433	87	4.79160	123	4.80822	159	4.8242
7.0					valoudus	1 464	. Libitat		
16	4.75684	52	4.77482	88	4.79207	124	4.80867	160	4.8246
17	4.75735	53	4.77530	89	4.79254	125	4.80913	161	4.8251
18	4.75786	54	4.77579	90	4.79301	126	4.80958	162	4.82553
20	4.75888	55 56	4.77628	91	4.79348	127	4.81003	163	4.8259
20	4.70000	50	4.77077	92	4.79395	128	4.81048	164	4.8264
21	4.75938	57	4.77725	93	4 79442	129	4.81093	165	4.8268
22	4.75989	58	4.77774	94	4.79489	130	4.81138	166	4.82727
23	4.76040	59	4.77823	95	4.79535	131	4.81183	167	4.82770
24	4.76090	60	4.77871	96	4.79582	132	4.81228	168	4.82814
25	4.76141	61	4.77919	97	4.79628	133	4.81273	169	4.8285
26	4.76191	62	4.77968	98	4.79675	134	4.81317	170	4.82900
27	4.76241	63	4.78016	99	4.79721	135	4.81362	171	4.82943
28	4.76292	64	4.78065	100	4.79768	136	4.81407	172	4.82986
29	4.76342	65	4.78113	101	4.79814	137	4.81452	173	4.83029
30	4.76392	66	4.78161	102	4.79861	138	4.81496	174	4.83072
31	4.76442	67	4.78209	103	4.79907	139	4.81541	175	4.83116
32	4.76492	68	4.78257	104	4.79953	140	4.81585	176	4.83158
33	4.76542	69	4.78305	105	4.79999	141	4.81630	177	4.83201
34	4.76592	70	4.78353	106	4.80045	142	4.81674	178	4.83244
35	4.76642	71	4.78401	107	4.80091	143	4.81719	179	4.83287
36	4.76692	72	4.78449	108	4.80137	144	4.81763	180	4.83330

	H.	III. LATITUDE OF THE PLACE.					
τ-τ'	В	$  \tau-\tau'  $	В	τ-τ'	В	φ	C
0	0.00000	0 20	0.00087	o 40	0.00174	0	0.00117
1	0.00004	21	0.00091	41	0.00174	5	0.00117
2	0.00009	22	0.00091	42	0.00173	10	0.00113
	0.00013	23	0.00100	43	0.00187	15	0.00110
3 4	0.00017	24	0.00104	44	0.00191	20	0.00090
	Salinia v E			1			
5	0.00022	25	0.00109	45	0.00195	25	0.00075
6	0.00026	26	0.00113	46	0.00200	30	0.00058
7	0.00030	27	0.00117	47	0.00204	35	0.00040
8	0.00035	28	0.00122	48	0.00208	40	0.00020
9	0.00039	29	0.00126	49	0.00212	45	0.00000
				25 M	aid The second	- Home	
10	0.00043	30	0.00130	50	0.00217	50	9.99980
11	0.00048	31	0.00135	51	0.00221	55	9.99960
12	0.00052	32 ·	0.00139	52	0.00225	60	9.99942
13	0.00056	33	0.00143	53	0.00230	65	9.99925
14	0.00061	34	0.00148	54	0.00234	70	9.99910
15	0.00065	35	0.00152	55	0.00238	75	9,99900
16	0.00069	36	0.00156	56	0.00243	80	9.99890
17	0.00074	37	0.00161	57	0.00247	85	9.99885
18	0.00078	38	0.00165	58	0.00251	90	9.99883
19	0.00083	39	0.00169	59	0.00256		0.0000

# Example.

	Upper Station.	Lower Station.
Thermometer in open air,	t' = 70.4,	t = 77.6.
Attached Thermometer,	$\tau' = 70.4$ ,	$\tau = 77.6.$
Barometer,	$\beta' = 23.66$ inches.	$\beta = 30.05$ inches.
Latitude of the place	$\phi = 21^{\circ}$ .	ciclements but embed &
B = 0.00031	$\log D = 9$ .	01502
$\log \beta' = 1.37401$	C=0	00087
1.37432	A=4	81940
$\log \beta = 1.47784$	$\overline{3}$	83529
D = 0.10352	= 6	843.7 English feet.

## VIII.

#### TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS,

BASED ON BESSEL'S FORMULA.

#### BY E. PLANTAMOUR.

[These Tables, computed by Professor E. Plantamour, Director of the Observatory at Geneva, Switzerland, are found in Vol., XIII. Part 1, of the Mémoires de la Société de Physique, &c. de Genève, p. 63, together with the following explanations.]

In No. 356 of the Astronomische Nachrichten, Bessel published a paper on the measurement of heights by means of the barometer, in which he deduces a formula which contains a factor depending on the humidity of the air. This formula is:

$$\log \frac{P}{P'} = \frac{(g) \cdot H' - H}{L(1 + KT)} \left[ 1 - a \frac{0.002561}{\sqrt{PP'}} \cdot 10 \frac{0.0279712 \, T - 0.0000625826 \, T^2}{\sqrt{PP'}} \right],$$

where the various quantities have the following signification: -

h being the elevation of the lower station, and

h' the elevation of the upper station above the level of the sea,

a = the radius of the Earth,

$$H = \frac{ah}{a+h},$$

$$H'=\frac{a\,h'}{a+h'};$$

P = the weight of the atmosphere at the lower station,

P' = the weight of the atmosphere at the upper station,

the unit of weight assumed being the pressure of a column of mercury

#### BAROMETRICAL MEASUREMENT OF HEIGHTS.

of 336.905 Paris lines, at the temperature of the freezing point, or zero Reaumur, and under the 45th degree of latitude.

In order to recise the formula into tables, I

(g) = the gravity, at the level of the sea, in the mean latitude between the two places of observation.

Therefore, calling  $\phi$  the latitude,

 $(g) = 1 - 0.0026257 \cos \phi$ 

L = the constant barometrical coefficient depending on the relative density of the mercury and of the air,

K = the coefficient of the expansion of the air,

T = the mean temperature of the layer of air between the lower and upper station,

a = the fraction of saturation of the same layer.

The second term in the parenthesis, destined to take into account the aqueous vapor in the air, was obtained by assuming that the elastic force of vapor for a temperature T is represented, in unit of weight, by the expression,

$$p = 0.0067407 \times 10^{-0.0279712} \text{ T} - 0.0000625826 \text{ T}^2$$
.

Multiplying the second member by 336.905 we find the expression of the elastic force of vapor that Laplace deduced from Dalton's experiments. Substituting, in the computation, Regnault's results, the numerical value of these coefficients is somewhat changed, and we find then

$$p = 0.0060527 \times 10^{-0.0301975} \,\mathrm{T} - 0.000080170 \,\mathrm{T}$$
.

Bessel's tables give the difference of elevation in toises. The logarithm of the difference is obtained by the sum of four logarithms. The same form is preserved in the following tables; but the differences of elevation are given in metres.

The term due to the expansion of the air is computed in Bessel's tables for two values of the coefficient, viz. that of Gay-Lussac, 0.00375, and that of Rudberg, 0.003648; in the new tables it is only computed for that of Regnault, 0.003665.

The relative density of dry air at the freezing point, under a barometrical pressure of 0<sup>m</sup>·.76, and at the 45th degree of latitude, and of mercury in the same circumstances, adopted by Bessel, is that determined by the experiments of Biot and Arago, viz.

1 10466.8. The value of that constant derived from Regnault's experiments has been substituted. Regnault found the weight of a litre of dry air, at zero Centigrade, under a pressure of 0<sup>m</sup>.76, and at the latitude of Paris, to be 1.293187 grammes, which, reduced to the gravity of the 45th degree of latitude, becomes 1.292732 grammes. The weight of a litre of mercury, at zero Centigrade, he found to be 13596 grammes; the ratio is thus:

$$D = \frac{1}{10517.3},$$

or about  $2\sqrt[3]{5}$  smaller than the value adopted by Bessel. If the constant coefficient L is expressed by  $L = \frac{0^{m_*}.76}{D \cdot \mu}$ ,  $\mu$  being the modulus of the common logarithms, its numerical value becomes

$$L = 18404^{m}.8.$$

In order to reduce the formula into tables, Bessel caused it to undergo several modifications, which we have followed, introducing the values of the constants above mentioned.

Let b and b' be the heights of the barometer, expressed in the metrical scale, at the two stations; t and t', the temperatures of the mercury measured with a brass scale; we have,

$$P = \frac{b}{0^{m} \cdot .76} \cdot (g) \cdot \left(\frac{a}{a+h}\right)^{2} \frac{(1+0.00001879 t)}{(1+0.00018018 t)}$$

and

$$P' = \frac{b'}{0^{m} \cdot .76} \cdot (g) \cdot \left(\frac{a}{a+b'}\right)^{2} \frac{(1+0.00001879 \, t')}{(1+0.000018018 \, t')}.$$

Therefore,

$$\log P = \log b + \log (g) - \log 0^{m}.76 - \frac{2 H \mu}{a} - \mu t [0.00018018 - 0.00001879],$$

$$\log P' = \log b' + \log (g) - \log 0^{m} \cdot .76 - \frac{2 H' \mu}{a} - \mu t' [0.00018018 - 0.00001879].$$

If we call B, B' the heights of the barometer reduced to the freezing point, which we obtain by making

$$\log B = \log b - t \cdot 0.000070095; \qquad \log B' = \log b' - t' \cdot 0.000070095,$$

$$\log \frac{P}{P'} = \log B - \log B' + \frac{H' - H}{7329755},$$

and with sufficient accuracy,

$$\checkmark PP' = \frac{\checkmark BB'}{0^{m} \cdot .76}.$$

Substituting these expressions in the formula, it becomes,

$$\log B - \log B' = \frac{(g) \cdot H' - H}{L (1 + K T)} \left[ 1 - \frac{L (1 + K T)}{(g) \cdot 7329755} - \frac{a \cdot 0.001748}{\sqrt{BB'}} \cdot 10^{0.0301975} T - 0.000080170 T^{2} \right].$$

If we set instead of a the half sum  $\frac{a+a}{2}$  of the fraction of saturation observed at both stations, we find, after some transformations,

BAROMETRICAL MEASUREMENT OF HEIGHTS.

$$\log B - \log B' = \frac{(g) (H' - H) (397.25 - KT)}{398.25 \cdot L (1 + KT)} \times \left[1 - \frac{(a + a') \cdot 0.34807}{(397.25 - KT) \sqrt{BB'}} \cdot 10^{0.0301975 T - 0.000080170 T^{2}}\right].$$

Making further,

$$V = \frac{398.25}{397.25 - KT} L (1 + KT),$$

$$W = \frac{0.34807}{397.25 - KT} \cdot 10^{-0.0301975} T - 0.000080170 T^{2}$$

we shall have for the logarithm of the approximate difference of level between the two stations H' — H,

$$\log (H' - H) = \log \left[\log B - \log B'\right]$$

$$+ \log V + \log \frac{1}{1 - W \frac{\alpha + \alpha'}{\sqrt{B B'}}} + \log \frac{(g)}{1}.$$

Table I. gives the values of log V and log W, both of which only depend on the temperature; the argument is the sum of the temperature of the air,  $\tau$  and  $\tau'$ , observed at both stations, supposing  $\tau + \tau' = 2 \text{ T}$ .

Table II. gives the factor depending on the humidity of the air; with the argument

W. 
$$\log \frac{(a+a')}{\sqrt{BB'}}$$
,

we obtain

$$\log \frac{1}{1 - W \frac{(\alpha + \alpha')}{\sqrt{BB'}}} = \log V'.$$

Table III. gives the factor depending on the latitude for every degree, viz.

$$\log G' = \log \frac{1}{(g)}.$$

The logarithm of the approximate difference is thus given by the sum of four logarithms. To obtain the exact elevation, the small correction found in Table IV. must be added to the number corresponding to that logarithm. For we have, with the necessary accuracy,

$$h' - h = H' - H + \frac{H'^2}{a} - \frac{H^2}{a}$$

Table IV. gives, for every 200 metres, the quantity  $\frac{H^2}{a}$ ; the number in the table corresponding to  $\frac{H'^2}{a}$  must be added to the approximate elevation; and the number corresponding to  $\frac{H^2}{a}$  must be subtracted from the same.

#### USE OF THE TABLES.

Reduce first the observed height of the barometer at both stations to the freezing point by means of the usual tables, or by the logarithmic formula,

$$\log B = \log b - t \cdot 0.00007$$
,  $\log B' = \log b' - t' \cdot 0.00007$ ;

b and b' being, in fractions of metre, the observed heights at the temperatures t and t' marked by the attached thermometers; and B and B' the reduced height at the lower and upper station.

Take the difference of log B and log B', and find, in the tables of the common logarithms, the logarithm of that difference, viz. log (log B — log B'); find also the logarithm of the product  $\sqrt{B}$  B', or

$$\log \checkmark B B' = \frac{\log B + \log B'}{2}.$$

Make further the sum  $\tau + \tau'$  of the temperature of the air at both stations, and likewise the sum of a + a' of the fraction of saturation.

Then, in Table I., with argument  $\tau + \tau'$ , take log V and log W; further, to log W add log (a + a'), and subtract log  $\checkmark BB'$ ; and with the logarithm thus obtained as argument, take in Table II. log V'.

Table III. with the mean latitude of the stations gives log G'.

H' — H being the approximate difference of level between the two stations, we have

$$\log (H' - H) = \log (\log B - \log B') + \log V + \log V' + \log G'.$$

The altitude of the lower station being known, we deduce from H' - H the approximate altitude, H', of the upper station; h', the exact altitude, or h' - h, the difference of elevation, is given by the formula,

$$h' - h = H' - H + \frac{H'^2}{a} - \frac{H^2}{a}$$

Table IV. gives the values of  $\frac{H'^2}{a}$  and  $\frac{H^2}{a}$  for the values of H' or H for every 200 metres.

## Example 1.

Computing the height of St. Bernard, taking Geneva, 407 metres above the level of the sea, as the lower station. The observation gives,

$$\log \left[\log B - \log B'\right] = 9.04215$$
In Table I. argt.  $\tau + \tau' = +7.08$ ,  $\log V = 4.27164$ 
In Table II. argt.  $7.4409$ ,  $\log V' = 0.00120$ 
In Table III. argt.  $46^\circ$ ,  $\log G' = -0.00004$ 

$$\log (H' - H) = 3.31495$$

$$H' - H = 2065.1 \text{ metres.}$$
In Table IV.  $\frac{H'^2}{a} - \frac{H^2}{a} = + 0.9$ 

$$h' - h = 2066.0$$
Geneva altitude  $h = 407.0$ 
St. Bernard above the level of the sea  $h' = 2473.0$  metres.

# Example 2.

Computing the height of Mont Blanc from the observations of Bravais and Martins, on the 29th of August, 1844, taking St. Bernard (2473.0 metres) as the lower station. The observation gives,

II.	MADY D. I.												
					TABLE						E IV.		
			Argu	ıment =	$\tau + \tau'$ . Cer	tigrade Deg	grees.			Arg't. =	Height.		
	τ + τ··	log. V.	log. W.	τ + τ'.	log. V.	log. W.	τ + τ <sup>1</sup> .	log. V.	log. W.	H'. H.	+		
	0	La production	PER LA	0			0	4.00017	W W000	Metres.	Metres.		
1	-24	4.24644	6.5362	+15	4.27783	7.1692	+54	4.30711	7.7033	200 400	0.01		
I	-23	4.24728 4.24811	6.5441	+16	4.27861 4.27938	7.1839 7.1985	+56	4.30784	7.7287	600	0.03		
1	-22 -21	4.24811	6.5797	+18	4.28016	7.2131	+57	4.30929	7.7413	800	0.10		
	-20	4.24977	6.5974	+19	4.28093	7.2275	+58	4.31001	7.7539	1000	0.16		
l		-	Wh. B. 15	120	er Wad	out in	aville	att words	Inmed !	100			
	-19	4.25059	6.6157	+20	4.28170	7.2420	+59	4.31073	7.7664	1200	0.23		
	-18	4.25142	6.6341	+21	4.28247	7.2564	+60	4.31145	7.7789	1400	0.31		
	-17	4.25225	6.6521	+22	4.28323	7.2708	+61	4.31217	7.7914	1600	0.40		
	-16	4.25307	6.6700	+23	4.28400	7.2850	+62	4.31288	7.8038	1800	0.51		
	-15	4.25389	6.6879	+24	4.28477	7.2993	+63	4.31360	7.8161	2000	0.63		
	-14	4.25471	6.7057	+25	4.28553	7.3135	+64	4.31432	7.8285	2200	0.76		
	-13	4.25553	6.7232	+26	4.28629	7.3276	+65	4.31503	7.8407	2400	0.90		
ı	-12	4.25634	6.7407	+27	4.28705	7.3417	+66	4.31574	7.8530	2600	1.06		
I	-11	4.25716	6.7581	+28	4.28781	7.3557		THE REAL PROPERTY.	All the E	2800	1.23		
	-10	4.25797	6.7755	+29	4.28857	7.3697		Carlo Santo	HER INDICATE	3000	1.41		
1	- 9	4 9 0 0 0 0	C 700C	120	4.00000	w 800w	F 14	District	Date of	9900	1.01		
I	- 8	4.25878 4.25959	6.7926	+30	4.28933	7.3837			- A-9	3200 3400	1.61		
H	- 7	4.26040	6.8266	+32	4.29008	7.3975	WO L		- Dar	3600	2.04		
II	- 6	4.26121	6.8436	+33	4.29159	7.4252	A LAURA	No. of the last of		3800	2.27		
II	- 5	4.26202	6.8603	+34	4.29234	7.4389	4507 85	W. E	Page 4	4000	2.51		
1	N. T			20.00	61		124	LABY	301-	I wife			
	- 4	4.26282	6.8770	+35	4.29319	7.4526		0.3100.000	ALT L	4200	2.77		
	- 3	4.26362	6.8935	+36	4.29384	7.4662	100	1	100	4400	3.04		
	- 2	4.26443	6.9100	+37	4.29459	7.4798	Time B	(T - 1/2-T - 1	of Jack	4600	3.32		
	- 1	4.26523	6.9263	+38	4.29534	7.4933	28			4800	3.62		
	0	4.26603	6.9426	+39	4.29608	7.5068				5000	3.93		
	+ 1	4.26682	6.9581	+40	4.29683	7.5202		4	000	5200	4.25		
	+ 2	4.26762	6.9736	+41	4.29757	7.5336	F	Bullet 1		5400	4.58		
	+ 3	4.26841	6.9889	+42	4.29831	7.5470	12.1	R see Vill	301-	5600	4.93		
	+ 4	4.26921	7.0043	+43	4.29905	7.5602		District In	13.7 3	5800	5.28		
	+ 5	4.27000	7.0195	+44	4.29979	7.5735		119	MEST	6000	5.65		
-	+ 6	4.00000	* 00 (=				1874	HAT THE	11 6 6	0000	000		
	+ 6 + 7	4.27079	7.0347	+45	4.30053	7.5867		Albert Lat	100	6200	6.04		
	+ 8	4.27157	7.0499	+46 +47	4.30127	7.5999	FREE	Control of	Sec. 11	6400	6.43		
1	+ 9	4.27315	7.0800	+48	4.30200	7.6130	- 1	LIPER LITTE	-34	6800	7.26		
-	+10	4.27393	7.0950	+49	4.30347	7.6390	busel.	A Want	10 8- 1	7000	7.70		
-		THUNE	TILLER	-	N premior		occus##	Mode "	1000		1		
1	+11	4.27471	7.1099	+50	4.30420	7.6519		STREET L	23.8/06	7200	8.14		
1	+12	4.27550	7.1248	+51	4.30493	7.6648	123			7400	8.60		
	+13	4.27628	7.1397	+52	4.30566	7.6777			18 m /	. 9 - 3			
	+14	4.27705	7.1545	+53	4.30639	7.6905	ABL			1 1 M	-		
	+15	4.27783	7.1692	+54	4.30711	7.7033	184	The state of	1		1		
L						To law is	1	119 (50.10)			1		

	Ar		LE II.	to an	72T.	TABL			
Argum't.	log. V'.	Argum't.	log. V'.	Argum't.	log. V'.	φ.	log. G'.	φ.	log. G <sup>1</sup> .
0 = 70	0.00014	7.70	0.00218	8.09	0.00590	0	10.00114	0	10,00000
6.5	0.00014	7.71	0.00218	8.10	0.00538	1	+0.00114	40	+0.00020 +0.00016
6.7	0.00022	7.72	0.00229	8.11	0.00563	2	+0.00114	42	+0.00012
6.8	0.00022	7.73	0.00223	8.12	0.00576	3	+0.00114	43	+0.000012
6.9	0.00034	7.74	0.00239	8.13	0.00590	4	+0.00113	44	+0.00004
7.0	0.00043	7.75	0.00245	8.14	0.00604	5	+0.00112	45	0.00000
7.1	0.00055	7.76	0.00251	8.15	0.00618	6	+0.00112	46	-0.00004
7.2	0.00069	7.77	0.00256	8.16	0.00632	7	+0.00111	47	-0.00008
7.3	0.00087	7.78	0.00262	8.17	0.00647	8	+0.00110	48	-0.00012
7.4	0.00109	7.79	0.00269	8.18	0.00662	9	+0.00109	49	-0.00016
Bigit in			TOTAL GET	THE REAL PROPERTY.	3 1 1 1 1			ME	
7.41	0.00112	7.80	0.00275	8.19	0.00678	10	+0.00107	50	-0.00020
7.42	0.00114	7.81	0.00281	8.20	0.00694	11	+0.00106	51	-0.00024
7.43	0.00117	7.82	0.00288	8.21	0.00710	12	+0.00104	52	-0.00028
7.44	0.00120	7.83	0.00295	8.22	0.00727	13	+0.00103	53	-0.00031
7.45	0.00123	7.84	0.00302	8.23	0.00744	14	+0.00101	54	-0.00035
7.46	0.00125	7.85	0.00309	8.24	0.00761	15	+0.00099	55	-0.00039
7.47	0.00128	7.86	0.00316	8.25	0.00779	16	+0.00097	56	-0.00043
7.48	0.00131	7.87	0.00323	8.26	0.00798	17	+0.00095	57	-0.00046
7.49	0.00134	7.88	0.00331	8.27	0.00816	18	+0.00092	58	-0.00050
7.50	0.00138	7.89	0.00338	8.28	0.00835	19	+0.00090	59	-0.00054
7.51	0.00141	7.90	0.00346	8.29	0.00855	20	+0.00087	60	-0.00057
7.52	0.00144	7.91	0.00354	8.30	0.00875	21	+0.00085	61	-0.00060
7.53	0.00147	7.92	0.00363	8.31	0.00896	22	+0.00082	62	-0.00064
7.54	0.00151	7.93	0.00371	8.32	0.00917	23	+0.00079	63	-0.00067
7.55	0.00154	7.94	0.00380	8.33	0.00939	24	+0.00076	64	-0.00070
7.56	0.00158	7.95	0.00389	8.34	0.00961	25	+0.00073	65	-0.00073
7.57	0.00162	7.96	0.00398	8.35	0.00983	26	+0.00070	-66	-0.00076
7.58	0.00165	7.97	0.00407			27	+0.00067	67	-0.00079
7.59	0.00169	7.98	0.00417	***************************************	North Contract	28	+0.00064	68	-0.00082
7.60	0.00173	7.99	0.00427	COLUMN TO THE PARTY OF THE PART		29	+0.00060	69	-0.00085
7.61	0.00177	8.00	0.00437			30	+0.00057	70	-0.00087
7.62	0.00181	8.01	0.00447			31	+0.00054	71	-0.00090
7.63	0.00186	8.02	0.00457	note M	. Tour	32	+0.00050	72	-0.00092
7.64	0.00190	8.03	0.00468			33	+0.00046	73	-0.00094
7.65	0.00194	8.04	0.00479	STORES.		34	+0.00043	74	-0.00097
7.66	0.00199	8.05	0.00490	a total	and the	35	+0.00039	75	-0.00099
7.67	0.00199	8.06	0.00490	No. of Contract of	1	36	+0.00035	76	-0.00099
7.68	0.00204	8.07	0.00502	A PAGE AND ADDRESS OF		37	+0.00033	77	-0.00101
7.69	0.00203	8.08	0.00515	DOLLAR TO		38	+0.00031	78	-0.00102
7.70	0.00218	8.09	0.00538	white to	B. Car	39	+0.00024	79	-0.00104
				1000		40	+0.00020	80	-0.00107

#### CORRECTION

FOR THE HOUR OF THE DAY AND THE SEASON OF THE YEAR AT WHICH THE OBSERVATIONS HAVE BEEN TAKEN.

In all the preceding tables, the mean temperature of the layer of air between the two stations is assumed to be given by the half-sum of the temperatures observed at each station, or by  $\frac{t+t'}{2}$ . Experience, however, has proved that this assumption is not true under all meteorological circumstances, and that, not to speak of more irregular influences, the temperature expressed by  $\frac{t+t'}{2}$  differs in + or - from the true mean temperature by a quantity which considerably varies with the hour of the day, the season of the year, and the elevation at which the observations are taken. The amount of the correction for the temperature of the air, as given by the various formulas, thus needs to be modified accordingly. In the absence of the data necessary for establishing the law of the decrease of heat on the vertical in the various layers of the atmosphere, at the different periods of the day and of the year, and in different latitudes, which alone would furnish the means of determining the true value of this correction in these various circumstances, the following empirical tables enable us to form a judgment of the importance of that correction.

Tables IX. and X. are taken from Berghaus, Grundriss der Geographie, p. 91, and in the Tables accompanying the same work, p. 71. The correction to be applied for the hour of the day at which the observations have been taken, is found by multiplying the approximate height obtained by the factors in Table IX., giving to the correction the sign of the factor. This table and the following are calculated to be used in the climate of Germany, and for elevations not much exceeding 5,000 feet. The influence of the seasons on the correction is not taken into the account; judging from Table X., the correction may be, perhaps, too small for the summer months, and may better answer for the autumn. Using these factors, we obtain for the differences of level, in toises, placed at the head of each column, in Table X., the correction corresponding to each hour, from 6 A. M. to 10 P. M.

TABLE IX.

Hour.	Factor.	Hour.	Factor.	Hour.	Factor.
A. M. 6	+0.0075	Noon.	-0.0054	P. M. 5	-0.0011
7	+0.0050	P. M. 1	-0.0057	6	+0.0013
. 8	+0.0025	2	-0.0059	7	+0.0022
9	-0.0005	3	-0.0045	8	+0.0032
10	-0.0035	4	-0.0031	9	+0.0043
11	-0.0044	5	-0.0011	10	+0.0054

TABLE X.

#### CORRECTION FOR THE HOUR OF THE DAY.

#### ARGUMENT, THE HOUR, AND THE APPROXIMATE HEIGHT IN TOISES.

Correction, in Toises, for											
Hour.	100	200	300	400	500	600	700	800	900	Hour.	
A. M. 6	+0.7	+1.5	+2.2	+3.0	+3.7	+4.5	+5.2	+6.0	+6.7	6 A. M.	
7	+0.5	+1.0	+1.5	+2.0	+2.5	+3.0	+3.5	+4.0	+4.5	7	
8	+0.2	+0.5	+0.7	+1.0	+1.2	+1.5	+1.8	+2.0	+2.3	8	
9	-0.0	-0.1	-0.1	-0.2	-0.2	-0.3	-0.3	-0.4	-0.4	9	
10	-0.3	-0.7	-1.0	-1.4	-2.1	-2.4	-2.8	-3.1	-3.5	10	
11	-0.4	-0.9	-1.3	-1.8	-2.2	-2.7	-3.1	-3.6	-4.0	11	
	10.75		WIN Y								
Noon.	-0.5	-1.1	-1.6	-2.2	-2.7	-3.3	-3.8	-4.4	-4.9	Noon.	
P. M. 1	-0.6	-1.1	-1.7	-2.3	-2.8	-3.4	-4.0	-4.5	-5.1	1 P. M.	
2	-0.6	-1.2	-1.8	-2.4	-3.0	-3.5	-4.1	-4.7	-5.3	2	
3	-0.4	-0.9	-1.3	-1.8	-2.2	-2.7	-3.1	-3.6	-4.0	3	
4	-0.3	-0.6	-0.9	-1.2	-1.5	-1.8	-2.1	-2.4	-2.7	4	
Charles of Box	6.61.1	PAR H	20.				o will	10.61	1000		
5	-0.1	-0.2	-0.3	-0.4	-0.5	-0.6	-0.7	-0.8	-0.9	5	
6	+0.1	+0.2	+0.4	+0.5	+0.5	+0.8	+0.9	+1.0	+1.1	6	
7	+0.2	+0.4	+0.7	+0.9	+1.1	+1.3	+1.6	+1.8	+2.0	7	
8	+0.3	+0.6	+0.9	+1.3	+1.6	+1.9	+2.2	+2.5	+2.9	8	
9	+0.4	+0.8	+1.3	+1.7	+2.1	+2.6	+3.0	+3.4	+3.8	9	
10	+0.5	+1.1	+1.6	+2.1	+2.7	+3.2	+2.8	+4.3	+4.8	10	

Table XI. is found in the Résumé des Observations Thermométrique et Baromériques faites à Genève et au Grand St. Bernard pendant les dix années 1841 à 1850, very elaborate paper by Professor E. Plantamour, Director of the Observatory at Geneva, published in Vol. XIII. of the Mémoires de la Société de Physique de Genève. The author, after having determined the difference of elevation between Geneva 407.0 metres above the level of the sea) and the Great St. Bernard, by means of he corresponding observations, made during these 10 years, and using his own tables given above, reversed the problem. Assuming the difference of level thus found, iz. 2066 metres, to be the true height of the layer of air between the two stations, and its weight being given by the barometrical observations, he deduced from these lata its mean density, and from the density its mean temperature at every even lour in every month of the year. Comparing these mean temperatures with those given at the same hours by the half-sum of the temperatures taken at the upper and he lower station, he found the differences contained in Table XI., which are the corections to be applied to the half-sums of the temperatures to obtain, in this particular ase, the true mean temperatures. The second part of the table has been computed y multiplying each temperature in the first by 7.5 metres, in order to show the value of that correction in barometrical measurements.

# TABLE XI.

CORRECTION TO BE APPLIED TO THE HALF-SUMS OF THE TEMPERATURES OF THE AIR,
OBSERVED AT GENEVA AND AT THE GREAT ST. BERNARD, TO OBTAIN THE TRUE
MEAN TEMPERATURE OF THE AIR BETWEEN THE TWO STATIONS.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
	0	0	0	0	0'	0	0	0	0	0	0	0	0
Noon.	-0.5	-1.7	-3.0	-3.9	-4.1	-4.4	-4.4	-3.8	-2.7	-1.6	-0.4	+0.7	-2.
2	-0.2	-1.5	-2.8	-3.7	-4.0	-4.4	-4.4	-3.8	-2.6	-1.5	-0.2	+0.7	-2.
4	+0.4	-0.6	-1.6	-2.5	-2.7	-3.4	-3.6	-2.9	-1.7	-0.7	+0.4	+1.3	-1.
6	+1.2	+0.7	-0.2	-0.9	-1.3	-2.1	-2.2	-1.6	-0.5	+0.4	+1.3	+2.1	-0.
8	+1.5	+1.4	+0.6	0.0	0.0	-0.6	-0.7	-0.5	+0.3	+1.3	+1.7	+2.6	+0.
10	+1.7	+1.5	+1.2	+0.6	+0.7	+0.5	-0.1	+0.1	+0.8	+1.7	+1.8	+2.6	+1.
Mid- night.	+1.9	+1.8	+1.9	+1.3	+1.8	+1.6	+0.9	+1.2	+1.3	+2.3	+2.1	+2.5	+1.
2	+2.0	+2.2	+2.5	+1.9	+2.2	+2.0	+1.5	+2.0	+1.9	+2.5	+2.4	+2.6	+2.
4	+2.3	+2.5	+2.6	+1.8	+1.7	+1.4	+1.1	+1.8	+2.1	+2.5	+2.7	+2.9	+2.
6	+2.0	+2.0	+1.7	+0.7	+0.4	+0.1	0.0	+0.7	+1.5	+1.7	+2.3	+2.9	+1.
8	+1.5	+1.1	0.0	-1.3	-2.0	-2.2	-2.4	-1.7	-0.4	+0.6	+1.7	+2.5	-0.
10	+0.4	-0.4	-2.0	-3.1	-3.5	-3.8	-3.7	-3.1	-2.0	-1.0	+0.3	+1.3	-1.
Mean,	+1.2	+0.8	+0.1	-0.8	-0.9	-1.2	-1.5	-0.9	-0.2	+0.7	+1.3	+2.1	0.0

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
TOWN.	The same		Alviera	5473	1965-19	Carte Cart	179 141						
Noon.	-3.7	-12.7	-22.5	-29.2	-30.7	-33.0	-33.0	-28.5	-20.2	-12.0	- 3.0	+ 5.2	-18.7
2	- 1.5	-11.2	-21.0	-27.7	-30.0	-33.0	-33.0	-28.5	-19.5	-11.2	- 1.5	+ 5.2	-17.2
4	+ 3.0	- 4.5	-12.0	-18.7	-20.2	-25.5	-27.0	-21.7	-12.7	- 5.2	+ 3.0	+ 9.7	-11.2
6	+ 9.0	+ 5.2	- 1.5	- 6.7	- 9.7	-15.7	-16.5	-12.0	- 3.7	+ 3.0	+ 9.7	+15.7	- 2.2
8	+11.2	+10.5	+ 4.5	0.0	0.0	- 4.5	- 5.2	- 3.7	+ 2.2	+ 9.7	+12.7	+19.5	+ 4.5
10	+12.7	+11.2	+ 9.0	+ 4.5	+ 5.2	+ 3.7	- 0.7	+ 0.7	+ 6.0	+12.7	+13.5	+19.5	+ 8.5
201	THE SELECTION OF S	7	ALL P	CHES.	and IX	opinic	444	DOM:	39 4 3884	20		Miller a	
Mid- night.	+14.5	+13.5	+14.5	+ 9.7	+13.5	+12.0	+ 6.7	+ 9.0	+ 9.7	+17.2	+15.7	+18.7	+12.7
2	+15.0	+16.5	+18.7	+14.2	+16.5	+15.0	+11.2	+15.0	+14.2	+18.7	+18.0	+19.5	+16.5
4	+17.2	+18.7	+19.5	+13.5	+12.7	+10.5	+ 8.2	+13.5	+15.7	+18.7	+20.2	+21.7	+15.7
6	1	1775	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1977222100	The state of the s			1.0720-1.112	F 7 / 2 / 2 / 2 / 2 / 2 / 2 / 2 / 2 / 2 /	102 S.S. 745 S.S. D.	CARL LA COLOR	+21.7	1
8		100000	1	Company of the Compan	The Assessment	A STEP SHOULD SEE STATE OF SECOND	The second second	- 1722000-1	Committee of the commit	CHARLEST LESSON	A DOMESTIC OF THE PARTY OF THE	+18.7	100000000000000000000000000000000000000
10												+ 9.7	
	7 11	A STATE	Eld of	30/8/34	No.	Helino	e việt	A TENT	Port Ger	nation.			
1	100	100		0.0	0.7		10000						0.0
Mean,	₹9.0	+6.0	+0.7	-6.0	-6.7	-9.0	-11.2	-6.7	-1.5	+5.2	+9.7	+15.7	0.0

The elevation of a place in the interior of a continent where regular meteorological observations are made, may be ascertained by taking the yearly means of the barometer reduced to the freezing point, and of the temperature of the air, as data for the upper station, and the yearly means of the reduced barometer and of the free thermometer at the level of the sea, as the data for the lower station. The Hypsometric Tables then will give the difference of level. As observation, however, has shown that the mean height of the barometer at the level of the sea is not the same in all latitudes, it is necessary to take for such a comparison the mean height of the barometer which belongs to the latitude of the station the elevation of which is to be computed, or that which is nearest to it.

Table XII., published by Schouw, in Poggendorf's Annalen, and in the Comptes Rendus de l'Académie des Sciences, Tom. III. p. 573, gives in Paris lines the mean height of the barometer in various latitudes. The reduction into millimetres is from Martins's French translation of Kaemtz's Meteorology, p. 278; the corresponding values in English inches, and the new stations, Savannah, Ga., Philadelphia, Pa., and Cambridge, Mass., have been added. The mean heights last mentioned have been derived from three years of observations at Savannah, by Dr. John F. Posey, from June, 1853, to June, 1856, published in the American Almanac; from four years of hourly observations at Girard College, Philadelphia, by Prof. A. D. Bache; and from ten years of observations at Cambridge Observatory. They have been reduced to a common absolute standard and to mean tide-water at the respective places.

These mean barometric heights, corrected for the variation of gravity in latitude, according to the proposition of Poggendorf, by the formula b=b 45 (1 — 0.0025935 cos 2  $\phi$ ), where b is the height of the barometer in latitude  $\phi$ , and b 45 the corresponding height at the forty-fifth degree of latitude, are found in another column. For computing the elevations, the uncorrected heights are to be used.

The mean barometric pressure, as shown by Table XIII. from Kaemtz's Précis de Météorologie, French translation, p. 281, is not the same in all seasons, and the monthly means differ by a quantity which also varies with the latitude. If, therefore, he height of an inland station is to be ascertained from the barometrical means of one or more months only, the computation must be made with the mean pressure in he corresponding months at the level of the sea; or if this is not known, the yearly means taken from Table XII. must be corrected for the difference between the monthly neans of the given month, or months, and the annual mean in the same latitude, as lerived from the comparison of the numbers in Table XIII.

## Example.

Suppose an inland station, in latitude 40° N.; the mean barometric pressure for July is 26.30 inches, and its elevation is to be computed from it.

Table XII. gives for latitude 40°, at Philadelphia, reduced to the level of the sea, 30.053 inches. Table XIII. gives as the mean for July, at the same place, 759.80 nillimetres, and for the year, 760.25 millimetres (both not reduced to the level of he sea), difference — 0.45 millimetres = — 0.017 English inches, which is to be subtracted from the annual mean, 30.053, to reduce it to the mean of July; or

30.053 - 0.017 = 30.036. This last number is to be used in the computation, with the mean temperature of July at both stations.

Towards the tropical regions, the irregular or non-periodic variations of the barometer, which in high and middle latitudes are so considerable as to render simultaneous observations indispensable for the measurement of heights, gradually decrease and nearly cease to exist, while the monthly and daily periodic variations, which are small in high latitudes, considerably increase. Within the tropics, therefore, the oscillations of the barometer being far more uniform, observations made during a short period of time, or even single observations, may be used for computing heights, without corresponding observations, by referring them to the mean pressure at the level of the sea as to a constant, provided this last has been corrected for the monthly and daily periodic variation at the place.

Table XIII. furnishes the means of applying the correction for the monthly variation, as described above. Table XIV., which gives the mean height of the barometer at all hours of the day in various latitudes, enables the observer to correct the data according to the hour at which the observations have been taken. This table is from Kaemtz's Vorlesungen über Meteorologie, French translation, p. 249. The column Bossekop is from the observations of the French Scientific Expedition in the North; the column Philadelphia, from the observations at Girard College, has been added.

The correction for the hourly variation is found by taking the difference between the mean of the hour of observation and the daily mean, and correcting accordingly, with due regard to the signs, either the yearly mean at the sea level, or the observation at the upper station.

### Example.

The barometer at Caracas, latitude 10° 30' N., on the 20th of August, at 4 o'clock P. M., reads 680.57 millimetres.

which is the number to be used for the computation of the height of Caracas. In this case, however, the monthly correction, being derived from a higher latitude, may be too small. Both corrections can of course be applied, with contrary signs, to the observation at Caracas, leaving then the mean height at the level of the sea as a constant.

Mean barometer at La Guayra in August, at 4 P. M. = 756.05 millimetres,

#### TABLE XII.

### MEAN HEIGHT OF THE BAROMETER,

IN VARIOUS LATITUDES, REDUCED TO THE LEVEL OF THE SEA, AND TO THE FREEZING POINT.

The state of		In Milli	metres.	In Englis	sh Inches.	In Pari	is Lines.
Places.	Latitude.	Observed.	Corrected for Gravity.	Observed.	Corrected for Gravity.	Observed.	Corrected for Gravity.
Cape of Good Hope,	o , 33 S.	763.01	762.20	30.041	30.008	338.24	337.88
Rio Janeiro, Brazil,	23 S.	764.03	762.65	30.080	30.026	338.69	338.08
Christiansborg, Guinea,	5 30N.	760.10	758.16	29.925	29.850	336.95	336.09
La Guayra, Venezuela,	10	760.17	758.32	29.928	29.855	336.98	336.16
St. Thomas, W. Indies,	19	760.51	758.95	29.942	29.881	337-13	336.44
Macao, China,	23	762.99	761.61	30.040	29.986	338.23	337.62
Teneriffe, Canary Isles,	28	764.21	763.10	30.087	30.044	338.77	338.28
Savannah, Georgia,	32	764.59	763.74	30.102	30.070	338.93	338.57
Funchal, Madeira,	32 30	765.18	764.34	30.126	30.093	339.20	338.83
Tripoli, Northern Africa,	33	767.41	766.60	30.214	30.182	340.19	339.83
Palermo, Sicily,	38	762.95	762.47	30.038	30.019	338.21	338.00
Philadelphia, Penn.	40	763.35	763.00	30.053	30.040	335.38	338.23
Naples, Italy,	41	762.34	762.06	30.014	30.003	337.94	337.82
Cambridge, Mass.	42	762.44	762.24	30.018	30.010	337.99	337.90
Florence, Italy,	43 30	761.93	761.81	29.997	29.993	337.76	337.71
Avignon, France,	44	762.02	761.95	30.001	29.998	337.80	337.77
Bologna, Italy,	44 30	762.18	762.13	30.007	30.005	337.87	337.85
Padua, Italy,	45	762.18	762.18	30.007	30.007	337.87	337.87
Paris, France,	49	761.41	761.68	29.978	29.988	337.53	337.65
London, England,	51 30	760.96	761.41	29.960	29.978	337.33	337.53
Altona, Denmark,	53 30	760.42	761.01	29.938	29.961	337.09	337.35
Dantzig, Prussia,	54 30	760.10	760.76	29.925	29.952	336.95	337.24
Königsberg, Prussia,	54 30	760.49	761.14	29.941	29.967	337.12	337.41
Apenrade, Denmark,	55	759.58	760.71	29.906	29.950	336.72	337.22
Edinburgh, Scotland,	56	758.25	759.00	29.853	29.882	336.13	336.46
Christiania, Norway,	60	758.64	759.63	29.868	29.908	336.30	336.71
Hardanger, Norway,	60	756.94	757.04	29.801	29.841	335.55	335.99
Bergen, Norway,	60	757.01	758.00	29.804	29.844	335.58	336.02
Reikiavig, Iceland,	64	752.00	753.20	29.607	29.654	333.36	333.89
Godthaab, S. Greenland,	64	751.94	753.13	29.605	29.651	333.33	333.86
Eyafiord, Iceland,	66	753.58	754.89	29.669	29.721	334.06	334.64
Godhavn, Disco, Greenl.	68	753.76	755.16	29.677	29.731	334.14	334.76
Upernavik, N. Greenl.	73	755.18	756.80	29.732	29.796	334.77	335.49
Melville Isl., Arct. Amer.	74 30	757.08	758.75	29.807	29.872	335.61	336.35
Spitzbergen,	75 30	756.76	758.48	29.794	29.862	335.47	336.23

#### XIII. MEAN HEIGHT OF THE BAROMETER, IN ALL MONTHS OF THE YEAR, IN VARIOUS LATITUDES.

Not reduced to the Level of the Sea.

Places,	HAVANA.	CAL- CUTTA.	MACAO.	CAIRO.	SA- VANNAH.	PHILA- DELPHIA.	CAM- BRIDGE.	PARIS.	ST. PE-
Latitude,	230 9'	220 331	220 11'.	30° 2′	320 51	390 581	420 231	48° 50′	590 56'
			745			201 201 201	X and a second		7. 24
Jan.	765.24	764.57	767.93	762.40	762.80	760.97	761.37	758.86	762.54
Feb.	760.15	758.86	767.01	66	763.76	759.63	760.90	759.09	763.10
March,	760.98	756.24	766.08	759.43	763.05	760.51	759.09	756.33	760.76
April,	759.58	753.83	761.93	760.10	763.10	760.05	759.37	755.18	761.19
May,	758.19	750.81	761.64	758.23	763.39	759.09	759.63	755.61	760.94
June,	760.67	748.10	757.31	754.42	764.37	759.22	758.91	757.28	759.83
July,	760.67	747.54	757.91	753.90	764.02	759.80	760.34	756.52	758.25
Aug.	757.33	748.53	757.91	754.06	765.54	760.54	761.11	756.74	759.94
Sept.	757.46	751.83	762.22	756.70	763.36	761.25	761.83	756.61	761.19
Oct.	758.19	755.25	763.37	759.70	763.13	760.68	761.07	754.42	760.52
Nov.	761.25	758.37	766.17	760.76	763.41	760.49	760.85	755.75	758.05
Dec.	763.62	760.59	768.65	761.82	761.12	760.82	760.80	755.09	760.22
Year,	760.28	754.54	763.18	758.32	763.41	760.25	760.44	756.46	760.57

#### XIV. MEAN HEIGHT OF THE BAROMETER, AT ALL HOURS OF THE DAY, IN VARIOUS LATITUDES.

			1101 16	duced to the	e Level of th	ie sea.			
Places,	PACIFIC OCEAN.	CUMANA.	LA GUAYRA.	CAL- CUTTA.	PHILADEL-	PADUA.	HALLE.	ST. PE- TERSBURG	Bosseroi
Latitude,	00 0'	10° 28′N.	10° 36′n.	22° 35′N.	39° 58′N.	45° 24'N.	51° 29'N.	59° 56'N.	69° 58'1
Observers,	Horner.	Hum- boldt.	Boussin- gault.	Balfour.	Bache.	Ciminello.	Kaemtz.	Kupffer.	Bravais.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
Midnight,	752.47	756.86	759.64	758.80	760.49	757.01	753.23	759.35	754.90
1	752.20	756.53	759.34	758.62	760.46	756.90	753.14	66	66
2	751.77	756.21	759.05	758.57	760.41	756.84	753.05	759.32	754.79
3	751.63	755.89	758.81	758.49	760.34	756.78	752.99	66	66
4	751.32	755.66	758.68	758.47	760.39	756.74	752.99	759.32	754.70
5	751.65	755.79	758.85	758.44	760.49	756.75	753.34	66	44
6	751.95	756.18	759.32	758.68	760.75	756.79	753.12	759.39	754.68
7	752.48	756.58	759.94	759.16	761.00	756.89	753.24	66	66
8	752.95	756.98	760.50	759.88	761.15	757.01	753.37	759.49	754.75
9	753.16	757.31	759.63	760.11	761.22	757.08	753.44	66	66
10	753.15	757.32	760.50	760.19	761.17	757.14	753.46	759.51	754.96
11	752.80	757.01	759.99	760.09	760.97	757.07	753.40	66	"
Noon,	752.35	756.57	759.41	759.61	760.56	757.02	753.29	759.47	755.01
1	751.87	755.99	758.91	759.22	760.13	756.85	753.11	66	66
2	751.55	755.47	758.41	758.39	759.83	756.67	752.99	759.38	754.96
3	751.15	755.14	758.12	758.12	759.65	756.54	752.89	66	66
4	751.02	754.96	758.05	757.91	759.65	756.47	753.84	759.32	754.82
5	751.31	755.14	758.10	757.93	759.70	756.46	752.86	66	66
6	751.71	755.41	758.40	758.01	759.85	756.50	752.91	759.31	754.87
7	751.93	755.81	758.90	758.02	760.08	756.63	753.02	66	66
8	752.35	756.21	759.19	758.54	760.31	756.79	753.14	759.32	754.89
9	752.74	756.59	759.69	759.24	760.49	756.92	753.24	66	66
10	752.85	756.87	759.93	759.33	760.59	757.02	753.31	759.36	754.92
11	752.86	757.15	759.98	759.09	760.72	757.02	753.29	66	"
Mean,	752.13	756.33	759.22	758.87	760.43	756.83	753.19	759.38	754.85

Table XIV. shows that, after all irregular variations of the barometer have been liminated, there remains a double period of rise and fall within the twenty-four ours, and that the amplitude of these daily oscillations is greatest within the tropics, and goes on diminishing towards the polar regions.

According to Kaemtz, the mean time of the daily maxima and minima, or the nean tropic hours for the northern hemisphere, are as follows:—

The minimum of the afternoon is reached at 7.05 P. M.

The maximum of the evening is reached at 10.11 P. M.

The minimum of the night is reached at 3.45 A. M.

The maximum of the morning is reached at 9.37 A. M.

Even in temperate and high latitudes these diurnal variations, though small, must be aken into account, if great accuracy is required, in reducing corresponding obserations made at a somewhat different hour to the time of the observation at the tation the height of which is to be determined. But in so doing, it must be rememered that the times of the minima and maxima change with the seasons, as is shown y Table XV. from Kaemtz, p. 251 of the French translation.

XV. TROPIC HOURS OF THE DAILY VARIATION OF THE BAROMETER AT HALLE. LAT.  $51^{\circ}~30'$  N.

Month.	Minimum, P. M.	, Maximum, Minimum, Maximu P. M. A. M. A. M		Maximum, A. M.	Month.	Minimum, P. M.	Maximum, P. M.	Minimum, A. M.	Maximum, A. M.
	h.	h.	h.	h.	IFT IT IN	h.	h.	h.	h.
Jan.	2.81	9.17	4.91	9.91	July,	5.21	11.04	3.04	8.73
Feb.	3.43	9.46	3.86	. 9.66	Aug.	4.86	10.66	3.06	8.96
March,	3.82	9.80	3.87	10.10	Sept.	4.55	10.45	3.45	9.71
April,	4.46	10.27	3.53	9.53	Oct.	4.17	10.24	3.97	10.07
May,	5.43	10.93	3.03	9.13	Nov.	3.52	9.85	4.68	10.08
June,	5.20	10.93	2.83	8.73	Dec.	3.15	9.11	4.91	10.18

This shifting of the times of maxima and minima with the seasons diminishes with he latitude, and tends to disappear towards the equator, with the inequality of the ays and nights. The elevation above the level of the sea also causes a change in ne tropic hours of the daily variation which is not yet sufficiently studied.

Table XIV. gives evidence that the amplitude of the hourly oscillation is greatest nder the equator, and gradually decreases towards the pole. Kaemtz computes its nean value in various latitudes and at the level of the sea, as follows:—

XV'. AMPLITUDE OF DAILY VARIATIONS IN VARIOUS LATITUDES.

Latitude.	Variation.	Latitude.	Variation.	Latitude.	Variation.	Latitude	Variation.
0 1	Millim.	0 1	Millim.	0 1	Millim.	0 1	Millim.
0 0	2.28	23 55	1.80	39 4	1.13	52 33	0.45
5 26 N.	2.26	29 28	1.58	43 34	0.90	57 17	0.23
17 52	2.03	34 26	1.35	48 1	0.67	62 25	0.00

The amplitude also decreases with the elevation, at least in our latitudes; it was bound to be on the Faulhorn, in Switzerland, 9000 feet above the sea level, 0.27 millimetres, while it was 0.90 millimetres at Geneva.

#### TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO THE LEVEL OF THE SEA, OR TO ANOTHER LEVEL.

To reduce barometric means taken at a given elevation to the height they would have if taken at the level of the sea, or barometric observations made at different elevations to a common level, in order to eliminate the influence of altitude in the comparison of barometric pressures, is a problem, the solution of which is often needed in meteorology.

For a complete and accurate reduction, embracing all cases, Tables IV. and V., by Dippe, given above, pages 54 et seq., may be used. But when the difference of height between the two stations, or above the sea-level, does not exceed a few hundred feet, the small tables XVI. to XIX., in three different scales, will be found more convenient.

Tables XVI. and XVII. have been computed from the constants of Laplace's formula, the barometric coefficient, including the correction for the decrease of gravity on a vertical, being respectively 60,345.51 English feet and 56,621.83 Paris feet; and the coefficient for expansion of moist air 0.00222 and 0.005.

In Table XVIII. the coefficient 18,420 metres, deduced from Regnault's experiments (see *Proceedings of the Amer. Assoc. for Adv. of Science*, 1857), and his coefficient for expansion of dry air, 0.003665, increased to 0.0039, in order to include the effect of moisture, have been used.

#### USE OF THE TABLES.

The correction for reducing the barometer to the level of the sea is found by the formula

$$C = \frac{f}{N} \times \frac{h'}{h},$$

where C is the correction required; f, the elevation of the station; N, the number in the tables; h', the reading of the barometer; h, the normal height of barometer at the sea-level.

## Example.

At Cambridge Observatory, Massachusetts, at 71.34 English feet above mean tide, the mean barometer is = 29.939 inches; the mean temperature 47°.3 Fahrenheit; what would be the height at the level of the sea?

In Table XVI. we take for 47°.3 = 90.49, or, in order to get the correction in a fraction of an inch, 904.9.

Then

$$C = \frac{71.34}{904.9} \times \frac{29.939}{30} = 0.079$$
, correction required;

and

29.939 + 0.079 = 30.018 inches, height of the barometer at the level of the sea.

It will be seen that the quantity represented by the second member can be neglected without causing a sensible error in the correction. In this case the error does not amount to .001; it scarcely would reach .002 for 250 feet of elevation; so that the reduction can be made in most cases by a simple division; viz.  $\frac{f}{N}$ .

# CVI. HEIGHT, IN ENGLISH FEET, OF A COLUMN OF AIR CORRESPONDING TO A TENTH OF AN ENGLISH INCH IN THE BAROMETER, AT TEMPERATURES BETWEEN 32° AND 100° FAHRENHEIT,

The Barometric Pressure at the Lower Station being = 30 English Inches.

Temper- ature of Air, Fahren.	Height in English Feet.	Temperature of Air, Fahren.	Height in English Feet.	Temperature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.
32°	87.51	46°	90.23	60°	92.95	74°	95.67	87°	98.20
33	87.70	47	90.42	61	93.15	75	95.87	88	98.40
34	87.90	48	90.62	62	93.34	76	96.06	89	98.59
35	88.09	49	90.81	63	93.53	77	96.26	90	98.79
36	88.28	50	91.01	64	93.73	78	96.45	91	98.98
37	88.48	51	91.20	65	93.92	79	96.65	92	99.17
38	88.67	52	91.40	66	94.12	80	96.84	93	99.37
39	88.87	53	91.59	67	94.31	81	97.04	94	99.56
40	89.06	54	91.78	68	94.51	82	97.23	95	99.76
41	89.26	55	91.98	69	94.70	83	97.42	96	99.95
42	89.45	56	92.17	70	94.90	84	97.62	97	100.15
43	89.65	57	92.37	71	95.09	85	97.81	98	100.34
44	89.84	58	92.56	72	95.29	86	98.01	99	100.54
45	90.03	59	92.76	73	95.48	87	98.20	100	100.73

XVII. HEIGHT, IN FRENCH FEET, OF A COLUMN OF AIR CORRESPONDING TO A PARIS LINE IN THE BAROMETER, AT TEMPERATURES OF THE AIR BETWEEN  $0^\circ$  AND  $34^\circ$  REAUMUR,

The Barometric Pressure at the Lower Station being = 337 Paris Lines.

Temper- ature of Air, Reaumur.	Height in French Feet.								
0°	73.08	7°	75.63	14°	78.19	21°	80.75	28°	83.31
1	73.44	8	76.00	15	78.56	22	81.11	29	83.67
2	73.81	9	76.36	16	78.92	23	81.48	30	84.04
3	74.17	10	76.73	17	79.29	24	81.85	31	84.40
4	74.54	11	77.10	18	79.65	25	82.21	32	84.77
5	74.90	12	77.46	19	80.02	26	82.58	33	85.13
6	75.27	13	77.83	20	80.38	27	82.94	34	85.50

XVIII. HEIGHT, IN METRES, OF A COLUMN OF AIR CORRESPONDING TO A MILLIMETRE IN THE BAROMETER, AT TEMPERATURES BETWEEN  $0^{\circ}$  AND  $39^{\circ}$  CENTIGRADE,

The Barometric Pressure at the Lower Station being = 760 Millimetres.

Temper- ature of Air, Centigr	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres.						
0°	10.54	8°	10.86	16°	11.19	24°	11.52	32°	11.85
1	10.58	9	10.91	17	11.23	25	11.56	33	11.89
2	10.62	10	10.95	18	11.28	26	11.60	34	11.93
3	10.66	11	10.99	19	11.32	27	11.64	35	11.97
4	10.70	12	11.03	20	11.36	28	11.69	36	12.01
5	10.74	13	11.07	21	11.40	29	11.73	37	12.06
6	10.78	14	11.11	22	11.44	30	11.77	38	12.10
7	10.82	15	11.15	23	11.48	31	11.81	39	12.14

Table XIX. gives, in metrical measure, the values of a millimetre in the barometer at different elevations and Centigrade temperatures. The values are derived from Laplace's constants, as in Tables XVI. and XVII.

This table may be used, as the preceding ones, for reducing barometrical observations to the level of the sea, and also to any other level by a similar process.

#### Example.

Suppose the barometer to read 700 millimetres at the altitude of 750 metres, the temperature of air being = 16° Centigrade; what would be the reading at a station lower by 350 metres, assuming the temperature of the air downwards to increase at the rate of 1° Centigrade for 185 metres?

The temperature of air at lower station will be  $16^{\circ} + 1^{\circ}.9 = 17^{\circ}.9$ 

The approximate height of barometer about 73 centimetres.

Then, in Table XIX. we find for 16° and 70 centimetres, 12.15 " for 17°.9 and 73 centimetres, 11.73

Mean 11.94

And

 $\frac{350}{11.94}$  = 29.31, or barometer at lower station 700 + 29.31 = 729.31 millimetres.

Delcros's tables, with these data, would give for the difference of level 349.76, instead of 350 metres; the corresponding error in the height of the barometrical column does not exceed 0.08 millimetre, and thus remains within the limits of error which may be expected in an ordinary observation.

The principal object of this table, however, is to furnish the scientific traveller with the means of readily computing on the spot approximate differences of level, by simply multiplying the difference between the readings of the barometer at each station by the half sum of the numbers in the table corresponding to the data given by the observations.

## Example.

Suppose the barometer at the lower station to read 732.5, and at the upper station 703.2 millimetres; the temperature of the air being respectively 18° and 16° Centigrade.

The difference of the barometers, supposed to be reduced to the same temperature, is 29.3 millimetres.

Then, Table XIX. gives for 18° Centigrade and 73 centimetres, 11.73

"for 16° Centigrade and 70 centimetres, 12.15

Half sum, or mean, 11.94

And,  $29.3 \times 11.94 = 349.8$  metres = difference of level required.

By the large tables of Delcros, we find for the same data 350.1 metres.

This table can be considered as a complement to Delcros's tables, and may save the traveller the trouble of carrying the larger tables.

A similar table in English measures is found above, at the end of the author's larger tables (Table VI.), page 48 of this series, and another, more extensive one, below, page 92, the use of which is explained by the examples just given.

XIX. HEIGHT, IN METRES, OF A COLUMN OF AIR, CORRESPONDING TO A MILLIMETRE IN THE BAROMETER, AT DIFFERENT TEMPERATURES AND ELEVATIONS.

Temper- ature of			Barome	eter at the	Lower Stat	tion, Readi	ng in Cent	imetres.		1
Air, Centig.	76	75	74	73	72	71	70	69	68	67
0	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metre
0	10.52	10.66	10.80	10.94	11.10	11.26	11.42	11.59	11.75	11.9
2	10.60	10.74	10.89	11.03	11.19	11.35	11.51	11.68	11.85	12.0
4	10.69	10.83	10.97	11.12	11.28	11.44	11.60	11.77	11.94	12.1
6	10.77	10.91	11.06	11.20	11.37	11.53	11.69	11.86	12.04	12.2
8	10.85	11.00	11.15	11.29	11.46	11.62	11.78	11.96	12.13	12.3
10	10.94	11.08	11.23	11.38	11.55	11.71	11.87	12.05	12.22	12.4
12	11.02	11.17	11.32	11.47	11.63	11.80	11.97	12.14	12.32	12.5
14	11.11	11.25	11.41	11.55	11.72	11.89	12.06	12.23	12.41	12.6
16	11.19	11.34	11.49	11.64	11.81	11.98	12.15	12.33	12.51	12.7
18	11.27	11.43	11.58	11.73	11.90	12.07	12.24	12.42	12.60	12.7
20	11.36	11.51	11.67	11.82	11.99	12.16	12.33	12.51	12.69	12.8
22	11.44	11.60	11.75	11.90	12.08	12.25	12.42	12.61	12.79	12.9
24	11.53	11.68	11.84	11.99	12.17	12.34	12.51	12.70	12.88	13.0
26	11.61	11.77	11.93	12.08	12.26	12.43	12.61	12.79	12.98	13.1
28	11.70	11.85	12.01	12.17	12.35	12.52	12.70	12.88	13.07	13.2
30	11.78	11.94	12.10	12.25	12.43	12.61	12.79	12.98	13.16	13.3
32	11.86	12.02	12.18	12.34	12.52	12.70	12.88	13.07	13.26	13.4
34	11.95	12.11	12.27	12.43	12.61	12.79	12.97	13.16	13.35	13.5
36	12.03	12.19	12.36	12.52	12.70	12.88	13.06	13.25	13.45	13.6
38	12.12	12.28	12.44	12.60	12.79	12.97	13.15	13.35	13.54	13.7
Temper- ature of Air,		0.5		V-01111	rometer in				<b>#</b> 6	
Centig.	66	65	64	63	62	61	60	59	58	57
0	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metre
.0	12.11	12.30	12.49	12.69	12.89	13.10	13.32	13.55	13.78	14.03
2	12.21	12.40	12.59	12.79	13.00	13.21	13.43	13.66	13.89	14.1
4	12.31	12.50	12.69	12.89	13.10	13.31	13.54	13.77	14.00	14.2
6	12.40	12.60	12.79	13.00	13.20	13.42	13.64	13.88	14.11	14.3
8	12.50	12.69	12.89	13.10	13.31	13.52	13.75	13.98	14.22	14.4
10	12.60	12.79	12.99	13.20	13.41	13.63	13.86	14.09	14.34	14.59
12	12.69	12.89	13.09	13.30	13.51	13.73	13.96	14.20	14.45	14.70
14	12.79	12.99	13.19	13.40	13.62	13.84	14.07	14.31	14.56	14.81
16	12.89	13.09	13.29	13.50	13.72	13.94	14.18	14.42	14.67	14.92
	12.98	13.19	13.39	13.61	13.82	14.05	14.28	14.53	14.78	15-0-
18	12.00	THE RESERVE AND DESCRIPTION OF THE PERSON NAMED IN	13.49	13.71	13.93	14.15	14.39	14.63	14.89	15.18
	13.08	13.28	10.40		400 Jan 1	14.26	14.50	14.74	15.00	15.26
13		13.28 13.38	13.59	13.81	14.03					
13 20	13.08	12 / million 1		13.81 13.91	14.03	14.36	14.60	14.85	15.11	15.37
13 20 22	13.08 13.18	13.38	13.59	The state of the state of	Company of the Control of the Contro	14.36 14.47	14.60 14.71	14.85 14.96	15.11 15.22	
18 20 22 24	13.08 13.18 13.27	13.38 13.48	13.59 13.69	13.91	14.13		The second second	The second second		15.48
13 20 22 24 26	13.08 13.18 13.27 13.37	13.38 13.48 13.58	13.59 13.69 13.79	13.91 14.01	14.13 14.24	14.47	14.71	14.96	15.22	15.48 15.60
18 20 22 24 26 28	13.08 13.18 13.27 13.37 13.47	13.38 13.48 13.58 13.68	13.59 13.69 13.79 13.89	13.91 14.01 14.11	14.13 14.24 14.34	14.47 14.57	14.71 14.82	14.96 15.07	15.22 15.33	15.48 15.60 15.71
18 20 22 24 26 28	13.08 13.18 13.27 13.37 13.47	13.38 13.48 13.58 13.68	13.59 13.69 13.79 13.89	13.91 14.01 14.11 14.22	14.13 14.24 14.34 14.44	14.47 14.57 14.68	14.71 14.82 14.92	14.96 15.07 15.18	15.22 15.33 15.44	15.37 15.48 15.60 15.71 15.82 15.93

XIX'. HEIGHT, IN ENGLISH FEET, OF A COLUMN OF AIR, CORRESPONDING TO A TENTH OF AN INCH IN THE BAROMETER, AT DIFFERENT TEMPERATURES AND ELEVATIONS.

Barometer				Ten	peratur	e of the	Air, Fahr	enheit, b	eing			
Reading in English Inches.	40°	450	500	550	600	65°	700	750	800	850	90°	95
22.0	121.5	122.8	124.2	125.5	126.8	128.2	129.5	130.8	132.1	133.5	134.8	136
22.2	120.4	121.7	123.1	124 4	125.7	127.0	128.3	129.6	130.9	132.2	133.6	134
22.4	119.3	120.6	121.9	123.2	124.6	125.9	127.2	128.5	129.8	131.1	132.4	133
22.6	118.2	119.5	120.8	122.1	123.4	124.7	126.0	127.3	128.6	129.9	131.2	132
22.8	117.2	118.5	119.8	121.1	122.3	123.6	124.9	126.2	127.5	128.8	130.0	131
23.0	116.2	117.5	118.7	120.0	121.3	122.6	123.8	125.1	126.4	127.6	129.9	130
23.2	115.2	116.5	117.7	119.0	120.2	121.5	122.7	124.0	125.3	126.5	127.8	129
23.4	114.2	115.5	116.7	118.0	119.2	120.5	121.7	123.0	124.2	125.4	126.7	127
23.6	113 2	114.4	115.7	116.9	118.1	119.4	120.6	121.8	123.1	124.3	125.5	126
23.8	112.3	113.5	114.8	116.0	117.2	118.4	119.7	120.9	122.1	123.3	124.6	125
24.0	111.4	112.6	113.8	115.0	116.2	117.4	118.7	119.9	121.1	122.3	123.5	124
24.2	110.5	111.7	112.9	114.1	115.3	116.5	117.7	118.9	120.1	121.3	122.5	123
24.4	109.5	110.7	111.9	113.1	114.3	115.5	116.7	117.9	119.1	120.3	121.5	122
24.6	108.6	109.8	111.0	112.2	113.4	114.6	115.8	116.9	118.1	119.3	120.5	121
24.8	107.8	108.9	110.1	111.3	112.5	113.7	114.8	116.0	117.2	118.4	119.5	120
25.0	106.9	108.1	109.2	110.4	111.6	112.7	113.9	115.1	116.2	117.4	118.6	119
25.2	106.0	107.2	108.4	109.5	110.7	111.8	113.0	114.1	115.3	116.5	117.6	118
25.4	105.2	106.4	107.5	108.7	109.8	111.0	112.1	113.3	114.4	115.6	116.7	117
25.6	104.4	105.5	106.7	107.8	108.9	110.1	111.2	112.4	113.5	114.6	115.8	116
25.8	103.6	104.7	105.8	107.0	108.1	109.2	110.4	111.5	112.6	113.8	114.9	116
26.0	102.8	103.9	105.0	106.1	107.3	108.4	109.5	110.6	111.8	112.9	114.0	115
26.2	102.0	103.1	104.2	105.3	106.5	107.6	108.7	109.8	110.9	112.0	113.1	114
26.4	101.2	102.3	103.4	104.6	105.7	106.8	107.9	109.0	110.1	111.2	112.3	113
26.6	100.5	101.6	102.7	103.8	104.9	106.0	107.1	108.2	109.3	110.4	111.4	112
26.8	99.7	100.8	101.9	103.0	104.1	105.2	106.3	107.4	108.5	109.5	110.6	111
27.0	99.0	100.1	101.2	102.2	103.3	104.4	105.5	106.6	107.6	108.7	109.8	110
27.2	98.3	99.3	100.4	101.5	102.6	103.6	104.7	105.8	106.8	107.9	109.0	110
27.4	97.5	98.6	99.7	100.7	101.8	102.9	103.9	105.0	106.1	107.1	108.2	109
27.6	96.8	97.9	98.9	100.0	101.1	102.1	103.2	104.2	105.3	106.3	107.4	108
27.8	96.1	97.2	98.2	99.3	100.3	101.4	102.4	103.5	104.5	105.6	106.6	107
28.0	95.4	96.5	97.5	98.6	99.6	100.6	101.7	102.7	103.8	104.8	105.9	106
28.2	94.8	95.8	96.8	97.9	98.9	99.9	101.0	102.0	103.0	104.1	105.1	106
28.4	94.1	95.1	96.1	97.2	98.2	99.2	100.2	101.3	102.3	103.3	104.3	105
28.6	:93.4	94.4	95.5	96.5	97.5	98.5	99.5	100.6	101.6	102.6	103.6	104
28.8	92.8	93.8	94.8	95.8	96.8	97.8	98.8	99.8	100.8	101.8	102.8	103
29.0	92.1	93.1	94.1	95.1	96.2	97.2	98.2	99.2	100.2	101.2	102.2	103
29.2	91.5	92.5	93.5	94.5	95.5	96.5	97.5	98.5	99.5	100.5	101.5	102
29.4	90.9	91.9	92.9	93.9	94.8	95.8	96.8	97.8	98.8	99.8	100.8	101
29.6	90.3	91.3	92.2	93.2	94.2	95.2	96.2	97.2	98.2	99.1	100.1	101
20.5	89.7	90.6	91.6	92.6	93.6	94.5	95.5	96.5	97.5	98.5	99.4	100
30.0	89.1	90.0	91.0	92.0	92.9	93.9	94.9	95.9	96.8	97.8	98.8	99
30.2	88.5	89.4	90.4	91.4	92.3	93.3	94.3	95.2	96.2	97.2	98.1	99
30.4	87.9	88.8	89.8	90.8	91.7	92.7	93.6	94.6	95.6	96.5	97.5	98.

When the Barometrical means to be used have been derived from observations taken at such hours of the day as, if combined, do not give the true mean pressure, they must be reduced to the true means by using the Tables XX. and XXI. These tables give the corrections to be applied to the hourly means, in each month, for reducing them to the means which would have been given by observations made at each of the twenty-four hours. The correction for any given set of hours is found by taking the mean of the corrections due to each of the combined hours, paying due attention to the signs. Table XX. has been computed from the hourly observations made under the superintendence of Professor A. D. Bache, at Girard College, Philadelphia. Table XXI. is from the Greenwich Observations, by Glaisher.

XX.

NORTH AMERICA. - PHILADELPHIA. Lat. 39° 58' N. Long. 75° 11' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Barometric Pressure of the respective Days, Months, and of the Year.

Barometer	in English	Inches.

Hour.	Jan.	Feb	March	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
									-				
2012.1.1.	Inch.	Inch.	Inch.		Inch.	Inch.	Inch.		Inch.	Inch.	Inch.	Inch.	Inch. 0024
Midnight.				7 45 47 61	The latest the same	COS. Sc., 511	1 2 3 4 11	19.5000000000	1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -				+.0007
1		The state of the s	100000	100	The second second	the state of the s	100 100 100 100	12000-1-0	1 1 2 2 2 1 1 1 1 1	the state of the state of	CONTRACTOR OF THE PARTY OF THE	2000	+.0007
2 3		The Part of the Section of the Secti		14									+.0036
3	008	T.002	₩.009	+.005	T.007	T.001	T.005	7.005	7.009	T.011	7.007	014	T.0030
4	003	+.003	+.009	+.002	+.003	+.002	.000	+.004	+.005	+.007	+.003	010	+.0038
5	003	.000	+.002	007	006	007	010	005	006	003	006	008	0050
6	009	004	011	020	019	022	019	017	016	012	012	015	0147
7	021	013	020	029	026	024	025	023	023	021	019	023	0222
	000	000	000	00.4	007	000	000	000	000	000	000	000	0000
8	the second of	The second	10, Var. 2 2	22.000,007		3 40 5 7 7 7	1000000	SCHOOL STREET	1-1275 - 5 TO	1		7-35-17-1	0290
9		Date of the contract of the co	I THE RESERVE	The state of the s		42.0		CONTRACTOR OF THE PARTY OF THE		1		-	0307
10		100	The same of the sa		7 7 1 5 1	2 1 2 1 2 1			0.00	1		10. TO 10.	0296
11	023	019	016	023	018	019	019	022	021	014	017	011	0185
Noon.	+.006	004	002	008	006	010	012	012	009	+.001	+.006	+.005	0037
1	+.028	+.017	+.014	+.006	+.005	.000	.000	.000	+.005	+.006	+.023	+.024	+.0107
2	+.037	+.032	+.031	+.021	+.017	+.011	+.011	+.012	+.020	+.028	+.033	+.034	+.0240
3	+.034	+.034	+.034	+.034	+.028	+.019	+.020	+.022	+.024	+.028	+.033	+.034	+.0287
										Jan 1		elient o	
4	A. C. Contract	1 1 1 1 1 1 1	Charles Street	COLUMN TO SERVICE		C. D. Chillian		200 C. L. C. C.	MATERIAL SECTION AND ADDRESS OF THE PARTY OF		10.00	-	+.0306
5					Contract of the Contract of th		A STATE OF THE STA	4	100000000000000000000000000000000000000			1 1 1 1 1 1 1 1	+.0267
6			4			100 March 1997							+.0202
7	+.003	+.006	+.007	+.022	+.016	+.018	+.021	+.018	+.016	+.001	002	+.018	+.0123
8	+.003	.000	003	+.009	+.002	+.010	+.014	+.008	+.007	009	006	+.013	+.0040
9													0027
10													0065
11													0064
		VALUE		0.00				1	130	100	-38		
6, 2, 10	+.008	+.005	+.003	001	007	005	004	002	.000	.000	+.004	+.009	+ .001
7, 2, 9													.000
1, 12, 3, 9													
	"						The Assessment of the Assessme		100 100				

XXI. England. — Greenwich. Lat. 51° 29' N.; Long. 0° 0'. Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours, to obtain the true Mean Barometric Pressure for the respective Months. — Glaisher.

English Inches.

	neng) o	11100111	TO THE	1450	En,	glish In	ches.	3000			( Epites	CAUSE	100
Hours.	Jan.	Feb.	March	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Hapita and	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
Midn	.000	001	002	008	005	.000	006	010	005	005	011	004	005
1	.001	.004	.013	.000	.002	.004	.000	.000	.000	.004	005	.001	.002
2	.002	.008	.020	.007	.004	.005	.003	.007	.005	.010	.003	.006	.007
3	.005	.012	.023	.010	.005	.004	.005	.011	.010	.015	.008	.010	.009
4	.011	.014	.022	.011	.005	.001	.005	.014	.012	.020	.013	.012	.012
5	.015	.015	.019	.011	.006	002	.006	.011	.014	.022	.016	.014	.012
6	.015	.012	.012	.006	.006	006	.002	.005	.010	.018	.015	.011	.009
7	.010	.007	.005	003	.006	010	004	.000	.001	.008	.010	.006	.003
8	.003	.000	004	008	.003	012	008	007	006	003	.003	.004	003
9	008	008	010	011	007	012	010	008	011	009	005	010	009
10	010	015	015	014	009	011	010	009	013	014	007	015	012
11	014	016	015	011	006	009	009	008	010	014	005	015	011
Noon:	005	012	010	008	002	006	006	005	005	010	.002	009	006
1	.002	006	005	004	.000	003	003	.000	.000	003	.007	.003	001
2	.005	.003	.000	.003	.003	.003	.001	.003	.004	.004	.011	.008	.004
3	.004	.006	003	.009	.006	.007	.005	.005	.008	.005	.010	.010	.006
4	.002	.008	.005	.004	.010	.013	.009	.009	.010	.003	.008	.009	.007
5	.000	.006	.004	.014	.014	.017	.013	.011	.011	.000	.004	.006	.008
6	003	.002	.000	.011	.015	.017	.013	.011	.006	005	.000	.002	.006
7	005	004	006	007	.010	.014	.010	.005		008	006	003	.000
8	006	000	019	00=	000	000	004	005	005	011	010	000	005
9	A 0.0 (15, 15)	1000	012 015	005 009	.000 006	.008		005	009	011	012 017	009	177.00
10	005			012	008			015	The same of	A STATE OF THE PARTY OF	019	010	777
11	004	005	012	012	008	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1		015			017	009	009
THE PARTY	.004	.003	.010	012	000	.002	.012	015	011	003	017	003	.003
0.0	000	000	000	000	0	00-	000	000	000	000	00-	000	000
6. 6	.006	.007	.006	.008	.011	.005	.008	.008	.008	.006	.007	.006	.008
7. 7 8. 8	002	.002 003	.000 008	005 006	.008	.002	.003 002	.002	.000 006	.000	.002 004	.002 001	.001 004
0. 0	002	003	008	006	.002	002	002	006	006	007	004	001	004
9. 9		LOW MARKET STATE	013	V / 5 5 THE LOCAL TO	TO SANTERE	1	005	54 M.T. 9 CS	C 00000	012		009	009
10.10	007	011	014	013	W. 64953	1	007	1000	012	013	013	012	011
7. 2. 9	.003	.001	003	003	.001	001	001	002	001	001	.001	.002	.001
6. 2. 8	.005	.003	.000	.001	.003	.002	.002	.001	.003	.004	.005	.004	.003
6. 2.10	.005	.003	.000	001	.000		001	002	.001	.003	.002	.003	.001
6. 2. 6	.006	.006	.004	.007	.008		.005	.006	.007	.006	.009	.007	.006
7. 2	.007	.005	.003	.000	.004	001	001	.002	.002	.006	.010	.007	.003
8. 2	.004	.002		002	100000000000000000000000000000000000000	004	100000	002	001	.000	.007	.006	.001
8. 1	.002		004	006	.001	The second second	006	003	003	003	.005	.003	002
7. 1	.006	.001	- 167	003	124-0	006	520000	.000	.000	.002	.008	.004	.001
9.12.3.9	004	005	008	005	002	002	003	004	004	007	002	004	004
		1				1							-

#### XXII. TABLE TO REDUCE, BY INTERPOLATION,

#### THE OBSERVATIONS TO THE SAME ABSOLUTE TIME.

#### DECIMALS OF AN HOUR.

Min.	Decimal.	Min.	Decimal.	Min.	Decimal.	Min.	Decimal.	Min.	Decimal.	Min.	Decimal.
0 3-72	2	Million .	200		25				48,0000		ORGANIE .
1	.017	11	.183	21	.350	31	.517	41	.683	51	.850
2	.033	12	.200	22	.367	32	.533	42	.700	52	.867
3	.050	13	.217	23	.383	33	.550	43	.717	53	.883
4	.067	14	.233	24	.400	34	.567	44	.733	54	.900
5	.083	15	.250	25	.417	35	.583	45	.750	55	.917
6	.100	16	.267	26	.433	36	.600	46	.767	56	.933
7	.117	17	.283	27	.450	37	.617	47	.783	57	.950
8	.133	18	.300	28	.467	38	.633	48	.800	58	.967
9	.150	19	.317	29	.483	39	.650	49	.817	59	.983
10	.167	20	.333	30	.500	40	.667	50	.833	60	1.000

#### TABLE FOR CORRECTION OF CURVATURE AND REFRACTION.

From a mountain, when furnished with a barometer, or with an apparatus for deermining the temperature of boiling water, and a pocket level, an observer can ind the elevations of distant points, which are in sight, but lower than the mountain tself on which he stands. He has only to seek, with the level, the point on the lope of the mountain which corresponds to the point at a distance that he wishes to etermine, and to take there a barometrical, or a boiling point observation. This bservation is to be calculated in the usual way, but the result must be corrected for ne curvature of the surface of the globe, and for the atmospheric refraction, by neans of the following Table.

This method, which furnishes the means of multiplying, without much trouble, ne measurements of heights, gives approximations which are sufficient for most f the purposes of Physical Geography. It may even seem preferable to direct neasurements for determining the mean elevation of certain physical lines, which re best estimated when seen from a distance; such as the upper limit of the rowth of trees, the limits of different kinds of vegetation, that of permanent snow, nat of the mean elevation of the crest of a mountain range, &c.

Table XXIII. is taken from Captain Lee's Collection of Tables and Formula, d edit., page 81.

#### XXIII. CORRECTIONS FOR CURVATURE AND REFRACTION.

Showing the Difference of the Apparent and True Level, in feet and decimals, for Distances in feet and miles.

	C	orrection in F	eet.		C	orrection in F	eet.
Distances				Distances			and No
in Feet.	For Curvature.	For Re- fraction.	For Curva- ture and Refraction.	in Miles.	For Curvature.	For Re- fraction.	For Curve ture and Refraction
100	.00024	.00004	.00020	14	.0417	.0060	.035
150	.00054	.00008	.00046	1 2	.1668	.0238	.1430
200	.00094	.00013	.00083	3 4	.3752	.0536	.321
250	.00149	.00021	.00128	1	.6670	.0953	.571
300	.00215	.00031	.00184	11/2	1.5008	.2144	1.286
350	.00293	.00042	.00251	2	2.6680	.3811	2.286
400	.00383	.00055	.00328	21/2	4.1688	-5955	3.573
450	.00484	.00069	.00415	3	6.0030	.8561	5.146
500	.00598	.00085	.00513	31/2	8.1708	1.1673	7.003
550	.00724	.00103	.00621	4	10.6720	1.5246	9.147
600	.00861	.00123	.00738	$4\frac{1}{2}$	13.5468	1.9295	11.577
650	.01010	.00144	.00866	5	16.6750	2.3821	14.2929
700	.01172	.00167	.01005	51/2	20.1769	2.8824	17.294
750	.01345	.00192	.01153	6	24.0120	3.4303	20.581
800	.01531	.00219	.01312	61/2	28.1809	4.0258	24.155
850	.01728	.00247	.01481	7	32.6830	4.6690	28.0143
900	.01938	.00277	.01661	71/2	37.5190	5.3599	32.159
950	.02159	.00308	.01851	8	42.6880	6.0997	36.5883
1000	.02392	.00333	.02059	81/2	48.1910	6.8844	41.3066
1050	.02638	.00377	.02261	9	54.0270	7.7181	46.3089
1100	.02895	.00414	.02481	91/2	60.1971	8.5996	51.5975
1150	.03164	.00452	.02712	10	66.7000	9.5286	57.1714
1200	.03445	.00492	.02953	11	80.7070	11.5296	69.1774
1250	.03738	.00534	.03204	12	96.0480	13.7211	82.3269
1300	.04043	.00578	.03465	13	112.7230	16.1033	96.6197
1350	.04361	.00623	.03738	14	130.7320	18.6760	112.0560
1400	.04689	.00670	.04019	15	150.0750	21.4393	128.6357
1450	.05030	.00719	.04311	16	170.7520	24.3931	146.3589
1500	.05383	.00769	.04614	17	192.7630	27.5376	165.2254
1550	.05748	.00821	.04927	18	216.1086	30.8727	185.2359
1600	.06125	.00875	.05250	19	240.7870	34.3981	206.3889
1650	.06514	.00931	.05583	20	266-8000	38-1143	228.6857
1700	.06914	.00988	.05926				THE PROPERTY.
1750	.07327	.01047	.06280	- 74	HE LINES	The east	
1800	.07752	.01107	.06645		the second	Paging a	
1850	.08188	.01170	.07018		A COURT OF	to (in unit)	
1900	.08637	.01234	.07403	1			
1950	.09098	.01300	.07798		48000		
2000	.09570	.01367	.08203				

## THERMOMETRICAL

## MEASUREMENT OF HEIGHTS,

OR

## TABLES

FOR DEDUCING DIFFERENCES OF LEVEL FROM OBSERVATIONS OF THE TEMPERATURE OF BOILING WATER.

#### THERMOMETRICAL MEASUREMENT OF HEIGHTS.

#### TABLES

FOR DEDUCING DIFFERENCES OF LEVEL FROM THE TEMPERATURE OF THE BOILING POINT OF WATER.

When water is heated in the open air, the elastic force of the vapors produced from it gradually increases, until it becomes equal to the incumbent weight of the atmosphere. Then, the pressure of the atmosphere being overcome, the steam escapes rapidly in large bubbles, and the water boils. The temperature at which, in the open air, water boils, thus depends upon the weight of the atmospheric column above it, and under a less barometric pressure the water will boil at a lower temperature than under a greater pressure. Now, as the weight of the atmosphere decreases with the elevation, it is obvious that, in ascending a mountain, the higher the station where an observation is taken, the lower the temperature at which water boils at that station will be.

The difference of elevation between two places, therefore, can be deduced from the temperature of boiling water observed at each station. It is only necessary to find the barometric pressures which correspond to those temperatures, and, the atmospheric pressures at both places being known, to compute the difference of level by a formula, or by the tables given above for computing heights from barometrical observations.

From the above, it may be seen that the heights determined by means of the temperature of boiling water are less reliable than those deduced from barometrical observations. Both derive the difference of altitude from the difference of atmospheric pressure. But the temperature of boiling water gives only indirectly the atmospheric pressure, which is given directly by the barometer. This method is thus liable to all the chances of error which may affect the measurements by means of the barometer, besides adding to them new ones peculiar to itself, the principal of which, not to speak of the differences exhibited in the various tables of the force of vapor, is the difficulty of ascertaining with the necessary accuracy the true temperature of boiling water. In the present state of thermometry it would hardly be safe, indeed, to answer, in the most favorable circumstances, for quantities so small as hundredths of degrees, even when the thermometer has been constructed with the utmost care; moreover, the quality of the glass of the instrument, the form and the substance of the vessel containing the water, the nature of the water itself, the place at which the bulb of the thermometer is placed, whether in the current of steam or in the water, - all these circumstances cause no inconsiderable variations to take place in the indications of thermometers observed under the same atmospheric

#### THERMOMETRICAL MEASUREMENT OF HEIGHTS.

pressure. Owing to these various causes, an observation of the boiling point, differing by one tenth of a degree from the true temperature, ought to be still admitted as good one. Now, as the tables show, an error of one tenth of a degree Centigrade in the temperature of boiling water would cause an error of 2 millimetres in the arometric pressure, or of from 70 to 80 feet in the final result, while with a good arometer the error of pressure will hardly ever exceed one tenth of a millimetre, taking a difference of 3 feet in altitude.

Notwithstanding these imperfections, the hypsometric thermometer, or thermo-arometer, is of the greatest utility to travellers traversing distant or rough countries, n account of its being more conveniently transported, and much less liable to ecidents than the mercurial barometer. The best form for it is that contrived and escribed by Regnault in the *Annales de Chimie et de Physique*, Tom. XIV. p. 202. consists of an accurate thermometer with long degrees, subdivided into tenths, whose ulb is placed, about 2 or 3 centimetres above the surface of the water, in the steam rising from distilled water in a cylindrical vessel, the water being made to boil by a pirit-lamp. The whole instrument when closed is about 6 inches long; when drawn at for observation, about 14 inches.

Table XXIV. of barometric pressures corresponding to temperatures of boiling ater, has been calculated by Regnault from his Tables of Forces of Vapor, and ablished in the *Annales de Chimie et de Physique*, Tom. XIV. p. 206. It gives, in aillimetres of mercury, the barometric pressures corresponding to every tenth of a entigrade degree; for greater convenience, the values for every hundredth have sen added.

The accuracy of this table has been tested by direct observation by Mr. Wisse, a aveller competent in such matters, who noted down simultaneously the temperares of the boiling point of water and the height of the barometer, in various parts the Andes, up to the summit of the volcano of Pichincha, including in his obsertions barometrical pressures ranging from 752 to 430 millimetres of mercury. he agreement between the barometric pressures given here by Regnault and those and by Wisse are very satisfactory, the differences never exceeding a few tenths a millimetre. See Annales de Chimie et de Physique, Tom. XXVIII. p. 123.

Table XXV. is the same table, revised by A. Moritz, who, in a communication to Académie des Sciences, in October, 1856, called the attention to some slight crors of computation in Regnault's table, and gave the corrected numbers for every pole degree from 40° to 102° Centigrade. Those numbers are given here from upwards, as published in the Journal de l'Institut; the values for every tenth of degree, and their differences, have been computed to fit the table for practical use. The comparison of the two tables will show that the corrections mostly amount to a we hundredths, and never exceed one tenth of a millimetre.

Table XXVI. is table XXV. reduced to English measures.

Centig.					Hundredths	of a Degr	ee.			
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millir
85.0	433.04	433.21	433.38	433.55	433.72	433.89	434.07	434.24	434.41	434.5
85.1	434.75	434.92	435.09	435.26	435.43	435.60	435.78	435.95	436.12	436.2
85.2	436.46	436.63	436.80	436.97	437.14	437.31	437.49	437.66	437.83	438.0
85.3	439.17	438.34	438.51	438.69	438.86	439.03	439.20	439.37	439.55	439.7
85.4	439.89	440.06	440.23	440.41	440.58	440.75	440.93	441.10	441.27	441.4
85.5	441.62	441.79	441.97	442.14	442.31	442.48	442.66	442.83	443.00	443.1
85.6	443.35	443.52	443.70	443.87	444.05	444.22	444.39	444.57	444.74	444.9
85.7	445.09	445.26	445.44	445.61	445.79	445.96	446.14	446.31	446.49	446.6
85.8	446.84	447.01	447.19	447.36	447.54	447.71	447.89	448.06	448.24	448.4
85.9	448.59	448.76	448.94	449.11	449.29	449.46	449.64	449.81	449.99	450.1
86.0	450.34	450.52	450.69	450.87	451.04	451.22	451.40	451.57	451.75	451.9
86.1	452.10	452.28	452.45	452.63	452.81	452.98	453.16	453.34	453.52	453.6
86.2	453.87	454.05	454.22	454.40	454.58	454.75	454.93	455.11	455.29	455.4
86.3	455.64	455.82	456.00	456.17	456.35	456.53	456.71	456.89	457.06	457.2
86.4	457.42	457.60	457.78	457.96	458.14	458.31	458.49	458.67	458.85	459.0
86.5	459.21	459.39	459.57	459.75	459.93	460.10	460.28	460.46	460.64	460.8
86.6	461.00	461.18	461.36	461.54	461.72	461.90	462.08	462.26	462.44	462.6
86.7	462.80	462.98	463.16	463.34	463.52	463.70	463.88	464.06	464.24	464.4
86.8	464.60	464.78	464.96	465.14	465.32	465.50	465.69	465.87	466.05	466.2
86.9	466.41	466.59	466.77	466.95	467.13	467.31	467.50	467.68	467.86	468.0
87.0	468.22	160 10	100 70	400 80	400.05	400 10	400 07	100 10	100.00	100.0
87.1	470.04	468.40	468.58	468.77	468.95	469.13	469.31	469.49	469.68	469.8
87.2	471.87	472.05	472.24	470.59	470.77	472.78	471.14	471.32	471.50 473.33	471.6
87.3	473.70	473.88	474.07	474.25	474.44	474.62	474.80	474.99	475.17	475.3
87.4	475.54	475.72	475.91	476.09	474.44	476.46	476.64	476.83	477.01	477.2
	110104	410.12	470.51	470.09	410.20	470.40	470.04	410.00	477.01	4/1.2
87.5	477.38	477.56	477.75	477.93	478.12	478.30	478.49	478.67	478.86	479.0
87.6	479:23	479.41	479.60	479.78	479.97	480.15	480.34	480.52	480.71	480.8
87.7	481.08	481.27	481.45	481.64	481.82	482.01	482.20	482.38	482.57	482.7
87.8	482.94	483.13	483.31	483.50	483.69	483.87	484.06	484.25	484.44	484.6
87.9	484.81	485.00	485.19	485.37	485.56	485.75	485.94	486.13	486.31	486.5
88.0	486.69	486.88	487.07	487.25	487.44	487.63	487.82	488.01	488.19	488.3
88.1	488.57	488.76	488.95	489.13	489.32	489.51	489.70	489.89	490.07	490.2
88.2	490.45	490.64	490.83	491.02	491.21	491.39	491.58	491.77	491.96	492.1
88.3	492.34	492.53	492.72	492.91	493.10	493.29	493.48	493.67	493.86	494.0
88.4	494.24	494.43	494.62	494.81	495.00	495.19	495.39	495.58	495.77	495.90
88.5	496.15	496.34	106 59	406 70	406.07	107 10	107 00	107 10	40,00	40* 0
88.6	498.06	498.25	496.53	496.72	496.91	497.10	497.30	497.49	497.68	497.8
88.7	499.98	500.17	500.36	498.64	498.83	499.02	499.21	499.40	499.60	499.79
88.8	501.90	502.09	502.28	500.56	500.75	500.94	501.13	501.32	501.52	501.7
88.9	503.82	504.01	504.21	504.40	504.60	504.79	504.98	503.24   505.18	503.44	505.5
	0.	1.	2.	3.						9.

Centig.				Н	lundredths	of a Degre	ee.			
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
89.0	505.76	505.95	506.15	506.34	506.54	506.73	506.92	507.12	507.31	507.5
89.1	507.70	507.89	508.09	508.28	508.48	508.67	508.87	509.06	509.26	509.4
89.2	509.65	509.84	510.04	510.23	510.43	510.62	510.82	511.01	511.21	511.4
89.3	511.60	511.80	511.99	512.19	512.38	512.58	512.78	512.97	513.17	513.3
89.4	513.56	513.76	513.95	514.15	514.35	514.54	514.74	514.94	515.14	515.3
89.5	515.53	515.73	515.92	516.12	516.32	516.51	516.71	516.91	517.11	517.3
89.6	517.50	517.70	517.90	518.09	518.29	518.49	518.69	518.89	519.08	519.2
89.7	519.48	519.68	519.88	520.07	520.27	520.47	520.67	520.87	521.06	521.2
89.8	521.46	521.66	521.86	522.06	522.26	522.46	522.66	522.86	523.05	523.2
89.9	523.45	523.65	523.85	524.05	524.25	524.45	524.65	524.85	525.05	525.2
90.0	525.45	525.65	525.85	526.05	526.25	526.45	526.65	526.85	527.05	527.2
90.1	527.45	527.65	527.85	528.05	528.25	528.45	528.66	528.86	529.06	529.2
90.2	529.46	529.66	529.86	530.07	530.27	530.47	530.67	530.87	531.08	531.2
90.3	531.48	531.68	531.88	532.09	532.29	532.49	532.69	532.89	533.10	533.3
90.4	533.50	533.70	533.91	534.11	534.31	534.51	534.72	534.92	535.12	535.3
90.5	535.53	535.73	535.94	536.14	536.35	536.55	536.75	536.96	537.16	537.3
90.6	537.57	537.77	537.98	538.18	538.39	538.59	538.79	539.00	539.20	539.4
90.7	539.61	539.81	540.02	540.22	540.43	540.63	540.84	541.04	541.25	541.4
90.8	541.66	541.87	542.07	542.28	542.48	542.69	542.90	543.10	543.31	543.5
90.9	543.72	543.93	544.13	544.34	544.54	544.75	544.96	545.16	545.37	545.5
91.0	545.78	545.99	546.19	546.40	546.61	546.81	547.03	547.23	547.44	547.6
91.1	547.85	548.06	548.26	548.47	548.68	548.88	549.09	549.30	549.51	549.7
91.2	549.92	550.13	550.34	550.54	550.75	550.96	551.17	551.38	551.58	551.7
91.3	552.00	552.21	552.42	552.63	552.84	553.04	553.25	553.46	553.67	553.8
91.4	554.09	554.30	554.51	554.72	554.93	555.14	555.35	555.56	555.77	555.9
91.5	556.19	556.40	556.61	556.82	557.03	557.24	557.45	557.66	557.87	558.0
91.6	558.29	558.50	558.71	558.92	559.13	559.34	559.55	559.76	559.97	560.1
91.7	560.39	560.60	560.81	561.03	561.24	561.45	561.66	561.87	562.09	562.3
91.8	562.51	562.72	562.93	563.15	563.36	563.57	563.78	563.99	564.21	564.45
91.9	564.63	564.86	565.06	565.27	565.48	565.69	565.91	566.12	566.33	566.5
92.0	566.76	566.97	567.19	567.40	567.61	567.85	568.04	568.25	568.46	568-68
92.1	568.89	569.10	569.32	569.53	569.75	569.96	570.17	570.39	570.60	570.8
92.2	571.03	571.24	571.46	571.67	571.89	572.10	572.32	572.53	572.75	572.90
92.3	573.18	573.40	573.61	573.83	574.04	574.26	574.48	574.69	574.91	575.12
92.4	575.34	575.56	575.77	575.99	576.20	576.42	576.64	576.85	577.07	5.77-28
92.5	577.50	577.72	577.93	578.15	578.37	578.58	578.80	579.02	579.24	579.4
92.6	579.67	579.89	580.10	580.32	580.54	580.75	580.97	581.19	581.41	581.62
92.7	581.84	582.06	582.28	582.49	582.71	582.93	583.15	583.37	583.58	583.80
92.8	584.02	584.24	584.46	584.68	584.90	585.11	585.33	585.55	585.77	585.99
92.9	586.21	586.43	586.65	586.87	587.09	587.31	587.53	587.75	587.97	588.19
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centig.			9 10	- I	Hundredths	of a Degr	ee.			
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
93.0	588.41	588.63	588.85	589.07	589.29	589.51	589.73	589.95	590.17	590.39
93.1	590.61	590.83	591.05	591.27	591.49	591.71	591.94	592.16	592.38	592.60
93.2	592.82	593.04	593.26	593.49	593.71	593.93	594.15	594.37	594.60	594.82
93.3	595.04	595.26	595.48	595.71	595.93	596.15	596.37	596 59	596.82	597.04
93.4	597.26	597.48	597.71	597.93	598.15	598.37	598.60	598.82	599.04	599.27
93.5	599.49	599.71	599.94	600.16	600.38	600.60	600.83	601.05	601.27	601.50
93.6	601.72	601.94	602.17	602.39	602.62	602.84	603.07	603.29	603.52	603.74
93.7	603.97	604.19	604.42	604.64	604.87	605.09	605.32	605.54	605.77	605.99
93.8	606-22	606.45	606.67	606.90	607.12	607.35	607.58	607.80	608.03	608.25
93.9	608.48	608.71	608.93	609.16	609.38	609-61	609.84	610.06	610.29	610.51
94.0	610.74	610.97	611.19	611.42	611.65	611.87	612.10	612.33	612.56	612.78
94.1	613.01	613.24	613.47	613.69	613.92	614.15	614.38	614.61	614.83	615.06
94.2	615.29	615.52	615.75	615.97	616.21	616.43	616.66	616.89	617.12	617.35
94.3	617.58	617.81	618.04	618.27	618.50	618.72	618.95	619.18	619.41	619.64
94.4	619.87	620.10	620.33	620.56	620.79	621.02	621.25	621.48	621.71	621.94
94.5	622.17	622.40	622.63	622.86	623.09	623.32	623.56	623.79	624.02	624.25
94.6	624.48	624.71	624.94	625.17	625.40	625.63	625.87	626.10	626.33	626.56
94.7	626.79	627.02	627.25	627.49	627.72	627.95	628.18	628.41	628.65	628.88
94.8	629.11	629.34	629.58	629.81	630.04	630.27	630.51	630.74	630.97	631.21
94.9	631.44	631.67	631.91	632.14	632.38	632.61	632.84	633.08	633.31	633.55
95.0	633.78	634.01	634.25	634.48	634.72	634.95	635.18	635.42	635.65	635.89
95.1	636.12	636.35	636.59	636.82	637.06	637.29	637.53	637.76	638.00	638.23
95.2	638.47	638.71	638.94	639.18	639.41	639.65	639.89	640.12	640.36	640.59
95.3	640.83	641.07	641.30	641.54	641.77	642.01	642.25	642.48	642.72	642.95
95.4	643.19	643.43	643.67	643.90	644.14	644.38	644.62	644.86	645.09	645.33
95.5	645.57	645.81	646.05	646.28	646.52	646.76	647.00	647.24	647.47	647.71
95.6	647.95	648.19	648.43	648.67	648.91	649.14	649.38	649.62	649.86	650.10
95.7	650.34	650.58	650.82	651.06	651.30	651.53	651.77	652.01	652.25	652.49
95.8 95.9	652.73 655.13	652.97	653.21	653.45	653.69	653.93	654.17	654.41	654.65	654.89
93.9	055.15	655.37	655.61	655.85	656.09	656.33	656.58	656.82	657.06	657.30
96.0	657.54	657.78	658.02	658.26	658.50	658.74	658.99	659.23	659.47	659.71
96.1	659.95	660.19	660.43	660.68	660.92	661.16	661.40	661.64	661.89	662.13
96.2	662.37	662.61	662.86	663.10	663.34	663.58	663.83	664.07	664.31	664.56
96.3	664.80	665.04	665.29	665.53	665.78	666.02	666.26	666.51	666.75	667.00
96.4	667.24	667.48	667.73	667.97	668.22	668.46	668.71	668.95	669.20	669.44
96.5	669.69	669.93	670.18	670.42	670.67	670.91	671.16	671.40	671.65	671.99
96.6	672.14	672.39	672.63	672.88	673.12	673.37	673.62	673.86	674.11	674.35
96.7	674.60	674.85	675.09	675.34	675.59	675.83	676.08	676.33	676.58	676.82
96.8	677.07	677.32	677.57	677.81	678.06	678.31	678.56	678.81	679.05	679.30
96.9	679.55	679.80	680.05	680.29	680.54	680.79	681.04	681.29	681.53	681.78
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

				V W W E	Iundredths	of a Degre	ев.			
Centig. Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	S.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
97.0	682.03	682.28	682.53	682.78	683.03	683.27	683.52	683.77	684.02	684.27
97.1	684.52	684.77	685.02	685.27	685.52	685.77	686.02	686.27	686.52	686.77
97.2	687.02	687.27	687.52	687.77	688.02	688.27	688.53	688.78	689.03	689.28
97.3	689.53	689.78	690.03	690.28	690.53	690.78	691.04	691.29	691.54	691.79
97.4	692.04	692.29	692.54	692.80	693.05	693.30	693.55	693.80	694.06	694.31
97.5	694.56	694.81	695.06	695.32	695.57	695.82	696.07	696.32	696.58	696.83
97.6	697.08	697.33	697.59	697.84	698.09	698.34	698.60	698.85	699.10	699.36
97.7	699.61	699.86	700.12	700.37	700.63	700.88	701.13	701.39	701.64	701.90
97.8	702.15	702.40	702.66	702.91	703.17	703.42	703.68	703.93	704.19	704.44
97.9	704.70	704.96	705.21	705.47	705.72	705.98	706.24	706.49	706.75	707.00
98.0	707.26	707.52	707.77	708.03	708.28	708.54	708.80	709.05	709.31	709.56
98.1	709.82	710.08	710.33	710.59	710.85	711.10	711.36	711.62	711.88	712.13
98.2	712.39	712.65	712.91	713.16	713.42	713.68	713.94	714.20	714.45	714.71
98.3	714.97	715.22	715.49	715.75	716.01	716.26	716.52	716.78	717.04	717.30
98.4	717.56	717.82	718.08	718.34	718.60	718.85	719.11	719.37	719.63	719.89
98.5	720.15	720.41	720.67	720.93	721.19	721.45	721.71	721.97	722.23	722.49
98.6	722.75	723.01	723.27	723.53	723.79	724.05	724.31	724.57	724.83	725.09
98.7	725.35	725.61	725.87	726.13	726.39	726.65	726.92	727.18	727.44	727.70
98.8	727.96	728.22	728.48	728.75	729.01	729.27	729.53	729.79	730.06	730.32
98.9	730.58	730.84	731.11	731.37	731.63	731.89	732.16	732.42	732.68	732.95
99.0	733.21	733.47	733.74	734.00	734.27	734.53	734.79	735.06	735.32	735.59
99.1	735.85	736.11	736.38	736.64	736.91	737.17	737.44	737.70	737.97	738.23
99.2	738.50	738.77	739.03	739.30	739.56	739.83	740.10	740.36	740.63	740.89
99.3	741.16	741.43	741.69	741.96	742.23	742.49	742.76	743.03	743.30	743.56
99.4	743.83	744.10	744.36	744.63	744.90	745.16	745.43	745.70	745.97	746.23
99.5	746.50	746.77	747.04	747.30	747.57	747.84	748.11	748.38	748.64	748.91
99.6	749.18	749.45	749.72	749.99	750.26	750.52	750.79	751.06	751.33	751.60
99.7	751.87	752.14	752.41	752.68	752.95	753.22	753.49	753.76	754.03	754.30
99.8	754.57	754.84	755.11	755.38	755.65	755.92	756.20	756.47	756.74	757.01
99.9	757.28	757.55	757.82	758.10	758.37	758.64	758.91	759.18	759.46	759.73
100.0	760.00	760.27	760.55	760.82	761.09	761.36	761.64	761.91	762.18	762.46
100.1	762.73	763.00	763.28	763.55	763.82	764.09	764.37	764.64	764.91	765.19
100.2	765.46	765.73	766.01	766.28	766.56	766.83	767.10	767.38	767.65	767.93
100.3	768.20	768.47	768.75	769.02	769.30	769.57	769.85	770.12	770.40	770.67
100.4	770.95	771.23	771.50	771.78	772.05	772.33	772.61	772.88	773.16	773.43
100.5	773.71	773.99	774.26	774.54	774.82	775.09	775.37	775.65	775.93	776.20
100.6	776.48	776.76	777.04	777.31	777.59	777.87	778.15	778.43	778.70	778.98
100.7	779.26	779.54	779.82	780.09	780.37	780.65	780.93	781.21	781.48	781.76
100.8	782.04	782.32	782.60	782.88	783.16	783.43	783.71	783.99	784.27	784.55
100.9	784.83	785.11	785.39	785.67	785.95	786.23	786.51	786.79	787.07	787.35
101.0	787.63	787.91	788.19	788.47	788.75	789.03	789.31	789.59	789.87	790.15
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

#### TABLE XXV.

## BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF THE BOILING POINT OF WATER,

#### . EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES.

By REGNAULT, REVISED BY MORITZ.

Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.
0			0	THE RESERVE		0	Terror	7
80.0	354.62		83.0	400.07		86.0	450.30	
80.1	356.06	1.44	83.1	401.66	1.60	86.1	452.06	1.76
80.2	357.50	1.45	83.2	403.26	1.60	86.2	453.83	1.77
80.3	358.96	1.45	83.3	404.87	1.61	86.3	455.60	1.77
80.4	360.41	1.46	83.4	406.48	1.61	86.4	457.38	1.78
	AND ILLA	1.46		HUTES IN	1.62	T-10.133	Litezine (B)	1.78
80.5	361.87	A MEDICAL	83.5	408.10	ad Line	86.5	459.17	
80.6	363.34	1.47	83.6	409.72	1.62	86.6	460.96	1.79
80.7	364.81	1.47	83.7	411.35	1.63	86.7	462.75	1.80
80.8	366.29	1.48	83.8	412.98	1.63	86.8	464.55	1.80
80.9	367.77	1.48	83.9	414.62	1.64	86.9	466.36	1.81
		1.49	Slevio	un Wit Line	1.64	TO THE OWN	400.00	1.81
81.0	369.26	L Wedler	84.0	416.26	rate of the	87.0	468.17	Aug Se
81.1	370.75	1.49	84.1	417.91	1.65	87.1	469.99	1.92
81.2	372.25	1.50	84.2	419.57	1.66	87.2	471.82	1.83
81.3	373.75	1.50	84.3	421.23	1.66	87.3	473.65	1.83
81.4	375.25	1.51	84.4	422.89	1.67	87.4	475.49	1.84
		1.51	04.4	444.03	1.67	07.4	475.49	1.84
81.5	376.77	A Ace.	84.5	424.56		87.5	477 00	
81.6	378.28	1.52	84.6	426.24	1.68	87.6	477.33	1.85
81.7	379.81	1.52	84.7	427.92	1.68	87.7	479.18	1.86
81.8	381.33	1.53	84.8	427.52	1.69		481.04	1.86
81.9	382.87	1.53	84.9	429.01	1.69	87.8	482.90	1.87
	002.01	1.54	04.9	431.30	1.70	87.9	484.76	1.87
82.0	384.40	1000	85.0	499.00	THE PARTY	00.0	10000	- Miles
82.1	385.95	1.54	85.1	433.00	1.70	88.0	486.64	1.88
82.2	387.49	1.55	85.1	434.71	1.71	88.1	488.52	1.89
\$2.3	389.05	1.55	85.2 85.3	436.42	1.72	88.2	490.40	1.89
82.4	390.61	1.56	-	438.13	1.72	88.3	492.29	1.90
	000.01	1.56	85.4	439.85	1.73	88.4	494.19	1.90
82.5	392.17	W Mark	05.5	447.00	1000			
82.6	393.74	1.57	85.5	441.58	1.73	88.5	496.09	1.91
82.7	395.31	1.57	85.6	443.31	1.74	88.6	498.00	1.92
82.8	396.89	1.58	85.7	445.05	1.74	88.7	500.92	1.92
82.9	398.48	1.58	85.8	446.80	1.75	88.8	501.84	1.93
83.0	400.07	1.59	85.9	448.55	1.76	88.9	503.77	1.93

Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres.	Difference.
11.45 144	222.07	OM WAS	r or o	ere konus	1000 9			EDET
89.0	505.70	3	93.0	F00 99	11/2	97.0	681.93	4 T/11
89.1	507.65	1.94	93.1	588.33	2.20	97.1	684.42	2.49
89.2	509.59	1.95	93.1	590.53	2.21	97.1	686.92	2.50
89.3	511.54	1.95	93.3	592.74 594.96	2.22	97.3	689.42	2.51
89.4	513.50	1.96	93.4	594.96	2.22	97.4	691.94	2.51
03.4	919.00	1.97	30.4	997.10	2:23	31.4	091.94	2.52
89.5	515.47		93.5	599.41		97.5	694.46	
89.6	517.44	1.97	93.6	601.65	2.24	97.6	696.98	2.53
89.7	519.42	1.98	93.7	603.89	2.24	97.7	699.52	2.54
89.8	521.40	1.98	93.8	606.14	2.25	97.8	702.06	2.54
89.9	523.39	1.99	93.9	608.40	2.26	97.9	704.62	2.55
march.		2.00		LEWS -44-	2.26			2.56
90.0	525.39	0.00	94.0	610.66	0.00	98.0	707.17	
90.1	527.40	2.00	94.1	612.93	2.27	98.1	709.74	2.57
90.2	529.41	140-70-	94.2	615.21	2.28	98.2	712.31	2.57
90.3	531.42	2.02	94.3	617.50	2.29	98.3	714.90	2.58
90.4	533.44	2.02	94.4	619.79	2.29	98.4	717.49	2.59
5000	100000000000000000000000000000000000000	2.03	20.00	No.	2.30		W. William	2.60
90.5	535.47		94.5	622.09	0.01	98.5	720.08	
90.6	537.51	2.04	94.6	624.39	2.31	98.6	722.69	2.61
90.7	539.55	1000	94.7	626.71	2.31	98.7	725.30	2.61
90.8	541.60	2.05	94.8	629.93	2.32	98.8	727.93	2.62
90.9	543.65	2.05	94.9	631.36	2.33	98.9	730.55	2.63
Marwi "	20-15-0-0-1-US	2.00	otolis (		2.33	1. 1. 1. 1. 1. 1.	CO. E. Silling	2.64
91.0	545.71	0.05	95.0	633.69	0.04	99.0	733.19	
91.1	547.78	2.07	95.1	636.03	2.34	99.1	735.84	2.64
91.2	549.86	2.07	95.2	638.38	2.35	99.2	738.49	2.65
91.3	551.94		95.3	640.74	2.36	99.3	741.15	2.66
91.4	554.03	2.09	95.4	643.10	2.36	99.4	743.82	2.67
ARREST N	0855063-001	2.09	ANTAL		2.87			2.68
91.5	556.12	2.10	95.5	645.48	2.38	99.5	746.50	0.40
91.6	558.22	2.10	95.6	647.86	2.39	99.6	749.18	2.68
91.7	560.33	2.11	95.7	650.24	2.39	99.7	751.87	2.69
91.8	562.44	2.12	95.8	652.63	The state of the s	99.8	754.57	2.70
91.9	564.56	2.12	95.9	655.04	2.40	99.9	757.28	2.71
428.		2.10	= 1100000		4.41			2.12
92.0	566.69	2.13	96.0	657.44	2.42	100.0	760.00	2.73
92.1	568.82	2.13	96.1	659.86	2.42	100.1	762.73	2.73
92.2	570.96	2.14	96.2	662.28	2.42	100.2	765.46	2.73
92.3	573.11	2.15	96.3	664.71	2.44	100.3	768.20	2.74
92.4	575.27	2.16	96.4	667.15	2.44	100.4	770.95	2.76
1000	4,01	2.10		1000		A CHEST	State of the state	2.10
92.5	577.43	2.17	96.5	669.59	2.45	100.5	773.71	2.77
92.6	579.59	2.17	96.6	672.05	2.46	100.6	776.47	2.77
92.7	581.77	2.18	96.7	674.51	2.47	100.7	779.25	2.78
92.8	583.95	2.19	96.8	676.97	2.47	100.8	782.03	2.79
92.9	586.14	2.19	96.9	679.45	2.48	100.9	784.82	2.60
93.0	588.33	Charles b	97.0	681.93	2.40	101.0	787.62	2.00

#### TABLE XXVI.

## BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF THE BOILING POINT OF WATER,

#### EXPRESSED IN ENGLISH INCHES FOR TEMPERATURES OF FAHRENHEIT.

REDUCED FROM REGNAULT'S TABLE, REVISED BY MORITZ.

		- MANUE	4			mh=	510	G - PAY	1111/-0		165
Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Difference.	Boiling Point, Fahren.	Barom- eter in English Inches,	Difference.	Boiling Point, Fahren.	Barom- eter in English Inches.	Diffe
0	17.564	(21)	0	92 -	195	0	distribution in	11.845	. 0	nafa-41	(HAD
185.0	17.048	0.037	188.0	18.195	0.039	191.0	19.407	0.042	194.0	20.685	000
185.1	17.085	.037	188.1	18.235	.039	191.1	19.448	.042	194.1	20.729	0.04
185.2	17.122	.037	188.2	18.274	.039	191.2	19.490	.042	194.2	20.773	.04
185.3	17.160	.037	188.3	18.314	.040	191.3	19.532	.042	194.3	20.817	.04
185.4	17.197	.038	188.4	18.353	.040	191.4	19.573	.042	194.4	20.861	.04
185.5	17.235		188.5	18.393	01	191.5	19.615	100	194.5	20.905	0.00
185.6	17.272	.038	188.6	18.432	.040	191.6	19.657	.042	194.6	20.949	•04
185.7	17.310	.038	188.7	18.472	•040	191.7	19.699	.042	194.7	20.993	.04
185.8	17.348	.038	188.8	18.512	•040	191.8	19.741	.042	194.8	21.038	.04
185.9	17.385	.038	188.9	18.552	-040	191.9	19.783	.042	194.9	21.082	.04
	THE SHAPE	.038	renau i	BINARS	.040		receive to	.042	100		.04
186.0	17.423	.028	189.0	18.592	.040	192.0	19.825		195.0	21.126	
186.1	17.461	.038	189.1	18.632	.040	192.1	19.868	.042	195.1	21.171	.04
186.2	17.499	.038	189.2	18.672	.040	192.2	19.910	.042	195.2	21.216	•04
186.3	17.537	.038	189.3	18.712	.040	192.3	19.952	.042	195.3	21.260	.04
186.4	17.575	.038	189.4	18.753	.040	192.4	19.995	.042	195.4	21.305	•04
Control of	OF CHIEF		TAN 1		.040	20.1	4000100	•045		restly and I	•04
186.5	17.614	-038	189.5	18.793	.040	192.5	20.037	.043	195.5	21.350	.04
186.6	17.652	.038	189.6	18.833	.040	192.6	20.080	.043	195.6	21.395	.04
186.7	17.690	.038	189.7	18.874	.041	192.7	20.123	.043	195.7	21.440	.04
186.8	17.729	.038	189.8	18.914	.041	192.8	20.166	.043	195.8	21.485	.04
186.9	17.767	.039	189.9	18.955	.041	192.9	20.208	.043	195.9	21.530	.04
187.0	17.806		190.0	18.996		193.0	20.251	100	196.0	21.576	
187.1	17.844	•039	190.1	19.036	.041	193.1	20.294	•043	196.1	21.621	.04
187.2	17.883	.039	190.2	19.077	•041	193.2	20.338	.043	196.2	21.666	.04
187.3	17.922	.039	190.3	19.118	.041	193.3	20.381	.043	196.3	21.712	.040
187.4	17.961	.039	190.4	19.159	.041	193.4	20.424	.043	196.4	21.758	.046
187.5	18.000		100 5		1 60	ma. T	Yeller	.043	12.00		.090
187.6	18.039	.039	190.5	19.200	.041	193.5	20.467	.043	196.5	21.803	.046
187.7	18.078	.039	190.6	19.241	.041	193.6	20.511	.043	196.6	21.849	.046
187.8	18.117	.039	190.7	19.283	.041	193.7	20.554	.044	196.7	21.895	.04
187.9	18.156	.039	190.8	19.324	.041	193.8	20.598	.044	196.8	21.941	.040
188.0	18.195	0.039	190.9	19.365	0.041	193.9	20.641	0.044	196.9	21.987	0.046
		1	191.0	19.407		194.0	20.685		197.0	22.033	49

Boiling Point, Fahren.	Barom- eter in English Inches.	Difference.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Difference.	Boiling Point, Fahren.	Barom- eter in English Inches.	Difference.
0 197.0	22.033		201.0	23.943		205.0	25,990		o 209.0	28.180	
197.1	22.079	0.046	201.1	23.993	0.049	205.1	26.043	0.053	209.1	28.237	0.057
197.2	22.125	.046	201.1	24.042	.050	205.2	26.096	.053	209.2	28.293	.057
197.3	22.172	•046	201.2	24.092	.050	205.2	26.149	.053	209.2	28.350	-057
197.4	22.218	.046	201.4	24.142	.050	205.4	26.202	.053	209.4	28.407	.057
10111		.046	20111	21.112	.050	200.1	20.202	.053	200.4	20.401	.057
197.5	22.264		201.5	24.191		205.5	26.255		209.5	28,464	
197.6	22.311	.047	201.6	24.241	.050	205.6	26.309	.053	209.6	28.521	.057
197.7	22.358	.047	201.7	24.291	•050	205.7	26.362	.054	209.7	28.579	.057
197.8	22.404	-047	201.8	24.341	•050	205.8	26.416	.054	209.8	28.636	.057
197.9	22.451	.047	201.9	24.391	•050	205.9	26.470	.054	209.9	28.693	.057
		.047			.050			.054			.058
198.0	22.498	.047	202.0	24.442	.050	206.0	26.523	.054	210.0	28.751	0.50
198.1	22.545	.047	202.1	24.492	.050	206.1	26.577	.054	210.1	28.809	.058
198.2	22.592	.047	202.2	24.542	.050	206.2	26.631	.054	210.2	28.866	.058
198.3	22.639	.047	202.3	24.593	.051	206.3	26.685	.054	210.3	28.924	.058
198.4	22.686	.047	202.4	24.644	.051	206.4	26.740	.054	210.4	28.982	.058
	00 -0.										
198.5	22.734	-047	202.5	24.694	.051	206.5	26.794	.054	210.5	29.040	.058
198.6	22.781	.047	202.6	24.745	.051	206.6	26.848	.054	210.6	29.098	.058
198.7	22.829	.048	202.7	24.796	.051	206.7	26.903	.055	210.7	29.156	.058
198.8	22.876	.048	202.8	24.847	-051	206.8	26.957	-055	210.8	29.215	.058
198.9	22.924	.048	202.9	24.898	.051	206.9	27.012	.055	210.9	29.273	•059
199.0	22.971		203.0	24.949		207.0	27.066		211.0	29.331	
199.1	23.019	-048	203.1	25.000	.051	207.1	27.121	-055	211.1	29.390	.059
199.2	23.067	.048	203.2	25.051	.051	207.2	27.176	.055	211.2	29.449	.059
199.3	23.115	.048	203.3	25.103	.051	207.3	27.231	•055	211.3	29.508	.059
199.4	23.163	.048	203.4	25.154	.051	207.4	27.286	.055	211.4	29.566	.059
100 -	00 011		000 =	05 000	1	00===	07.047			20 227	.000
199.5 199.6	23.211 23.259	.048	203.5	25.206 25.257	.052	207.5	27.341	.055	211.5	29.625	.059
199.7	23.308	.048	203.7	25.309	.052	207.7	27.397 27.452	.055	211.6	29.684	.059
199.8	23.356	.048	203.8	25.361	.052	207.8	27.507	.055	211.8	29.744 29.803	.059
199.9	23.405	.048	203.9	25.413	.052	207.9	27.563	.056	211.9	29.862	.059
100.0	20.400	.049	200.0	20.110	.052	201.0	27.505	.056	211.3	23.002	.059
200.0	23,453		204.0	25.465		208.0	27.618		212.0	29,922	
200.1	23.502	.049	204.1	25.517	.052	208.1	27.674	.056	212.1	29.981	.060
200.2	23.550	.049	204.2	25.569	.052	208.2	27.730	.056	212.2	30.041	.060
200.3	23.599	.049	204.3	25.621	.052	208.3	27.786	.056	212.3	30.101	•060
200.4	23.648	.049	204.4	25.674	.052	208.4	27.842	.056	212.4	30.161	.060
	-16	.049		STA DE	.052	No.	JONE STATE	.056		The same	.060
200.5	23.697	048	204.5	25.726	.053	208.5	27.898	056	212.5	30.221	000
200.6	23.746	.049	204.6	25.779	.053	208.6	27.954	.056	212.6	30.281	.060
200.7	23.795	.049	204.7	25.831	.053	208.7	28.011	.056	212.7	30.341	•060
200.8	23.845	.049	204.8	25.884	.053	208.8	28.067	.056	212.8	30.401	•060
200.9	23.894	0.049	204.9	25.937	0.053	208.9	28.123	0.057	212.9	30.461	0.060
201.0	23.943		205.0	25.990		209.0	28.180		213.0	30.522	

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## APPENDIX

20

## THE HYPSOMETRICAL TABLES.

COMPARISON OF THE DIFFERENT MEASURES OF LENGTH MOST GENERALLY USER FOR INDICATING ALTITUDES.

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## APPENDIX

THE HYPSOMETRICAL TAGES

#### COMPARISON

OF THE MEASURES OF LENGTH MOST GENERALLY USED FOR INDICATING ALTITUDES.

It is too well known that the measures used in scientific researches among civilized nations are not uniform, as the convenience of all would require. In France the metre is employed; in England and North America, the yard and its third part, the English foot; in Germany, most commonly, the Old French or Paris foot, the sixth part of the French toise called the *Toise du Pérou*; at the same time, however, though not so extensively, the Rhine foot, in Denmark and Holland, and especially in Prussia, where it has been declared, under the name of Prussian foot, the legal measure in that kingdom; in Austria, the klafter of Vienna and its sixth part, the foot of Vienna; in Switzerland, the Swiss or federal foot, which has been adjusted to the metrical system, and is three tenths of a metre; and so on.

The numerous altitudes ascertained, either by private efforts, or in connection with the public works, and quite especially with the extensive geodetic operations carried on by the governments of these various countries for the survey of a regular map, are expressed in the measures respectively adopted by each of them. These heights, however, before they can be compared, require to be uniformly reduced to any one of these measures. Their relation to each other, therefore, is given here, together with numerous reduction tables, designed to save both the useless expenditure of time and the almost unavoidable errors arising from so numerous reductions.

The exact relation of the standard measures above mentioned is not easily ascertained, and the numbers given by the best authorities by no means always agree; for the manufacture of exact copies of a standard scale, and the accurate comparison of it, require considerable skill, and belong to the most delicate operations of physics. The numbers used for computing the following tables have been adopted, after a careful review of the authorities, as the most reliable. A few words on the most important original legal standards of measures may not be unwelcome. For further details on the subject the reader is referred principally to Dove's work, Maas und Messen, 2d edition, Berlin, 1835.

The principal original, legal standards are the following: -

1. The Toise du Pérou, the old French standard, made in 1735, in Paris, by Langlois, under the direction of Godin, is a bar of iron which has its standard length at the temperature of 13° Reaumur. It is known as the Toise du Pérou, because it was used by the French Academicians Bouguer and La Condamine in their measurement D

of an arc of the meridian in Peru. What follows will show that it may almost be called the only common standard, to which all the others are referred for comparison.

- 2. The Metre is a standard bar of platina, made by Lenoir in Paris, which has its normal length at the temperature of zero Centigrade, or the freezing point. Its length is intended to make it a natural standard, and to represent the ten-millionth part of the terrestrial arc comprised between the equator and the pole, or of a quarter of the meridian. The length of this arc given by the measurement ordered for the purpose by the Assemblée Nationale, of the arc of the meridian between Barcelona, through France, to Dunkirk, combined with the measurements previously made in Peru and in Lapland, gave for the distance of the equator from the pole 5,130,740 toises, with an ellipticity of  $\frac{1}{334}$ , and for the length of the metre 443.29596 lines of the toise du Perou, assumed to be 443.296 lines, or 3 feet 11.296 lines. This last quantity was declared in 1799 to be the length of the legal metre, and vrai et définitif, and is the length of Lenoir's platina standard. Later and more extensive measurements in various parts of the globe, however, seem to indicate that this quantity is somewhat too small. The latest and most exact results we now possess, combined and computed by Bessel, would make the quarter of the meridian 10,000,856 metres, and the metre = 443.29979 Paris lines; Schmidt's computation would make it 443.29977 lines, and both numbers are confirmed by Airy's results. The legal metre is thus, in fact, as Dove remarks, a legalized part of the toise du Pérou, and this last remains the primitive standard. But it must be added that a natural standard, in the absolute sense of the word, is a utopian one, which ever-changing Nature never will give us. The metre is, for all practical purposes, what it was intended to be, a natural standard; though it must be confessed that, in practice, the question is not whether and how far a standard is a natural or a conventional one, but how readily and accurately it can be obtained, or recovered when lost.
- 3. The English Standard Yard is a brass bar, made by Bird in 1760, which was declared, by act of Parliament, 1st May, 1825, the legal measure of length when at the temperature of 62° Fahrenheit, under the name of Imperial Standard. Another standard, sometimes also called Parliamentary Standard, was made by Bird in 1758. Sir George Shuckburgh found both to be nearly identical, at least within 0.0002 of an inch. (Philos. Trans. for 1798, p. 170.)

Another scale of brass, however, made by Troughton for Sir George Shuckburgh, described in the *Philosophical Transactions for* 1798, and known as Shuckburgh's scale, obtained among scientific men, perhaps, a higher degree of authority, on account of the great accuracy of its division, and of its apparatus, devised by Troughton, for delicate comparisons. That scale was used by Captain Kater, in 1818, in his researches for determining the length of the pendulum beating a second at London, and also the length of the metre, expressed in English inches of the imperial standard. (*Phil. Trans. for* 1818.)

Numerous attempts to determine the relation between the English and the French measures show no inconsiderable discrepancies in their results. Omitting the older comparisons with the toise, we give here the value of the metre in English imperial inches, as resulting from the most reliable comparisons.

A standard scale made and divided by Troughton, and in all particulars identical

with Shuckburgh's scale, was brought to France in 1801 by Pictet. The comparison of it with the standard metre, made by Prony, Legendre, and Méchain, gave, after due reduction of the two standards to their respective normal temperatures,

1 metre at 32° Fahr. = 39.371 English imperial inches at 62° Fahr.

This determination was adopted for all reductions in Kelly's Universal Cambist, and in the French translation of the work, published in Paris in 1823.

A new comparison was made with great care by Captain H. Kater, in 1818. (See *Philos. Trans. for* 1818, p. 103.) The standards used were a brass scale metre, by Fortin, terminated with parallel planes (*mètre à bouts*), and a bar of platina on which the length of the metre was marked by two very fine lines (*mètre à traits*). Both were compared with Shuckburgh's scale, and a double series of experiments gave as the mean result:

Brass metre at 32° Fahr. = 39.37076 inches of Shuckburgh's scale at 62° Fahr.

Platina metre at 32° Fahr. =  $\frac{39.37081}{39.37079}$  " " " " " " " "

On this value of the metre are based the reduction tables by Matthieu, published yearly in the *Annuaire du Bureau des Longitudes*; and it has come into general use, both in Europe and in this country.

Captain Kater gives besides, in the same paper, p. 109, note, the value of the metre compared with Bird's Parliamentary standard as being

1 metre at 32° F. = 39.37062 imp. inches of Bird's Parliamentary standard at 62° F. This value has been adopted by Dove, as being the legal one, in his reduction tables in his work, *Maas und Messen*, p. 175, &c., and by many German authorities.

According to Baily's experiments, made in 1835, when engaged in constructing a new standard for the Royal Astronomical Society (Memoirs R. Ast. Soc., Vol. IX.), the value of the metre is (Lee, Collection of Tables and Formulæ, p. 62)

1 metre at 32° F. = 39.370092 imperial standard inches at 62° F.

The original legal standards having been lost in the fire which destroyed, several years ago, the Parliament Houses, an act of Parliament provided for the construction of new ones; but as the report of the committee having charge of the construction of the new British standard has not yet been published, the discussion of the subject must be postponed.

The value adopted in the following tables, is that determined by Captain Kater, viz. 1 metre = 39.37079 English inches.

It may not be out of place to remark that Schumacher, in the first edition of his Sammlung von Hülfstafeln, used the value 1 metre = 39.3827 English inches, as given in the Base du Système Métrique; but this number, which expresses the relation of both standards when at the freezing point, becomes 39.37079 when they are respectively reduced to their normal temperatures. Schumacher's tables, therefore, must be corrected accordingly.

4. The actual standard of length of the United States is a brass scale of eighty-two inches in length, prepared for the Coast Survey of the United States, by Troughton of London, meant to be identical with the English Imperial Standard, and deposited in the office of weights and measures. The temperature at which it is a standard is 62° Fahrenheit, and the yard measure is between the 27th and 63d inches of the

scale. (See Report on the Construction and Distribution of Weights and Measures, by Prof. A. D. Bache, 1857.)

Hassler, first Superintendent of the United States Coast Survey, made an elaborate comparison of eleven different standard metres with the brass scale of eighty-two inches, by Troughton. Three of the standard metres, certified to be correct by high authorities, seem to deserve especial confidence: — 1. An iron metre, presented to Mr. Hassler by Tralles, which was one of the three that Tralles had made by Lenoir at the same time with those distributed to the committee on the weights and measures.

2. Another metre of iron, also by Lenoir, verified by Bouvard and Arago, and declared by them to be identical with the original.

3. A platina standard by Fortin, verified by Arago, and found to be  $\frac{1}{1000}$  of a millimetre too long, for which error allowance was made. Their comparison with the Troughton scale at the temperature of the freezing point gave:

- 1. Iron metre of Tralles = 39.3809171 inches of the Troughton scale.
- 2. Iron metre of Lenoir = 39.3799487 " " "
- 3. Platina metre of Fortin = 39.3804194 " "

Or, correcting for expansion, and reducing them to their respective standard temperatures:

- Iron metre of Tralles at 32° F. = 39.36850
   Iron metre of Lenoir at 32° F. = 39.36754
   Platina metre of Fortin at 32° F. = 39.36789

  English inches of the Troughton scale of 82 inches at 62° F.
- Hassler, in his Report to Congress on Weights and Measures, in 1832, adopts the first value, viz.:

1 metre at 32° F. = 39.3809171 inches of the Troughton scale at 32° F; and the Troughton scale was declared the United States standard, from which copies were to be made.

This value materially differs from those given by other careful comparisons, while, on the other hand, the close accordance of the numbers corresponding to the various standard metres proves the accuracy of Hassler's method and comparison. It is, therefore, difficult not to ascribe, with Baily, this discrepancy to some inaccuracy in the length of the Troughton scale of 82 inches. But as that scale has been declared the standard of length of the United States, it seems better to call it, as is done in the Coast Survey Reports, the American yard, and its subdivisions the American foot and inch, and to consider it as a new standard, similar to, but not identical with, the English imperial standard. The value of the metre expressed in American standard inches is given in the Coast Survey Report for 1853, as

1 metre at 32° F. = 39.36850535 United States standard inches at 62° F.

We learn from the Report on Weights and Measures, by Prof. A. D. Bache, 1857, p. 18, that two copies of the new British standards, now in progress of construction, viz. a bronze standard, No. 11, and a malleable iron standard, No. 57, have been presented by the British government to the United States. A series of careful comparisons, made in 1856, by Mr. Saxton, under the direction of Prof. A. D. Bache, of the British bronze standard, No. 11, with the Troughton scale of eighty-two inches, showed that the British bronze standard yard is shorter than the American yard by 0.00087 inch.

Comparisons of the American standards with new French standards, recently presented to the United States by the French government, are still in progress.

For the present, however, it seems best to adhere to the value of the metre, expressed in American standard inches, adopted by the Coast Survey as given above. From this value the separate tables, which will be found below, for the reduction of the American yard and foot, were computed.

- 5. The Klafter of Vienna is a silver line let into a prismatic bar of iron, on which the length of the klafter was engraved by Voigtländer. It has its normal length at 13° Reaumur, and was declared by law, in 1816, the standard Klafter of Vienna. On the same silver line the French toise is marked, from the standard toise sent, in 1760, by La Caille and La Condamine to the Observatory of Vienna. According to a recent and very careful comparison by Struve (Mem. of the Austrian Acad., Vol. V., I. p. 117), the value of the klafter of Vienna is 0.9730317 toise du Pérou.
- 6. The Prussian Foot is marked on a standard iron bar, 3 feet long, made by Pistor in Berlin; it is a standard at the temperature of 13° Reaumur. The length of the Prussian foot was declared by law to be = 139.13 lines of the toise du Pérou.
- 7. A Mexican Vara, the standard length, brought from Mexico at the close of the war, by Major Turnbull of the Topographical Engineers, was presented to the Office of Weights and Measures. This standard was made by soldering sheet-brass upon the tinned surface of an iron bar. A careful comparison of its length with the American standard was made under the direction of Prof. Bache, which gave its length to be = 32.9682 inches at 58°.7 Fahrenheit, or 32.9680 when reduced to 62° Fahrenheit.

The relation of that particular Mexican standard to the Spanish standard not being known, it was thought better to adopt, for the present, the value of the Spanish Vara, and of its third part, the Castilian foot, found in Thionville, *Traité des Poids et Mesures*, &c., in Balbi's *Abrégé de Géographie*, viz. 1 vara = 0.847965 metre.

From the fundamental equations indicated above have been derived all those which have been used for computing the reduction tables given in the Appendix. At the head of each table will be found the value from which it was computed.

The tables are so arranged as to give *directly* the reduction of any whole number not exceeding three or four figures, and larger numbers within the limits needed for altitudes, by means of a *single* addition.

## Example.

Reduce 25,351 English feet into metres.

In Table XVI., on the line beginning with 25,000 and in the column headed 300, take for 25,300 = 7711.30 metres.

In the second part of the table, on the line beginning with 50, and in column headed 1, take for

or 51 = 15.54 "
English feet 25,351 = 7726.84 "

The fractions, which seldom occur, are treated as whole numbers, taking care only properly to move the decimal point.

Tables XL. to XLIV. will be found convenient for converting fractional parts of a toise or of a foot into each other.

### TO CONVERT

## FRENCH TOISES

## INTO DIFFERENT MEASURES OF LENGTH.

I. CONVERSION OF FRENCH TOISES INTO METRES.

1 Toise = 1.94903631 Metre.

The state of	4 4 30		Cherton.		Un	its.		ion allic	Minnie	Mark Control
Toises.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
e ver	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.000	1.949	3.898	5.847	7.796	9.745	11.694	13.643	15.592	17.54
10	19.490	21.439	23.388	25.337	27.287	29.236	31.185	33.124	35.073	37.02
20	38.981	40.930	42.879	44.828	46.777	48.726	50.675	52.624	54.573	56.52
30	58.471	60.420	62.369	64.318	66.267	68.216	70.165	72.114	74.063	76.01
40	77.961	79.911	81.860	83.809	85.758	87.707	89.656	91.605	93.554	95.50
50	97.452	99.401	101.350	103.299	105.248	107.197	109.146	111.095	113.044	114.9
60	116.942	118.891	120.840	122.789	124.738	126.687	128.636	130.585	132.534	134.4
70	136.433	138.382	140.331	142.280	144.229	146.178	148.127	150.076	152.025	153.9
80	155.923	157.872	159.821	161.770	163,719	165.668	167.617	169.566	171.515	173.4
90	175.413	177.362	179.311	181.260	183.209	185.158	187.108	189.057	191.006	192.9
Twise,		A Same	h Lit.	. Janet	Hund	lreds.	animar	and to	walker.	
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
ATT OF	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metre
0	0.00	194.90	389.81	584.71	779.61	974.52	1169.42	1364.33	1559.23	1754.
1000	1949.04	2143.94	2338.84	2533.75	2728.65	2923.55	3118.46	3312.36	3507.27	3702.
2000	3898.07	4092.98	4287.88	4482.78	4677.69	4872.59	5067.50	5262.40	5457.30	5652.
3000	5847.11	6042.01	6236.92	6431.82	6626.72	6821.63	7016.53	7211.44	7406.34	7601.
4000	7796.15	7991.05	8185.95	8380.86	8575.76	8770.66	8965.57	9160.47	9355.38	9550.
5000	9745.18	9940.09	10135.0	10329.9	10524.8	10719.7	10914.6	11109.5	11304.4	11499

#### II. CONVERSION OF TOISES INTO FRENCH OR PARIS FEET. 1 Toise = 6 French Feet.

Toises.					Un	its.				alem
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Par Feet 0.00	Par.Feet.	Par.Feet.	Par.Feet.	Par.Feet.	Par Feet.	Par.Feet.	Par. Feet.	Par Feet 48	Par.Feet
10	60	66	72	78	84	90	96	102	108	114
20	120	126	132	138	144	150	156	162	168	174
30	180	186	192	198	204	210	216	222	228	234
40	240	246	252	258	264	270	276	282	288	294
50	300	306	312	318	324	330	336	342	348	354
60	360	366	372	378	384	390	396	402	408	414
70	420	426	432	438	444	450	456	462	468	474
80	480	486	492	498	504	510	516	522	528	534
90	540	546	552	558	564	570	576	582	588	594

					Un	its.				
Toises.	0,	1.	2.	3.	4.	5.	6.	7.	8.	9.
V-MAN (ST	Eng. feet.	Eng. feet.	Eng feet.	Eng feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng feet.	Eng. feet.	Eng. fee
0	0.000	6.395	12.789	19.184	25.578	31.973	38.368	44.762	51.157	57.55
10	63.946	70.340	76.735	83.130	89.524	95.919		108.708		
20		134.286	140.681	and the same	153.470	159.865		Aller and		185.44
30	191.838	11,40,17	204.627	211.021	217.416	223.811	230.205			249.38
40	255.784	262.178	268.573	274.967	281.362	287.757	294.151	300.546	306.940	313.33
50	319.729	326.124	332.519	338.913	345.308	351.702	359.097	364.492	370.886	377.28
60	383.675	390.070	396.465	402.859	409.254	415.648	422.043	428.438	434.832	441.22
70	447.621	454.016	460.410	466.805	473.200	479.594	485.989	492.383	498.778	505.17
80	511.567	517.962	524.356	530.751	537.146	543.540	549.935	556.329	562.724	569.1
90	575.513	581.908	588.302	594.697	601.091	607.486	613.881	620.275	626.670	633.00
				P. P. P. P. W.	Hund	lreds.				
housands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet	Eng feet.	Eng. fe
0	0.0	639.5	1278.9	1918.4	2557.8	3197.3	3836.8	4476.2	5115.7	5755
1000	6394.6	7034.0	7673.5	8313.0	8952.4	9591.9	10231.3	10870.8	11510.3	12149
2000	12789.2	13428.6	14068.1	14707.6	15347.0	15986.5	16625.9	17265.4	17904.9	18544
3000	19183.8	19823.2	20462.7	21102.1	21741.6	22381.1	23020.5	23660.0	24299.4	24938
4000					28136.2		29415.1			
5000	31972.9	32612.4	33251.9	33891.3	34530.8	35170.2	35809.7	36449.2	37088.6	37728
	IV. COI	NVERSIO			TOISES 942205 Ame			N FEET		
Toises.			1 T	oise = 6.39	942205 Ame Un	erican Feet				9.
Toises.	0.	1.	1 T	oise = 6.39	942205 Ame Un	its.	6.	7.	8.	9.
Tens.	O. Am. Feet.	1.	2. Am. Feet.	3. Am. Feet.	042205 Ame Un  4.  Am. Feet.	its.  5. Am. Feet	6.	7.	S. Am. Feet.	Am.Fee
Tens.	0. Am. Feet. 0.000	1. Am.Feet 6.394	2. Am. Feet. 12.788	3. Am. Feet. 19.183	4. Am. Feet. 25.577	its.  5.  Am. Feet 31.971	6. Am Feet. 38.365	7. Am Feet. 44.760	8. Am. Feet. 51.154	Am.Fee
0 10	Am. Feet. 0.000 63.942	1. Am. Feet 6.394 70.336	2. Am. Feet. 12.788 76.731	3. Am. Feet. 19.183 83.125	4. Am. Feet. 25.577 89.519	5. Am. Feet 31.971 95.913	Am Feet 38.365 102.308	7. Am Feet. 44.760 108.702	8. Am. Feet. 51.154 115.096	Am.Fee 57.5-
0 10 20	Am. Feet. 0.000 63.942 127.884	1. Am.Feet 6.394 70.336 134.279	2. Am. Feet. 12.788	3. Am. Feet. 19.183	Un  4. Am. Feet. 25.577 89.519 153.461	its.  5.  Am. Feet 31.971	6. Am Feet 38.365 102.308 166.250	7. Am Feet. 44.760 108.702 172.644	8. Am. Feet. 51.154 115.096 179.038	Am.Fee 57.5- 121.49 185.43
0 10	Am. Feet. 0.000 63.942 127.884 191.827	1. Am.Feet 6.394 70.336 134.279	2. Am. Feet. 12.788 76.731 140.673	3. Am. Feet. 19.183 83.125 147.067	4. Am. Feet. 25.577 89.519 153.461 217.403	5. Am. Feet 31.971 95.913 159.855	Am Feet. 38.365 102.308 166.250 230.192	7. Am Feet. 44.760 108.702 172.644	8. Am. Feet. 51.154 115.096 179.038 242.980	Am. Fee 57.5- 121.49 185.43 249.37
0 10 20 30 40	0. Am. Feet. 0.000 63.942 127.884 191.827 255.769	1. Am. Feet 6.394 70.336 134.279 198.221 262.163	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557	3. Am. Feet. 19.183 83.125 147.067 211.009 274.951	4. Am. Feet. 25.577 89.519 153.461 217.403 281.346	5. Am. Feet 31.971 95.913 159.855 223.798 287.740	6. Am Feet 38.365 102.308 166.250 230.192 294.134	7. Am Feet. 44.760 108.702 172.644 236.586 300.528	8. Am. Feet. 51.154 115.096 179.038 242.980 306.923	Am. Fee 57.5- 121.49 185.43 249.37 313.31
0 10 20 30 40	0. Am. Feet. 0.000 63.942 127.884 191.827 255.769 319.711	1. Am. Feet 6.394 70.336 134.279 198.221 262.163 326.105	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 332.499	3. Am. Feet. 19.183 83.125 147.067 211.009 274.951 338.894	4. Un  4. Am Feet 25.577 89.519 153.461 217.403 281.346 345.288	5. Am. Feet 31.971 95.913 159.855 223.798 287.740 351.682	6. Am Feet 38.365 102.308 166.250 230.192 294.134 358.076	7. Am Feet. 44.760 108.702 172.644 236.586 300.528 364.470	8. Am. Feet. 51.154 115.096 179.038 242.980 306.923 370.865	Am. Fee 57.5- 121.49 185.43 249.37 313.31
0 10 20 30 40 50 60	0. Am. Feet. 0.000 63.942 127.884 191.827 255.769 319.711 383.653	1. Am. Feet 6.394 70.336 134.279 198.221 262.163 326.105 390.047	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 332.499 396.442	3. Am. Feet. 19.183 83.125 147.067 211.009 274.951 338.894 402.836	4. Am. Feet. 25.577 89.519 153.461 217.403 281.346 345.288 409.230	5. Am. Feet 31.971 95.913 159.855 223.798 287.740 351.682 415.624	Am Feet 38.365 102.308 166.250 230.192 294.134 358.076 422.018	7. Am Feet. 44.760 108.702 172.644 236.586 300.528 364.470 428.413	8. Am. Feet. 51.154 115.096 179.038 242.980 306.923 370.865 434.807	Am. Fee 57.5- 121.49 185.43 249.37 313.31 377.25 441.20
0 10 20 30 40 50 60 70	0. Am. Feet. 0.000 63.942 127.884 191.827 255.769 319.711 383.653 447.595	1. Am.Feet 6.394 70.336 134.279 198.221 262.163 326.105 390.047 453.990	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 332.499 396.442 460.384	3. Am. Feet. 19.183 83.125 147.067 211.009 274.951 338.894 402.836 466.778	4. Am. Feet. 25.577 89.519 153.461 217.403 281.346 345.288 409.230 473.172	5. Am. Feet 31.971 95.913 159.855 223.798 287.740 351.682 415.624 479.566	Am. Feet. 38.365 102.308 166.250 230.192 294.134 358.076 422.018 485.961	7.  Am Feet. 44.760 108.702 172.644 236.586 300.528 364.470 428.413 492.355	8. Am. Feet. 51.154 115.096 179.038 242.980 306.923 370.865 434.807 498.749	Am. Fee 57.5- 121.49 185.43 249.37 313.31 377.23 441.20 505.1-
0 10 20 30 40 50 60	0. Am. Feet. 0.000 63.942 127.884 191.827 255.769 319.711 383.653 447.595 511.538	1. Am.Feet 6.394 70.336 134.279 198.221 262.163 326.105 390.047 453.990 517.932	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 332.499 396.442 460.384 524.326	3. Am. Feet. 19.183 83.125 147.067 211.009 274.951 338.894 402.836 466.778 530.720	4. Am. Feet. 25.577 89.519 153.461 217.403 281.346 345.288 409.230 473.172	5. Am. Feet 31.971 95.913 159.855 223.798 287.740 351.682 415.624 479.566 543.509	Am. Feet. 38.365 102.308 166.250 230.192 294.134 358.076 422.018 485.961 549.903	7. Am Feet. 44.760 108.702 172.644 236.586 300.528 364.470 428.413 492.355 556.297	8. Am. Feet. 51.154 115.096 179.038 242.980 306.923 370.865 434.807 498.749 562.691	Am. Fee 57.5- 121.49 185.43 249.37 313.31 377.23 441.20 505.1- 569.08

	No.				Hund	ireds.			aftibuet -	NI WAR
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
WE LES	Am. Feet	Am Feet	Am Feet	Am. Feet.	Am. Feet.	Am Feet	Am Feet.	Am. Feet.	Am Feet.	Am. Feet.
0	0.0	639.4	1278.8	1918.3	2557.7	3197.1	3836.5	4476.0	5115.4	5754.8
1000	6394.2	7033.6	7673.1	8312.5	8951.9	9591.3	10230.8	10870.2	11509.6	12149.0
2000	12788.4	13427.9	14067.3	14706.7	15346.1	15985.5	16625.0	17264.4	17903.8	18543.2
3000	19182.7	19822.1	20461.5	21100.9	21740.3	22379.8	23019.2	23658.6	24298.0	24937.5
4000	25576.9	26216.3	26855.7	27495.1	28134.6	28774.0	29413.4	30052.8	30692.3	31331.7
5000	31971.1	32610.5	33249.9	33889.4	34528.8	35168.2	35807.6	36447.0	37086.5	37725.9

## TO CONVERT

## METRES

## INTO DIFFERENT MEASURES OF LENGTH.

1 LEGAL METRE = 443.296 FRENCH OR PARIS LINES.

#### V. CONVERSION OF METRES INTO TOISES AND DECIMALS.

1 Metre = 0.513074074 Toise.

Metres.	- Hundreds.											
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900		
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	Toises		
0	0.00	51.31	102.61	153.92	205.23	256.54	307.84	359.15	410.46	461.7		
1000	513.07	564.38	615.69	667.00	718.30	769.61	820.92	872.23	923.53	974.8		
2000	1026.15	1077.46	1128.76	1180.07	1231.38	1282.69	1333.99	1385.30	1436.61	1487.9		
3000	1539.22	1590.53	1641.84	1693.14	1744.45	1795.76	1847.07	1898.37	1949.68	2000.9		
4000	2052.30	2103.60	2154.91	2206.22	2257.53	2308.83	2360.14	2411.45	2462.76	2514.0		
5000	2565.37	2616.68	2667.98	2719.29	2770.60	2821.91	2873.21	2924.52	2975.83	3027.		
6000	3078.44	3129.75	3181.06	3232.37	3283.67	3334.98	3386.29	3437.60	3488.90	3540.		
7000	3591.52	3642.83	3694.13	3745.44	3796.75	3848.06	3899.36	3950.67	4001.98	4053.2		
8000	4104.59	4155.90	4207.21	4258.51	4309.82	4361.13	4412.44	4463.74	4515.05	4566.		
0000	120 2.00											
9000		CESA COLO	4720.28	4771.59	4822.90		4925.51	4976.82	5028.13	5079.4		
Fig. 177 (1) - #111	4617.67	4668.97			Uni	its.						
9000 Metres.		CESA COLO	<b>2.</b>	<b>3.</b>			4925.51 <b>6.</b>	7.	5028.13	9.		
9000 Metres. Tens.	0. Toises.	1. Toises.	2. Toises.		4. Toises.	its.		7.	S. Toises.	9.		
9000 Metres. Tens.	0. Toises. 0.000	1. Toises. 0.513	2. Toises. 1.026	3. Toises. 1.539	Toises. 2.052	5. Toises. 2.565	6. Toises. 3.078	7. Toises. 3.592	S. Toises. 4.105	9. Toises 4.61		
9000 Metres. Tens.	0. Toises. 0.000 5.131	1. Toises. 0.513 5.644	Toises. 1.026 6.157	Toises. 1.539 6.670	Toises. 2.052 7.183	Toises. 2.565 7.696	Toises. 3.078 8.209	Toises. 3.592 8.722	Toises. 4.105 9.235	9. Toises 4.61 9.74		
9000 Metres. Tens.	O. Toises. 0.000 5.131 10.261	1. Toises. 0.513 5.644 10.775	Toises. 1.026 6.157 11.288	Toises. 1.539 6.670 11.801	Toises. 2.052 7.183 12.314	Toises. 2.565 7.696 12.827	Toises. 3.078 8.209 13.340	7. Toises. 3.592 8.722 13.853	Toises. 4.105 9.235 14.366	9. Toises 4.61 9.74 14.87		
9000 Metres. Tens.	Toises. 0.000 5.131 10.261 15.392	Toises. 0.513 5.644 10.775 15.905	Toises. 1.026 6.157 11.288 16.418	Toises. 1.539 6.670 11.801 16.931	Toises. 2.052 7.183 12.314 17.445	Toises. 2.565 7.696 12.827 17.958	Toises. 3.078 8.209 13.340 18.471	7. Toises. 3.592 8.722 13.853 18.984	Toiscs. 4.105 9.235 14.366 19.497	Toises 4.61 9.74 14.87 20.01		
9000 Metres. Tens.	O. Toises. 0.000 5.131 10.261	1. Toises. 0.513 5.644 10.775	Toises. 1.026 6.157 11.288	Toises. 1.539 6.670 11.801	Toises. 2.052 7.183 12.314	Toises. 2.565 7.696 12.827	Toises. 3.078 8.209 13.340	7. Toises. 3.592 8.722 13.853	Toises. 4.105 9.235 14.366	9. Toises 4.61 9.74 14.87 20.01		
9000 Metres. Tens.	Toises. 0.000 5.131 10.261 15.392	Toises. 0.513 5.644 10.775 15.905	Toises. 1.026 6.157 11.288 16.418	Toises. 1.539 6.670 11.801 16.931	Toises. 2.052 7.183 12.314 17.445	Toises. 2.565 7.696 12.827 17.958	Toises. 3.078 8.209 13.340 18.471	7. Toises. 3.592 8.722 13.853 18.984	Toiscs. 4.105 9.235 14.366 19.497			
9000 Metres. Tens. 0 10 20 30 40	Toises. 0.000 5.131 10.261 15.392 20.523	1. Toises. 0.513 5.644 10.775 15.905 21.036	2. Toises. 1.026 6.157 11.288 16.418 21.549	3. Toises. 1.539 6.670 11.801 16.931 22.062	Uni Toises. 2.052 7.183 12.314 17.445 22.575	Toises. 2.565 7.696 12.827 17.958 23.088	Toises. 3.078 8.209 13.340 18.471 23.601	7. Toises. 3.592 8.722 13.853 18.984 24.114	S.  Toises. 4.105 9.235 14.366 19.497 24.628	9. Toises 4.61 9.74 14.87 20.01 25.14		
9000  Metres. Tens.  0 10 20 30 40	Toises. 0.000 5.131 10.261 15.392 20.523	1. Toises. 0.513 5.644 10.775 15.905 21.036 26.167	Toises. 1.026 6.157 11.288 16.418 21.549 26.680	3. Toises. 1.539 6.670 11.801 16.931 22.062 27.193	Uni Toises. 2.052 7.183 12.314 17.445 22.575 27.706	Toises. 2.565 7.696 12.827 17.958 23.088 28.219	Toises. 3.078 8.209 13.340 18.471 23.601 28.732	7. Toises. 3.592 8.722 13.853 18.984 24.114 29.245	Toises. 4.105 9.235 14.366 19.497 24.628 29.758	Toises 4.61 9.74 14.87 20.01 25.14 30.27		
9000  Metres. Tens.  0 10 20 30 40 50 60	Toises. 0.000 5.131 10.261 15.392 20.523 25.654 30.784	Toises. 0.513 5.644 10.775 15.905 21.036 26.167 31.298	Toises. 1.026 6.157 11.288 16.418 21.549 26.680 31.811	3. Toises. 1.539 6.670 11.801 16.931 22.062 27.193 32.324	Uni Toises. 2.052 7.183 12.314 17.445 22.575 27.706 32.837	Toises. 2.565 7.696 12.827 17.958 23.088 28.219 33.350	6. Toises. 3.078 8.209 13.340 18.471 23.601 28.732 33.863	7. Toises. 3.592 8.722 13.853 18.984 24.114 29.245 34.376	Toises. 4.105 9.235 14.366 19.497 24.628 29.758 34.889	Toises 4.61 9.74 14.87 20.01 25.14 30.27 35.40		

1 Metre = 3.078444 Paris Feet.

Fr.Feet.	Metres.				4	Metres.	Units.				
0         0.00         3.08         6.16         9.24         12.31         15.39         18.47         21.55         24.63         27.           10         30.78         33.86         36.94         40.02         43.10         46.18         49.26         52.33         55.41         58.           30         92.35         95.43         98.51         101.59         104.67         107.75         110.82         113.90         116.98         120.           40         123.14         126.22         129.29         182.37         135.45         138.53         141.61         144.69         147.77         150.           60         184.71         187.79         190.86         193.94         197.02         200.10         203.18         206.29         209.33         212.           70         215.49         218.57         221.65         224.73         227.00         203.14         203.22         226.30         229.37         292.45         295.53         295.01         200.33         212.           80         246.28         249.35         252.43         253.22         237.33         224.73         227.50         266.75         267.52         200.93         212.	Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
10	SATE A	11			TALK STATE OF THE STATE OF	The second of the second	Mr. Parket Transaction			105.00	Fr. Feet
20		The second			Land Barrier	THE PERSON NAMED IN				W. C. T. W. T. W.	27.7
30		The state of the s				100000	2007 F. C. C. C. C.	THE PERSON NAMED IN	275000000000000000000000000000000000000	TOP TO THE PARTY	58.4
123.14   126.22   129.29   132.37   135.45   138.53   141.61   144.69   147.77   150.55     153.92   157.00   160.08   163.16   166.24   169.31   172.39   175.47   178.55   181.50     184.71   187.79   190.86   193.94   197.02   200.10   203.18   206.26   209.33   212.50     1215.49   218.57   221.65   224.73   227.80   230.88   233.96   237.04   240.12   243.50     180   246.28   249.35   252.43   255.51   258.59   261.67   264.75   267.82   270.90   273.09     100   307.84   310.92   314.00   317.03   320.16   323.24   326.32   329.39   332.47   335.110     100   336.63   341.71   344.79   347.86   350.94   354.02   357.10   360.18   363.63     110   336.63   341.71   344.79   347.86   350.94   354.02   357.10   360.18   363.63     130   400.20   403.28   406.35   409.43   412.51   415.59   418.67   421.75   421.83   427.40     140   430.98   434.06   437.14   440.22   443.30   446.37   449.45   452.53   455.61   458.40     150   461.77   464.85   467.92   471.00   474.08   477.16   480.24   483.32   486.39   489.40     160   492.55   495.63   498.71   501.79   504.86   507.94   511.02   514.10   517.18     170   523.34   526.41   529.49   532.57   556.56   538.73   541.81   544.88   547.96   551.18     180   554.12   557.20   560.28   563.36   566.43   569.51   572.59   575.67   578.75   581.8     190   584.90   587.98   591.06   594.14   597.22   600.30   603.38   606.45   609.53   612.6     200   615.69   618.77   621.85   624.92   628.00   631.08   634.16   637.24   640.32   643.3     200   661.67   649.55   652.63   655.71   658.79   661.87   664.94   668.02   671.10   674.1     200   677.26   680.34   686.49   689.57   692.65   695.73   698.81   701.89   704.2     200   615.69   618.77   621.85   624.92   628.00   631.08   634.16   637.24   640.32   643.3     200   672.66   680.34   686.49   689.57   692.65   695.73   698.81   701.89   704.2     200   666.94   689.55   689.63   812.71   815.79   818.87   821.94   825.02   825.1     200   800.40   803.47   806.55   809.68   812.71   815.99   818.87   8		H C	Marine Dallace	Lo 5 (30) (30 (40)	The state of the s		Section Contract to	The second second		and the second	89.2
153.92   157.00   160.08   163.16   166.24   169.31   172.39   175.47   178.55   181.60   181.71   187.79   190.86   193.94   197.02   200.10   203.18   206.26   209.33   212.   216.28   218.57   221.65   224.73   227.80   230.88   233.96   237.04   240.12   243.   246.28   249.35   252.43   255.51   255.59   261.67   264.75   267.82   270.90   273.   277.06   280.14   283.22   286.30   289.37   292.45   295.53   298.61   301.69   304.   307.84   310.92   314.00   317.03   320.16   323.24   326.32   329.39   332.47   335.110   338.63   341.71   344.79   347.86   330.94   354.02   357.10   360.18   363.26   366.11   369.41   372.49   375.57   378.65   381.73   844.81   387.88   399.96   394.04   397.   310   400.20   403.28   406.35   409.43   412.51   415.59   418.67   421.75   424.83   427.   430.95   434.06   437.14   440.22   443.30   446.87   449.45   452.53   455.61   458.41   430.95   434.06   437.14   440.22   443.30   446.87   449.45   452.53   455.61   458.41   430.95   436.83   498.71   501.79   504.86   507.94   511.02   514.10   517.18   520.170   523.34   526.41   529.49   532.57   535.65   538.73   541.81   544.88   547.96   511.00   554.12   557.20   560.28   563.36   566.43   569.51   572.59   575.67   578.75   581.8   590.06   587.98   591.06   594.14   597.22   600.30   603.38   606.45   609.53   612.60   615.69   618.77   621.85   624.92   628.00   631.08   634.16   637.24   640.32   643.40   640.47   649.55   652.63   655.71   658.79   661.87   664.94   668.02   671.10   674.1   672.00   677.26   680.34   683.41   686.49   689.57   692.65   695.73   698.81   701.89   703.20   708.04   711.12   714.20   717.28   720.36   723.43   726.51   729.59   732.67   738.83   741.90   744.98   744.80   894.57   892.65   895.73   898.81   701.89   703.20   703.34   703.04							- E399FULL		The street of the last of the	The state of	AHEGOS III
184.71	40	123.14	126.22	129.29	132.37	135.45	138.53	141.61	144.69	147.77	150.8
70         215.49         218.57         221.65         224.73         227.80         230.88         233.96         237.04         240.12         243.8           80         246.28         249.35         252.43         255.51         255.59         261.67         264.75         267.82         270.90         273.3           90         277.06         280.14         283.22         286.30         289.37         292.45         295.53         298.61         301.69         304.1           100         307.84         310.92         314.00         317.08         320.16         323.24         326.32         329.39         332.47         335.1           110         338.63         341.71         344.79         375.67         378.65         381.73         384.81         387.88         390.96         394.04         397.11         397.51         375.67         378.65         381.73         384.81         387.88         390.96         394.04         397.11         290.43         492.55         495.63         497.14         440.22         443.30         446.37         494.95         425.53         495.61         455.11         557.20         560.28         563.36         566.43         569.79         511.02         5	50	11	V		USE AND COM	A SHORT HERE	169.31	172.39	175.47	178.55	181.6
80         246.28         249.35         252.43         255.51         258.59         261.67         264.75         267.82         270.90         273.3           90         277.06         280.14         283.22         286.30         289.37         292.45         295.53         298.61         301.69         304.7           100         307.84         310.92         314.00         317.08         320.16         323.24         326.32         329.39         332.47         335.11           110         338.63         341.71         344.79         347.86         350.94         354.02         357.10         360.18         363.26         366.11           120         369.41         372.49         375.57         378.65         381.73         384.81         387.88         390.96         394.04         397.11           130         400.20         403.28         406.35         409.43         412.51         415.69         418.67         421.75         424.83         427.44         427.44           140         430.98         484.04         487.14         440.22         443.30         446.37         494.45         452.53         455.61         455.41           150         451.72 <t< td=""><td></td><td>11</td><td></td><td></td><td></td><td>CARROLA RESIDEN</td><td>200.10</td><td>203.18</td><td>206.26</td><td>209.33</td><td>212.4</td></t<>		11				CARROLA RESIDEN	200.10	203.18	206.26	209.33	212.4
90         277.06         280.14         283.22         286.30         289.37         292.45         295.53         298.61         301.69         304.100           100         307.84         310.92         314.00         317.08         320.16         323.24         326.32         329.39         332.47         335.11           110         338.63         341.71         344.79         347.56         350.94         354.02         357.10         360.18         363.26         366.1           120         369.41         372.49         375.57         378.65         381.73         384.81         387.88         390.96         394.04         397.           130         400.20         403.28         406.35         409.43         412.51         415.67         421.75         424.83         427.4           140         430.98         434.06         437.14         440.22         443.30         446.37         449.45         452.53         455.61         458.4           150         461.77         464.85         467.92         471.00         474.08         477.16         480.24         483.32         486.39         489.1           160         492.55         495.63         498.71						TOTAL DATE		233.96	237.04		243.2
100         307.84         310.92         314.00         317.03         320.16         323.24         326.32         329.39         332.47         335.11           110         338.63         341.71         344.79         347.86         350.94         357.10         360.13         364.02         369.41         372.49         375.57         378.65         381.73         384.81         387.88         390.96         394.04         397.           130         400.20         403.28         406.35         409.43         412.51         415.59         418.67         421.75         424.83         427.16         421.75         424.83         427.16         409.25         421.60         437.14         440.22         443.30         446.37         449.45         452.53         455.61         458.4           160         492.55         495.63         498.71         501.79         504.86         507.94         511.02         514.10         517.18         520.3           170         523.34         526.41         529.49         532.57         535.65         538.73         541.81         544.88         547.96         551.6           180         554.12         557.20         560.28         563.66         566.49<		The second			and the second	258.59	261.67	264.75	267.82	270.90	273.9
110         338.63         341.71         344.79         347.86         350.94         354.02         357.10         360.18         363.26         366.13           120         369.41         372.49         375.57         378.65         381.73         384.81         387.83         390.96         394.04         397.1           130         400.20         403.28         406.35         409.43         412.51         415.59         418.67         421.75         424.83         427.1           140         430.98         434.06         437.14         440.22         443.30         446.37         449.45         452.53         455.61         458.4           150         461.77         464.85         467.92         471.00         474.08         477.16         480.24         483.32         486.39         489.1           160         492.55         495.63         498.71         501.79         504.86         507.94         511.02         514.10         514.10         517.10         523.34         526.41         529.49         532.57         535.65         538.73         541.81         544.88         547.96         551.0           180         554.99         587.98         591.06         594.14	90	277.06	280.14	283.22	286.30	289.37	292.45	295.53	298.61	301.69	304.7
120         369.41         372.49         375.57         378.65         381.73         384.81         387.88         390.96         394.04         397.11           130         400.20         403.28         406.35         409.43         412.51         415.59         418.67         421.75         424.83         427.1           140         430.98         434.06         437.14         440.22         443.30         446.37         449.45         452.53         455.61         458.6           150         461.77         464.85         467.92         471.00         474.08         477.16         480.24         483.32         486.39         489.11           160         492.55         495.63         498.71         501.79         504.86         507.94         511.02         514.10         517.18         520.1           170         523.34         526.41         529.49         532.57         535.65         538.73         541.81         544.88         547.96         551.0           180         554.19         587.98         591.06         594.14         597.22         600.30         603.38         606.45         609.53         612.6           200         615.69         618.77 <td< td=""><td>100</td><td>307.84</td><td>310.92</td><td>314.00</td><td>317.08</td><td>320.16</td><td>323.24</td><td>326.32</td><td>329.39</td><td>332.47</td><td>335.5</td></td<>	100	307.84	310.92	314.00	317.08	320.16	323.24	326.32	329.39	332.47	335.5
130         400.20         403.28         406.35         409.43         412.51         415.59         418.67         421.75         424.83         427.1           140         430.98         434.06         437.14         440.22         443.30         446.37         449.45         452.53         455.61         458.4           150         461.77         464.85         467.92         471.00         474.08         477.16         480.24         483.32         486.39         489.1           160         492.55         495.63         498.71         501.79         504.86         507.94         511.02         514.10         517.18         520.3           170         523.34         526.41         529.49         532.57         535.65         538.73         541.81         544.88         547.96         551.10           180         554.12         557.20         560.28         563.36         566.43         569.51         572.59         575.67         578.75         581.8           190         581.90         587.98         591.06         594.14         597.22         600.30         603.38         606.45         609.53         612.6           200         615.69         618.77	110	338.63	341.71	344.79	347.86	350.94	354.02	357.10	360.18	363.26	366.3
140         430.98         434.06         437.14         440.22         443.30         446.37         449.45         452.53         455.61         458.61           150         461.77         464.85         467.92         471.00         474.08         477.16         480.24         483.32         486.39         489.11           160         492.55         495.63         498.71         501.79         504.86         507.94         511.02         514.10         517.18         520.1           170         523.34         526.41         529.49         532.57         535.65         538.73         541.81         544.88         547.96         551.12           180         551.12         557.20         560.28         563.36         566.43         569.51         572.59         575.67         578.75         581.8           190         581.90         587.98         591.06         594.14         597.22         600.30         603.88         606.45         609.53         612.6           200         615.69         618.77         621.85         624.92         628.00         631.08         634.16         637.24         640.32         643.1           210         646.47         649.55 <t< td=""><td>120</td><td>369.41</td><td>372.49</td><td>375.57</td><td>378.65</td><td>381.73</td><td>384.81</td><td>387.88</td><td>390.96</td><td>394.04</td><td>397.1</td></t<>	120	369.41	372.49	375.57	378.65	381.73	384.81	387.88	390.96	394.04	397.1
150         461.77         464.85         467.92         471.00         474.08         477.16         480.24         483.32         486.39         489.1           160         492.55         495.63         498.71         501.79         504.86         507.94         511.02         514.10         517.18         520.1           170         523.34         526.41         529.49         532.57         535.65         538.73         541.81         544.88         547.96         551.1           180         554.12         557.20         560.28         563.36         566.43         569.51         572.59         575.67         578.75         581.8           190         584.90         587.98         591.06         594.14         597.22         600.30         603.38         606.45         609.53         612.6           200         615.69         618.77         621.85         624.92         628.00         631.08         634.16         637.24         640.32         643.3           210         646.47         649.55         652.63         655.71         658.79         661.87         664.94         668.02         671.10         674.1           220         677.26         680.34         6	130	400.20	403.28	406.35	409.43	412.51	415.59	418.67	421.75	424.83	427.9
160         492.55         495.63         498.71         501.79         504.86         507.94         511.02         514.10         517.18         520.1           170         523.34         526.41         529.49         532.57         535.65         538.73         541.81         544.88         547.96         551.0           180         554.12         557.20         560.28         563.36         566.43         569.51         572.59         575.67         578.75         581.8           190         584.90         587.98         591.06         594.14         597.22         600.30         603.38         606.45         609.53         612.6           200         615.69         618.77         621.85         624.92         628.00         631.08         634.16         637.24         640.32         643.3           210         646.47         649.55         652.63         655.71         658.79         661.87         664.94         668.02         671.10         674.1           220         677.26         680.34         683.41         686.49         689.57         692.65         695.73         698.81         701.89         704.2           230         769.61         772.69         7	140	430.98	434.06	437.14	440.22	443.30	446.37	449.45	452.53	455.61	458.6
160         492.55         495.63         498.71         501.79         504.86         507.94         511.02         514.10         517.18         520.1           170         523.34         526.41         529.49         532.57         535.65         538.73         541.81         544.88         547.96         551.0           180         554.12         557.20         560.28         563.36         566.43         569.51         572.59         575.67         578.75         581.8           190         584.90         587.98         591.06         594.14         597.22         600.30         603.38         606.45         609.53         612.6           200         615.69         618.77         621.85         624.92         628.00         631.08         634.16         637.24         640.32         643.3           210         646.47         649.55         652.63         655.71         658.79         661.87         664.94         668.02         671.10         674.1           220         677.26         680.34         683.41         686.49         689.57         692.65         695.73         698.81         701.89         704.2           230         769.61         772.69         7	150	461.77	464.85	467.92	471.00	474.08	477.16	480.24	483.32	486.39	489.4
170         523.34         526.41         529.49         532.57         535.65         538.73         541.81         544.88         547.96         551.0           180         554.12         557.20         560.28         563.36         566.43         569.51         572.59         575.67         578.75         581.8           190         584.90         587.98         591.06         594.14         597.22         600.30         603.38         606.45         609.53         612.6           200         615.69         618.77         621.85         624.92         628.00         631.08         634.16         637.24         640.32         643.3           210         646.47         649.55         652.63         655.71         658.79         661.87         664.94         668.02         671.10         674.1           220         677.26         680.34         686.49         689.57         692.65         695.73         698.81         701.89         704.24           230         708.04         711.12         714.20         717.28         720.36         723.43         726.51         729.59         732.67         735.7           250         769.61         772.69         775.77		11					0.000 10.000		200	1100	
180         554.12         557.20         560.28         563.36         566.43         569.51         572.59         575.67         578.75         581.5           190         584.90         587.98         591.06         594.14         597.22         600.30         603.38         606.45         609.53         612.6           200         615.69         618.77         621.85         624.92         628.00         631.08         634.16         637.24         640.32         643.3           210         646.47         649.55         652.63         655.71         658.79         661.87         664.94         668.02         671.10         674.1           220         677.26         680.34         683.41         686.49         689.57         692.65         695.73         698.81         701.89         704.52           240         738.83         741.90         744.98         748.06         751.14         754.22         757.30         760.38         763.45         766.8           250         769.61         772.69         775.77         778.85         781.92         785.00         788.08         791.16         794.24         797.5           260         800.40         803.47		523.34	OF SURES STORY	12 2 2 C L C L C L C L C L C L C L C L C	ACCOUNT OF THE	TO SEE HERE	and the same				
190         584.90         587.98         591.06         594.14         597.22         600.30         603.38         606.45         609.53         612.6           200         615.69         618.77         621.85         624.92         628.00         631.08         634.16         637.24         640.32         643.5           210         646.47         649.55         652.63         655.71         658.79         661.87         664.94         668.02         671.10         674.1           220         677.26         680.34         683.41         686.49         689.57         692.65         695.73         698.81         701.89         704.8           230         708.04         711.12         714.20         717.28         720.36         723.43         726.51         729.59         732.67         735.7           240         738.83         741.90         744.98         748.06         751.14         754.22         757.30         760.38         763.45         766.6           250         769.61         772.69         775.77         778.85         781.92         785.00         788.08         791.16         794.24         797.5           260         800.40         803.47         8	180	554.12	557.20	560.28	563.36	PASSES (15/4)	370 E. C. S. W. C.			The state of the s	
210       646.47       649.55       652.63       655.71       658.79       661.87       664.94       668.02       671.10       674.1         220       677.26       680.34       683.41       686.49       689.57       692.65       695.73       698.81       701.89       704.8         230       708.04       711.12       714.20       717.28       720.36       723.43       726.51       729.59       732.67       735.7         240       738.83       741.90       744.98       748.06       751.14       754.22       757.30       760.38       763.45       766.8         250       769.61       772.69       775.77       778.85       781.92       785.00       788.08       791.16       794.24       797.8         260       800.40       803.47       806.55       809.63       812.71       815.79       818.87       821.94       825.02       828.1         270       831.18       834.26       837.34       840.42       843.49       846.57       849.65       852.73       855.81       858.2         280       861.96       865.04       868.12       871.20       874.28       877.36       880.43       883.51       866.59 <td< td=""><td></td><td>11</td><td></td><td></td><td></td><td></td><td>TO 100 (100 )</td><td>13 (D) (C)</td><td></td><td>100000000000000000000000000000000000000</td><td>612.6</td></td<>		11					TO 100 (100 )	13 (D) (C)		100000000000000000000000000000000000000	612.6
210       646.47       649.55       652.63       655.71       658.79       661.87       664.94       668.02       671.10       674.1         220       677.26       680.34       683.41       686.49       689.57       692.65       695.73       698.81       701.89       704.8         230       708.04       711.12       714.20       717.28       720.36       723.43       726.51       729.59       732.67       735.7         240       738.83       741.90       744.98       748.06       751.14       754.22       757.30       760.38       763.45       766.8         250       769.61       772.69       775.77       778.85       781.92       785.00       788.08       791.16       794.24       797.8         260       800.40       803.47       806.55       809.63       812.71       815.79       818.87       821.94       825.02       828.1         270       831.18       834.26       837.34       840.42       843.49       846.57       849.65       852.73       855.81       858.2         280       861.96       865.04       868.12       871.20       874.28       877.36       880.43       883.51       866.59 <td< td=""><td>200</td><td>615.69</td><td>618.77</td><td>621.85</td><td>624.92</td><td>628.00</td><td>631.08</td><td>634.16</td><td>637.24</td><td>640.32</td><td>643.3</td></td<>	200	615.69	618.77	621.85	624.92	628.00	631.08	634.16	637.24	640.32	643.3
220         677.26         680.34         683.41         686.49         689.57         692.65         695.73         698.81         701.89         704.8           230         708.04         711.12         714.20         717.28         720.36         723.43         726.51         729.59         732.67         735.7           240         738.83         741.90         744.98         748.06         751.14         754.22         757.30         760.38         763.45         766.6           250         769.61         772.69         775.77         778.85         781.92         785.00         788.08         791.16         794.24         797.5         260         800.40         803.47         806.55         809.63         812.71         815.79         818.87         821.94         825.02         828.1         280         861.96         865.04         868.12         871.20         874.28         877.36         880.43         883.51         886.59         889.6         290         892.75         895.83         898.91         901.98         905.06         908.14         911.22         914.30         917.38         920.4           300         923.53         926.61         929.69         932.77         935.85 <td></td> <td></td> <td></td> <td>and the second</td> <td></td> <td></td> <td>Challenger St. St.</td> <td>C Promise</td> <td></td> <td></td> <td></td>				and the second			Challenger St. St.	C Promise			
230         708.04         711.12         714.20         717.28         720.36         723.43         726.51         729.59         732.67         735.7           240         738.83         741.90         744.98         748.06         751.14         754.22         757.30         760.38         763.45         766.6           250         769.61         772.69         775.77         778.85         781.92         785.00         788.08         791.16         794.24         797.5           260         800.40         803.47         806.55         809.63         812.71         815.79         818.87         821.94         825.02         828.1           270         831.18         834.26         837.34         840.42         843.49         846.57         849.65         852.73         855.81         888.29           290         892.75         895.83         898.91         901.98         905.06         908.14         911.22         914.30         917.38         920.4           300         923.53         926.61         929.69         932.77         935.85         938.93         942.00         945.08         948.16         951.2           320         985.10         988.18		11						Maria Land		CONTRACTOR OF THE PARTY OF THE	
240         738.83         741.90         744.98         748.06         751.14         754.22         757.30         760.38         763.45         766.6           250         769.61         772.69         775.77         778.85         781.92         785.00         788.08         791.16         794.24         797.5           260         800.40         803.47         806.55         809.63         812.71         815.79         818.87         821.94         825.02         828.1           270         831.18         834.26         837.34         840.42         843.49         846.57         849.65         852.73         855.81         858.5           280         861.96         865.04         868.12         871.20         874.28         877.36         880.43         883.51         886.59         889.6           290         892.75         895.83         898.91         901.98         905.06         908.14         911.22         914.30         917.38         920.4           300         923.53         926.61         929.69         932.77         935.85         938.93         942.00         945.08         948.16         951.2           320         985.10         988.18         9	230	11						THE STATE OF		CONTRACTOR	
260         800.40         803.47         806.55         809.63         812.71         815.79         818.87         821.94         825.02         828.1           270         831.18         834.26         837.34         840.42         843.49         846.57         849.65         852.73         855.81         858.5           280         861.96         865.04         868.12         871.20         874.28         877.36         880.43         883.51         886.59         889.6           290         892.75         895.83         898.91         901.98         905.06         908.14         911.22         914.30         917.38         920.4           300         923.53         926.61         929.69         932.77         935.85         938.93         942.00         945.08         948.16         951.2           310         954.32         957.40         960.47         963.55         966.63         969.71         972.79         975.87         978.95         982.6           320         985.10         988.18         991.26         994.34         997.42         1000.49         1003.57         1006.65         1009.73         1012.8           340         1046.67         1049.75	240	738.83	741.90	744.98	748.06	THE DESIGNATION OF THE PERSON		BOATS BUT I			766.5
260         800.40         803.47         806.55         809.63         812.71         815.79         818.87         821.94         825.02         828.1           270         831.18         834.26         837.34         840.42         843.49         846.57         849.65         852.73         855.81         858.5           280         861.96         865.04         868.12         871.20         874.28         877.36         880.43         883.51         886.59         889.6           290         892.75         895.83         898.91         901.98         905.06         908.14         911.22         914.30         917.38         920.4           300         923.53         926.61         929.69         932.77         935.85         938.93         942.00         945.08         948.16         951.2           310         954.32         957.40         960.47         963.55         966.63         969.71         972.79         975.87         978.95         982.6           320         985.10         988.18         991.26         994.34         997.42         1000.49         1003.57         1006.65         1009.73         1012.8           340         1046.67         1049.75	250	769.61	772.69	775.77	778.85	781.02	785.00	788 08	791 16	701 21	707 3
270         831.18         834.26         837.34         840.42         843.49         846.57         849.65         852.73         855.81         858.5           280         861.96         865.04         868.12         871.20         874.28         877.36         880.43         883.51         886.59         889.62           290         892.75         895.83         898.91         901.98         905.06         908.14         911.22         914.30         917.38         920.4           300         923.53         926.61         929.69         932.77         935.85         938.93         942.00         945.08         948.16         951.2           310         954.32         957.40         960.47         963.55         966.63         969.71         972.79         975.87         978.95         982.0           320         985.10         988.18         991.26         994.34         997.42         1000.49         1003.57         1006.65         1009.73         1012.8           340         1046.67         1049.75         1052.83         1055.91         1058.98         1062.06         1065.14         1068.22         1071.30         1074.5           350         1077.46         1080.53<				100000			William No.				
280         861.96         865.04         868.12         871.20         874.28         877.36         880.43         883.51         886.59         889.62           290         892.75         895.83         898.91         901.98         905.06         908.14         911.22         914.30         917.38         920.4           300         923.53         926.61         929.69         932.77         935.85         938.93         942.00         945.08         948.16         951.2           310         954.32         957.40         960.47         963.55         966.63         969.71         972.79         975.87         978.95         982.6           320         985.10         988.18         991.26         994.34         997.42         1000.49         1003.57         1006.65         1009.73         1012.8           340         1046.67         1049.75         1052.83         1055.91         1058.98         1062.06         1065.14         1068.22         1071.30         1074.5           350         1077.46         1080.53         1083.61         1036.69         1089.77         1092.85         1095.93         1099.00         1102.08         1105.3           360         1108.24 <t< td=""><td></td><td></td><td>00 300 PEG</td><td></td><td>The second second</td><td>The State of the S</td><td></td><td></td><td></td><td></td><td></td></t<>			00 300 PEG		The second second	The State of the S					
290         892.75         895.83         898.91         901.98         905.06         908.14         911.22         914.30         917.38         920.33           300         923.53         926.61         929.69         932.77         935.85         938.93         942.00         945.08         948.16         951.2           310         954.32         957.40         960.47         963.55         966.63         969.71         972.79         975.87         978.95         982.6           320         985.10         988.18         991.26         994.34         997.42         1000.49         1003.57         1006.65         1009.73         1012.8           340         1016.89         1018.96         1022.04         1025.12         1028.20         1031.28         1034.36         1037.44         1040.51         1043.8           350         1077.46         1080.53         1083.61         1036.69         1089.77         1092.85         1095.93         1099.00         1102.08         1105.3           360         1108.24         1111.32         1114.40         1117.48         1120.55         1123.63         1126.71         1129.79         1132.87         1135.8           370         1139.02			TO THE PARTY	12 COM 27 NOTES	Committee of the commit	THE ZET WORK					
310         954.32         957.40         960.47         963.55         966.63         969.71         972.79         975.87         978.95         982.0           320         985.10         988.18         991.26         994.34         997.42         1000.49         1003.57         1006.65         1009.73         1012.8           330         1015.89         1018.96         1022.04         1025.12         1028.20         1031.28         1037.44         1040.51         1043.5           340         1046.67         1049.75         1052.83         1055.91         1058.98         1062.06         1065.14         1068.22         1071.30         1074.5           350         1077.46         1080.53         1083.61         1086.69         1089.77         1092.85         1095.93         1099.00         1102.08         1105.3           360         1108.24         1111.32         1114.40         1117.48         1120.55         1123.63         1126.71         1129.79         1132.87         1135.8           370         1139.02         1142.10         1145.18         1148.26         1151.34         1157.49         1160.57         1166.7           380         1169.81         1172.89         1175.97			12000		THE RESTRICTION OF			STATE OF LABOR		O LONG THE LAND	920.4
310         954.32         957.40         960.47         963.55         966.63         969.71         972.79         975.87         978.95         982.0           320         985.10         988.18         991.26         994.34         997.42         1000.49         1003.57         1006.65         1009.73         1012.8           330         1015.89         1018.96         1022.04         1025.12         1028.20         1031.28         1037.44         1040.51         1043.5           340         1046.67         1049.75         1052.83         1055.91         1058.98         1062.06         1065.14         1068.22         1071.30         1074.5           350         1077.46         1080.53         1083.61         1086.69         1089.77         1092.85         1095.93         1099.00         1102.08         1105.3           360         1108.24         1111.32         1114.40         1117.48         1120.55         1123.63         1126.71         1129.79         1132.87         1135.8           370         1139.02         1142.10         1145.18         1148.26         1151.34         1157.49         1160.57         1166.7           380         1169.81         1172.89         1175.97	200	002 52	026 61	020 60	099 77	095 05	000 00	0.49.00	0.48.00	0.40.10	051.0
320         985.10         988.18         991.26         994.34         997.42         1000.49         1003.57         1006.65         1009.73         1012.6           330         1015.89         1018.96         1022.04         1025.12         1028.20         1031.28         1037.44         1040.51         1043.6           340         1046.67         1049.75         1052.83         1055.91         1058.98         1062.06         1065.14         1068.22         1071.30         1074.8           350         1077.46         1080.53         1083.61         1086.69         1089.77         1092.85         1095.93         1099.00         1102.08         1105.3           360         1108.24         1111.32         1114.40         1117.48         1120.55         1123.63         1126.71         1129.79         1132.87         1135.8           370         1139.02         1142.10         1145.18         1148.26         1151.34         1157.49         1160.57         1163.65         1166.5           380         1169.81         1172.89         1175.97         1179.04         1185.20         1188.28         1191.36         1194.44         1197.6           390         1200.59         1203.67         1206.75 </td <td></td> <td></td> <td>and the second</td> <td>A CANADA TANDA</td> <td>Water Barry</td> <td>24-21 128</td> <td>William Street, Street</td> <td>The second section</td> <td></td> <td>-UP-NEDIS</td> <td></td>			and the second	A CANADA TANDA	Water Barry	24-21 128	William Street, Street	The second section		-UP-NEDIS	
330       1015.89       1018.96       1022.04       1025.12       1028.20       1031.28       1034.36       1037.44       1040.51       1043.5         340       1046.67       1049.75       1052.83       1055.91       1058.98       1062.06       1065.14       1068.22       1071.30       1074.5         350       1077.46       1080.53       1083.61       1086.69       1089.77       1092.85       1095.93       1099.00       1102.08       1105.3         360       1108.24       1111.32       1114.40       1117.48       1120.55       1126.71       1129.79       1132.87       1135.87         370       1139.02       1142.10       1145.18       1148.26       1151.34       1157.49       1160.57       1163.65       1166.5         380       1169.81       1172.89       1175.97       1179.04       1185.20       1188.28       1191.36       1194.44       1197.6         390       1200.59       1203.67       1206.75       1209.83       1212.91       1215.99       1219.06       1222.14       1225.22       1228.2		11				Marie Charles	A. S. D. Black	1 CAST 14.0	TO THE TANK	7 3 7 1 1 1 3 3 2	
340       1046.67       1049.75       1052.83       1055.91       1058.98       1062.06       1065.14       1068.22       1071.30       1074.6         350       1077.46       1080.53       1083.61       1036.69       1089.77       1092.85       1095.93       1099.00       1102.08       1105.3         360       1108.24       1111.32       1114.40       1117.48       1120.55       1123.63       1126.71       1129.79       1132.87       1135.8         370       1139.02       1142.10       1145.18       1148.26       1151.34       1154.42       1157.49       1160.57       1163.65       1166.7         380       1169.81       1172.89       1175.97       1179.04       1182.12       1185.20       1188.28       1191.36       1194.44       1197.4         390       1200.59       1203.67       1206.75       1209.83       1212.91       1215.99       1219.06       1222.14       1225.22       1228.3		No. of the last of			770.00 770.00		the Park of the Late of		and the second second		
350							1062.06	1065.14	1068.22	1071.30	1074.3
360     1108.24     1111.32     1114.40     1117.48     1120.55     1123.63     1126.71     1129.79     1132.87     1135.8       370     1139.02     1142.10     1145.18     1148.26     1151.34     1154.42     1157.49     1160.57     1163.65     1166.7       380     1169.81     1172.89     1175.97     1179.04     1182.12     1185.20     1188.28     1191.36     1194.44     1197.6       390     1200.59     1203.67     1206.75     1209.83     1212.91     1215.99     1219.06     1222.14     1225.22     1228.3		1				F12.8			COLUMN STATE	- CT 12	
370     1139.02     1142.10     1145.18     1148.26     1151.34     1154.42     1157.49     1160.57     1163.65     1166.7       380     1169.81     1172.89     1175.97     1179.04     1182.12     1185.20     1188.28     1191.36     1194.44     1197.6       390     1200.59     1203.67     1206.75     1209.83     1212.91     1215.99     1219.06     1222.14     1225.22     1228.3		1100 04	1111 20	1114 40	1117 49	1190 55	1192.85	1195.93	1099.00	1102.08	1105.1
380   1169.81   1172.89   1175.97   1179.04   1182.12   1185.20   1188.28   1191.36   1194.44   1197.6   1200.59   1203.67   1206.75   1209.83   1212.91   1215.99   1219.06   1222.14   1225.22   1228.5		1108.21	1111.32	1114.40	1117.48	1120.55	1123.63	1126.71	1129.79	1132.87	1135.9
390   1200.59   1203.67   1206.75   1209.83   1212.91   1215.99   1219.06   1222.14   1225.22   1228.5		1160 01	1172 90	1175.07	1170.04	1101.34	1194.42	1107.49	1100.57	1163.65	1166.7
		1200.59	1203.67	1206.75	1209.83	1212.91					
0. 1. 2. 3. 4. 5. 6. 7. 8. 9.											

1 Metre = 3.078444 Paris Feet.

Metres.				tas di	Metres.	Units.				Siction 2
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
ales a	Fr. Feet.			Fr. Feet.						
400	1231.38	1234.46	1237.53	1240.61	1243.69	1246.77				
410	1262.16	1265.24	1268.32	1271.40	1274.48	1277.55				
420	1292.95	1296.02	1299.10	1302.18	1305.26					
430	1323.73	1326.81	1329.89	1332.97	1336.04		1 10 10 10 10 10 10 10 10 10 10 10 10 10	1345.28		
440	1354.52	1357.59	1360.67	1363.75	1366.83	1369.91	1372.99	1376.06	1379.14	1382.
450	1385.30	1388.38	1391.46	1394.54	1397.61	1400.69	1403.77	1406.85	1409.93	1413.0
460	1416.08	1419.16	1422.24	1425.32	1428.40	1431.48	1434.55	1437.63	1440.71	1443.
470	1446.87	1449.95	1453.03	1456.10	1459.18	1462.26	1465.34	1468.42	1471.50	1474.
480					1489.97					
490	1508.44	1511.52	1514.59	1517.67	1520.75	1523.83	1526.91	1529.99	1533.07	1536.
500					1551.54					
510					1582.32					
520					1613.10					
530	1631.58	1634.65	1637.73	1640.81	1643.89	1646.97	1650.05	1653.12	1656.20	1659.
540	1662.36	1665.44	1668.52	1671.60	1674.67	1677.75	1680.83	1683.91	1686.99	1690.
550	1693.14	1696.22	1699.30	1702.38	1705.46	1708.54	1711.61	1714.69	1717.77	1720.
560	1723.93	1727.01	1730.09	1733.16	1736.24	1739.32	1742.40	1745.48	1748.56	1751.
570					1767.03					
580	11				1797.81			1807.05		
590	1816.28	1819.36	1822.44	1825.52	1828.60	1831.67	1834.75	1837.83	1840.91	1843.
600	1847.07	1850.14	1853.22	1856.30	1859.38	1862.46	1865.54	1868.62	1871.69	1874.
610	1877.85	1880.93	1884.01	1887.09	1890.16	1893.24	1896.32	1899.40	1902.48	1905.
620	1908.64	1911.71	1914.79	1917.87	1920.95	1924.03	1927.11	1930.18	1933.26	1936.
630	1939.42	1942.50	1945.58	1948.66	1951.73	1954.81	1957.89	1960.97	1964.05	1967.
640	1970.20	1973.28	1976.36	1979.44	1982.52	1985.60	1988.67	1991.75	1994.83	1997.
650	2000.99	2004.07	2007.15	2010.22	2013.30	2016.38	2019.46	2022.54	2025.62	2028.
660	2031.77	2034.85	2037.93	2041.01	2044.09	2047.17	2050.24	2053.32	2056.40	2059.
670	2062.56	2065.64	2068.71	2071.79	2074.87	2077.95	2081.03	2084.11	2087.19	2090.
680					2105.66			2114.89		
690	2124.13	2127.20	2130.28	2133.36	2136.44	2139.52	2142.60	2145.68	2148.75	2151.
700	2154.91	2157.99	2161.07	2164.15	2167.22	2170.30	2173.38	2176.46	2179.54	2182.
710	2185.70	2188.77	2191.85	2194.93	2198.01	2201.09	2204.17	2207.24	2210.32	2213.
720	2216.48	2219.56	2222.64	2225.72	2228.79	2231.87	2234.95	2238.03	2241.11	2244.
730					2259.58					
740					2290.36					
750					2321.15					
760	2339.62	2342.70	2345.77	2348.85	2351.93	2355.01	2358.09	2361.17	2364.24	2367.
770	2370.40	2373.48	2376.56	2379.64	2382.72	2385.79	2388.87	2391.95	2395.03	2398.
780					2413.50			2422.74		
790	2431.97	2435.05	2438.13	2441.21	2444.28	2447.36	2450.44	2453.52	2456.60	2459.
									-	-

1 Metre = 3.078444 Paris Feet.

Metres.				Series !	Metres.	Units.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
200	Fr. Feet.	Fr. Feet.		Fr. Feet.	Fr. Feet.	Fr. Feet.	Fr. Feet.		Fr Feet.	Fr. Fee
800	1 17 662 17 2 5	1993/953 433	Company of the	100000000000000000000000000000000000000	2475.07	XX4-04 1 2 13 13 13 13 13 13 13 13 13 13 13 13 13	74-11-11-11	2484.30		200
810	Market Street	100 may 1 mg	A STATE OF THE STA	2502.77	1	State of the State	-23 Per - 11 P. I	The same of the same of	77.7	1
820	The Court of the	THE PERSON NAMED IN	1517537763	1900000	2536.64	10 10 2 3 CO.		2545.87		
830	11	MARKEN AND	2561.27	74936411	711577 X	120-120-100-100-2	STANDARD CONT.	1		THE PERSON NAMED IN
840	2585.89	2588.97	2592.05	2595.13	2598.21	2601.29	2604.36	2607.44	2610.52	2613.6
850	2616.68	2619.76	2622.83	2625.91	2628.99	2632.07	2635.15	2638.23	2641.30	2644.3
860	2647.46	2650.54	2653.62	2656.70	2659.78	2662.85	2665.93	2669.01	2672.09	2675.1
870	2678.25	2681.32	2684.40	2687.48	2690.56	2693.64	2696.72	2699.80	2702.87	2705.9
880	2709.03	2712.11	2715.19	2718.27	2721.34	2724.42	2727.50	2730.58	2733.66	2736.7
890	2739.82	2742.89	2745.97	2749.05	2752.13	2755.21	2758.29	2761.36	2764.44	2767.5
900	2770.60	2773.68	2776.76	2779.83	2782.91	2785.99	2789.07	2792.15	2795.23	2798.3
910	2801.38	2804.46	2807.54	2810.62	2813.70	2816.78	2819.85	2822.93	2826.01	2829.0
920	2832.17	2835.75	2838.33	2841.40	2844.48	2847.56	2850.64	2853.72	2856.80	2859.8
930	2862.95	2866.03	2869.11	2872.19	2875.27	2878.35	2881.42	2884.50	2887.58	2890.6
940	2893.74	2896.82	2899.89	2902.97	2906.05	2909.13	2912.21	2915.29	2918.36	2921.4
950	2924.52	2927.60	2930.68	2933.76	2936.84	2939.91	2942.99	2946.07	2949.15	2952.5
960	2955.31	2958.38	2961.46	2964.54	2967.62	2970.70	2973.78	2976.86	2979.93	2983.0
970	2986.09	2989.17	2992.25	2995.33	2998.40	3001.48	3004.56	3007.64	3010.72	3013.8
980	3016.88	3019.95	3023.03	3026.11	3029.19	3032.27	3035.35	3038.42	3041.50	3044.5
990	3047.66	3050.74	3053.82	3056.89	3059.97	3063.05	3066.13	3069.21	3072.29	3075.8
Metres.	French I	leet. M	letres.	rench Fee	t. Metr	es. Fre	nch Feet.	Metre	s. Fren	ch Feet.
1000	3078.	44 5	000	15392.22	90	00 23	7706.00	1300	0 400	019.78
2000	6156.	89 6	000	18470.67	100	00 30	784.44	1400	0 430	098.22
3000	9235.	33 7	000	21549.11	110	00 33	3862.89	1500	0 46	176.67
4000	12313.	78 8	3000	24627.56	120	00 36	6941.33	16000	0 495	255.11
					Decim	e tres.				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fr. Feet.	Fr.Feet.	Fr.Feet.	Fr.Feet.	Fr.Feet.	Fr.Feet	Fr.Feet.	Fr. Feet.	Fr.Feet.	Fr. Fee
0	0.0000	0.3078	0.6157	0.9235	1.2314	1.5392	1.8471	2.1549	2.4628	2.770
1	3.0784	3.3863	3.6941	4.0020	4.3098	4.6177	4.9255	5.2334	5.5412	5.849
2	6.1569	6.4647	6.7726		7.3883	7.6961	8.0040		8.6196	8.927
3					10.4667					
4					13.5452					
5	15.3922	15,7001	16,0079	16.3158	16,6236	16,9314	17,2393	17,5471	17.8550	18,169
6	18,4707	18,7785	19.0864	19,3942	19.7020	20,0099	20.3177	20.6256	20.9334	21.241
7					22.7805					
8					25.8589					
9	27,7060	28.0138	28,3217	28,6295	28.9374	29.2452	29,5531	29.8609	30.1688	30,476
THE RESERVE OF THE PARTY OF THE	11			1						300216

1 Metre = 3.28089917 English Feet.

				unity.	Metres.	(Units.)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng.Feet.	Eng. Feet.	Eng.Fcet.	Eng.Feet.	Eng. Feet.		Eng. Feet.	Eng.Feet.	Eng.Feet.	Eng. Fe
0	0.0	3.28	6.56	9.84	13.12	16.40	19.69	22.97	26.25	29.
10	32.81	36.09	39.37	42.65	45.93	49.21	52.49	55.78	59.06	62.
20	65.62	68.90	72.18	75.46	78.74	82.02	85.30	88.58	91.87	95.
30	98.43	101.71	104.99	108.27	111.55	114.83	118.11	121.39	124.67	127.
40	131.24	134.52	137.80	141.08	144.36	147.64	150.92	154.20	157.48	160.
50	164.04	167.33	170.61	173.89	177.17	180.45	183.73	187.01	190.29	193.
60	196.85	200.13	203.42	206.70	209.98	213.26	216.54	219.82	223.10	226.
70	229.66	232.94	236.22	239.51	242.79	246.07	249.35	252.63	255.91	259.
80	262.47	265.75	269.03	272.31	275.60	278.88	282.16	285.44	288.72	292.
90	295.28	298.56	301.84	305.12	308.40	311.69	314.97	318.25	321.53	324.
100	328.09	331.37	334.65	337.93	341.21	344.49	347.78	351.06	354.34	357.
110	360.90	364.18	367.46	370.74	374.02	377.30	380.58	383.87	387.15	390.
120	393.71	396.99	400.27	403.55	406.83	410.11	413.39	416.67	419.96	423.
130	426.52	429.80	433.08	436.36	439.64	442.92	446.20	449.48	452.78	456.
140	459.33	462.61	465.89	469.17	472.45	475.73	479.01	482.29	485.57	488.
150	492.13	495.42	498.70	501.98	505.26	508.54	511.82	515.10	518.38	521.
160	524.94	528.22	531.51	534.79	538.07	541.35	544.63	547.91	551.19	554.
170	557.75	561.03	564.31	567.60	570.88	574.16	577.44	580.72	584.00	587.
180	590.56	593.84	597.12	600.40	603.69	606.97	610.25	613.53	616.81	620.
190	623.37	626.65	629.93	633.21	636.49	639.78	643.06	646.34	649.62	652.
200	656.18	659.46	662.74	666.02	669.30	672.58	675.87	679.15	682.43	685.
210	688.99	692.27	695.55	698.83	702.11	705.39	708.67	711.96	715.24	718.
220	721.80	725.08	728.36	731.64	734.92	738.20	741.48	744.76	748.05	751.
230	754.61	757.89	761.17	764.45	767.73	771.01	774.29	777.57	780.85	784.
240	787.42	790.70	793.98	797.26	800.54	. 803.82	807.10	810.38	813.66	816.
250	820.22	823.51	826.79	830.07	833.35	836.63	839.91	843.19	846.47	849.
260	853.03	856.31	859.60	862.88	866.16	869.44	872.72	876.00	879.28	882.
270	885.84	889.12	892.40	895.69	898.97	902.25	905.53	908.81	912.09	915.
280	918.65	921.93	925.21	928.49	931.78	935.06	938.34	941.62	944.90	948.
290	951.46	954.74	958.02	961.30	964.58	967.87	971.15	974.43	977.71	980.
300	984.27	987.55	990.83	994.11	997.39	1000.67	1003.96	1007.24	1010.52	1013.
310	1017.08	The state of the s	1023.64	STATE AND ADDRESS.	1030.20	1033.48	1036.76	1040.05	1043.33	1046.
320	1049.89	1053.17	1056.45	1059.73	1063.01	1066.29	1069.57	1072.85	1076.13	1079.
330	1092.70	1085.98	1089.26		1095.82	1099.10	1102.38	1105.66	1108.94	1112.
340	1115.51	1118.79	1122.07	1125.35	1128.63	1131.91	1135.19	1138.47	1141.75	1145.
350	11					1164.72	1168.00	1171.28	1174.56	1177.
360	1181.12	County Street Washington	and the second second	1190.97	1194.25	1197.53	1200.81		1207.37	1210.
370	1213.93	The second second second	THE PERSON NAMED IN	1223.78	The second second	1230.34	1233.62	1236.90	1240.18	1243.
380	1246.74	The second second	CALL STATE OF THE STATE OF	1256.58	OF THE PERSON	1263.15	1266.43	LOCALIDAD NO.	1272.99	1276.
390	1279.55	1282.83	1286.11	1289.39	1292.67	1295.96	1299.24	1302.52	1305.80	1309.
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

400 to 799.

				Sall.	Metres.	(Units.)				
Metres.	0.	1.	2.	3,	4.	5.	6.	7.	8.	9.
9-1-1-2-8	Eng.Feet.	Eng.Feet.	Eng. Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng. Feet.	Eng. Feet.	
400	1312.36	1315.64	1318.92	1322.20	1325.48	1328.76	1332.05	1335.33	1338.61	1341.89
410	1345.17	1348.45	1351.73	1355.01		1361.57	1364.85	1368.13	1371.42	1374.70
420	1377.98	1381.26	1384.54	1387.82		1394.38	1397.66	1400.94	1404.22	1407.51
430	1410.79	1414.07	1417.35	1420.63		1427.19	1430.47	1433.75	1437.03	1440.31
440	1443.60	1446.88	1450.16	1453.44	1456.72	1460.00	1463.28	1466.56	1469.84	1473.12
450	1476.40	1479.69	1482.97	1486.25	1489.53	1492.81	1496.09	1499.37	1502.65	1505.93
460	1509.21	1512.49	1515.78	1519.06	1522.34	1525.62	1528.90	1532.18	1535.46	1538.74
470	1542.02	1545.30	1548.58	1551.87	1555.15	1558.43	1561.71	1564.99	1568.27	1571.55
480	1574.83	1578.11	1581.39	1584.67	1587.96	1591.23	1594.52	1597.80	1601.08	1604.36
490	1607.64	1610.92	1614.20	1617.48	1620.76	1624.05	1627.33	1630.61	1633.89	1637.17
500	1640.45	1643.73	1647.01	1650.29		1656.85	1660.13	1663.42	1666.70	1669.98
510	1673.26	1676.54	1679.82	1683.10		1689.66	1692.94	1696.22	1699.51	1702.79
520	1706.07	1709.35	1712.63	1715.91		1722.47	1725.75	1729.03	1732.31 1765.12	1735.60
530 540	1738.88 1771.69	1742.16 1774.97	1745.44 1778.25	1748.72 1781.53	1784.81	1755.28 1788.09	1758.56 1791.37	1761.84 1794.65	1797.93	1768.40 1801.21
550	1804.49	1807.78	1811.06	1814.34	1817.62	1890 00	1824.18	1827.46	1830.74	1834.02
560	1837.30	1840.58	1843.87	1847.15	1850.43		1856.99	1860.27	1863.55	1866.83
570	1870.11	1873.39	1876.67	1879.96	1883.24		1889.80	1893.08	1896.36	1899.64
580	1902.92	1906 20	1909.48	1912.76	1916.05		1922.61	1925.89	1929.17	1932.45
590	1935.73	1939.01	1942.29	1945.57	1948.85		1955.42	1958.70	1961.98	1965.26
330	1333.73	1000.01	1012.20	1340.01	1040.00	1002.10	1000.12	1000110	2002.00	
600	1968.54	1971.82	1975.10	1978.38	1981.66	1984.94	1988.22	1991.51	1994.79	1998.07
610	2001.35	2004.63	2007.91	2011.19	2014.47	2017.75	2021.03	2024.31		2030.88
620	2034.16	2037.44	2040.72	2044.00	2047.28	2050.56	2053.84	100000000000000000000000000000000000000		2063.69
630	2066.97	2070.25	2073.53	2076.81	2080.09		2086.65	2089.93	2093.21	2096.49
640	2099.78	2103.06	2106.34	2109.62	2112.90	2116.18	2119.46	2122.74	2126.02	2129.30
650	2132.58	2135.87	2139.15	2142.43	2145.71	2148.99	2152.27	2155.55	2158.83	2162.11
660	2165.39	2168.67	2171.96	2175.24	2178.52	2181.80	2185.08	2188.36	2191.64	2194.92
670	2198.20	2201.48	2204.76	2208.05	2211.33	2214.61	2217.89	2221.17	2224.45	2227.73
630	2231.01	2234.29	2237.57	2240.85	2244.13	2247.42	2250.70	2253.98	2257.26	2260.54
690	2263.82	2267.10	2270.38	2273.66	2276.94	2280.22	2283.51	2286.79	2290.07	2293.35
700	2296.63	2299.91	2303.19	2306.47	2309.75	2313.03	2316.31	2319.60	2322.88	2326.16
710	2329.44	2332.72	2336.00	2339.28		2345.84	2349.12	2352.40	2355.69	2358.97
720	2362.25	2365.53	2368.81	2372.09	2375.37	2378.65	2381.93	2385.21	2388.49	2391.78
730	2395.06	2398.34	2401.62	2404.90	2408.18	2411.46	2414.74	2418.02	2421.30	2424.58
740	2427.87	2431.15	2434.43	2437.71	2440.99	2444.27	2447.55	2450.83	2454.11	2457.39
750	2460.67	2463.96								
760	2493.48	2496.76		2503.33	2506.61		2513.17	2516.45	2519.73	2523.01
770	2526.29			2536.14		2542.70	2545.98		2552.54	11/20
780	2559.10	1	2565.66			2575.51	2578.79	2582.07	2585.35	2588.63
790	2591.91	2595.19	2598.47	2601.75	2605.03	2608.31	2611.60	2614.88	2618.16	2621.44
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

800 to 1199.

				244	Metres.	(Units.)				
Metros.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
AND A K	Eng.Feet.	Eng. Feet.	Eng.Feet.	Eng.Feet.	Eng. Feet	Eng.Feet.		Eng.Feet.	Eng.Feet.	Eng. Feet.
800	2624.72	2628.00	2631.28	2634.56	2637.84	2641.12	2644.40		2650.97	2654.25
810	2657.53	2660.81	2664.09	2667.37	2670.65	2673.93	2677.21	2680.49	2683.78	2687.06
820	2690.34	2693.62	2696.90	2700.18	2703.46	2706.74	2710.02		2716.58	
830	2723.15	2726.43	2729.71	2732.99	2736.27	2739.55	2742.83		2749.39	1
840	2755.96	2759.24	2762.52	2765.80	2769.08	2772.36	2775.64	2778.92	2782.20	2785.48
850	2788.76	2792.05	2795.33	2798.61	2801.89	2805.17	2808.45	2811.73	2815.01	2818.29
860	2821.57	2824.85	2828.14	2831.42	2834.70	2837.98	2841.26	2844.54	2847.82	2851.10
870	2854.38	2857.66	2860.94	2864.22	2867.51	2870.79	2874.07	2877.55	2880.63	2883.91
880	2887.19	2890.47	2893.75	2897.03	2900.31	2903.60	2906.88	2910.16	2913.44	2916.72
890	2920.00	2923.28	2926.56	2929.84	2933.12	2936.40	2939.69	2942.97	2946.25	2949.53
900	2952.81	2956.09	2959.37	2962.65	2965.93	2969.21	2972.49	2975.78	2979.06	2982.34
910	2985.62	2988.90	2992.18	2995.46	2998.74	3002.02	3005.30	The Part of the Pa	3011.87	3015.15
920	3018.43	3021.71	3024.99	3028.27		3034.83	3038.11	3041.39	3044.67	3047.96
930	3051.24	3054.52	3057.80	3061.08	3064.36	3067.64	3070.92	3074.20	3077.48	3080.76
940	3084.05	3087.33	3090.61	3093.89	3097.17	3100.45	3103.73		3110.29	3113.57
950	3116.85	3120.14	3123.42	3126.70	2120 08	3133.26	3136.54	3139.82	3143.10	3146.38
960	3149.66	3152.94	3156.22	3159.51	3162.79	3166.07	3169.35	3172.63	3175.91	3179.19
970	3182.47	3185.75	3189.03	3192.31	3195.60		3202.16	3205.44	3208.72	3212.00
980	3215.28	3218.56		3225.12	3228.40	3231.69	3234.97	3238.25	3241.53	3244.81
990	3248.09	3251.37	3254.65	3257.93	3261.21	3264.49	3267.78	3271.06	3274.34	3277.62
1000	2020 00	2004 10	200# 40	2200 =4	2004 00	200* 20	2000 50	2202 0#	2207 15	2010 42
1000	3280.90	3284.18 3316.99	3287.46	3290.74		3297.30	3300.58	3303.87 3336.67	3307.15	3310.43
1020	3313.71 3346.52	State Land To be	3320.27	3323.55	3326.83		3333.39	3369.48	3339.96	3343.24
1030	3379.33	3349.80 3382.61	3353.08 3385.89	3356.36 3389.17	3359.64 3392.45	3395.73	3366.20 3399.01	3402.29	3372.76 3405.57	3376.05 3408.85
1040	3412.14	3415.42	3418.70	3421.98	3425.26		3431.82	3435.10	3438.38	3441.66
1040	0412.14	0410.44	3413.70	3441.90	3423.20	9420.94	9491.04	0400.10	9490.90	0441.00
1050	3444.94	3448.22		3454.79	3458.07			3467.91	3471.19	3474.47
1060	3477.75	3481.03	3484.31	3487.60		3494.16	3497.44	3500.72	3504.00	3507.28
1070	3510.56	3513.84	3517.12	3520.40	3523.69		3530.25	3533.53	3536.81	3540.09
1080	3543.37 3576.18	3546.65 3579.46	3549.93 3582.74	3553.21 3586.02	3556.49 3589.30		3563.06 3595.87	3566.34 3599.15	3569.62 3602.43	3572.90 3605.71
		0010110	000211.1	0000102	5000.00	0002.00	0000.01	0000110	0002,10	0000111
1100	3608.99	3612.27	3615.55		3622.11		3628.67	3631.96	3635.24	3638.52
1110	3641.80	3645.08			3654.92	3658.20	3661.48	3664.76	3668.05	3671.33
1120	3674.61	3677.89	3681.17	3684.45			3694.29	3697.57	3700.85	3704.14
1130 1140	3707.42 3740.22	3710.70 3743.51	3713.98	3717.26 3750.07	3720.54		3727.10 3759.91	3730.38 3763.19	3733.66 3766.47	3736.94 3769.75
			aven vi				0100.01	9109.19	5100.41	0100.10
1150	3773.03	3776.31	3779.60	3782.88	3786.16		3792.72			3802.56
1160	3805.84	3809.12	3812.40	3815.69	3818.97	3822.25			3832.09	3835.37
1170			3845.21					3861.62		3868.18
1180	3871.46		3878.02			3887.87	3891.15	3894.43	3897.71	3900.99
1190	3904.27	3907.55	3910.83	3914.11	3917.39	3920.67	3923.96	3927.24	3930.52	3933.80
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1200 to 1599.

				والرهب	Metres.	(Units.)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
1000	Eng.Feet.	Eng. Feet.	Eng. Feet.	of the Property of the		Eng.Feet.	Eng.Feet.	Eng. Feet.	Eng.Feet. 3963.33	Eng.Feet. 3966.61
1200	3937.08	3940.36	3943.64	3946.92		3953.48	3956.76	3960.05		3999.42
1210	3969.89	3973.17	3976.45	3979.73	3983.01	man who had	3989.57	3992.85	3996.14	
1220	4002.70	4005.98	4009.26	4012.54	Company of the Control of the Contro	4019.10	4022.38		4028.94	4032.23
1230	4035.51	4038.79	4042.07	4045.35	4048.63	A STATE OF THE PARTY OF THE PAR	4055.19	4058.47	4061.75	4065.03
1240	4068.31	4071.60	4074.88	4078.16	4081.44	4084.72	4088.00	4091.28	4094.56	4097.04
1250	4101.12	4104.40	4107.69	4110.97	4114.25	4117.53	4120.81	4124.09	4127.37	4130.65
1260	4133.93	4137.21	4140.49	4143.78	4147.06	4150.34	4153.62	4156.90	4160.18	4163.46
1270	4166.74	4170.02	4173.30	4176.58	4179.87	4183.15	4186.43	4189.71	4192.99	4196.27
1280	4199.55	4202.83	4206.11	4209.39	4212.67	4215.96	4219.24	4222.52	4225.80	4229.08
1290	4232.36	4235.64	4238.92	4242.20	4245.48	4248.76	4252.05	4255.33	4258.61	4261.89
1300	4265.17	4268.45	4271.73	4275.01	4278.29	4281.57	4284.85	4288.14	4291.42	4294.70
1310	4297.98	4301.26	4304.54	4307.82	4311.10	4314.38	4317.66	4320.94	4324.23	4327.51
1320	4330.79	4334.07	4337.35	4340.63	4343.91	4347.19	4350.47	4353.75	4357.03	4360.31
1330	4363.60	4366.88	4370.16	4373.44	4376.72	4380.00	4383.28	4386.56	4389.84	4393.12
1340	4396.40	4399.69	4402.97	4406.25	4409.53	4412.81	4416.09	4419.37	4422.65	4425.93
1350	4429.21	4432.49	4435.78	4439.06	4442.34	4445.62	4448.90	4452.18	4455.46	4458.74
1360	4462.02	4465.30	4468.58	4471.87	4475.15	4478.43	4481.71	4484.99	4488.27	4491.55
1370	4494.83	4498.11	4501.39	4504.67	4507.96	4511.24	4514.52	4517.80	4521.08	4524.36
1380	4527.64	4530.92	4534.20	4537.48	4540.76	4544.05	4547.33	4550.61	4553.89	4557.17
1390	4560.45	4563.73	4567.01	4570.29	4573.57	4576.85	4580.14	4583.42	4586.70	4589.98
1400	4593.26	4596.54	4599.82	4603.10	4606.38	4609.66	4612.94	4616.23	4619.51	4622.79
1410	4626.07	4629.35	4632.63	4635.91	4639.19	4642.47	4645.75	4649.03	4652.31	4655.60
1420	4658.88	4662.16	4665.44	4668.72	4672.00	4675.28	4678.56	4681.84	4685.12	4688.40
1430	4691.69	4694.97	4698.25	4701.53	4704.81	4708.09	4711.37	4714.65	4717.93	4721.21
1440	4724.49	4727.78	4731.06	4734.34	4737.62	4740.90	4744.18	4747.46	4750.74	4754.02
1450	4757.30	4760.58	4763.87	4767.15	4770.43	4773.71	4776.99	4780.27	4783.55	4786.83
1460	4790.11	4793.39	4796.67	4799.96	4803.24	4806.52	4809.80	4813.08	4816.36	4819.64
1470	4822.92	4826.20	4829.48	4832.76	4836.05	4839.33	4842.61	4845.89	4849.17	4852.45
1480	4855.73	4859.01	4862.29	4865.57	4868.85	4872.14	4875.42	4878.70	4881.98	4885.26
1490	4888.54	4891.82	4895.10	4898.38	4901.66	4904.94	4908.23	4911.51	4914.79	4918.07
1500	4921.35	4924.63	4927.91	4931.19	4934.47	4937.75	4941.03	4944.31	4947.60	4950.88
1510	4954.16	4957.44	4960.72	4964.00	4967.28	4970.56	4973.84	4977.12	4980.40	4983.69
1520	4986.97	4990.25	4993.53	4996.81	5000.09	5003.37	5006.65	5009.93	5013.21	5016.49
1530	5019.78	5023.06	5026.34	5029.62	5032.90	Contract of the Contract of th	5039.46	5042.74	5046.02	5049.30
1540	5052.58	5055.87	5059.15	5062.43	5065.71	5068.99	5072.27	5075.55	5078.83	5082.11
1550	Harris and the same of the sam	5088.67	The Control of the Co			N. Charles and S. C.				
1560	III and the state of the state	5121.48	AND RESIDENCE OF THE PARTY OF T		5131.33	California (California)	5137.89	The second second	5144.45	5147.73
1570	5151.01	A CONTRACTOR OF THE PARTY OF TH	the second second	5160.85	5164.14	Annual State of the State of th	5170.70		5177.26	5180.54
1580	5183.82	No. of Street,	5190.38		5196.94	CONTRACTOR OF STREET	5203.51		5210.07	5213.35
1590	5216.63	5219.91	5223.19	5226.47	5229.75	5233.03	5236.32	5239.60	5242.88	5246.16
No.	0.	1.	2.	3.	4.	5.	. 6.	7.	8.	9.

1600 to 2000.

1600   1610   1620   1630   1640   1650   1660   1670   1680   1690   1710   51730   51740   51740   51820   51830   601840   601850   61850   61850   61850   61850   62850	0. Eng.Feet 5249.44 5282.25 5315.06 5347.87 5380.67 5413.48 5446.29 5479.10 5511.91 5544.72 5577.53 5610.34 5643.15 5675.96 5708.76 5774.38 5807.19 5840.00 5872.81 5905.62	5252.72 5285.53 5318.34 5351.15	5256.00 5288.81 5321.62 5354.43 5387.24 5420.05 5452.85 5485.66 5518.47 5551.28 5584.09 5616.90 5649.71 5682.52 5715.38 5748.14 5780.94 5813.75 5846.56	5259.28 5292.09 5324.90 5357.71 5390.52 5423.33	5262.56 5295.37 5328.18 5860.99 5393.80 5426.61 5492.23 5525.03 5557.84 5590.65 5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5. Eng.Feet. 5265.84 5298.65 5331.46 5364.27 5397.08 5429.89 5462.70 5495.51 5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17	Eng.Feet. 5269.12 5301.93 5334.74 5367.55 5400.36 5433.17 5465.98 5498.79 5531.60 5564.40 5597.21 5662.83 5695.64 5728.45 5761.26 5794.07 5826.88	5272.40 5305.21 5338.02 5370.85 5403.64 5436.45 5502.07 5534.88 5567.69 5600.49 5633.30 5666.11 5698.92 5731.73	5275.69 5308.49	9. Eng.Feet 5278.97 5311.78 5344.58 5377.39 5410.20 5443.01 5475.82 5508.63 5541.44 5574.25 5607.06 5639.87 5672.67 5705.48 5738.29 5771.10 5803.91 5836.72
1600 1610 1620 1630 1640 1650 1670 1770 1780 1770 1780 1770 1780 1770 1780 178	Eng.Feet 5249.44 5282.25 5315.06 5347.87 5380.67 5413.48 5446.29 5479.10 5511.91 5544.72 5577.53 5610.34 5643.15 5675.96 5708.76 5774.38 5807.19 5840.00 5872.81 5905.62	Eng.Feet 5252.72 5285.53 5318.34 5351.15 5383.96 5416.76 5449.57 5482.38 5515.19 5548.00 5580.81 5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	Eng. Feet. 5256.00 5288.81 5321.62 5354.43 5387.24 5420.05 5452.85 5485.66 5518.47 5551.28 5584.09 5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	Eng.Feet 5259.28 5292.09 5324.90 5357.71 5390.52 5423.33 5456.14 5488.94 5521.75 5554.56 5587.37 5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	Eng. Feet 5262.56 5295.37 5328.18 5860.99 5393.80 5426.61 5459.42 5492.23 5525.03 5557.84 5590.65 6666.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	Eng.Feet. 5265.84 5298.65 5331.46 5397.08 5429.89 5462.70 5495.51 5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	Eng.Feet. 5269.12 5301.93 534.74 5367.55 5400.36 5433.17 5465.98 5498.79 5531.60 5564.40 5597.21 5662.83 5695.64 5728.45 5761.26 5794.07	Eng.Feet. 5272.40 5305.21 5338.02 5370.83 5403.64 5436.45 5469.26 5502.07 5534.88 5567.69 5600.49 5633.30 5666.31 5698.92 5731.73	Eng.Feet. 5275.69 5308.49 5341.30 5374.11 5406.92 5439.73 5472.54 5505.35 5538.16 5570.97 5603.78 56669.39 5702.20 5735.01 5767.82 5800.63	Eng.Feet 5278.97 5311.78 5344.58 5377.39 5410.20 5443.01 5475.82 5508.63 5541.44 5574.25 5607.06 5639.87 5775.48 5738.29 5771.10 5803.91
1600   1610   1620   1630   1640   1650   1660   1670   1680   1690   1710   51730   51740   51740   51820   51830   601840   601850   61850   61850   61850   61850   62850	5249.44 5282.25 5315.06 5347.87 5380.67 5413.48 5446.29 5479.10 5511.91 5544.72 5577.53 5610.34 5643.15 5675.96 5708.76 5741.57 5774.38 5807.19 5840.00 5872.81 5905.62	5252.72 5285.53 5318.34 5351.15 5383.96 5416.76 5449.57 5482.38 5515.19 5548.00 5580.81 5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5256.00 5288.81 5321.62 5354.43 5387.24 5420.05 5452.85 5485.66 5518.47 5551.28 5584.09 5649.71 5682.52 5715.38 5748.14 5780.94 5813.75 5846.56	5259.28 5292.09 5324.90 5357.71 5390.52 5423.33 5456.14 5488.94 5521.75 5554.56 5587.37 5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5262.56 5295.37 5328.18 5560.99 5393.80 5426.61 5429.42 5492.23 5557.84 5590.65 5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5265.84 5298.65 5331.46 5364.27 5397.08 5429.89 5462.70 5495.51 5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5269.12 5301.93 5334.74 5367.55 5400.36 5433.17 5465.98 5498.79 5531.60 5564.40 5597.21 5630.02 5662.83 5695.64 5728.45	5272.40 5305.21 5338.02 5370.85 5403.64 5436.45 5502.07 5534.88 5567.69 5600.49 5633.30 5666.11 5698.92 5731.73	5275.69 5308.49 5341.30 5374.11 5406.92 5439.73 5472.54 5505.35 5538.16 5570.97 5603.78 5669.39 5702.20 5735.01 5767.82 5800.63	5278.97 5311.78 5344.58 5377.39 5410.20 5443.01 5475.82 5508.63 5541.44 5574.25 5607.06 5639.87 5672.67 5705.48 5738.29 5771.10 5803.91
1610	5282.25 5315.06 5347.87 5380.67 5413.48 5446.29 5479.10 5511.91 5544.72 5577.53 5610.34 5643.15 5675.96 5741.57 5741.38 5807.19 5840.00 6872.81 5905.62	5285.53 5318.34 5351.15 5383.96 5416.76 5449.57 5482.38 5515.19 5548.00 5580.81 5613.62 5646.43 5679.24 5772.65 5744.85 5810.47 5813.28 5876.09	5288.81 5321.62 5354.43 5387.24 5420.05 5452.85 5485.66 5518.47 5551.28 5584.09 5616.90 5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5292.09 5324.90 5357.71 5390.52 5423.33 5456.14 5488.94 5521.75 5554.56 5587.37 5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5295.37 5328.18 5360.99 5393.80 5426.61 5459.42 5492.23 5525.03 5557.84 5590.65 5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5298.65 5331.46 5364.27 5397.08 5429.89 5462.70 5495.51 5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5301.93 5334.74 5367.55 5400.36 5433.17 5465.98 5498.79 5531.60 5564.40 5597.21 5630.02 5662.83 5695.64 5728.45	5305.21 5338.02 5370.85 5403.64 5436.45 5469.26 5502.07 5534.88 5567.69 5600.49 5633.30 5666.11 5698,92 5731.73	5308.49 5341.30 5374.11 5406.92 5439.73 5472.54 5505.35 5538.16 5570.97 5603.78 5636.58 5669.39 5702.20 5735.01 5767.82 5800.63	5311.78 5344.58 5377.39 5410.20 5443.01 5475.82 5508.63 5541.44 5574.25 5607.06 5639.87 5705.48 5738.29 5771.10 5803.91
1620	5315.06 5347.87 5380.67 5413.48 5446.29 5479.10 5511.91 5544.72 5577.53 5610.34 5643.15 5675.96 5741.57 5774.38 5840.00 5872.81 5905.62	5318.34 5351.15 5383.96 5416.76 5449.57 5482.38 5515.19 5548.00 5580.81 5613.62 5646.43 5679.24 5777.66 5777.66 5810.47 5813.28 5876.09	5321.62 5354.43 5387.24 5420.05 5452.85 5485.66 5518.47 5551.28 5584.09 5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5324.90 5357.71 5390.52 5423.33 5456.14 5488.94 5521.75 5554.56 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5328.18 5360.99 5393.80 5426.61 5459.42 5492.23 5525.03 5557.84 5590.65 5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5331.46 5364.27 5397.08 5429.89 5462.70 5495.51 5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5334.74 5367.55 5400.36 5433.17 5465.98 5498.79 5531.60 5597.21 5630.02 5662.83 5695.64 5728.45 5761.26 5794.07	5338.02 5370.85 5403.64 5436.45 5469.26 5502.07 5534.88 5567.69 5600.49 5633.30 5666.11 5698,92 5731.73	5341.30 5374.11 5406.92 5439.73 5472.54 5505.35 5538.16 5570.97 5603.78 5636.58 5669.39 5702.20 5735.01 5767.82 5800.63	5344.58 5377.39 5410.20 5443.01 5475.82 5508.63 5541.44 5574.25 5607.06 5639.87 5705.48 5738.29 5771.10 5803.91
1630	5347.87 5380.67 5413.48 5446.29 5479.10 5511.91 5544.72 5577.53 5610.34 5643.15 5675.96 5774.38 5807.19 5840.00 5872.81 5905.62	5351.15 5383.96 5416.76 5449.57 5482.38 5515.19 5548.00 5580.81 5613.62 5646.43 5679.24 5772.66 5810.47 5813.28 5876.09	5354.43 5387.24 5420.05 5452.85 5485.66 5518.47 5551.28 5584.09 5616.90 5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5357.71 5390.52 5423.33 5456.14 5488.94 5521.75 5554.56 5587.37 5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5360.99 5393.80 5426.61 5459.42 5492.23 5525.03 5557.84 5590.65 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5364.27 5397.08 5429.89 5462.70 5495.51 5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5367.55 5400.36 5433.17 5465.98 5498.79 5531.60 5564.40 5597.21 5630.02 5662.83 5695.64 5728.45 5761.26 5794.07	5370.85 5403.64 5436.45 5469.26 5502.07 5534.88 5567.69 5600.49 5633.30 5666.11 5698,92 5731.73 5764.54 5797.35	5374.11 5406.92 5439.73 5472.54 5505.35 5538.16 5570.97 5603.78 5636.58 5669.39 5702.20 5735.01 5767.82 5800.63	5377.39 5410.20 5443.01 5475.82 5508.63 5541.44 5574.25 5607.06 5639.87 5705.48 5738.29 5771.10 5803.91
1640   5 1650   5 1660   5 1670   5 1680   5 1690   5 1700   5 1710   5 1720   5 1740   5 1740   5 1750   5 1760   5 1760   5 1780   5 1800   6 1810   5 1820   5 1830   6 1840   6 1850   6 1870   6 1870   6 1890   6	5380.67 5413.48 5446.29 5479.10 5511.91 5544.72 5577.53 5610.34 5643.15 5675.96 57741.57 5774.38 5807.19 5840.00 5872.81 5905.62	5383.96 5416.76 5449.57 5482.38 5515.19 5548.00 5580.91 5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5387.24 5420.05 5452.85 5485.66 5518.47 5551.28 5584.09 5616.90 5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5390.52 5423.33 5456.14 5488.94 5521.75 5554.56 5587.37 5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5393.80 5426.61 5459.42 5492.23 5525.03 5557.84 5590.65 5623.46 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5397.08 5429.89 5462.70 5495.51 5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5400.36 5433.17 5465.98 5498.79 5531.60 5564.40 5597.21 5630.02 5662.83 5695.64 5728.45 5761.26 5794.07	5403.64 5436.45 5469.26 5502.07 5534.88 5567.69 5600.49 5666.11 5698.92 5731.73 5764.54 5797.35	5406.92 5439.73 5472.54 5505.35 5538.16 5570.97 5603.78 5669.39 5702.20 5735.01 5767.82 5800.63	5410.20 5443.01 5475.82 5508.63 5541.44 5574.25 5607.06 5639.87 5672.67 5705.48 5738.29 5771.10 5803.91
1650   5   1660   5   1670   5   1680   5   1740   5   1740   5   1740   5   1750   5   1760   5   1760   5   1760   5   1760   5   1760   5   1760   5   1800   1810   1820   1830   1840   60   1850   61   1870   61   1890   62   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900	5413.48 5446.29 5479.10 5511.91 5544.72 5577.53 5610.34 5643.15 5675.96 5708.76 5774.38 5807.19 5840.00 5872.81 5905.62	5416.76 5449.57 5482.38 5515.19 5548.00 5580.81 5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5420.05 5452.85 5485.66 5518.47 5551.28 5584.09 5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5423.33 5456.14 5488.94 5521.75 5554.56 5587.37 5622.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5426.61 5459.42 5492.23 5525.03 5557.84 5590.65 5623.46 5665.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5429.89 5462.70 5495.51 5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5433.17 5465.98 5498.79 5531.60 5564.40 5597.21 5630.02 5662.83 5695.64 5728.45	5436.45 5469.26 5502.07 5534.88 5567.69 5600.49 5633.30 5666.11 5698.92 5731.73 5764.54 5797.35	5439.73 5472.54 5505.35 5538.16 5570.97 5603.78 5669.39 5702.20 5735.01 5767.82 5800.63	5443.01 5475.82 5508.63 5541.44 5574.25 5607.06 5639.87 5775.48 5738.29 5771.10 5803.91
1660   5   1690   5   1700   5   1710   5   1740   5   1740   5   1750   1760   1770   5   1780   5   1800   1810   1820   1830   1840   60   1850   61   1850   61   1850   61   1850   62   1890   62   1900   62   1900   62   1900   62   1900   62   1800   62   1900   62   1800   62   1900   62   1800   62   1900   62   1800   62   1900   62   1800   62   1900   62   1800   6	5446.29 5479.10 5511.91 5544.72 5577.58 5610.34 5643.15 5675.96 5708.76 5741.57 5774.38 5807.19 5840.00 5872.81 5905.62	5449.57 5482.38 5515.19 5548.00 5580.91 5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5452.85 5485.66 5518.47 5551.28 5584.09 5616.90 5649.71 5682.52 5715.38 5748.14 5780.94 5813.75 5846.56	5456.14 5488.94 5521.75 5554.56 5587.37 5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5459.42 5492.23 5525.03 5557.84 5590.65 5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5462.70 5495.51 5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5465.98 5498.79 5531.60 5564.40 5597.21 5630.02 5662.83 5695.64 5728.45 5761.26 5794.07	5469.26 5502.07 5534.88 5567.69 5600.49 5633.30 5666.11 5698.92 5731.73 5764.54 5797.35	5472.54 5505.35 5538.16 5570.97 5603.78 5636.58 5669.39 5702.20 5735.01 5767.82 5800.63	5475.82 5508.63 5541.44 5574.25 5607.06 5639.87 5072.67 5705.48 5738.29 5771.10 5803.91
1670   5   1680   5   1700   5   1710   5   1720   5   1740   5   1740   5   1760   1770   1780   1810   1820   1820   1840   60   1850   61   1870   61   1890   62   1900   62   1900   62   1900   62   1900   62   1900   62   1800   62   1900   62   1800   62   1900   62   1800   62   1900   62   1800   62   1900   62   1800   62   1900   1900   62   1900	5479.10 5511.91 5544.72 5577.58 5610.34 5643.15 5675.96 5708.76 5774.38 5807.19 5840.00 5872.81	5482.38 5515.19 5548.00 5580.81 5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5485.66 5518.47 5551.28 5584.09 5616.90 5649.71 5682.52 5715.38 5748.14 5780.94 5813.75 5846.56	5488.94 5521.75 5554.56 5587.37 5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5492.23 5525.03 5557.84 5590.65 5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5495.51 5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5498.79 5531.60 5564.40 5597.21 5630.02 5662.83 5695.64 5728.45 5761.26 5794.07	5502.07 5534.88 5567.69 5600.49 5633.30 5666.11 5698.92 5731.73 5764.54 5797.35	5505.35 5538.16 5570.97 5603.78 5636.58 5669.39 5702.20 5735.01 5767.82 5800.63	5508.63 5541.44 5574.25 5607.06 5639.87 5672.67 5705.48 5738.29 5771.10 5803.91
1680   5   1700   5   1710   5   1720   5   1740   5   1740   5   1760   1770   1780   1810   5   1820   5   1820   1840   60   1850   61   1850   61   1850   62   1890   62   1900   62   1900   62   1900   62   1900   62   1800   62   1900   62   1800   62   1900   62   1800   62   1900   62   1800   62   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   1900   190	5511.91 5544.72 5577.53 5610.34 5643.15 5675.96 5708.76 57741.57 5774.38 5807.19 5840.00 5872.81	5515.19 5548.00 5580.81 5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5518.47 5551.28 5584.09 5616.90 5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5521.75 5554.56 5587.37 5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5525.03 5557.84 5590.65 5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5528.32 5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5531.60 5564.40 5597.21 5630.02 5662.83 5695.64 5728.45 5761.26 5794.07	5534.88 5567.69 5600.49 5633.30 5666.11 5698.92 5731.73 5764.54 5797.35	5538.16 5570.97 5603.78 5636.58 5669.39 5702.20 5735.01 5767.82 5800.63	5541.44 5574.25 5607.06 5639.87 5672.67 5705.48 5738.29 5771.10 5803.91
1690   5 1700   5 1710   5 1720   5 1730   5 1740   5 1760   5 1770   56 1790   58 1800   58 1810   58 1820   58 1830   66 1840   60 1850   61 1870   61 1890   62 1900   62	5544.72 5577.53 5610.34 5643.15 5675.96 5708.76 5741.57 5774.38 5807.19 5840.00 5872.81 5905.62	5548.00 5580.91 5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5551.28 5584.09 5616.90 5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5554.56 5587.37 5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5557.84 5590.65 5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5561.12 5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5564.40 5597.21 5630.02 5662.83 5695.64 5728.45 5761.26 5794.07	5567.69 5600.49 5633.30 5666.11 5698.92 5731.73 5764.54 5797.35	5570.97 5603.78 5636.58 5669.39 5702.20 5735.01 5767.82 5800.63	5574.25 5607.06 5639.87 5672.67 5705.48 5738.29 5771.10 5803.91
1700   5   1710   5   1720   5   1730   5   1740   5   1750   1760   5   1770   5   1780   1810   5   1820   5   1820   5   1830   6   1840   6   1850   6   1870   6   1890   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6   1890   1890   6   1890   6   1890   6   1890   6   1890   6   1890   6	5577.53 5610.34 5643.15 5675.96 5708.76 5741.57 5774.38 5807.19 5840.00 5872.81 5905.62	5580.81 5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5584.09 5616.90 5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5587.37 5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5590.65 5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5593.93 5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5597.21 5630.02 5662.83 5695.64 5728.45 5761.26 5794.07	5600.49 5633.30 5666.11 5698.92 5731.73 5764.54 5797.35	5603.78 5636.58 5669.39 5702.20 5735.01 5767.82 5800.63	5607.06 5639.87 5672.67 5705.48 5738.29 5771.10 5803.91
1710   5   1720   5   1730   5   1740   5   1750   5   1760   5   1770   5   1790   5   1800   1810   1820   1830   60   1840   60   1850   61   1870   61   1890   62   1900   62   1900   62   1900   62   1900   62   1900   62   1900   62   1900   62   1700   1700   1700   62   1700   62   1700   62   1700   62   1700   62   1700   62   1700   62   1700   62   1700   62   1700	5610.34 5643.15 5675.96 5708.76 5741.57 5774.38 5807.19 5840.00 5872.81	5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5616.90 5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5620.18 5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5626.74 5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5630.02 5662.83 5695.64 5728.45 5761.26 5794.07	5633.30 5666.11 5698.92 5731.73 5764.54 5797.35	5636.58 5669.39 5702.20 5735.01 5767.82 5800.63	5639.87 5672.67 5705.48 5738.29 5771.10 5803.91
1710   5   1720   5   1730   5   1740   5   1750   5   1760   5   1770   5   1790   5   1800   1810   1820   1830   60   1840   60   1850   61   1870   61   1890   62   1900   62   1900   62   1900   62   1900   62   1900   62   1900   62   1900   62   1700   1700   1700   62   1700   62   1700   62   1700   62   1700   62   1700   62   1700   62   1700   62   1700   62   1700	5610.34 5643.15 5675.96 5708.76 5741.57 5774.38 5807.19 5840.00 5872.81	5613.62 5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5623.46 5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5662.83 5695.64 5728.45 5761.26 5794.07	5666.11 5698.92 5731.73 5764.54 5797.35	5669.39 5702.20 5735.01 5767.82 5800.63	5639.87 5672.67 5705.48 5738.29 5771.10 5803.91
1720   5   1730   5   1740   5   1750   5   1760   5   1770   5   1780   5   1800   1810   1820   1830   60   1840   60   1850   61   1870   61   1890   62   1900   1900	5643.15 5675.96 5708.76 5741.57 5774.38 5807.19 5840.00 6872.81	5646.43 5679.24 5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5649.71 5682.52 5715.33 5748.14 5780.94 5813.75 5846.56	5652.99 5685.80 5718.61 5751.42 5784.23 5817.03 5849.84	5656.27 5689.08 5721.89 5754.70 5787.51 5820.32 5853.12	5659.55 5692.36 5725.17 5757.98 5790.79 5823.60	5662.83 5695.64 5728.45 5761.26 5794.07	5666.11 5698.92 5731.73 5764.54 5797.35	5669.39 5702.20 5735.01 5767.82 5800.63	5672.67 5705.48 5738.29 5771.10 5803.91
1730   5   1740   5   1750   5   1760   5   1770   5   1780   5   1890   6   1810   1820   1830   6   1840   6   1850   6   1870   6   1890   6	5708.76 5741.57 5774.38 5807.19 5840.00 6872.81	5712.05 5744.85 5777.66 5810.47 5843.28 5876.09	5715.33 5748.14 5780.94 5813.75 5846.56	5718.61 5751.42 5784.23 5817.03 5849.84	5721.89 5754.70 5787.51 5820.32 5853.12	5725.17 5757.98 5790.79 5823.60	5728.45 5761.26 5794.07	5731.73 5764.54 5797.35	5735.01 5767.82 5800.63	5738.29 5771.10 5803.91
1740   5 1750   5 1760   5 1770   5 1780   5 1790   5 1800   5 1810   5 1820   5 1830   6 1840   6 1850   6 1860   6 1870   6 1890   6 1890   6 190	5708.76 5741.57 5774.38 5807.19 5840.00 6872.81	5744.85 5777.66 5810.47 5843.28 5876.09	5748.14 5780.94 5813.75 5846.56	5751.42 5784.23 5817.03 5849.84	5754.70 5787.51 5820.32 5853.12	5757.98 5790.79 5823.60	5761.26 5794.07	5764.54 5797.35	5767.82 5800.63	5771.10 5803.91
1760   50   1770   56   1780   56   1790   56   1810   58   1820   56   1840   60   1850   61   1850   61   1850   62   1890   62   1900   1900   62   1900	5774.38 5807.19 5840.00 5872.81 5905.62	5777.66 5810.47 5843.28 5876.09	5780.94 5813.75 5846.56	5784.23 5817.03 5849.84	5787.51 5820.32 5853.12	5790.79 5823.60	5794.07	5797.35	5800.63	5803.91
1760   50   1770   56   1780   56   1790   56   1810   58   1820   56   1840   60   1850   61   1850   61   1850   62   1890   62   1900   1900   62   1900	5774.38 5807.19 5840.00 5872.81 5905.62	5777.66 5810.47 5843.28 5876.09	5780.94 5813.75 5846.56	5784.23 5817.03 5849.84	5787.51 5820.32 5853.12	5790.79 5823.60	5794.07	5797.35	5800.63	5803.91
1770   56 1780   58 1790   58 1810   58 1820   56 1830   60 1840   60 1850   61 1870   61 1890   62 1900   62	5807.19 5840.00 5872.81 5905.62	5810.47 5843.28 5876.09	5813.75 5846.56	5817.03 5849.84	5820.32 5853.12	5823.60	7	MANAGEMENT OF THE PARTY OF THE	SAMONE	
1780   50   1790   58   1810   58   1820   58   1840   60   1850   61   1870   61   1890   62   1900   62   1900   62	5840.00 5872.81 5905.62	5843.28 5876.09	5846.56	5849.84	5853.12		5826.88	5830.16	5833.44	5836 79
1790   58 1800   58 1810   58 1820   58 1830   60 1840   60 1850   60 1870   61 1890   62 1900   62	5872.81 5905.62	5876.09				5856.401		17.5	C. L. Contraction of the Contrac	
1800 55 1810 55 1820 55 1830 66 1840 60 1850 60 1870 61 1890 62 1900 62	5905.62		5879.37	5882.651			5859.69	5862.97	5866.25	5869.53
1810 59 1820 58 1830 60 1840 60 1850 61 1870 61 1890 62 1900 62		5008 00			0000.00	5889.21	5892.49	5895.78	5899.06	5902.34
1820 59 1830 60 1840 60 1850 60 1860 61 1870 61 1890 62 1900 62		0000.00	5912.18	5915.46	5918.74	5922.02	5925.30	5928.58	5931.87	5935.15
1830 60 1840 60 1850 60 1860 61 1870 61 1890 62 1900 62	938.43	5941.71	5944.99	5948.27	5951.55	5954.83	5958.11	5961.39	5964.67	5967.96
1840 60 1850 60 1860 61 1870 61 1880 61 1890 62	971.24	5974.52	5977.80	5981.08	5984.36	5987.64	5990.92	5994.20	5997.48	6000.76
1850 60 1860 61 1870 61 1880 61 1890 62	004.05	6007.33	6010.61	6013.89	6017.17	6020.45	6023.73	6027.01	6030.29	6033.57
1860   61 1870   61 1880   61 1890   62 1900   62	036.85	6040.14	6043.42	6046.70	6049.98	6053.26	6056.54	6059.82	6063.10	6066.38
1870   61 1880   61 1890   62 1900   62	069.66	6072.94	6076.23	6079.51	6082.79	6086.07	6089.35	6092.63	6095.91	6099.19
1880   61 1890   62 1900   62	102.47	6105.75	CONTRACTOR OF STREET	IC NITEDA	6115.60		THE RESERVE OF THE PARTY OF THE	Charles Indiana	6128.72	6132.00
1890   62 1900   62	135.28	6138.56	6141.84	6145.12	6148.40	Mile Stored	OF BELLEVILLE	and the same of the last	6161.53	6164.81
1900 62	168.09	6171.37	100000	OR WHILE BY	DAY LESS WILL	THE PARKET !	C. HOLL	March Street	6194.34	6197.62
The state of the s	200.90	6204.18	1000	CALL STREET	6214.02	NOT YOUR IN	GO STREET	OVER MANAGES		6230.43
The state of the s	233.71	6236.99	6240.27	6243.55	6246.83	6250 11	6253.39	6256.67	6259.96	6263.24
1910 62	Contractor (see	6269.80	Control of the last	and the same				C2 Table 54.5		6296.05
BARRIOTE STATE OF	and the same of th	6302.61	-	SECTION AND ADDRESS.	6312.45	STREET, STREET	And the same			6328.85
Marine Co.	are the suite	6335.42		and the second	6345.26		and the last of th		6358.38	6361.66
The second second	Children of the	THE CASE VALUE OF	The state of the s	STATISTICS.		61.01/6.003.32.31				6394.47
1950 63	397 75	6401.02	6104 99	6407 00	6410.00	0414.10	C415 44	C490 = 2	0.101.00	0.40# 00
1960 6	6430.56	6433.84	6437.12	6440 41	6442 60	6414.16				
		6466.65	6469.93	6472 21	6476 40	6470 70	6450.25			6460.09
	6463.37	200.00	6502 74	6506.09	6500 20	6519 50	6483.06 6515.87	The second second	A STATE OF THE STA	6492.90 6525.71
	6463.37	6499.46	COOM. 14	6538 83	6542 11	6545 20		202223 41714	6555.24	6558.52
	6463.37 6496.18	6499.46 6532.27	6535.55	000000	0072011			0001.00	Charles and the same of the sa	
	5463.37 5496.18 5528.99	6532.27	6535.55 6568.36	6571.64	6574.92	6578.20	6581.48	6584.76	6588.05	6591.33

2000 to 2399.

Metres.		7-1		( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (	Metres.	(Units)				
1120100	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
2000	Eng.Feet. 6561.80	Eng.Feet. 6565.08		1	Eng.Feet. 6574.92	Eng.Feet. 6578.20	Eng.Feet. 6581.48	Eng.Feet. 6584.76	Eng.Feet. 6588.05	
2010	6594.61	6597.89	The state of the s		6607.73	6611.01	6614.29	6617.57	6620.85	6624.1
2020	6627.42	6630.70	1		6640.54	6643.82	6647.10	6650.38	St. 100 1 1 1 2	11327140
2030	6660.23	6663.51	6666.79			6676.63	6679.91	6683.19	6686.47	6689.7
2040	6693.03	6696.32				6709.44	6712.72		6719.28	6722.5
2050	6725.84	6729.12	6732.41	6735.69	6738.97	6742.25	6745.53	6748.81	6752.09	6755.8
2060	6758.65	6761.93	6765.21	6768.49	6771.78	6775.06	6778.34	6781.62	6784.90	6788.1
2070	6791.46	6794.74	6798.02	6801.30	6804.58	6807.87	6811.15	6814.43	6817.71	6820.9
2080	6824.27	6827.55	6830.83	6834.11	6837.39	6840.67	6843.96	6847.24	6850.52	6853.8
2090	6857.08	6860.36	6863.64	6866.92	6870.20	6873.48	6876.76	6880.05	6883.33	100000
2100	6889.89	6893.17	6896.45	6899.73	6903.01	6906.29	6909.57	6912.85	6916.14	6919.4
2110	6922.70	6925.98	6929.26	6932.54	6935.82	6939.10	6942.38	6945.66	6948.94	6952.5
2120	6955.51	6958.79	The second second		6968.63	6971.91	6975.19	6978.47	6981.75	6985.0
2130	6988.32	6991.60	6994.88	6998.16	7001.44	7004.72	7008.00	7011.28	7014.56	7017.8
2140	7021.12	7024.41	7027.69	7030.97	7034.25	7037.53	7040.81	7044.09	7047.37	7050.6
2150	7053.93	7057.21	7060.49	7063.78	7067.06	7070.34	7073.62	7076.90	7080.18	7083.4
2160	7086.74	7090.02	7093.30	7096.58	7099.87	7103.15	7106.43	7109.71	7112.99	7116.5
2170	7119.55	7122.83	7125.11	7129.39	7132.67	7135.96	7139.24	7142.52	7145.80	7149.0
2180	7152.36	7155.64	7158.92	7162.20	7165.48	7168.76	7172.05	7175.33	7178.61	7181.8
2190	7185.17	7188.45	7191.73	7195.01	7198.29	7201.57	7204.85	7208.14	7211.42	7214.7
2200	7217.98	7221.26	7224.54	7227.82	7231.10	7234.38	7237.66	7240.94	7244.23	7247.5
2210	7250.79	7254.07	7257.35	7260.63	7263.91	7267.19	7270.47	7273.75	7277.03	7280.3
2220	7283.60	7286.88	7290.16	7293.44	7296.72	7300.00	7303.28	7306.56	7309.84	7313.1
2230	7316.41	7319.69	7322.97	7326.25	7329.53	7332.81	7336.09	7339.37	7342.65	7345.9
2240	7349.21	7352.49	7355.78	7359.06	7362.34	7365.62	7368.90	7372.18	7375.46	7378.7
2250	7382.02	7385.30	7388.58	7391.87	7395.15	7398.43	7401.71	7404.99	7408.27	7411.5
2260	7414.83	7418.11	7421.39	7424.67	7427.96	7431.24	7434.52	7437.80	7441.08	7444.8
2270	7447.64	7450.92	7454.20	7457.48	7460.76	7464.05	7467.33	7470.61	7473.89	7477.1
2280	7480.45	7483.73	7487.01	7490.29		7496.85	7500.14	7503.42	7506.70	7509.9
2290	7513.26	7516.54	7519.82	7523.10	7526.38	7529.66	7532.94	7536.23	7539.51	7542.7
2300	7546.07	7549.35	7552.64	7555.91	7559.19	7562.47	7565.75	7569.03	7572.32	7575.6
2310	7578.88	7582.16	7585.44	7588.72	7592.00	7595.28	7598.56	7601.84	7605.12	7608.4
2320	7611.69	7614.97		7621.53		7628.09	7631.37	7634.65	7637.93	7641.2
2330	7644.50	7647.78		7654.34		7660.90	7664.18	7667.46	7670.74	7674.0
2340	7677.30	7680.58	7683.87	7687.15	7690.43	7693.71	7696.99	7700.27	7703.55	7706.8
2350	7710.11	7713.39		Contract of the Contract of th	7723.24			7733.08	7736.36	7739.6
2360	7742.92	7746.20	OF THE STREET	7752.76		7759.33	7762.61	7765.89		7772.4
2370	7775.73	7779.01	100 - 100 100 100	7785.57	Control of the Contro	7792.14	7795.42	7798.70	7801.98	7805.2
2380 2390	7808.54 7841.35	7811.82 7844.63		7818.38 7851.19	THE RESERVE TO THE PARTY OF	7824.94 7857.75	7828.23 7861.03	7831.51 7864.32	A COLUMN TO THE PARTY OF	7838.0 7870.8
								.004.02		1010.0
(S. S. A. )	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

## 2400 to 2799.

					Metres.	(Units)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
18	Eng.Feet.	Eng.Feet.		Eng.Feet.	-	Eng. Feet.	Eng.Feet.	Eng.Feet.		Eng.Fee
2400 •	7874.16	7877.44		100000000000000000000000000000000000000	7887.28	7890.56	7893.84	7897.12		7903.6
2410	7906.97	7910.25		7916.81		7923.37	7926.65	7929.93	STATE OF THE PARTY	7936.5
2420	7939.78	7943.06		7949.62	7952.90	7956.18	7959.46	7962.74		7969.3
2430	7972.59	7975.87		7982.43		7988.99	7992.27	7995.55		8002.1
2440	8005.39	8008.67	8011.96	8015.24	8018.52	8021.80	8025.08	8028.36	8031.64	8034.9
2450	8038.20	8041.48	8044.76	8048.05	8051.33	8054.61	8057.89	8061.17	8064.45	8067.7
2460	8071.01	8074.29	8077.57	8080.85	8084.14	8087.42	8090.70	8093.98	8097.26	8100.
2470	8103.82	8107.10	8110.38	8113.66	8116.94	8120.22	8123.51	8126.79	8130.07	8133.
2480	8136.63	8139.91	8143.19	8146.47	8149.75	8153.03	8156.32	8159.60	8162.88	8166.
2490	8169.44	8172.72	8176.00	8179.28	8182.56	8185.84	8189.12	8192.41	8195.69	8198.
2500	8202.25	8205.53	8208.81	8212.09	8215.37	8218.65	8221.93	8225.21	8228.50	8231.
2510	8235.06	8238.34		8244.90		8251.46	8254.74	8258.02	8261.30	8264.
2520	8267.87	8271.15		8277.71	8280.99	8284.27	8287.55	8290.83		8297.
2530	8300.67	8303.96		8310.52	8313.80	8317.08	8320.36	8323.64	8326.92	8330.
2540	8333.48	8336.76		8343.33		8349.89	8353.17	ADDITION OF THE PARTY OF THE PA	8359.73	8363.
2550	8366.29	8369.37	8372 85	8376.14	8379 49	8382.70	8385.98	8389 26	8392.54	8395.
2560	8399.10	8402.38		8408.94		8415.51	8418.79	A CONTRACTOR	8425.35	8428.
2570	8431.91	8435.19		8441.75		8448.32	8451.60	Library Control	8458.16	8461.
2580	8464.72	8468.00		8474.56		8481.12	8484.41	The State of the S	8490.97	1000000
2590	8497.53	8500.81			8510.65	8513.93	8517.21	8520.50	MARKET THE PARTY OF	8527.
2600	8530.34	8533.62	8526 00	8540.18	95 19 16	8546.74	8550.02	8559 90	8556.58	8559.
2610	8563.15	8566.43		8572.99		8579.55	8582.83		8589.39	8592.
2620	8595.96	8599.24		8605.80		8612.36	8615.64		8622.20	8625.
2630	8628.76	8632.05		8638.61	8641.89	8645.17	8648.45		8655.01	8658.
2640	8661.57	8664.85		8671.42	The second	8677.98	8681.26		8687.82	8691.
2650	8694.38	000m cc	0=00 04	000400	000000	00000000	083408	0818 05	0=00 00	0700
2660	8727.19	8697.66		8704.23		8710.79	8714.07		8720.63	8723.
2670	8760.00	8730.47 8763.28		8737.03		8743.60	8746.88		8753.44	8756.
2680	8792.81	8796.09		8769.84 8802.65		8776.41	8779.69		8786.25	8789. 8822.
2690	8825.62	8828.90		8835.46	1231	8809.21 8842.02	8812.50 8845.30	8848.59	8819.06 8851.87	8855.
2700	8050 40	9961 #1	0064.00	0000 0	00**	00#1.00	00#0 **	000* 60	0004.0~	000=
2710	8858.43	8861.71		8868.27		8874.83	2.00		8884.67	8887.
2720	8891.24 8926.05	8894.52		8901.08		8907.64	8910.92		8917.48	8920.
2730		8927.33		8933.89		8940.45	8943.73	8947.01	A STATE OF THE PARTY OF THE PAR	8953.
2740	8956.85 8989.66	8960.14 8992.94		8966.70 8999.51		8973.26 9006.07	8976.54 9009.35	8979.82 9012.63		8986. 9019.
9750	0000 45	0007								00=0
2750	9022.47	9025.75				9038.88			9048.72	9052.
2760	9055.28	9058.56	9061.84			9071.69		ALCOHOLD TO THE	9081.53	9084.
2770	9088.09	9091.37		9097.93		9104.50	9107.78	9111.06	a transmitted	9117.
2780 2790	9120.90 9153.71	9124.18 9156.99		9130.74 9163.55		9137.30 9170.11	9140.59 9173.39	9143.87 9176.68	The second	9150. 9183.
-	0.	1.	2.	3.	4.	5.	6,	7.	8.	9.

#### 2800 to 3000.

				ALCOHOL:	Metres.	(Units.)				-
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.
	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng. Feet.	Eng. Feet.	Eng.Feet.	Eng.Fee
2800	9186.52	9189.80	9193.08	9196.36	9199.64	9202.92	9206.20	9209.48	9212.76	9216.0
2810	9219.33	9222.61	9225.89	9229.17	9232.45	9235.73	9239.01	9242.29	9245.57	9248.8
2820	9252.14	9255.42	9258.70	9261.98	9265.26	9268.54	9271.82	9275.10	9278.38	9281.6
2830	9284.94	9288.23	9291.51	9294.79	9298.07	9301.35	9304.64	9307.91	9311.19	9314.4
2840	9317.75	9321.03	9324.32	9327.60	9330.88	9334.16	9337.44	9340.72	9344.00	9347.2
2850	9350.56	9353.84	9357.12	9360.41	9363.69	9366.97	9370.25	9373.53	9376.81	9380.0
2860	9383.37	9386.65	9389.93	9393.21	9396.50	9399.78	9403.06	9406.34	9409.62	9412.9
2870	9416.18	9419.46	9422.74	9426.02	9429.30	9432.59	9435.87	9439.15	9442.43	9445.7
2880	9448.99	9452.27	9455.55	9458.83	9462.11	9465.39	9468.68	9471.96	9475.24	9478.5
2890	9481.80	9485.08	9488.36	9491.64	9494.92	9498.20	9501.48	9504.76	9508.05	9511.3
2900	9514.61	9517.89	9521.17	9524.45	9527.73	9531.01	9534.29	9537.57	9540.85	9544.1
2910	9547.42	9550.70	9553.98	9557.26	9560.54	9563.82	9567.10	9570.38	9573.66	9576.9
2920	9580.23	9583.51	9586.79	9590.07	9593.35	9596.63	9599.91	9603.19	9606.47	9609.7
2930	9613.03	9616.32	9619.60	9622.88	9626.16	9629.44	9632.72	9636.00	9639.28	9642.5
2940	9645.84	9649.12	9652.41	9655.69	9658.97	9662.25	9665.53	9668.81	9672.09	9675.3
2950	9678.62	9681.93	9685.21	9688.50	9691.78	9695.06	9698.34	9701.62	9704.90	9708.1
2960	41	THE RESERVOIS	9718.02	THE RESERVE OF THE PARTY.	and the same of the same	Committee of the Commit	The second		Name of Street	
2970	9744.27	9747.55	9750.83	9754.11	9757.39	9760.68	9763.96	9767.24	9770.52	9773.8
2980	9777.08	9780.36	9783.64	9786.92	9790.20	9793.48	9796.76	9800.05	9803.33	9806.6
2990	9809.89	9813.17	9816.45	9819.73	9823.01	9826.29	9829.57	9832.85	9836.14	9839.4
3000	9842.70	9845.98	9849.26	9852.54	9855.82	9859.10	9862.38	9865.66	9868.94	9872.2

## Proportional Parts.

Metres.			1	1	1	1	1	1	1	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng.Feet.	Eng.Fee								
0	0.0000	0.3281	0.6562	0.9843	1.3124	1.6404	1.9685	2.2966	2.6247	2.952
1	3.2809	3.6090	3.9371	4.2652	4.5933	4.9213	5.2494	5.5775	5.9056	6.233
2	6.5618	6.8899	7.2180	7.5461	7.8742	8.2022	8.5303	8.8584	9.1865	9.514
3	9.8427	10.1708	10.4989	10.8270	11.1551	11.4831	11.8112	12.1393	12.4674	12.795
4	13.1236	13.4517	13.7798	14.1079	14.4360	14.7640	15.0921	15.4202	15.7483	16.076
5	16.4045	16.7326	17.0607	17.3888	17.7169	18.0449	18.3730	18.7011	19.0292	19.357
6	19.6854	20.0135	20.3416	20.6697	20.9978	21.3258	21.6539	21.9820	22.3101	22.638
7	22.9663	23.2944	23.6225	23.9506	24.2787	24.6067	24.9348	25.2629	25.5910	25.919
8	26.2472	26.5753	26.9034	27.2315	27.5596	27.8876	28.2157	28.5438	28.8719	29.200
9	29.5281	29.8562	30.1843	30.5124	30.8405	31.1685	31.4966	31.8247	31.1528	32,480
April 1	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 3.28070878 American Feet.

Metres.					Hund	lreds.				
housands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Am Feet.	Am Feet	Am. Feet.	Am. Feet.	Am. Feet.	Am.Feet	Am.Feet.	Am. Feet.	Am.Feet	Am.Fe
0	0.0	328.1	656.1	984.2	1312.3	1640.4	1968.4	2296.5	2624.6	2952
1000	3280.7	3608.8	3936.9	4264.9	4593.0	4921.1	5249.1	5577.2	5905.3	623
2000	6561.4	6889.5	7217.6	7545.6	7873.7	8201.8	8529.8	8857.9	9186.0	951
3000	9842.1	10170.2	10498.3	10826.3	11154.4	11482.5	11810.6	12138.6	12466.7	1279
4000	13122.8	13450.9	13779.0	14107.0	14435.1	14763.2	15091.3	15419.3	15747.4	1607
5000	16403.5	16731.6	17059.7	17387.8	17715.8	18043.9	18372.0	18700.0	19028.1	1935
6000	19684.3	20012.3	20340.4	20668.5	20996.5	21324.6	21652.7	21980.7	22308.8	2263
7000	22965.0	23293.0	23621.1	23949.2	24277.2	24605.3	24933.4	25261.5	25589.5	2591
8000	26245.7	26573.7	26901.8	27229.9	27558.0	27886.0	28214.1	28542.2	28870.2	2919
9000	29526.4	29854.4	30182.5	30510.6	30838.7	31166.7	31494.8	31822.9	32150.9	3247
Tens.		E T	2.	3.	4.	5.	6.	7.	8.	9
Alexander of the second	0.	1.								
	100000		Am Foot	Am Foot	Am Foot	Am Foot	Am Feet	Am Foot	Am Feet	Am T
	Am. Feet	Am Feet.	Am. Feet	Am. Feet. 9.842	Am.Feet 13.123	Am Feet. 16.404	Am. Feet. 19.684	Am.Feet. 22.965	Am Feet. 26.246	1
0	Am Feet 0.000	Am Feet. 3.281	6.561	9.842	13.123	16.404	19.684	22.965	26.246	29.
0 10	Am Feet 0.000 32.807	Am Feet. 3.281 36.088	6.561 39.369	9.842 42.649	13.123 45.930	16.404 49.211	19.684 52.491	22.965 55.772	26.246 59.053	29. 62.
0	Am Feet 0.000	Am Feet. 3.281 36.088 68.895	6.561 39.369 72.176	9.842	13.123 45.930 78.737	16.404 49.211 82.018	19.684	22.965 55.772 88.579	26.246	29. 62. 95.
0 10 20	Am Feet 0.000 32.807 65.614	Am Feet. 3.281 36.088 68.895 191.702	6.561 39.369 72.176 104.983	9.842 42.649 75.456	13.123 45.930 78.737 111.544	16.404 49.211	19.684 52.491 85.298 118.106	22.965 55.772 88.579	26.246 59.053 91.860 124.667	29. 62. 95. 127.
0 10 20 30 40	Am Feet 0.000 32.807 65.614 98.421	Am Feet. 3.281 36.088 68.895 191.702	6.561 39.369 72.176 104.983	9.842 42.649 75.456 108.263	13.123 45.930 78.737 111.544	16.404 49.211 82.018 114.825 147.632	19.684 52.491 85.298 118.106 150.913	22.965 55.772 88.579 121.386 154.193	26.246 59.053 91.860 124.667 157.474	29. 62. 95. 127. 160.
0 10 20 30	Am Feet 0.000 32.807 65.614 98.421 131.228	Am Feet. 3.281 36.088 68.895 191.702 134.509	6.561 39.369 72.176 104.983 137.790	9.842 42.649 75.456 108.263	13.123 45.930 78.737 111.544 144.351	16.404 49.211 82.018 114.825 147.632	19.684 52.491 85.298 118.106 150.913 183.720	22.965 55.772 88.579 121.386 154.193 187.000	26.246 59.053 91.860 124.667 157.474	29. 62. 95. 127. 160.
0 10 20 30 40	Am Feet 0.000 32.807 65.614 98.421 131.228 164.035	Am Feet. 3.281 36.088 68.895 191.702 134.509	6.561 39.369 72.176 104.983 137.790 170.597	9.842 42.649 75.456 108.263 141.070 173.878	13.123 45.930 78.737 111.544 144.351	16.404 49.211 82.018 114.825 147.632	19.684 52.491 85.298 118.106 150.913 183.720	22.965 55.772 88.579 121.386 154.193	26.246 59.053 91.860 124.667 157.474	29. 62. 95. 127. 160.
0 10 20 30 40	Am Feet 0.000 32.807 65.614 98.421 131.228 164.035 196.843	Am Feet. 3.281 36.088 68.895 191.702 134.509 167.316 200.123	6.561 39.369 72.176 104.983 137.790 170.597 203.404	9.842 42.649 75.456 108.263 141.070 173.878	13.123 45.930 78.737 111.544 144.351 177.158 209.965	16.404 49.211 82.018 114.825 147.632 180.439 213.246	19.684 52.491 85.298 118.106 150.913 183.720 216.527	22.965 55.772 88.579 121.386 154.193 187.000	26.246 59.053 91.860 124.667 157.474 190.281 223.088	29. 62. 95. 127. 160.
0 10 20 30 40 50 60	Am Feet 0.000 32.807 65.614 98.421 131.228 164.035 196.843 229.650	Am Feet. 3.281 36.088 68.895 191.702 134.509 167.316 200.123 232.930	6.561 39.369 72.176 104.983 137.790 170.597 203.404 236.211	9.842 42.649 75.456 108.263 141.070 173.878 206.685 239.492	13.123 45.930 78.737 111.544 144.351 177.158 209.965	16.404 49.211 82.018 114.825 147.632 180.439 213.246 246.053	19.684 52.491 85.298 118.106 150.913 183.720 216.527 249.334	22.965 55.772 88.579 121.386 154.193 187.000 219.807	26.246 59.053 91.860 124.667 157.474 190.281 223.088 255.895	160. 193. 226. 259.

#### IX. CONVERSION OF METRES INTO RHINE OR PRUSSIAN FEET AND DECIMALS.

1 Metre = 3.1861995 Rhine Feet.

Metres.					Hun	dreds.				
Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
MANGE ST	Rhine Ft.	Rhine Ft.	Rhine Ft.	Rhine Ft.	Rhine Ft.	Rhine Ft	Rhine Ft.	Rhine Ft.	Rhine Ft.	Rhine Ft.
0	0.0	318.6	637.2	955.9	1274.5	1593.1	1911.7	2230.3	2549.0	2867.6
1000	3186.2	3504.8	3823.4	4142.1	4460.7	4779.3	5097.9	5416.5	5735.2	6053.8
2000	6372.4	6691.0	7009.6	7328.3	7646.9	7965.5	8284.1	8602.7	8921.4	9240.0
3000	9558.6	9877.2	10195.8	10514.5	10833.1	11151.7	11470.3	11788.9	12107.6	12426.2
4000	12744.8	AND REAL PROPERTY.	A STATE OF THE PARTY OF THE PAR	170 700	14019.3	The second second second			1 1 1 1 1 1 1 C	
5000	15931.0	16249.6	16568.2	16886.9	17205.5	17524.1	17842.7	18161.3	18480.0	18798.6
6000					20391.7					
7000					23577.9					
8000					26764.1					
9000					29950.3					

## PARIS OR FRENCH FEET

## INTO DIFFERENT MEASURES OF LENGTH.

#### X. CONVERSION OF PARIS OR FRENCH FEET INTO TOISES.

1 French Foot = 0.1666666 Toise.

French Feet.					Hun	dreds.	nin est			
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
THE RESIDEN	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	Toises.	Toises-
0	0.00	16.67	33.33	50.00	66.67	83.33	100.00	116.67	133.33	150.00
1000	166.67	183.33	200.00	216.67	233.33	250.00	266.67	283.33	300.00	316.6
2000	333.33	350.00	366.67	383.33	400.00	416.67	433.33	450.00	466.67	483.3
3000	500.00	516.67	533.33	550.00	566.67	583.33	600.00	616.67	633.33	650.0
4000	666.67	683.33	700.00	716.67	733.33	750.00	766.67	783.33	800.00	816.6
5000	833.33	850.00	866.67	883.33	900.00	916.67	933.33	950.00	966.67	983.3
6000	1000.00	1016.67	1033.33	1050.00	1066.67	1083.33	1100.00	1116.67	1133.33	1150.0
7000	1166.67	1183.33	1200.00	1216.67	1233.33	1250.00	1266.67	1283.33	1300.00	1316.6
8000	1333.33	1350.00	1366.67	1383.33	1400.00	1416.67	1433.33	1450.00	1466.67	1483.3
9000	1500.00	1516.67	1533.33	1550.00	1566.67	1583.33	1600.00	1616.67	1633.33	1650.0
10000	1666.67	1683.33	1700.00	1716.67	1733.33	1750.00	1766.67	1783.33	1800.00	1816.6
11000	1833.33	1850.00	1866.67	1883.33	1900.00	1916.67	1933.33	1950.00	1966.67	1983.3
12000	2000.00	2016.67	2033.33	2050.00	2066.67	2083.33	2100.00	2116.67	2133.33	2150.0
13000	2166.67	2183.33	2200.00	2216.67	2233.33	2250.00	2266.67	2283.33	2300.00	2316.6
14000	2333.33	2350.00	2366.67	2383.33	2400.00	2416.67	2433.33	2450.00	2466.67	2483.3
15000	2500.00	2516.67	2533.33	2550.00	2566.67	2583.33	2600.00	2616.67	2633.33	2650.00
16000	2666.67	2683.33	2700.00	2716.67	2733.33	2750.00	2766.67	2783.33	2800.00	2816.6
17000	2833.33	2850.00	2866.67	2883.33	2900.00	2916.67	2933.33	2950.00	2966.67	2983.3
18000	3000.00	3016.67	3033.33	3050.00	3066.67	3083.33	3100.00	3116.67	3133.33	3150.00
19000	3166.67	3183.33	3200.00	3216.67	3233.33	3250.00	3266.67	3283.33	3300.00	3316.6
20000	3333.33	3350.00	3366.67	3383.33	3400.00	3416.67	3433.33	3450.00	3466.67	3483.33
21000	3500.00	3516.67	3533.33	3550.00	3566.67	3583.33	3600.00	3616.67	3633.33	3650.0
22000	3666.67	3683.33	3700.00	3716.67	3733.33	3750.00	3766.67	3783.33	3800.00	3816.6
23000	3833.33	3850.00	3866.67	3883.33	3900.00	3916.67	3933.33	3950.00	3966.67	3983.3
24000	4000.00	4016.67	4033.33	4050.00	4066.67	4083.33	4100.00	4116.67	4133.33	4150.0
25000	4166.67	4183.33	4200.00	4216.67	4233.33	4250.00	4266.67	4283.33	4300.00	4316.6
26000	4333.33	4350.00	4366.67	4383.33	4400.00	4416.67	4433.33	4450.00	4466.67	4483.3

## XI. CONVERSION OF PARIS OR FRENCH FEET INTO METRES.

1 Paris Foot = 0.32483943 Metres.

French Feet.					Huno	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	000.00	32.48	64.97	97.45	129.94	162.42	194.90	227.39	259.87	292.3
1000	324.84	357.32	389.81	422.29	454.78	487.26	519.74	552.23	584.71	617.1
2000	649.68	682.16	714.65	747.13	779.61	812.10	844.58	877.07	909.55	942.0
3000	974.52	1007.00	1039.49	1071.97	1104.45	1136.94	1169.42	1201.91	1234.39	1266.8
4000	1299.36	1331.84	1364.33	1396.81	1429.29	1461.78	1494.26	1526.75	1559.23	1591.7
5000	1624.20	1656.68	1689.16	1721.65	1754.13	1786.62	1819.10	1851.58	1384.07	1916.
6000	1949.04	1931.52	2014.00	2046.49	2078.97	2111.46	2143.94	2176.42	2208.91	2241.
7000	2273.88	2306.36	2338.84	2371.33	2403.81	2436.30	2468.78	2501.26	2533.75	2566.2
8000	2598.72	2631.20	2663.68	2696.17	2728.65	2761.14	2793.62	2826.10	2858.59	2891.0
9000	2923.55	2956.04	2988.52	3021.01	3053.49	3085.97	3118.46	3150.94	3183.43	3215.9
10000	3248.39	3280.88	3313.36	3345.85	3378.33	3410.81	3443.30	3475.78	3508.27	3540.
11000	11					3735.65		The second second	H. C. C. C.	
12000	100000000000000000000000000000000000000	3930.56	C025 000	100000000000000000000000000000000000000	100	4060.49		100000000000000000000000000000000000000		4190.
13000	4222.91	4255.40	4287.88	4320.36	4352.85	4385.33	4417.82	4450.30	4482.78	4515.
14000		4580.24	Director by		45	4710.07	San	ADDITION COMMITTEE	Market Colored	
15000	4872.59	4905.08	4937.56	4970.04	5002.53	5035.01	5067.49	5099.98	5132.46	5164.
16000		000	C. A		77.7	5359.85	The second second	WELL HOLD	HOS INC.	
17000				THE REAL PROPERTY.		5684.69	Control of the State of	The state of	1	1
18000		5879.59	70 10 10 10 10 10 10 10 10 10 10 10 10 10	5944.56	A.711, S.C. 10, A.7574	6009.53	6042.01	The state of the s	6106.98	11.11.11.11.11.11
19000		6204.43		1000	6301.88	T. 100 Page 1997	1000 1000	6399.34		
20000	6496.79	6529.27	6561.76	6594.24	6626.72	6659.21	6691.69	6724.18	6756.66	6789.
21000				1. 14. 1 P. 2 V. D.	the state of the state of	6984.05				
22000		7178.95		COLUMN TO STATE OF THE PARTY OF	7276.40	The second second	7341.37	10000	7406.34	13414
23000		7503.79	7536.27	7568.76	C. Leading		7666.21	CONTRACTOR OF STREET	7731.18	
24000		7828.63				7958.57			0.000	-
25000	8120.99	8159 17	8185 05	2912 44	8950 09	8283.41	8915 80	8118 27	8880 86	8413
26000				11 11 11 11 11 11 11 11 11 11 11	THE PARTY OF THE P	8608.24	7			
27000	8770.66									
		NEED NO.	A tel Sen		Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
100 1001	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metre
0	0.0000	0.3248	0.6497	0.9745	1.2994	1.6242	1.9490	2.2739	2.5987	2.92
, 10	3.2484	3.5732	3.8981	4.2229	4.5478	4.8726	5.1974	5.5223	5.8471	6.17
20	6.4968	6.8216		7.4713					9.0955	
30	9.7452	10.0700	10.3949	10.7197	11.0445	11.3694	11.6942	12.0191	12.3439	12.668
40	12.9936	13.3184	13.6433	13.9681	14.2929	14.6178	14.9426	15.2675	15.5923	15.91
50	16.2420	16.5668	16.8916	17.2165	17.5413	17.8662	18.1910	18.5158	18.8407	19.16
60	19.4904	19.8152	20.1400	20.4649	20.7897	21.1146	21.4394	21.7642	22.0891	22.41
70	22.7388	23.0636	23.3884	23.7133	24.0381	24.3630	24.6878	25.0126	25.3375	25.66
80	25.9872	26.3120	26.6368	26.9617	27.2865	27.6114	27.9362	28.2610	28.5859	28.910
90	90 9955	20 5601	90 9959	20 2101	20 52 10	30.8597	91 1016	91 500 (	21 82 12	29 150

1 French Foot = 1.06576527 English Feet.

rench Feet.					Hund	lreds.				
housands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
with a	Eng. feet.	Eng. feet.	Eng feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. fee
0	0.0	106.6	213.2		426.3	532.9	639.5	746.0		959.
1000	1065.8	1172.3	1278.9			1598.6			1	2025.
2000	2131.5	2238.1	2344.7			2664.4			-171	3090.
3000	3197.3	3303.9	3410.4	CONTRACT OF		3730.2		10.77	Land State Control	THE .
4000	4263.1	4369.6	4476.2	4582.8	4689.4	4795.9	4902.5	5009.1	5115.7	5222
5000	5328.8	5435.4	5542.0	5648.6	5755.1	5861.7	5968.3	6074.9	6181.4	6288.
6000	6394.6	6501.2	6607.7	6714.3	6820.9	6927.5	7034.1	7140.6	7247.2	7353.
7000	7460.4	7566.9	7673.5	7780.1	7886.7	7993.2	8099.8	8206.4	8313.0	8419.
8000	8526.1	8632.7	8739.3	8845.9	8952.4	9059.0	9165.6	9272.2	9378.7	9485
9000	9591.9	9698.5	9805.0	9911.6	10018.2	10124.8	10231.3	10337.9	10444.5	10551.
10000	10657 7	10764 9	10870 8	10077 4	11084.0	11190 5	11207 1	11.102 7	11510.3	11616
11000	7.7	11830.0	DESCRIPTION OF THE PARTY OF THE	12043.1	DY-12 1 2	TOTAL STREET, TO	STANGET OF STA	CONTRACTOR OF THE PARTY OF THE	12576.0	AMERICA.
12000	12 11 2	12895.8	MARKET STATE	13108.9	C-5-5-12 11	DESIGNATION OF THE PARTY OF THE	Tall States of the	Control of the contro	13641.8	A STATE OF THE STA
13000	1 1/6	WHICH SHELL		14174.7	FROM BUILDING		1990 DOLL W. J. S.	PRIDATE PERO	14707.6	
14000	14920.7		ONNESTE	15240.4		ESISSIBILANDO	TOTAL STATE OF THE PARTY OF THE	CANDO PULS.	15773.3	
		LICILIA I	20091	etairle.		anchi c	ALC:			0000
15000		THE STREET STREET	PS 14 8000 34 1 6.4	COLLEGE	16412.8	<b>医中国自由公司</b>		NOTES THE PERSON NAMED IN		
16000		17158.8		17372.0		17585.1	TO SHALL THE		17904.9	3371375
17000	The second second	10(4/4) 11 11	1	18437.7	DESCRIPTION OF	18650.9	Carried State of Table	100000000000000000000000000000000000000	18970.6	
18000		19290.4 20356.1	19396.9 20462.7	19503.5 20569.3	F 2 5 5 5 5 5 1	19716.7	19823.2		20036.4 21102.2	7 2 7 7 7
13000	40245.5	20330.1	20402.1	20.909.9	20075.0	20102.4	20009.0	20333.0	21102.2	21200
20000	21315.3	21421.9	21528,5	21635.0	21741.6	21848.2	22054.8	22161.3	22167.9	22274
21000				22700.8		22914.0		17.1		
22000			D. F. ST. SHOW SEE	23766.6	A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	(300017/TH)	20 To 100		24299.5	
23000	24512.6	24619.2	24725.8	24832.3	24938.9	25045.5	25152.1	25258.6	25365.2	25471.
24000	25578.4	25684.9	25791.5	25898.1	26004.7	26111.3	26217.8	26324.4	26431.0	26537.
25000	266441	96750 7	96057 9	20000	27070.4	27177.0	97909 B	97900 9	97106 7	97609
26000	C 72 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	27816.5	AND THE STATE OF T	28029.6		28242.8	CARLEST PARTY			
27000					29202.0					
				and the	Un					
Tens.					OII.	165.				
.0	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
William !		Eng. feet.			Eng. feet.	Eng. feet.		-		Eng. fee
0	0.000	1.066	2.132	3.197	4.263	5.329	6.395	7.460	8.526	9.59
10	10.658	11.723	12.789	13.855	14.921	15.986	17.052	18.118	19.184	20.25
20	21.315	22.381	23.447		25.578		27.710	28.776	29.841	30.90
30 40	31.973 42.631	33.039 43.696	34.104 44.762	35.170 45.828	36.236 46.894	37.302 47.959	38.368 49.025	39.433 50.091	40.499 51.157	41.56 52.22
							Salvin.	A		
50	53.288	54.354	55.420	56.486	57.551	58.617	59.683	60.749	THE RESERVE OF THE PARTY OF THE	62.88
60	63.946	65.012	66.077	67.143	68.209	69.275	70.341	71.406	CONTRACTOR OF THE PARTY OF THE	73.53
CONTRACTOR OF THE PARTY OF THE										
70 80	74.604 85.261	75.669 86.327	76.735 87.393	77.801 88.459	78.867 89.524	79.932	80.998 91.656	82.064 92.722	83.130 93.787	84.19 94.85

1 French Foot = 1.0657034 American Foot.

French Feet.				9	Hun	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
E PACK A	Am. Feet.	Am. Feet	Am. Feet.	Am. Feet.	Am Feet	Am. Feet.	Am. Feet.	Am. Feet.	Am.Feet	Am.Feet
0	0.0		213.1	319.7	426.3	532.9	639.4	746.0	852.6	959.1
1000	1065.7			1385.4	1492.0	1598.6	1705.1	1811.7		2024.8
2000	2131.4	2238.0	2344.5	2451.1	2557.7	2664.3	2770.8	2877.4		3090.
3000	3197.1	3303.7	3410.3		- 10-010	3730.0	3836.5	3943.1	4049.7	4156.
4000	4262.8	4369.4	4476.0	4582.5	4689.1	4795.7	4902.2	5008.8	5115.4	5221.
5000	5328.5	5435.1	5541.7	5648.2		5861.4	5967.9	6074.5	1000	6287.
6000	6394.2	6500.8	6607.4	6713.9	6820.5	V 4 V 4 C C C C	7033.6			
7000	7459.9	7566.5	7673.1	7779.6	7886.2	7992.8	8099.3	8205.9	8312.5	8419.
8000	8525.6	8632.2	8738.8	8845.3	8951.9	9058.5	9165.1	9271.6	9378.2	9484.
9000	9591.3	9697.9	9804.5	9911.0	10017.6	10124.2	10230.8	10337.3	10443.9	10550.
10000	10657.0	10763.6	10870.2	10976.7	11083.3	11189.9	11296.5	11403.0	11509.6	11616.
11000	11722.7	11829.3	11935.9	12042.5	12149.0	12255.6	12362.2	12468.7	12575.3	12681.
12000	12788.4	12895.0	13001.6	13108.2	13214.7	13321.3	13427.9	13534.4	13641.0	13747.
13000	13854.1	13960.7	14067.3	14173.9	14280.4	14387.0	14493.6	14600.1	14706.7	14813.
14000	14919.9	15026.4	15133.0	15239.6	15346.1	15452.7	15559.3	15665.8	15772.4	15879.
15000	15985.6	16092.1	16198.7	16305.3	16411.8	16518.4	16625.0	16731.5	16838.1	16944.
16000	HIPP TO C	100 S 100 P 100	17 A B U.S. B 1	Contract to	3 52 2 6 5	17584.1	DINCE OF	0.000.37164	MARKET STATES	1.035882021
17000	WALLEY TO STATE OF	CONTRACTOR OF	11.05.24.30	22222222	1277	18649.8		Secretary State of the	LOUGHTER	7131A722
18000	ACCURATE TO	1 1000 1000 1000		Contract Con	4.0	19715.5	# 11 C C C C C C C C C C C C C C C C C C	2149 3.45 3.45	20035.2	Charles I
19000						20781.2				
20000	212141	91490 G	91597 9	91699 2	21740 4	21846.9	21052 5	22060 1	22166 6	22272
21000						22912.6				
22000	A			TO HIS YOUR BEEN		23978.3				
23000	CALL TO SERVICE					25044.0				and the second
24000		Acres and a second		THE R. P. LEWIS CO., LANSING, MICH.		26109.7		and the second second	16429.4	The second state of
25000	26642 6	96740 0	OCOEE W	00000	0#000 O	00105 4	0*000 A	0#900 e	07405 0	07601
26000	the state of the state of	The second second		The second second	The second second	27175.4	Street Bridge			
27000					THE RESERVE TO THE RE	28241.1	Contract of the Contract of th			
						29306.8 30372.6				
					Un					
Tens.					OII	105.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
		Am. Feet.	Am Feet	Am.Feet.	Am Feet	Am Feet.	Am.Feet.	Am Feet.	Am. Feet	Am. Feet
0	0.00	1.07	2.13	3.20	4.26	5.33	6.39	7.46	8.53	9.59
10	10.66	11.72	12.79	13.85	14.92	15.99	17.05	18.12	19.18	20.25
20	21.31	22.38	23.45	24.51	25.58	26.64	27.71	28.77	29.84	30.91
30	31.97	33.04	34.10	35.17	36.23	37.30	38.37	39.43	40.50	41.56
40	42.63	43.69	44.76	45.83	46.89	47.96	49.02	50.09	51.15	52.22
50	53.29	54.35	55.42	56.48	57.55	58.61	59.68	60.75	61.81	62.88
60	63.94	65.01	66.07	67.14	68.21	69.27	70.34	71.40	72.47	73.53
70	74.60	75.66	76.73	77.80	78.86	79.93	80.99	82.06	83.12	84.19
80	85.26	86.32	87.39	88.45	89.52	90.58	91.65	92.72	93.78	94.85
90	95.91	96.98	98.04	99.11	A STATE OF THE PARTY OF THE PAR				The second second	105.50

## ENGLISH YARDS AND FEET

INTO DIFFERENT MEASURES OF LENGTH.

XIV. CONVERSION OF ENGLISH YARDS INTO FRENCH TOISES.

1 English Yard = 0.4691465 Toise.

English Yards	3-23-3	(fleibins	tomit?		Hund	lreds.	<b>-2006</b> (1)		LAPET .	POSE
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	Toises.
0	0.00	46.91	93.83	140.74	187.66	234.57	281.49	328.40	375.32	422.23
1000	469.15	516.06	562.98	609.89	656.80	703.72	750.63	797.55	844.46	891.38
2000	938.29	985.21	1032-12	1079.04	1125.95	1172.87	1219.78	1266.70	1313.61	1360.52
3000	1407.44	1454.35	1501.27	1548.18	1595.10	1642.01	1688.93	1735.84	1782.76	1829.67
4000	1876.59	1923.50	1970.41	2017.33	2064.24	2111.16	2158.07	2204.99	2251.90	2298.82
5000	2345.73	2392.65	2439.56	2486.48	2533.39	2580.31	2627.22	2674.13	2721.05	2767.96
6000	2814.88	2861.79	2908.71	2955.62	3002.54	3049.45	3096.37	3143.28	3190.20	3237.11
7000		BOLD THE STATE OF	OF THE REAL PROPERTY.	11111011111	3471.68	CHECKS 4-17 ACL J	200 37170	0.052 (0.1 No. 1 a)	CONTRACTOR OF THE PARTY OF THE	
8000		1 1 1000 - 1000	THE RESERVE TO SERVE BY	1512 2000 610	3940.83	HORESCO TO A CITY	CONTRACTOR OF THE	The second second		
9000	1453400000200	4269.23	200	CONTRACTOR	PERMITTED STATES	CONTRACTOR OF THE PARTY OF THE	CONTRACT 1 WILL	ALT THE RESERVE	- Awar 5 11 -	

#### XV. CONVERSION OF ENGLISH YARDS INTO METRES.

1 English Yard = 0.91438348 Metre.

English Yards.			MANAGE S	atter.	Hune	ireds.			Ven en u	
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
Tel.ha	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	CONTRACTOR OF THE PARTY OF THE		A STATE OF THE STA	T02-05-9:359	A35-58, 171-4	THE STATE OF	SALES YOUR	And better states	100
1000	914.38	1005.82	1097.26	1188.70	1280.14	1371.58	1463.01	1554.45	1645.89	1737.33
2000	1828.77	1920.21	2011.64	2103.08	2194.52	2285.96	2377.40	2468.84	2560.27	2651.71
3000	2743.15	2834.59	2926.03	3017.47	3108.90	3200.34	3291.78	3383.22	3474.66	3566.10
4000	3657.53	3748.97	3840.41	3931.85	4023.29	4114.73	4206.16	4297.60	4389.04	4480.48
5000	4571.92	4663.36	4754.79	4846.23	4937.67	5029.11	5120.55	5211.99	5303.42	5394.86
6000	5486.30	5577.74	5669.18	5760.62	5852.05	5943.49	6034.93	6126.37	6217.81	6309.25
7000	6400.68	6492.12	6583.56	6675.00	6766.44	6857.88	6949.31	7040.75	7132.19	7223.63
8000					THE PERSON AND	7772.26		DITELLY STREET	CAPTER TO THE PERSON	and the same of
9000	8229.45			MALE AND ADDRESS OF THE PARTY O	125 CO. W. L. 1853	SECTION AND ADDRESS.	1940.152.15	COLUMN TWO IS NOT	CONTRACTOR OF STREET	C 4143 CC

## XVI. CONVERSION OF ENGLISH FEET INTO METRES.

1 English Foot = 0.30479449 Metre.

English Feet.					Hund	reds.				
housands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	. Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	000.000	13000000	60.9589	91.4383	121.918	152.397		213.356	100000000000000000000000000000000000000	
1000	1					457.192		518.151		
2000			670.548	701.027	731.507	761.986				883.90
3000				2010114		1066.78		1127.74		
4000	1219.18	1249.66	1280.14	1310.62	1341.10	1371.58	1402.05	1432.53	1463.01	1493.4
5000	1523.97	1554.45	1584.93	1615.41	1645.89	1676.37	1706.85	1737.33	1767.81	1798.2
6000	1828.77	1859.25	1889.73	1920.21	1950.68	1981.16	2011.64	2042.12	2072.60	2103.0
7000	2133.56	2164.04	2194.52	2225.00	2255.48	2285.96	2316.44	2346.92	2377.40	2407.8
8000	2438.36	2468.84	2499.31	2529.79	2560.27	2590.75	2621.23	2651.71	2682.19	2712.6
9000	2743.15	2773.63	2804.11	2834.59	2865.07	2895.55	2926.03	2956.51	2986.99	3017.4
10000	3047.94	3078.42	3108.90	3139.38	3169.86	3200.34	3230.82	3261.30	3291.78	3322.5
11000	3352.74	3383.22	3413.70	3444.18	3474.66	3505.14	3535.62	3566.10	3596.57	3627.0
12000		AND THE RESERVE	3718.49	3748.97			3840.41	Store on a		
13000		3992.81		4053.77		4114.73	4145.21	4175.68	4206.16	4236.0
14000		4297.60	4228.08		<b>生态扩展型流电影</b>	4419.52	4450.00	4480.48	4510.96	4541.
15000			4632.88	CHARLE AND		The same of the sa	4754.79			THE PERSON LAND
16000	HOLD TO STOR	4907.19	400000	4968.15	The Part of the	5029.11	CHROLIN P. T. V. H.	5090.07		300000
17000	5181.51	5211.99	5242.47	5272.94	5303.42	5333.90	5364.38	5394.86	5425.34	5455.8
18000		5516.78		5577.74		5638.70		5699.66		
19000		5821.57		5882.53	ALTERNATION CO.	5943.49	5973.97	DOLL N. U.	6034.93	Disto
20000	10,111,122	6126.37	1,013	6187.33		6248.29	6278.77	100000	6339.73	1
21000	0.0000000000000000000000000000000000000	ARREST LOSS	DESCRIPTION OF LIB	MANGE STATE	6522.60	6553.08	6583.56	116/1900	CANCEL SECTION	1000000
22000		6735.96	15 ING 17 ( P. II)	6796.92	THE RESERVE	6857.88	100000000000000000000000000000000000000	6918.83	1375 A TO 1 1 1 1	A65/31754
23000	7010.27	7040.75	7071.23	7101.71	7132.19	7162.67	7193.15	7223.63	7254.11	7284.
24000	Contraction of	The state of the state of			7436.99					
25000		7650.34	Participant of	7711.30	CAP BY LEVEL OF	7772.26	Laboration of the laboration o	7833.22		
26000		7955.14		1420539.1	8046.57	A PERSONAL PROPERTY.			to ble to l	THE REAL PROPERTY.
27000				AND DESCRIPTION OF	8351.37	With a Print Tales (School)	Charles and the later had	The second second	The state of the s	
28000			CONTRACTOR OF	The State of the Land	8656.16		The second second			CONTRACTOR DESIGNATION OF THE PERSON OF THE
					Un	its.				AND HER
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	35.4	35.1	75.4	35.4	36.7	75./	35.1	35.1	75.1
0		Metres. 0.30479	Metres.	Metres. 0.91438	Metres. 1.21918	Metres. 1.52397	Metres. 1.82877	Metres.	Metres. 2.43836	Metre
10	PARTY 18 14	1-11-12-12	The second second	LABORAGO AND	4.26712	44-84-20-490	1 C T	ARTHARAS TOR	1.0.2.5	4 Part 12.3
20	1	102777 A. O. L. W.	AL ALLES SAN	THE RESERVE AND THE PARTY OF TH	7.31507	14 SARRY 33 S 40 db	LONG TO SERVICE TO SER	Lateral		1 1 2 2 3 1 1
30										
					10.3630					
40	20000	132		344	13.4110					0.00
50 60					16.4589					
	10.2877	18.5925	118.8973	119.2021	19.5068	119.8116	20.1164	20.4212	20.7260	21.03
HOLDING AND AND	07 0000	01 010	0. 6	20 5-4-						
70 80	21.3356	21.6404	21.9452	22.2500	22.5548 25.6027	22.8596	23.1644	23.4692	23.7740	24.07

1 English Foot = 0.9382929 Paris Foot.

English Feet.				CATEDO N E A P	Hund	ireds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	1	13.	1
0	0.000	93.8	187.7	281.5	375.3	469.1	563.0	656.8	750.6	ALCO TO THE
1000	938.3	1032.1	1126.0	1219.8	1313.6	1407.4	1501.3	\$1000 A 1517 K	1688.9	- Cara Cara
2000	1876.6	1970.4	2064.2	2158.1	2251.9	2345.7	The second second	2010-00-0	NUMBER OF STREET	ARIO
3000	2814.9	2908.7	3002.5	3096.4	3190.2	3284.0	Deville Can	CALL STREET, N. S. V.	3565.5	
4000	3753.2	3847.0	3940.8	4034.7	4128.5	4222.3	4316.1	4410.0	4503.8	4597
5000	4691.5	4785.3	4879.1	4973.0	5066.8	5160.6	5254.4	5348.3	5442.1	5535
6000	5629.8	5723.6	5817.4	5911.2	6005.1	6098.9	6192.7	6286.6	6380.4	6474
7000	6568.0	6661.9	6755.7	6849.5	6943.4	7037.2	7131.0	7224.9	7318.7	7412
8000	7506.3	7600.2	7694.0	7787.8	7881.7	7975.5	8069.3	8163.1	8257.0	8350
9000	8444.6	8538.5	8632.3	8726.1	8820.0	8913.8	9007.6	9101.4	9195.3	9289
10000	9382.9	9476.8	9570.6	9664.4	9758.2	9852.1	9945.9	10039.7	10133.6	10227
11000		10415.0		10602.7	The second second	Action to the contract of		Control of the Control	11071.9	100000
12000		AND DESCRIPTION OF THE PARTY OF	11447.2	11541.0	San	2.71.21.27.20.21		TO SERVICE STREET	12010.1	
13000		1 MO AL	AND DESCRIPTION OF		12573.1		Control of the Control	Date In Co.	12948.4	Part Comment
14000	13136.1	13229.9	the same of the same	13417.6	Charles and the same	13605.2	13699.1	13792.9	13886.7	13980
75000	7.107.1		7 1000 0		11110		1 4000 4	* 4507 0	1,005.0	1 4070
15000				14355.9					14825.0	
16000					15388.0					
17000 18000					16326.3		1000	77.00	16701.6	1
19000	16889.3				17264.6 18202.9		Carlotte Control		17639.9	1000
13000	17027.0	17921.4	10013.2	10109.0	10202.9	10290.7	10000.0	10454.4	10010.2	10072
20000	18765.9	18859.7	18953.5	19047.3	19141.2	19235.0	19328.8	19422.7	19516.5	19610
21000	19704.1	19798.0	19891.8	19985.6	20079.5	20173.3	20267.1	20361.0	20454.8	20548
22000	20642.4	20736.3	20830.1	20923.9	21017.8	21111.6	21205.4	21299.2	21393.1	21486
23000	21580.7	21674.6	21768.4	21862.2	21956.0	22049.9	22143.7	22237.5	22331.4	22425
24000	22519.0	22612.9	22706.7	22800.5	22894.3	22988.2	23082.0	23175.8	23269.7	23363
25000	99 (57 9	09551 1	99615 0	99798 8	23832.6	22026 5	94090 9	94114 1	24208 0	2 1201
26000					24770.9					
27000			100000000000000000000000000000000000000		25709.2					
28000					26647.5					
20000	1	2000010	2010010	2000011			2000012	2002010	12102210	
Tens.	A ANTO			1 W 10 T	Un	its.	Sauch	Service	Million	THE SERVICE STREET
Et lie	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par.Feet.	Par. Fe
0	0.00	0.94	1.88	2.81	3.75	4.69	5.63	6.57	7.51	8.4
10	9.38	10.32	11.26	12.20	13.14	14.07	15.01	15.95	16.89	17.8
20	18.77	19.70	20.64	21.58	22.52	23.46	24.40	25.33	26.27	27.2
30	28.15	29.09	30.03	30.96	31.90	32.84	33.78	34.72	35.66	36.59
40	37.53	38.47	39.41	40.35	41.28	42.22	43.16	44.10	45.04	45.98
50	46.91	47.85	48.79	49.73	50.67	51.61	52.54	53.48	54.42	55.30
60	56.30	57.24	58.17	59.11	60.05	60.99	61.93	62.87	63.80	64.74
70	65.68	66.62	67.56	68.50	69.43	70.37	71.31	72.25	73.19	74.18
80	75.06	76.00	76.94	77.88	78.82	79.75	80.69	81.63	82.57	83.51

1 English Foot = 0.99994197 American Foot.

				14772.41	Hune	lreds.				
Eng. Feet. Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Am Feet.	Am. Feet.	Am. Feet.	Am Feet.	Am.Feet.	Am Feet	Am Feet.	Am. Feet.	Am Feet.	Am. Feet
0	0.00	The second second second	199.99	The state of the s			599.97	699.96	799.95	899.98
1000	999.94	1099.94	1199.93	1299.92	1399.92	1499.91	1599.91	1699.90	1799.90	1899.89
2000	1999.88	2099.88	2199.87	2299.87	2399.86	2499.85	2599.85	2699.84	2799.84	2899.83
3000	2999.83	3099.82	3199.81	3299.81	3399.80	3499.80	3599.79	3699.79	3799.78	3899.77
4000	3999.77	4099.76	4199.76	4299.75	4399.74	4499.74	4599.73	4699.73	4799.72	4899.72
5000	4999.71	5099.70	5199.70	5299.69	5399.69	5499.68	5599.68	5699.67	5799.66	5899.66
6000	5999.65	6099.65	6199.64	6299.63	6399.63	6499.62	6599.62	6699.61	6799.61	6899.60
7000	6999.59	7099.59	7199.58	7299.58	7399.57	7499.56	7599.56	7699.55	7799.55	7899.54
8000	7999.54	8099.53	8199.52	8299.52	8399.51	8499.51	8599.50	8699.50	8799.49	8899.48
9000	8999.48	9099.47	9199.47	9299.46	9399.45	9499.45	9599.44	9699.44	9799.43	9899.43
10000	9999.42	10099.4	10199.4	10299.4	10399.4	10499.4	10599.4	10699.4	10799.4	10899.4
11000	10999.4	11099.4	11199.4	11299.3	11399.3	11499.3	11599.3	11699.3	11799.3	11899.3
12000	11999.3	12099.3	12199.3	12299.3	12399.3	12499.3	12599.3	12699.3	12799.3	12899.2
13000	12999.2	13099.2	13199.2	13299.2	13399.2	13499.2	13599.2	13699.2	13799.2	13899.2
14000	13999.2	14099.2	14199.2	14299.2	14399.2	14499.2	14599.2	14699.1	14799.1	14899.1
15000	Design of the		10000	777	a share a london	15499.1	15599.1	15699.1	15799.1	15899.1

The following Table of Differences between English and American Feet, for every hundred feet, will make it easy to convert English into American Feet, or American into English Feet, by adding to, or subtracting from, the number of feet to be converted, which is contained in the first column, the numbers found in the other columns.

XIX. DIFFERENCES BETWEEN ENGLISH AND AMERICAN FEET.

To obtain English Feet add. To obtain American Feet subtract.

10000 American Feet = 10000.5803 English Feet.

Number of Feet.	A SOLITON	7-034-6	Hundreds			Number of Feet.			Hundreds	J.	
Thou- sands.	0.	200.	400.	600.	800.	Thou- sands.	0.	200.	400.	600.	800.
	Diff feet	Diff.feet	Diff feet	Diff.feet.	Diff feet		Diff.feet.	Diff.feet	Diff.feet	Diff feet.	Diff.feet
0	+0.000	+0.012	+0.023	±0.035	+0.046	15000	±0.870	+0.882	+0.894	+0.905	+0.917
1000	0.058	0.070	0.082	0.093	0.105	16000	0.928	0.940	0.952	0.963	0.975
2000	0.116	0.128	0.139	0.151	0.162	17000	0.987	0.998	1.010	1.021	1.033
3000	0.174	0.186	0.197	0.209	0.221	18000	1.045	1.056	1.068	1.079	1.091
4000	0.232	0.244	0.255	0.267	0.279	19000	1.103	1.114	1.126	1.137	1.149
5000	0.290	0.302	0.313	0.325	0.337	20000	1.161	1.172	1.184	1.195	1.207
6000	0.348	0.360	The same	0.383	0.395	21000	1.219	1.230	1.242	1.253	1.265
7000	0.406	0.418	0.429	0.441	0.453	22000	1.277	1.288	1.300	1.311	1.323
8000	0.464	0.476	0.487	0.499	0.511	23000	1.335	1.346	1.358	1.370	1.381
9000	0.522	0.534	0.546	0.557	0.569	24000	1.393	1.404	1.416	1.428	1.439
10000	0.580	0.592	0.604	0.615	0.627	25000	1.451	1.462	1.474	1.486	1.497
11000	0.638	0.650	0.662	0.673	0.685	26000	1.509	1.520	1.532	1.544	1.555
12000	0.696	0.708	0.720	0.731	0.743	27000	1.567	1.578	1.590	1.602	1.613
13000	0.754	0.766	0.778	0.789	0.801	28000	1.625	1.636	1.648	1.660	1.671
14000	0.812	0.824	17.00	0.847	0.859	29000	1.683	1.694	1.606	1.718	1.729

## AMERICAN YARDS AND FEET

INTO DIFFERENT MEASURES OF LENGTH

#### XY. CONVERSION OF AMERICAN YARDS INTO FRENCH TOISES.

1 American Yard = 0.4691737 Toise.

American Yards		94			Huno	ireds.	Paker.			
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
y and the	Torses.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	Coises.
0	0.30	46.92	93.83	140.75	187.67	234.59	281.50	328.42	375.34	422.2
1000	469.17	516.09	563.01	609.93	656.84	703.76	750.68	797.60	844.51	891.4
2000	938.35	985.26	1032-18	1079.10	1126.02	1172.93	1219.85	1266.77	1313.69	1360.6
3000	1407.52	1454.44	1501.36	1548.27	1595.19	1642.11	1689.02	1735.94	1782.86	1829.7
4000	1876.69	1923.61	1970.53	2017.45	2064.36	2111.28	2158.20	2205.12	2252.03	2298.9
5000	2345.87	2392.79	2439.70	2486.62	2533.54	2580.45	2627.37	2674.29	2721.21	2768.13
6000	2815.04	2861.96	2908.88	2955.79	3002.71	3049.63	3096.55	3143.46	3190.38	3237.30
7000	3284.22	3331.13	3378.05	3424.97	3471.88	3518.80	3565.72	3612.64	3659.55	3706.4
8000	3753.39	3800.31	3847.22	3894.14	5941.06	3987.98	4034.89	4081.81	4128.73	4175.6
9000	4222.56	4269.48	4316.40	4363.31	4410.23	4457.15	4504.07	4550.98	4597.90	4644.8

#### XXI. CONVERSION OF AMERICAN YARDS INTO METRES.

1 American Yard = 0.91443655 Metre.

American Yards.				(participate areas aces	Hune	ireds.	libes us,	ATTENDS:	generally.	O LINK
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	91.44	182.89	274.33	365.77	457.22	548.66	640.11	731.55	822.99
1000	914.44	1005.88	1097.32	1188.77	1280.21	1371.65	1463.10	1554.54	1645.99	1737.43
2000	1828.87	1920.32	2011.76	2103.20	2194.65	2286.09	2377.54	2468.98	2560.42	2651.87
3000	2743.31	2834.75	2926.20	3017.64	3109.08	3200.53	3291.97	3383.42	3474.86	3566.30
4000	3657.75	3749.19	3840.63	3932.08	4023.52	4114.96	4206.41	4297.85	4389.30	4480.74
5000	4572.18	4663.63	4755.07	4846.51	4937.96	5029.40	5120.84	5212.29	5303.73	5395.18
6000	5486.62	5578.06	5669.51	5760.95	5852.39	5943.84	6035.28	6126.72	6218.17	6309.61
7000	6401.06	6492.50	6583.94	6675.39	6766.83	6858.27	6949.72	7041.16	7132.61	7224.05
8000	7315.49	7406.94	7498.38	7589.82	7681.27	7772.71	7864.15	7955.60	8047.04	8138.49
9000	8229.93	8321.37	8412.82	8504.26	8595.70	8687.15	8778.59	8870.03	8961.48	9052.92

## XXII. CONVERSION OF AMERICAN FEET INTO METRES.

1 American Foot = 0.30481218 Metre.

Amer. Feet.				day's	Hund	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.00		60.96	91.44	121.92	152.41	182.89	213.37	243.85	274.3
1000	304.81	335.29	365.77	396.26	426.74	457.22	487.70	518.18	548.66	579.1
2000	609.62	640.11	670.59	701.07	731.55	762.03	792.51	822.99	853.47	883.9
3000	914.44	944.92	975.40	1005.88	1036.36	The state of the s	1097.32		19 July 19 19 19 19 19 19 19 19 19 19 19 19 19	
4000	1219.25	1249.73	1280.21	1310.69	1341.17	1371.65	1402.14	1432.62	1463.10	1493.5
5000	1524.06	1554.54	1585.02	1615.50	1645.99	1676.47	1706.95	1737.43	1767.91	1798.3
6000	1828.87	1859.35	1889.84	1910.32	1940.80	1971.28	2001.76	2032.24	2062.72	2093.2
7000	2123.69	2154.17	2184.65	2225.13	2255.61	2286.09	2316.57	2347.05	2377.54	2408.0
8000	2438.50	2468.98	2499.46	2529.94	2560.42	2590.90	2621.38	2651.87	2682.35	2712.8
9000	27,43.31	2773.79	2804.27	2834.75	2865.23	2895.72	2926.20	2956.68	2987.16	3017.6
10000	3048.12	3078.60	3109.08	3139.57	3170.05	3200.53	3231.01	3261.49	3291.97	3322.4
11000	3352.93	3383.42	3413.90	3444.38	3474.86	3505.34	3535.82	3566.30	3596.78	3627.2
12000	3657.75	3688.23	3718.71	3749.19	3779.67	3810.15	3840.63	3871.11	3901.60	3932.0
13000	3962.56	3993.04	4023.52	4054.00	4084.48	4114.96	4145.45	4175.93	4206.41	4236.8
14000	4267.37	4297.85	4328.33	4358.81	4389.30	4419.78	4450.26	4480.74	4511.22	4541.7
15000	4572.18	4602.66	4633.15	4662.63	4694.11	4724.59	4755.07	4785.55	4816.03	4846.5
16000		4907.48	the latest and the la	4968.44		THE RESERVE THE PARTY OF	5059.88	5090.36	5120.84	5151.8
17000		5212.29			5303.73	0.11100.11000.11	5364.69	PA 3 - 3 - 4	73 TO 8 10 CO	1000
18000		5517.10	5547.58	5578.06		5639.03	5669.51		5730.47	5760.9
19000				- N. C.	5913.36	12 3 4 4 5 4 5 7 1	5974.32	6004.80	6035.28	6065.7
20000	6096.24	6126.72	6157.21	6187.69	6218.17	6248.65	6279.13	6309.61	6340.09	6370.5
21000	6401.06	6431.54	6462.02	6492.50	6522.98	6553.46	6583.94	6614.42	6644.91	6675.3
22000	6705.87	6736.35	6766.83	6797.31	6827.79	6858.27	6888.76	6919.24	6949.72	6980.2
23000	7010.68	7041.16	7071.64	7102.12	7132.61	7163.09	7193.57	7224.05	7254.53	7285.0
24000	7315.49	7345.97	7376.45				7498.38	7528.86	7559.34	7589.8
25000	7620.30	7650.79	7681.27	7711.75	7742.23	7772.71	7803.19	7833.67	7864.15	7894.6
26000					8047.04					
27000					8351.85					
28000					8656.67					
Tens.					Un	its.		l wi		
-	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
AGE TOO	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.0000	0.3048	0.6096	0.9144	1.2192	1.5241	1.8289	2.1337	2.4385	2.743
10	3.0481	3.3529	3.6577	3.9626	4.2674	4.5722	4.8770	5.1818	5.4866	5.791
20	6.0962	6.4011	6.7059	7.0107	7.3155	7.6203	7.9251	8.2299	8.5347	
30 40	9.1444 12.1925	9.4492 12.4973	9.7540 12.8021	10.0588 13.1069	10.3636 13.4117	10.6684 13.7165	10.9732 14.0214	11.2781 14.3262	11.5829 14.6310	11.887 14.935
50	SOUTH LITTER	100	2/4/2		16.4599				II ERW	
60	18.2887	18.5935	18.8984	19.1032	19.4080	19.7128	20.0176	20.3224	20.6272	20.932
70	21.2369	21.5417	21.8465	22.2513	22.5561	22.8609	23,1657	23.4705	23.7754	24.080
80	24.3850	24.6898	24.9946	25.2994	25.6042	25.9090	26,2138	26.5187	26.8235	27.128
90	00 1001	04 4040	20 0	THE PARTY OF THE P	28.6523			-		A.

#### XXIII. CONVERSION OF AMERICAN FEET INTO PARIS OR FRENCH FEET.

1 American Foot = 0.93834737 Paris Foot.

Amer. Feet.					Hun	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par. Feet.	Par.Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par.Feet.	Par. Feet.	Par.Feet.	Par. Feet.	Par.Feet.
0	0.0	93.8	187.7	281.5	375.3	469.2	563.0	AT A STREET, SALES	750.7	844.5
1000	938.3	1032.2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10.11	and the second	1407.5	1501.4		1689.0	The state of the s
2000	1876.7	1970.5			The state of the s	2345.9	2439.7		2627.4	
3000	2815.0	2908.9		A CONTRACTOR OF THE PARTY OF TH	SELENIA VI	The state of the s	3378.1	100000000000000000000000000000000000000	3565.7	
4000	3753.4	3847.2	3941.1	4034.9	4128.7	4222.6	4316.4	4410.2	4504.1	4597.9
5000	4691.7	4785.6	4879.4	4973.2	5067.1	5160.9	5254.7	5348.6	5442.4	5536.2
6000	5630.1	5723.9	10 012000		CHARLES THE STREET	STATE OF STREET		797		6474.6
7000	6568.4	6662.3	6756.1	6849.9	6943.8	7037.6	7131.4	7225.3	7319.1	7412.9
8000	7506.8	7600.6	7694.4	7788.3	7882.1	7976.0	8069.8	8163.6	8257.5	8351.3
9000	8445.1	8539.0	8632.8	8726.6	8820.5	8914.3	9008.1	9102.0	9195.8	9289.6
	0000 =	0.000		00000	0	0040.0	0010 #		-0-0.	10000 0
10000	9383.5	9477.3				The second of th		10040.3		
11000 12000	100000000000000000000000000000000000000	THE RESERVE	CONTRACTOR OF THE PARTY OF THE	1.7 5.0		10791.0			C. Carlotte Property	The second second
13000						11729.3 12667.7		0.0000000000000000000000000000000000000	17.111.11	Link and the
14000	BOTTO STATE	The state of the s		The second		13606.0				11100
14000	101.00.9	10200.1	10024.0	19410.4	15512.2	13000.0	10000.0	19199.1	13007.3	10901.4
15000	14075.2	14169.0	14262.9	14356.7	14450.5	14544.4	14638.2	14732.1	14825.9	14919.7
16000	C 41 64 2 6 6 1 2	100 - 1		THE RESERVE TO STATE OF THE PARTY OF THE PAR	The state of the state of	15482.7				
17000				A CONTRACTOR OF THE PARTY OF TH	POR THUMB	16421.1		100000000000000000000000000000000000000	The second second	
18000	The second second			The Late Section		17359.4			Contract to the contract of	Particular and
19000	17828.6	17922.4	18016.3	18110.1	18203.9	18297.8	18391.6	18485.4	18579.3	18673.1
		1		acution			A STATE			
20000		V Arrest Land			12.00	19236.1	7.0	The state of the s		
21000			C 100 100 110	POST CALL IN		20174.5	ACTION AND DESCRIPTION OF THE PERSON OF THE	17.00		
22000		H 52 - 5 - 7 - 7 - 7		ALC: YES	THE STATE OF THE S	21112.8				
23000	A STATE OF THE PARTY.	CARRY LEFT.	120 1 100 17 12	Contract to the second	Delibera Charles	22051.2	STATES AND ADDRESS OF THE	122 - A. OD SO		
24000	22520.3	22614.2	22708.0	22801.8	22895.7	22989.5	23083.3	23177.2	23271.0	23364.8
25000	23458.7	23552.5	23646.4	23740.2	23834.0	23927.9	24021.7	24115.5	24209.4	24303.2
26000	The state of the state of	and the same	Alberta Market State State	and the state of t	Carlot and Control	24866.2		A STATE OF THE PARTY OF THE PAR		
27000					The second second	25804.5				
28000						26742.9				
					**					
MACE IN					Un	its.	Message			A TOLLUS
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
Harrie	Par.Feet.	Par. Feet.	Par.Feet.	Par. Feet.	Par.Feet.	Par.Feet.	Par.Feet.	Par.Feet	Par Feet	Par. Feet
0	0.00	0.94	1.88	2.82	3.75	4.69	5.63	6.57	7.51	8.45
10	9.38	10.32	11.26	12.20	13.14	14.08	15.01	15.95	16.89	17.83
20	18.77	19.71	20.64	21.58	22.52	23.46	24.40	25.34	26.27	27.21
30	28.15	29.09	30.03	30.97	31.90	32.84	33.78	34.72	35.66	36.60
40	37.53	38.47	39.41	40.35	41.29	42.23	43.16	44.10	45.04	45.98
50	46.92	47.86	48.79	49.73	50.67	51.61	52.55	53.49	54 49	55.96
60	56.30	57.24	58.18	59.12	60.05	60.99	61.93	62.87	54.42 63.81	55.36
70	65.68	66.62	67.56	68.50	69.44	70.38	71.31	72.25	73.19	64.75
80	75.07	76.01	76.94	77.88	78.82	79.76	80.70	81.64	82.57	83.51
90	84.45	85.39	86.33	87.27	88.20	89.14	90.08	91.02	91.96	92.90
	0 2.10	00.00	00.00	0,121	00.20	00.11	00.00	01.02	01.00	02.00

## KLAFTER AND FEET OF VIENNA

## INTO DIFFERENT MEASURES OF LENGTH.

1 KLAFTER OF VIENNA = 6 FEET OF VIENNA = 0.9730317 TOISE DU PÉROU.

From this value are derived the equations used in computing the following tables.

## XXIV. CONVERSION OF KLAFTER OF VIENNA INTO FRENCH TOISES.

1 Klafter = 0.9730317 Toise.

Klafter of Vienna				وعاليك	Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
They be was	Toises.	Toises	Toises.	Toises.						
0	0.00	97.30	194.61	291.91	389.21	486.52	583.82	681.12	778.43	875.73
1000	973.03	1070.33	1167.64	1264.94	1362.24	1459.55	1556.85	1654.15	1751.46	1848.76
2000	1946.06	2043.37	2140.67	2237.97	2335.28	2432.58	2529.88	2627.19	2724.49	2821.79
3000	2919.10	3016.40	3113.70	3211.00	3308.31	3405.61	3502.91	3600.22	3697.52	3794.82
4000	3892.13	3989.43	4086.73	4184.04	4281.34	4378.64	4475.95	4573.25	4670.55	4767.86
5000	4865.16	4962.46	5059.76	5157.07	5254.37	5351.67	5448.98	5546.28	5643.58	5740.89
Klafter.					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
(A) E P (A)	Toises.									
0	0.000	0.973	1.946	2.919	3.892	4.865	5.838	6.811	7.784	8.757
10	9.730	10.703	11.676	12.649	13.622	14.595	15.569	16.542	17.515	18.488
20	19.461	20.434	21.407	22.380	23.353	24.326	25.299	26.272	27.245	28.218
30	29.191	30.164	31.137	32.110	33.083	34.056	35.029	36.002	36.975	37.948
40	38.921	39.894	40.867	41.840	42.813	43.786	44.759	45.732	46.706	47.679
50	48.652	49.625	50,598	51.571	52.544	53.517	54.490	55.463	56.436	57.409
60	58.382	59.355	60.328	61.301	62.274	63.247	64.220	65.193	66.166	67.139
70	68.112	69.085	70.058	71.031	72.004	72.977	73.950	74.923	75.896	76.870
80	77.843	78.816	79.789	80.762	81.735	82.708	83.681	84.654		86.600
THE RESERVE AND THE PARTY OF TH	10.0			00.102	010100	020100	00.001	01.004	00.001	00.000

#### XXV. CONVERSION OF KLAFTER OF VIENNA INTO METRES.

1 Klafter = 1.8964741 Metres.

Klafter of Vienna.	A management of				Hun	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	189.65	379.29	568.94	758.59	948.24	1137.88	1327.53	1517.18	1706.88
1000	1896.47	2086.12	2275.77	2465.42	2655.06	2844.71	3034.36	3224.01	3413.65	3603.30
2000	3792.95	3982.60	4172.24	4361.89	4551.54	4741.19	4930.83	5120.48	5310.13	5499.77
3000	5689.42	5879.07	6068.72	6258.36	6448.01	6637.66	6827.31	7016.95	7206.60	7396.28
4000	7585.90	7775.54	7965.19	8154.84	8344.49	8534.13	8723.78	8913.43	9103.08	9292.72
Klafter.					Ur	its.				
Tens,	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.000		3.793	5.689		9.482	1000	13.275	15.172	17.068
10	18.965	20.861	22.758	24.654	26.551	28.447	30.344	32.240	34.136	36.033
20	37.929	39.826	41.722	43.619	45.515	47.412	49.308	51.205	53.101	54.998
30	56.894	58.791	60.687	62.584	64.480	66.377	68.273	70.170	72.066	73.962
40	75.859	77.755	79.652	81.548	83.445	85.341	87.238	89.134	91.031	92.927
50	94.824	96.720	93.617	100 519	102.409	101 200	106.203	108 000	100 005	111 909
60	DVISING	115.685	HARTELL .		121.374	123.271	THE RR.	127.064		
70	THE STREET	William T. Hallo	136.546	Company of the Park			144.132	The state of the s	Company of the Company	
80		The second second	The Contract	CONTRACT COMME	159.304	A STATE OF THE STA	163.097		185 16	172
90			C03/10000	REAL TOUR		180.165	The second		The second	Charles and the
Klafter of Vienna.					200,000	r French F				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par. Feet.	Par.Feet.		Par. Feet.			Par.Feet.			
0.00	0.00	583.82	1167.64	1751.46	2335.28	2919.10	3502.91	4086.73	4670.55	5254.37
1000			7005.83				9341.10			
2000			12844.0				15179.3	The state of the s		
3000			18682.2			Same Market and the	21017.5			
4000	23352.8	23936.6	24520.4	25104.2	25688.0	26271.9	26855.7	27439.5	28023.3	28607.1
Klafter.			101,22	arreit.	Un	its.		ta aka		
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.Feet.	Par.Feet.	Par.Feet.	Par.Feet.	Par. Feet.	Par.Feet.	Par. Feet.	Par.Feet.	Par.Feet.	Par.Feet.
0	0.00	5.84	. 11.68	17.51	23.35	29.19	35.03	40.87	46.71	52.54
10	58.38	64.22	70.06	75.90	81.73	87.57	93.41	99.25	105.09	110.93
20	116.76	122.60	128.44	134.28	140.12	145.95	151.79	157.63	163.47	169.31
30	175.15	180.98	186.82	192.66	198.50	204.34	210.17	216.01	221.85	227.69
40	233.53	239.37	245.20	251.04	256.88	262.72	268.56	274.39	280.23	286.07
50	291.91	297.75	303.59	309.42	315.26	321.10	326.94	332.78	338.62	344.45
60	350.29	356.13	361.97	367.81		379.48	385.32	391.16	397.00	402.84
70	408.67	414.51	420.35	426.19	432.03	437.86	443.70	449.54		461.22
80	467.06	472.89	478.73	484.57	490.41	496.25	502.08	507.92	455.38 513.76	519.60
						554.63		566.30		
30	020.74	301.20	201111	0 X 21.00	040.10	001.00	000.47	200.20	012.14	977.98

1 Klafter = 6.2221403 English Feet.

Klafter of Vienna				displaying the second	Hund	lreds.	1	1	Veh %	H 67
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
Mary III	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng fee
0	0.00					3111.07				
1000	6222.14	6844.35	7466.57	8088.78	8711.00	9333.21	9955.42	10577.6	11199.9	11822.
2000						15555.4				
3000	18666.4	19288.6	19910.8	20533.1	21155.3	21777.5	22399.7	23021.9	23644.1	24266.
4000	24888.6	25510.8	26133.0	26755.2	27377.4	27999.6	28621.8	29244.1	29866.3	30488.
Klafter.					Un	its.	A			inut.
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. fee
0	0.00	6.22	12.44	18.67	24.89	31.11	37.33	43.55	49.78	56.00
10	62.22	68.44	74.67	80.89	87.11	93.33	99.55	105.78	112.00	118.2
20	124.44	130.66	136.89	143.11	149.33	155.55	161.78	168.00	174.22	180.4
30	186.66	192.89	199.11	205.33	211.55	217.77	224.00	230.22	236.44	242.6
40	248.89	255.11	261.33	267.55	273.77	280.00	286.22	292.44	298.66	304.8
50	311.11	317.33	323.55	329.77	336.00	342.22	348.44	354.66	360.88	367.1
60	373.33	379.55	385.77	391.99	398.22	404.44	410.66	416.88	423.11	429.3
70	435.55	441.77	447.99	454.22	460.44	466.66	472.88	479.10	485.33	491.5
10	497.77	503.99	510.22	516.44	522.66	528.88	535.10	541.33	547.55	553.7
80	431.11									

#### XXVIII. CONVERSION OF FEET OF VIENNA INTO METRES.

1 Foot of Vienna = 0.3160790 Metre.

Feet of Vienna.					Huno	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
en 1 44	Metres.	Metres.	Metres.	Metres.						
0	0.00	31.61	63.22	94.82	126.43	158.04	189.65	221.26	252.86	284.4
1000	316.08	347.69	379.29	410.90	442.51	474.12	505.73	537.33	568.94	600.5
2000	632.16	663.77	695.37	726.98	758.59	790.20	821.81	853.41	885.02	916.6
3000	948.24	979.84	1011.45	1043.06	1074.67	1106.28	1137.88	1169.49	1201.10	1232.7
4000	1264.32	1295.92	1327.53	1359.14	1390.75	1422.36	1453.96	1485.57	1517.18	1548.7
5000	1580.40	1612.00	1643.61	1675.22	1706.83	1738.43	1770.04	1801.65	1833.26	1864.8
6000	1896.47	1928.08	1959.69	1991.30	2022.91	2054.51	2086.12	2117.73	2149.34	2180.9
7000						2370.59		the second second		
8000						2686.67		The second of the second		
9000	11					3002.75	12774118.00			
10000	3160.79	3192.40	3224.01	3255.61	3287.02	3318.83	3350.44	3382.05	3413.65	3445.2
11000						3634.91				
12000						3950.99				
13000						4267.07				
14000						4583.15				
15000									4994.05	

1 Foot of Vienna = 0.9730317 Paris Foot.

Feet of					Hund	reds.				
Vienna. Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par. feet.	Par. fee								
0	0.0	97.30	19.46	29.19	38.92	48.65	58.38	68.11	77.84	87.5
1000	973.0	1070.3	1167.6	1264.9	1362.2	1459.5	1556.9	1654.2	1251.5	1848.
2000	1946.1	2043.4	2140.7	3238.0	2335.3	2432.6	2530.0	2627.2	2724 5	2821.
3000	2919.1	3016.4	3113.7	3211.0	3308.3	3405.6	3502.9	3600.2	3697.5	3794.
4000	3892.1	3989.4	4086.7	4184.0	4281.3	4378.6	4475.9	4573.2	4670.6	4767.
5000	4865.2	4962.5	5059.8	5157.1	5254.4	5351.7	5449.0	5546.3	5643.6	5740.
6000	5838.2	5935.5	6032.8	6130.1	6227.4	6324.7	6422.0	6519.3	6616.6	6713
7000	6811.2	6908.5	7005.8	7103.1	7200.4	7297.7	7395.0	7492.3	7589.6	7687
8000	7784.3	7881.6	7978.9	8076.2	8173.5	8270.8	8368.1	8465.4	8562.7	8660
9000	8757.3	8854.6	8951.9	9049.2	9146.5	9243.8	9341.1	9438.4	9535.7	9633
10000	9730.3	9827.6	9924.9	10022.2	10119.5	10216.8	10314.1	10411.4	10508.7	10606
11000	10703.3	10800.7	10898.0	10995.3	11092.6	11189.9	11287.2	11384.5	11481.8	11579
12000	11676.4	11773.7	11871.0	11968.3	12065.6	12162.9	12260.2	12357.5	12454.8	12552
13000	12649.4	12746.7	12844.0	12941.3	13038.6	13135.9	13233.2	13330.5	13427.8	13525
14000	13622.4	13719.7	13817.1	13914.3	14011.7	14109.0	14206.3	14303.6	14400.9	14498
15000	14595.5	14692.8	14790.1	14887.4	14984.7	15082.0	15179.3	15276.6	15373.9	15471
16000	15568.5	15665.8	15763.1	15860.4	15957.7	16055.0	16152.3	16249.6	16346.9	16444

#### XXX. CONVERSION OF FEET OF VIENNA INTO ENGLISH FEET AND DECIMALS.

1 Foot of Vienna = 1.0370234 English Foot.

Feet of Vienna.				20040	Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. fee					
0	0.0	103.7	207.4	311.1	414.8	518.5	622.2	725.9	829.6	933.
1000	1037.0	1140.7	1244.4	1348.1	1451.8	1555.5	1659.2	1762.9	1866.6	1970.
2000	2074.0	2177.7	2281.5	2385.2	2488.9	2592.6	2696.3	2800.0	2903.7	3007.
3000	3111.1	3214.8	3318.5	3422.2	3525.9	3629.6	3733.3	3837.0	3940.7	4044.
4000	4148.1	4251.8	4355.5	4459.2	4562.9	4666.6	4770.3	4874.0	4977.7	5081.
5000	5185.1	5288.8	5292.5	5496.2	5599.9	5703.6	5807.3	5911.0	6014.7	6118.
6000	6222.1	6325.8	6429.5	6533.2	6636.9	6740.7	6844.4	6948.1	7051.8	7155.
7000	7259.2	7362.9	7466.6	7570.3	7674.0	7777.7	7881.4	7985.1	8088.8	8192.
8000	8296.2	8399.9	8503.6	8607.3	8711.0	8814.7	8918.4	9022.1	9125.8	9229.
9000	9333.2	9436.9	9540.6	9644.3	9748.0	9851.7	9955.4	10059.1	10162.8	10266.
10000	10370.2	10473.9	10577.6	10681.3	10785.0	10888.7	10992.4	11096.2	11199.9	11303.
11000	11407.3	11511.0	11614.7	11718.4	11822.1	11925.8	12029.5	12133.2	12236.9	12340.
12000					12859.1				13273.9	
13000	13481.3	13585.0	13688.7	13792.4	13896.1	ACCOUNT OF THE PARTY OF THE PAR	Charles Tolking		14310.9	
14000	14518.3	14622.0	14725.7	14829.4	14933.1				15347.9	
15000	15555.4	15659.1	15762.8	15866.5	15970.2	16073.9				
16000	16592.4									

## RHINE OR PRUSSIAN FEET

#### INTO DIFFERENT MEASURES OF LENGTH.

The Rhine Foot is used in Physical Geography, though not so extensively as the French or Paris Foot, in the northwestern part of Germany, Denmark, and Holland. Its legal value in the Prussian system of weights and measures is 139.13 French or Paris Lines, from which are derived the equations used in computing the following tables.

#### XXXI. CONVERSION OF RHINE OR PRUSSIAN FEET INTO FRENCH TOISES.

1 Rhine Foot = 0.1610301 Toise.

thine Feet.					Hune	dreds.		her beg		
housands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.
0	0.00	16.10	32.21	48.31	64.41	80.52	96.62	112.72	128.82	144.9
1000	161.03	177.13	193.24	209.34	225.44	241.55	257.65	273.75	289.85	305.9
2000	322.06	338.16	354.27	370.37	386.47	402.58	418.68	434.78	450.88	466.9
3000	483.09	499.19	515.30	531.40	547.50	563.61	579.71	595.81	611.91	628.0
4000	634.12	650.22	666.33	692.43		724.64		756.84	772:94	789.0
5000	805.15	821.25	837.36	853.46	869.56	885.67	901.77	917.87	933.97	950.0
6000	966.18	982.28			ALCOHOLD BY	1046.70			13217	
7000	1127.21	1				1207.73		and the same of	The second second	111111111111111111111111111111111111111
8000						1368.76				
9000						1529.79				

1 Rhine Foot = 0.31385350 Metre.

Rhine Feet.				R	hine Feet	Hundred	3.			
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
1000000	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	31.39	62.77	94.16	125.54	156.93	188.31	219.70	251.08	282.47
1000	313.85	345.24	376.62	408.01	439.39	470.78	502.17	533.55	564.94	596.32
2000	627.71	659.09	690.48	721.86	753.25	784.63	816.02	847.40	878.79	910.18
3000	941:56	972.95	1004.33	1035.72	1067.10	1098.49	1129.87	1161.26	1192.64	1224.03
4000	1255.41	1286.80	1318.18	1349.57	1380.96	1412.34	1443.73	1475.11	1506.50	1537.88
5000	1569.27	1600.65	1632.04	1663.42	1694.81	1726.19	1757.58	1788.97	1820.35	1851.74
6000	1883.12	1914.51	1945.89	1977.28	2008.66	2040.05	2071.43	2102.82	2134.20	2165.59
7000	2196.97	2228.36	2259.75	2291.13	2322.52	2353.90	2385.29	2416.67	2448.06	2479.44
8000	2510.83	2542.21	2573.60	2604.98	2636.37	2667.76	2699.14	2730.53	2761.91	2793.30
9000	2824.68	2856.07	2887.45	2918.84	2950.22	2981.61	3012.99	3044.38	3075.76	3107.15

#### XXXIII. OF RHINE OR PRUSSIAN FEET INTO FRENCH FEET AND DECIMALS. 1 Rhine Foot = 0.96618056 French Foot.

Rhine Feet.				R	hine Feet.	Hundred	s.			
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
10,8371	Fr. Feet.	Fr Feet.	Fr. Feet	Fr.Feet.	Fr. Feet	Fr Feet.	Fr.Feet.	Fr.Feet.	Fr Feet.	Fr. Feet.
0	0.00	96.62	193.24	289.85	386.47	483.09	579.71	676.33	772.94	869.56
1000	966.18	1062.80	1159.42	1256.03	1352.65	1449.27	1545.89	1642.51	1739.13	1835.74
2000	1932.36	2028.98	2125.60	2222.22	2318.83	2415.45	2512.07	2608.69	2705.31	2801.92
3000	2898.54	2995.16	3091.78	3188.40	3285.01	3381.63	3478.25	3574.87	3671.49	3768.10
4000	3864.72	3961.34	4057.96	4154.58	4251.19	4347.81	4444.43	4541.05	4637.67	4734.28
5000	4830.90	4927.52	5024.14	5120.76	5217.38	5313.99	5410.61	5507.23	5603.85	5700.47
6000	5797.08	5893.70	5990.32	6086.94	6183.56	6280.17	6376.79	6473.41	6570.03	6666.65
7000	6763.26	6859.88	6956.50	7053.12	7149.74	7246.35	7342.97	7439.59	7536.21	7632.83
8000	7729.44	7826.06	7922.68	8019.30	8115.92	8212.53	8309.15	8405.77	8502.39	8599.01
9000		8792.24		10 55 Tu 3 50	W. Carrier H.		The second second		STATE OF THE PARTY	

#### XXXIV. OF RHINE OR PRUSSIAN FEET INTO ENGLISH FEET AND DECIMALS. 1 Rhine Foot = 10297217 English Foot.

Rhine Feet.	100	Rhine Feet. Hundreds.												
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.				
old seed to	Eng. feet.	Eng. feet.	Eng. feet.		Eng. feet.		Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.				
0	0.00	102.97	205.94	308.92	411.89	514.86	617.83	720.81	823.78	926.75				
1000	1029.72	1132.69	1235.67	1338.64	1441.61	1544.58	1647.55	1750.53	1853.50	1956.47				
2000	2059.44	2162.42	2265.39	2368.36	2471.33	2574.30	2677.28	2780.25	2883.22	2986.19				
3000	3089.17	3192.14	3295.11	3398.08	3501.05	3604.03	3707.00	3809.97	3912.94	4015.92				
4000	4118.89	4221.86	4324.83	4427.80	4530.78	4633.75	4736.72	4839.69	4942.66	5045.64				
5000	5148.61	5251.58	5354.55	5457.53	5560.50	5663.47	5766.44	5869.41	5972.39	6075.36				
6000	6178.33	6281.30	6384.28	6487.25	6590.22	6693.19	6796.16	6899.14	7002.11	7105.08				
7000	7208.05	7311.02	7414.00	7516.97	7619.94	7722.91	7825.89	7928.86	8031.83	8134.80				
8000	8237.77	8340.75	8443.72	8546.69	8649.66	8752.64	8855.61	8958.58	9061.55	9164.52				
9000	9267.50	9370.47	9473.44	9576.41	9679.38	9782.36	9885.33	9988.30	10091.3	10194.2				

## SPANISH OR MEXICAN VARAS AND FEET

INTO DIFFERENT MEASURES OF LENGTH.

XXXV. CONVERSION OF SPANISH OR MEXICAN VARAS INTO METRES.

1 Vara = 0.847965 Metre.

Varas.	his his	Hundreds.												
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.				
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.				
0	0.00	84.80	169.59	254.39	339.19	423.98	508.78	593.58	678.37	763.17				
1000	847.96	932.76	1017.56	1102.35	1187.15	1271.95	1356.74	1441.54	1526.34	1611.13				
2000	1695.93	1780.73	1865.52	1950.32	2035.12	2119.91	2204.71	2289.51	2374.30	2459.10				
3000	2543.89	2628.69	2713.49	2798.28	2883.08	2967.88	3052.67	3137.47	3222.27	3307.06				
4000	3391.86	3476.66	3561.45	3646.25	3731.05	3815.84	3900.64	3985.44	4070.23	4155.03				
5000	4239.82	4324.62	4409.42	4494.21	4579.01	4663.81	4748.60	4833.40	4918.20	5002.99				
6000	5087.79	5172.59	5257.38	5342.18	5426.98	5511.77	5596.57	5681.37	5766.16	5850.96				
7000					6274.94					10000000				
8000		+ + 250 1 200 4	177		7122.91	L. A. C.	1200 1000							
9000					7970.87					100000000000000000000000000000000000000				

XXXVI. OF SPANISH OR MEXICAN VARAS INTO ENGLISH FEET AND DECIMALS.

1 Vara = 2.78209 English Feet.

Varas.	Hundreds,												
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.			
-	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet			
0	0.0	278.2	556.4	834.6	1112.8	1391.0	1669.3	1947.5	2225.7	2503.9			
1000	2782.1	3060.3	3338.5	3616.7	3894.9	4173.1	4451.3	4729.6	5007.8	5286.0			
2000	5564.2	5842.4	6120.6	6398.8	6677.0	6955.2	7233.4	7511.6	7789.9	8068.1			
3000	8346.3	8624.5	8902.7	9180.9	9459.1	9737.3	10015.5	10293.7	10571.9	10850.2			
4000	11128.4	11406.6	11684.8	11963.0	12241.2	12519.4	12797.6	13075.8	13354.0	13632.2			
5000	13910.4	14188.7	14466.9	14745.1	15023.3	15301.5	15579.7	15857.9	16136.1	16414.8			
6000	16692.5	16970.7	17249.0	17527.2	17805.4	18083.6	18361.8	18640.0	18918.2	19196.4			
7000		STATE OF THE PARTY	IN THE PARTY NAMED IN		THE RESERVE OF THE PARTY OF THE	20865:7	A STATE OF THE PARTY OF THE PAR			000			
8000		CONTRACT CONTRACT	100 mm 2 mm	100 DE 10	E VEST TENDER	23647.8	THE RESERVE OF THE PARTY OF		THE RESERVE TO SERVE THE PERSON NAMED IN COLUMN TWO IN COL	The state of the state of			
9000	25038.8	The state of the s	1.75	1000 0000 0000 0000	0.00	THE REAL PROPERTY.	THE RESERVE OF THE PARTY OF THE		A STATE OF THE PARTY OF THE PAR	TO TOWN			

#### XXXVII. CONVERSION OF CASTILIAN FEET INTO METRES.

1 Castilian Foot = 0.282655 Metre.

Castilian Feet.	dig or	entoris.	illoud!		Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
Kan (1999)	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	28.27	56.53	84.80	113.06	141.33	169.59	197.86	226.12	254.39
1000	282.65	310.92	339.19	367.45	395.72	423.98	452.25	480.51	508.78	537.04
2000	565.31	593.58	621.84	650.11	678.37	706.64	734.90	763.17	791.43	819.70
3000	847.96	876.23	904.50	932.76	961.03	989.29	1017.56	1045.82	1074.09	1102.35
4000	1130.62	1158.89	1187.15	1215.42	1243.68	1271.95	1300.21	1328.48	1356.74	1385.01
5000	1413 27	1.141 54	1469 81	1498 07	1596 34	1554.60	1589 87	1611 12	1639 40	1667 66
6000	of the land		P. Sharman	Court of the Court of	AND DESCRIPTION OF THE PARTY OF	1837.26	Townson and the		100	100000000000000000000000000000000000000
7000				THE PARTY NAMED IN		2119.91	7.36			
				7.77						
8000				the carried		2402.57				
9000	2543.89	2572.16	2600.43	2628.69	2656.96	2685.22	2713.49	2741.75	2770.02	2798.28

#### XXXVIII. CONVERSION OF CASTILIAN FEET INTO PARIS OR FRENCH FEET. 1 Castilian Foot = 0 870138 Paris Foot.

Castilian Feet.		8.8% 6.2% 6.2%	aritmen	(BALLE)	Hune	lreds.	(CRITE)	- Jugari		H VIII LA
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par. Feet.	Par. Feet.	Par. Feet.	Par Feet.	Par Feet.	Par. Feet.	Par. Feet.	Par Feet.	Par.Feet.	Par. Feet.
0	0.00	87.01	174.03	261.04	348.06	435.07	522.08	609.10	696.11	783.12
1000	870.14	957.15	1044.17	1131.18	1218.19	1305.21	1392.22	1479.23	1566.25	1653.26
2000	1740.28	1827.29	1914.30	2001.32	2088.33	2175.35	2262.36	2349.37	2436.39	2523.40
3000	2610.41	2697.43	2784.44	2871.46	2958.47	3045.48	3132.50	3219.51	3306.52	3393.54
4000	3480.55	3567.57	3654.58	3741.59	3828.61	3915.62	4002.64	4089.65	4176.66	4263.68
5000	4350.69	4437.70	4524.72	4611.73	4698.75	4785.76	4872.77	4959.79	5046.80	5133.82
6000	111111111111111111111111111111111111111	1000	5394.86		P. D. STATE OF CO.	0 -0.700	SER STORY	100000000000000000000000000000000000000		6003.95
7000			6265.00							6874.09
8000	Talle a paragraph	10 may 10 mm	7135.13	C 10.00	10 FOR 9, 917)		100000000000000000000000000000000000000	10 February 1980 Vice		7744.23
9000		SHEET THE	1.5 6 7 1/4 30	A SHEET AND	THE RESERVE OF THE PERSON NAMED IN	8266.31				

#### XXXIX. CONVERSION OF CASTILIAN FEET INTO AMERICAN FEET.

1 Castilian Foot = 0.927309 American Foot.

Castilian Feet.	Hundreds.												
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.			
Parcett State	Am. Feet.	Am Feet.	Am. Feet.	Am. Feet.	Am. Feet.	Am. Feet.	Am.Feet.	Am. Feet.	Am. Feet	Am. Feet.			
0	0.00	92.73	185.46	278.19	370.92	463.65	556.39	649.12	741.85	834.58			
1000	927.31	1020.04	1112.77	1205.50	1298.23	1390.96	1483.69	1576.43	1669.16	1761.89			
2000	1854.62	1947.35	2040.08	2132.81	2225.54	2318.27	2411.00	2503.74	2596.47	2689.20			
3000	2781.93	2874.66	2967.39	3060.12	3152.85	3245.58	3338.31	3431.04	3523.78	3616.51			
4000	3709.24	3801.97	3894.70	3987.43	4080.16	4172.89	4265.62	4358.35	4451.08	4543.82			
5000	4636.55	4729.28	4822.01	4914.74	5007.47	5100.20	5192.93	5285.66	5378.39	5471.12			
6000	5563.86	5656.59	5749.32	5842.05	5934.78	6027.51	6120.24	6212.97	6305.70	6398.43			
7000	6491.17	6583.90	6676.63	6769.36	6862.09	6954.82	7047.55	7140.28	7233.01	7325.74			
8000	7418.47	7511.21	7603.94	7696.67	7789.40	7882.13	7974.86	8067.59	8160.32	8253.05			
9000	8345.78	8438.51	8531.25	8623.98	8716.71	8809.44	8902.17	8994.90	9087.63	9180.36			

The length of the Spanish Vara, and of the Spanish or Castilian foot, used in the late Spanish Colonies of Mexico and South America, owing, no doubt, to the imperfection of the local standards, shows considerable variations from the value on which the preceding tables are based.

A careful comparison of the standard Vara, brought from Mexico by Major Turnbull, and deposited in the United States Office of Weights and Measures, (see above p. 113,) gave for its length 32.9682 American inches = 2.7473333 American feet = 2.7474928 English feet = 0.8374206 metre.

From a series of altitudes published in Mexico, by Cortina, in Castilian feet, and by Orbegozo in metres and Castilian feet, Jul. Schmidt derives the following value of the Vara and of the Castilian foot, used by these authors (see Petermann's *Mittheil*. 1857, p. 371): One Vara = 2.573296 Paris feet = 0.8358065 metre; and one Castilian foot = 0.857764 Paris foot = 0.91417 English foot.

According to Colonel J. Ondarza, one of the authors of the new official Map of Bolivia, the Bolivian government has declared the legal value of the Spanish Vara to be in the ratio of 100 metres = 118 Varas = 354 Spanish feet, which value has been adopted by him in publishing his measured altitudes.

XXXVIII' MEXICO. — CONVERSION OF CASTILIAN FEET INTO METRES, PARIS AND ENGLISH FEET.

Mexican or	Accordin	ng to Turnbull's	Standara.	According	g to Schmidt, fro	m Cortina.
Castilian Feet.	Metres.	Paris Feet.	English Feet.	Metres.	Paris Feet.	English Feet
1000	279.14	859.30	915.83	278.64	857.76	914.17
2000	558.28	1718.60	1831.66	557.27	1715.53	1828.34
3000	837.42	2577.89	2747.49	835.91	2573.29	2742.51
4000	1116.56	3437.19	3663.32	1114.54	3431.06	3656.68
5000	1395.70	4296.49	4579.15	1393.18	4288.82	4570.85
6000	1674.84	5155.79	5494.99	1671.81	5146.58	5485.02
7000	1953.98	6015.08	6410.82	1950.45	6004.35	6399.19
8000	2233.12	6874.38	7326.65	2229.08	6862.11	7313.36
9000	2512.26	7733.68	8242.48	2507.72	7719.88	8227.53

XXXIX'. BOLIVIA. — CONVERSION OF SPANISH VARA AND SPANISH FEET.

1 Spanish foot = 0 2824859 metre = 0.8696171 Paris foot, = 0.9268078 English foot.

Bolivian or Spanish Feet.	Metres.	Paris Feet.	English Feet.	Metres.	Spanish Varas.	Spanish Feet.
1000	282.49	869.62	926.81	1000	1180	3540
2000	564.97	1739.23	1853.61	2000	2360	7080
3000	847.46	2608.85	2780.42	3000	3540	10620
4000	1129.94	3478.47	3707.23	4000	4720	14160
5000	1412.43	4348.09	4634.04	5000	5900	17700
6000	1694.92	5217.70	5560.85	6000	7080	21240
7000	1977.40	6087.32	6487.65	7000	8260	24780
8000	2259.89	6956.94	7414.46	8000	9440	28320
9000	2542.37	7826.55	8341.27	9000	10620	31860

## FRACTIONAL PARTS OF A TOISE AND OF A FOOT

INTO EACH OTHER.

XL. CONVERSION OF INCHES INTO DUODECIMAL LINES.

1 Inch = 12 Lines.

iches.		Inches. Units.														
ens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.						
	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.						
0	0	12	24	36	48	60	72	84	96	108						
10	120	132	144	156	168	180	192	204	216	228						
20	240	252	264	276	288	300	312	324	336	348						
30	360	372	384	396	408	420	432	444	456	468						
40	480	492	504	516	528	540	552	564	576	588						
50	600	612	624	636	648	660	672	684	696	708						
60 .	720	732	744	756	768	780	792	804	816	828						
70	840	852	864	876	888	900	912	924	936	948						
80	960	972	984	996	1008	1020	1032	1044	1056	1068						
90	1080	1092	1104	1116	1128	1140	1152	1164	1176	1188						
100	1200	1212	1224	1236	1248	1260	1272	1284	1296	1308						

XLI. CONVERSION OF DECIMALS OF A TOISE INTO FEET AND INCHES.

1 Toise = 6 Feet = 72 Inches = 864 Lines.

		81-37 E C			Hundredtha	of a Toise			107A	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
							ft. in. lin. f			
۱	0.0.0,00	0. 0. 8,64	0. 1. 5,28	0. 2. 1,92	0. 2.10,56	0. 3.7,20	0. 4. 3,84	0.5. 0,48 0.	5. 9,12	0. 6. 5,76
	0.7.2,40	0. 7.11,04	0. 8. 7,68	0. 9. 4,32	0.10. 0,96	0.10.9,60	0.11. 6,24	1.0. 2,88 1.	0.11,52	1. 1. 8,16
	1.2.4,80	1. 3. 1,44	1. 3.10,08	1. 4. 6,72	1. 5. 3,36	1. 6.0,00	1. 6. 8,64	1.7. 5,28 1.	8. 1,92	1. 8.10,56
	1.9.7,20	1.10. 3,84	1.11. 0,48	1.11. 9,12	2. 0. 5,76	2. 1.2,40	2. 1.11,04	2.2. 7,68 2.	3. 4,32	2. 4. 0,96
	2.4.9,60	2. 5. 6,24	2. 6. 2,88	2. 6.11,52	2. 7. 8,16	2. 8.4,80	2. 9. 1,44	2.9.10,08 2.	10. 6,72	2.11. 3,36
ı	3.0.0,00	3. 0. 8,64	3. 1. 5,28	3. 2. 1,92	3. 2.10,56	3. 3.7,20	3. 4. 3,84	3.5. 0,48 3.	5. 9.12	3. 6. 5.76
							3.11. 6,24			
							4. 6. 8,64			
							5. 1.11,04			
							5. 9. 1,44			

Week	1			1	Hundredth	s of a Foot				
Feet. Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
0.0	0.00	0.12	0.24	0.36	0.48	0.60	0.72	0.84	0.96	1.08
0.1	1.20	1.32	1.44	1.56	1.68	1.80	1.92	2.04	2.16	2.28
0.2	2.40	2.52	2.64	2.76	2.88	3.00	3.12	3.24	3.36	3.48
0.3	3.60	3.72	3.84	3.96	4.08	4.20	4.32	4.44	4.56	4.68
0.4	4.80	4.92	5.04	5.16	5.28	5.40	5.52	5.64	5.76	5.88
0.5	6.00	6.12	6.24	6.36	6.48	6.60	6.72	6.84	6.96	7.08
0.6	7.20	7.32	7.44	7.56	7.68	7.80	7.92	8.04	8.16	8.28
0.7	8.40	8.52	8.64	8.76	8.88	9.00	9.12	9.24	9.36	9.48
0.8	9.60	9.72	9.84	9.96	10.08	10.20	10.32	10.44	10.56	10.68
0.9	10.80	10.92	11.04	11.16	11.28	11.40	11.52	11.64	11.76	11.88

XLIII. CONVERSION OF DECIMALS OF A FOOT INTO INCHES AND DUODECIMAL LINES.

	There	Hundredths of a Foot.											
Feet. Tens.		0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
		In. Line.	In. Line.	In. Line.	In. Line.	In. Line.	In. Line.	In. Line	In. Line.	In. Line	In. Line.		
	0.0	0.0,00	0. 1,44	0. 2,88	0. 4,32	0. 5,76	0.7,20	0. 8,64	0.10,08	0.11,52	1. 0,96		
	0.1	1.2,40	1. 3,84	1. 5,28	1. 6,72	1. 8,16	1.9,60	1.11,04	2. 0,48	2. 1,92	2. 3,36		
	0.2	2.4,80	2. 6,24	2. 7,68	2. 9,12	2.10,56	3.0,00	3. 1,44	3. 2,88	3. 4,32	3. 5,76		
	0.3	3.7,20	3. 8,64	3.10,08	3.11,52	4. 0,96	4.2,40	4. 3,84	4. 5,28	4. 6,72	4. 8,16		
	0.4	4.9,60	4.11,04	5. 0,48	5. 1,92	5. 3,36	5.4,80	5. 6,24	5. 7,68	5. 9,12	5.10,56		
1	0.5	6.0,00	6. 1,44	6. 2,88	6. 4,32	6. 5,76	6.7,20	6. 8,64	6.10,08	6.11,52	7. 0,96		
	0.6	7.2,40	7. 3,84	7. 5,28	7. 6,72	7. 8,16	7.9,60	7.11,04	8. 0,48	8. 1,92	8. 3,36		
	0.7	8.4,80	8. 6,24	8. 7,68	8. 9,12	8.10,56	9.0,00	9. 1,44	9. 2,88	9. 4,32	9. 5,76		
	0.8	9.7,20	9. 8,64	9.10,08	9.11,52	10. 0,96	10.2,40	10. 3,84	10. 5,28	10. 6,72	10. 8,16		
	0.9	10.9,60	10.11,04	11. 0,48	and the second	,					11.10,56		

XLIV. CONVERSION OF INCHES AND DUODECIMAL LINES INTO DECIMALS OF A FOOT.  $1 \ \text{Inch} = 0.08333 \ \text{of a Foot.} \qquad 1 \ \text{Line} = 0.006944 \ \text{of a Foot.}$ 

	Lines.											
Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.
	Foot.											
0	0.0000	0.0069	0.0139	0.0208	0.0278	0.0347	0.0417	0.0486	0.0556	0.0625	0.0694	0.0764
1	0.0833	0.0903	0.0972	0.1042	0.1111	0.1181	0.1250	0.1319	0.1389	0.1458	0.1528	0.1597
2	0.1667	0.1736	0.1806	0.1875	0.1944	0.2014	0.2083	0.2153	0.2222	0.2292	0.2361	0.2431
3							0.2917					
4							0.3750					
5							0.4583					
6	0.5000	0.5069	0.5139	0.5208	0.5278	0.5347	0.5417	0.5486	0.5556	0.5625	0.5694	0.5764
7	0.5833	0.5903	0.5972	0.6042	0.6111	0.6181	0.6250	0.6319	0.6389	0.6458	0.6528	0.6597
8	0.6667	0.6736	0.6806	0.6875	0.6944	0.7014	0.7083	0.7153	0.7222	0.7292	0.7361	0.7431
9	0.7500	0.7569	0.7639	0.7708	0.7778	0.7847	0.7917	0.7986	0.8056	0.8125	0.8194	0.8264
10	0.8333	0.8403	0.8472	0.8542	0.8611	0.8681	0.8750	0.8819	0.8889	0.8958	0.9028	0.9097
11	0.9167	0.9236	0.9306	0.9375	0.9444	0.9514	0.9583	0.9653	0.9722	0.9792	0.9861	0.9931

## METEOROLOGICAL TABLES.

V.

## METEOROLOGICAL CORRECTIONS,

OR

## TABLES

FOR CORRECTING SERIES OF OBSERVATIONS FOR THE PERIODIC AND NON-PERIODIC VARIATIONS.

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# THE ENDERGY OF THE PARTY.

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[The figures refer to the folio at the bottom of the page.—The letters near them mean, D. = calculated by Dove;

Gl. = Glaisher; G. = Guyot; L. = Lefroy. For the letters before the latitudes, see page 12.]

## Temperature.

### Hourly Corrections for Periodic Variations.

### NORTH AMERICA.

	Station.			Latitude.	Scale.		Page.
LE I.	Washington, District Columbia,	B 1.	38	54 N.	Reau.	D.	15
II.	Philadelphia, Girard College,	A'3.	39	58 N.	Reau.	D.	15
III.	Philadelphia, Girard College,	A'3.	39	58 N.	Fahr.	G.	16
IV.	Frankfort Arsenal, Penn.,	C.	39	57 N.	Reau.	D.	17
V.	Frankfort Arsenal, Penn.,	C.	39	57 N.	Fahr.	D.	18:
VI.	Toronto, Canada West,	B.	43	40 N.	Fahr.	D.	19
VII.	Toronto, Canada West,	В.	43	40 N.	Reau.	D.	20
VIII.	Toronto, Canada West,	A'6.	43	40 N.	Fahr.	L.	21
IX.	Toronto, Canada West,	'A'6.	43	40 N.	Reau.	D.	22
X.	Montreal, Canada East,	A'1.	45	30 N.	Fahr.	G.	22
XI.	Sitka, Russian America,	'A'5.	57	3 N.	Reau.	D.	23
XII.	Boothia Felix, Arctic America,	Α.	69	59 N.	Reau.	D.	24
XIII.	Lake Athabasca, Arctic America,	C.	59	N.	Fahr.	L.	25
XIV.	Melville Island, Arctic America,	C.	74	47 N.	Reau.	D.	25
XV.	Hecla Cove, Spitzbergen,	C.	79	55 N.	Reau.	D.	25
A AGO	Appendix.	No PETER			AND ADDRESS		
V'.	Amherst College, Mass.,	A'1.	42	22 N.	Fahr.	D.	28
GP	AND THE TANK THE						
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SOUTH AMERICA.

3

C.

C.

22 54 S.

22 54 S.

Fahr.

Reau.

D. 26

D.

27

Rio Janeiro, Brazil,

Rio Janeiro, Brazil,

" XVII.

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46	XX. XXI.		A.	13 4 N.	Reau.	D.	34
"	XXII.	Madras, India,	A.	18 56 N.	Fahr.	D.	35
"	XXIII.	Bombay, India, Bombay, India,	A.	18 56 N.	Reau.	D.	36
66	XXIV.	Madras, India,	A'5.	13 4 N.	Reau.	D.	37
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66	XXVI.	Calcutta, India,	A'2.	22 33 N.	Reau.	D.	38
66	XXVII.	Tiflis, Georgia,	A'4.	41 41 N.	Reau.	D.	39
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66	XXX.	Nertchinsk, Siberia,	A.	51 18 N.	Reau.	D.	
66	XXXI.	Barnaul, Siberia,	A.	53 20 N.			41
66	XXXII.	Barnaul, Siberia,	A.	53 20 N. 53 20 N.	Fahr. Reau.	D. D.	42 43
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	AAAIII.	Damaui, Siberia,	Λ.0.	33 20 IV.	neau.	D.	44
		EUROPE.					
	a const		and the	te il meleti	Qui N	F au	
66	XXXIV.	Rome, Italy,	C.	41 54 N.	Reau.	D.	47
"	XXXV.	Padua, Italy,	C.	45 24 N.	Reau.	D.	48
66	XXXVI.	Geneva, Switzerland,		46 12 N.	Reau.	D.	49
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	XXXVIII.	St. Bernard, Switzerland,		45 52 N.	Reau.	D.	50
66	XXXIX.	St. Bernard, Switzerland,	C'4.	45 52 N.	Reau.	D.	50
66	XL.	Kremsmünster, Austria,	C.	48 3 N.	Reau.	D.	51
44	XLI.	Salzburg, Austria,	A'6.	47 48 N.	Reau.	D.	52
"	XLII.	Munich, Bavaria,	A'6.	48 9 N.	Reau.	D.	52
66	XLIII.	Prague, Bohemia,	A'10.	50 5 N.	Reau.	D.	53
66	XLIV.	Prague, Bohemia,	A.	50 5 N.	Reau.	D.	54
66	XLV.	Plymouth, England,	C.	50 22 N.	Fahr.	D.	55
66	XLVI.	Plymouth, England,	C.	50 22 N.	Reau.	D.	56
46	XLVII.	Brussels, Belgium,	В.	50 51 N.	Reau.	D.	57
66	XLVIII.	Brussels, Belgium,	B'.	50 51 N.	Reau.	D.	58
46	XLIX.	Schwerin, Germany,	B'3.	53 36 N.	Reau.	D.	58
46	L.	Mühlhausen, Prussia,	C.	51 13 N.	Reau.	D.	59
"	LI.	Utrecht, Holland,	A'2.	52 5 N.	Reau.	D.	60
"	LII.	Greenwich, England,	B'7.	51 29 N.	Reau.	D.	60
"	LIII.	Greenwich, England,	В.	51 29 N.	Reau.	D.	61
"	LIV.	Greenwich, England,	В.	51 29 N.	Fahr.	Gl.	62
"	LV.	Halle, Prussia,	C.	51 30 N.	Reau.	D.	63
E	LVI.	Göttingen, Hanover,	C.	51 32 N.	Reau.	D.	64
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		Station.		Latitude.	Scale.		Page.
TABL	E LVII.	Berlin, Prussia,	A.	52 30 N.	Reau.	D.	65
"	LVIII.	Salzuflen, Germany,	A.	52 5 N.	Reau.	D.	66
"	LIX.	Stettin, Germany,	A'.	53 25 N.	Reau.	D.	67
"	LX.	Apenrade, Sleswick,	C.	55 3 N.	Reau.	D.	68
2 66	LXI.	Leith, Scotland,	A.	55 59 N.	Fahr.	D.	69
66	LXII.	Leith, Scotland,	A.	55 59 N.	Reau.	D.	70
"	LXIII.	Makerstoun, Scotland,	A'3.	55 36 N.	Reau.	D.	71
66	LXIV.	Dublin, Ireland,	B'4.	53 23 N.	Reau.	D.	71
66	LXV.	Catharinenburg, Russia,	A.	56 50 N.	Reau.	D.	72
66	LXVI.	Catharinenburg, Russia,	A'6.	56 50 N.	Reau.	D.	73
66	LXVII.	St. Petersburg, Russia,	A'10.	59 56 N.	Reau.	D.	73
66	LXVIII.	Helsingfors, Finland,	A'3.	60 10 N.	Reau.	D.	74
**	LXIX.	St. Petersburg, Russia,	A.	59 56 N.	Reau.	Ď.	75
66	LXX.	Helsingfors, Finland,	C.	60 10 N.	Reau.	D.	76
"	LXXI.	Christiania, Norway,	C.	59 55 N.	Reau.	D.	77
"	LXXII.	Drontheim, Norway,	C.	63 26 N.	Reau.	D.	78
66	LXXIII.	Strait of Kara, Russia,	A	70 37 N.	Reau.	D.	79
"	LXXIV.	Matoschkin Schar, Novaia Zemlia,	A.	73 N.	Reau.	D.	80
66	LXXV.	Bossekop, Norway,	C.	69 58 N.	Reau.	D.	81
66	LXXV'.	Bossekop, Norway,	C.	69 58 N.	Centig	. G.	81
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		AFRICA AND AUSTRAI	LIA.				
"	LXXVI.	St. Helena, Africa,	A'5.	15 55 S.	Reau.	D.	85
66	LXXVII.	Cape of Good Hope, Africa,	A'5.	33 56 S.	Reau.	D.	85
"	LXXVIII.	Hobarton, Tasmania,	A'8.	42 53 S.	Reau.	D.	86
		Monthly Corrections for Non-period	odic Vo	riations.			
		Station.		Latitude.	Scale.		Page.
TABL	E LXXIX.	Madras, India,		13 4 N.	Reau.	D.	90
66	LXXX.	Palermo, Sicily,		38 7 N.	Reau.	D.	91
"	LXXXI.	Milan, Italy,	4	45 28 N.	Reau.	D.	92
66	LXXXII.	Geneva, Switzerland,	4	46 12 N.	Reau.	D.	94
	LXXXIII.	Vienna, South Germany,	4	48 13 N.	Reau.	D.	96
"	LXXXIV.	Ratisbon, South Germany,	4	19 1 N.	Reau.	D.	97
66	LXXXV.	Stuttgard, South Germany,	4	48 46 N.	Reau.	D.	99
66	LXXXVI.	Carlsruhe, South Germany	4	19 1 N.	Reau.	D.	100
**	LXXXVII.	Berlin, North Germany,		52 30 N.	Reau.	D.	102
"]	LXXXVIII.	Copenhagen, Denmark,		55 41 N.	Reau.	D.	105
66	LXXXIX.	Paris, France,	4	18 50 N.	Reau.	D.	107
66	XC.	Zwanenburg, Holland,		52 23 N.	Reau.	D.	108
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66	XCIV.	Albany, N. Y., North America,	42	39 N.	Reau.	D.	113
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# METEOROLOGICAL CORRECTIONS.

ONE of the prominent objects of a prolonged series of meteorological observations is to determine the mean condition of the atmosphere, during a given interval of time, such as a day, a month, or a year, as to its temperature, moisture, and barometric pressure. In order to furnish the true means of these elements, free from the periodic changes which depend upon the daily course of the sun and upon the seasons, the observations ought to be made at equal intervals of time, and be so often repeated as actually to represent the sum of the variations which took place during the stated time. It is generally admitted that observations taken at every one of the twenty-four hours of the day give means which do not sensibly differ from the means which would be obtained from a still larger number of observations during the same time; so that means derived from hourly observations may be considered as the true daily, monthly, and annual means of the year in which the observations were taken.

However, as the means of a given month, or year, will generally be found somewhat to differ from those of another year, at the same place, from causes which are not of a periodic nature, it is obvious that the absolute means can only be derived from the means of a series of years, in which the differences arising from these non-periodic variations may be considered as sufficiently balancing each other.

Hourly observations can be expected only from a very few stations, favored with peculiar arrangements for the purpose. By far the larger number of observers must necessarily confine themselves to three or four observations a day. The means, therefore, deduced from such a set of observations, generally differ from the true means which would be given by hourly observations, by a quantity which varies with the hours selected for the observations. If that quantity, however, is known by having been previously determined for every hour, or set of hours, by a long series

#### METEOROLOGICAL CORRECTIONS.

of hourly observations taken at some station in a similar climatic situation, it is evident that, whatever be the hours at which observations are taken, the means derived from them can always be reduced to the true means by correcting them for that difference.

The following tables furnish such corrections, both for periodic and non-periodic variations of temperature, and for stations situated in various latitudes. They give the quantities which must be added to, or subtracted from, the hourly means, in order to obtain the true means of the day, of the month, and of the year.

Two tables of the same description, for moisture, which may be considered as specimens of the kind, close the set.

Two other tables, for correcting the mean barometric pressures, are found at the end of the Hypsometrical Tables, pp. 92, 93.

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8

# CORRECTIONS FOR TEMPERATURE.

HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OR

# TABLES

FOR REDUCING THE MEANS OF THE OBSERVATIONS TAKEN AT ANY HOUR OF THE DAY TO THE TRUE MEAN TEMPERATURE OF THE DAY, OF THE MONTH, AND OF THE YEAR.

### HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OR

CORRECTIONS TO BE APPLIED TO THE MEANS OF THE HOURS OF OBSERVATION, OR SETS OF HOURS, IN ORDER TO OBTAIN THE TRUE MEAN TEMPERATURES OF THE RESPECTIVE DAYS, MONTHS, AND OF THE YEAR.

The following set contains all the tables for correcting the means of observations on atmospheric temperature for the effect of diurnal variation which have been published by Dove, together with a few others of the same description. Dove's tables are found in two papers, published in the Memoirs of the Royal Academy of Berlin for 1846 and for 1856, and in the first Report on the Observations of the Meteoro-

logical Institute of Prussia, Berlin, 1851.

In the first paper are twenty-nine tables, in Reaumur's scale, nine of which have been republished, in Fahrenheit's scale, in the *Proceedings of the British Association* for 1847, and will also be found below. In that series the corrections have been formed by finding first the differences between the hourly and the true means, and then computing the observations by Bessel's formula, in order to eliminate the accidental irregularities due to the shortness of the period during which the observations were taken. Calling x the horary angle reckoned from noon, Bessel's formula is

$$tx = u + u' \sin(x + U') + u'' \sin(2x + U'') + u''' \sin(3x + U''').$$

The stations at which hourly observations were made are Trevandrum, Madras, Bombay, Salzuflen, Prague, St. Petersburg, Catharinenburg, Barnaul, Nertchinsk, Matoschkin-Schar, Strait of Kara, and Boothia Felix. Bi-hourly observations were taken at Brussels, Greenwich, and Toronto; in all others the night observations are wanting, and were obtained by interpolation. Moreover, in several stations the number of observations was small, at Madras even only thirty-six days. The tables of that series may be readily distinguished from those belonging to the same stations in the second, by their containing the corrections for several sets of hours, which are not found in the tables of the other.

In Dove's second series, and in all other tables, the corrections given are simply the differences, with reverse signs, between the hourly and the true means, excepting, however, the stations of Toronto, in which the corrections were computed, by Bessel's formula, by Colonel Sabine; of Prague, by Jelineck; of Salzburg, and those of

Geneva and St. Bernard, by Plantamour.

The observations from which these tables are derived were made hourly at Hobarton during 8 years; at the Cape of Good Hope, for  $5\frac{1}{4}$  years; St. Helena, 5 years; Madras, 5 years; Bombay, 4 years; Calcutta,  $1\frac{1}{2}$  years; Toronto, 6 years; Philadelphia, 3 years; Makerstoun, 3 years; Utrecht,  $1\frac{3}{4}$  years; Prague,  $10\frac{1}{2}$  years; Munich, 7 years; Salzburg, 6 years; St. Petersburg, 10 years; Catherinenburg, 6 years; Barnaul, 5 years; Tiflis, 4 years; Nertchinsk, 6 years; Peking, 4 years; Sitka, 5 years. In the following stations the observations were bi-hourly:—Washington, for  $1\frac{1}{2}$  years; Greenwich, 7 years; Dublin, 4 years; Brussels, 9 years; Geneva and St. Bernard, 4 years; Schwerin, 3 years.

The observations made in England, and in her colonies, are found in the various government publications. Those of the Russian stations are taken from the Annuaire Météorologique et Magnétique des Ingénieurs des Mines, and in the Annales de

l'Observatoire Physique Central de Russie. The observations made at Prague, Munich, Geneva, with those at St. Bernard, Makerstoun, Greenwich, Brussels, and Washington, were published by their respective Observatories; those of Utrecht, by Buys-Ballot; of Dublin, by Lloyd, in his Notes on the Meteorology of Ireland; those of Schwerin were communicated in manuscript by Dippe; the observations at Melville Island are published in No. 42 of the Parliamentary papers for 1854; and those at Bossekop, by Martins and Bravais, in the Voyage de la Commission Scientifique du Nord.

The tables of this second series being mostly deduced from longer series of observations than those in the first, when the same station is found in both, the table in the

second is generally to be preferred.

Glaisher's table for Greenwich has been taken from the Greenwich Observations. Captain Lefroy kindly furnished the tables for Toronto and Lake Athabasca. To him the author is also indebted for the observations made at Montreal by Mr. McCord, from which Table X. was computed. Table III., for Philadelphia, was deduced by the writer from the observations made at Girard College under the direction of Prof. A. D. Bache.

In order to facilitate the selection of the tables, they are marked in the table of

contents with capitals, which have the following signification: -

A and B mean that the tables have been derived from hourly and bi-hourly observations, and have been computed by Bessel's formula; C, that the tables contain values obtained by interpolation.

A', B', and C' indicate the tables based respectively on hourly and bi-hourly or partly interpolated observations, which give simply the differences between the hourly

and the true means.

The figures added to the letters indicate the number of years during which the observations used in forming the table were carried on. The stations are arranged, in each continent, in the order of their latitude.

### USE OF THE TABLES.

In order to reduce meteorological means obtained from any set of hours to the true means, the table best suited to the purpose must first be selected. The diurnal variation changing with the seasons, the latitude, the altitude, and the distance from the sea-shore, the station which comes nearest, in all these respects, to the station the observations of which are to be corrected, must be adopted.

Suppose the thermometer has been observed at Baltimore, during the month of January, at 7 A. M., 1 P. M., and 7 P. M., and the monthly means of these hours to be respectively 27°, 35°, and 31° Fahrenheit. We take Table III., Philadelphia, it being the nearest in latitude and climatic situation. We find the correction for the

hours 7, 1, and 7, and we have

For 7		ved Means. 27°	Corrections.				
For 1 I	P. M.	35°	- 3°.87				
For 7 I	P. M.	31°	— 1°.13	=	29°.87		
	Sums,	93°	— 1°.37	=	91°.63		
	Means,	31°	0°.46	=	30°.54 True	Mean for	January.

It is obvious that the corrections can be applied, either separately to each hour, as is done above, or collectively, in taking the mean of the three hourly corrections and applying it to the mean of the three observations, as in the last line, which is the more convenient method. Therefore, in order to find the correction for any set of hours, it suffices to take the mean of the corrections given in the table for the hours composing the set. The true daily means can be found in the same way, and the true yearly means can be derived from the corrected monthly means, or by applying the corrections given in the last column.

# HOURLY CORRECTIONS

FOR

# PERIODIC VARIATIONS.

NORTH AMERICA. - SOUTH AMERICA.

THE COURSE CONTRACTOR SECTION AND THE PROPERTY OF THE PROPERTY

NORTH AMERICA. - WASHINGTON. Lat. 38° 54' N. Long. 77° 3' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees	of	Reaumur.
---------	----	----------

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.M. 0 12'	1.15	1.26	1.60	1.95	2.33	2.87	2.94	2.31	2.39	1.73	0.85	0.96	1.86
2 12'	1.28	1.86	2.14	2.40	3.15	3.21	3.25	3.07	2.75	2.27	1.34	1.12	2.32
4 12'	1.45	2.18	2.67	2.75	3.56	3.64	3.83	3.49	3.15	2.89	1.92	1.54	2.76
6 12'	1.88	2.32	-2.76	2.59	2.20	2.23	2.12	2.81	3.02	3.19	2.18	1.81	2.43
8 12'	1.48	1.76	1.68	1.05	0.32	-0.16	0.09	0.28	1.04	1.69	1.88	1.68	1.07
10 12'	-0.18	-0.58	-0.88	-0.76	-1.24	-1.82	-1.32	-1.81	-1.31	-1.25	-0.17	-0.15	-0.96
P.M. 0 12'	-1.47	-2.05	-2.36	-2.39	-2.64	-2.69	-2.55	-2.97	-2.92	-2.89	-1.90	-1.57	-2.37
2 12'	-2.60	-3.15	-3.35	-3.41	-3.57	-3.84	-3.49	-3.83	-3.74	-3.64	-2.44	-2.50	-3.30
4 12'	-2.32	-3.05	-3.20	-3.51	-3.66	-4.29	-4.16	-3.59	-3.65	-3.29	-2.08	-2.19	-3.25
6 12'	-0.76	-1.25	-1.73	-2.18	-2.44	-1.60	-2.24	-1.74	-1.88	-1.84	-1.59	-1.01	-1.69
8 12'	-0.23	0.02	-0.05	0.06	0.27	0.44	-0.21	-0.26	-0.23	0.18	-0.22	-0.26	-0.04
10 12'	0.33	0.69	0.76	1.42	1.67	2.04	1.26	1.79	1.41	0.98	0.23	0.43	1.08
Means.	1.32	1.52	6.26	9.02	12.64	18.34	19.29	17.78	16.04	7.47	5.20	1.63	

II.

N. AMERICA. — PHILADELPHIA. Lat. 39° 58' N. Long. 75° 11' W. Gr. — Dove.

Degrees of Resumur.

	THE			1000	The street	-Broom or	200000		A. D. T.				
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.64	1.27	1.33	1,81	2.06	2.34	2.10	1.94	2.12	1.70	1.31	0.62	1.60
1	0.94	1.48	1.61	2.20	2.32	2.63	2.45	2.19	2.04	1.87	1.22	0.81	1.81
2	1.00	1.67	1.85	2.58	2.64	2.86	2.69	2.41	2.22	2.18	1.43	0.98	2.0
3	1.13	1.95	. 2.00	2.76	2.96	3.20	2.88	2.44	2.43	2.36	1.50	1.12	2.23
4	1.24	2.05	2.08	2.97	3.27	3.40	3.04	2.74	2.56	2.58	1.74	1.28	2.4
5	1.36	2.13	2.50	3.06	3.32	3.28	3.11	2.89	2.68	2.78	1.83	1.38	2.53
6	1.50	2.24	2.44	2.84	2.63	2.54	2.56	2.64	2.65	2.95	1.89	1.44	2.30
7	1.60	2.28	2.24	2.15	1.68	1.45	1.53	1.84	1.92	2.40	1.88	1.36	1.80
8	1.40	1.46	1.26	1.17	0.65	0.40	0.54	0.67	0.78	1.08	1.21	1.14	0.98
9	0.78	0.57	0.35	0.23	-0.39	-0.52	-0.36	-0.20	-0.18	-0.15	0.26	0.52	0.08
10	0.02	-0.39	-0.46	-0.71	-1.06	-1.23	-1.00	-1.05	-1.08	-1.17	-0.56	-0.22	-0.74
11	-0.68	-1.20	-1.38	-1.54	-1.74	-1.93	-1.74	-1.84	-1.90	-1.96	-1.27	-0.92	-1.50
(B) P	10.4	ante	HILLING.	98410	C1000	riens u	GN	493 (0				1.00	
Noon.	1	1. A. A. a. A. 11.	10000		44.30	2 Peter		AND THE REAL PROPERTY.	111111111111111111111111111111111111111	The state of	-1.77	DIMINUM	3500
2	THE PARTY OF	Table of the Control	breit		444	1444	1415	THE PARTY OF THE P	A STATE OF THE PARTY OF THE PAR	AND SERVE	-2.26	127 137	
3	1		1. 5 6 5 W. A.	200	Marie and	-3.32				-3.45	27/7	-1.84	-
136.57	the state of the s	2.4	Colorest Color		TO SECURE AND ADDRESS OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN	-3.40	1932/333	1936 135	AND VALUE OF	-3.45	W. Hisch	-1.85	-2.90
5	-			14000	The second of	-3.44	CA STORY OF THE	A LANCON SING	VAREE I SEE	ALMERICA CO.	0.000	-1.63 -1.10	
9	-1.50	-2.18	-2.52	-3.14	-3.20	-3.05	-2.94	-2.70	-2.11	-2.40	-1.40	-1.10	-2.4
6	-0.91	-1.37	-1.60	-2.49	-2.46	-2.47	-2.30	-2.03	-1.77	-1.33	-0.82	-0.64	-1.68
7	-0.51	-0.80	-0.88	-1.23	-1.28	-1.38	-1.44	-1.02	-0.76	-0.52	-0.33	-0.31	-0.87
8	-0.20	-0.21	-0.20	-0.29	-0.06	0.06	0.03	0.01	0.28	0.18	-0.14	-0.04	-0.0
9	0.07	0.11	0.90	0.35	0.65	0.82	0.57	0.60	0.81	0.65	0.29	0.09	0.49
10	0.33	0.48	0.77	0.93	1.24	1.37	1.08	1.09	1.33	1.24	0.45	0.27	0.88
11	0.56	0.75	0.96	1.44	1.74	1.91	1.55	1.44	1.64	1.63	0.79	0.40	1.23
Mean.	0.30	1.12	5.18	8.75	12.18	16.22	18.19	17.52	14.66	8.72	3.67	0.58	

North America. — Philadelphia. Lat. 39° 58' N. Long. 75° 11' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Guyot. Degrees of Fahrenheit.

				A m-22	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	eepu.		Nov.	Dec.	1 car.
Midnight.	1.47	2.90	2.90	4.13	4.68	5.28	4.70	4.37	4.47	3.80	2.70	1.40	3.57
1	2.13	3.37	3.63	4.88	5.25	5.93	5.57	4.93	4.60	4.17	2.73	1.83	4.08
2	2.20	3.57	4.17	5.88	5.95	6.45	6.10	5.43	5.00	4.87	3.20	2.20	4.59
3	2.57	4.43	4.50	6.28	6.68	7.23	6.53	5.50	5.47	5.27	3.37	2.53	5 03
4	2.80	4.67	4.70	6.75	7.38	7.68	6.90	6.17	5.77	5.77	3.90	2.87	5.45
5	3.07	4.83	5.63	6.95	7.48	7.40	7.03	6.50	6.03	6.23	4.10	3.10	5.70
6	3.40	5.10	5.50	6.45	5.93	5.73	5.80	5.93	5.97	6.60	4.23	3.23	5.32
7	3.63	5.17	5.03	4.90	3.80	3.28	3.50	4.13	4.33	5.37	4.20	3.07	4.20
8	3.17	3.33	2.80	2.50	1.48	0.90	1.27	1.50	1.93	2.40	2.70	2.57	2.10
9	1.77	1.33			C		-0.77	17.5	F		0.57	1.17	0.19
10	0.07						-2.20					-0.50	-1.6
11	-1.40	-2.63	-3.10	-3.40	-3.90	-4.33	-3.87	-4.13	-4.27	-4.43	-2.87	-2.07	-3.3
Noon.	-2.70	-3.93	-4.43	-4.72	-5.03	-5.63	-5.03	-5.27	-5.50	-5.90	-4.00	-2.87	-4.5
1	-3.87	-5.27	-5.50	-6.38	-6.08	-6.88	-5.93	-6.00	-6.47	-7.10	-5.10	-3.67	-5.6
2	-4.57	-5.97	-6.17	-7.12	-6.98	-7.45	-6.63	-6.83	-7.20	-7.80	-5.67	-4.13	-6.4
3	-4.70	-6.30	-6.90	-7.63	-7.55	-7.63	-7.03	-7.00	-7.33	-7.80	-5.60	-4.17	-6.6
4	-4.43	-6.00	-6.73	-7.65	-7.78	-7.73	-6.83	-6.70	-7.13	-7.53	-5.07	-3.67	-6.4
5	-2.90	-4.87	-5.67	-7.00	-7.33	-6.85	-6.57	-6.07	-6.23	-5.57	-3.30	-2.47	-5.4
6	-2.03	-3.03	-3.60	-5.55	-5.53	-5.55	-5.13	-4.57	-3.97	-3.03	-1.87	-1.43	-3.7
7	-1.13	-1.77	-1.97	-2.70	-2.88	-3.10	-3.20	-2.30	-1.70	-1.20	-0.77	-0.70	-1.9
8	-0.43	-0.43	-0.43	-0.60	-0.13	0.15	0.08	0.03	0.63	0.37	0.15	-0.10	-0.1
9	0.17	0.30	0.73	0.85	1.48	1.85	1.33	1.37	1.83	1.43	0.63	0.20	1.0
10	0.77	1.13	1.73	2.15	2.80	3.10	2.47	2.47	3.00	2.77	1.00	0.60	2.0
11	1.27	1.73	2.17	3.30	3.93	4.30	3.53	3.23	3.70	3.63	1.77	0.90	2.7
WATER BUILD	4/19		14	1-16	in-os		12= 1	0.4=	95.0-	8F.O.		t (tab.)	
6, 6	0.69	1.04	0.95	0.45	0.20	0.09	0.34	0.68	1.00	1.79	1.18	0.90	0.7
7, 7	1.25	1.70	1.53	1.10	0.46	0.09	0.15	0.92	1.32	2.09	1.72	1.19	1.1
8, 8	1.37	1.45	11-19-	Day of the last	0.68	A Comment			1.01	1.38	1.35	1.24	1.0
9, 9	0.97	0.82	0.76	0.72	0.32	0.35	0.28	0.47	0.72	0.53	0.60	0.69	0.6
10, 10	0.42	0.15	0.35	0.31	0.21	0.18	0.14	0.05	0.29	0.05	-0.13	0.05	0.1
7, 2, 9	-0.22	-0.17	-0.15	-0.53	-0.57	-0.77	-0.61	-0.44	-0.35	-0.33	-0.28	-0.29	-0.3
6, 2, 8	-0.53	-0.43	-0.37	-0.42	-0.39	-0.52	-0.37	-0.29	-0.20	-0.28	-0.43	-0.67	-0.4
6, 2, 10	-0.13	0.09	0.53	0.74	0.58	0.46	0.55	0.52	0.59	0.52	-0.15	-0.10	0.4
6, 2, 6	-1.07	-0.72	-1.42	-2.07	-2.19	-2.42	-1.43	-1.82	-1.73	-1.41	-1.10	-0.78	-1.4
7, 2	-0.47	-0.40	-0.57	-1.11	-1.59	-2.09	-1.57	-1.35	-1.44	-1.22	-0.74	-0.53	-1.0
8, 2	-0.70	-1.32	-1.68	-2.31	-2.75	-3.28	-2.68	-2.67	-2.90	-2.70	-1.49	-0.78	-2.1
8, 1							-2.33						
7, 1	-0.12	-0.03	-0.24	-0.74	-1.14	-1.80	-1.22	-0.94	-1.07	-0.87	-0.45	-0.30	-0.7
9, 12, 3, 9	-1.37	-2.15	-2.45	-2.73	-2 99	-3.14	-2 88	-2.83	-2.85	-3 16	-2.39	-1.42	-2.5

N. AMERICA. — FRANKFORT ARSENAL. Lat. 39° 57' N. Long. 75° 8' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

		0000			Degree	s of Re	aumur.					1	
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.34	1.46	1.75	1.87	2.60	3.41	3.07	2.69	2.63	2.40	1.18	1.34	2.15
2	1.51	1.73	2.13	2.33	3.05	3.73	3.51	3.04	3.05	2.67	1.27	1.50	2.46
3	1.82	1.98	2.56	2.88	3.43		3.83	3.32	3.49	2.94	1.41	1.66	2.77
4	2.13	2.23	2.90	3.29	3.57	3.84	3.84	3.36	3.73	3.13	1.51	1.80	2.94
5	2.31	2.46	2.95	3.31	3.32	100	3.40	2.99	3.54	3.12	1.73	35 /	2.86
6	2.25	2.35	2.62	2.83	2.65	Part Land	2.52	2.21	2.84	2.82	1.38	1.80	2.39
7	1.88	2.01	1.91	1.94	1.66	35F0 (C)	1.34	1.15	1.71	2.19	1.06	1.52 0.97	1.64
8	1.22	1.33	0.94	0.85	0.57	-0.03	0.08	0.01	0 36	1.26	0.58	0.97	0.68
9	0.34	0.30	-0.07	-0.20	-0.45	-1.20	-1.06	-1.00	-0.96	0.12	-0.02	0.18	-0.34
10	-0.62											-0.76	
11	-1.54		-1.76										
Noon	-2.30	-2.60	-2.32	-2.22	-2.35	-3.17	-3.16	-2.78	-3.47	-3.35	-1.96	-2.45	-2.68
1	-2.85	-3.01	-2.74	-2.72	-3.07	-3.51	-3.58	-3.16	-3.86	-4.05	-2.38	-2.87	-3.15
2												-2.89	
3												-2.54	
4	-2.53	-2.44	-2.95	-3.55	-3.70	-3.75	-3.67	-3.42	-3.63	-3.66	-1.96	-1.94	-3.10
5	-1 00	-1.87	_2 50	-2 11	-3 20	_3.23	-3 00	-2 81	-2.84	-2.75	-1.52	-1.23	-2.50
6	-1.14	Dill Bau	315.	-2.23		A 10 30 TO	4.379 100	-1.83	45-5 PR	100000	-0.56		
7		-0.46	STALL STREET			ALC: THE	-0.83	-9/35 W.		PAGE VAL	0.14	0.01	-0.63
8	0.29	0.12	-0.06	0.02	-0.10	0.07	0.28	0.43	0.66	0.43	0.69	0.42	0.27
9	0.76	0.66	0.61	0.85	0.80	1.17	1.17	1.29	1.49	1.17	1.02	0.71	0.98
10	1.02	0.00	1.05	1.32	1.43	Arrian Burn	1.79	1.84	1.96	1.66	1.15	0.90	1.42
11	1.13	1.18	1.31	1.50	1.85		2.24	2.15	2.18	1.96		1.06	1.67
Midn	1.19	1.36	1.48	1.62	2.01		2.63	2.40	2.35	2.18	1.15	1.20	1.88
		384				No.				77.00		10.112	
6. 6	0.56	0.62	0.42	0.30	0.17	0.07	0.26	0.19	0.56	0.58	0.41	0.62	0.40
7. 7	0.76	0.78	0.50	0.42	0.24		0.26	0.24	0.62	0.83	The second second		0.51
8.8	0.76	0.72	0.44	0.43	0.24		0.18	0.22	0.51	0.85	0.00	0.70	0.48
9. 9	0.55	0.48	0.27	0.33	0.18	-0.02	0.06	0.14	0.26	0.64	0.50	0.44	0.32
10.10	0.20	0.11	0.03	0.13	0.07	-0.05	-0.08	0.03	-0.05	0.26	0.23	0.07	0.08
7. 2. 9	-0.13	-0.17	-0.16	-0 13	-0.35	-0.45	-0.45	-0.35	-0.29	-0.33	-0.15	-0.22	-0.27
6. 2. 8												-0.22	
6. 2.10	0.08	13:55 The 18	1000 1000 100	0.32					0.24	0.04		-0.06	0.14
6. 2. 6	-0.64	-0.65	-0.72	-0.86	-1.06	-1.21	-1.12	-1.03	-0.98	-1.06	-0.57	-0.55	-0.87
7. 2	-0.57	-0.59	-0.55	-0.63	-0.93	-1.26	-1.27	-1.17	-1.18	-1.09	-0.74	-0.69	-0.89
8. 2						0.4	1772.7619	No. of the last of	Ext. Color			-0.96	
8. 1				The second second						ALL DESCRIPTION OF THE PARTY OF		-0.95	
7. 1	-0.49	-0.50	-0.42	-0.39	-0.71	-1.13	-1.12	-1.10	-1.08	-0.93	-0.66	-0.68	-0.76
9.12.3.9	-1.03	-1.14	-1.22	-1.28	-1.45	-1.77	-1.75	-1.53	-1.74	-1.57	-0.84	-1.03	-1.36
7. 2.2(9)	0.10		-0.03				-0.05	1000000		0.04	C. C. C. C. C.	The second	0.04
Dail. ext.	-0.36	-0.36	-0.08	-0.12	-0.11	0.02	-0.05	-0.13	-0.17	-0.62	-0.41	-0.51	-0.24

N. AMERICA. — FRANKFORT ARSENAL. Lat. 39° 57' N. Long. 75° 8' W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

O HE IS			Taylor .			Degree	s of Fai	hrenheit	•					
Hou	ırs.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
10000	shdi	- 00				- 0-	~ 0=	0.01	0.05	- 00	- 10	0.00	0.00	
Mor		3.02	10 TO	3.94	10.5 F2 C45	5.85	A CARL	- Shall	6.05	V 1 1 1 1 1 1 1	To the same	The second	1 500	
	2	3.40	F-6. F-12. Th.	4.79	5.24		TO START	1000	6.84	6.86	PER SEC. 18-11-11-11	1.00		1 1000
	3	4.10	4.46	5.76	6.48	7.72	8.82	8.62	7.47	7.85	6.62	3.17	3.74	6.23
	4	4.79	5.02	6.53	7.40	8.03	8.64	8.64	7.56	8.39	7.04	3.40	4.05	6.62
	5	5.20	L. P. Commission	6.64	7.45	7.74	12.5	CHARLE	6.73	7.97	7.02	100 St. 100 St. 100	4.21	6.44
1	6	5.06	5.29	5.90	6.37	5.96	5.54	5.67	4.97	6.39	6.35	3.11	4.05	5.38
	-7	4.23	4.52	4.30	4.37	3.74	2.84	3.02	2.59	3.85	4.93	2.39	3.42	3.69
	8	2.75	2.99	2.12	1.91	1.28	-0.07	0.18	0.02	0.81	2.84	1.31	2.18	1.53
	9	0.77	0.68	-0.16	-0.45	-1.01	-2.70	-2.39	-2.25	-2.16	0.27	-0.05	0.41	-0.77
	10	111111111111111111111111111111111111111	-1.62	-2.25	-2.36	I I I I I I I I I I	1	-4.41		The second second	K 1 400-	1		-2.86
A STATE	24.0	-3.47			100000	7.15		-5.94	ALLEY BOTH	100	IN THE REAL PROPERTY.	40.00		
NT.	11	District Co.	0.00	4 5 5 5 5		A PARTY	10000	ACCRECATE TO	200	and the same of the	99911225	Company of the last of the las		100000 441
Noor	1	-3.18	-5.85	-5.22	-5.00	-5.29	-7.13	-7.11	-0.20	<b>-7.81</b>	-7.54	-4.41	-5.51	-6.03
1000	1	-6.41	-6.77	-6.17	-6.12	-6.91	-7.90	-8.06	-7.11	-8.69	-9.11	-5.36	-6.46	-7.09
THE STATE OF	2	-6.80	-7.16	-6.77	-7.18	-7.92	-8.48	-8.71	-7.83	-9.16	-9.81	-5.72	-6.58	
	3	-6.57	-6.59	-6.98	-7.94	-8.51	-8.75	-8.87	-8.12	-9.05	-9.50	-5.40	-5.72	-7.67
	4	-5.69	23024	Service and	0.00	142/24	-8.44	7	STATE OF THE PARTY OF		-8.24	1	-4.37	
	5	-4.28	-4.21	-5.63	-7.00	-7.20	-7.27	-6.75	-6.32	-6.39	-6.19	-3.42	-2.77	-5.63
	6	-2.57	-2.50	-4.01	-5.02	-5.20	-5.24	-4.50	-4.12	-3.87	-3.71	-1.26	-1.24	-3.60
Traces of	7	-0.83	-1.04	-2.07	-2.45	-2.68	-2.61	-1.87	-1.51	-1.08	-1.22	0.32	0.02	-1.42
	8	0.65	0.27	-0.14	0.05	-0.23	0.16	0.63	0.97	1.49	0.97	1 55	0.95	0.61
	9	1.71	1.48	1.37	1.91	1.80	2.63	2.63	2.90	3.35	2.63	2.30	1.60	2.21
	10	2.30	2.09	2.36	1.97	3.22	4.55	4.03	4.14	4.41	3.74	2.59	2.03	3.20
	11	2.54	2.66	2.95	3.38	4.16	5.87	5.04	4.84	4.91	4.41	2.05	2.39	3.76
Midn		2.68	3.06	3.33	3.65	4.52	6.84	5.92	5.40	5.29	4.91	2.59	2.10	4.23
					7.15							2.00	2.10	
6.	G	1.26	1 40	0.0-	0.00	0.00	0.10	0.50	0.40	1 00	100	0.00	- 10	0.00
7.	- 11		1.40	0.95	0.68	0.38	0.16	0.59	0.43	1.26	1.31	0.92	1.40	0.90
		1.71	1.76	1.13	0.95	0.54	0.11	0.59	0.54	1.40	1.87	1.35	1.71	1.15
3.		1.71	1.62	0.99	0.97	0.54	0.05	0.41	0.50	1.15	1.91	1.42	1.58	1.08
9.		1.24	1.08	0.61	0.74	0.41	-0.05	0.14	0.32	0.59	1.44	1.13	0.99	0.72
10.1	0	0.45	0.25	0.07	0.29	0.16	-0.11	-0.18	0.07	-0.11	0.59	0.52	0.16	0.18
7. 2.	9	-0.29	-0.38	-0.36	-0.29	-0.79	-1.01	-1.01	-0.79	-0.65	-0.74	-0.34	-0.50	-0.61
6. 2.	8	-0.36		-0.39	-0.25	-0.72				-0.43	-0.83	-0.36		-0.56
6. 2.		0.18	0.07	0.50	0.72	0.43	0.54		0.43	0.54	0.09	1000000	-0.14	0.32
6. 2.	11	1	0 - 0	-1.62	-1.94	-2.39	-2.72		1000	-2.21	-2.39			
STORY OF	17.16	10	SU.	5.54	21(1)	-	10.374	E 10	20.00	to 04	24 3	-1.28	-1.24	-1.96
7. 2		-1.28				-2.09	-2.84	-2.86	-2.63	-2.66	-2.45	-1.67	-1.55	-2.00
8. 2	100	-2.03	-2.09	-2.34	-2.63	-3.33	-4.28	-4.28	-3.92	-4.19	-3.49	-2.21	-2.16	-3.08
8. 1	200	-1.85	-1.89	-2.03	-2.12		-3.98	-3.94				-2.03		-2.79
7. 2							-2.54	-2.52	-2.27	-2.43	-2.09	-1.49		-1.71
9.12.	3.9	-2.32	-9 57	-0	0.00	0.00	9.00	001	-de	A TO	53.59	17:27	-55	ERAS P
7. 2.5		0.23	0.09	0.07						1000	-3.53	-1.89	- 1	-3.06
Dail.	( )	0.20	0.03	0.07	0.25	-0.10	-0.09	-0.11	0.14	0.36	0.09	0.32	0.02	0.09
		00	-0.81				-	-0.11			01-5		ALC: NO	THE REAL PROPERTY.

N. AMERICA. — TORONTO. Lat. 43° 39′ 35″ N. Long. 79° 21′ 30″ W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

					Degree	B OI I I	hrennen						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.87	0.92	3.04	4,43	5.90	5.94	6.30	5.06	5.74	4.16	1.91	1.04	3.87
2	2.16	1.33	3.56	5.11	6.64	6.62	7.13	5.68	6.68	4.68	2.14	1.13	4.41
3	2.39	1.91	4.19	5.76	7.36	7.29	8.01	6.82	7.63	5.04	2.39	1.40	5.02
4	2.68	2.66	4.75	6.17	7.65	7.56	8.44	7.61	8.19	5.20	2.61	1.78	5.45
5	3.02	3.40	4.95	5.94	7.07	6.98	7.88	7.49	7.94	5.02	2.68	2.16	5.38
6	3.29	3.92	4.61	4.97	5.49	5.38	6.14	6.14	6.71	4.48	2.52	2.39	4.68
7	3.26	3.98	3.65	3.38	3.17	3.04	3.49	3.67	4.52	3.44	2.05	2.27	3.33
8	2.72	3.40	2.12	1.42	0.68	0.43	0.52	0.68	1.78	1.91	1.15	1.71	1.55
9	1.58	2.33	0.29	-0.50	-1.51	-1.85	-2.12	-2.09	-1.06	-0.05	-0.07	0.79	-0.36
10	0.00	0.61	-1.60	2012/01/20 12:3	AND SHAPE OF THE PARTY OF THE P	and the same	-4.01	COLUMN TO SERVICE	-3.62	-2.25	-1.46	-0.34	-2.12
11	-1.71						-5.15				-2.79	-1.44	-3.58
Noon	-3.11		-4.55				-5.90				-3.78	-2.30	
		110			14.1		435	1000			13.50		100
1	-3.89	-3.67	-5.36	-5.00	-5.99	-5.94	-6.59	-6.50	-8.33	-7.11	-4.28	-2.77	-5 45
2	-3.98	2300000	-5.72	- NORTH 18		C.75815.701	-7.47	22 House 187	3 TO 1 TO 1	-7.25	LUCK TO THE REAL PROPERTY.	-2.86	
3	-3.53	COSTON IN	-5.60	2017/01/2015	-8.15	C12 25 To 1 TO 1	-8.28		-8.87	12000	A THE WAY	-2.66	
. 4	-2.84	C PROUB	-5.02	COMPETE:	-8.51		0.13915-07	11000000000	1 The Late of the	1100000		-2.23	. 11 15 69
an ollass	2.01	0.00	101.0	0.10	0.01	2000	0.00	NAUK!	Ware.	1	1371.51		
5	-2.14	-2.63	-4.03	-5.94	-7.76	-7.43	-7.83	-6.95	-6.59	-3.53	-1.44	-1.71	-4.84
6	-1.62	-1.89	-2.75	-4.66	-5.83	-5.65	-5.94	-5.00	-4.43	-1.91	-0.45	-1.13	-3.44
7	-1.24	-1.24	-1.31	-2.81	-3.08	-3.04	-3.17	-2.25	-1.94	-0.50	0.32	-0.54	-1.73
8	-0.88	-0.68	0.05		-0.16	-0.18		0.65	0.43	0.65	0.86	0.02	-0.02
British HA.	Visual	1880	Bei	LAND A	- Intitul		ille.	1926	THE R	Thin.	Aller	T &	TANK I
9	-0.43	-0.25	1.15	1.06	2.30	2.30	2.39	2.97	2.30	1.53	1.17	0.47	1.42
10	0.16	0.11	1.89	2.41	3.94	3.98	4.14	4.32	3.58	2.25	1.37	0.81	2.41
11	0.83	0.38	2.34	3.26	4.82	4.93	5.11	4.77	4.37	2.90	1.53	0.97	3.02
Midn	1.42	0.63	2.66	3.85	5.33	5.45	5.64	4.84	5.00	3.56	1.71	1.01	3.42
TALL SEE	100.0	100.0	West of	130	10.4	Disco.	- Marie					a like	
6. 6	0.83	1.01	0.95	0.16	-0.18	0.14	0.11	0.56	1.13	1.28	1.04	0.63	0.61
7. 7	1.01	1.27	1.17	0.29	10000000	0.00	0.16	0.72	1.28	1.49	1.19	0.86	0.81
8. 8	0.92	1.37	1.08	0.23	0.27	0.14	0.16	0.68	1.10	1.28	1.01	0.86	0.77
9. 9	0.59	0.99	0.72	0.29	0.41	0.23	0.14	0.45	0.63	0.74	0.56	0.63	0.54
10.10	0.07	0.36	0.14	0.16		0.27	0.07	0.09	-0.02	0.00	-0.05	0.23	0.14
20.10	0.01	0.00	0.14	0.10	0.10		0.01	0.00	0.02	0.00	0.00	0.20	R. A.
7. 2. 9	-0.38	-0.11	-0.32	-0.45	-0.56	-0.52	-0.54	-0.16	-0.70	-0.77	-0.32	-0.05	-0.41
6. 2. 8		-0.27	V 10.00	- 10 Track C	-0.61		CONTRACTOR OF THE PARTY OF THE	10000000	77000-30	PS-2507-1202		-0.16	200 1200 110
6. 2.10	10.000000	-0.02	0.27	0.54	0.77	0.83	0.95	1.13	152.77	-0.18	-0.09	0.11	0.38
6. 2. 6	1	-0.68		-1.82			-2.43		-2.21	100	-0.70		-1.58
	2 612	100			(Eller		Silve		PADY.	-	148		
7. 2	-0.36	-0.05	-1.04	-1.19	-2.00	-1.94	-2.00	-1.73	-2.18	-1.91	-1.06	-0.29	-1.31
8. 2		-0.34	C. C. C.		200 200 300				2000	A.V. C. S. C.	PARTY AND THE PA	DOMESTIC:	The second second
8. 1	-0.59			and the same of		and the second second	-3.04	15 1 1 1 1 1 1 1 1 1 1 1			23.33	-0.54	A STATE OF THE STA
7. 1	-0.32		The second second				-1.55	Committee of the Commit	the same of		and the same of th	-0.25	-1.06
9.12.3.9	-1 27	-1.15	_2 19	-2 50	-3 08	_3 12	_3 40	_3 20	-3.71	-2 70	_1 55	-0.92	-2.43
7. 2.2(9)		-0.16		-0.07		The state of the s	0.20	0.63	The same	-0.18	0.07	0.09	0.05
1. 2.2(3)	0.41	0.10	0.07	0.07	0.10	0.10	0.20	0.00	0.07	0.10	0.07	0.03	0.00
-													

The numbers without sign must be added; those with the sign — must be subtracted.

N. AMERICA. — TORONTO. Lat. 43° 39′ 35″ N. Long. 79° 21′ 30″ W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — DOVE.

Degrees of Reaumur.

						Degree	s of Re	aumur.						
	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	Morn. 1	0.83	0.41	1.35	1.97	2.62	2.64	2.80	2.25	2.55	1.85	0.85	0.46	1.72
1	2	0.96	0.59	1.58	2.27	2.95	2.94	3.17	2.57	2.97	2.08	0.95	0.50	1.96
1	3	1.06	0.85	1.86	2.56	3.27	3.24	3.56	3.03	3.39	2.24	1.06	0.62	2.23
	4	1.19	1.18	2.11	2.74	3.40	3.36	3.75	3.38	3.64	2.31	1.16	0.79	2.42
1	and Toronto			10000				0.70	0.00	0.40				
	5	1.34	1.51	2.20	2.64	3.14	3.10	3.50	3.33	3.53	2.23	1.19	0.96	2.39
1	6	1.46	1.74	2.05	2.21	2.44	2.39	2.73	2.73	2.98	1.99	1.12	1.06	2.08
	7	1.45	1.77	1.62	1.50	1.41	1.35	1.55	1.63	2.01	1.53	0.91	1.01	1.48
	8	1.21	1.51	0.94	0.63	0.30	0.19	0.23	0.30	0.79	0.85	0.51	0.76	0.69
			×	150	112	- IL		The sale		ENE	2019			P. 30
	9	0.70	0.99	0.13	-0.22	-0.67	-0.82	-0.94	-0.93	-0.47	-0.02	-0.03	0.35	-0.16
1	10	-0.00	0.27	-0.71	-0.92	-1.37	-1.54	-1.78	-1.84	-1.61	-1.00	-0.65	-0.15	-0.94
	11	-0.76	-0.51	-1.45	-1.45	-1.84	-1.98	-2.29	-2.37	-2.54	-1.95	-1.24	-0.64	-1.59
-	Noon	-1.38	100,00	-2.02	-1.86	THE RESERVE	7711	-2.62	-2.65	-3.22	-2.72	-1.68	-1.02	-2.07
1		1980	THE PERSON	200 g	- Interes	1000	05.0	100	337	- 60.	199-3	THE REAL PROPERTY.	11 52	THE
1	1	-1.73	-1.63	-2.38	-2.22	-2.66	-2.64	-2.93	-2.89	-3.70	-3.16	-1.90	-1.23	-2.42
-	2	-1.77	-1.81	-2.54	-2.56	-3.18	-3.06	-3.32	-3.16	-3.95	-3.22	-1.84	-1.27	-2.64
1	3	-1.57	-1.74	-2.49	-2.82	-3.62	-3.44	-3.68	-3.42	-3.94	-2.90	-1.56	-1.18	-2.70
1	4	100000	-1.50	1000	1 (1) 7 TO TO.	400000			-3.47	1,000	12 D. Fr. 10	-1.12	C. 721 7 ROS	
1		1.20	2.00	9 1 5	y Ing	10.0	TO SEE	e Merch	- TT 18	1000	DE STEVE	119.5	= 1 1	
1	5	-0.95	-1.17	-1.79	-2.64	-3.45	-3.30	-3.48	-3.09	-2.93	-1.57	-0.64	-0.76	-2.15
1	6	Contract Contract	-0.84			1000	-2.51	-2.64	-2.22	-1.97	-0.85	-0.20	-0.50	-1.53
1	7		-0.55		A 2010-11			100	-1.00		-0.22	1466	-0.24	
-	8	-0.39		0.02			-0.08	17 19 GZ 76 KG	0.29	0.19	0.29	0.38	0.01	-0.01
1	0	-0.59	-0.50	0.02	-0.54	-0.07	-0.00	-0.00	0.25	0.19	0.25	0.00	0.01	-0.01
1	9	-0.19	-0.11	0.51	0.47	1.02	1.02	1.06	1.32	1.02	0.68	0.52	0.21	0.63
	10	0.07	0.05	0.84	1.07	1.75	1.77	1.84	1.92	1.59	1.00	0.61	0.36	1.07
	11	0.37	0.17	1.04	1.45	2.14	2.19	2.27	2.12	1.94	1.29	0.68	0.43	1.34
		1		1 - 7	A 41 APT 2	1 7 2 7 4			1000	4.5		1755191		
	Midn	0.63	0.28	1.18	1.71	2.37	2.42	2.53	2.15	2.22	1.58	0.76	0.45	1.52
1		WOOD !		10.0		14.52	50.00	(Aprile An		W.	Lebels		1	
	6. 6	0.37	0.45	0.42	0.07	_0 08	-0.06	0.05	0.25	0.50	0.57	0.46	0.28	0.27
	7. 7	The second second	0.43	0.42	0.07			0.07	0.23	0.57	0.66	0.53	0.28	0.36
1		0.45	10000	YOU AND	Service of the latest	0.02	0.00	1 THE REAL WINE	111111111111111111111111111111111111111	Landa Maria	11 L D AV A TO	- 100 OW	100-31	1 - 12
	8.8	0.41	0.61	0.48	0.15	0.12	0.06	0.07	0.30	1000	0.57		0.38	
	9. 9	0.26	0.44	0.32	0.13	0.18	0.10	0.06	The Control of	0.28	0.33	- 5400 Ship	0.28	0.24
	10.10	0.03	0.16	0.06	0.07	0.19	0.12	0.03	0.04	-0.01	0.00	-0.02	0.10	0.06
	7. 2. 9	_0 17	-0.05	_0.14	_0 00	_0 25	_0 00	_0 24	_0 0~	_0 91	_0 94	-0.14	_0.00	-0.18
		-0.17		1	5.00		100000000000000000000000000000000000000	-0.24		-0.31	1300000		1	
	6. 2. 8		-0.12		-0.23	/ N/D / Co.	LIND O	-0.22	13000	105 0	-0.31	COLUMN TO SERVICE	-0.07	
	6. 2.10		-0.01	0.12	0.24	0.34	- SAZ-176	120 6530 625	LINDUM D	15000 130	C. 19 (E) (O)	10000		100
	6. 2. 6	-0.34	-0.30	-0.57	-0.81	-1.11	-1.06	-1.08	-0.88	-0.98	-0.69	-0.31	-0.24	-0.70
	7. 2	_0.10	-0.00	0.40	0 50	0.00	0.00	0.00	0 ==	0.0-	0.00	0.4	0.10	-0.50
			1000	-0.46	1					-0.97				-0.58
	8. 2				1	1		1	1	-1.58	1	The second second		A Commence of the
	8. 1	-0.26	100000			-1.18		-1.35		-1.46		100000	TE	1
	7. 1	-0.14	0.07	-0.38	-0.36	-0.63	-0.65	-0.69	-0.63	-0.85	-0.82	-0.50	-0.11	-0.47
	0.10.20	0.00	0.5-	1				1	MARCO		314.0	0.55		- 00
	9.12.3.9	11	-0.51	1	-1.11	100000000000000000000000000000000000000		-1.55		-1.65		1		-1.08
	7. 2.2(9)	-0.18	-0.07	0.03	-0.03	0.07	0.08	0.09	0.28	0.03	-0.08	0.03	0.04	0.02
16	Dell and	-0.10	0.00	0.7-	00-	0.70	0.10	0.00	0.00	0.10	0.10	0.00	0.77	0.74
1	Dail. ext.	11-0.16	0.02	-0.17	-0.07	-0.19	-0.12	-0.03	-0.05	-0.16	-0.46	-0.36	-0.11	-0.14
-0									-					

### VIII.

NORTH AMERICA. - TORONTO. Lat. 43° 40' N. Long. 79° 21' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Lefroy.

Degrees of Fahrenheit.

			1	B 100	A TOP		1000		Had I	(age)		SILLA	97777
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec	Year
Midnight.	1.47	1.73	2.63	3.22	5.02	5.15	6.37	5.33	5.96	3.22	1.80	0.90	3.5
1	1.95	2.09	3.11	3.79	5.93	6.00	7.13	6.06	4.57	3.80	2.10	1.50	4.0
2	2.05	2.46	3.47	4.48	6.77	6.70	7.68	6.69	5.17	4.13	2.36	1.85	4.4
3	2.20	2.82	3.76	5.08	7.45	7.50	8.41	7.29	5.59	4.31	2.66	1.96	4.9
4	2.28	3.20	4.07	5.38	7.93	8.06	9.03	7.63	6.18	4.61	2.85	2.04	5.2
5	2.46	3.62	4.35	5.75	7.83	7.88	9.02	7.89	6.77	4.77	2.76	2.07	5.4
6	1.83	4.23	4.75	5.48	5.40	5.21	5.92	6.57	6.17	4.71	2.52	2.39	4.6
7	1.94	4.34	3.93	3.22	2.43	2.41	2.38	3.28	3.68	3.94	2.52	2.55	3.0
			E pre	-			NO-T		1.1	2			
8	1.66	3.29	1.89	1.09	0.06	0.10	-0.31	0.21	1.02	1.66	1.53	2.12	1.2
9	0.63	1.02	-0.25	-1.01	-2.11	-1.82	-2.39	-2.26	-1.52	-1.01	0.01	0.92	-0.8
10	-0.59	-0.95	-1.91	-2.45	-3.81	-3.49	-3.98	-4.18	-3.47	-2.93	-1.41	-0.53	-2.4
11	-1.70	-2.44	-3.14	-3.85	-4.92	-4.77	-5.49	-5.57	-4.85	-4.33	-2.44	-1.72	-3.7
Noon.	-2.48	-3.56	-4.15	-4.86	-5.87	-5.88	-6.72	-6.39	-5.95	-5.36	-3.34	-2.52	-4.7
1			-4.79					-7.11		-5.76	-3.74		-5.4
2	12 12 17 17 17	- 1 TO TO TO - NO	-5.31	The second second	207 (201 (201	100	-8.26	-7.62		-6.04	-3.82	-3.31	-5.8
3	-3.16	-4.90	-5.15	-6.16	-7.20	-7.37	-8.34	-7.98	-7.01	-5.85	-3.64	-3.13	-5.8
0 100	will die	1	1	17 12	I R	1	0.1	中台	(0)	0.0	E WIT	0.91	
4	300000000000000000000000000000000000000	(303/7)	-4.65		1 1 1 1 1 1 1	100	100	-7.79	THE REAL PROPERTY.	10,700	-2.83		-5.4
5	100000	9.3527.31	-3.92		-	100000000000000000000000000000000000000					-1.58		-4.6
6 7	-0.90 -0.40	3000	-2.35 $-0.91$		-5.05 -2.19		-6.57 -3.28	-5.39 -1.64	-3.16 -0.43	-1.37 $-0.25$	-0.76 -0.15	-0.82	-3.1 $-1.2$
						THE PARTY					Sact.		
8	-0.12	-0.13	0.03	0.66	0.43	0.33	0.68	1.23	0.81	0.48	0.19	-0.12	0.3
9	0.07	0.52	1.00	1.78	2.31	2.44	2.99	2.70	1.90	1.25	0.44	0.18	1.4
10	0.44	1.06	1.63	2.59	3.29	3.80	4.24	3.73	2.94	1.97	0.78	0.47	2.2
11	0.77	1.60	2.01	3.07	4.20	4.76	5.21	4.54	3.61	2.68	1.13	0.59	2.8
100,1	0.10	18.5	1.0	- 00	0.75	0.00	.1 10	0.50	1.00	1.00	1.00	0 =0	
6, 6	0.46	1.18	1.20	1.03	0.17	-0.26 $-0.29$	-0.32 $-0.45$	0.59	1.50	1.67	1.38	0.78	0.7
7, 7	0.77	1.67	0.96	1.14 0.87	0.12	0.21	0.18	0.82	0.91	1.45	0.98	1.15	0.9
9, 9	0.35	0.77	0.37	0.38	0.10	0.21	0.30	0.72	0.19	0.10	0.30	0.55	0.3
0-10.1	100	2 200	- No	On THE	A L	0	219-11	1.9: 12	A POPULATION OF THE PARTY OF TH	g.0- 1	Sales	T. East	304
10, 10	-0.07	0.05					0.13	-0.22			7	-0.03	
3, 2, 10	-0.31	0.14	0.36	0.64	0.52	0.66	0.63	0.89	0.72	0.21	-0.17	-0.15	0.3
7, 2, 9 $12, 3, 9$	-0.40 $-1.23$	-0.01 $-1.73$	-0.09 $-2.01$	-0.38 $-2.56$	10000000	-0.73 $-3.16$	-0.96 -3.61	-0.55 -3.48	-0.46 -3.14	-0.28 $-2.74$	-0.29 -1.63	-0.19 -1.14	-0.4 $-2.4$
	0.00		2 7 10		7	0-0		<u> </u>			0.0	(t),t)	No.
Mean.	25.82	23.70	29.79	41.99	52.92	60.67	66.39	65.86	57.55	44.14	36.18	27.40	44.3

NORTH AMERICA. — TORONTO. Lat. 43° 40' N. Long. 79° 21' W. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.68	0.81	1.10	1.45	2.24	2.36	2.91	2.43	1.76	1.44	0.81	0.40	1.53
1	0.88	0.98	1.31	0.78	2.62	2.67	3.29	2.72	2.03	1.71	0.94	0.66	1.80
2	0.92	1.13	1.48	2.08	2.99	2.98	3.54	3.02	2.29	1.85	1.06	0.83	2.01
3	0.99	1.32	1.61	2.17	3.31	3.32	3.86	3.32	2.49	1.92	1.20	0.88	2.20
4	1.03	1.45	1.78	2.36	3.52	3.58	4.14	3.48	2.76	2.06	1.28	0.90	2.36
5	1.11	1.61	2.01	2.52	3.49	3.49	4.16	3.57	3.04	2.13	1.23	0.91	2.44
6	0.79	1.86	2.13	2.47	2.40	2.32	2.74	2.92	2.74	2.04	1.11	1.09	2.05
7	0.83	1.92	1.75	1.45	1.08	1.07	1.11	1.60	1.60	1.70	1.11	1.16	1.36
8	0.73	1.47	0.87	0.45	0.09	0.03	-0.05	0.15	0.38	0.70	0.64	0.97	0.56
9	0.30	0.44	-0.10	-0.43	-0.94	-0.81	-1.03	-0.96	-0.69	-0.49	-0.04	0.45	-0.36
10	-0.25	-0.45	-0.87	-1.11	-1.69	-1.55	-1.78	-1.84	-1.57	-1.35	-0.68	-0.20	-1.11
11	-0.77	-1.16	-1.41	-1.72	-2.20	-2.12	-2.47	-2.48	-2.20	-1.96	-1.13	-0.75	-1.70
Noon.	-1.12	-1.69	-1.87	-2.18	-2.62	-2.61	-3.05	-3.04	-2.64	-2.36	-1.48	-1.11	-2.15
1	-1.34	-2.07	-2.16	-2.60	-3.03	-2.93	-3.46	-3.25	-2.90	-2.55	-1.66	-1.42	-2.45
2	-1.46	-2.25	-2.41	-2.76	-3.18	-3.12	-3.84	-3.51	-3.08	-2.70	-1.69	-1.49	-2.62
3	-1.44	-2.24	-2.32	-2.80	-3.21	-3.29	-3.92	-3.66	-3.09	-2.60	-1.62	-1.38	-2.63
4	-1.21	-2.00	-2.11	-2.62	-3.19	-3.40	-3.93	-3.60	-3.00	-2.28	-1.22	-1.09	-2.47
5	-0.77	-1.47	-1.78	-2.30	-3.02	-3.13	-3.72	-3.35	-2.57	-1.50	-0.68	-0.67	-2.08
6	-0.40	-0.82	-1.03	-1.50	-2.24	-2.55	-3.08	-2.51	-1.38	-0.59	-0.32	-0.36	-1.40
7	-0.17	CONTRACTOR OF THE PARTY OF THE		-0.37	-0.96	-1.33	-1.54	-0.74	-0.18	-0.10	-0.06	-0.21	-0.53
8	-0.03	0.00	0.05	0.33	0.24	0.13	0.33	0.56	0.39	0.23	0.08	-0.04	0.19
9	0.06	0.28	0.50	0.81	1.02	1.09	1.38	1.26	0.85	0.57	0.20	0.07	0.67
10	0.23	0.53	0.79	1.16	1.45	1.69	1.93	1.72	1.32	0.90	0.36	0.20	1.02
11	0.37	0.76	1.08	1.38	1.86	2.12	2.45	2.07	1.60	1.20	0.52	0.25	1.31
Mean.	-2.97	-3.88	-0.98	4.72	9.29	12.75	15.11	15.00	11.37	5.42	1.88	-2.03	

X.

NORTH AMERICA. — MONTREAL. Lat. 45° 30' N. Long. 73° 22' E. Gr.

Degrees of Fahrenheit.

Hour.	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	March.	April.	May.	June.	July.	Year.
Midn.	4.00	3.89	2.83	1.36	1.68	1.10	1.28	1.31	2.52	4.55	5.25	4.39	2.85
2	5.39	4.34	4.01	1.59	1.00	2.36	2.69	2.88	4.37	6.95	7.42	7.17	4.20
4	6.34	5.60	4.84	1.81	1.38	2.88	3.36	5.56	7.09	6.95	7.18	7.57	4.96
6	5.99	4.59	4.93	1.36	1.32	3.54	3.90	5.22	5.56	6.61	5.55	5.46	4.50
8	2.79	2.19	2.52	0.78	0.92	3.10	3.22	3.30	3.44	3.06	0.88	0.60	2.24
10	-1.74	-1.48	-0.99	-0.41	0.21	-0.21	-0.81	-0.03	-0.79	-0.97	-1.75	-2.85	-0.93
Noon.	-5.63	-5.43	-4.22	-1.87	-1.22	-2.82	-3.50	-4.23	-5.01	-7.10	-5.17	-5.46	-4.30
2	-7.93	-6.60	-6.96	-2.37	-2.54	-4.07	-5.43	-6.49	-5.99	-8.76	-7.72	-7.36	-6.02
4	-7.72	-6.70	-5.62	-2.52	-3.22	-3.88	-3.60	-5.96	-5.79	-8.35	-7.00	-7.51	-5.65
6	-5.63	-2.80	-2.79	-1.04	-1.30	-1.77	-1.50	-3.43	-3.88	-3.87	-5.02	-5.40	-3.20
8	-0.70	0.10	-0.25	0.03				-1.23			-	1	-0.65
10	1.99	2.39	1.42	1.18		100000000000000000000000000000000000000		-0.30			1000	2.64	1.30
Mean.	66.40	57.70	48.31	30.39	23.42	8.10	20.84	27.31	42,27	56.61	64.38	70.39	43.01

## NORTH AMERICA. - MONTREAL, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year.

Degrees of Fahrenheit.

Hour.	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	March.	April.	May.	June.	July.	Year.
A.M.1	5.03	4.92	2.53	1.16	0.88	1.43	1.61	4.38	3.12	4.85	4.55	5.07	3.30
3	5.99	5.20	3.61	1.58	1.79	1.30	2.72	5.18	5.14	6.51	5.10	6.80	4.25
5	6.44	5.43	4.45	2.08	2.21	1.87	3.95	6.84	6.54	6.56	6.30	7.76	5.05
7	2.10	3.47	3.61	2.01	2.08	1.98	5.22	7.07	3.84	3.56	4.72	3.04	3.56
9	-0.58	0.73	0.77	0.63	1.14	1.16	3.99	2.96	0.71	0.50	-0.02	0.22	1.02
11	-3.61	-2.20	-2.73	-1.35	-0.49	-1.08	-0.17	-2.51	-2.48	-2.79	-3.42	-3.21	-2.17
P.M.1	-6.61	-5.12	-5.41	-3.47	-2.38	-1.49	-4.80	-7.41	-4.93	-5.78	-5 97	-6.08	-4.95
3	-7.34	-6.65	-5.80	-3.22	-2.78	-2.36	-6.08	-9.03	-6.33	-6.46	-6.93	-8.01	-5.91
5	-5.47	-5.S3	-3.15	-1.19	-1.44	-0.63	-4.12	-6.48	-5.63	-6.62	-6.18	-6.53	-4.43
7	-1.45	-0.62	-1.00	-0.44	-0.70	-0.60	-1.23	-2.40	-2.93	-3.50	-3.17	-2.88	-1.74
9	1.58	1.32	0.32	0.13	-0.71	-0.66	-0.96	-0.75	0.44	0.61	1.58	1.17	0.34
11	3.10	3.02	2.47	1.48	0.22	0.61	0.24	1.78	2.06	2.52	3.55	3.39	2.02
Mean.	69.69	57.53	44.70	32.76	15.91	18.96	14.52	22,50	34.47	51.33	65.08	67.42	41.24

XI.

NORTH AMERICA. —SITKA. Lat. 57° 3' N. Long. 135° 18' W. Gr. — Dove.

Degrees of Reaumur.													
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.33	0.58	0.97	1.51	1.80	1.81	1.68	1.34	1.07	1.19	0.41	0.23	1.08
1	0.34	0.66	1.09	1.68	2.04	2.06	1.88	1.53	1.18	1.11	0.46	0.33	1.20
2	0.35	0.72	1.17	1.81	2.20	2.25	2.04	1.66	1.33	1.18	0.49	0.33	1.29
3	0.51	0.78	1.36	1.89	2.43	2.49	2.16	1.77	1.24	0.64	0.48	0.18	1.33
4	0.45	0.86	1.47	2.02	2.55	2.57	2.20	1.82	1.29	0.68	0.49	0.18	1.38
5	0.45	0.83	1.57	2.07	2.39	2.47	2.95	1.89	1.33	0.70	0.49	0.14	1.52
	0.45	0.84	1.56	1.89	1.76	1.77	1.67	1.62	1.33	0.78	0.46	0.18	1-26
6	0.43	0.82	1.37	1.13	0.96	1.08	0.96	1.02	1.05	0.78	0.40	0.10	
7	0.32	0.76	0.75	0.31	0.00	0.26		0.40		0.53	0.33	0.17	
9	0.39	0.49	The second second		-0.82	100 100 200	-0.58			0.12	0.23		-0.15
10	0.16	100000000000000000000000000000000000000	0.77	10/2/2005	-1.35	THE RESERVE	-1.27	-0.95			0.00	-0.11	THE RESIDENCE OF
11	-0.19	the second	-1.29		28/20 mai	-1.70	CO.	-1.57	-1.28	TO REAL PROPERTY.	-0.35	-0.11	
11	-0.15	-0.00	1.25	-1.00	1.75	-1.10	1.51	1.51	1.20	0	0.00	0.11	1.11
Noon.	-0.57	-1.05	-1.71	-2.13	-2.17	-2.11	-2.11	-2.04	-1.65	-1.14	-0.72	-0.32	-1.48
1	-0.83	-1.36	-1.74	-2.33	-2.35	-2.35	-2.25	-2.33	-1.56	-1.38	-0.84	-0.46	-1.65
2	-0.95	-1.44	-1.99	-2.28	-2.40	-2.42	-2.31	-2.16	-1.86	-1.42	-1.00	-0.50	-1.73
3	-0.95	-1.47	-1.94	-2.10	-2.28	-2.31	-2.13	-2.00	-1.72	-1.37	-0.94	-0.44	-1.64
4	-0.78	-1.20	-1.67	-1.91	-2.04	-2.09	-1.94			-1.13		-0.32	-1.43
5	-0.50	-0.85	-1.17	-1.63	-1.73	-1.76	-1.65	-1.43	-1.24	-0.88	-0.45	-0.20	-1.12
6	-0.25	-0.45	-0.82	_1 13	-1 37	-1.48	-1 26	_1 02	-0.61	-0.50	-0.21	-0.10	-0.77
7	-0.15	-0.10		The same of the sa		-1.00	THE RESERVE		-0.28	0.631300		-0.03	
8	-0.01	0.11	0.13	DV ICELIES	-0.23		-0.22	0.12	0.19	0.06	0.07	0.01	
9	0.15	0.30	0.44	0.70	0.48	0.27	0.33	0.66	0.52	0.21	0.22	0.12	0.37
10	0.23	0.37	0.64	1.07	1.02	0.97	0.99	0.96	0.76	0.30	0.29	0.19	0.65
11	0.31	0.48	0.84	STATE OF THE PARTY	1.57	1.46	A CONTRACTOR OF THE PARTY OF TH	1.19	0.90	0.95	0.43	0.22	0.93
						33 10 40			1000				
Mean.	-1.39	-1.07	0.55	3.51	6.21	9.10	10.24	10.28	7.96	5.26	2.52	1.73	

ARCTIC AMERICA. — BOOTHIA FELIX. Lat. 69° 59' N. Long. 92° 1' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Degrees of Reaumur.													
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
		terr				7 7	15 18	RE III				To and	7 000
Morn. 1	0.08	0.42	1.61	2.17	2.64	2.38	1.78	1.34	0.56	0.30	0.02	0.12	1.12
2	0.10	0.28	1.85	2.25	2.75	2.55	1.78	1.30	0.62	0.32	0.18	0.13	1.15
3	0.11	0.25	2.10	2.30	2.61	2.45	1.65	1.17	0.66	0.33	0.29	0.10	1,12
4	0.11	0.21	2.30	2.26	2.23	2.05	1.35	1.02	0.66	0.34	0.31	0.06	1.02
WENT IVE	传生物		250		E to				OF T	41.44			
5	0.10	0.22	2.38	2.02	1.76	1.39	0.99	0.86	0.56	0.32	0.24		0.87
6	0.10	0.26	2.23	1.53	1.02	0.65	0.61	0.70	0.46	0.27	A STATE OF	-0.04	The second
7	0.09	0.29	1.77	0.81	0.35	-0.04	0.26	0.50	0.27	0.17	30037772	-0.07	0.37
8	0.08	0.22	0.98	-0.06	-0.32	-0.58	-0.03	0.24	0.05	0.01	0.01	-0.10	0.04
	0.00	0.00	0.00	0.00	0.05	0.00	0.98	0.10	0.10	0.00	0.04	0.10	0.00
9	0.06	100000000000000000000000000000000000000							Production 1		0011	-0.10	
10			-1.22				14,700 4,550		100000	ALCOHOL: A P.		-0.10	1/2-1/2
11	1								1			-0.11	2
Noon	-0.05	-0.87	-3.05	-2.86	-2.46	-2.02	-1.43	-1.16	-0.82	-0.69	-0.32	-0.12	-1.32
1	-0.11	-1.02	-3.38	-3.03	-2.66	-2.33	-1.70	-1.34	-0.93	-0.68	-0.30	-0.14	-1.47
2			-3.26			57.00		-1.38				-0.13	
3		-0.78	-2.78		-	To the state of th	The state of the s	-1.32					- MI 100
4	A	-0.46					A STATE OF THE PARTY OF THE PAR	-1.18	Carried Street			-0.05	100
*	-0.14	-0.40	4.00	-2.10	-1.30	-1.30	-1.50	-1.10	-0.00	-0.10	0.00	0.00	1.00
5	-0.11	-0.14	-1.29	-1.50	-1.45	-1.36	-1.18	-1.01	-0.44	0.01	0.24	0.01	-0.69
6	-0.09	0.13	-0.57			100		-0.78		0.14	0.31	1000	-0.34
7	-0.06	0.32	0.01	0.06		-0.01		-0.50		0.22	0.36		-0.01
8	-0.05	0.43	0.44	0.78	0.20			-0.16		0.25	0.38	0.11	0.27
inter the later		0110		00	0.20	0.01	0.01	0.10	0	0.20	0.00		
9	-0.03	0.50	0.76	1.35	0.74	0.92	0.50	0.24	0.38	0.26	0.38	0.10	0.51
10	-0.02	0.51	0.99	1.74	1.28	1.26	0.90	0.66	0.44	0.26	0.35	0.10	0.71
11	0.02	0.52	1.19	1.95	1.82	1.63	1.20	1.01	0.48	0.26	0.28	0.09	0 37
Midn	0.05	0.49	1.38	2.08	2.30	2.04	1.59	1.25	0.51	0.28	0.15	0.12	1.02
	100.0	250	Corne	101	- Con	7.27	To all	90 Pg	3	86 1	Sept.	09.0	
	(Electrical Property of the Control	180	1104	L.C.	3 500		8) 14	0.0	131_1	\$ W. W	200	10.00	A CANA
6. 6	0.01	0.20	0.83	0.40			-0.09		0.15	0.21	0.09	O SHANE	0.15
7. 7	0.02	0.31	0.89	0.44		The second second	-0.04	-0.00	0.18	0.20	0.17	0.02	0.18
8.8	0.02	0.33	0.71		-0.06		0.02	0.04	0.16	0.13	0.20	0.01	0.16
9. 9	0.02	0.28	0.35	0.19	-0.11	-0.04	0.07	0.07	0.13	0.03	0.17	The second second	0.10
10.10	-0.00	0.13	-0.12	-0.04	-0.13	-0.04	0.10	0.09	0.01	-0.08	0.11	-0.00	0.00
7. 2. 9	-0.03	-0.06	-0.24	_0 0**	0 50	_0 =0	_0 2**	0.07	-0.10	-0.05	0.00	-0.03	-0.20
6. 2. 8								-0.21 -0.28				-0.03	100
6. 2.10		-0.10	-0.20									-0.02	
6. 2. 6		-0.20						-0.01				1	
	0.04	0.20	0.00	0.12	U.04	-0.53	-0.08	-0.49	-0.22	-0.05	-0.00	-0.03	0.09
7. 2	-0.03	-0.35	-0.75	-1.08	-1.15	-1.26	-0.80	-0.44	-0.34	-0.20	-0.11	-0.10	-0.55
8. 2	-0.03	-0.38	-1.14	-1.51	-1.49	-1.53	-0.95	-0.57	-0.45	-0.28	-0.09	-0.12	-0.71
8. 1	-0.02	-0.40	-1.20	-1.55	-1.49	-1.46	-0.87	-0.55	-0.44	-0.34	-0.15	-0.12	-0.72
7. 1	-0.01											-0.11	
0.10.00	30.6	1980	LAWRIG	40000	1	12 120	100		14	R RES	W-15- F	400	
9.12.3.9	-0.04	110000	1.000	-1.29	-1.27	-1.12	-0.77	-0.59	-0.37	-0.25	-0.01	-0.06	-0.61
7. 2.2(9)	-0.03	0.08	0.01	0.14	-0.21	-0.17	-0.15	-0.10	0.02	0.03	0.14	-0.00	-0.02
Dail.ext.	-0.09	-0 25	-0.50	0.00	0.0-	0.04	00.	0.00	0.7.	0.10	0.00	0.03	0.70
Dan. CAL.	0.02	0.20	0.50	-0.37	0.05	0.04	-0.04	-0.02	-0.14	-0.18	0.03	-0.01	-0.16

## N. AMERICA. - LAKE ATHABASCA. Lat. 59° N. Long. 111° W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Lefroy.

The corrections for April and May are derived from observations made at Fort Simpson, Lat. 620 N.

Degrees of Fahrenheit.

Hour.	April.	May.	October.	November.	December.	January.	February.
daily ext.	1.58	1.71	0.33	0.25	-0.17	0.77	1.19
6, 6	1.15	0.51	1.07	0.59	0.27	0.84	1.19
7,7	1.50	- 0.16	0.76	0.54	0.30	0.58	1.31
8,8	. 1.72	0.18	0.69	0.55	0.62	0.95	1.27
9, 9	0.54	0.30	0.37	0.32	0.84	0.80	0.78
10, 10	-0.43	-0.08	-0.32	-0.06	0.34	0.12	0.31
11, 11	-1.68	-1.20	-0.57	-0.37	0.10	-0.62	-0.23
6, 2, 10	0.47	0.46	-0.31	-0.21	-0.22	-0.17	-0.05
7, 3, 11	0.46	0.59	-0.40	-0.16	0 17	0.06	-0.26
Mean.	32.48	44.56	21.44	9.76	0.40	-23.00	4.79

### XIV.

Arctic America. — Melville Island. Lat. 74° 47' N. Long. 110° 48' W. Gr. — Dove.

Degrees of Reaumur.

Hour.	January.	February.	March.	October.	Hour.	November.	December
A.M. 1	0.12	0.10	1.04	0.04	A.M. 2	-0.12	-0.09
3	0.18	0.05	1.22	0.12	4	-0.02	-0.06
5	0.07	0.25	0.90	0.24	6	0.00	0.11
7	0.11	0.29	0.57	0.20	8	-0.22	0.07
9	-0.13	-0.24	0.29	-0.15	10	-0.38	0.11
11	-0.35	-0.43	-1.33	-0.46	12	-0.41	0.24
P.M. 1	-0.22	-0.65	-1.72	-0.43	P.M. 2	-0.27	0.14
3	-0.25	-0.52	-1.00	0.22	4	0.16	0.00
5	0.04	0.04	-0.43	-0.24	6	0.27	-0.12
7	0.04	0.24	0.06	-0.10	8	0.38	-0.26
9	0.11	0.35	0.33	0.11	10	0.36	-0.12
11	0.40	0.49	0.66	0.43	12	0.25	0.00
Mean.	-29.75	-27.58	-22.73	-14.32	Mean.	-18.65	-25.75

#### XV.

Spitzbergen. — Hecla Cove. Lat. 79° 55' N. Long. 16° 49' E. Gr. — Dove.

Degrees of Reaumur.

Hour.	June.	July.	August.	Hour.	June.	July.	August.
A.M. 1	0.63	0.62	0.42	P.M. 1	-0.67	-0.67	-0.63
3	0.43	0.84	0.54	3	-0.58	-0.42	-0.58
5	0.26	0.51	0.53	5	-0.27	-0.44	-0.32
7	-0.12	-0.02	0.25	7	0.26	-0.17	-0.06
9	-0.29	-0.09	-0.09	9	0.21	0.06	0.14
11	-0.47	-0.49	-0.45	11	0.61	0.26	0.24
	52.9 15.0	Temps with	100	Mean.	1.71	3.63	2.84

S. America. - Rio Janeiro. Lat. 22° 54' S. Long. 43° 16' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove. Degrees of Fahrenheit.

	Tales	SILOUS	11-11-10		Degre	es of Fa	hrenhei			may 10			
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
				THE			1000						HITTON Y
Morn. 1	0.74	1.51	1.80	0.90	1.13			1.31	1.04	0.97	1.76	1.31	1.24
2	1.64	2.41	2.48	1.64	2.12	1.53	1	2.00	1.69	1.64	2.32	2.05	2.03
3	2.50	3.11	3.02	2.32	2.93	2.43	3.47	2.66	2.27	2.21	2.75	2.66	2.70
4	3.08	3.90	3.24	2.79	3.38	3.04	3.87	3.04	2.59	2.50	2.93	2.99	3.06
5	3.22	3.29	3.15	2.90	3.40	3.29	3.83	3.08	2.66	2.52	2 79	2.99	3.08
6	2.93	2.84	2.75	2.75	3.40	3.20	3.47	2.79	2.41	2.27	2.32	2.68	
7	2.30	2.21	2.13	2.30	2.48	2.84	2.70	2.25	2.00	1.82	1.67	2.12	2.23
8	1.49	1.49	1.40	1.71	1.85	2.39	1.96	1.60	1.46	1.28	0.90	1.40	1.58
	1.20	1.20	1.40		1.00	2.00	1.00	2.00			0.00	1.10	2.00
9	0.68	0.72	0.59	1.04	1.15	1.82	1.15	0.90	0.86	0.68	0.14	0.59	0.86
10	-0.07	-0.05	-0.23	0.32	0.50	1.13	0.32	0.23	0.18	0.05	-0.56	-0.23	-0.14
11	-0.77	-0.86	-1.01	-0.45	-0.23	0.32	-0.50	-0.50	-0.54	-0.59	-1.22	-1.04	-0.61
Noon	-1.40	-1.64	-1.71	-1.22	-0.99	-0.65	-1.31	-1.19	-1.26	-1.22	-1.80	-1.82	-1.35
200	0.00	0.00	0.00	10.		7 00	0.10	10-	1.00	7	0.00	0.40	0.00
1		-2.30			-1.71	-1.67		-1.91					
2	-2.41		-2.66			-2.48		-2.48				-2.81 $-2.86$	
3 4	-2.59		-2.84	-2.66		-2.99		-2.84 $-2.93$		-2.27			700
4	-2.45	-2.70	-2.77	-2.57	-2.75	-3.04	-3.00	-2.93	-2.50	-2.12	-2.00	-2.09	-2.70
5	-2 05	-2.30	-2.50	-2.21	-2.54	-2.75	-3.47	-2.68	-2.00	-1.78	-2.25	-2.09	-2.39
6		-1.82			40.00		110000000	-2.23				-1.49	
7		-1.40				7		-1.67		7,223	-1.08	The same of	
8	-0.72		-1.22			-1.42		-1.13					
LANCE TO S	1924	100	ng i		77		g. o		0,000	1	i Sherry		1
9	-0.59		-0.77	-0.72	-1.44	-1.26	-1.22	-0.70	-0.61	-0.61	-0.14	-0.38	-0.79
0	-0.56		-0.25		-1.13		-0.59		-0.41			-0.16	-0.50
11	-0.41		0.36		-0.63		0.09		-0.09		0.65	0.14	0.09
Midn	0.00	0.59	1.06	0.23	0.14	-0.29	0.92	0.61	0.38	0.32	1.15	0.65	0.47
					Total Control		45.00			4 3	1		enii exe
6. 6	0.72	0.52	0.32	0.50	0.43	0.50	0.30	0.29	0.43	0.45	0.34	0.61	0.45
7. 7	0.63	0.41	0.25	0.52	0.29	0.54	0.16	0.29	0.45	0.41	0.29	0.56	0.41
8. 8	0.38	0.18	0.09	0.38	0.09	0.50	0.07	0.25	0.32	0.27	0.16	0.41	0.25
9. 9	0.05	-0.11	-0.09	-0.16	-0.16	0.29	-0.05	0.11	0.14	0.05	0.00	0.11	0.05
10.10	-0.00	0.00	0.00	0		0.00	0 -			0.00	0.10	0.00	0.70
10.10 7. 2. 9		-0.34						-0.05			-0.18		The second second
6. 2. 8						2007	3	-0.32	THE STREET	14.4	117.111.111.111.11	334-1305	The same of the sa
6. 2.10		-0.34 -0.18				715	-0.43	4.79		110000	-0.32 $-0.05$	-0.25	
0. 2.10	0.02	-0.18	-0.05	-0.07	-0.11	-0.14	0.00	0.00	-0.11	-0.11	-0.03	-0.09	-0.07
6. 2. 6	-0.34	-0.59	-0.68	-0.47	-0.47	-0.50	-0.81	-0.63	-0.50	-0.43	-0.68	-0.54	-0.56
7. 2		-0.27			0.09			-0.11					
8. 2	-0.47	-0.63	-0.63		-0.23	STATE OF THE PARTY		-0.45	985797 / 5	100000000000000000000000000000000000000	-0.88	1100	The second second
8. 1	-0.27	-0.41	-0.45	-0.11	0.07			-0.16			-0.72	-0.52	-0.23
7 1				AL	E. C.		11/2	116-11	tore :				52,000
7. 1 9.12.3.9	0.16	-0.05	-0.09	0.18	0.38	100000	-0.27	0.18	0.07	291	-0.34	9	15550000000
7. 2.2(9)	-0.97	-1.19	-1.19	- H- SC-00	Security Co.	11425	-1.19	0.000	. 101	CT10000	7 VOR 2 VOR		1200
1. 2.2(3)	0.32	-0.61	-0.52	-0.38	-0.68	-0.54	-0.65	-0.41	-0.38	-0.38	-0.32	-0.36	-0.47
Dail. ext.	0.32	0.27	0.20	0.14	0.34	0.14	0.14	0.09	0.09	0.14	0.07	0.07	0.16
						12/15/20							

### XVII.

S. AMERICA. - RIO JANEIRO. Lat. 22° 54' S. Long. 43° 16' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.33	0.67	0.80	0.40	0.50	0.25	0.82	0.58	0.46	0.43	0.78	0.58	0.55
2	0.73	1.07	1.10	0.73	0.94	0.68	1.22	0.89	0.75	0.73	1.03	0.91	0.90
3	1.11	1.38	-1.34	1.03	1.30	1.08	1.54	1.18	1 01	0.98	1.22	1.18	1.20
4	1.37	1.51	1.44	1.24	1.50	1.35	1.72	1.35	1.15	1.11	1.30	1.33	1.36
19 W. L.		Y F	90	Kan .	14.3	10.5	10.00	100					7.00
5	1.43	1.46	1.40	1.29	1.51	1.46	1.70	1.37	1.18	1.12	1.24	1.33	1.37
6	1.30	1.26	1.22	1.22	1.36	1.42	1.54	1.24	1.07	100000000000000000000000000000000000000	1.03		1.24
7	1.02	0.98	0.95	1.02	1.10	1.26	1.20	1.00	0.89	0.81	0.74	0.94	
8	0.66	0.66	0.62	0.76	0.82	1.06	0.87	0.71	0.65	0.57	0.40	0.62	0.70
9	0.30	0.32	0.26	0.46	0.51	0.81	0.51	0.40	0.38	0.30	0.06	0.26	0.38
10	-0.03		-0.10	0.14	0.22	0.50	0.14	0.10	0.08		-0.25	SAN CO.	0.06
11	-0.34		100	-0.20	WEST TO THE	0.14	-0.22	-0.22	DINTE		-0.54		-0.27
Noon		-0.73	WW 237 W	WITH TOWN	(SC23) 49-111	-0.29		-0.53		CTLASTO O	-0.80	-0.81	-0.60
							M.J.	70.4	1 5			1	
1		100		1 W 1		-0.74							
2				7711 12 14	The second second	-1.10					122 200	CIDE.	
3	The state of the s	Carlo Contract		711	The second second	-1.33				•	Carlotte Control		
4	-1.09	-1.20	-1.23	-1.14	-1.22	-1.35	-1.60	-1.30	-1.05	-0.94	-1.18	-1.15	-1.20
5	0.01	-1.09	1 11	0.00	1 10	-1.22	1 54	1 10	0.00	0.70	_1 00	_0 02	_1 06
6						-0.99							
7						-0.33							
8						-0.63							
		-0.00	-0.04	-0.42	-0.14	-0.05	-0.02	-0.50	-0.07	0.01	0.20	0.2.	0.40
9	-0.26	-0.41	-0.34	-0.32	-0.64	-0.56	-0.54	-0.31	-0.27	-0.27	-0.06	-0.17	-0.35
10						-0.50					0.10	-0.07	-0.22
11	-0.18	-0.06	0.16	-0.11	-0.28	-0.38	0.04	-0.04	-0.04	-0.07	0.29	0.06	-0.04
Midn	0.00	0.26	0.47	0.10	0.06	-0.13	0.41	0.27	0.17	0.14	0.51	0.29	0.21
			100	05.00	ELY.			NOTE OF					
6. 6	0.32	0.23	0.14	0.22	0.19	0.22	0.10	0.13	0.19	0.20	0.15	0 27	0.20
7. 7	0.28	0.18	0.11	0.23	0.13	0.24	0.07	0.13	0.20	0.18	0.13	0.25	0.18
8. 8	0.17	0.08	0.04	0.17	0.04	0.22	0.03	0.11	0.14	0.12	0.07	0.18	0.11
9. 9	0.02	-0.05	-0.04	0.07	-0.07	0.13	-0.02	0.05	0.06	0.02	-0.00	0.05	0.02
10.10	-0.14	-0.15	-0.11	-0.05	-0.14	-0.00	-0.06	-0.02	-0.05	-0.09	-0.08	-0.09	-0.08
		2		TRY DE	STATE OF	107: EV.		100		0.7	0.7-	0.11	0.70
7. 2. 9						-0.13							
6. 2. 8	The second second	200700		1 2 2 2 2 2	The State of the S	-0.10	PERSONAL PROPERTY.	2.0000000000000000000000000000000000000	THE RESERVE	TO ALL WATER	The state of the s	41 (41 (41)	P 525 F 56 B
6. 2.10				20.00	THE R. P. LEWIS CO., LANSING, MICH. 49-14	-0.06		A COLUMN	PT 6 S S NO. 7	THE RESERVE OF	ALCOHOL: N	0.079	
6. 2. 6	-0.10	-0.20	-0.30	-0.21	-0.21	-0.22	-0.30	-0.23	0.22	-0.19	-0.50	U.24	0.20
7. 2	-0.03	-0.12	-0.12	-0.03	0.04	0.08	-0.04	-0.05	-0.08	-0.08	-0.22	-0.16	-0.07
8. 2		1300,37000	10.00	STATE OF THE PARTY.	THE REST OF	-0.02	30 CL 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	100 Day 100 W	401 311	1133611	CO 17 T.2.7	200 7 7 75 7	
8. 1			-0.20	100000000000000000000000000000000000000	0.03	Thereon Co	-0.05			-0.11	The second second	11111	
7. 1		THE REAL PROPERTY.	-0.04		0.17	0.26	0.12	0.08	5333336	9-0-2-12-2	-0.15	THE WAR	0.05
			Page 12	ET		6 25		1373	Aleos lo	Temelo	PO SO	No.	154
9.12.3.9		Carlotte Co.	The state of the s	The second second	1.1202778636.0	-0.34	200	The second second	S	100000000000000000000000000000000000000	The State of State of	ALC: A COLOR OF THE PARTY OF TH	and the second
7. 2.2(9)	-0.14	-0.27	-0.23	-0.17	-0.30	-0.24	-0.29	-0.18	-0.17	-0.17	-0.14	-0.16	-0.21
Dail.ext.	0.14	0.12	0.09	0.06	0.15	0.06	0.06	0.04	0.04	0.06	0.03	0.03	0.07

N. AMERICA. — AMHERST COLLEGE. — Lat. 42° 22' N. Long. 72° 30' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dewey.

Degrees of Fahrenheit.

MARKE THE	O TOWN	No. of the	A	S. J. S. G.				rable.	TOTAL !	million of	4.	-1000	
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Morn. 1	3.90	2.78	4.73	6.23	5.51	6.64	6.39	5.14	5.36	4.87	2.34	1.63	4.68
2	4.24	3.03	4.81	6.69	6.48	7.28	6.83	5.66	6.12	5.65	2.99	2.20	5.16
3	4.13	3.20	5.36	7.42	7.41	7.92	7.28	6.03	6.92	6.46	3.49	2.55	5.68
4	4.50	3.94	5.69	7.85	7.88	8.04	7.42	6.29	6.56	7.09	3.72	2.70	6.0
The same	1183			- Y	-KCUP	Mind.	TELT .	Marie 1	2011	unt :	BUT TO	3	1.
5	4.72	4.20	6.04	8.12	8.18	7.80	7.54	6.66	7.88	7.72	4.03	3.32	6.3
6	4.68	4.78	6.12	7.77	6.77	5.96	6.02	5.81	7.44	7.65	4.34	3.78	5.9
7	4.75	4.78	4.62	5.97	4.22	4.20	3.80	4.48	5.32	6.87	4.28	3.97	4.7
8	3.83	3.78	2.08	3.04	1.62	1.40	1.09	1.96	2.52	4.31	2.68	4.13	2.7
activity for	-			-	54.5		-0.30	10		0.0	1		
9	1.46	1.45	-0.46	0.08	-0.60	-0.88	-0.87	-0.93	-0.56	0.83	0.34	2.40	0.1
10	-1.26	-0.85	-2.57	- 2.69	-1.12	-3.12	-3.80	-3.04	-3.32	-2.24	-1.43	-0.55	-2.3
11	-4.10	-2.72	-4.77	- 5.65	-5.12	-5.68	-6.43	-5.45	-6.04	-5.02	-3.01	-2.76	-4.7
Noon.	-6.32	-4.26	-6.38	- 7.92	-6.75	-8.08	-8.50	-6.86	-8.16	-7.06	-5.01	-4.30	-6.6
27.12-152	-11	1991	- 104	- of 1-	Hi.los	TIVE-	97, 5-	10.11-	Bit-	DH-	0.1-1	8 - 4	ve la
1	-7.46	-5.35	-7.65	- 9.46	-8.15	-9.36	-8.83	-8.23	-9.12	-8.24	-6.12	-6.14	-7.8
2	-7.80	-6.06	-8.34	-10.42	-8.75	-9.00	-9.50	-7.86	-9.80	-9.28	-5.97	-6.30	-8.2
3	-7.32	-5.80	-8.11	- 9.81	-8.27	-8.60	-7.50	-7.67	-9.20	-9.24	-5.28	-5.60	-7.7
4	-5.84	-4.89	-7.23	- 8.61	-7.86	-7.84	-7.17	-6.23	-8.40	-8.24	-3.85	-3.76	-6.6
Service Process						ALC: STATE	an n				125-3	1	
5	-3.32	-3.10	-5.65	- 7.04	-5.97	-6.00	-5.83	-5.26	-6.44	-5.65	-2.28	-2.03	-4.8
6	-2.06	-1.18	-3.46	-4.50	-4.08	-4.20	-4.17	-2.82	-3.52	-3.50	-0.85	-0.68	-2.9
7	0.24	-1.05	0.17	- 1.69	-2.38	-1.92	-1.54	-1.44	-1.47	-1.24	-0.64	-0.31	-1.1
8	0.64	-0.43	0.93	0.27	-0.19	0.04	0.98	0.33	0.11	0.13	0.08	0.20	0.2
HER PARK	Liesa	Tribal	- 1000	- eun-	(420	Miller	AUGUS.				MAY .	THE STATE OF	
9	1.50	0.28	1.89	1.77	1.66	1.96	3.05	1.59	1.99	1.16	0.80	0.69	1.5
10	2.01	0.57	3.29	3.31	2.73	3.20	3.79	3.02	3.53	1.90	1.16	1.20	2.4
11	2.42	1.19	4.29	4.23	3.99	4.20	4.24	3.79	4.61	3.24	1.96	1.58	3.3
Midnight.	2.50	1.70	4.85	4.92	4.75	5.48	5.31	4.52	5.34	4.09	2.40	1.98	3.9
2020	0.05	0.00	0.00	0.75	0.00	0.70			1	1			
3, 9, 3, 9	-0.05	-0.22	-0.08	- 0.13	0.05	0.10	0.49	0.26	-0.21	-0.20	-0.16	-0.01	-0.0
9, 9	1.48 0.38	0.87	0.72	0.93	0.53	0.54	1.09	0.33	0.72	1.00	0.57	1.55	0.80
7, 2, 9	-0.48	-0.14	0.36	0.31	0.81	0.04	0.00	-0.51	0.11	-0.17	-0.13	0.33	0.12
,, 4, 3	0.40	-0.33	-0.61	- 0.89	-0.96	-0.95	-0.88	-0.60	-0.83	-0.42	-0.29	-0.55	-0.65
6, 2, 10	-0.37	-0.24	0.90	0.04	0.05	0.05	0.10	0.00	0.00	0.00	0.10	0.4	0.00
APPLICATION OF THE PARTY.	OF THE PERSON NAMED IN	-0.24	0.36	- 0.24	0.25	0.05	0.10	0.32	0.39	0.09	-0.16	-0.44	0.01
A STATE OF THE PARTY OF THE PAR	C-244	-0.03	0.19	- 0.38	-0.60	-0.53	-0.64	-0.12	-0.32	-0.17	-0.18	-0.38	-0.32
69041	-0.09	0.03	0.19	- 0.07	-0.18	-0.20	-0.49	0.14	0.04	0.28	0.09	-0.25	-0.07
7,2,2,(9)	heart State of	-0.18	0.13	0.00 - 0.23	-0.12	-0.13	-0.08	0.20	0.11	0.07	0.13	0.17	0.03
				- 0.23	-0.30	-0.22	0.10	-0.05	-0.12	-0.02	-0.02	-0.24	-0.11
Mean.	22.94	28.57	34.81	48.54	56.92	61.60	71.61	67.41	59.80	50.46	34.80	29.28	47.23
120 138.	- 25.	- 19,0	T 155,0	Ulder (1)	20,0	2,00		3,,44	30.00	30.40	34.00		2,,20

The numbers without sign must be added; those with the sign — must be subtracted.

The above Table has been derived from one year of hourly observations made at Amherst College, Massachusetts, in 1839, under the direction of Professor Snell, and communicated by Professor Chester Dewey. It gives the simple differences of the monthly means of each hour from the monthly means of the twenty-four hours which are found in the last line.

# HOURLY CORRECTIONS

FOR

# PERIODIC VARIATIONS.

ASIA.

the last last the that the street of the following street erania. Nel como en la como en 2 de 1900 de La como en the transition was not a long to the same of the same to be substituted by the 

### XVIII.

India. — Trevandrum. Lat. 8° 31' N. Long. 74° 50' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fabrenheit.

Hours. Jan. Feb. March. April. May. June. July. Oct. Dec. Aug. Sept. Nov. Mean. Morn. 1 4.03 4.41 3.80 3.85 3.26 2.66 2.88 2.99 3.06 3.33 2.41 4.25 3.42 5.13 4.95 4.64 4.46 3.80 3.02 3.24 3.44 3.83 2.75 3.44 4.86 3.96 6.03 3 6.12 5.67 5.15 4.39 3.47 3.17 3.74 3.98 3.92 4.46 5.67 4.66 4 6.95 7.31 6.64 5.74 3.80 3.58 5.04 4.82 4.21 4.48 4.34 6.50 5.29 5 7.56 8.15 7.13 5.81 4.82 3.83 3.76 4.41 4.61 4.46 5.22 6.93 5.56 6 7.34 8.01 6.73 5.11 4.14 3.35 3.49 4.07 4.14 4.01 4.73 6.57 5.15 7 6.01 6.59 5.20 3.53 2.81 2.34 3.06 3.02 2.68 2.88 3.40 5.11 3.89 8 3.56 3.92 2.66 1.22 0.95 0.90 1.35 1.26 1.13 2.70 1.49 1.40 1.87 0.41 0.50 -0.47 -1.42 -1.13 -0.74 -0.27 -0.45 -0.81-0.99 -0.92 -0.29 -0.5410 -2.84 -2.97 -3.53 -3.89 -3.04 -2.30 -1.91 -2.41 -2.86 -3.06 -3.11 -3.24 -2.9311 -5.51 -5.85 -5.94 -5.76 -4.48 -3.53 -3.33 -4.05 -4.50 -4.73 -4.75 -5.58 -4.84Noon. . . -7.25 -7.58 -7.36 -6.82 -5.33 -4.34 -4.32 -5.18 -5.54 -5.72 -5.67 -7.00 -6.011 -7.92 - 8.17 - 7.72 - 7.04 - 5.60 - 4.68 - 4.79 - 5.69 - 5.87 - 5.94 - 5.90 - 7.49 - 6.412 -7.76 -7.83 -7.22 -6.59 -5.38 -4.61 -4.77 -5.60 -5.60 -5.54 -5.60 -7.25 -6.143 -7.09 -6.98 -6.26 -5.65 -4.79 -4.19 -4.30 -5.04 -4.86 -4.66 -4.95 -6.57 -5.454 -6.17 -5.99 -5.06 -4.46 -3.94 -3.47 -3.51 -4.10 -3.80 -3.53 -4.12 -5.67 -4.485 -5.15 |-4.88 |-3.83 |-3.11 |-2.88 |-2.52 |-2.52 |-2.90 |-2.59 |-2.32 |-3.15 |-4.61 |-8.386  $-3.92 \begin{vmatrix} -3.74 \end{vmatrix} -2.57 \begin{vmatrix} -1.71 \end{vmatrix} -1.69 \begin{vmatrix} -1.42 \end{vmatrix} -1.40 \begin{vmatrix} -1.58 \end{vmatrix} -1.31$ -1.10 -2.03 -3.35 -2.167 -2.50 -2.45 -1.31 -0.34 -0.50 -0.32 -0.29 -0.27-0.110.00 -0.81 -1.89 -0.908 -0.92 | -1.04 | -0.070.92 0.63 0.70 0.68 0.90 0.92 0.97 0.38 - 0.320.32 9 1.71 0.68 0.38 1.06 1.91 1.53 1.46 1.40 1.76 1.69 1.42 1.19 1.35 10 2.05 1.64 1.96 2.61 2.16 1.96 1.85 2.30 2.18 2.25 2.21 2.43 2.14 3.08 2.57 2.63 3.06 2.57 2.23 2.09 2.54 2.48 2.57 2.68 3.26 2.66 Midn. . . 3.83 3.31 3.17 3.42 2.88 2.41 2.23 2.68 2.70 2.81 2.99 3.80 3.02 6. 6 2.09 1.71 2.14 1.71 1.24 0.97 1.04 1.24 1.42 1.46 1.35 1.60 1.51 7. 7 1.76 2.07 1.96 1.60 1.17 1.01 1.19 1.40 1.44 1.44 1.28 1.62 1.49 8. 8 1.33 1.44 1.31 1.06 0.79 0.79 1.01 1.19 1.08 1.06 0.88 1.19 1.10 9. 9 0.54 0.43 0.29 0.25 0.20 0.36 0.56 0.65 0.43 0.36 0.25 10.10 -0.41 -0.65 | -0.79-0.63 -0.45 -0.18 | -0.02 | -0.07 |-0.34 | -0.41-0.45-0.40 -0.41 7. 2. 9 -0.36 |-0.29| |-0.32| |-0.38| |-0.34| |-0.27| |-0.23| |-0.27| |-0.29| |-0.32| |-0.27| |-0.32| |-0.32|6. 2. 8 -0.45 -0.29 -0.18 -0.18 -0.20 -0.18 -0.20 -0.20 -0.18 -0.18 -0.16 -0.34 -0.236. 2.10 0.50 0.38 0.32 0.23 0.18 0.25 0.25 0.25 0.45 6. 2. 6 -1.44 | -1.19 | -1.01 | -1.06 | -0.97 | -0.90 | -0.90 | -1.04 | -0.92 | -0.88 | -0.97 | -1.35 | -1.06 | -0.97 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.90 | -0.97. 2 -0.88 |-0.63| |-1.01| |-1.53| |-1.28| |-1.15| |-1.06| |-1.28| |-1.31| |-1.33| |-1.10| |-1.08| |-1.13|8. 2 -2.12 - 1.96 - 2.30 - 2.70 - 2.23 - 1.87 - 1.71 - 2.07 - 2.18 - 2.21 - 2.12 - 2.27 - 2.148. 1 -2.18 -2.14 -2.54 -2.93 -2.34 -1.89 -1.73 -2.12 -2.32 -2.41 -2.25 -2.41 -2.277. 1 -0.97 -0.79 -1.26 -1.76 -1.40 -1.17 -1.06 -1.33 -1.44 -1.53 -1.26 -1.19 -1.269.12.3.9 -3.31 -3.42 -3.26 -2.99 -2.43 -1.96 -1.87 -2.23 -2.39-2.41-2.54-3.17 - 2.667. 2.2(9) -0.11 | -0.110.02 0.20 0.14 0.16 0.18 0.25 0.20 0.07 0.11 0.20 0.16

The numbers without sign must be added; those with the sign - must be subtracted.

### XIX.

## India. — Trevandrum. Lat. 8° 31' N. Long. 74° 50' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Lie III San					Degre	es of R	eaumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.96			1		1						1.89	1.52
2	2.28	12000						1000	1.53		1000000	2.16	1.76
3	2.68		2.52		The same of	10000	1 22 - 0	1 -0 -0	1.77	1.74		2.52	2.07
4	3.09	3.25	2.95	2.55	2.14	1.69	1.59	1.87	1.50	1.90	2.24	2.89	2.35
5	3.36	3.62	3.17	2.58	2.14	1.70	1.67	1.96	2.05	1.98	2.32	3.08	2.47
6	3.26	3.56	2.99	2.27	1.85	1.49	1.55	1.81	1.84	1.78	2.10	2.92	2.29
7	2.67	2.93	2.31	1.57	1.25	1.04	1.19	1.36	1.34	1.28	1.51	2.27	1.73
8	1.58	1.74	1.18	0.54	0.42	0.40	0.60	0.66	0.56	0.50	0.62	1.20	0.83
9	0.18	0.22	-0.21	-0.63	-0.50	-0.33	-0.12	-0.20	-0.36	-0.44	-0.41	-0.13	-0.24
10	-1.26		100	-1.73				-1.07		-1.36	1000000	-1.44	-1.30
11	-2.45				1		1300000	-1.80		200		-2.48	-2.15
Noon	-3.22	100000		-3.03			-1.92	250 1.000		1000	LANDY	-3.11	-2.67
					J. San			1 2 2	. Anna		THE STATE OF		H
1	-3.52		-3.43	1.55	-2.49	1000	-2.13			and the same of	-2.62		-2.85
2	1	-3.48		1.100	-2.39	- 130	-2.12	-111511		SECTION SECTION		-3.22	-2.73
3		-3.10	-2.78	-2.51	- 1005		-1.91	-7719610	- 1000	CATHOLIS CO.		-2.92	-2.42
4	-2.74	-2.66	-2.25	-1.98	-1.75	-1.54	-1.50	-1.82	-1.09	-1.57	-1.83	-2.52	-1.99
5	-2.28	-2.17	-1.70	-1.38	-1.28	-1.12	-1.12	-1.29	-1.15	-1.03	-1.40	-2.05	-1.50
6	-1.74	-1.66	-1.14	-0.76	-0.75	-0.63	-0.62	-0.70	-0.58	-0.49	-0.90	-1.49	-0.96
7	-1.11	-1.09	-0.58	-0.15	-0.22	-0.14	-0.13	-0.12	-0.05	0.00	-0.36	-0.84	-0.40
8	-0.41	-0.46	-0.03	0.41	0.28	0.31	0.30	0.40	0.41	0.43	0.17	-0.14	0.14
9	0.30	0.17	0.47	0.85	0.68	0.65	0.62	0.70	0.75	0.76	0.63	0.53	0.60
10	0.91	0.17	0.47	1.16	0.96	0.87	0.82	1.02	0.75	1.00	0.03	1.08	0.95
11	1.37	1.14	1.17	1.36	1.14	0.99	0.93	1.13	1.10	1.14	1.19	1.45	1.18
Midn	1.70	1.47	1.41	1.52	1.28	1.07	0.99	1.19	1.20	1.25	1.33	1.69	1.34
and wa	SUIT	180	17,15	Palas				24.2	AT.	1	1		11177
	0	2 2 -	4			Turne		4					
6. 6	0.76	0.95	0.93	0.76	0.55	0.43	0.46	0.55	0.63	0.65	0.60	0.71	0.67
8.8	0.78	0 92 0.64	0.87	0.71	0.52	0.45	0.53	0.62	0.64	0.64	0.57	0.72	0.66
9. 9	0.24	0.19	0.38	0.47	0.09	0.35	0.45	0.53	0.48	0.47	0.39	0.33	0.49
10.10	-0.18		-0.35	-0.28	-0.20	-0.08	-0.01	-0.03	-0.15	-0.18	-0.20	-0.18	-0.18
ing a had	TIL SL		0.00	0.20			0.02	0.00	0.10	0.20	0.20		10.2
7. 2. 9	1	-0.13	Section 1	-0.17	-0.15	-0.12	-0.10	-0.12	-0.13	-0.14	-0.12	-0.14	-0.14
6. 2. 8	-0.20			-0.08	100	2 0 0	-0.09	-0.09	7-200-1	-0.08	-0.07		-0.10
6. 2.10	0.24	0.27	0.22	0.17	0.14	0.10	0.08	0.11	0.11	0.11	0.20	0.26	0.17
6. 2. 6	-0.64	-0.53	-0.45	-0.47	-0.43	-0.40	-0.40	-0.46	-0.41	-0.39	-0.43	-0.60	-0.47
7. 2	-0.39	-0.28	-0.45	-0.68	-0.57	-0.51	-0.47	-0.57	-0.58	-0.59	-0.49	-0.48	-0.50
8. 2								-0.92					
8. 1	-0.97	-0.95	-1.13	-1.30	-1.04	-0.84	-0.77	-0.94	-1.03	-1.07	-1.00	-1.07	-1.01
7. 1	-0.43	-0.35	-0.56	-0.78	-0.62	-0.52	-0.47	-0.59	-0.64	-0.68	-0.56	-0.53	-0.56
9.12.3.9	-1.47	_1 50	1 48	1.00	1.00	0.00	0.00	0.00	7.00	7.00	1 70	1 41	1 10
7. 2.2(9)	-0.05		0.01	0.09	0.06	-0.87	-0.83			-1.07	-1.13	0.03	0.05
(0)	000	10.2	13.5	222.0	43725-18	0.07	0.08	0.11	0.09	0.09	0.07	1860	1
Dail. ext.	-0.08	-0.01	-0.13	-0.28	-0.18	-0.19	-0.23	-0.29	-0.28	-0.33	-0.15	-0.13	-0.19
					-			1					

# INDIA. - MADRAS. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

Hour.   Jan.   Feb.   March   April.   May.   June.   July.   Aug.   Sept.   Oct.   Nov.   Dec.   Year.									e 110 110 11					
1	Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1	Widnisht	0.05		0.00		0.00	0.00	0.00	0.00	0.01		0.00	1 00	0.50
2   2.96   3.95   3.60   3.57   3.72   3.86   3.55   3.39   3.10   2.79   3.03   2.63   3.57   3.33   3.33   3.35   3.30   3.55   3.12   3.50   2.96   3.77   3.33   3.50   3.55   3.12   3.50   2.96   3.77   3.83   3.62   5.66   4.79   4.40   4.45   4.68   4.95   4.66   4.34   4.23   3.71   4.23   3.60   4.45   66   4.05   5.64   5.11   3.78   3.86   4.21   4.31   4.07   3.82   3.23   4.05   3.73   4.16   7   2.43   3.33   2.54   1.78   2.07   2.51   2.92   2.79   2.43   1.80   2.00   2.38   2.41   2.43   3.33   2.54   1.78   2.07   2.51   2.92   2.79   2.43   1.80   2.00   2.38   2.41   2.43   3.33   2.54   1.78   2.07   2.51   2.92   2.79   2.43   1.80   2.00   2.38   2.41   2.43   3.33   2.54   1.78   2.07   2.51   2.92   2.79   2.43   1.80   2.00   2.38   2.41   2.43   3.33   2.54   1.78   2.07   2.51   2.92   2.79   2.43   1.80   2.00   2.38   2.41   2.43   3.33   2.54   3.53   3.55   3.6	15.4 119.		1 5 1 4	-	1770003	1 29 25 16		-	1 1000 0		1	The same of the same of	1	
3	Della Control	11	10/10/1	130.1	1.75 44 4	1. D 1976 1 C	1000.7	THE STATE OF	7500 381	1000000	100000000000000000000000000000000000000	The second	-	1
4 3.62 5.06 4.79 4.40 4.45 4.68 4.31 3.98 3.95 3.46 3.91 3.19 4.15 5 3.81 5.49 5.24 4.45 4.68 4.95 4.66 4.34 4.23 3.71 4.23 3.60 4.45 6 4.05 5.64 5.11 3.78 3.86 4.21 4.31 4.07 3.82 3.28 4.05 3.73 4.16 7 2.43 3.33 2.54 1.78 2.07 2.51 2.92 2.79 2.43 1.80 2.00 2.38 2.41 8 9 -2.02 -1.93 -1.59 -2.41 -2.43 -1.73 -0.76 -0.99 0.72 0.13 -0.56 0.00 0.23 9 -2.02 -1.93 -1.59 -2.41 -2.43 -1.73 -0.76 -0.99 -1.12 -1.26 -2.49 -1.73 -1.72 100 -3.26 -3.60 -3.67 -4.14 -4.68 -3.67 -2.67 -2.74 -2.96 -2.34 -3.53 -3.05 -3.86 11 -4.02 -4.81 -4.81 -4.83 -5.75 -5.02 -4.25 -4.16 -4.54 -3.17 -4.09 -3.62 -4.42 -4.31 -4.83 -5.75 -5.02 -4.25 -4.16 -4.54 -3.17 -4.09 -3.62 -4.42 -4.14 -5.30 -4.99 -4.95 -6.99 -5.69 -6.02 -5.75 -5.04 -3.73 -4.25 -3.86 -5.09 2 -4.14 -5.30 -4.99 -4.95 -4.99 -5.69 -6.02 -5.75 -5.04 -3.73 -4.25 -3.86 -5.09 2 -4.14 -5.30 -4.99 -4.95 -4.99 -5.69 -6.02 -5.40 -4.66 -2.55 -3.73 -3.60 -4.75 3 -3.46 -4.85 -4.27 -4.07 -4.00 -4.61 -4.92 -4.59 -3.73 -3.03 -3.05 -2.88 -3.95 4 -2.41 -3.64 -3.10 -2.65 -2.45 -3.57 -3.73 -3.44 -2.56 -2.38 -1.98 -2.04 -2.83 5 -1.19 -2.27 -1.66 -1.03 -1.01 -1.91 -2.18 -1.84 -1.44 -1.26 -0.88 -1.01 -4.47 -0.93 -1.10 -0.52 0.20 0.11 -0.58 -0.81 -0.70 -0.52 -0.63 -0.25 -0.38 -0.46 7 0.09 -0.36 0.17 0.83 0.76 0.36 0.16 0.13 0.07 -0.18 0.09 0.00 0.18 8 0.54 0.27 0.58 0.99 1.19 0.97 0.83 0.74 0.47 0.16 0.47 0.34 0.63 1.1 1.84 1.87 1.84 2.25 2.34 2.41 2.29 2.14 1.89 1.28 1.46 1.44 1.92 8, 8 0.25 0.28 0.37 0.40 0.54 0.67 0.94 0.81 0.59 0.14 -0.04 0.17 0.43 9, 9 -0.54 -0.56 -0.46 -0.42 -0.43 -0.15 0.29 0.13 -0.06 -0.38 -0.87 -0.53 -0.33 -0.33 -0.35 -0.33 -0.35 -0.33 -0.35 -0.35 -0.33 -0.35		11				W. Company	1			1				li
5         3.81         5.49         5.24         4.45         4.68         4.95         4.66         4.34         4.23         3.71         4.23         3.60         4.45           6         4.05         5.64         5.11         3.78         3.86         4.21         4.31         4.07         3.82         3.23         4.05         3.73         4.16           7         2.43         3.33         2.54         1.78         2.07         2.51         2.92         2.79         2.43         1.80         2.00         2.38         2.41           8         -0.04         0.29         0.16         -0.18         -0.11         0.38         1.06         0.99         0.72         0.13         -0.56         0.00         0.23           9         -2.02         -1.93         -1.89         -2.41         -2.43         -1.73         -0.76         -0.90         -1.12         -1.26         -2.49         -1.73         -1.72           10         -3.26         -3.60         -3.67         -1.14         -4.68         -3.67         -2.67         -2.74         -9.90         -1.12         -1.26         -2.34         -3.53         -3.33         -3.40         -2.24 <t< td=""><td></td><td></td><td>1.02</td><td></td><td></td><td></td><td></td><td></td><td>0.00</td><td>0.00</td><td></td><td>0.00</td><td></td><td></td></t<>			1.02						0.00	0.00		0.00		
5         3.81         5.49         5.24         4.45         4.68         4.95         4.66         4.34         4.23         3.71         4.23         3.60         4.45           6         4.05         5.64         5.11         3.78         3.86         4.21         4.31         4.07         3.82         3.23         4.05         3.73         4.16           7         2.43         3.33         2.54         1.78         2.07         2.51         2.92         2.79         2.43         1.80         2.00         2.38         2.41           8         -0.04         0.29         0.16         -0.18         -0.11         0.38         1.06         0.99         0.72         0.13         -0.56         0.00         0.23           9         -2.02         -1.93         -1.89         -2.41         -2.43         -1.73         -0.76         -0.90         -1.12         -1.26         -2.49         -1.73         -1.72           10         -3.26         -3.60         -3.67         -1.14         -4.68         -3.67         -2.67         -2.74         -9.90         -1.12         -1.26         -2.34         -3.53         -3.33         -3.40         -2.24 <t< td=""><td>20-1</td><td></td><td></td><td>1000</td><td></td><td></td><td></td><td></td><td></td><td></td><td>100</td><td></td><td></td><td></td></t<>	20-1			1000							100			
6	180024141	1	1000000	1000	1 1000	10000	1 1 1 1 1 1 1 1 1 1	1	1 10000	1 C 10 C	222.4	Market Street	12.00	1
7         2.43         3.33         2.54         1.78         2.07         2.51         2.92         2.79         2.43         1.80         2.00         2.38         2.41           8         -0.04         0.29         0.16         -0.18         -0.11         0.38         1.06         0.99         0.72         0.13         -0.56         0.00         0.23           9         -2.02         1.93         1.89         2.41         -2.43         -1.73         -0.76         -0.90         -1.12         -1.26         -2.49         -1.73         -1.72           10         -3.26         -3.60         -3.67         -4.14         -4.68         -3.67         -2.67         -2.74         -2.96         -2.34         -3.53         -3.05         -3.36           11         -4.02         -4.81         -4.81         -4.83         -5.75         -5.02         -4.25         -4.16         -4.31         -3.93         -5.01           1         -4.40         -5.35         -5.66         -5.87         -5.85         -5.51         -5.28         -5.04         -3.73         -4.25         -3.86         -5.09           2         -4.14 -5.30         -4.99         -9.95				1		13.0								
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		N. C. C.		1 10 cm	C48.7×3		1 10000	P1000 40	COLLEGE	100000	1		1500	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	THE PARTY OF THE P	2.45	3.33	2.34	1.78	2.01	2.51	4.92	2.19	2.45	1.50	2.00	2.58	2.41
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	ER-E-BILL					1.7	10013	PHASE I	Sept.	15/4/0	HELE	514	7	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	8	-0.04	0.29	0.16	-0.18	-0.11	0.38	1.06	0.99	0.72	0.13	-0.56	0.00	0.23
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	-2.02	-1.93	-1.89	-2.41	-2.43	-1.73	-0.76	-0.90	-1.12	-1.26	-2.49	-1.73	-1.72
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	The state of the state of	-3.26	-3.60	-3.67	-4.14	-4.68	-3.67	-2.67	-2.74	-2.96	-2.34	-3.53	-3.05	-3 36
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	-4.02	-4.81	-4.81	-4.83	-5.75	-5.02	-4.25	-4.16	-4.54	-3.17	-4.09	-3.62	-4.42
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	antr. S.	-100.3	- FD./	100		- 19.1	- IX	- 1111			1963	37.5		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Noon.	-4.43	-5.06	-5.35	-5.66	-5.87	-5.85	-5.51	-5.28	-5.04	-3.76	-4.31	-3.93	-5.01
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1		100 March 1997	A				LA SATE OF	10-71-71	100				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	THE RESERVE AND ADDRESS.	-4.14	-5.30	-4.99	-4.95	-4.99	-5.69	-6.02	-5.40	-4.66	-3.55	-3.73	-3.60	-4.75
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	-3.46	-4.85	-4.27	-4.07	-4.00	-4.61	-4.92	-4.59	-3.73	-3.03	-3.05	-2.88	-3.95
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			11000		1000	September 1		The state						7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	-2.41	-3.64	-3.10	-2.65	-2.45	-3.57	-3.73	-3.44	-2.56	-2 38	-1.98	-2.04	-2.83
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			. 12		1000	101111111111111111111111111111111111111			11016		Call 17505	7		10000
7         0.09         -0.36         0.17         0.83         0.76         0.36         0.16         0.13         0.07         -0.18         0.09         0.00         0.18           8         0.54         0.27         0.58         0.99         1.19         0.97         0.83         0.74         0.47         0.16         0.47         0.34         0.63           9         0.94         0.81         0.97         1.57         1.42         1.35         1.17         0.99         0.49         0.74         0.67         1.06           10         1.39         1.33         1.39         1.89         1.96         2.11         1.87         1.64         1.39         0.90         1.08         1.03         1.50           11         1.84         1.87         1.84         2.25         2.34         2.41         2.29         2.14         1.89         1.28         1.46         1.44         1.92           6, 6         1.83         2.27         2.29         1.99         1.81         1.75         1.65         1.65         1.32         1.90         1.67         1.84           7, 7         1.26         1.48         1.35         1.30         1.41 </td <td>Total San State</td> <td></td> <td>123 L</td> <td></td> <td>-72.200</td> <td></td> <td></td> <td></td> <td>1000</td> <td>ALC: NO</td> <td>Description of the last of the</td> <td>40.00</td> <td>100</td> <td></td>	Total San State		123 L		-72.200				1000	ALC: NO	Description of the last of the	40.00	100	
9	the state of the state of	11.	1 1 1 1 1 1	1000	Section 1			1 CON 100 L	15.5 CM		2.00			
9							NAS.		To the					V 41
9	0	0.54	0.97	0.58	0 90	1 10	0.97	0.83	0.74	0.47	0.16	0.47	0.31	0.63
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					0.70		12000	11/4/31/A	1000	1011-01	14.00	27/2/20	1 1000	1000
11       1.84       1.87       1.84       2.25       2.34       2.41       2.29       2.14       1.89       1.28       1.46       1.44       1.92         6, 6       1.83       2.27       2.29       1.99       1.98       1.81       1.75       1.65       1.65       1.32       1.90       1.67       1.84         7, 7       1.26       1.48       1.35       1.30       1.41       1.43       1.54       1.46       1.25       0.81       1.04       1.19       1.29         8, 8       0.25       0.28       0.37       0.40       0.54       0.67       0.94       0.81       0.59       0.14       -0.04       0.17       0.43         9, 9       -0.54       -0.56       -0.46       -0.42       -0.43       -0.15       0.29       0.13       -0.06       -0.38       -0.87       -0.53       -0.33         10, 10       -0.93       -1.13       -1.14       -1.12       -1.36       -0.78       -0.40       -0.55       -0.78       -0.70       -1.22       -1.01       -0.93         7, 1       -0.98       -1.01       -1.44       -1.87       -1.73       -1.77       -1.57       -1.48       -1.30 <td></td> <td></td> <td></td> <td></td> <td></td> <td>- 1 TO 1 TO 1</td> <td></td> <td>40000</td> <td>1.4. V. 3.0.c.</td> <td>1 1 1 1 1 1 1</td> <td>0.000</td> <td></td> <td>100</td> <td></td>						- 1 TO 1 TO 1		40000	1.4. V. 3.0.c.	1 1 1 1 1 1 1	0.000		100	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			1000000	100000		ARTIC	7-114 28	1 TO 1 TO 1 TO 1 TO 1	1	The same	120000000000000000000000000000000000000	177-57		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	er. 0 - 121.	- 70.0	-11/3	- 12:57	1000	200	- 156.019	Basilia	attite	Maria.	Lanca.	27 35		he cui
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						e la constitución	Em				The second			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6, 6	1.83	2.27	2.29	1.99	1.98	1.81	1.75	1.65	1.65	1.32	1.90	1.67	1.84
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1.26	1.48	1.35	1.30	1.41	1.43	1.54	1.46	1.25	0.81	1.04	1.19	1.29
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	8, 8	0.25	0.28	0.37	0.40	- Carrier	0.67	0.94	0.81	0.59	0.14	-0.04	0.17	0.43
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9, 9	-0.54	-0.56	-0.46	-0.42	-0.43	-0.15	0.29	0.13	-0.06	-0.38	-0.87	-0.53	-0.33
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	46.0 Vis.	I made	08.1	L ENV	- 12.0	1 13 3	1	A A ST	1000	1200	1	ly es		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10, 10	-0.93	-1.13	-1.14	-1.12	-1.36	-0.78	-0.40	-0.55	-0.78	-0.70	-1.22	-1.01	-0.93
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				C 91 100	47			CONTRACT OF	10000	10000	1000	10000	W.	The state of the s
6, 2, 10         0.43         0.56         0.50         0.24         0.28         0.21         0.05         0.10         0.18         0.21         0.47         0.39         0.30		-0.26	-0.39	100000000000000000000000000000000000000	0.5		-0.59		-0.48		170 1100	A STATE OF THE STATE OF	3	Figure 20 to 12
Mean. 76.77 78.25 82.24 85.73 87.10 87.01 86.22 84.51 83.50 81.18 78.53 76.75		0.43	0.56	0.50	0.24	0.28	0.21	0.05	0.10	0.18	0.21	0.47	0.39	0.30
76.77 78.25 82.24 85.73 87.10 87.01 86.22 84.51 83.50 81.18 78.53 76.75				00.0	0.5	0= -6	000					1 1 1 1	9 90	
	Mean.	76.77	78.25	82.24	85.73	87.10	87.01	86.22	84.51	83.50	81.18	78.53	76.75	9 5 6
								1					91500	ELEVA B

### XXI.

# India. - Madras. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

TATEL CO.			7315	113	Degree	es of Re	aumur.		alt Ore		BEN W	3 2 7 1	11000
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
			THE STATE OF										
Morn. 1	1.41	1.22	1.32	1.06		1.15	0.93		1.26	1.18	1.04	1.38	1
2	1.79	1.64	1.42	1.36	1000.31	1.42	1.09	100000	1.52	1.46	1.32	1.50	SCHOOL S
3	2.14	2.10	1.50	1.76	100000	1.70 1.90	1.26 1.42		1.67	1.70 1.88	1.70 1.90	1.68	100
4	2.38	2.42	1.58	2.10	2.17	1.30	1.42	1.00	1.70	1.00	1.30	1.93	1.52
5	2.42	2.43	1.61	2.20	2.18	1.95	1.42	1.45	1.62	1.88	2.02	2.17	1.95
6	2.22	2.05	1.48	1.91	1.86	1.77	1.33	1.10	1.39	1.64	1.81	2.25	1.73
7	1.76	1.30	1.14	1.24	1.19	1.30	1.12	0.75	1.02	1.14	1.27	2.00	1.27
8	1.05	0.36	0.54	0.30	0.27	0.70	0.78	0.46	0.47	0.40	0.50	1.32	0.60
9	0.15	-0.59	-0.23	-0.71	-0.75	-0.06	0.35	0.16	-0.23	-0.46	-0.35	0.27	-0.20
10	-0.82	-1.38	-1.04	-1.56	-1.67	-0.82	-0.21	-0.18		-1.26	-1.10	-0.94	-1.00
11	-1.74	-1.94	-1.70	-2.12	-2.31	-1.46	-0.86	-0.62		-1.83		-2.20	-1.69
Noon	-2.48	-2.23	-2.06	-2.36	-2.58	-1.94	-1.52	-1.12	-2.29	-2.18	-2.12	-2.76	-2.14
1	-2.90	-2.34	-2.10	-2.34	-2.48	-2.20	-2.13	-1.57	-2.47	-2.17	-2.25	-2.98	-2.33
2	-2.97			-2.14		-2.24		-1.82	1700		200	-2.76	
3	-2.68	-2.12	-1.52	-1.84	-1.62	-2.07	-2.48	-1.77	-1.77	-1.50	-1.98	-2.25	-1.97
4	-2.14	-1.81	-1.14	-1.46	-1.11	-1.74	-2.12	-1.43	-1.12	-1.08	-1.61	-1.65	-1.53
5	-1.47	-1.34	-0.83	-1.00	-0.65	-1.28	-1.44	-0.94	-0.50	-0.70	-1.10	-1.13	-1.03
6	-0.81	-0.78	-0.58	-0.48	-0.27	-0.78	-0.65	-0.46	-0.06	-0.38	-0.58	-0.72	-0.55
7	-0.26	-0.18	-0.35	0.04	0.02	-0.30	0.08	-0.14	0.18	-0.14	-0.14	-0.39	-0.13
8	0.13	0.30	-0.08	0.49	0.26	0.12	0.62	-0.04	0.27	0.06	0.36	-0.06	0.20
9	0.38	0.62	0.42	0.71	0.45	0.42	0.86	-0.06	0.33	0.26	0.64	0.30	0.44
10	0.58	0.77	0.60	0.90	0.61	0.63	0.91	-0.06	0.44	0.46	0.81	0.66	0.61
11	0.79	0.84	0.91	0.91	0.78	0.79	0.87	0.11	0.66	0.67	0.83	0.99	0.76
Midn	1.06	0.96	1.16	0.92	0.98	0.94	0.84	0.47	0.95	0.91	0.89	1.22	0.94
				J. C.						Hye A			
6. 6	0.71	0.64	0.45	0.72	0.80	0.50	0.34	0.32	0.67	0.63	0.62	0.77	0.60
7. 7	0.75	0.56	0.40	0.64	0.61	0.50	0.60	0.31	0.60	0.50	0.57	0.81	0.57
8. 8	0.59	0.33	0.23	0.40	0.27	0.41	0.70	0.21	0.37	0.23	0.43	0.63	0 40
9. 9	0.27	0.02	0.10	-0.00	-0.15	0.18	0.61	0.05	0.05	-0.10	0.15	0.29	0.12
10.10	-0.12	-0.31	-0.22	-0.33	-0.53	-0.10	-0.35	-0.12	-0.29	-0.40	-0.15	-0.14	-0.20
7. 2. 9	-0.28	-0.13	-0.11	-0.06	-0.16	-0.17	-0 16	-0.38	-0.31	-0.17	-0.09	-0.15	-0.18
6. 2. 8	-0.21	0.02	-0.16	0.09				-0.25		-0.07		-0.19	
6. 2.10	-0.06	0.17	0.07	0.22	0.11		1,11	-0.26		0.06		0.05	- C - C - C - C - C - C - C - C - C - C
6. 2. 6	-0.52	-0.34		-0.24	-0.18			-0.39		1000	-0.32	-0.41	-0.36
7. 2	-0.61	-0.50	-0.37	-0.45	-0.47	-0.47	-0.68	-0.54	-0.63	-0.32	-0.46	-0.38	-0.50
8. 2	The same of							-0.68					
8. 1	-0.93	-0.99	-0.78	-1.02	-1.11	-0.75	-0.68	-0.56					
7. 1	-0.57	-0.52	-0.48	-0.55	-0.65	-0.45	-0.51	-0.41		-0.52			
9.12.3.9	-1.16	-1.08	-0.85	-1.05	-1.13	-0.01	-0.70	-0.70	_0 00	-0.97	-0.95	-1.11	-0.97
7. 2.2(9)	-0.11	0.06	0.03		-0.01			-0.70				-0.04	
Dail.ext.	-0.28	0.05	-0.25	-0.08	-0.20	-0.15	-0.53	-0.08	-0.39	-0.15	-0.12	-0.37	-0.19
h-a						1							

### · XXII.

## India. — Bombay. Lat. 18° 56' N. Long. 72° 54' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

						es of Fa			1.	1	1		
Hours.	· Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
		4	20 20 7	1,500		The state of	Parailin	TE TIME			30.30	DEPT.	Vie S
Morn. 1	1.49	1.40	0.99	1.13	1.42	1.15	0.79	0.97	1		CONTRACTOR AND	1.55	1.26
2	1.80	1.69	1.33	1.51	1.78	1.40	0.88	1.13	0.97	1.87		1.87	1.53
3	2.27	2.21	1.91	2.05	2.14	1.69	0.90	1.24	1.24	2.32	100000000000000000000000000000000000000	2.41	1.91
4	2.86	2.84	2.59	2.48	2.32	1.91	0.90	1.31	1.53	.2.75	2.81	3.11	2.27
5	3.47	9.40	3.04	9.01	2.23	1.96	0.00	1 91	1.71	2.95	3.11	3.78	2.54
4	3.83	3.40	3.04	2.61 2.34	1.80	1.80	0.86	1.31 1.24	1.67	2.79	THE RESIDENCE OF	4.16	2.52
7	3.69	3.33	2.54	1.67	1.15	1.42	0.65	1.04	1.22	2.21	2.79	4.01	2.14
8	2.97	2.48	1.58	0.77	0.36	0.88	0.38	0.74	0.79	1.28	3000	3.24	1.44
			1.00		0.00	0.00	0.00	0	47	-			
9	1.69	1.22	0.38	-0.14	-0.41	0.23	0.00	0.32	0.09	0.16	0.63	1.87	0.50
10	0.07	-0.23	-0.77	-0.90		-0.43	-0.52	-0.20	-0.65	-0.95		0.16	-0.52
11	-1.55	-1.55	-1.67	-1.49	-1.55	-6.08	-6.08	-0.79	-1.28	-1.91	-2.21	-1.60	-1.49
Noon	-2.86	-2.61	-2.30	-1.91	-1.94	-1.64	-1.55	-1.35	-1.80	-2.59	-3.29	-3.08	-2.25
		Y name	N. Eg			305			Will.	4,00	1		marrie
1	-3.69			11 24		The second	-1.82	-0.7	-2.12				-2.75
2	-3.98		-2.84	-2.50	100000000000000000000000000000000000000	-2.41	CONTRACTOR OF THE	WITE A RESIDEN		-3.13	37.00	-4.59	
3	-3.85	-3.65				-2.45	444		-2.16			-4.55	
4	-3.42	-3.42	-2.72	-2.50	-2.09	-2.25	-0.92	-1.69	-1.87	-2.66	-3.33	-4.12	-2.59
5	-2.84	-2.95	-2.34	9.08	-1.64	1 70	0.90	104	1 977	914	-2.61	-3.38	-2.07
6	Par Treat	-2.95 $-2.27$	-2.54 $-1.71$	-2.07 $-1.37$		1000	NAME OF TAXABLE PARTY.	-1.24 $-0.72$		-2.14 $-1.46$	SOUTH CAN	-3.35 $-2.45$	
7	-1.49	-1.44	-0.88	-0.54	-0.38	-0.47	0.03	-0.72 $-0.23$		-0.72		-2.45 $-1.46$	-0.68
8	-0.79	-0.56	A Company of	0.23	0.18	0.14	0.50	0.16	100000	-0.02		-0.52	-0.02
	0	0.00	0.01	0.20	0.10	0.14	0.00	0.10	100 13	0.02	0.00	0.02	0102
9	-0.11	0.23	0.56	0.72	0 59	0.54	0.54	1.43	0.86	0.52	0.77	0.29	0.50
10	0.47	0.81	0 90	0.92	0.83	0.79	0.54	0.59	0.99	0.88	1.35	0.86	0.83
11	0.92	1.10	0.97	0.92	0.99	0.96	0.61	0.72	0.97	1.08	1.71	1.19	1.01
Midn	1.24	1.26	0 92	0.95	1.15	0.99	0.70	0.83	0.88	1.26	1.91	1.37	1.13
	Was I	- No.	1000					110					
	81.718		1882			Tage					a to		
6. 6	0.81	0.68	0.68	0.50	0.38	0.34	0.43	0.25	0.45	0.68	0.70	0.86	0.56
7. 7	1.10	0.95	0.83	0.56	0.38	0.47	0.52	0.41	0.63	0.74	0.95	1.28	0.74
8. 8 9. 9	1.08	0.97	0.77	0.50	0.27	0.50	0.45	0.45	0.63	0.63	0.95	1.35	0.72
10.10	0.79	0.72	0.47	0.29	0.09	0.38	0.27	0.36	0.47	0.34 $-0.05$	0.70	1.08	0.50
23.10	0.21	0.29	0.07	0.00	-0.11	0.18	0.02	0.20	0.18	-0.05	0.25	0.52	0.16
7. 2. 9	-0.14	-0.02	0.09	-0.05	-0.20	-0.16	-0.20	-0.18	-0.07	-0.14	-0.18	-0.09	-0.11
6. 2. 8	-0.32	-0.18	0.05	0.02	-0.11	-0.16	The second second	-0.20	200	-0.11	The same	-0.03	-0.16
6. 2.10	0.11	0.27	0 38	0.25	0.09	0.07	- "Line - "	-0.07	0.14	0.18	0.14	0.14	0.14
6. 2. 6	-0.79	-0.74	-0.50		-0.52	-0.59	the second second	-0.50		-0.61		-0.97	-0.61
	PER	P. Pre	09 55	LL Y		THE STATE OF							
7. 2	-0.16	-0.14	-0.16	-0.43	-0.61	-0.50	-0.56	-0.50	-0.52	-0.47	-0.65	-0.29	-0.41
8. 2	-0.52	-0.56	-0.63	-0.88	-0.99	-0.77	-0.70	-0.63				-0.68	
8. 1	9-130	-0.41	-0.54	100		-0.63		-0.52		- 3-21 1		-0.43	
7. 1	0.00	0 02	-0.07	-0 29	-0 54	-0.36	-0.59	-0.38	-0.45	-0.41	-0.56	-0.05	-0.32
9.12.3.9	-1.00	1.00	1.00	0.00	1.00	0.00		1 10		100	C PROPE		
7. 2.2(9)	-1.28 -0.14	-1.22 $0.05$	-1.06 $0.20$	100000000000000000000000000000000000000		-0.83				A Secretary	100000	-1.37	-1.04
2.2(8)	-0.14	0.05	0.20	0.16	0.00	0.02	-0.02	-0.02	0.18	0.02	0.07	0.00	0.05
		umham											

### XXIII. "

# India. — Bombay. Lat. 18° 56′ N. Long. 72° 54′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Morn. 1							es of Re							
1.01	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
1.01		188		1119		· · · · · · · · · · · · · · · · · · ·	The state of	Wid	The same	The c	-ford	les,		ni nati
1.01	Morn, 1	0.66	0.62	0.44	0.50	0.63	0.51	0.35	0.43	0 38	0.66	0.90	0.69	0.56
1.01   0.98   0.85   0.91   0.95   0.75   0.40   0.55   0.65   1.03   1.09   1.07   0.85     1.27   1.26   1.15   1.10   1.03   0.85   0.40   0.55   0.68   1.22   1.25   1.38   1.01     5		0.80	0.75	0.59	0.67	0.79	0.62	0.39	0.50	0.43	0.83	0.97	0.83	0.68
1.27   1.26   1.15   1.10   1.03   0.85   0.40   0.58   0.68   1.22   1.25   1.38   1.01			10000	1000			32000	1 1 1 1 1 1	1	1 - 1-1		1	100	
5	THE RESERVE				1		1			1/200	1	165	1 1 1 1 1 1 1 1 1	
6	4	1.41	1.20	1.10	1.10	1.00	0.00	0.40	0.00	0.00	1.22	1.20	1.00	1.01
6	35/2 /	1 54	1 51	1 95	1 16	0.00	0.87	0.38	0.58	0.76	1 91	1 38	1 68	1 12
7	11		D. T. 10	47791				1000	TATAL	197010		1 0 CK		
8	III .		1			1000	1 1 1 1 1 1 1		1000		1 1 1 1 1 1 1	-090016		
$\begin{array}{c} 9 \\ 10 \\ 0.03 \\ -0.10 \\ -0.34 \\ -0.10 \\ -0.34 \\ -0.40 \\ -0.47 \\ -0.66 \\ -0.69 \\ -0.48 \\ -0.48 \\ -0.48 \\ -0.48 \\ -0.48 \\ -0.48 \\ -0.48 \\ -0.69 \\ -0.69 \\ -0.69 \\ -0.69 \\ -0.69 \\ -0.69 \\ -0.69 \\ -0.69 \\ -0.69 \\ -0.69 \\ -0.69 \\ -0.69 \\ -0.85 \\ -0.86 \\ -0.73 \\ -0.66 \\ -0.69 \\ -0.80 \\ -0.73 \\ -0.66 \\ -0.69 \\ -0.80 \\$	III III TO THE TOTAL OF THE PARTY OF THE PAR		1. 10	46.71	100						0.000	100,000		- NOOD
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	1.32	1.10	0.70	0.34	0.16	0.39	0.17	0.33	0.35	0.57	0.85	1.44	0.64
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					0.00	0.00	0.00		0 - 1		0.00	0.00	0.00	0.00
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$									SHOW	The second second			1.000	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				- 14						The second second	The best and	- 11	Contract Con	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	-0.69	-0.69	-0.74	-0.66	-0.69	-0.48	-0.48	-0.35	-0.57	-0.85	-0.98	-0.71	-0 66
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Noon	-1.27	-1.16	-1.02	-0.85	-0.86	-0.73	-0.69	-0.60	-0.80	-1.15	-1.46	-1.37	-1.00
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		133					HE ?				110.5	11.8	. 1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	-1.64	-1.46	-1.18	-1.00	-0.98	-0.94	-0.81	-0.79	-0 94	-1 33	-1.74	-1.82	-1.22
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	-1.77	-1.60	-1.26	-1.11	-1.04	-1.07	-0.79	-0.89	-1.00	-1 39	-1.81	-2 04	-1.31
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3	-1.71	-1.62	-1.27	-1.16	-1.03	-1.09	-0.64	-0.88	-0.96	-1 33	-1.71	-2.02	-1.29
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	-1.52	-1.52	-1.21	-1.11	-0.93	-1.00	-0.41	-0.75	-0.83	-1.18	-1.48	-1.83	-1.15
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												4	11 100	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	-1.26	-1.31	-1.04	-0.92	-0.73	-0.79	-0.17	-0.55	-0.61	-0.95	-1.16	-1.50	-0.92
7								100000	10000					1011-11
8														
9						5,014	10000			4 1 2 1 1 1 1	100000		11/10/02/20	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0	-0.55	70.20	0.00	0.10	0.00	0.06	0.22	0.07	0.21	-0.01	0.	-0.25	-0 01
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	-0.05	0.10	0.25	0 39	0.96	0.21	0.94	0.10	0 20	0 22	0.94	0.12	0 22
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	THE RESERVE OF THE PARTY OF THE					5-1-2-1		1000		The Control	S. CINIS	7 6 7 6 1		100000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					100		1000				3. 79.367.3		The same of	
6. 6						1 7 5 5 1 1 3				C. Carlo	11111111		1 1000	4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Mian	0.55	0.56	0.41	0.42	0.51	0.44	0.31	0.37	0.39	0.56	0.85	0.61	0.50
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			8 1						1					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0	0.00	0.00	0.00								1		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							30000	A COLOR		4 34	V 10000	Feb. 10 (2011)	A STATE OF	The same of
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							The state of the s			- (CHO 15)				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				0.34	0.22	0.12	0.22	0.20	0.20	0 28	0.28	0 42	0.60	0.32
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	0.35	0 32	0.21	0.13	0.04	0.17	0.12	0.16	0.21	0.15	0.31	0.48	0.22
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.10	0.12	0.13	0.03	0.00	-0.05		0.01	and the same of	The state of		10000	0.23	100/2000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	REQUEST TO THE	Total San	100	- 38	HE	村鎮	9 84	DITTE !	7-133	1400	105	D TE	4	TO THE
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		-0.06	-0.01	0.04	-0.02	-0.09	-0.07	-0.09	-0.08	-0.03	-0.06	-0.08	-0.04	-0.05
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.14	-0.08	0.02	0.01	-0.05	-0.07	-0.07	-0.09	-0.02	-0.05	-0.14	-0.14	-0.07
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6. 2.10	0 05	0.12	0.17				2.14						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6. 2 6	-0.35			1 1 1 1	100		1.43		1000				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		L. Land				0.140	0120	0.10	0-22	0.20	0.21	0.40	0.10	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7. 2	-0.07	-0.06	-0.07	-0.19	-0.27	-0.22	-0.25	-0.22	-0.23	-0.21	-0.29	-0.13	-0.18
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8. 2					- Company				0.00				- A 15
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8. 1				THE RESERVE						V44 - VC24			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
7. $2.2(9)$ $\begin{vmatrix} -0.06 \\ 0.02 \end{vmatrix}$ $\begin{vmatrix} 0.02 \\ 0.09 \end{vmatrix}$ $\begin{vmatrix} 0.07 \\ 0.07 \end{vmatrix}$ $\begin{vmatrix} 0.01 \\ 0.00 \end{vmatrix}$ $\begin{vmatrix} 0.01 \\ -0.01 \end{vmatrix}$ $\begin{vmatrix} -0.01 \\ -0.01 \end{vmatrix}$ $\begin{vmatrix} 0.02 \\ 0.08 \end{vmatrix}$ $\begin{vmatrix} 0.01 \\ 0.03 \end{vmatrix}$ $\begin{vmatrix} 0.01 \\ 0.03 \end{vmatrix}$ $\begin{vmatrix} 0.01 \\ 0.02 \end{vmatrix}$	1000000		0.01	0.00	0.10	0.24	0.10	0.20	-0.17	-0.20	-0.18	.0.20	0.02	0.14
7. 2.2(9) -0.06 0.02 0.09 0.07 0.00 0.01 -0.01 -0.01 0.08 0.01 0.03 0.00 0.02	9.12.2.9	-0.57	-0.54	-0.47	-0.44	-0.45	-0.37	-0.27	-0.20	-0.34	-0.55	-0.61	-0.61	-0.46
	7. 2.2(9)			-3-3-	200			4000					1	1
Dail.ext.   -0.04   -0.01   0.05   0.01   0.00   -0.11   -0.21   -0.16   -0.12   -0.04   -0.21   -0.10   -0.09				0.03	0.07	0.00	0.01	0.01	0.01	0.00	0.01	. 0.00	0 00	0.02
0.10 0.12 0.01 0.10 0.10	Dail.ext.	-0.04	-0.01	0.05	0.01	0.00	-0.11	-0.21	-0.16	-0.12	-0.04	-0.21	-0.10	-0.09
The numbers without size was built at the state of the st						0.00	0.11	0.21	0.10	0.12	0.04	0.21	0.10	0.00

### XXIV.

### India. - Madras. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0.01	1 10	7.00	7.00	1.00	7.05	1.10	1.00	1.04	0.82	0.91	0.84	1.11
Midn.	0.91	1.13	1.00	1.62	1.22	1.35	1.19	1.27		4040 000	26 2 11 11	1.00	1.11
1	1.13	1.45	1.29	1.37	1.47	1.56	1.38	1.34	1.20	1.01	1.13		
2	1.32	1.76	1.60	1.59	1.65	1.72	1.58	1.51	1.38	1.24	1.35	1.17	1.49
3	1.48	2.01	1.88	1.81	1.81	1.90	1.75	1.64	1.58	1.39	1.56	1.32	1.68
4	1.61	2.25	2.13	1.96	1.98	2.08	1.92	1.77	1.76	1.54	1.74	1.42	1.85
5	1.74	2.44	2.33	1.98	2.08	2.20	2.07	1.93	1.88	1.65	1.88	1.60	1.98
6	1.80	2.51	2.27	1.68	1.72	1.87	1.92	1.81	1.70	1.46	1.80	1.66	1.85
7	1.08	1.48	1.13	0.79	0.92	1.12	1.30	1.24	1.08	0.80	1.89	1.06	1.07
8	-0.02	0.13	0.07	-0.08	-0.05	0.17	0.47	0.44	0.32	0.06	-0.25	0.00	0.10
9	-0.90	-0.86	-0.84	-1.07	-1.08	-0.77	-0.34	-0.40	-0.50	-0.56	-1.11	-0.77	-0.77
10	-1.45	-1.60	-1.63	-1.84	-2.08	-1.63	-1.19	-1.22	-1.32	-1.04	-1.57	-1.36	-1.49
11	-1.79	-2.14	-2.14	-2.15	-2.56	-2.23	-1.89	-1.85	-2.02	-1.41	-1.82	-1.61	-1.47
Noon.	_1 97	_9 95	_9 28	_9 59	_2 61	_2 60	-9 45	-2.35	-2 21	_1 67	_1.92	-1.75	-2.23
1	1	THE RESERVE	-2.41		-2.51	7	VANDO BULL	-2.56	100000	EN VETT	10000		
2	1		-2.22		OF STREET	A	-2.67	37	-2.07	Contract of	The state of the s	-1.60	1
3	1000000			The second of	A Property and the	-2.05		-2.04	12.0000			-1.28	
4			-1.38	The Laboratory	-1.09	Contract of	A STATE OF THE STA	-1.53				-0.91	-1.26
5	56/600		-0.74	and would	A SHAREST CO.			-0.82	LATER LANGE OF THE PARTY OF THE		-0.39	-0.45	
6	-0.17	-0.49	-0.23	0.09	0.05	-0.26	-0.36	-0.31	-0.23	-0.28	-0.11	-0.17	-0.21
7		-0.16	0.07	0.03	0.03	0.16	0.07	0.06	0.03		0.04	0.00	0.08
8	0.04		0.26	0.44	0.53	0.10	0.37	0.33	0.03	0.07	0.04	0.15	0.28
9	0.42	0.36		0.70	0.70	0.63	0.60	0.52	0.44	0.22	0.33	0.30	0.47
10	0.62	0.59	0.43	0.84	0.87	0.94	0.83	0.73	0.62	0.40	0.48	0.46	0.67
11	0.82		1111	1.00	1.04	1.07	1.02	0.95	0.84	0.57	0.65	0.64	0.85
Mean.	19.90	20.56	22.33	23.88	24.49	24.45	24.10	23.34	22.89	21.86	20.68	19.89	

### XXV.

India. — Bombay. Lat. 18° 56′ N. Long. 72° 54′ E. Greenw. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	1.76	1.68	1.43	1.40	1.30	0.80	0.57	0.59	0.92	1.36	1.74	1.93	1.29
1	1.91	1.88	1.65	1.54	1.40	0.89	0.65	0.64	0.98	1.52	1.80	2.00	1.40
2	2.04	2.04	1.80	1.75	1.54	0.88	0.63	1.16	1.09	1.62	1.97	2.18	1.56
3	2.18	2.22	1.90	1.92	1.69	0.94	0.65	0.81	1.18	1.74	2.11	2.28	1.63
4	2.39	2.44	2.26	2.02	1.81	1.04	0.76	0.82	1.25	1.89	2.23	2.41	1.78
5	2.65	2.68	2.42	2.26	1.92	1.09	0.83	0.90	1.25	1.96	2.40	2.62	1.92
6	2.88	2.88	2.60	2.20	1.65	1.03	0.84	0.84	1.21	2.00	2.55	2.66	1.94
7	2.53	2.37	1.61	0.76	0.44	0.60	0.55	0.51	0.61	1.02	1.47	2.08	1.21
8	0.72	0.48	-1.04	-0.62	-0.51	-0.01	0.02	0.08	-0.20	-0.31	-0.12	0.20	-0.11
9	-1.04	-1.05	-1.49	-1.53	-1.30	-0.46	-0.46	-0.45	-0.84	-1.53	-1.40	-1.00	-1.05
10	-2.40	-2.29	-2.28	-2.00	-1.73	-0.79	-0.74	-0.76	-1.32	-2.17	-2.38	-2.14	-1.75
11	-3.08	-2.98	-2.54	-2.20	-2.08	-1.18	-1.07	-1.12	-1.51	-2.38	-3.18	-2.94	-2.19

### XXV.

## INDIA. - BOMBAY, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-3.40	-3.29	-2.52	-2.44	-2.32	-1.40	-1.09	-1.34	-1.72	-2.39	-3.26	-3.32	-2.37
1	-3.02	-3.12	-2.67	-2.53	-2.28	-1.50	-1.12	-1.35	-1.77	-2.22	-2.96	-3.35	-2.3
2	-2.78	-2.89	-2.56	-2.32	-2.14	-1.52	-0.97	-1.35	-1.55	-2.09	-2.55	-2.97	-2.1
3	-2.38	-2.54	-2.25	-2.05	-1.85	-1.31	-0.85	-1.09	-1.37	-1.79	-2.22	-2.59	-1.S
4	-1.96	-2.07	-1.72	-1.49	-1.36	-0.89	-0.63	-0.76	-0.95	-1.38	-1.55	-2.03	-1.40
5	-1.30	-1.41	-1.08	-0.96	-0.83	-0.49	-0.36	-0.34	-0.36	-0.61	-0.67	-1.09	-0.7
6	-0.64	-0.44	-0.16	0.00	0.09	-0.02	0.03	0.13	0.14	0.01	-0.14	-0.52	-0.1
7	-0.28	-0.07	0.19	0.43	0.63	0.22	0.21	0.26	0.28	0.30	0.09	-0.23	0.1
8	0.00	0.23	0.48	0.66	0.87	0.39	0.28	0.34	0.44	0.53	0.36	0.10	0.3
9	0.58	0.63	0.80	0.83	0.92	0.44	0.36	0.41	0.58	0.76	0.85	0.75	0.6
10	1.16	1.15	1.04	1.09	0.95	0.52	0.41	0.52	0.78	0.96	1.32	1.35	0.9
11	1.47	1.48	1.20	1.24	1.17	0.71	0.48	0.56	0.89	1.18	1.58	1.65	1.1
Tean	18.38	19.30	21.00	22.50	23,43	22.35	21.67	21.45	21.42	22.08	21.28	19.54	

### XXVI.

India. — Calcutta. Lat. 22° 33′ 5″ N. Long. 88° 19′ 2″ E. Greenw. — Dove.

Degrees of Resumur.

						0							
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	1.86	1.69	2.06	1.60	1.90	1.12	0.69	0.69	0.71	1.00	1.24	1.51	1.34
1	2.24	2.00	2.37	1.96	2.06	1.12	0.80	0.78	0.76	1.17	1.47	1.77	1.5
2	2.53	2.22	2.62	2.18	2.21	1.16	0.91	0.85	0.84	1.26	1.69	2.00	1.7
3	2.80	2.44	2.84	2.27	2.32	1.29	1.02	0.92	0.93	1.26	1.82	2.31	1.8
4	3.06	2.71	3.08	2.40	2.41	1.29	1.11	0.96	1.04	1.46	2.00	2.40	1.9
5	3.33	2.89	3.28	2.47	2.50	1.34	1.24	1.07	1.16	1.53	2.22	2.66	2.1
6	3.53	3.11	3.42	2.53	2.41	1.34	1.24	1.12	1.16	1.62	2.36	2.80	2.2
7	3.71	3.24	3.42	2.22	1.90	1.03	0.96	0.89	0.93	0.86	2.31	2.93	2.0
8	2.73	2.20	1.97	1.18	0.81	0.45	0.42	0.32	0.27	0.31	0.93	1.68	1.1
9	0.91	0.71	0.46	0.11	-0.34	-0.13	-0.16	-0.22	-0.24	-0.47	-0.13	0.35	0.0
10	-0.78	-0.62	-0.98	-0.44	-1.39	-0.66	-0.69	-0.33	-0.73	-0.58	-1.02	-0.76	-0.7
11	-2.09	-1.64	-2.14	-1.82	-2.14	-1.15	-1.13	-1.08	-1.16	-1.60	-1.91	-1.87	-1.6
Noon.	-3.31	-2.62	-3.16	-2.67	-2.76	-1.60	-1.51	-1.51	-1.40	-1.94	-2.44	-2.80	-2.3
1	-4.14	-3.28	-3.87	-3.09	-3.12	-1.68	-1.58	-1.55	-1.44	-2.05	-2.80	-3.29	-2.6
2	-4.52	-3.64	-4.25	-3.47	-3.32	-1.73	-1.29	-1.80	-1.63	-2.12	-3.07	-3.69	-2.8
3	-4.65	-3.87	-4.40	-3.62	-3.43	-1.92	-1.24	-1.20	-1.27	-1.83	-2.98	-3.69	-2.8
4	-3.78	-3.69	-4.23	-3.40	-3.10	-1.53	-0.96	-0.95	-0.91	-1.49	-2.18	-2.76	-2
5	-3.07	-3.13	-3.36	-2.73	-2.43	-1.20	-0.64	-0.68	-0.56	-0.92	-1.60	-2.18	-1.8
6	-1.87	-1.91	-1.96	-1.42	-1.23	-0.57	-0.31	-0.31	-0.16	-0.25	-0.76	-1.34	-1.0
7	-0.96	-0.93	-0.78	-0.31	-0.14	-0.11	-0.07	-0.09	0.04	0.13	-0.22	-0.63	-0.3
8	-0.20	-0.22	0.00	0.40	0.68	0.20	0.09	0.25	0.22	0.42	0.27	-0.05	0.1
9	0.42		0.73	0.89	1.08	0.49	0.22	0.45	0.33	0.60	0.62	0.44	0.5
10	0.95	1	1.22	1.20	1.46	0.63	0.36	0.56	0.47	0.75	1.07	0.93	0.8
11	1.37	1.20	1.66	1.54	1.64	0.74	0.49	0.65	0.60	0.88	1.16	1.20	1.0
Mean.	15.49	17.57	21.19	22.51	24.01	23.29	22.68	22.86	22.42	21.73	18.88	16.36	1

#### XXVII.

## Asia. - Tiflis. Lat. 41° 41' N. Long. 45° 17' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
00)				-		-			-				-
Midn.	0.87	1.01	1.54	1.81	1.95	2.38	2.43	2.22	1.60	1.38	0.99	0.80	1.58
1	1.02	1.15	1.80	2.10	2.28	2.67	2.79	2.52	1.81	1.64	1.16	0.94	1.82
2	1.17	1.33	2.02	. 2.40	2.58	2.94	3.13	2.82	2.08	1.88	1.37	1.04	2.06
3	1.32	1.47	2.23	2.64	2.84	3.22	3.49	3.13	2.29	2.11	1.59	1.14	2.28
4	1.46	1.57	2.39	2.94	3.14	3.43	3.73	3.44	2.59	2.39	1.73	1.25	2.51
. 5	1.60	1.69	2.58	3.12	3.09	3.09	3.55	3.59	2.74	2.62	1.85	1.35	2.57
6	1.76	1.75	2.63	2.89	2.39	2.35	2.77	3.06	2.63	2.77	1.99	1.40	2.37
7	1.87	1.75	2.14	2.19	1.53	1.28	1.50	2.16	1.99	2.38	1.85	1.42	1.84
8	1.40	1.23	1.23	0.99	0.53	0.35	0.70	1.05	1.07	1.52	1.44	1.19	1.06
9	0.05	0.50	0.16	100000000000000000000000000000000000000	-0.51	-0.65	-0.32	-0.21	-0.03	0.30	0.54	0.49	0.01
10	-0.41	-0.46	-0.94	-1.20	-1.41	-1.66	-1.35	-1.32	-1.15	-0.47	-0.46	-0.19	-0.92
11	-1.17	-1.33	-1.85	-2.06	-2.19	-2.40	-2.27	-2.20	-2.01	-1.77	-1.31	-1.11	-1.81
Noon.	-1.91	-1.94	-2.64	-2.77	-2.89	-2.42	-2.99	-2.89	-2.67	-2.53	-2.07	-1.76	-2.46
1	-2.37	-2.45	-3.12	-3.29	-3.21	-3.42	-3.53	-3.60	-3.17	-3.07	-2.50	-2.21	-3.00
_ 2	-2.59	-2.65	-3.25	-3.37	-3.34	-3.50	-3.68	-3.85	-3.41	-3.56	-2.81	-2.38	-3.20
3	-2.33	-2.58	-3.21	-3.41	-3.25	-3.51	-3.82	-3.98	-3.37	-3.41	-2.55	-2.08	-3.12
4	-1.78	-2.07	-2.78	-3.20	-2.97	-3.39	-3.82	-3.72	-2.95	-2.81	-1.87	-1.43	-2.73
5	-0.99	-1.24	-2.08	-2.46	-2.65	-2.86	-3.47	-3.20	-1.53	-1.85	-1.27	-0.90	-2.04
6	-0.57	-0.60	-1.11	-1.56	-1.47	-1.81	-2.36	-2.01	-1.18	-1.17	-0.73	-0.49	-1.26
7	-0.17	-0.19	-0.48	-0.69	-0.45	-0.63	-0.86	-0.85	-0.46	-0.50	-0.35	-0.13	-0.48
8	0.15	0.19	0.12	-0.02	0.26	NITH A	0.13	-0.02	0.18	0.11		0.19	0.12
9	0.33	0.44	0.51	0.64		0.92	0.87	0.72	0.61	0.50	0.24	0.36	0.58
10	0.55	0.65	0.91	1.05	1.28	1.51	1.44	1.33	1.00	0.81	0.48	0.53	0.96
11	0.69	0.89	1.25	1.45		1.95	1.96	1.80	1.32	1.10	0.76	0.68	1.29
Mean.	-0.20	3.00	5.64	9.99	13.54	16.10	19.01	19.43	15.03	11.40	5.07	2.45	

#### XXVIII.

CHINA. — PEKING. Lat. 39° 54' N. Long. 116° 26' E. Greenw. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June	July.	Aug	Sept.	Oct.	Nov.	Dec	Year
Midn.	1.16	1.70	1.83	1.75	2.19	2.24	1.61	1.49	1.69	1.64	1.19	1.25	1.64
1	1.47	2.07	2.19	2.26	2.76	2.73	1.89	1.80	2.04	2.05	1.47	1.39	2.01
2	1.66	2.35	2.78	2.67	3.20	3.12	2.23	2.04	2.32	2.37	1.68	1.65	2.34
3	1.93	2.55	2.93	3.18	3.72	3.47	2.50	2.31	2.55	2.62	1.88	1.83	2.62
4	2.13	2.81	3.27	3.57	4.13	3.82	2.74	2.54	2.97	2.92	2.01	2.46	2.95
5	2.41	2.94	3.57	3.89	4.30	3.88	2.78	2.71	3.10	3.19	2.20	2.10	3.09
6	2.58	3.15	3.65	3.81	3.37	2.86	2.10	2.46	2.96	3.43	2.32	2.18	2.91
7	2.63	3.21	3.19	2.91	2.30	1.95	1.34	1.65	2.10	2.98	2.30	2.29	2.40
8	2.23	2.37	1.84	1.65	1.19	1.07	0.52	0.76	0.87	1.68	1.39	1.73	1.44
9	0.77	0.70	0.49	0.34	0.00	0.03	-0.12	-0.20	-0.24	0.15	0.19	0.31	0.20
10	-0.57	-0.65	-0.81	-0.79	-1.20	-1.06	-0.97	-1.09	-1.36	-1.05	-0.84	-0.97	-0.95
11	-1.35	-1.90	-1.93	-2.03	-1.24	-2.17	-1.71	-1.67	-2.17	-2.18	-1.74	-1.96	-1.84

#### XXVIII.

### CHINA. - PEKING, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-2.83	-2.80	-2.95	-2.92	-3.05	-2.92	-2.24	-2.02	-2.77	-3.03	-2.39	-2.64	-2.71
1	-3.01	-3.54	-3.54	-3.59	-3.74	3.55	-2.65	-2.64	-3.10	-3.65	-2.87	-3.18	-3.25
2 .	-3.37	-3.84	-4.03	-3.98	-4.08	-3.97	-2.58	-2.90	-3.38	-3.96	-3.07	-3.41	-3.57
3	-3.40	-3.94	-4.12	-4.06	-4.24	-4.00	-2.85	-2.94	-3.44	-3.97	-2.88	-2.74	-3.58
4	-2.88	-3.65	-3.92	-3.86	-4.03	-3.74	-2.74	-2.79	-3.06	-2.43	-2.23	-2.50	-3.15
5	-1.79	-2.83	-3.21	-3.24	-3.65	-3.31	-2.36	-2.20	-2.34	-2.34	-1.18	-1.34	-2.48
	0.00	0	0.00	0.04		0.11					0.50	0.04	
6			71110			7/1			111111111111111111111111111111111111111	to be a second	111111111111111111111111111111111111111	-0.64	200
7	-0.48	-0.15	-1.05	-1.13	-1.18	-1.21	-0.72	-0.45	-0.50	-0.54	-0.48	-0.26	-0.68
. 8	-0.02	-0.27	-0.30	-0.33	-0.19	-0.11	0.12	0.08	0.09	-0.02	0.01	0.18	-0.06
9	0.30	0.26	0.26	0.24	0.59	0.59	0.63	0.51	0.57	0.42	0.30	0.54	0.43
10	0.57	0.73	0.83	0.84	1.15	1.14	1.04	0.83	0.97	0.86	0.59	0.77	0.86
11	0.90	1.20	1.30	1.28	1.67	1.65	1.35	1.18	1.32	1.00	0.81	1.01	1.22
Mean.	-3.57	-2.04	3.42	9.66	15.83	19.61	21.27	19.30	15.68	9.61	1.79	-2.44	

#### XXIX.

Siberia. — Nertchinsk. Lat. 51° 18′ N. Long. 117° 20′ E. Gr. — Dove.

200		A Wal			D	egrees o	Reaum	ur.				100	100
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.78	1.38	1.92	2.53	3.10	3.13	2.63	2.51	2.12	1.66	0.96	0.75	1.96
1	1.06	1.61	2.25	2.95	3.71	3.55	3.00	2.87	2.58	1.98	1.22	0.94	2.31
2	1.24	1.84	2.65	3.36	4.20	3.98	3.34	3.25	2.93	2.27	1.42	1.16	2.64
3	1.45	2.15	3.02	3.75	4.78	4.32	3.64	3.57	3.28	2.57	1.70	1.33	2.96
4	1.70	2.40	3.38	4.09	5.04	4.29	3.86	3.79	3.62	2.80	1.91	1.45	3.19
5	1.93	2.72	3.70	4.15	3.97	3.27	3.17	3.68	3.97	3.00	2.06	1.63	3.10
6	2.08	2.94	3.89	2.96	2.31	2.03	1.99	2.61	3.63	3.16	2.15	1.76	2.63
7	2.26	3.00	2.88	1.43		0.74	1.01	1.31	2.07	2.46	2.35	1.95	1.86
8	2.20	1.82	1.36	0.19		-0.45	# 15-15	0.11	0.66	0.84	1.61	1.98	0.71
9	0.56					-1.59	-1-2-1		-0.72	-0.69	-0.03	0.62	
10	-0.96	-1.27				-2.52	10.00	-2.10	-1.99	-1.82	-1.17	-0.89	-1.80
11	-1.90	-2.34	-2.61				-2.79				-2.12	-1.85	-2.65
Noon.	-2.70	-3.16	-3.43	-3.70	-3.82	-3.62	-3.28	-3.49	-3.71	-3.41	-2.84	-2.58	-3.31
1	-3.06						-3.58			- TO TO THE			
2	-3.00						-3.66		The second second	Carry and	-2.97		
3							-3.48		-3.86	113000	-2.27		-3.33
4							-3.02		-3.34	-2.43	-1.34	-0.96	-2.70
5	-0.71	-1.61	-2.75	-2.85	-3.02	-3.73	-2.38	-2.56	-2.48	-1.42	-0.87	-0.43	-1.98
6	-0.28	-0.63	-1.71	-1.97	-2.27	-2.06	-1.73	-1.68	-1.22	-0.50	-0.10	-0.17	-1.20
7	0.02			-0.34		1 - 3 - 3	-0.82	-0.66	-0.49	-0.24	-0.17		-0.47
8	0.13	0.39	0.24	0.61	0.27	0.97	THE PERSON	0.41	0.34	0.30	0.06	0.08	0.29
9	0.27	0.63	0.66	1.19	1.34	1.32	1.24	1.30	0.89	100000000000000000000000000000000000000	0.34	0.22	0.84
10	0.43	0.86	1.06	1.72	1.92	2.02	1.78	1.70	1.30	1.01	0.54	0.43	1.23
11	0.57	1.16	1.47	2.17	2.63	2.63	LANGUAGE CO.	2.14	1.71	1.31	0.75	0.56	1.62
Mean.	-21.94	-17.94	-8.35	0.04	7.51	1.78	13.91	11.91	6.55	-1.80	-13.44	-21.36	1

SIBERIA. - NERTCHINSK. Lat. 51° 18' N. Long. 119° 21' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					208.0	00 01 100	-							
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
Morn. 1	0.91	1.42	2.07	2.69	4.07	4.29	3.07	3.00	2.16	2.31	0.76	0.66	2.28	
					0.000	77 HE TEST				1373675				
NAME OF THE PARTY OF			-	100	1 D47600			- 120 L		V.2-525WV.Z		1		
			1 2000	1 . D. Con	111111111111111111111111111111111111111		The state of the s	TANK TO SE	7710000000	111111111111111111111111111111111111111			3.04	
4	1.42	2.52	3.63	3.97	4.98	4.70	3.76	4.04	3.81	3.61	1.66	1.07	3.26	
5	1.78	2.84	3.73	3.69	4.24	3.96	3.37	3.72	3.94	3.66	2.06	1.41	3.20	
6	2.07	2.80	3.28	2.88	2.86	2.67	2.54	2.89	3.15	3.30	2.30	1.75	2.71	
7	2.06	2.28	2.31	1.63	1.07	0.99	1.37	1.62	2.38	2.47	2.18	1.87	1.85	
8	1.60	1.28	0.99	0.16	- O. JOSH	-0.79	0.06	0.15	0.87		1.58	1.59	0.66	
	F. S	100	S LYTE		12	1 5 6	100			alle .	ALL I	MILIE		
9	0.65	-0.05	-0.41	-1.26	-2.33	-2.34	-1.19	-1.25	-0.70	-0.23	0.55	0.87	-0.64	
10	-0.59	-1.43	-1.67	-2.42	-3.40	-3.41	-1.98	-2.38	-1.74	-1.70	-0.69	-0.17	-1.80	
11	-1.79	-2.58	-2.64		Non-Section 1			A Committee of the Comm			-1.84	-1.23	-2.77	
										100000000000000000000000000000000000000		1		
2.0011			0.20	0.01	1.10		0.00	0.01	0.40	0.04		1	0.01	
1	-2.87	-3.49	-3.61	-3.76	-4.22	-4.05	-3.64	-3.83	-3.69	-4.25	-2.81	-2.30	-3.54	
2	17 17 16 16	0.5				- CO-1101	-3.72	The contract of		-22 01	APRIL DESCRIPTION			
3	2000	-2.76		1 5 5 1 V 2 5 5			-3.62				DE LA TON	-1.54		
4		-2.12					-3.29			7907 Aur 2012		40.00		
7	1.14	2.12	70.01	-2.04	-3.09	-0.04	-3.23	-0.40	-5.24	-3.00	1.11	0.32	2.00	
5	-0.56	-1.45	-2.65	-2 17	-3 04	-3.07	-2.68	-2.76	-2.68	-2.24	-0.61	-0.47	-2.03	
6	-0.23		-1.78		ACC.		-1.82				-0.27		-1.31	
7	-0.11									14 12 2 11 11	Table 1	-0.23		
		0.00		-	100,000,000	-	-0.81		100	0.5955		The state of the s	0.000	
8	-0.04	0.31	0.18	0.20	0.26	0.00	0.20	0.24	0.17	0.17	-0.25	-0.24	0.12	
9	0.09	0.74	0.90	0.82	1.29	1.21	1.06	1.11	0.97	0.74	0.05	-0.17	0.73	
10	0.31	1.02		A DOME	Carlo Colo	2.25	A STATE OF	A POST OF THE PARTY			0.20	0.02	1.18	
		14000	1.34	1.29	2.11		1.51	1.74	1.17	1.18			4/1/200	
11	0.57	1.19	1.56	1.71	2.78	3.09	2.23	2.19	1.73	1.54	0.39	0.28	1.61	
Midn	0.78	1.29	1.76	2.15	3.41	3.75	2.65	2.57	1.88	1.90	0.58	0.52	1.94	
ton Thurs	SELL	WANG	3	300		WE YE							310	
6. 6	0.92	1.00	0 ==	'0 ==	0.00	0.10	0.96	0.50	0 80	0.00	1.01	0.75	0.70	
DESCRIPTION OF THE PROPERTY OF	Leave Value		0.75	0.75	27 14 14 14					0.97	1.130	0.000		
7. 7	0.98	1.04	0.77	0.53		-0.12	0.28	400	0.76	0.97	1.03	0.82	0.63	
8. 8	0.78	0.80	0.58		-0.26		0.13	0.20	0.52	0.71	0.77	0.67	0.39	
9. 9	0.37	0.34	0.24	1000000	-0.52	All the second	-0.06	-0.07	0.13	0.26	0.30	0.35	0.05	
10.10	-0.14	-0.20	-0.16	-0.57	-0.65	-0.58	-0.24	-0.32	-0.29	-0.26	-0.25	-0.07	-0.31	
w 0 0	0.74	0.00	0.70	0.40	0.03	0 ==	0.40	0.00	0.00	0.00	0.00	0.10	-0.00	
7. 2. 9	-0.14						-0.43	100						
6. 2. 8	100000000000000000000000000000000000000				COLUMN LAND	VALUE OF COORS	-0.33			741/15				
6. 2.10	-0.06	0.18	0.29	0.17	0.26	0.33	0.11	0.25	0.11	0.09	CONTRACTOR OF	-0.01	0.14	
6. 2. 6	-0.24	-0.43	-0.75	-0.72	-1.13	-1.18	-1.00	-0.95	-0.80	-0.75	-0.16	-0.19	-0.69	
~ 0	0.4-	0.0-	0.0-	0.00	1	1 00	1		0.00	0.00	0.00	0.00	0.05	
7. 2		TATION OF STREET	A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		10 GL W		-1.14		Annual Control	THE RESERVE AND ADDRESS OF THE PARTY OF THE	ALC: NO COLUMN	THE PERSON NAMED IN		
8. 2	The second	10000			The same of	150000000000000000000000000000000000000	-1.78		100	APRIL 7755	40.00			
8. 1	The second second	1000		The second second		100.000.000	-1.79			A COLUMN TO A COLU	and the second second	the Committee of the Co		
7. 1	-0.25	-0.50	-0.72	-1.01	-1.56	-1.47	-1.18	-1.13	-0.81	-0.87	-0.16	-0.11	-0.81	
0.10.00				NAME OF			1 3	1		is at				
9.12.3.9	-0.48						-1.83							
7. 2.2(9)	-0.08	0.12	0.09	-0.09	-0.13	-0.13	-0.06	-0.01	0.08	-0.04	-0.05	-0.14	-0.04	
D-11	0 10	0.00	0.03	0.11	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.74	
Dail.ext.	-0.40	-0.33	-0.01	-0.11	0.43	0.39	0.02	0.08	-0.03	-0.30	-0.26	-0.22	-0.14	
A Date Library	(TO)											W. W. H.		

#### XXXI.

## Siberia. — Barnaul. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

1000	2010				Degre	es of Fe	hrenhei						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
					0.00	- 00	0.00		- 1-	0.00	0.40		
Morn. 1	2.54	1000				7.83		7.11	5.45	3.06	2.48	1.82	4 95
2	2.81	2.14	5.47	6.30	177	8.87		8.35	6.50		2.97	2.00	5.76
3	2.70		6.28	7.07		9.59		9.52	7.65	4.52	3.35	2.07	6.41
4	2.39	2.81	7.02	7.45	10.76	9.14	10.67	10.15	8.48	5.15	3.71	2.18	6.66
	0.00	0.70	- 10	m 00	0.00	0	0.50	0 ==	0.00		1		0.00
5	2.07	3.13	7.43	7.09	9.32	7.58	9.50	9.77	8.60	5.47	4.01	2.45	6.37
6	1.96	7.00	9.38	5.87	6.68	5.45	7.18	8.12	5.58		1002 500		5.65
7	2.00	3.20	5.90	3.87	3.38	2.50	4.05	5.36	2.70	4.46	3.96	13- 500	3.94
8	1.98	2.59	3.71	1.37	-0.11	-0.18	0.70	1.96		2.97	3.15	2.70	1.96
9	1.53	1.37	0.86	-1 28	-3.02	-2.48	-2.32	-1 44	-0.56	0.99	1.64	1 72	-0.25
10	0.45	-0.36	-2.18		-5.06				1 THOU INC.			0.11	
11	-1.22	-2.30			-6.35			-6.48		T I A CONTRACT		23 - 6 5	
Noon		-4 03	4 35 / 13%	<b>-7.34</b>		- Company 1		-7.97		WARRANT - 19.	And the last of th	The late of the	-6.01
Noon.	-5.00	-4 09	-0.09	-1.04	-7.20	-1.51	-1.52	-1.91	-1.99	-5.00	-4.45	-3.42	-6.01
1	-4.59	-5.13	-7 97	-8.35	-8.03	-8.39	-8.42	-8.96	-8.96	-6.05	-5.58	-4.39	-7.07
2	-5.27		-8.21			T (0.11) NO		-9.63					
3	-4.93	-4.77	1	-8.39		-8.91	-9.56		-8.82			-3.78	-7.27
4				75 5				-9.50	111111111111111111111111111111111111111			285 500	
			0.01		0.00	0.01	0.00	0.00	,	0.22	0.00	2.00	0.40
5	-2.25	-2.14	-5.65	-5.58	-8.66	-6.32	-8.35	-8.28	-6.26	-4.05	-2.57	-1.60	5.15
6	-0.90	-0.83	-6.46	-3.35	-6.82	-4.39	-6.48	-6.19	-4.25	-2.75	-1.55	-0.83	-3.74
7	0.02	0.09			-4.16		A	-3.51	F . 78 . 7	100 ME - 33 -		HEROTOPINE	
8	0.47	0.63	-0.97	1.04	-1.31	0.11	100	-0.68	2023254	-0.36	-0.41	1000	-0.25
	11		7			31.0	Paul						
9	0.70	0.92	0.63	2.61	1.46	1.80	1.24	1.80	1.76	0.54	0.00	0.00	1.13
10	0.95	1.10	2.00	3.62	3.78	3.49	3.38	3.67	2.99	1.28	0.52	0.38	2.27
11	1.42	1.28	3.13	4.25	5.69	4.75	5.20	4.97	3.85	1.87	1.15	0.92	3.22
Midn	2.03	1.55	3.98	4.82	7.36	6.26	6.82	6.03	4.59	2.45	1.85	1:44	4.10
	6.00	78 1-1				2 1	40						
6. 6	0-4	1 21	7 10					4					
	0.54	1.24	1.46		-0.07	0.54	0.34	0.97	1.69	1.28	1.31	0 99	0.97
7. 7	1.01	1.64	1.64		-0.41	0.27	0.02	0.92	1.76	1.49	1.55	1 28	1.06
8.8	1.24	1.62	1.37			1	-0.29	0.65	1.35	1.31	1.37	1.24	0.86
9. 9	1.10	1.15	0.74		-0.79	100	-0.54	0.18	0.59	0.77	0.83	0.86	0.43
10.10	0.70	0.38	-0.09	-0.07	-0.63	-0.56	-0.65	-0.34	-0.34	0.05	0.07	0.25	-0.11
7. 2. 9	-0.86	-0.43	-0.56	-0.74	_1 91	1 40	1.00	0.00	0.00	0.42	0 -0	0.50	-0.61
6. 2. 8	-0.95				-1.31					-0.47	-0.59		-0.81
6. 2.10		-0.47 $-0.32$	1.649.20		-1.13						-0.65		-0.70
6. 2. 6	-1.10		1.06	0.27	0.56	0.05	0.47	0.72	0.47			-0.43	0.16
2.0	1.10	0.37	-1.70	-2.07	-2.97	-2.57	-2.81	-2.57	-1.94	-1.28	-1.04	0 83	-1.85
7. 2	-1.64	-1.09	-1.16	-2.42	-2.70	-3.14	-2.56	-2.14	-1.83	-0.97	-0.88	-0.75	-1.77
8. 2	-1.65	-1.40	-2 25	-3.67	-4.45	-1.18	-1.22	-3.84	-3.27	-1.71	-1.20	-0.80	-2.76
8. 1	-1.31	-1.27	-2.13	-3.49	-4.07	-4.29	-3.86	-3.50	-3.13	-1.54	-1.22	-0.85	-2.56
7. 1	-1.30	-0.97	-1.04	-2.24	-2.33	-2.95	-2.19	-1.80	-1.69	-0.80	-0.81	-0.70	-1.57
	1	(I)		10.9		STREET, STREET	CION I	32 - 3	1	E	1		(1) (7) (F)
9.12.3.9	-1.45	-1.62	-3.29	-3.60	-4.55	-4.23	-4.55	-4.37	-3.92	-2.39	-1.96	-1.37	-3.11
7. 2.2(9)	-0.47	-0.09	-0.27	0.09	-0.63	-0.68	-0.65	-0.18	-0.05	-0.23	-0.45	-0.38	-0.34
Doi!	1.04			Just S.		1,00	The Late		134	1		7.3	5736
Dail. ext.	-1.24	-1.04	0.59	-0.63	0.74	0.34	0.56	0.14	-0.32	-0.47	-0 79	-0.74	-0.41
											1		-

#### XXXII.

## SIBERIA. - BARNAUL. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Dogra	00 01 100	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
						20.10			0.10	7.00	- 10	0.01	0.00
Morn. 1	1.13	0.82	2.09	2.44	3.92	3.48	1	1	2.42	25-001	1.1100.000	000	2.20
2	1.25	0.95	2.43	2.80		3.94	4.34	3.71	2.89	1.68	1.32	26 123	2.56
3	1.20	1.10	2.79	3.14	4.87	4.26	12 3 5 8 7 D V	A CONTRACTOR	3.40	2.01	1.49	100000	2.85
4	1.06	1.25	3.12	3.31	4.78	4.06	4.74	4.51	3.77	2.29	1.65	0.97	2.96
5	0.92	1.39	3.30	3.15	4.14	3.37	4.22	4.34	3.82	2.43	1.78	1.09	2.83
6	0.87	1.48	4.17	2.61	2.97	2.42	3.19	1000	3.40	2.35	1.85	The second second	2.51
7	0.89	1.42	2.62	1.72	1.50	1.11	1.80	100	2.48	1.98	1.76	1 10 5 -	1.75
8	0.88	1.15	1.65	0.61	-0.05	-0.08	0.31	0.87	1.20	1.32	1.40	1.20	0.87
all - Line	000		47.89		1-133	1/2/3	4		3-1-1		40.75		
9	0.68		0.38				-1.03		-0.25		0.73	0.77	-0.11
10	0.20	4 - 17 - 1		THE REAL PROPERTY.	0.0000000		1	-1.92	CHEST COL	The second			
11	-0.54		1000	1 200	THE COUNTY SERVICE	4.0	-2.82	0.00.00.00		11000	5.40	100	
Noon	-1.37	-1.79	-3.06	-3.26	-3.20	-3.25	-3.34	-3.54	-3.55	-2.22	-1.99	-1.52	-2.67
1	_2 04	-2.28	_2 54	_9 77	_9 57	_9 79	_2 74	-3.98	_9 00	_9 60	_9 40	-1.95	_2 14
2		110000000000000000000000000000000000000	THE PARTY		TO 1-18 770	- Transition	THE RESERVE	-3.98 -4.28				-1.99	-3.14 -3.32
3	-2.19		-3.45		The second second			-4.39	1000			-1.68	-3.23
4		1000000	-750		0-100 BURGO			-4.22	- 4-8	7/20/11	10000000	-1.19	-2.87
4	1.00	-1.90	-5.04	9.20	-4.22	3.00	4.10	4.22	-3.47	4.04	1.41	-1.13	-2.01
5	-1.00	-0.95	-2.51	-2.48	-3.85	-2.81	-3.71	-3.68	-2.78	-1.80	-1.14	-0.71	-2.29
6	-0.40	-0.37	-2.87	-1.49	-3.03	-1.95	-2.88	-2.75	-1.89	-1.22	-0.69	-0.37	-1.66
7	0.01	A TENER OF A STATE OF	-1.16	-0.46	THE PARTY NAMED IN		1.11	-1.56	100000000000000000000000000000000000000		10 PORT NO.	-0.19	
8	0.21	0.28	-0.43	0.46	-0.58	0.05	-0.58	-0.30	0.01	-0.16	-0.18	-0.10	-0.11
44.7	1,807.00		0.58	1		4 37	Le sit		8121	4.0	Her	OF A	200
9	0.31	0.41	0.28	1.16	0.65	0.80		0.80	0.78	0.24	0.00		0.50
10	0.42	0.49	0.89	1.61	1.68	1.55	1.50	1.63	1.33	0.57	0.23	0.17	1.01
11	0.63	0.57	1.39	1.89	2.53	2.11	2.31	2.21	1.71	0.83	0.51	0.41	1.43
Midn	0.90	0.69	1.77	2.14	3.27	2.78	3.03	2.68	2.04	1.09	0.82	0.64	1.82
		in a			on w			T W	N		May!		
6. 6	0.24	0.55	0.65	0.56	-0.03	0.24	0.15	0.43	0.75	0.57	0.58	0.44	0.43
7. 7	0.45	0.73	0.73		-0.18	0.12		0.41	0.78	0.66	0.69	0.57	0.47
8. 8	0.55	0.72	0.61	. V.	-0.32	-0.02	30000	0.29	0.60	0.58	0.61	0.55	0.38
9. 9	0.49	0.51	0.33	The Country of the	-0.35	-0.15	12.00	0.08	0.26	0.34	0.37	0.38	0.19
10.10	0.31	0.17	-0.04	COLUMN TO SERVICE AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON AND ADDRESS OF T	-0.28	-0.25		-0.15	-0.15	0.02	0.03	0.11	-0.05
				10.3	Paral.				201		The same	17	CENTRAL PROPERTY.
7. 2. 9	-0.38	-0.19	-0.25	-0.33	-0.58	-0.66	-0.57	-0.37	-0.28	-0.21	-0.26	-0.22	-0.36
6. 2. 8	-0.42	-0.21	0.03	-0.27	-0.50	-0.48	-0.49	-0.32	-0.23	-0.22	-0.29	-0.28	-0.31
6. 2.10	-0.35	-0.14	0.47	0.12	0.25	0.02	0.21	0.32	0.21	0.03	-0.15	-0.19	0.07
6. 2. 6	-0.62	-0.43	-0.78	-0.92	-1.32	-1.14	-1.25	-1.14	-0.86	-0.57	-0.46	-0.37	-0.82
7. 2	0 ***	-0.40	-0 50	_1 00	_1 00	_1 40	_1.14	_0.05	0.03	_0.49	0.00	0.00	0 =0
8. 2		-0.49 $-0.62$	THE COLD	-1.80	7-10-1-127	THE RESERVE		-0.95			THE RESIDENCE OF	-0.33	
8. 1	- 2000	-0.62 $-0.57$	The Second Street Street	-1.55	The second second	1.000	11 Table 10 April 10	-1.71 -1.56		C-10-10-10-10-10-10-10-10-10-10-10-10-10-		1001101101	
7. 1	1	No. of Street,	7 to 60 cm, 1 to 1 cm	7 3 11 5 5 1	1.357	COLUMN TO A		-0.80					
	0.00	0.40	0.40	1.00	1.04	1.01	0.91	0.00	0.19	0.00	0.00	-0.91	-0.70
9.12.3.9	-0.64	-0.72	-1.46	-1.60	-2.02	-1.88	-2.02	-1.94	-1.74	-1.06	-0.87	-0.61	-1.38
7. 2.2(9)	-0.21	-0.04	-0.12					-0.08					
			View I				. 311.5						
Dail.ext.	-0.55	-0.46	0.26	-0.28	0.33	0.15	0.25	0.06	-0.14	-0.21	-0.35	-0.33	-0.18

#### XXXIII.

SIBERIA. - BARNAUL. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Dammaga	06	Reaumur.	

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.99	1.98	2.43	2.65	3.70	3.75	3.48	3.10	2.80	1.99	1.06	0.77	2.39
1	1.15	2.21	2.77	3.03	4.11	4.30	4.07	3.50	3.20	2.24	1.22	0.86	2.72
2	1.26	2.36	3.13	3.24	4.47	4.83	4.49	3.90	3.63	2.50	1.39	0.95	3.00
3	1.41	2.47	3.34	3.49	4.72	4.95	4.77	4.29	3.92	2.69	1.46	1.01	3.21
4	1.56	2.56	3.61	3.59	4.20	4.41	4.40	4.23	4.11	2.89	1.51	1.07	3.18
5	1.55	2.68	3.70	2.78	2.85	3.12	3.34	3.60	3.90	2.91	1.57	1.10	2.76
6	1.61	2.69	2.90	1.58	1.44	1.75	1.88	2.29	3.06	2.68	1.59	1.09	2.05
7	1.53	2.30	1.63	0.46	0.28	0.49	0.50	0.85	1.54	1.84	1.50	1.18	1.17
8	0.94	1.15	0.13	-0.69	-0.80	-0.65	-0.54	-0.51	-0.08	0.87	0.95	0.93	0.14
9	0.27	-0.47	-1.35	-1.80	-1.94	-1.78	-1.81	-1.79	-1.62	-0.73	-0.03	0.11	-1.08
10	-0.79	-1.90	-2.36	-2.68	-2.71	-2.75	-2.70	-2.80	-2.84	-1.96	-1.12	-0.83	-2.12
11	-1.69	-2.95	-3.31	-3.27	-3.39	-3.39	-3.44	-3.41	-3.75	-2.81	-1.93	-1.62	-2.91
Noon.	-2.35	-3.89	-3.78	-3.66	-3.73	-3.98	-3.90	-3.81	-4.19	-3.48	-2.42	-2.04	-3.44
1	-2.61	-4.25	-4.11	-3.68	-4.04	-4.19	-4.09	-4.11	-4.41	-3.72	-2.57	-2.12	-3.66
2	-2.39	-4.23	-4.07	-3.65	-4.13	-4.34	-4.21	-4.10	-4.34	-3.64	-2.39	-1.70	-3.60
3	-1.88	-3.62	-3.69	-3.39	-4.09	-4.19	-3.89	-3.91	-4.11	-3.17	-1.66	-1.09	-3.22
4	-1.19	-2.30	-2.67	-2.62	-3.51	-3.57	-3.65	-3.68	-3.21	-2.53	-1.05	-0.76	-2.56
5	-0.81	-1.30	-1.69	-1.82	-3.09	-3.04	-3.07	-2.78	-2.29	-1.49	-0.71	-0.53	-1.89
6	-0.41	-0.56	-0.84	-0.62	-1.92	-2.19	-2.09	-1.54	-1.05	-0.72	-0.33	-0.28	-1.05
7	-0.20	0.09	0.35	0.27	-0.46	-0.84	-0.69	-0.20	-0.17	-0.08	-0.03	-0.02	-0.17
8	0.12	0.69	0.39	0.99	0.77	0.51	0.52	0.67	0.60	0.31	0.23	0.19	0.50
9	0.32	1.08	0.88	1.50	1.64	1.48	1.42	1.46	1.26	0.82	0.42	0.39	1.06
10	0.73	1.47	1.46	2.02	2.42	2.31	2.22	2.04	1.85	1.29	0.58	0.58	1.58
11	0.78	1.76	1.92	2.35	3.11	3.05	2.88	2.58	2.36	1.68	0.83	0.75	2.00
Mean.	-14.71	-13.47	-5.47	1.77	7.78	13.62	14.98	12.76	7.53	1.58	-8.36	-13.07	4.94

The numbers without sign must be added; those with the sign - must be subtracted.

TO BE BY THE SECOND SECOND SECOND

## HOURLY CORRECTIONS

FOR

PERIODIC VARIATIONS.

EUROPE.

the two detectors are a frequency of the way to be a supplied to the the state of the s

#### XXXIV.

## ITALY. - ROME. Lat. 41° 54' N. Long. 12° 25' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Morn. 1						Degree	s of Re	wantar.						
1.14   1.68   1.96   2.31   2.56   2.47   2.49   1.91   1.75   1.29   1.02   1.76	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
1.14   1.68   1.96   2.31   2.56   2.47   2.49   1.91   1.75   1.29   1.02   1.76				The L		7					1		Post in	
1.14   1.58   1.96   2.31   2.56   3.02   2.99   3.00   2.38   2.12   1.53   1.19   2.15	Morn. 1	0.90	1.08	1.22	1.55	1.88	2.44	2.17	2.20	1.63	1.50	1.15	0.93	1.55
1.60   2.36   2.80   3.07   3.00   3.51   3.68   3.54   2.91   2.58   1.87   1.43   2.60	2	0.99	1.26	1.50	1.84	2.10	2.59	2.41	2.49	1.91	1.75	1.29	1.02	1.76
5	3	1.14	1.58	1.96	2.31	2.56	3.02	2.99	3.00	2.38	2.12	1.53	1.19	2.15
6   1.77   2.52   2.76   2.92   3.04   3.36   3.81   3.53   3.17   3.10   2.42   1.87   2.86   7   1.74   2.33   2.24   2.25   2.19   2.38   2.82   2.62   2.58   2.82   2.25   2.33   1.83   2.34   3.8   1.40   1.73   1.29   1.15   0.93   0.98   1.27   1.22   1.51   2.05   1.82   1.47   1.40   9   0.72   0.78   0.10   -0.15   -0.47   -0.51   -0.44   -0.35   0.15   0.86   0.93   0.78   0.20   10   -0.24   -0.35   -1.08   -1.39   -1.68   -1.75   -1.89   -1.78   -1.23   -0.58   -0.22   -0.15   -1.03   11   -1.27   -1.54   -2.06   -2.36   -2.53   -2.59   -2.87   -2.84   -2.41   -2.00   -1.41   -1.14   -2.09   Noon.   -2.15   -2.49   -2.71   -2.98   -3.01   -3.08   -3.38   -3.49   -3.24   -3.14   -2.39   -1.99   -2.84     1   -2.69   -3.07   -3.02   -3.27   -3.23   -3.40   -3.61   -3.81   -3.70   -3.82   -3.00   -2.52   -3.26   2   -2.78   -3.25   -2.45   -2.72   -3.14   -4.05   -3.88   -3.62   -3.11   -3.04   -2.41   -1.95   -2.89     -1.11   -1.81   -1.89   -2.15   -2.70   -3.70   -3.58   -3.05   -2.38   -2.21   -1.76   -1.35   -2.30     -2.52   -3.44   -0.53   -0.84   -1.42   -1.38   -1.01   -0.51   -0.50   -0.48   -0.24   -0.64     -0.64   -0.54   -0.54   -0.54   -0.54   -0.54   -0.54   -0.54   -0.54   -0.54   -0.55   -0.54   -0.55   -0	4	1.36	1.99	2.46	2.80	3.06	3.51	3.68	3.54	2.91	2.58	.1.87	1.43	2.60
Total   1.74   2.33   2.24   2.25   2.19   2.38   2.82   2.62   2.58   2.82   2.33   1.83   2.34   8   1.40   1.73   1.29   1.15   0.93   0.98   1.27   1.22   1.51   2.05   1.52   1.47   1.40   9   0.72   0.78   0.10   -0.15   -0.47   -0.51   -0.44   -0.35   0.15   0.56   0.93   0.78   0.20   0.00	5	1.60	2.36	2.80	3.07	3.30	3.71	4.06	3.79	3.25	2.96	2.22	1.70	2.90
8	6	1.77	2.52	2.76	2.92	3.04	3.36	3.81	3.53	3.17	3.10	2.42	1.87	2.86
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7	1.74	2.33	2.24	2.25	2.19	2.38	2.82	2.62	2.58	2.82	2.33	1.83	2.34
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	1.40	1.73	1.29	1.15	0.93	0.98	1.27	1.22	1.51	2.05	1.82	1.47	1.40
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	0.72	0.78	0.10	-0.15	-0.47	-0.51	-0.44	-0.35	0.15	0.86	0.93	0.78	0.20
Noon.   -2.15   -2.49   -2.71   -2.98   -3.01   -3.08   -3.38   -3.49   -3.24   -3.14   -2.39   -1.99   -2.84     1	10	-0.24	-0.38	-1.08	-1.39	-1.68	-1.75	-1.89	-1.78	-1.23	-0.58	-0.22	-0.15	-1.03
1	11	-1.27	-1.54	-2.06	-2.36	-2.53	-2.59	-2.87	-2.84	-2.41	-2.00	-1.41	-1.14	-2.09
2	Noon	-2.15	-2.49		THE POST	The state of the s				4				1
2	1	-2.69	-3.07	-3.02	-3.27	-3.23	-3.40	-3.61	-3.81	-3.70	-3.82	-3.00	-2.52	-3.26
3	2	1	2000	2000	A STATE OF THE STA	100	CONTRACT PROPERTY.		Contract to the		DIAMETER OF			100
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1		ALC: NO INC.	1 2 25 35 37 3			25 100 100	1000000				1771	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4			The second	The second second		Automatical Association							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	-1.11	-1.81	-1.89	-2.15	-2.70	-3.70	-3.53	-3.05	-2.38	-2.21	-1.76	-1.35	-2.30
8         0.39         0.25         0.26         0.30         0.29         0.13         0.08         0.21         0.38         0.19         0.05         0.17         0.23           9         0.59         0.67         0.78         0.94         1.22         1.46         1.33         1.22         1.05         0.71         0.46         0.46         0.91           10         0.71         0.90         1.07         1.31         1.76         2.29         2.10         1.86         1.43         1.05         0.76         0.66         1.33           11         0.78         0.99         1.15         1.44         1.93         2.57         2.33         2.11         1.54         1.24         0.95         0.79         1.49           Midn.         .         0.84         1.02         1.15         1.46         1.88         2.51         2.24         2.14         1.55         1.49         0.66         0.85         0.89         0.67         0.56         0.67           7. 7         0.90         1.00         0.90         0.86         0.68         0.48         0.72         0.81         1.12         0.94         0.82         0.81           8. 8 <td>6</td> <td>-0.45</td> <td>-1.05</td> <td>-1.20</td> <td>-1.39</td> <td>-1.91</td> <td>-2.79</td> <td>-2.67</td> <td>-2.18</td> <td>-1.48</td> <td>-1.32</td> <td>-1.09</td> <td>-0.75</td> <td>-1.52</td>	6	-0.45	-1.05	-1.20	-1.39	-1.91	-2.79	-2.67	-2.18	-1.48	-1.32	-1.09	-0.75	-1.52
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7	0.05	-0.34	-0.44	-0.53	-0.84	-1.42	-1.38	-1.01	-0.51	-0.50	-0.48	-0.24	-0.64
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	0.39	0.25	0.26	0.30	0.29	0.13	0.08	0.21	0.38	0.19	0.05	0.17	0.23
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	0.59	0.67	0.78	0.94	1.22	1.46	1.33	1.22	1.05	0.71	0.46	0.46	0.91
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	10	0.71	0.90	1.07	1.31	1.76	2.29	2.10	1.86	1.43	1.05	0.76	0.66	1.33
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	0.78	0.99	1.15	1.44	1.93	2.57	2.33	2.11	1.54	1.24	0.95	0.79	1.49
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Midn	0.84	1.02	1.15	1.46	1.88	2.51	2.24	2.14	1.55	1.36	1.06	0.86	1.51
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					11				Sec.					- pur
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6. 6	0.66	0.74	0.78	0.76	0.57	0.28	0.57	0.68	0.85	0.89	0.67	0.56	0.67
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						200	100000	1/4/10/10		100000000000000000000000000000000000000				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1795.00	100		7190000	The second of	12-17-73-73		1 1 Gen (A.)	The second second		PER STATE		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		The same of the	-		THE RESERVE AND ADDRESS.	TO SALES	THE PERSON NAMED IN		Carrier Land				1000000	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	The second second second	10000	LIN AL	J. J. S.	The Land of	the field the sale of	The same of		Contract of the Contract of th	THE RESERVE	1000	The same of		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7. 2. 9	-0.15	-0.08	-0.01	-0.03	0.03	0.05	0.13	-0.03	-0.06	-0.15	-0.12	-0.12	-0.05
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	THE RESERVE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAME	The Carlo State of the Carlo		A COLOR OF THE PARTY		The second second	The state of the s	SACATE !	307.00	A COLUMN TWO IS NOT THE OWNER.	100 100 100		1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				1000000	1100000	V 420 T 175-1	The second second	1 0000000	1 Charles   100 cm	Contract of	Fig. Con., other 1	The same of the same	The second	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	the state of the s	100-00		Contract Con-	- MOV- AL	1000000	7 ( 100 )	1.00			A LONG TO	Contract of the Contract of th	13 A 30 A 4	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7. 2	-0.52	-0.46	-0.40	-0.52	-0.56	-0.66	-0.47	-0.65	-0.61	-0.59	-0.42	-0.42	-0.52
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	CONTRACTOR OF THE	-0.00		The second second		110000000000000000000000000000000000000				The second second	The second second			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	The state of the s		Table 1271				THE RESERVE TO SERVE	The state of the s		NOT SET	110 March 2007			
7. 2.2(9) 0.04 0.11 0.19 0.21 0.33 0.40 0.43 0.29 0.22 0.06 0.02 0.02 0.19	The same was you		00000	Charles and the		Charles of Marie	to officially the second		Control of the last	and the same of th	and the same	The State of the S	William Cont. 18	
7. 2.2(9) 0.04 0.11 0.19 0.21 0.33 0.40 0.43 0.29 0.22 0.06 0.02 0.02 0.19	0.10.00	0.00	1.00	1.10	1.00	7 00	1	1 00	1 00		1.00	0.00	0.00	7.00
		0.00	- CAN	1	100	10.00	1,1100000	100	2500000		Contract to the	The second		
Dail.ext.   -0.51 -0.37 -0.12 -0.11 -0.01 -0.17  0.09 -0.07 -0.28 -0.45 -0.37 -0.40 -0.25			65	100	Total Control	500		12.5						
	Dail.ext.	-0.51	-0.37	-0.12	-0.11	-0.01	-0.17	0.09	-0.07	-0.28	-0.45	-0.37	-0.40	-0.25

### XXXV.

# ITALY. - PADUA. Lat. 45° 24' N. Long. 11° 52' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						es of the							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
To design	0.50	0.55	0.00	1 00	2.43	2.21	2.86	2.27	1.59	0.86	1.04	0.83	1.45
Morn. 1	0.58		0.89		1			1 - 1 - 2	10000	1976	1)11100000	ALL PROPERTY	1-1997 770001
2	0.58		1.20	1	2.70	2.40	3.20	2.70	1.85	1.03	1.16	0.96	1.67
3	0.76	0.97	1.42	1.66	3.00	2.68	3.53	3.05	2.10	1.20	1.26	0.98	1.88
4	0.79	1.13	1.68	1.97	3.14	2.71	3.78	3.44	2.34	1.39	1.35	1.05	2.06
5	1.06	1.31	1.89	2.26	2.97	2.39	3.34	3.44	2.66	1.58	1.42	1.12	2.12
6	1.13	1.46	2.06	700	1.96	1.22	2.07	2.93	2.54	1.54	1.49	1.16	1.82
7	1.25	1.58	1.86	1.82	0.66	0.08	0.56	1.82	1.78	1.37	1.58	1.23	1.30
8	1.07	1.42	0.66		-0.23	-0.65	-0.25	0.58	0.79	0.81	0.97	1.00	0.60
	1.07	1.42	0.00	1.00	0.20	0.00	0.20	0.00	0.,0	0.01	0.01	1.00	0.00
9	0.70	0.82	0.61	0.18	-1.07	-1.24	-1.63	-1.65	-0.58	0.18	0.02	0.33	-0.28
10	0.10	-0.08	-0.83	-0.42	-1.70	-1.66	-2.29	-1.90	-1.03	-0.51	-0.81	-0.26	-0.95
11	-0.58	-0.62		-0.85		-2.23	-2.77	-2.38	DAY WAS	-0.99		2.	-1.48
Noon		-1.24	13-15 THE		-2.74		-3.16	-2.97	2.30 across	C. A. A. A. A.		-1.50	
1,001					1,				10.17		15000	AN EST	110076
1	-1.38	-1.45	-1.54	-1.68	-2.88	-2.61	-3.53	-3.34	-2.54	-1.74	-2.42	-1.90	-2.25
2	-1.51	-1.62	-1.74	-1.92	-2.94	-2.62	-3.74	-3.73	-2.84	-2.01	-2.55	-2.06	-2.44
3	-1.45	-1.65	-1.90	-2.14	-2.94	-2.59	-3.54	-3.81	-2.87	-2.04	-2.22	-1.68	-2.40
4		1000000				0.00	400		100	-1.94	A 100 TO	-1.14	-2.02
1124								I FATTY				1	
5	-0.87	-0.98	-1.39	-1.98	-2.08	-1.60	-2.44	-2.49	-1.60	-1.05	-0.73	-0.74	-1.50
6	-0.59	-0.79	-1.02	-1.51	-1.20	-1.00	-1.41	-1.34	-0.83	-0.54	-0.15	-0.33	-0.89
7	-0.32	-0.62	-0.73	-1.12	-0.26	-0.12	-0.46	-0.32	-0.18	-0.14	0.12	-0.15	-0.36
8	-0.07	-0.42	-0.43	-0.47	-0.14	0.38	1.01	0.50	-0.10	0.05	0.33	0.04	0.06
Le Maria	4		14.16										
9	0.05	-0.14	-0.10	-0.11	1.11	1.38	1.54	1.01	0.23	0.26	0.49	0.26	0.50
10	0.18	0.09	0.24	0.27	1.44	1.72	1.67	1.36	0.58	0.52	0.72	0.46	0.77
11	0.29	0.31	0.48	0.60	1.75	1.86	2.14	1.78	0.84	0.68	0.86	0.59	1.02
Midn	0.37	0.49	0.72	0.85	2.02	2.10	2.43	2.23	1.36	0.78	0.94	0.70	1.25
						-							
6.6	0.00	0.04	0.50	0.00	0.00		0.00		0.00	0.40	0.00	0.40	0.40
6. 6	0.27	0.34	0.52	0.36	0.38	0.11	0.33	0.80	0.86	0.50	0.67	0.42	0.46
7. 7	0.47	0.48	0.57	0.35	0.20	-0.02	0.05	0.75	0.80	0.62	0.85	0.54	0.47
8. 8	0.50	0.50	0.12	0.28	-0.19	-0.14	0.38	0.54	0.35	0.43	0.65	0.52	0.33
9. 9	0.38	0.34	0.26	0.04	0.02	0.07	-0.05	-0.32	-0.18	0.22	0.26	0.30	0.11
10.10	0.14	0.01	-0.30	-0.08	-0.13	0.03	-0.31	-0.27	-0.23	0.01	-0.05	0.10	-0.09
7. 2. 9	-0.07	-0.06	0.01	-0.0~	-0.39	_0.20	_0.55	0.20	0.00	. 0.19	-0.16	-0.10	-0 21
6. 2. 8	-0.15		-0.04	1500000		TALL TAKE			10.11997	-0.13		100	
6. 2.10	-0.13	-0.19		-0.06	-0.37	18.00	-0.22	-0.10	-0.13	-0.14	1000000	-0.29	-0.19
6. 2. 6		1000	0.19	0.19	0.15		-0.00	0.19	0.09		-0.11		0.05
	0.02	-0.32	-0.23	-0.40	-0.73	-0.80	-1.03	-0.71	-0.38	-0.34	-0.40	-0.41	-0.51
7. 2	-0.13	-0.02	0.06	-0.05	-1.14	-1.27	-1.59	-0.96	-0.53	-0.32	-0.49	-0.42	-0.57
8. 2			-0.54	-0.45	-1.59	-1.64	-2.00	-1.58	-1.03	-0.60	-0.79	-0.53	-0.92
8. 1	-0.16	-0.02	-0.14	-0.33	-1.56	-1.63				-0.47			
7. 1	-0 07	0.07	0.16							-0.19			
0.10.00		his III	100		35.0			1-7-1			1100	14/17	
9.12.3.9	-0.42	-0.55	-0.68	-0.84	-1.41	-1.24	-1.70	-1.86	-1 34	-0.75	-0.93	-0.65	-1.03
7. 2.2(9)	-0.04	-0.08	-0.02	-0.08	-0.02		-0.03			-0.03			
Dail.ext.	-0.13	-004	0.00	0.00	0.70	0.0			7				0.70
Dail. ext.	0.13	-0.04	0.08	0.06	0.10	0.05	0.02	-0.19	-0.11	-0.23	-0.49	-0.42	-0.16
	-	-	100		-	-							

#### XXXVI.

SWITZERLAND. - GENEVA. Lat. 46° 12' N. Long. 6° 9' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.50	0.68	1.38	1.68	2.16	2.77	2.54	2.38	1.86	1.44	0.80	0.48	1.56
1	0.62	0.83	1.88	2.14	2.72	3.32	3.19	3.08	2.41	1.71	0.97	0.54	1.95
2	0.74	1.01	2.34	2.53	3.16	3.68	3.70	3.68	2.93	1.95	1.14	0.61	2.29
3	0.83	1.22	2.70	2.76	3.40	3.74	3.89	4.03	3.34	2.14	1.30	0.70	2.50
4	0.92	1.46	2.89	2.78	3.34	3.50	3.80	4.00	3.49	2.22	1.43	0.81	2.5
5	0.98	1.66	2.83	2.54	2.93	2.88	3.26	3.52	3.30	2.14	1.51	0.91	2.3
6	1.02	1.75	2.49	2.03	2.22	2.03	2.39	2.65	2.72	1.85	1.48	0.97	1.9
7	0.97	1.66	1.90	1.33	1.28	1.05	1.38	1.54	1.84	1.34	1.26	0.92	1.3
8	0.78	1.33	1.09	0.50	0.27	0.08	0.26	0.37	0.78	0.65	0.84	0.70	0.6
9	0.46	0.74	0.17	-0.34	-0.69	-0.82	-0.71	-0.70	-0.30	-0.15	0.23	0.34	-0.1
10	-0.02	-0.01	-0.77	-1.10	-1.51	-1.57	-1.53	-1.58	-1.26	-0.98	-0.47	-0.16	-0.9
11	-0.57	-0.80	-1.61	-1.75	-2.17	-2.18	-2.24	-2.29	-2.06	-1.70	-1.14	-0.67	-1.6
Noon.	-1.06	-1.49	-2.26	-2.23	-2.66	-2.70	-2.74	-2.85	-2.66	-2.22	-1.66	-1.10	-2.1
1	-1.40	-1.98	-2.70	-2.55	-2.98	-3.10	-3.18	→3.29	-3.08	-2.53	-1.94	-1.37	-2.5
2	-1.50	-2.18	-2.87	-2.67	-3.12	-3.35	-3.48	-3.58	-3.29	-2.58	-1.94	-1.41	-2.6
3	-1.41	-2.10	-2.81	-2.61	-3.07	-3.42	-3.51	-3.65	-3.28	-2.41	-1.74	-1.26	-2.6
4	-1.14	-1.82	-2.54	-2.37	-2.80	-3.25	-3.37	-3.43	-3.04	-2.06	-1.38	-0.97	-2.3
5	-0.79	-1.37	-2.10	-1.97	-2.32	-2.78	-2.90	-2.92	-2.57	-1.59	-0.99	-0.64	-1.9
6	-0.46	-0.94	-1.59	-1.46	-1.70	-2.11	-2.22	-2.18	-1.91	-1.06	-0.62	-0.32	-1.3
7	-0.20	-0.51	-1.06	-0.90	-1.00	-1.29	-1.40	-1.31	-1.16	-0.53	-0.30	-0.07	-0.8
8	-0.01	-0.14	-0.54	-0.34	-0.29	-0.42	-0.49	-0.46	-0.42	-0.02	-0.03	0.11	-0.2
9	0.12	0.14	0.05	0.20	0.38	0.47	0.34	0.32	0.26	0.42	0.20	0.24	0.2
10	0.25	0.37	0.42	0.70	0.91	1.30	1.10	1.02	0.83	0.82	0.42	0.34	0.7
11	0.37	0.54	0.90	1.20	1.51	2.07	1.87	1.70	1.35	1.15	0.62	0.41	1.1
Mean	-0.53	1.24	3.41	6.77	10.37	13.31	14.30	13.58	11.46	7.48	3.76	0.58	187

#### XXXVII.

SWITZERLAND. — GENEVA. Lat. 46° 12′ N. Long. 6° 9′ E. Gr. — Dove.

		D	egrees of	neaum	ur.
h.	April.	May.	June.	July.	A

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.45	0.69	1.26	1.44	1.54	1.98	2.12	1.63	1.44	0.94	0.50	0.59	1.21
2	0.70	0.96	2.21	2.62	2.60	3.20	3.18	2.83	2.72	1.46	0.73	0.66	1.99
4	1.01	1.33	2.91	3.36	3.11	3.55	3.82	3.51	3.26	1.90	1.02	0.80	2.46
6	1.19	1.49	2.70	2.87	2.26	2.38	2.47	2.82	2.79	1.74	1.13	0.97	2.07
8	1.22	1.22	1.42	0.74	0.27	0.13	0.22	0.49	0.72	0.94	0.90	0.95	0.77
10	-0.02	-0.25	-0.68	-1.70	-1.30	-1.34	-1.25	-1.01	-1.10	-0.73	-0.26	-0.14	-0.73
		19/6	la la		0.10		0.00	001	0.00		1	(topie)	
Noon.	-0.13	-1.30	-1.97	-2.14	-2.42	-2.54	-2.50	-2.34	-2.38	-1.86	-1.18	-1.22	-1.91
2	-1.69	-1.70	-2.82	-2.94	-2.97	-3.09	-3.11	-3.17	-3.03	-2.35	-1.55	-1.46	-2.49
14	-1.30	-1.61	-2.70	-2.94	-2.46	-2.87	-2.89	-3.04	-2.86	-1.53	-1.19	-1.05	-2.20
6	-0.54	-0.90	-1.79	-2.06	-1.40	-1.89	-2.24	-2.04	-1.74	-0.88	-0.45	-0.43	-1.36
8	-0.09	-0.21	-0.89	-0.70	-0.10	-0.25	-0.58	-0.38	-0.38	-0.08	0.03	0.10	-0.29
10	0.20	0.28	0.34	0.40	0.86	0.78	0.78	0.69	0.57	0.47	0.29	0.18	0.49
	-			-				-					
Mean.	1.20	0.47	2.28	6.81	9.48	12.82	14.43	13.74	10.66	7.73	3.30	0.12	

#### XXXVIII.

SWITZERLAND. - St. BERNARD. Lat. 45° 52' N. Long. 9° 22' E. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.48	0.81	1.34	1.96	2.10	1.72	1.62	1.30	0.76	1.02	0.59	0.31	1.17
1	0.63	0.91	1.58	2.22	2.45	1.99	1.93	1.53	0.97	1.17	0.66	0.33	1.36
2	0.81	1.09	1.82	2.40	2.73	2.15	2.14	1.82	1.17	1.30	0.78	0.40	1.55
3	0.99	1.26	1.98	2.46	2.81	2.24	2.24	1.94	1.34	1.36	0.89	0.50	1.67
4	1.08	1.38	2.02	2.34	2.67	2.14	2.17	1.91	1.41	1.34	0.98	0.52	1.66
5	1.08	1.34	1.84	2.00	2.28	1.88	1.90	1.70	1.35	1.19	0.98	0.66	1.52
6	0.91	1.14	1.42	1.45	1.72	1.42	1.44	1.34	1.14	0.92	0.86	0.62	1.20
7	0.60	0.74	0.79	0.70	0.81	0.81	0.82	0.76	0.77	0.83	0.61	0.50	0.73
8	0.17	0.18	0.00	-0.16	-0.08	0.09	0.10	0.12	0.29	0.06	0.26	0.26	0.11
9	-0.31	-0.48	-0.85	-1.06	-1.10	-0.66	-0.66	-0.53	-0.26	-0.46	-0.22	-0.06	-0.55
10	-0.78	-1.13	-1.63	-1.86	-1.94	-1.36	-1.34	-1.13	-0.78	-0.94	-0.68	-0.41	-1.16
11	-1.14	-1.66	-2.23	-2.50	-2.58	-1.95	-1.90	-1.60	-1.22	-1.33	-1.09	-0.71	-1.66
Noon.	-1.34	-1.98	-2.58	-2.87	-2.96	-2.34	-2.26	-1.90	-1.51	-1.58	-1.36	-0.94	-1.97
1	-1.38	-2.04	-2.62	-2.98	-3.06	-2.51	-2.40	-2.02	-1.62	-1.66	-1.47	-1.03	-2.07
2	-1:24	-1.86	-2.38	-2.78	-2.89	-2.44	-2.33	-1.94	-1.56	-1.59	-1.39	-0.99	-1.95
3	-0.98	-1.47	-1.92	-2.36	-2.51	-2.21	-2.08	-1.74	-1.35	-1.38	-1.16	-0.82	-1.66
4	-0.65	-0.97	-1.34	-1.79	-1.98	-1.80	-1.70	-1.42	-1.05	The state of the s	-0.83	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
5	-0.32	-0.43	-0.73	-1.17	-1.40	-1.32	-1.26	-1.06	-0.70	-0.72	-0.46	-0.27	-0.82
6	-0.05	0.04	-0.19	-0.54	-0.81	-0.80	-0.80	-0.70	-0.38	-0.36	-0.10	0.00	-0.39
7	0.14	0.39	0.25	0.04	-0.25	-0.28	-0.34	-0.34	-0.11	-0.03	0.19	0.21	-0.01
8	0.25	0.60	0.56	0.54	0.27	0.20	0.09	0.00	0.10	-0.24	0.38	0.34	0.30
9	0.30	0.69	0.78	0.96	0.76	0.63	0.50	0.32	0.27	0.47	0.49	0.38	0.55
10	0.34	0.72	0.96	1.33	1.22	1.02	0.89	0.64	0.42	0.67	0.53	0.38	0.76
11	0.38	0.74	1.14	1.66	1.68	1.40	1.26	0.97	0.58	0.85	0.55	0.33	0.96
Mean.	-8.26	-6.62	-5.72	-2.97	0.74	3.55	4.82	4.32	2.40	-0.91	-3.95	-5.86	

## XXXIX.

SWITZERLAND. — St. Bernard. Lat. 45° 52' N. Long. 9° 22' E. Gr. — Dove.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.34	0.55	0.75	1.19	1.26	1.39	1.02	1.08	0.81	0.66	0.33	0.28	0.80
2	0.52	0.78	1.14	1.64	1.75	1.88	1.62	1.53	1.16	0.94	0.42	0.27	1.14
4	0.82	1.06	1.50	1.84	1.91	1.98	1.82	1.71	1.34	1.17	0.65	0.42	1.35
6	0.65	0.86	1.20	1.50	1.53	1.46	1.46	1.27	0.98	0.88	0.50	0.32	1.05
8	0.48	0.26	0.14	-0.08	-0.25	0.01	0.22	0.16	0.08	0.28	0.27	0.15	0.14
10	-0.35	-0.91	-1.06	-1.26	-1.39	-1.18	-1.11	-0.94	-0.86	-0.68	-0.54	-0.23	-0.88
Noon.	-1.40	-1.66	-1.74	-2.11	-2.15	-1.92	-1.81	-1.77	-1.58	-1.45	-1.26	-0.91	-1.65
2	-1.37	-1.55	-1.89	-2.12	-2.12	-2.23	-2.01	-1.97	-1.54	-1.52	-1.23	-1.22	-1.73
4	-0.42	-0.71	-1.14	-1.55	-1.47	-1.65	-1.49	-1.30	-0.88	-0.86	-0.37	THE WAY	-0.99
6	0.09	0.17				-0.71			-0.26		0.08	0.22	-0.17
8	0.25	0.44			The second		1 10 10 10	10107	(12 y Th.)	400	0.70	0.30	0.38
10	0.37	0.55	0.55	0.71	0.76	0.64	Total Control	155,000	7500 /60	100	0.40	0.40	0.52
Mean.	-6.03	-8.83	-6.66	-3.01	-0.42	2.71	-4.82	4.70	2.07	-0.36	-5.46	-6.18	

XL.

## Austria. — Kremsmünster. Lat. 48° 3' N. Long. 14° 7' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	es of Re	aumui.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
04111 A	24.3	DE T	100 30	112	10			11-12-				0.10	
Morn. 1	0.58	0.90	1.05	1.14	2.30	2.77	1.86	1.94	1.52	1.26	0.61	0.40	1.36
2	0.66	1.03	1.30	1.36	2.66	3.08	2.16	2.26	1.94	1.58	0.72	0.42	1.60
3	0.71	1.07	-1.57	1.63	2.84	3.14	2.35	2.50	2.32	1.82	0.78	0.42	1.76
4	0.78	1.12	1.80	1.88	2.78	2.90	2.34	2.54	2.58	1.97	0.83	0.42	1.83
5	0.84	1.19	1.90	1.99	2.44	2.32	2.08	2.30	2.60	1.98	0.88	0.46	1.75
6	0.88	1.13	1.82	1.88	1.86	1.54	1.54	1.80	2.34	1.91	0.93	0.54	1.52
7	0.84	1.26	1.50	1.41	1.11	0.68	0.94	1.11	1.81	1.63	0.92	0.59	1.15
8	0.67	1.07	0.96	0.87	0.31	-0.15	0.23	0.35	1.09	1.21	0.80	0.56	0.66
8	0.01	1.01	0.00	0.0.	0.01	0.20	0.20	0.00	1.00		0.00	0.00	
9	0.35	0.67	0.30	0.14	-0.45	-0.86	-0.42	-0.37	0.28	0.62	0.51	0.38	0.10
10	-0.10	0.01	-0.41	-0.58	-1.10	-1.42	-0.95	-0.98	-0.52	-0.13	0.06	0.05	-0.56
11	-0.58	-0.72	-1.06	-1.20	-1.65	-1.84	-1.39	-1.47	-1.23	-0.92	-0.47	-0.38	-1.08
Noon	-0.98	-1.37	-1.56	-1.65	-2.09	-2.17	-1.75	-1.86	-1.81	-1.68	-0.97	-0.78	-1.56
The state	ASK C	ME S	NAME OF			- 44	HE DIE	- 4	10-20	162.5	in.	10-	
1		-1.78	0.033	THE PARTY NAMED IN			-2.05	- 10			Contract of the Contract of th	-1.03	
2	THE TANK	-1.90	and the second second	-2.06	30 30 00		-63	4 CT . S .	-2.56		The state of the s	-1.09	100
3	-1.12	-1.69	ALC: The same of	- 1 /200	CC00 3 100 0	District Control of the	-2.33	1.00				-0.94	21.13-3
4	-0.86	-1.32	-1.79	-1.89	-2.51	-2.49	-2.22	-2.34	-2.52	-2.17	-1.01	-0.66	-1.98
	0.50	0.00	1 40	1.00	0.15	0.10	1.00	0.00	0.10	1.00	0.00	0.95	1 40
5			× 2011 30	1700.10	172,750,000	The contract of	-1.88			100 0 100 100	3.00		
6		200	1		100000		-1.38			100000000000000000000000000000000000000	100000000000000000000000000000000000000		
7	1000	-0.36	-0.65		1 1 1 1 1 1 1 1	-1.03	683597	-0.86			10.00		-0.62
8	-0.04	-0.19	-0.23	-0.17	-0.34	-0.30	-0.15	-0.24	-0.46	-0.20	-0.11	0.09	-0.20
9	0.07	-0.02	0.13	0.28	0.28	0.34	0.38	0.30	0.05	0.06	-0.02	0.12	0.16
10	0.20	0.18	0.42	0.61	0.84	1.02	0.82	0.76	0.46	0.34	0.11	0.18	0.49
11	0.34	0.46	0.63	0.82	1.36	1.68	1.19	1.15	0.80	0.63	0.27	0.25	0.80
Midn	0.47	0.70	0.83	0.97	1.85	2.27	1.52	1.53	1.14	0.94	0.46	0.34	1.08
Mium													
			7 - 1		on di	100 P				The same			
6. 6	0.27	0.34	0.37	0.35	0.12	-0.06	0.08	0.16	0.34	0.39	0.26	0.22	0.24
7. 7	0.33	0.45	0.43	0.37	0.07	-0.18	0.09	0.13	0.38	0.48	0.35	0.29	0.27
8. 8	0.32	0.44	0.37	0.35	-0.02	-0.10	0.04	0.06	0.32	0.48	0.35	0.24	0.24
9. 9	0.21	0.33	0.22	0.21		-0.26	-0.02	-0.04	0.17	0.34	0.25	0.25	0.13
10.10	0.05	0.10	0.01	0.02	-0.13	-0.20	-0.07	-0.11	-0.03	0.11	0.09	0.12	0.00
	0.10	0.00	0.10	0.10	0.43	0.50	0.07	0.00	0.00	0.00	0.1~	0.10	0.05
7. 2. 9	-0.12	The same of	3		1		-0.31					-0.16	
6. 2. 8		-0.28		7.00	1000		-0.29			COLL NO.			KIND OF THE PARTY OF
6. 2.10	The same of	-0.16	0.07	C. C		-0.01	0.03 -0.70	4 4 4 4 6 6				-0.12 $-0.15$	
6. 2. 6	-0.24	-0.41	-0.43	-0.45	0.19	-0.90	-0.70	0.09	-0.03	0.94	0.00	-0.10	-0.00
7. 2	-0.21	-0.32	-0.26	-0.33	-0.76	-0.95	-0.66	-0.63	-0.38	-0.45	-0.24	-0.25	-0.45
8. 2	-0.30				100000		-1.02		77 P. J.	100000		CAN DO	
8. 1		C 4 W 30		100000000000000000000000000000000000000			-0.91	AND THE STREET	1717160	1 TO 1 TO 1			1 1 1 1 1 1
7. 1	12000	1	The second	1 2 2 2		The state of the s	-0.56	The Park Street of		ALC: YES			
	S. Paris	15.50		1000		13.195	1	B- 33	T8 12-	CR CH	13.5		
9.12.3.9		1	1	1			-1.03					1	and the second
7, 2.2(9)	-0.07	-0.17	-0.07	-0.02	-0.24	-0.31	-0.15	-0.17	-0.14	-0.19	-0.13	-0.07	-0.14
	0.10	0.00	0.00	000	0.00	0.00	0.03	000	0.00	0.00	00.	0.00	0.00
Dail. ext.	-0.19	-0.32	-0.06	-0.04	0.09	0.36	0.01	0.04	-0.03	-0.28	-0.24	-0.25	-0.08

## Austria. - Salzburg. Lat. 47° 48' N. Long. 13° 1' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees	of	Reaumur.	
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Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.54	0.70	1.06	1.31	2.03	2.07	1.87	1.57	1.21	1.02	0.48	0.42	1.19
1	0.59	0.79	1.29	1.58	2.37	2.27	2.13	1.81	1.45	1.15	0.65	0.50	1.38
2	0.72	0.97	0.51	1.79	2.64	2.56	2.36	2.05	1.61	1.27	0.81	0.59	1.49
3	0.82	1.08	1.75	2.04	2.90	2.73	2.64	2.24	1.87	1.41	0.88	0.70	1.75
4	0.96	1.09	1.89	2.21	3.10	2.82	2.62	2.23	2.04	1.52	0.91	0.69	1.84
5	1.03	1.28	2.01	2.37	3.10	2.75	2.59	2,24	2.14	1.72	1.03	0.81	1.92
6	1.06	1.34	2.14	2.28	2.76	2.45	2.31	2.26	2.18	1.77	1.03	0.87	1.87
7	1.09	1.36	2.06	1.86	1.89	1.53	1.61	1.74	1.94	1.74	1.06	0.94	1.57
8	1.12	1.24	1.58	1.06	0.84	0.63	0.67	0.89	1.15	1.26	1.07	1.00	1.04
9	0.91	0.75	0.76	0.14	-0.10	-0.25	0.20	0.04	0.33	0.48	0.64	0.74	0.39
10	0.38	0.04	-0.06	-0.67	-0.92	-1.10	-0.97	-0.76	-0.53	-0.35	.0.06	0.21	-0.39
11	-0.26	-0.62	-0.96	-1.39	-1.80	-1.87	-1.63	-1.40	-1.25	-1.17	-0.62	-0.35	-1.11
Noon.	-0.90	-1.19	-1.75	-1.99	-2.36	-2.90	-2.14	-2.13	-2.00	-1.84	-1.25	-0.93	-1.78
1	-1.47	-1.68	-2.26	-2.48	-2.82	-2.84	-2.59	-2.59	-1.48	-2.39	-1.68	-1.47	-2.15
2	-1.70	-1.96	-2.55	-2.74	-3.08	-3.03	-2.77	-2.73	-2.71	-2.55	-1.85	-1.64	-2.44
3	-1.68	-2.04	-2.61	-2.74	-3.21	-3.04	-2.90	-2.75	-2.67	-2.51	-1.75	-1.55	-2.45
4	-1.40	-1.80	-2.55	-2.60	-3.27	-3.00	-2.90	-2.85	-2.56	-2.21	-1.37	-1.19	-2.31
5	-1.00	-1.46	-2.26	-2.10	-2.97	-2.64	-2.64	-2.46	-2.09	-1.63	-0.85	-0.72	-1.90
6	-0.60	-0.76	-1.51	-1.52	-2.27	-2.10	-2.05	-1.78	-1.31	-0.83	-0.35	-0.42	-1.29
7	-0.31	-0.27	-0.76	-0.75	-1.43	-1.21	-1.24	-0.85	-0.48	-0.29	-0.10	-0.15	-0.65
8	-0.25	-0.02	-0.16	-0.07	-0.43	-0.13	-0.24	0.06	0.15	0.16	0.11	0.04	-0.06
9	-0.04	0.20	0.17	0.51	0.48	0.71	0.67	0.70	0.50	0.48	0.24	0.17	0.40
10	0.12	0.43	0.46	0.81	1.03	1.41	1.22	1.09	0.78	0.76	0.34	0.33	0.73
11	0.28	0.53	0.76	1.08	1.50	1.70	1.56	1.38	0.76	1.03	0.52	0.41	0.96
Mean.	-2.71	1.14	2.49	6.90	10.42	13.22	13.93	13.66	10.30	7.37	1.52	1.63	

#### XLII.

Germany. - Munich. Lat. 48° 9' N. Long. 11° 37' E. Greenw. - Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.71	0.92	1.54	2.27	2.58	2.49	2.84	2.37	2.17	1.53	0.91	0.46	1.73
1	0.90	1.04	1.83	2.37	3.02	3.06	3.27	2.64	2.33	1.59	0.87	0.58	1.96
2	0.97	1.18	2.04	2.62	3.30	3.39	3.56	2.94	2.61	1.67	0.94	0.67	2.16
3	1.04	1.30	2.16	2.89	3.61	3.66	3.80	3.19	2.81	1.78	1.00	0.77	2.33
4	1.03	1.33	2.25	3.12	3.85	3.82	4.05	3.41	2.98	1.91	1.04	0.85	2.47
5	1.07	1.43	2.37	3.29	3.69	3.25	3.71	3.50	3.16	2.01	1.12	0.92	2.46
6	1.14	1.52	2.56	2.93	2.61	2 11	2.41	2.79	3.08	2.14	1 13	0.99	2.12
7	1.17	1.55	2.17	1.80	1.21	0.77	0.93	1.48	2.22	1.84	1.13	0.97	1.44
8	1.10	1.14	1.14	0.36	-0.07	-0.35	-0.28	0.18	0.59	0.99	0.75	0.88	0.54
9	0.46	0.36	-0.11	-0.79	-1.00	-1.21	-1.25	-1.05	-0.74	-0.24	0.06	0.41	-0.42
10	-0.72	-0.61	-1.18	-1.80	-1.99	-1.96	-2.12	-1.88	-1.70	-1.34	-0.79	-0.42	-1.38
11	-1.06											-0.97	-2.06

#### XLII.

### GERMANY. - MUNICH, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon	-1.70	-1.93	-2.67	-2.99	-3.28	-2.98	-3.14	-3.09	-3.18	-2.69	-1.94	-1.02	-2.5
1	-2.08	-2.31	-3.01	-3.27	-3.59	-3.41	-3.48	-3.55	-3.58	-3.08	-2.23	-1.83	-2.95
2	-2.15	-2.40	-3.24	-3.60	-3.77	-3.79	-3.75	-3.72	-3.74	-3.15	-2.05	-1.85	-3.10
3	-1.83	-2.15	-3.17	-3.45	-3.77	-3.54	-3.83	-3.58	-3.56	-2.87	-1.75	-1.43	-2.9
4	-1.08	-1.67	-2.64	-3.18	-3.41	-3.34	-3.49	-3.30	-3.24	-2.27	-1.02	-0.76	-2.45
5	-0.46	-0.95	-1.98	-2.51	-2.87	-2.80	-3.07	-2.76	-2.56	-1.27	-0.43	-0.34	-1.83
6	-0.16	-0.37	-0.94	-1.53	-2.05	-1.94	-2.32	-1.81	-1.29	-0.44	-0.12	-0.13	-1.09
7	0.04	-0.07	-0.20	-0.36	-0.74	-0.84	-2.99	-0.47	-0.30	0.08	0.20	0.06	-0.4
8	0.23	0.22	0.28	0.40	0.41	0.61	0.40	0.55	0.37	0.56	0.44	0.14	0.38
9	0.39	0.45	0.55	0.91	1.13	1.35	1.20	1.15	0.93	0.88	0.57	0.23	0.81
10	0.49	0.59	1.02	1.31	1.65	1.86	1.87	1.60	1.40	1.14	0.74	0.33	1.17
11	0.61	0.77	1.33	1.69	2.18	2.28	2.41	2.06	1.80	1.34	0.85	0.40	1.48
Mean.	-2.15	-0.12	0.75	5.57	9.29	12.74	13.65	12.93	9.45	6.28	1.55	-1.28	owig.

### XLIII.

Bohemia. — Prague. Lat. 50° 5′ N. Long. 14° 25′ E. Greenw. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug	Sept.	Oct.	Nov.	Dec.	Year.
Midn	0.30	0.52	1.03	1.47	1.70	1.68	1.72	1.17	1.23	0.84	0.36	0.25	1.02
1	0.40	0.60	1.14	1.68	1.97	1.97	2.05	1.78	1.49	1.02	0.45	0.32	1.24
2.	0.50	0.71	1.29	1.95	2.25	2.23	2.34	2.10	1.72	1.19	0.54	0.39	1.43
3	0.55	0.83	1.44	2.17	2.46	2.47	2.60	2.38	1.96	1.31	0.61	0.50	1.61
4	0.65	0.89	1.60	2.39	2.75	2.71	2.91	2.63	2.19	1.49	0.70	0.56	1.79
5	0.71	0.99	1.72	2.64	2.96	2.86	3.07	2.88	2.43	1.65	0.77	0.65	1.94
6	0.77	1.00	1.81	2.75	2.96	2.71	2.92	2.93	2.61	1.73	0.82	0.72	1.98
7	0.68	0.99	1.53	2.32	2.11	1.88	2.13	2.34	2.29	1.65	0.79	0.73	1.62
8	0.73	0.88	1.28	1.29	0.98	0.82	1.02	1.30	1.62	1.29	0.66	0.70	1.05
9	0.62	0.57	0.63	0.32	0.06	-0.14	0.17	0.21	0.60	0.70	0.41	0.54	0.39
10	0.26	0.15	-0.11	-0.53	-0.91	-0.93	-0.95	-0.77		A THE WAY	-0.12	0.17	-0.36
11	-0.16	-0.45	-0.77	-1.51	-1.60	-1.58	-1.62	-1.50	-1.46	-0.86	-0.46	-0.22	-1.02
Noon.	-0.60	-0.92	-1.37	-2.09	-2.16	-2.08	-2.16	-2.18	-2.02	-1.53	-0.86	-0.65	-1.55
1	-0.93	-1.27	-1.83	-2.48	-2.56	-2.48	-2.59	-2.61	-2.56	-2.01	-1.13	-0.95	-1.95
2	-1.10	-1.50	-2.20	-2.74	-2.80	-2.73	-2.83	-2.89	-2.84	-2.31	-1.25	-1.07	-2.19
3	-1.11	-1.51	-2.29	-2.88	-2.90	-2.79	-2.93	-3.01	-2.96	-2.32	-1.28	-0.99	-2.25
4	-0.93	-1.35	-2.20	-2.76	-2.82	-2.71	-2.92	-2.85	-2.78	-2.10	-0.87	-0.79	-2.09
5	-0.68	-0.97	-1.83	-2.46	-2.53	-2.56	-2.83	-2.66	-2.35	-1.58	-0,62	-0.55	-1.80
6	-0.44	-0.61	-1.26	-1.91	-2.17	-2.10	-2.36	-2.11	-1.64	-1.01	-0.36	-0.37	-1.36
7	-0.31	-0.32	-0.70	-1.12	-1.49	-1.37	-1.59	-1.23	-0.87	-0.54	-0.19	-0.21	-0.83
8	-0.23	-0.06	-0.24	-0.33	-0.51	-0.39	-0.58	-0.34	-0.24	-0.10	0.01	-0.19	-0.27
9	0.01	0.12		0.20	0.27	0.30	0.22	0.20	0.27	0.23	0.16	0.06	0.18
10	0.10	0.26	Dec. 1190, 145 W	A CONTRACTOR	0.80	THE DESIGNATION OF THE PERSON	0.90	0.81	0.74	0.51	0.29	0.16	0.55
11	0.19	0.39	0.66	1.12	1.24	1.28	1.32	1.20	1.08	0.85	0.43	0.25	0.83
Mean.	-1.69	0.64	2.20	7.27	11.27	14.47	15.66	15.01	11.52	7.94	3.02	-0.12	

#### XLIV.

## Bohemia. — Prague. Lat. 50° 5′ N. Long. 14° 24′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					0	es of iv							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.45	0.76	0.86	1.73	1.47	1.90	1.93	1.59	1.46	1.06	0.73	0.45	1.20
11	0.52	0.88	1.05	2.06		2.22	2.24		1.69	1.18	0.79	0.52	1.40
2			1.24	2.45	2.08	2.62	2.36		1.85	1.23	0.82	0.54	1.56
3	0.54	0.98	1	The state of					5111	- 174		1 1 1 1 1	TOTAL TRANSPORT
4	0.53	1.06	1.42	2.82	2.31	3.02	2.27	2.10	1.95	1.24	0.78	0.55	1.67
5	0.50	1.14	1.55	3.02	2.35	3.22	2.01	2.01	1.97	1.22	0.78	0.60	1.70
6	0.49	1.15	1.60	2.92	2.12	3.03	1.62	1.76	1.90	1.19	0.80	0.70	1.61
7	0.47	1.09	1.51	2.43	1.62	2.40	1.16	1.36	1.69	1.10	0.77	0.80	1.37
8	0.42	0.91	1.24	1.59	0.92	1.40	0.66	0.83	1.28	0.90	0.69	0.82	0.97
		100			-10				80	STA S			
9	0.29	0.55	0.77	0.53	0.15	0.24	0.10	0.19	0.64	0.51	0.42	0.67	0.42
10	0.08	-1.01	0.16	-0.56	-0.57	-0.85	-0.52	-0.51	-0.20	-0.07	-0.02	0.31	-0.31
11	-0.21	-1.19	-0.52	-1.52	-1.16	-1.68	-1.19	-1.23	-1.14	-0.78	-0.55	-1.18	-0.95
Noon	-0.52	-1.10	-1.16	-2.25	-1.60	-2.23	-1.84	-1.86	-2.00	-1.47	-1.10	-0.70	-1.49
					all Y	1				-			
1	-0.76		0.000	-2.74				-2.33				-1.08	-1.91
2	1			-3.00	-2.14	-2.76	-2.66	-2.57	-2.89	-2.21	-1.58	-1.23	-2.13
3	-0.85	-1.64	-1.92	-3.08	-2.26	-2.92	-2.65	-2.53	-2.76	-2.08	-1.44	-1.13	-2.11
4	-0.71	-1.39	-1.75	-2.97	-2.26	<b>-2.9</b> 8	-2.36	-2.23	-2.31	-1.68	-1.08	-0.87	-1.88
5	-0.51	-1.05	-1.45	-2.65	-2.08	-2.86	-1.86	-1.75	-1.70	-1.14	-0.67	-0.56	_1.59
6		-0.66						-1.18					
7		-0.34						-0.62				-0.17	
8				-0.64					-0.08		-		
	-0.00	-0.03	-0.40	-0.04	-0.50	70.00	-0.24	-0.12	-0.00	0.13	0.10	-0.11	-0.24
9	0.02	0.11	0.10	0.11	0.03	0.06	0.19	0.30	0.26	0.34	0.20	0.07	0.12
10	0.11	1.35	0.18	0.71	0.52	0.81	0.61	0.65	0.57	0.51	0.32	0.01	0.53
11	0.22	1.10	0.42	1.15	0.89	1.32	1.05	0.97	0.87	0.70	0.44	0.14	0.77
Midn	0.34	0.61	0.65	1.46	1.18	1.64	1.51	1.28	1.17	0.89	0.61	0.31	0.97
	1000	300			1.10	2.01	1.01	1.20		0.00	0.01	0.01	0.51
CALL DE CO	130.0		100	F	219	CI					26	00.4	
6. 6	0.09	0.24	0.25	0.40	0.21	0.29	0.17	0.29	0.42	0.29	0.25	0.19	0.26
7. 7	0.15	0.38	0.39	0.50	0.22	0.33	0.22	0.37	0.59	0.47	0.37	0.32	0.36
8. 8	0.18	0.41	0.42	0.47	0.18	0.27	0.21	0.36	0.60	0.51	0.39	0.35	0.36
9. 9	0.16	0.33	0.34	0.32	0.90	0.15	0.15	0.25	0.45	0.42	0.31	0.30	0.27
10.10	0.09	0.17	0.17	0.08	-0.03	-0.02	0.04	0.07	0.18	0.22	0.15	0.16	0.11
		148	200	14 (E)		100	2				15-1-0	10 112	
7. 2. 9	-0.13	-0.17						-0.30					-0.21
6. 2. 8		-0.21	-0.23					-0.31					-0.25
6. 2.10	-0.09	0.27	-0.04	0.21	0.17			-0.05					0.01
6. 2. 6	-0.23	-0.40	-0.46	-0.74				-0.66					
7. 2	-0.97	0.07	0.00	0.00	13								
11	-0.21	-0.31	-0.19	-0.29	-0.26	-0.18	-0.75	-0.61	-0.60	-0.56	-0.41	-0.22	-0.38
8. 2	-0.23	-0.40	-0.33	-0.71	-0.61	-0.68	-1.00	-0.87	-0.81	-0.66	-0.45	-0.21	-0.58
8. 1	-0.17	-0.30	-0.20	-0.58	-0.50	-0.58	-0.86	-0.75	-0.68	-0.55	-0.39	-0.13	-0.97
7. 1	-0.15	-0.21	-0.06	-0.16	-0.15	-0.08	-0.61	-0.49	-0.47	-0.45	-0.35	-0.14	-0.28
9.12.3.9	-0.27	-0.52	-0.60	-1.17	-0.92	-1.91	-1.05	-0.98	_0 07	_0 60	_0.49	_0 21	-0.76
7. 2.2(9)	-0.09	-0.10	-0.15	-0.09	-0.12	-0.06	-0.29	-0.95	-0.97	-0.03	-0.48	_0.31	_0.70
TOWN	1	11000	1000	Jr 500	DOM: NO	0.00	0.20	0.19	0.17	-0.11	-0.10	-0.14	-0.13
Dail. ext.	-0.17	-0.18	-0.16	-0.03	0.05	0.12	-0.15	-0.24	-0.46	-0.49	-0.38	-0.21	-0.22

#### XLV.

England. — Plymouth. Lat. 50° 22' N. Long. 4° 7' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

Degrees of Fahrenheit.													
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
		TOL		E 185	700	13/5-	11000			10000			
Morn. 1	0.86	1.46	2 32	4.01	5.13	4.34	4.75	4.16	3.24	2.66	1.58	0.95	2.95
2	0.90	1.67	2.63	4.43	5.94	4.82	5.38	4.79	3.60	2.79	1.69	0.86	3.29
3	0.99	1.87	-3 02	4.91	6.62	5.13	5.69	5.45	4.03	3.02	1.80	0.74	3.60
4	1.15	2.12	3.31	5.13	6.75	5.00	5.58	5.76	4.34	3.31	1.96	0.81	3.76
	100			100	7	N/A							
5	1.37	2.36	3.40	4.91	6.03	4.57	4.82	5.42	4.25	3.51	2.09	1.04	3.65
6	1.53	2.48	3.08	3.98	4.37	2.79	3.35	4.21	3.62	3.38	2.14	1.31	3.02
7	1.46	2.30	2.25	2.39	2.00	0.95	1.92	2.25	2.32	2.66	1.89	1.40	1.94
8	1.10	1.67	0.97	0.29	-0.54	-1.01	-0.65	-0.11	0.50	1.26	1.24	1.13	0.50
											0.47		
9	0.36	0.59	-0.63	-1.94	-2.88	-2.70	-2.57	-2.39	-1.53	-0.65	0.16	0.41	-1.15
10	-0.61	-0.83	-2.23							-2.70	-1.17	-0.61	-2.68
11	-1.58	-2.25	-3.56	-5.40	-5.63	-4.64	-5.02	-5.36			-2.43	-1.67	-3.92
- FEET 12	-2.32	-3.33	-4.43	-6.17	-6.12	-4.93	-5.58	-5.87	-5.74	-5.40	-3.29	-2.43	-4.64
		Elejo	B. G. B.			Haber .	See 15	Section.		Flat.	2(4)		
Noon. 1			1 30 30 10								-3.56		1. 1000
2			-4.43								-3.22		-4.61
3	ISADS	0.0550000	-3.74		-6.12					-3.71		41177	
4	-1.26	-2.07	-2.81	-4.14	-5.47	-4.03	-4.64	-4.52	-3.49	-2.45	-1.55	-1.10	-3.13
		2014.65	1		1994				0.70		0		0.10
5	W 7 7 7 1 1 1 1 7 1	-1.10	-1.76		-4.32				- 200	10.00	-0.77	-0.41	
6	-0.07	-0.38	-0.74	-1.42	-2.68		-2.00	- 033	-0.88	-0.45	-0.23	0.05	-1.06
7	0.29	0.09	0.14	P. Contract of	-0.81	-0.27			0.36	0.23	0.07	0.34	
8	0.50	0.36	0.86	1.26	0.99	0.74	1.10	1.06	1.37	0.79	0.25	0.52	0.81
	0.00	0 40	1 05	0.05	2.36	0.01	2.27	2.23	2.12	1.33	0.47	0.72	1.55
9	0.63	0.56	1.35	2.25 2.93	3.29	2.21 2.93	3.11	2.23	2.59	1.85	0.47	0.72	2.05
10	0.72	0.77	1.69	3.35	3.89	3.44	1 1 1 1 1	3.40	2.84	2.23	1 1 1 1 1 1 1 1	1.01	2.39
Midn	0.13	1.26	2.07	3.67	4.46	3.87	4.21	3.71	2.99	2.48	- 1000	1.04	2.66
witun	0.00	1.20	2.01	0.01	1.10	0.01	7.21	0.11	2.00	2.40	1.0.	1.04	2.00
	1 3 20 20	on-all		8 160	Market S	Dr. Line	HELL	O AND	1 45 6	A. S	U. Land	P. 17.54	100
6. 6	0.74	1.06	1.17	1.28	0.86	0.54	0.68	0.99	1.37	1.46	0.97	0.68	0.99
7. 7	0.88	1.19	1	1.19		0.34		0.90	A Carlon	1.44		0.88	0.95
8. 8	0 81	1.01				10.01		1		The same of the sa		0.83	100
9. 9	0.50		1						0.29	0.34		0.56	0.20
10.10	0.07	1		1			- W.		-0.43			0.14	17.7
STALL SE	- 18	- 519	- 18 F	1188			9.41	1100	100	- 1			- King
7. 2. 9	-0.14	-0.27	-0.27	-0.45	-0.68	-0.59	-0.70	-0.41	-0.36	-0.29	→0.29	-0.11	-0.38
6. 2. 8	-0.16	-0.29	-0.16	-0.25	-0.34	-0.45	-0.43	-0.16	-0.16	-0.23	-0.27	-0.20	-0.25
6. 2.10	-0.09	-0.16	0.11	0.32	1		1		1		-0.11		
6. 2. 6	-0.34	-0.54	-0.70	-1.15	-1.55	-1.28	-1.46	-1.24	-0.92	-0.63	-0.43	-0.36	-0.88
		100		1	ALLES			D.I.S.		-	1	Sul 2	TE S
7. 2											-0.68		
8. 2											-0.99		
8. 1	H										-1.17		
7. 1	-0.59	-0.79	-1.24	-2.00	-2.18	-2.05	-2.21	-1.87	-1.80	-1.44	-0.83	-0.65	-1.46
0.10.00	0.00										P BOLL		
9.12.3.9	1	-1.31	1 30	1 11 11 11	100			The state of the s	1	1000000	-1.28	ALL PROPERTY.	1000000
7. 2.2(9)	0.07	-0.07	0.14	0.23	0.09	0.11	0.05	0.25	0.27	0.11	-0.09	0.09	0.11
1		<u> </u>		-			1		-	-	1		

#### XLVI.

England. — Plymouth. Lat. 50° 22' N. Long. 4° 7' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

			3 2 7 16	CONTRACTOR OF THE PARTY OF THE	Degree	s of Re	aumur.					0000	
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
100													
Morn. 1	0.38	0.65	1.03	1.78	2.28	1.93	2.11	1.85	1.44	1.18	0.70	0.42	1.31
2	0.40	0.74	1.17	1.97	2.64	2.14	2.39	2.13	1.60	1.24	0.75	0.38	1.46
3	0.44	0.83	1.34	2.18	2.94	2.28	2.53	2.42	1.79	1.34	0.80	0.33	1.60
4	0.51	0.94	1.47	2.28	3.00	2.22	2.48	2.56	1.93	1.47	0.87	0.36	1.67
5	0.61	1.05	1.51	2.18	2.68	2.03	2.14	2.41	1.89	1.56	0.93	0.46	1.62
6	0.68	1.10	1.37	1.77	1.94	1.24	1.49	1.87	1.61	1.50	0.95	0.58	1.34
7	0.65	1.02	1.00	1.06	0.89	0.42	0.63	1.00	1.03	1.18	0.84	0.62	0.86
8	0.49	0.74	0.43	0.13	- 19 m. 1	-0.45	-0.29	-0.05	0.22	0.56	0.55	0.50	0.22
1								LOSE				STEEL S	
9	0.16	0.26			-1.28	-1.20	-1.14		110000000000000000000000000000000000000		0.07	0.18	-0.51
10	-0.27	-0.37	The second			7065	-1.79	mail: 277		10.55 (0.00)	-0.52	1111	
11				A 30			-2.23	- 7-14-14	200	-1.96	377733000	WEST 100	
Noon	-1.03	-1.48	-1.97	-2.74	-2.72	-2.19	-2.48	-2.61	-2.55	-2.40	-1.46	-1.08	-2.06
1	-1.17	-1.71	-2.09	-2.83	-2.83	-2.23	-2.58	-2.65	-2.63	-2.45	-1.58	-1.20	-2.16
2	-1.11	ALC: NO	- PES-33	- N. W.	(1) W. F. T. T.		-2.56		-2.44		-1.43	-1.09	THE PERSON NAMED IN
3	-0.87		100.44	-2.32	-2.72		-2.40			DOI:035701	-1.09		
4		-0.92	11-11-11	-1.84	10710 94	111111111111111111111111111111111111111	-2.06	100000	100 4 7 100 100	100000000000000000000000000000000000000		1000	
				- 1-3									
5	-0.26	E	APR 2350 A20	-1.27	THE PERSON NAMED IN	-1.35	-1.54	-1.53	F T T T T T T T T T	-0.59	-0.34	-0.18	
6	-0.03	10 KS L O	9-52000 W.S.	-0.63	A 17 10 1 10 10 10 10 10 10 10 10 10 10 10 1	-0.77	-0.89	-0.99		-0.20	223374	01020.019	-0.47
7	0.13	0.04	0.06	-0.00	-0.36	-0.12	-0.17	-0.21	0.16	0.10	0.03	0.15	-0.02
8	0.22	0.16	0.38	0.56	0.44	0.33	0.49	0.47	0.61	0.35	0.11	0.23	0.36
9	0.28	0.25	0.60	1.00	1.05	0.98	1.01	0.99	0.94	0.59	0.21	0.32	0.69
10	0.32	0.34	0.75	1.30	1.46	1.30	1.38	1.32	1.15	0.82	0.34	0.39	0.91
11	0.35	0.44	0.84	1.49	1.73	1.53	1.63	1.51	1.26	0.99	0.48	0.45	1.06
Midn	0.37	0.56	0.92	1.63	1.98	1.72	1.87	1.65	1.33	1.10	0.61	0.46	1.18
PARTIES INC.	179.6		170	u iés	1344	18803	200	10 500			118	- Original	MP188
			ersy		Sec.	100					7111		
6. 6	0.33	0.47	0.52	0.57	0.38	0.24	0.30	0.44	0.61	0.65	0.43	0.30	
7. 7	0.39	0.53	0.53	0.53	0.27	0.15	0.23	0.40	0.60	0.64	0.44	0.39	0.42
9. 9	0.30	0.45	0.41 0.16	0.35	0.10 $-0.12$		0.10	0.21	0.42	0.46	0.33	0.37	
10.10	0.03	-0.02	-0.12	-0.23	13000	-0.11 -0.21	-0.07 -0.21	-0.04 -0.28	0.13 -0.19	0.15 -0.19	-0.09	0.25	and the same of
20020	0.00	0.02	0.12	0.20	0.23	-0.21	-0.21	-0.20	-0.19	-0.19	-0.05	0.00	-0.14
7. 2. 9	-0.06	-0.12	-0.12	-0.20	-0.30	-0.26	-0.31	-0.18	-0.16	-0.13	-0.13	-0.05	-0.17
6. 2. 8	-0.07	-0.13	-0.07	-0.11	-0.15	-0.20	-0.19	-0.07	-0.07	-0.10	-0.12	-0.09	-0.11
6. 2.10	-0.04	-0.07	0.05	0.14	0.19	0.12	0.10	0.22	0.11	0.06	-0.05	-0.04	0.07
6. 2. 6	-0.15	-0.24	-0.31	-0.51	-0.69	-0.57	-0.65	-0.55	-0.41	-0.28	-0.19	-0.16	-0.39
7. 2	-0.23	-0.31	-0.49	_0 00	-0.97	0.00	0.0*	_0 ~~	0.77	0.40	-0.00	004	_0.60
8. 2		1	-0.42 $-0.77$					-0.77	-0.71 -1.11		1		-0.60
8. 1							-1.43 $-1.44$					TOTAL STATE OF THE PARTY OF THE	-0.92 -0.98
7. 1	-0.26	-0.35	-0.55	-0.89	-0.97	-0.91	-0.98	-0.83	-0.80	-0.64			-0.65
MASSELLE I				1	1	0.01	0.00	0.00	0.00	0.04	0.01	0.20	0.00
9.12.3.9	H	-0.58	140000	12000000	-1.42	-1.12	-1.25	-1.26	-1.09	-0.94	-0.57	-0.35	-0.92
7. 2.2(9)	0.03	-0.03	0.06	0.10	0.04	0.05	0.02	0.11	0.12	0.05	-0.04	0.04	0.05
Dail.ext.	-0.25	-0.31	-0.20	_0 20	0.09	0.00	0.00	_0.0=	0.00	0.45	.0.00	_ 0.00	-0.05
- Juli CAG	11 0.20	1 0.01	0.29	1-0.28	0.09	0.03	-0.03	-0.05	-0.35	-0.45	-0.32	-0.29	-0.25

### XLVII.

Belgium. - Brussels. Lat. 50° 51' N. Long. 4° 22' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degree	es of Re	aumur.	0/201	-				
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
						200722							
Morn. 1	0.58	E COLUM	1.19		1000	2.83	2.34	2.49		10.700.000			100000
2	0.60	The state of	1.36	2.59	1 77.0	3.12	2.57	2.84	2.00	1000	FURL COST	100 7 7 7 7	
3	0.60	11/2/2017	1.54	2.99	3.17	3.18	2.74	3.20	ALC: U	1.30	Callering	0.08	100000
4	0.60	0.86	1.70	3.29	3.28	3.14	2.74	3.42	2.57	1.31	0.65	0.02	1.97
5	0.62	0.92	1.79	3.29	3.06	2.71	2.47	3.32	2.58	1.40	0.77	0.25	1.93
6	0.64	0.97	1.74	2.86		2.00	1.88	2.82	2.28	C. 24	1000	100000000000000000000000000000000000000	1.00
7	0.61	0.93	1.50	2.01	1.52	1.10	1.06	1.94	1.67	10000000	0.81	0.97	1
8	0.46	0.75	1.03	0.86		0.16	0.15	0.82	0.82		100 00	0.97	
												0.6	
9	0.18		0.39		The state of the s	-0.61	171-11		1 1 1 1 1 1 1 1 1 1 1	1	1	0.56	-0.08
10	-0.22	100000000000000000000000000000000000000	1111		-1.43							-0.13	
11	-0.65		-1.11	15	-2.06		Tar Charles	The second		-1.23		-0.84	
Noon	-1.01	-1.23	-1.72	-2.77	-2.52	-2.27	-2.06	-2.81	-2.48	-1.71	-1.16	-1.29	-1.92
1	-1.20	-1.57	_9 19	-3.11	_2 80	-2.65	-2.29	_2 2*	-2.88	_1 00	_1 20	_1 29	-2.22
2	-1.19		-2.13 $-2.29$	-3.11 $-3.29$	-2.89 $-3.21$	-2.05 $-2.97$	-2.29 $-2.51$	11 11 11 11	-2.88 $-3.05$	COM CE	-1.32 -1.27	-1.03	
3	-0.99			-3.33	O'CO TOTAL	-3.25	10000		-2.98	TOTAL CO. 1	ALC: U.S.	-0.59	166
4		-1.14	- 1,000		The same of	-3.16	THE CHARLES	a company to the company	-2.63	10000		-0.26	The state of
		10.1	1.00	0.10	0.00	0.10	2000	0.00	2.00	1.01	0	0.20	2.00
5	-0.39	-0.72	-1.51	-2.76	-2.97	-2.83	-2.47	-3.02	-2.05	-0.84	-0.45	-0.16	-1.68
6	-0.15	-0.33	-1.03	-2.05	-2.21	-2.17	-1.91	-2.19	-1.30	-0.39	-0.18	-0.25	-1.18
7	0.02	-0.03	-0.55	-1.13	-1.20	-1.28	-1.11	-1.15	-0.49	-0.01	0.03	-0.37	-0.61
8	0.12	0.17	-0.10	-0.16	-0.12	-0.31	-0.20	-0.09	0.23	0.28	0.19	-0.33	-0.03
9	0.21	0.31	0.28	0.69	0.82	0.68	0.64	0.82	0.78	0.48	0.32	0.05	0.50
10	0.31	0.41	0.59	1.31	1.51	1.37	1.31	1.48	1.13	0.60	0.41	0.37	0.90
Mid-	0.42	0.50	0.83	1.70	1.96	1.97	1.77	1.89	1.33	0.68	0.47	0.75	1.19
Midn	0.52	0.59	1.02	1.96	2.28	2.44	2.08	2.19	1.49	0.75	0.49	0.89	1.39
				14/4			4				THE STATE		
6. 6	0.25	0.32	0.35	0.41	0.12	-0.09	-0.01	0.31	0.49	0.48	0.33	0.20	0.26
7. 7	0.31	0.45	0.47	0.44	0.16	-0.09	-0.02	0.39	0.59	0.55	0.42	0.30	0.33
8.8	0.29	0.46	0.47	0.35	0.16	-0.07	-0.03	0.37	0.53	0.48	0.39	0.32	0.31
9. 9	0.20	0.35	0.34	0.17	0.12	0.04	-0.02	0.24	0.32	0.28	0.25	0.25	0.21
10.10	0.05	0.14	0.11	0.05	0.04	0.01	-0.01	0.05	0.03	0.00	0.05	0.12	0.05
* 0 0	0.50	0	0	0.00	0.00	0.10	0.00	0.00	0.00	0.00	0.00	0.0	00
7. 2. 9		-0.14	-0.17	= 13.75	-0.29	-0.40	1	-0.27			-0.05	1	-0.19
6. 2. 8	-0.14		-0.22	-0.20	-0.29	-0.43	-0.28	-0.28		120000	1		-0.22
6. 2.10	-0.08	THE REAL PROPERTY.	0.01	0.29	0.25	0.13	0.23	0.24	0.12		-0.00 -0.20		0.09
0. 2. 0	-0.23	-0.34	-0.53	-0.83	-0.99	-1.05	-0.00	-0.98	-0.09	0.33	-0.20	-0.21	-0.60
7. 2	-0.29	-0.36	-0.40	-0.64	-0.85	-0.94	-0.73	-0.82	-0.69	-0.42	-0.23	-0.03	-0.53
8. 2	100				-1.39					THE REAL PROPERTY.	200000	3417 - 41	1236 V C 1
8. 1					-1.23		1000			C. P. Control of		2017/10/20	
7. 1	-0.30	-0.32	-0.32	-0.55	-0.69	-0.78	-0.62	-0.67	-0.61	-0.43	-0.26	-0.18	-0.48
0.10.11													0.53
9.12.2.9	100000		Branch Co.		-1.42	ECU-UIII I	1	MARKET WAR	1	-0.72		-0.34	
7. 2.2(9)	-0.04	-0.03	-0.06	0.03	-0.01	-0.13	-0.04	-0.00	0.05	0.03	0.05	-0.04	-0.02
Dail.ext.	-0.28	-0.34	-0.25	-0.02	-0.06	-0.04	0.02	-0.14	-0.24	-0.28	-0.24	-0.18	-0.18
	0.20	0.04	0.20			0.01							

#### XLVIII.

Belgium. - Brussels. Lat. 50° 51' N. Long. 4° 22' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.30	0.60	1.09	1.72	2.27	2.46	2.20	1.88	1.52	0.92	0.51	0.30	1.31
2	0.56	0.82	1.39	2.19	3.00	2.82	2.77	2.44	2.03	1.20	0.77	0.47	1.70
4	0.64	0.97	1.66	2.64	3.32	3.53	3.14	2.76	2.38	1.44	0.83	0.62	1.99
6	0.66	1.03	1.83	2.43	2.44	2.27	2.30	2.44	2.47	1.56	0.93	0.63	1.78
8	0.67	0.84	1.02	0.76	0.49	0.41	0.32	0.68	1.03	0.96	0.79	0.63	0.72
9	0.36	0.33	0.21	-0.38	0.61	-0.61	-0.63	-0.39	-0.14	0.07	0.21	0.34	0.00
10	0.07	-0.09	-0.54	-1.18	-1.43	-1.32	-1.36	-1.26	-1.19	-0.78	-0.36	-0.08	-0.79
						4 64	111-25			13,00		+	
Noon.	-0.92	-1.27	-1.78	-2.42	-2.61	-2.47	-2.35	-2.47	-2.46	-1.87	-1.27	-0.83	-1.89
2			14 %	-2.95			-2.92				1		
4			-2.04			-3.18		-2.93	L. Santaland	-1.61		-0.65	-2.0
6	-0.21				-2.44		-2.38	-1.87	-1.21		-0.28	1000	13
8	-0.08		-0.00	0.13				0.17	0.21	0.23	0.07	-0.03	0.08
9	0.13	0.17	0.31	0.63				0.76	0.64	0.43	0.24	0.07	0.48
10	0.20	0.30	0.58	1.04		1.45	1.39	1.27	1.01	0.54	0.38	0.14	0.80
	ALC: N	71:27	19-11	S- 10	1000		1 4(4)			46.019	100	I date.	
High	0.50		2.70			10.10	10.00	10.50	11.00	- 00	1	1.00	
Mean.	0.52	2.45	3.56	7.27	10.37	13.10	13.69	13.58	11.22	7.69	4.72	1.89	1

#### XLIX.

Germany. — Schwerin. Lat. 53° 36' N. Long. 11° 30' E. Gr. — Dove.

29		BELL OF		1. 2				Tall.		20.00			150
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.05	0.49	0.92	1.66	1.97	2.10	2.12	1.92	1.70	0.87	0.21	0.16	1.18
2	0.08	0.69	1.20	2.17	2.44	2.69	2.72	2.41	2.19	1.14	0.24	0.34	1.53
4	0.27	0.83	1.43	2.53	2.96	2.97	2.96	2.62	2.54	1.51	0.42	0.48	1.79
6	0.35	0.86	1.62	2.67	2.07	1.80	1.94	2.13	2.70	1.67	0.62	0.48	1.55
8	0.59	1.19	1.24	0.98	0.56	0.25	0.12	0.32	0.95	1.21	0.70	0.63	0.73
10	0.17	0.18	-0.11	-0.97	-1.15	-1.20	-1.26	-1.17	-1.12	-0.34	0.01	0.13	-0.57
Par to	-		L.V.	-	/	lin itti				255,04	1000		34
		No.	3-1-10	45.44	98	Q HIGH	841	i lebri	- Burel	245	MONTH.	6013	
Noon.					-2.47	-2.36	-2.20	-2.29	-2.42	-1.80	-0.77	-0.43	-1.65
2	The second con-		-2.21		-3.38	-3.23	-3.26	-3.45	-3.58	-2.54	-0.91	-0.68	-2.42
4			-2.13	46046 6731	-2.70	-2.62	-2.76	-2.76	-3.03	-1.85	-0.62	-0.62	-1.97
6			-0.95		-1.62	-1.71	-1.70	-1.37	-1.32	-0.55	-0.23	-0.27	-0.98
8	100000	-0.07		0.13	0.11	-0.02	0.08	0.34	0.26	0.16	0.02	-0.14	0.06
10	0.06	0.21	0.45	1.01	1.15	1.28	1.29	1.30	1.19	0.57	0.24	-0.02	0.73
							113					- 411	
Mean.	-1.05	-2.00	1.18	5.26	8.45	12.19	13.50	13.02	10.42	7.48	1.42	-1.38	1

## PRUSSIA. — MÜHLHAUSEN. Lat. 51° 13' N. Long. 10° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean
1281700													N.
Morn. 1	0.71	1.28	1.10	1.84	2.40	30.101-61	2.91	2.49	1.95	1.39	0.47	0.58	1.7
2	0.75	1.30	1.28	2.19	2.80	3.97	3.30	2.80	2.20	1.65	0.53	0.59	1.9
3	0.77	1.33	1.46	2.40	3.06	4.16	3.50	3.06	3.29	1.85	0.60	0.60	2.1
4	0.82	1.40	1.60	2.74	3.06	3.98	3.42	3.14	2.70	1.99	0.66	0.62	2.1
5	0.86	1.47	1.62	2.61	2.67	3.40	3.00	2.98	2.73	2.05	0.68	0.66	2.0
6	0.91	1.50	1.46	2.25	2.06	2.49	2.22	2.51	2.46	1.93	0.63	0.67	1.7
7	0.86	1.36	1.11	1.41	1.15	1.32	1.20	1.73	1.03	1.50	0.46	0.59	1.1
8	0.62	0.98	0.55	0.58	0.16	0.11	0.09	0.86	0.87	0.84	0.16	0.46	0.5
9	0.21	0.33	-0.02	-0.38	-0.75	-1.02	-0.97	-0.36	-0.26	-0.03	-0.22	0.03	-0.2
10	-0.38	100000000000000000000000000000000000000	-0.70	A SECULARY			The second second		ALC: NO THE REAL PROPERTY.	MA TO STATE		111111111111111111111111111111111111111	
11		-1.35		-1.97	111 139 21 1		4 ( 5 ) ( )	1 to 15 cm	F (500) CA	Company of the			1000
Noon		-2.02	The state of the s	-2.42	100000000000000000000000000000000000000		1497 P. A. P. I		D-56000001	CALL PROPERTY.		-1.06	
1	_1 50	-2.38	_2 02	-2.80	-2.71	_2 26	_2 26	-3.29	_9 59	-2.82	-1.08	-1.15	-2.5
2	-1.52	-2.38	The second of		-2.87		100 110	-3.46	THE RESERVE	122 100 7 11			D T-00
3	77.72.97	-2.07		-2.85		14.0	ALCOHOL: THE	-3.39		15 10 10	7.7	-0.81	-2.4
4	100	-1.56	1 - 2 - 2 - 2	-2.39	-2.69	Charles Admin	<b>COOKING</b>	-3.07	HE SHOW THE PARTY		COLUMN TO STATE OF THE STATE OF	-0.50	
0-271-0	E-1140	estlor.	117.24	34,00	1	1- 3	25-310	31		0.083	4.000	G/E OF	6
5	-0.44	-1.02		-1.95	The second of	7.00	-2.52		-1.89	-1.21	-0.14	-0.23	56,0333
6	P. CECO	-0.54		-1.20				-1.76			0.02	-0.02	
7	-0.04	The second		-0.47		CL	E-96.0 (CO.)	-0.90			0.06	0.12	111111111111111111111111111111111111111
8	0.18	0.13	0.16	0.09	-0.08	0.05	0.03	-0.05	0.50	0.38	0.22	0.26	0.1
9	0.27	0.41	0.45	0.53	0.58	1.01	0.81	0.71	0.99	0.70	0.26	0.32	0.5
10	0.37	0.66	0.64	0.89	1.10	1.76	1.46	1.24	1.35	0.91	0.34	0.40	0.9
11	0.53	0.89		1.14	1.56		2.01	1.78	1.58	1.10	0.38	0.47	1.2
Midn	0.64	1.08	0.94	1.58	1.98	3.05	3.29	2.16	1.75	1.26	0.42	0.54	1.5
						.11.1							
6. 6	0.36	0.48	0.42	0.53	0.24	0.20	0.23	0.38	0.70	0.68	0.33	0.33	0.4
7. 7	0.41	0.60	0.47	0.47	0.16	0.15	0.18	0.42	0.40	0.74	0.26	0.36	0.8
8. 8	0.40	0.56	0.36	0.34	0.04	0.08	0.06	0.41	0.69	0.61	0.19	0.36	0.5
9. 9	0.24	0.37	0.22	0.08	-0.09	-0.01	-0.08	0.18	0.37	0.34	0.02	0.18	0.1
10.10	-0.01	0.08	-0.03	-0.14	-0.20	-0.11	-0.18	-0.07	-0.03	-0.04	-0.14	-0.07	-0.0
7. 2. 9	-0.13	-0.20	-0.17	-0.23	-0.38	-0.60	-0.47	-0.34	-0.51	-0.26	-0.06	-0.06	-0.2
6. 2. 8		-0.25	C. C. Connect			-0.53	100000	1 4 450 V F R	C 4.30	( ) The	1-00.000	CALL SHALL SHALL	
6. 2.10	-0.08	-0.07	0.01	0.07	0.10	0.04	0.09	0.10	0.09	-0.05	1	1	0.0
6. 2. 6	MC A LANGE	-0.47	PO 1700					-0.90					
7. 2	_0.32	-0.51	-0.48	-0.77	-0.86	-1.41	-1.11	-0.87	-1.26	-0.75	-0 22	-0.26	
8. 2			-0.76										
8. 1			-0.74										
7. 1			-0.46										
		1	To No.	-	. 1		1000		200				-6
9.12.3.9	11	1	-0.81		E-0758-0409	100	1 100		T-085-1456	500	1 10 10 3 11 1	A STATE OF	
7. 2.2(9)	-0.03	-0.05	-0.02	-0.12	-0.14	-0.20	-0.15	-0.08	-0.13	-0.02	0.02	0.03	-0.0
Dail.ext.	094	0.4	0.00	_0.10	0.00	0.01	001	0.16	0.10	0 10	007	1	

## HOLLAND. - UTRECHT. Lat. 52° 5' N. Long. 5° 8' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.36	0.62	1.13	1.71	2.56	2.74	2.64	1.87	1.91	1.07	0.76	0.11	1.4
1	0.37	0.74	1.18	1.87	2.86	3.29	2.67	1.91	2.10	1.11	0.70	0.19	1.5
2	0.46	0.82	1.24	2.00	3.00	3.21	2.82	2.02	2.21	1.18	0.78	0.32	1.6
3	0.51	0.87	1.27	2.10	3.02	3.25	2.97	2.07	2.34	1.25	0.82	0.42	1.7
4	0.57	0.90	1.31	2.16	2.70	2.84	2.76	2.06	2.45	1.31	0.82	0.44	1.6
5	0.61	0.97	1.26	1.92	1.80	1.82	1.86	1.80	2.42	1.42	0.90	0.50	1.4
6	0.66	0.98	1.02	1.30	0.67	0.44	0.33	1.05	1.87	1.22	0.91	0.46	0.9
7	0.64	0.84	0.62	0.37	-0.38	-0.70	-0.77	0.04	0.72	0.39	0.78	0.38	0.2
8	0.50	0.56	-0.01	-0.40	-1.17	-1.50	-1.28	-0.68	-0.39	0.12	0.29	0.31	-0.8
9	0.13	-0.07	-0.53	-1.20	-1.68	-2.02	-1.69	-1.33	-1.12	-0.50	-0.22	0.14	-0.8
10	-0.26	-0.49	-1.05	-1.71	-2.06	-2.42	-2.02	-1.65	-1.79	-1.12	-0.71	-0.14	-1.2
11	-0.62	-0.97	-1.50	-2.16	-2.46	-2.78	-2.27	-1.87	-2.34	-1.68	-1.15	-0.33	-1.6
Noon.	-0.85	-1.34	-1.77	-2.41	-2.78	-2.94	-2.53	-2.16	-2.83	-1.98	-1.49	-0.62	-1.9
1	-0.98	-1.58	-1.88	-2.42	-2.94	-3.00	-2.61	-2.40	-3.07	-2.11	-1.62	-0.75	-2.
2	-1.02	-1.54	-1.82	-2.42	-2.88	-2.94	-2.60	-2.30	-2.99	-1.99	-1.43	-0.66	-2.0
3	-0.81	-1.21	-1.54	-2.24	-2.58	-2.64	-1.58	-2.13	-2.68	-1.64	-1.08	-0.47	-1.
4	-0.60	-0.89	-1.25	-1.82	-2.06	-2.20	-2.00	-1.79	-2.06	-1.10	-0.70	-0.23	-1.3
5	-0.35	-0.48	-0.75	-1.23	-1.42	-1.53	-1.62	-1.30	-1.34	-0.52	-0.42	-0.17	-0.9
6	-0.19	-0.21	-0.24	-0.47	-0.76	-0.74	-0.76	-0.61	-0.52	-0.11	-0.18	-0.10	-0.4
7	-0.05	-0.03	0.14	0.20	0.07	0.17	0.02	0.14	0.10	0.22	-0.02	-0.03	0.0
8	0.05	0.12	0.48	0.72	0.85	1.01	0.82	0.86	0.62	0.53	0.18	0.02	0.
9	0.22	0.23	0.74	1.13	1.51	1.77	1.50	1.24	1.17	0.84	0.40	0.06	0.9
10	0.36	0.40	0.94	1.41	1.92	2.25	1.96	1.52	1.51	1.01	0.58	0.04	1.
11	0.36	0.67	1.02	1.58	2.16	2.53	2.17	1.70	1.76	1.14	1.06	0.02	1.
Mean	-2.83	4.18	3.20	7.14	10.55	12.95	13.75	12.90	10.87	6.88	4.65	0.76	

LII.

## England. — Greenwich. Lat. 51° 28′ 38″ N. Long. 0° 0′. — Dove.

Ho	ur.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.D	1.1	0.44	0.75	1.44	2.32	2.72	3.24	2.73	2.49	2.05	1.34	0.67	0.47	1.72
	3	0.62	0.94	1.66	2.66	3.04	3.70	3.11	2.82	2.40	1.42	0.80	0.56	1.98
	5	0.75	1.06	1.92	2.84	2.84	3.25	2.91	2.89	2.58	1.54	0.87	0.56	2.00
	7	0.86	1.08	1.60	1.31	0.75	0.80	0.88	1.22	1.65	1.26	0.88	0.60	1.07
	9	0.41	0.24	-0.22	-0.82	-1.30	-1.52	-1.14	-1.14	-0.76	-0.30	0.11	0.24	-0.50
	11	-0.74	-1.03	-1.90	-2.48	-2.60	-2.91	-2.67	-2.64	-2.57	-1.88	-1.06	-0.73	-1.93
P.N	1.1	-1.25	-1.73	-2.62	-3.31	-3.36	-3.75	-3.17	-3.40	-3.28	-2.40	-1.64	-1.20	-2.59
	3	-1.10	-1.59	-2.43	-3.08	-3.02	-3.60	-3.09	-3.20	-2.94	-2.04	-1.26	-0.85	-2.35
	5	-0.36	-0.63	-1.33	-2.04	-2.05	-2.51	-2.24	-2.11	-1.65	-0.73	-0.38	-0.24	-1.37
	7	0.03	0.05						-0.11			0.09	0.00	
1	9	0.10	0.32	0.71	0.99	1.20	1.40	1.13	1.22	0.89	0.63	0.40	0.21	0.77
	11	0.23	0.54	1.11	1.77	2.06	2.52	2.08	1.96	1.60	1.07	0.53	0.37	1.33
Me	an.	2.48	2.53	4.53	6.71	9.62	12.47	13.08	12.98	11.12	7.71	5.47	3.09	

### LIII.

### England. — Greenwich. Lat. 51° 29' N. Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	700						200	4	11.00		E.	3000	
Morn. 1	0.38	0.68	1.29	2.21	2.72	3.13	2.61	2.61	1.89	1.28	0.60		1.65
2	0.63	0.82	1.44	2.31	2.85	3.30	2.71	2.68	2.06	1.45	0.75	0.52	1.79
3	0.83	0.95	1.62	2.44	2.91	3.41	2.74	2.78	2.22	1.56	0.88	0.59	1.91
4	0.93	1.02	1.82	2.54	2.85	3.40	2.71	2.86	2.34	1.60	0.95	0.62	1.97
	0.00	1 00	7.05	0.40	0.00	9 14	2.53	2.81	0.05	1 50	0.95	0.62	1.01
5	0.93	1.03	1.95	2.46	2.60	3.14 2.52	2.53	2.48	2.35 2.15	1.56	0.95	0.62	1.91
6	0.84	0.97	1.93	2.17	2.08		1.38	1.77		The same of the sa	0.89	0.57	
7	0.71	0.84	1.66	1.56	1.25	1.53	STATE OF THE PARTY.		1.67	1.15	1100		1.24
8	0.53	0.61	1.11	0.66	0.20	0.28	0.40	0.72	0.88	0.71	0.52	0.48	0.59
9	0.30	0.26	0.30	-0.37	-0.92	-1.02	-0.71	-0.55	-0.13	0.09	0.19	0.28	-0.19
10	-0.01	-0.20	1.00	-1.43	1000	2.577	110000	1000	100000000000000000000000000000000000000	S PERMIT	-0.26		
11	-0.39	-0.75		-2.30					-2.22	14.07.77	-0.77		-1.73
Noon	-0.79	-1.27	-2.35		10.00	-3.28		-3.43		13.00	-1.25	-0.87	
		I CAL		Dr.	1000	180		3717		To la	1		
1	-1.12	-1.66	-2.79	-3.17	-3.26	-3.39	-3.04	-3.69	-3.28	-2.45	-1.59	-1.17	-2.55
2	-1.28	-1.81	-2.85	-3.14	-3.16	-3.34	-2.91	-3.63	-3.23	-2.48	-1.69	-1.25	-2.56
3	-1.21	-1.67	-2.57	-2.92	-2.90	-3.21	-2.67	-3.34	-2.86	-2.17	-1.51	-1.10	-2.34
4	-0.95	-1.29	-2.05	-2.54	-2.54	-3.01	-2.38	-2.89	-2.28	-1.63	-1.10	-0.76	-1.95
5	-0.58	-0.78	-1.40	-1.97	-2.06	-2.67	-2.30	-2.30	-1.60	-1.01	-0.59	-0.36	-1.45
6	-0.22	-0.26	-0.75	-1.34	-1.45	-2.10	-1.57	-1.56	-0.91	-0.43	-0.10	-0.01	-0.89
7	0.03	0.14	-0.17	-0.60	-0.71	-1.26	-0.96	-0.69	-0.27	0.02	0.24	0.20	-0.34
8	0.11	0.37	0.30	0.17	0.11	-0.24	-0.19	0.24	0.29	0.32	0.41	0.26	0.18
The second	Tue!	1-10	Jak to	I E				TA	100	133	I LEAD		The I
9	0.08	0.46	0.65	0.84	0.92	0.81	0.64	1.11	0.77	0.52	0.44	0.23	0.62
10	0.03	0.48	0.89	1.42	1.62	1.74	1.41	1.81	1.17	0.69	0.41	0.19	0.99
11	0.04	0.49	1.05	1.81	2.16	2.42	2.01	2.27	1.47	0.87	0.40	0.20	1.27
Midn	0.16	0.56	1.17	2.03	2.51	2.86	2.40	2.51	1.70	1.08	0.46	0.28	1.48
			-100	2 = 1	2.46				J.R				
6. 6	0.31	0.36	0.59	0.42	0.31	0.21	0.27	0.46	0.62	0.50	0.39	0.30	0.40
7. 7	0.37	0.49	0.75	0.48	0.27	0.13	0.21	0.54	0.70	0.59	0.50	0.38	0.45
8. 8	0.32	0.49	0.71	0.42	0.16	0.02	0.10	0.48	0.59	0.52	0.47	0.37	0.39
9. 9	0.19	0.36	0.48	0.24	0.00	-0.10	-0.04	0.28	0.32	0.31	0.31	0.25	0.22
10.10	0.01	0.14	0.12	-0.00	-0.16	-0.19	-0.16	0.01	-0.03	0.02	0.08	0.07	-0.01
7 2 0	0.10	0.75	0.10	0.05	0.00	-0.99	0.90	0.95	_0.00	_0 0~	_0.1	0.15	-0.94
7. 2. 9	-0.16	The same of the sa		1	-0.33	HOW BUILDING		1,26,30	455432	-0.27	1 1 may 2 mg	-0.15	24122
6. 2. 8	-0.11			-	-0.32 0.18	-0.35 0.31		0.22	0.03	- 10000	-0.13	11 1 1 2 2 2 2 2	-0.24
6. 2.10	-0.14			0.15					10.111111111111111111111111111111111111				0.04
6. 2. 6	-0.22	-0.37	-0.56	-0.77	-0.04	-0.97	-0.79	-0.90	70.00	-0.50	-0.30	-0.22	-0.59
7. 2	-0.29	-0.49	-0.60	-0.79	-0.96	-0.91	-0.77	-0.93	-0.78	-0.67	-0.47	-0.34	-0.67
8. 2	The sale of the sa	1	-0.87		Charles and	Contract of the		100000	Section Laboratory		2000	Delta Professional Assessment	Section 1
8. 1			-0.84										
7. 1		CC90,499 = 1	-0.57		100000000000000000000000000000000000000	C1340			The state of the s			- 11 DEC	CONTRACTOR OF THE PARTY OF THE
	1 MENT		13.33	667	1000					1,9	1		
9.12.3.9		PT 10-05	-0.99						The Part of the Pa	THE PARTY			CO CO CO
7. 2.2(9)	-0.10	-0.01	0.03	0.03	-0.02	-0.05	-0.06	0.09	-0.01	-0.07	-0.02	-0.06	-0.02
Dail.ext.	-0.18	-0.39	-0.45	-0.32	-0.18	0.01	-0.15	-0.42	-0.47	-0.44	-0.37	-0.32	-0.30
1													

LIV.

### England. — Greenwich. Lat. 51° 29' N. Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year.—GLAISHER.

Degrees of Fahrenheit.

					Degrees	of Fah	renheit.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
TO STATE OF											1		
Midn	1.0	1.6	2.9	4.8	5.4	6.2	5.0	5.1	4.0	2.9	1.7	0.9	3.5
1	0.9	1.8	3.0	5.2	6.0	7.1	5.5	5.5	4.5	3.0	1.8	1.0	3.8
2	1.2	2.0	3.3	5.7	6.4	8.0	6.0	6.0	5.5	3.4	2.0	1.2	4.2
3	1.3	2.1	3.6	6.2	6.7	8.7	6.4	6.3	6.4	3.6	2.0	1.3	4.5
4	1.6	2.3	3.9	6.6	6.7	9.3	6.6	6.5	6.6	3.8	2.1	1.4	4.8
5	1.8	2.2	4.0	6.7	6.3	8.8	6.2	6.5	6.2	3.8	2.0	1.4	4.7
6	1.9	2.3	3.9	6.0	4.8	6.4	4.5	5.5	5.3	3.5	1.9	1.4	3.9
7	1.9	2.1	3.6	4.3	2.6	3.0	2.5	3.3	4.0	2.8	1.7	1.5	2.8
8	1.5	1.6	2.5	2.0	0.5	0.0	0.0	0.9	2.1	1.6	1.0	1.3	1.2
9	1.0	0.7	0.2	-0.9	-2.0	-2.5	-2.0	-1.6	-0.4	0.0	0.4	0.9	-0.5
10	0.2	-0.5	-1.9	-3.2	-4.0	-4.5	-4.0	-3.5	-3.0	-2.0	-0.6	0.0	-2.2
11	-1.3	-2.1	-3.5	-5.3	-5.5	-5.8	-5.4	-5.4	-5.0	-3.8	-2.0	-1.3	-3.9
Noon	-2.3	-3.2	-5.0	-6.8	-6.7	-7.3	-6.4	-6.5	-6.4	-5.1	-3.1	-2.1	-5.1
1	-2.9	-3.9	-5.8	-7.9	-7.5	-8.1	-6.7	-7.5	-7.1	-5.5	-3.5	-2.4	-5.7
2	-3.0	-3.9	-5.8	-8.2	-7.7	-8.6	-6.7	-7.7	-7.1	-4.9	-3.6	-2.3	-5.8
3	-2.5	-3.6	-5.5	-7.7	-7.3	-8.4	-6.5	-7.0	-6.6	-3.7	-3.0	-1.9	-5.3
4	-1.9	-2.8	-4.5	-6.7	-6.1	-7.4	-5.8	-5.5	-5.5	-2.8	-2.1	-1.3	-4.4
5	-1.1	-1.6	-3.3	-5.4	-4.8	-6.1	-4.9	-3.6	-4.2	-1.7	-1.2	-0.8	-3.2
6	-0.6	-0.6	-1.8	-3.5	-3.0	-4.5	-3.5	-2.0	-2.5	-0.8	-0.4	-0.4	-2.0
7	-0.3	0.3	-0.4	-1.1	-1.0	-2.4	-1.5	-0.5	-0.6	0.0	0.1	-0.1	-0.6
BOY HES	10.00	Sec.	75501	1000	435/1	inter.	there	10.0	16030	(9/1)/07	(2.551)	100	11
8	0.1	0.6	0.9	0.7	0.9	0.0	0.3	1.0	1.0	0.7	0.6	0.2	0.6
9	0.4	1.0	1.7	2.0	2.3	1.8	1.9	2.4	1.8	1.3	1.0	0.4	1.5
10	0.6	1.3	2.3	3.2	3.5	3.6	3.3	3.3	2.7	1.9	1.3	0.5	2.3
11	0.7	1.5	2.6	4.1	4.5	5.0	4.2	4.3	3.4	2.4	1.5	0.8	2.9
			-81100	lacer.	1.0			2.0	A STATE OF				
	0.0	0.0	- 0							1000000			
6. 6	0.6	0.9	1.0	1.2	0.9	0.9	0.5	1.7	1.4	1.3	0.8	0.5	0.9
7. 7 8. 8	0.8	1.2	1.6	1.6	0.8	0.3	0.5	1.4	1.7	1.4	0.9	0.7	1.1
0. 8	0.8	1.1	1.7	1.3	0.7	0.0	0.1	0.9	1.5	1.1	0.8	0.8	0.9
9. 9	0.7	0.8	0.9	0.5	0.1	-0.3	-0.0	0.4	0.7	0.6	0.7	0.6	0.5
10.10	0.4	0.4	0.2	0.0	-0.2	-0.4	-0.4	-0.1	-0.1	-0.0	0.4	0.2	0.0
7. 2. 9	-0.2	-0.3	-0.2	-0.6	-0.9	-1.2	-0.8	-0.7	-0.4	-0.2	-0.3	-0.1	-0.5
6. 2. 8	-0.3	-0.3	-0.3	-0.5	-0.7	-0.7	-0.6	-0.4	-0.3	-0.2	-0.4	-0.2	-0.4
6. 2.10	-0.2	-0.1	0.1	0.3	0.2	0.5	0.4	0.3	0.3	0.2	-0.1	-0.1	0.1
6. 2. 6	-0.6	-0.7	-1.2	-1.9	-1.9	-2.2	-1.9	-1.4	-1.4	-0.7	-0.7	-0.4	-1.3
7. 2	-0.5	-0.9	-1.1	-1.9	-2.5	-2.8	-2.1	-2.2	1 5	_1.0	-0.9	-0.4	-1.5
8. 2	-0.7	-1.1	-1.6	-3.1	-3.6	Thomas A Torres	The same	The second	-1.5	-1.0	1 2 Dane		-1.3 -2.3
8. 1	-0.7	-1.1	-1.6	-3.1 $-2.9$		-4.3	-3.3	-3.4	-2.5	-1.7	-1.3	-0.5	
7. 1	-0.5	-0.9	-1.0	-2.9 -1.8	-3.5 -2.4	-4.0 -2.6	-3.4 -2.1	-3.3 -2.1	-2.5 -1.5	-1.9 -1.4	-1.3 -0.9	-0.5 -0.4	-2.2 -1.5
9.12.3.9	-0.8	-1.3	-2.1	-3.3	-3.4	-4.1	-3.2	-3.2	-2.9	-1.9	-1.2	-0.7	-2.4
	1 2.5	1 2.0	2.1	0.0	0.4	4.1	1 0.2	-3.Z	7-2.9	-1.9	-1.Z	1-0.7	-2.4

## PRUSSIA. - HALLE. Lat. 51° 30' N. Long. 11° 57' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						Degre	es of R	eaumur		1	-			
	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	Morn. 1	0.53	1.00	1.36	2.52	3.98	3.91	3.72	3.32	2.70	2.01	0.95	0.46	2.21
1	2	0.56	1.14	1.58	2.86	4.10	3.94	3.82	3.57	2.99	2.22	0.97	0.48	2.35
	3	0.60	1.26	1.74	3.00	3.78	3.62	3.56	3.56	3.12	2.37	1.01	0.50	2.34
	4	0.66		1.82	2.94				128					1
	5	0.72	1.36	1.72	2.62	2.18	2.09	2.14	2.64	2.62	2.25	1.00	0.55	1.82
1	6	0.72	1.30	1.42	1.98	1.30	1.18	1.24	1.90	1.97	1.90	0.92	0.58	1.37
1	7	0.65	1.10	0.94	1.07	0.32	0.25	0.23	0.84	0.98	1.32	0.74	0.55	0.75
	8	0.36		0.20	0.03	-0.56		-0.57	-0.20	0.12			1	
	9	0.05	-0.08	-0.66	-0.98	-1.34	-1.34	-1.30	-1.20	-1.14	-0.71	-0.31	-0.09	-0.76
1	10	-0.45	-0.76	-1.18	-1.86	-2.09	-2.01	-1.99	-2.10	-2.03	-1.66	-0.87	-0.54	-1.46
	11	-0.82	-1.29	-1.73	-2.58	-2.66	-2.68	-2.65	-2.90	-2.72	-2.44	-1.35	-0.90	-2.06
-	Noon	-1.09	-1.77	-2.06	-3.08	-3.14	-3.07	-3.16	-3.35	-3.11	-2.86	-1.66	-1.08	-2.45
	1	-1.17	-2.02	-2.22	-3.32	-3.33	-3.35	-3.46	-3.53	-3.30	-3.01	-1.73	-1.09	-2.63
1	2		-1.86	P. S. Contract	-3.26	-3.37	10000	-3.54			The state of the s	-1.52		-2.56
1	3	3 (3.2)	-1.49		-2.90	TO COLUMN		-3.29		-2.98		1	P. 1965.	
1	4		152	2.00	100								-0.74	
	4	-0.55	-1.01	-1.42	-2.39	-2.74	-2.14	-2.70	-2.84	-2.50	-1.81	-0.75	-0.42	-1.83
H	5	-0.30	-0.59	-0.91	-1.78	-2.24	-2.22	-2.16	-1.97	-1.83	-1.20	-0.40	-0.20	-1.32
	6	-0.13	-0.29	-0.52	-0.96	-1.58	-1.50	-1.39	-1.38	-1.12	-0.69	-0.14	-0.03	-0.81
I	7	-0.00	-0.09	-0.06	-0.34	-0.86	-0.73	-0.55	-0.59	-0.38	-0.21	0.04	0.09	-0.31
	8	0.11	0.13	0.26	0.32		0.07	0.26	0.15	0.29	0.25	0.21		-0.18
		III A		de la			140	dise.		Jaka	1-2			
	9	0.21	0.30	0.59	0.88	0.68	0.90	1.09	0.90	0.87	0.68	0.39	0.34	0.65
	10	0.31	0.46	0.79	1.33	1.64	1.81	1.87	1.61	1.42	1.12	0.59	0.37	1.11
	11	0.41	0.65	0.98	1.78	2.61	2.69	2.64	2.30	1.90	1.47	0.76	0.40	1.55
	Midn	0.48	0.83	1.16	2.17	3.43	3.42	3.29	2.86	2.33	1.77	0.89	0.43	1.92
							965				He V			
	6. 6	0.21	0.39	0.41	0.42	-0.03	-0.07	-0.01	0.34	0.40	0.53	0.30	0.18	0.26
	7. 7	0.30	0.51	0.45	0.51	-0.14	-0.16	-0.08	0.26	0.43	0.61	0.39	0.28	0.28
	8. 8	0.33	0.51	0.44	0.37	-0.27	-0.24	-0.16	0.13	0.30	0.56	0.39	0.32	0.22
I	9. 9	0.24	0.33	0.23	0.18	-0.33	-0.26	-0.16	-0.03	0.21	0.29	0.26	0.25	0.10
	10.10	0.13	0.11	-0.04	-0.05	-0.33	-0.22	-0.11	-0.15	-0.14	-0.02	0.04	0.13	-0.05
	7. 2. 9	-0.11	-0.20	-0.18	-0.34	-0.71	-0.70	-0.65	-0.49	-0.35	-0.29	-0.20	-0.10	-0.36
	6. 2. 8	-0.15	100000		1		The second second	A COURT OF THE PARTY OF THE PAR	-0.49	977			St. Co. Land	
	6. 2.10	-0.08		0.03	1000000	292	-0.12	ACCEPT.	1022	A STATE OF THE PARTY OF	100000000	-0.11		
ı	6. 2. 6	-0.25	1					12.00			100000000000000000000000000000000000000	-0.38	11.00	0.00
	0. 2. 0	0.20	0.12	0.1.	0.00	1.10	1.10	1.10	0.00	0.01	0.00	0.00	0.20	0.71
	7. 2		-0.36				47 30		110					
	8. 2	1	-0.46	0.100		and the same	7 7 7 7 1		1000	100000000000000000000000000000000000000	419 419 419		500000	1000
	8. 1	-0.22			The state of the s				-1.26	THE WAR PLANT		0.000	- C. II.	
-	7. 1	-0.19	-0.24	-0.32	-0.55	-0.92	-0.95	-0.96	-0.73	-0.57	-0.48	-0.37	-0.25	-0.54
	9.12.3.9	-0.35	-0.62	-0.84	-1.37	-1.67	-1.66	-1.63	-1.63	-1.40	-1.16	-0.59	-0.34	-1.10
-	7. 2.2(9)		-0.12	- 6										
-	Dail.ext.	-0.23	-0.33	-0.20	-0.16	0.37	0.24	0.14	0.00	-0.09	-0.30	-0.35	-0.26	-0.14
1														

LVI.

## Hanover. - Göttingen. Lat. 51° 32' N. Long. 9° 56' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Morn. 1						Degre	es of Re	aumur.						
1.1	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
1.1			10		la c					0.01		0.00		
3	Morn. 1								79				1000000	
4						1				9-5104		11/1/12/11	12 11 11 11	
5						197							- 7 - 1	
6	4	0.99	1.20	2.22	3.04	3.91	3.57	3.79	5.09	3.03	2.10	0.92	0.55	2.49
6	5	1 15	1.26	2.29	3.08	3,55	3.10	3.36	3.52	3.62	2.15	1.00	0.62	2.39
7		1000			- 3 -					4 - 4 (-1)				
8										1000000				77 79-54
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		1				0.75	0.49	0.48	0.56	1.36	1.08	0.53	0.54	0.80
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	REAL PROPERTY.		12.00						1348		1			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	0.50								10 A 1 L Mary 16/1	- Designation	- OF 1-	100000	N 12 - 1 - 1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$											The Party of the P		120000	C. CANTAGORIUS
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	The second second								6 3	111111111111111111111111111111111111111	- 17 - 5		412.00	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Noon	-1.83	-2.17	-2.43	-2.98	-3.30	-3.19	-3.48	-3.52	-3.37	-2.50	-1.46	-1.12	-2.61
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		_9 09	_0 20	_9 81	_2 27	_2 89	_2 70	_3 78	_3 89	_3 80	_2 80	-1 59	-1 49	_2 95
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$									1775		1000		The same of	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1		1					25,000 (19.00)	The Conduction	2 273.41	A STATE OF THE PARTY OF THE PAR	139.000.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			111111111111111111111111111111111111111										1000	
6		1.20	1.00	20.30	0121	0.01	0.00	0.02	01	0.02	2.10	0.00	0.00	2.00
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	-0.79	-0.59	-1.79	-2.64	-3.13	-3.09	-3.18	-3.15	-2.94	-1.74	-0.54	-0.36	-2.00
8	6	-0.33	-0.04	-1.06	-1.86	-2.40	-2.20	-2.40	-2.32	-1.97	-0.94	-0.23	-0.14	-1.32
9	7	-0.05	0.31	-0.26	-0.80	-1.44	-1.16	-1.30	-1.09	-0.87	-0.30	0.01	0.06	-0.57
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	0.24	0.58	0.34	0.04	0.22	-0.15	0.03	0.13	0.05	0.24	0.17	0.20	0.14
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				100		of all					Shue!	Ma.		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				STILL					5 3 4 4	LIKA L		170		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$									Profession of		100000	17 19 20 1		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	WELL STORY	17.9			3 10 10 10					TO SETTLE	0.00			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Midn	0.88	1.07	1.54	2.11	2.52	3.01	3.18	2.93	2.00	1.44	0.62	0.56	1.22
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					4								2.000	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6. 6	0.40	0.58	0.52	0.44	0.11	0.01	0.10	0.24	0.77	0.53	0.43	0.26	0.37
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			Company Company					0			- 1,000	S. T. Park Co.		CONTRACT DESIGNATION OF THE PERSON OF THE PE
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						2 4 4 11			A STATE OF THE PARTY OF THE PAR	DC0004C134		100000000000000000000000000000000000000		CATE THE
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			0.0		1000									1000000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10.10		1700	2							1000	-23100		11/2/11/2007
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		-	Ties in	Medi	100	800	-						Files	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										C 4611.1		0.00		1107727
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			0.3 8 6 6			V 2011				1771/2 1/4		1 7 - XX 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	CONTRACTOR OF THE PARTY OF THE	University
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Commence of the last			1	177.5			1		ATTENDED TO			100000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0. 2. 6	-0.41	-0.36	-0.67	-0.90	-1.25	-1.34	-1.30	-1.23	-0.82	-0.64	-0.25	-0.25	-0.79
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7. 2	-0.45	-0.55	-0.64	-0.66	-1.10	-1.41	-1 25	-1 22	-0.60	-0.70	-0 33	_0 39	-0.79
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	11				-1.34	-1.62	-1.77	-1.81	-1.80	-1.39	-0.95	-0.54	-0.37	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	The state of the s	-0.45	-0.76	-0.90	-1.24	-1.54	-1.62	-1.65	-1.63	-1.22	-0.91	-0.53	-0.44	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	7. 1	-0.45	-0.59											
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				T.						1				000
0.02 0.02 0.02 0.02 0.02 0.02 0.03	1		1000								-1.21	CLOSE IN NO.		A STATE OF THE STA
Dail. ext.   -0.44   -0.53   -0.38   -0.24   -0.03   -0.15   -0.09   -0.12   -0.20   -0.42   -0.26   -0.38   -0.30	7. 2.2(9)	-0.03	0.14	0.07	0.06	-0.11	-0.31	-0.13	-0.09	0.05	0.01	-0.02	-0.01	-0.03
	Dail ave	-0.41	-0.59	-0 20	-0.04	-0.00	_0 7-	0.00	0.70	0.00	0 10	0.00	0.00	0.00
	L Dail. CAL.	11 0.23	0.00	1-0.38	-U.Z4	-0.03	-0.19	1-0.09	-0.12	-0.20	<del>-0.42</del>	-0.26	-0.38	-0.30

#### LVII.

## PRUSSIA. - BERLIN. Lat. 52° 30' N. Long. 13° 24' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

	1		1			1	1			1			li.
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Midnight.	0.34	0.59	0.90	1.78	2.21	2.15	1.78	1.52	1.50	0.95	0.44	0.34	1.2
1	0.43	0.78	1.13	2.22	3.23	2.80	2.52	2.53	1.99	1.48	0.59	0.37	1.6
2	0.49	0.97	1.38	2.56	3.83	3.38	3.06	3.05	2.41	1.95	0.68	0.43	2.0
3	0.54	1.09	1.64	2.41	4.00	3.46	3.28	3.15	2.76	2.31	0.73	0.46	2.1
	0.58	1.05	1.85	3.03	3.77	3.18	0.10	0.40	0.04	0.45	0 =0	0.52	2.2
4 5	0.65	1.25 1.37	1.97	3.05	3.16	2.59	3.12 2.67	3.40	2.94	2.45	0.79	0.52	2.1
6	0.03	1.39	1.92	2.69	3.23	1.73	1.92	2.57	2.56	1.52	0.84	0.30	1.7
7	0.75	1.18	1.62	2.01	1.43	0.94	1.18	1.83	2.03	1.15	0.65	0.63	1.2
8	0.62	0.89	1.14	0.94	0.42	0.41	0.44	0.75	1.03	0.62	0.56	0.60	0.7
9	0.41	0.49	0.44	-0.17	-0.65	-0.40	-0.35	-0.36	-0.09	-0.04	0.35	0.38	0.0
10	0.19	-0.09	-0.25	-1.08	-1.47	-1.14	-1.15	-1.27	-0.81	-0.81	-0.09	0.05	-0.6
11	-0.30	-0.66	-1.02	-1.78	-2.20	-1.72	-1.78	-2.07	-1.90	-1.46	-0.55	-0.36	-1.8
Noon.	-0.55	-1.16	-1.44	-2.37	-2.65	-2.17	-2.26	-2.64	-2.49	-1.87	-0.95	-0.69	-1.7
1	CHARLES		-1.97						-2.96			-0.86	-2.1
2	-1.07		-2.20			-2.72		-3.17	-3.16	-2.23	-1.27	-0.96	-2.2
3	-1.03	-1.67	-2.28	-3.27	-3.34	-2.84	-2.82	-3.25	-3.19	-2.12	-1.20	-0.95	-2.3
4	-0.78								-3.16	THE RESERVE OF THE PARTY OF THE	100000	-0.73	-2.1
5									-2.34	CO TO		-0.48	-1.7
6		-0.74	-1.12		-2.35		-2.16	-2.21	-1.58	-0.87	-0.30	-0.25	-1.3
7	-0.22	-0.46	-0.64	-1.13	-1.55	-1.75	-1.44	-1.22	-0.82	-0.63	-0.11	-0.15	-0.8
8	-0.12	-0.20	-0.27	-0.34	-0.67	-0.57	-0.39	-0.30	-0.16	-0.30	0.05	-0.02	-0.2
9	0.06	0.03	0.05	0.40	0.13	0.31	0.38	0.84	0.36	-0.08	0.10	0.06	0.2
10	0.14	0.21	0.39	0.93	0.82	0.96	1.01	1.06	0.98	0.26	0.20	0.17	0.5
11	0.24	0.38	0.65	1.37	1.56	1.58	1.44	1.57	1.20	0.56	0.36	0.25	0.9
Aller al									3830				
6, 6	0.17	0.32	0.40		-0.06		-0.12	0.19	0.49	0.32	0.27	0.23	0.1
7, 7	0.27	0.36	0.49		-0.06		-0.13	0.30	0.60	0.26	0.27	0.24	0.2
8, 8	0.25	0.35	0.44		100F ART	-0.08	0.03	0.23	0.44	0.16	0.26	0.29	0.1
9, 9	0.24	0.26	0.30	0.12	0.21	-0.05	0.02	0.24	-0.23	-0.06	0.23	0.22	0.1
10, 10	0.17	0.06		100000000000000000000000000000000000000		CONTRACTOR OF STREET	-0.07		-0.09	ALC: 1 PATE 1	0.06	0.11	0.0
7, 1		-0.15	1		-0.79 $-0.56$	Carlo Carlos	-0.68 -0.36	-0.61 -0.17	-0.46 -0.26		-0.31	-0.12	-0.4
7, 2, 9	-0.09	-0.17	-0.18	100000000000000000000000000000000000000	-0.07	12 J. B. (15 to )	0.06	0.17		2000 431	-0.17	-0.09	-0.2
6, 2, 10	-0.07	-0.04	0.04						LICO.	4.0	-0.08	-0.03	-0.0
Daily ext.	-0.16	-0.17	-0.16	_0 11	0.33	0.31	0.23	0.08	-0.13	0 77	-0.22	A 10	0.0

#### LVIII.

## GERMANY. - SALZUFLEN. Lat. 52° 5' N. Long. 8° 40' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Re	aumur.		NEW Y	OF BETTE		Mark Par	and pe
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
M 1	0.00	1.10	1.05	2.11	2.41	2.57	2.05	1.71	2.12	1.24	0.90	0.31	1.46
Morn. 1	0.55	1.10	1.20	200	2.93	2.85			2.14	10,79,0000		0.48	1.77
3	0.60	1.27	1.34	2.64	3.29	2.98	E 1950	W 7/ 17 2 3	2.74	1 1 68	100000	100000000000000000000000000000000000000	1.96
4	0.62	1.26	1.38	2.62	3.37	2.86	A	Carried States	2.87	1.98	The second second	0.78	2.00
			1				C CONTR			L 5/10		A PO	
5	0.72	1.18	1.29	2.35	3.08	2.47		7777	100	1.97	1000	0.83	1.85
6	0.62	1.01	1.06	1.80	2.41	1.83			2.18	1.75		0.79	1.48
7	0.51	0.75	100000000000000000000000000000000000000	1.05	1.45	1.02			1.34	PARTIE DE		0.64	0.94
8	0.31	0.41	0.25	0.20	0.38	0.15	-0.06	0.08	0.30	0.75	0.62	0.38	0.31
9	0.08	-0.03	-0.22	-0.63	-0.59	-0.67	-0.74	-0.54	-0.65	0.09	0.14	0.06	-0.31
10	7.0	100000	200	- F.7 1944				-1.02	THE PERSON NAMED IN	The Personal Property lies	-0.35	6	
11	-0.74		-1.06		711	-1.94		-1.38			-0.02	12000	
Noon	-0.91	-1.42	-1.39	-2.32	-2.31	-2.39	-1.90	-1.72	-2.41	-1.78	-1.18	-0.62	-1.70
		The said			Selenti	ala.							
1	-1.01	-3" F 30 6		100 000 A							-1.48		
2		-1.74	5.0.00000000000000000000000000000000000							100	-1.56	1	
3	-0.79		-1.56					-2.42			-1.46	132	
4	-0.50	-1.29	-1.33	-2.21	-2.65	-2.71	-2.24	-2.30	-2.70	-1.76	-1.22	-0.41	-1.78
5	-0.20	-0.90	-0.98	-1.77	-2.39	-2.26	-1.89	-1.87	-2.25	-1.34	-0.92	-0.35	-1.43
6		-0.51	1000000	-1.22		1000	Part 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		A TOTAL OF		-0.65		- 1 - 1
7	0.01	-0.17	-0.15	-0.62	-1.34			0.47	-0.71		-0.44		
8	0.08	0.11	0.19	-0.04	-0.65	-0.09	0.09	0.21	0.12	-0.11	-0.31	-0.27	-0.06
							mac						
9	0.14	0.34	0.45	0.48	0.04	0.62	0.70		0.81		-0.20		0.34
10	0.21	0.55	0.63	0.94		1.22	1.26		1.30	1000	-0.06	1900	0.67
Midn	0.22	0.74	0.77	1.34	1.27	1.74	1.52	1.25	1.61	0.66		0.01	0.94
Widi	0.40	0.93	0.90	1.74	1.84	2.18	1.80	1.45	1.86	0.94	0.50	0.15	1.22
			3 17 1								1		321
6. 6	0.26	0.25	0.25	0.29	0.24	0.11	0.05	0.13	0.32	0.43	0.36	0.24	0.24
7. 7	0.26	0.29	0.28	0.22	0.06	0.08	0.04	0.16	0.32	0.44	0.30	0.17	0.22
8. 8	0.20	0.26	0.22	0.08	-0.14	0.03	0.02	0.15	0.21	0.32	0.16	0.06	0.13
9. 9	0.11	0.16	0.12	-0.08	-0.28	-0.03	-0.02	0.09	0.08	0.14	-0.03	-0.08	0.02
10.10	-0.06	0.01	-0.03	-0.21	-0.37	-0.08	0.06	0.01	-0.09	-0.11	-0.21	-0.18	-0.11
7. 2. 9	-0.10	-0.22	0.18	-0.90	0.00	0.40	0.00	0.00	0.00	0.00	0.01	0.05	0.05
6. 2. 8	-0.10		-0.17 -0.13	11200		7		-0.27 -0.20		100000000000000000000000000000000000000	-0.24	100000	
6. 2.10	-0.04	27.75.7	0.01	0.05	0.14	0.05	0.13	0.07	5 40 10 00	-0.18		0.03	0.04
6. 2. 6	-0.14		-0.38	THE PARTY NAMED IN	190000	2003-12017	1003 13.0	- 12 77 17	1000 FW	ALCOHOL: N	-0.28		
			0.00	0.01	00	.0.00	0.75	0.00	00	0.11	0.20	0.04	0101
7. 2	-0.22							-0.76					-0.54
8. 2											-0.47	-0.10	-0.86
8. 1		-0.64			C. C. C. Dark	C. SHIPPY	200000	-0.98	SCHOOL STATE	The state of the s	-0.43	-0.13	
7. 1	-0.25	-0.47	-0.45	-0.75	-0.54	-0.85	-0.72	-0.62	-0.71	-0.38	-0.22	-0.00	-0.50
9.12.3.9	-0.37	-0.67	-0.68	-1.94	_1.40	-1 24	-1.00	_0 00	-1.20	-0.80	-0.68	_0.39	-0.91
7. 2.2(9)	-0.04	-0.08	-0.01	-0.15	-0.28	-0.16	-0.05	-0.99	0.09		-0.68		
	March 1	1	19.01	650.33		0.10	0.00	0.02	0.02	0.12	0.23	0.03	0.10
Dail.ext.	-0.15	-0.24	-0.14	0.02	0.33	0.03	0.02	-0.08	-0.02	-0.10	0.04	0.10	-0.02

#### LIX.

PRUSSIA. - STETTIN. Lat. 53° 25' N. Long. 14° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

	TENOY.	Min.		1	Degre	es of A	eaumur.	Care la	1.16				
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Midnight.	0.26	0.54	0.98	1.66	2.21	2.21	1.83	1.93	1.53	0.88	0.50	0.39	1.2
1	0.38	0.59	1.17	1.91	2.66	2.46	2.25	2.24	1.61	1.01	0.44	0.46	1.4
2	0.43	0.70	1.30	2.15	3.03	2.84	2.62	2.54	1.87	1.13	0.47	0.50	1.6
3	0.49	0.88	1.41	2.39	3.39	3.10	2.95	2.83	2.11	1.24	0.51	0.56	1.9
		- Black		1803	III.			Ph. L		2:3	民儿	101	
4	0.53	0.89	1.51	2.60	3.58	3.08	3.07	3.08	2.33	1.33	0.55	0.61	1.9
5	0.55	0.89	1.63	2.67	3.45	2.78	2.85	3.10	2.46	1.40	0.58	0.61	1.9
6	0.55	0.94	1.62	2.40	2.78	2.12	2.21	2.78	2.45	1.42	0.60	0.56	1.
7	0.46	0.83	1.37	1.70	1.63	1.17	1.31	2.02	1.98	1.25	0.52	0.46	1.5
											172		
41-101	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00		0.00	0.40	0.00	
8	0.36	0.66	0.90	0.66 -0.42	0.33	0.20	March 1	0.96	1.11	0.79		0.38	
10	-0.04	-0.02		-0.42 $-1.36$		-0.72 $-1.54$	1 1000 1000		-0.05 $-1.11$	-0.55		-0.03	1000
11	-0.36	-0.53	4.01.5	Contract Contract	4 3 3 3 3 3 3			-2.23			1	-0.35	1000
	-0.00	0.00	1.00	2.01	2.02	2.10	1.00	2.20	1.50	1.20	-0.00	-0.00	
Noon.	_0.63	0 03	-1.59	_2 50	-3 00	_2.59	-2 46	-2.93	-2.58	_1 69	_0 00	-0.64	_1.5
1	-0.81	1 3 3 4 7 7 7	-1.92				1	-3.38		13. 1300		-0.86	1
2		-1.39	The second second second	-2.94			-2.99	-3.50		-2.06		-0.94	
3	11	1000000	-2.06	The same of the sa	122211		H-16 C C T T T	-3.38		1 - 1 - 1 - 1	1		-2,
		HALL THE			6					THE REAL PROPERTY.	CI S		
4	-0.63	-1.15	-1.84	-2.54	-2.99	-2.99	-2.60	-3.03	-2.44	-1.43	-0.68	-0.70	-1.9
5			1		A CONTRACTOR OF THE PARTY OF TH						National Asset	-0.48	
6	-0.25	-0.46	-0.90	-1.32	-1.74	-1.74	-1.62	-1.68	-1.14	-0.46	-0.19	-0.30	-0.9
7	-0.11	-0.23	-0.40	-0.55	-0.89	-0.89	-0.93	-0.78	-0.52	-0.10	-0.00	-0.18	-0.
						100	13						
8	0.01	-0.04	-0.02	0.10	-0.14	-0.14	-0.17	0.02	0.06	0.17	0.18	-0.06	-0.0
9	0.08	0.16	0.32	0.68	0.73	0.73	0.48	0.74	0.60	0.39	0.30	0.07	0.5
10	0.20	0.30	0.61	. 1.10	1.30	1.30	1.03	1.20	1.00	0.58	0.43	0.22	0.
11	0.25	0.42	0.79	1.42	1.76	1.76	1.47	1.60	1.31	0.74	0.50	0.32	1.0
		15 18	- CAU	E8,0		All Par				3475			
					0 40	0.00	0.00						
6, 6	0.15	0.24	0.36	0.54	0.52	0.19	0.29	0.55	0.65	0.48	0.21	0.13	0.5
7, 7	0.17	0.30	0.48	0.57	0.37	0.14	0.19	0.62	0.73	0.57	0.26	0.14	0.3
8, 8	0.19	0.31	0.44	0.38	-0.08		-0.03	0.49	0.59	0.48	0.31	0.16	0.3
9, 9	0.15	0.20	0.20	0.15	-0.00	0.01	-0.03	0.24	0.20	0.45	0.22	0.15	0.1
70.70	0.03	0.14	0.00	0.19	_0.20	_0.19	0.15	-0.10	0.00	0.02	0.77	0.70	1
10, 10	-0.17		-0.67							AND DESCRIPTION OF THE PERSON NAMED IN COLUMN TWO IN COLUM	0.11	0.10	-0.0 -0.8
7, 1	-0.17	100	-0.13	4115C 17C1			-0.40	A COLUMN	-0.45		-0.27		-0.2
6, 2, 10	-0.15	The same of the sa	0.38	0.19	0.19	0.14	0.08	0.16		100	-0.01		0.0
0, 2, 10		-	HAL	28.34		THE LE		AL-II-		0.02	0.01	0.00	0.0
Daily ext.	-0.16	-0.21	-0.23	-0.14	0.04	0.06	0.04	-0.20	-0.27	-0.32	-0.23	-0.15	-0.1
	N.E.	1 - 20	No.			E LUTE	10.00				The STU	1700	19

#### LX.

## SLESWICK. — APENRADE. Lat. 55° 3' N. Long. 9° 25' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — DOVE.

ATTACHED BY	SERVED OF		A SHOW		Degree	s of Re	aumur.		No.		and the	100	Sales Contract
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Mam 1	0.26	0.69	0.98	1.73	3.18	3.82	2.50	2.61	2.16	1.06	0.54	0.31	1.65
Morn. 1	100000000		2.7			AND 11.3			THE PARTY				
2	0.31	0.78	1.14	1.83	3.17	3.90	2.38	2.66	2.29	1.19	0.59	0.35	1.72
3	0.38	0.79	1.26	1.98	3.02	3.82	2.13	2.66	2.54	1.30	0.64	0.37	1.74
4	0.42	0.75	1.34	2.10	2.71	3.50	1.78	2.64	2.62	1.37	0.66	0.38	1.69
5	0.44	0.69	1.31	2.02	2.22	2.89	1.35	2.18	2.43	1.36	0.69	0.40	1.50
6	0.50	0.62	1.18	1.63	1.54	1.94	0.86	1.56	2.02	1.25	0.69	0.40	1.18
7	0.47	0.54	0.90	1.15	0.70	0.83	0.30	0.77	1.18	0.97	0.61	0.37	0.73
8	0.39	0.38	0.50	0.41	-0.23	100000000000000000000000000000000000000	-0.29	-0.18	0.18	0.52	0.42	0.27	0.17
9	0.23	0.10	-0.02	-0.42	-1.14	-1.38	-0.87	-1.10	-0.83	-0.10	0.10	0.10	-0.44
10	-0.06	-0.32	-0.66	-1.22	-1.90	-2.16	-1.40	-1.98	-1.71	-0.79	-0.30	-0.15	
11	0.00	-0.78		-1.90							-0.68	-0.43	-1.41
Noon	- 200	-1.19		-2.42				15.	2011/1	223/2/2		-0.66	
		ST-DE	3	ma, in		THE R.	11111	(= 22)		FLOX	130,30		St. St. St.
1	-0.78	-1.40	-1.90	-2.75	-3.08	-3.24	-2.23	-2.89	-3.03	-2.15	-1.10	-0.78	-2.11
2	-0.69	-1.34	-1.96	-2.89	-3.16	-3.49	-2.27			-2.07	-1.02	-0.75	-2.14
3	-0.61	-1.06	-1.78	-2.79	-3.10	-3.68	-2.21	-2.78	-2.93	-1.74	-0.82	-0.59	-2.01
4	-0.38	-0.64	-1.41	-2.43	<b>-2.</b> 86	-3.62	-2.02	-2.39	-2.54	-1.23	-0.59	-0.38	-1.71
5	-0.16	-0.23	-0.92	-1.80	-2.40	-3.34	-1.70	-2.02	-1.93	-0.71	-0.29	-0.15	-1.30
6	-0.03	0.05	-0.42	-0.99	-1.70	-2.57	-1.18	-1.23	-1.13	-0.25	-0.12	0.02	-0.80
7	0.01	0.18	0.02	-0.12	-0.79	-1.42	-0.57	-0.47	-0.26	0.10	0.02	0.10	-0.27
8	0.03	0.18	0.33	0.66	0.22	-0.07	0.18	0.40	0.56	0.34	0.03	0.14	0.25
9	0.01	0.17	0.54	1.25	1.22	1.25	0.97	1.21	1.21	0.51	0.09	0.15	0.71
10	0.02	0.22	0.66	1.57	2.05	2.33	1.63	1.72	1.61	0.65	0.18	0.18	1.07
11	0.07	0.33	0.76	1.69	2.66	3.10	2.14	2.25	1.83	0.85	0.30	0.21	1.35
Midn	0.15	0.52	0.86	1.70	3.02	3.57	2.43	1.68	1.97	0.92	0.42	0.26	1.46
6. 6	0.24	0.34	0.38	0.32	-0.08	-0.32	-0.16	0.17	0.45	0.50	0.29	0.21	0.19
7. 7	0.24	0.36	0.46	17771000		11000	-0.14		0.46	0.54		0.24	0.23
8. 8	0.21	0.30	0.42	100000000000000000000000000000000000000		-0.21	AND DESCRIPTION OF THE PERSON	0.11	OF THE PARTY.	0.43	0.23	0.21	0.21
9. 9	0.11	0.14	0.42	0.42	0.01	-0.07	0.05	0.06	0.19	0.21	0.10	0.13	0.14
10.10	-0.02	-0.05	-0.00	0.18	0.08	0.09	0.12	-0.13		-0.07		0.02	0.01
7. 2. 9	-0.08	-0.21	-0.17	-0.16	-0.41	-0.47	-0.33	-0.31	-0.23	-0.20	-0.11	-0.08	-0.23
6. 2. 8	711/200	- 1 To 1 To 1 To 1	-0.15				. 343	10000	000	30000		-0.07	100000000000000000000000000000000000000
6. 2.10	1000	-0.17		0.10	0.14	0.26		0.13	2007	12000	0.200	-0.06	0.04
6. 2. 6		-0.22	10000	-0.75	3200.00			1/11/11/19/19		The state of the s		-0.11	
		2249			Malar		Cat.com	1		(A)	-		
7. 2			-0.53	Market		14.00	112712100			4-01	1	1	
8. 2		-0.48		-1.24						THE STREET	.000	-0.24	
8. 1		-0.51		-1.17									
7. 1	-0.16	-0.43	-0.50	-0.80	-1.19	-1.21	-0.97	-1.06	-0.93	-0.59	-0.25	-0.21	-0.69
9.12.3.9	-0.25	-0.50	-0.72	-1.10	-1.47	-1.70	-1.05	-1.35	-1.34	-0.82	-0.40	-0.25	-0.91
7. 2.2(9)	-0.06	-0.12	0.01	0.19		-0.04	. DE90 OF B	0.07		-0.02			0.01
Dail.ext.	-0.14	-0.31	-0.31	-0.40	0.01	0.11	0.12	-0.12	-0.23	-0.39	-0.21	-0.19	-0.20

#### LXI.

Scotland. - Leith. Lat. 55° 59' N. Long. 3° 10' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

	200				Degree	s of Fal	пеппет	•					
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	0.00	0.00	1 20	0.00	0.04	0.00	4.70	0.05	0.54	1.10	1.00	0 **0	- 00
Morn. 1	0.38	0.86	1.76	3.02	3.04	3.29	4.10	2.95	2.54	1.10	1.26	2000	
2	0.61	0.77	1.98	3.92	3.47	3.62	4.28	3.20	2.77	1.19	1.53	0.65	2.33
3	0.68	0.77	2.41	4.57	3.96	3.74	4.66	3.49	3.29	1.31	1.40	0.61	2.57
4	0.95	0.95	2.59	5.31	4.41	3.98	5.11	3.71	3.65	1.33	1.46	0.70	2.84
5	1.06	1.17	2.75	5.49	4.28	3.94	4.59	3.65	3.78	1.62	1.37	0.77	2.87
6	1.06	1.31	2.79	5.36	3.51	3.04	3.56	3.26	3.51	2.03	1.28	0.59	2.61
7	0.97	1.24	2.48	3.47	2.66	2.25	2.39	2.25	2.75	1.62	1.06	0.68	1.98
8	0.88	1.26	1.80	2.18	1.40	1.10	1.15	1.08	1.46	0.97	1.04	0.54	1.24
9	0.61	0.77	0.81	-0.27	0.11	-0.18	-0.23	-0.50	-0.14	0.32	0.56	0.32	0.18
10	0.16	100000000000000000000000000000000000000	0.18	The same of the sa	1000 100			-1.26	1500000	-0.83	I SHOW MALE		
11	-0.34		23 -41					-2.03	The second			-0.86	
Noon		-1.69	The second	-3.92	CONTRACTOR OF THE PARTY OF THE	-2.79	ALCOVO CHEC		-3.13				-2.51
Page 1	7 40	9.05	0.05	4.00	9.05	9.15	9.0=	9.44	9.00	0 =0	0.00		
1	-1.42			The State of the S				-3.44		-2.79			
2			1000					-3.65					
3		-2.27	400000	Advisor to the same of	The second second	The second of the		-3.65	CONTRACT.			-1.13	
4	-1.19	-1.73	-3.33	-4.79	-4.19	-3.94	-4.46	-3.87	-3.56	-1.96	-1.69	-0.83	-2.96
5	-0.68	-0.95	-2.84	-4.25	-4.03	-3.71	-4.57	-3.76	-3.56	-1.31	-1.04	-0.50	-2.60
6	-0.45	-0.47	-2.14	-3.83	-3.51	-3.29	-4.41	-3.47	-2.30	-0.59	-0.68	-0.27	-2.12
7	-0.09	-0.09	-1.17	-2.45	-2.61	-2.52	-3.58	-1.69	-0.97	0.05	-0.25	0.18	-1.27
8	0.14	0.32	-0.45	-0.81	-1.17	-0.79	-1.31	-0.41	-0.16	0.59	0.05	0.29	-0.31
9	0.23	0.61	0.25	0.38	0.32	0.50	0.43	0.59	0.59	0.72	0.32	0.36	0.44
10	0.18	0.88	0.77	1.08	0.86	1.89	1.71	1.58	1.24	1.15	0.79	0.41	1.04
11	0.32	0.99	1.31	2.18	1.69	2.16	2.52	2.23	1.67	1.60	1.19	0.54	1.53
Midn	0.38	1.01	1.44	2.68	2.32	2.68	3.44	2.77	2.27	1.49	1.42	0.59	1.87
				1	100							0.00	
6. 6	0.32	0.43	0.34	0.77	0.00	-0.14	-0.43	-0.11	0.61	0.72	0.32	0.16	0.25
7. 7	0.45	0.59	0.65	0.52	200	-0.14	I SCHOOL SECTION	0.29	0.90	0.83	0.41	0.43	0.36
8.8	0.52	0.79	0.68	0.70	0.11	The second	-0.09	0.34	0.65	0.79	0.54	0.43	0.47
9. 9	0.43	0.70	0.54	0.07	0.23	0.16	0.11	0.05	0.23	0.52	0.45	0.34	0.32
10.10	0.18	0.41	0.47	-0.47	-0.11	0.29	0.18	0.16	0.07	0.16	0.23	0.20	0.15
		The same		12- 20			the last		-		Trans.		0.10
7. 2. 9	-0.14	25000000	100000	-0.29	-0.0	The State of the S	1. Table 1. No. 1		-0.32	Purchasing the second	-0.41	11/27	-0.26
6. 2. 8	-0.14	Addition of the	1000	Dec 100	ACCOUNT OF THE PARTY OF	-0.52	TO ANGLE STORY		-0.32	1.00	1-157 0000	-0.23	-0.30
6. 2.10	-0.11	-0.02	0.09	0.56	0.20	0.36	0.41	0.41	0.16	0.11	-0.16	-0.18	0.15
6. 2. 6	-0.32	-0.47	-0.88	-1.06	-1.26	-1.35	-1.64	-1.28	-1.01	-0.47	-0.65	-0.41	-0.90
7. 2	-0.32	-0.50	-0.41	-0.63	-0.56	-0.79	-0.86	-0.70	-0.77	-0.61	-0.77	-0.45	-0.61
8. 2								-1.28					
8. 1								-1.19					
7. 1	100000000000000000000000000000000000000	1		1000		TOTAL STREET		-0.61	11/20/2005	TOTAL GOOD	TARREST LAND	and the same of	
4 10 0 0	0.15	0.0-	104	0.00	1.00	1 83	104	1.04	1	0.05	0.00	0.45	1 00
9.12.3.9	C 1090 1150	-0.65	I KIE SPE	10000000	OLO SHEN	CONTRACTOR OF THE PARTY OF THE		-1.64 $-0.07$	OPS ALC:	1000 000	0.00	-0.45	
7. 2.2(9)	-0.05	0.07	-0.09	-0.14	-0.14	-0.10	-0.20	-0.07	-0.09	0.07	-0.23	-0.05	-0.09
Dail. ext.	-0.27	-0.49	-0.29	0.20	-0.11	-0.20	0.27	-0.09	-0.25	-0.40	-0.56	-0.40	-0.20

#### LXII.

## Scotland. - Leith. Lat. 55° 59' N. Long. 3° 10' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

	-						Degree	es of Re	aumur.			11-31-3			
2		Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean,
2	1			Line.					1	11.21.1				YE I	
3	-							1000				-100			
1.26	-	2								1.42	1.23	0.53	0.68	0.29	1.04
5	1	3	0.30	0.34	1.07	2.03	1.76	1.66	2.07	1.55	1.46	0.58	0.62	0.27	1.14
6	1	4	0.42	0.42	1.15	2.36	1.96	1.77	2.27	1.65	1.62	0.59	0.65	0.31	1.26
6	1	5	0.47	0.52	1.22	2.44	1.90	1.75	2.04	1.62	1.68	0.72	0.61	0.34	1.28
7		6		0.58	1.24	2.38	1.56		1.58						
8	1											1000000			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		8	0.39	0.56	0.80	0.97	0.62	0.49	0.51	0.48	0.65	0.43		1000000000	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		9	0.27	0.34	0.36	-0.12	0.05	-0.08	-0.10	-0.22	-0.06	0.14	0.25	0.14	0.08
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$											100000	4.			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						/									
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						1									
2		Zidon	0.10		2.10				1.00	2.00	2.00	2,00	0.01	0.00	1.12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	1	-0.63	-1.00	-1.32	-1.94	-1.49	-1.40	-1.63	-1.53	-1.74	-1.24	-1.02	-0.67	-1.30
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		2	-0.70	-0.99	-1.46	-2.10	-1.68	-1.70	-1.81	-1.62	-1.90	-1.26	-1.14	-0.69	-1.42
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		3	-0.71	-1.01	-1.50	-2.26	-1.71	-1.94	-1.94	-1.62	-1.85	-1.14	-1.17	-0.50	-1.45
6		4	-0.53	-0.77	-1.48	-2.13	-1.86	-1.75	-1.98	-1.72	-1.58	-0.87	-0.75	-0.37	-1.32
7		5	-0.30	-0.42	-1.26	-1.89	-1.79	-1.65	-2.03	-1.67	-1.58	-0.58	-0.46	-0.22	-1.15
8		6	-0.20	-0.21	-0.95	-1.70	-1.56	-1.46	-1.96	-1.54	-1.02	-0.26	-0.30	-0.12	-0.94
9 0.10 0.27 0.11 0.17 0.14 0.22 0.19 0.26 0.26 0.32 0.14 0.16 0.20 10 0.08 0.39 0.34 0.48 0.38 0.84 0.76 0.70 0.55 0.51 0.35 0.18 0.46 11 0.14 0.44 0.58 0.97 0.75 0.96 1.12 0.99 0.74 0.71 0.53 0.24 0.68 Midn 0.17 0.45 0.64 1.19 1.03 1.19 1.53 1.23 1.01 0.66 0.63 0.26 0.83    6. 6 0.14 0.19 0.15 0.34 0.00 -0.06 -0.19 -0.05 0.27 0.32 0.14 0.07 0.11 7. 7 0.20 0.26 0.29 0.23 0.01 -0.06 -0.27 0.13 0.40 0.37 0.18 0.19 0.16 8. 8 0.23 0.35 0.30 0.31 0.05 0.07 -0.04 0.15 0.29 0.35 0.24 0.19 0.21 9. 9 0.19 0.31 0.24 0.03 0.10 0.07 0.05 0.02 0.10 0.23 0.20 0.15 0.14 10.10 0.08 0.18 0.21 -0.21 -0.05 0.13 0.08 0.07 0.03 0.07 0.10 0.09 0.06    7. 2. 9 -0.06 -0.06 -0.08 -0.13 -0.12 -0.16 -0.19 -0.12 -0.14 -0.07 -0.18 -0.08 -0.12 6. 2.8 -0.06 -0.09 -0.14 -0.03 -0.21 -0.23 -0.27 -0.12 -0.14 -0.03 -0.18 -0.10 -0.13 6. 2.10 -0.05 -0.01 0.04 0.25 0.09 0.16 0.18 0.18 0.07 0.05 -0.07 -0.08 0.07 6. 2.6 -0.14 -0.21 -0.39 -0.47 -0.56 -0.60 -0.73 -0.57 -0.45 -0.21 -0.29 -0.18 -0.40    7. 2 -0.14 -0.22 -0.18 -0.28 -0.25 -0.35 -0.38 -0.31 -0.34 -0.27 -0.34 -0.20 -0.27 8. 2 -0.16 -0.22 -0.33 -0.57 -0.53 -0.61 -0.65 -0.57 -0.63 -0.42 -0.34 -0.23 -0.44 8. 1 -0.12 -0.23 -0.11 -0.20 -0.16 -0.20 -0.29 -0.27 -0.26 -0.26 -0.28 -0.18 -0.21 -0.21 -0.20 -0.29 -0.27 -0.20 -0.29 -0.27 -0.20 -0.29 -0.27 -0.20 -0.29 -0.27 -0.20 -0.29 -0.27 -0.20 -0.29 -0.20 -0.29 -0.27 -0.20 -0.29 -0.27 -0.20 -0.29 -0.20 -0.29 -0.20 -0.29 -0.20 -0.29 -0.20 -0.29 -0.20 -0.20 -0.29 -0.20 -0		7	-0.04	-0.04	-0.52	-1.09	-1.16	-1.12	-1.59	-0.75	-0.43	0.02	-0.11	0.08	-0.56
9 0.10 0.27 0.11 0.17 0.14 0.22 0.19 0.26 0.26 0.32 0.14 0.16 0.20 10 0.08 0.39 0.34 0.48 0.38 0.84 0.76 0.70 0.55 0.51 0.35 0.18 0.46 11 0.14 0.44 0.58 0.97 0.75 0.96 1.12 0.99 0.74 0.71 0.53 0.24 0.68 Midn 0.17 0.45 0.64 1.19 1.03 1.19 1.53 1.23 1.01 0.66 0.63 0.26 0.83    6. 6 0.14 0.19 0.15 0.34 0.00 -0.06 -0.19 -0.05 0.27 0.32 0.14 0.07 0.11 7. 7 0.20 0.26 0.29 0.23 0.01 -0.06 -0.27 0.13 0.40 0.37 0.18 0.19 0.16 8. 8 0.23 0.35 0.30 0.31 0.05 0.07 -0.04 0.15 0.29 0.35 0.24 0.19 0.21 9. 9 0.19 0.31 0.24 0.03 0.10 0.07 0.05 0.02 0.10 0.23 0.20 0.15 0.14 10.10 0.08 0.18 0.21 -0.21 -0.05 0.13 0.08 0.07 0.03 0.07 0.10 0.09 0.06    7. 2. 9 -0.06 -0.06 -0.08 -0.13 -0.12 -0.16 -0.19 -0.12 -0.14 -0.07 -0.18 -0.08 -0.12 6. 2. 8 -0.06 -0.09 -0.14 -0.03 -0.21 -0.23 -0.27 -0.12 -0.14 -0.03 -0.18 -0.10 -0.13 6. 2.10 -0.05 -0.01 0.04 0.25 0.09 0.16 0.18 0.18 0.07 0.05 -0.07 -0.08 0.07 6. 2 6 -0.14 -0.21 -0.39 -0.47 -0.56 -0.60 -0.73 -0.57 -0.45 -0.21 -0.29 -0.18 -0.40    7. 2 -0.14 -0.22 -0.18 -0.28 -0.25 -0.35 -0.38 -0.31 -0.34 -0.27 -0.34 -0.20 -0.27 8. 2 -0.16 -0.22 -0.33 -0.57 -0.53 -0.61 -0.65 -0.57 -0.63 -0.42 -0.34 -0.23 -0.44 8. 1 -0.12 -0.22 -0.26 -0.49 -0.44 -0.46 -0.56 -0.53 -0.55 -0.41 -0.28 -0.22 -0.38 7. 1 -0.10 -0.23 -0.11 -0.20 -0.16 -0.20 -0.29 -0.27 -0.26 -0.26 -0.28 -0.18 -0.21 -0.21 -0.20 -0.29 -0.27 -0.20 -0.29 -0.27 -0.26 -0.26 -0.28 -0.18 -0.21 -0.20 -0.09 -0		8	0.06	0.14	-0.20	-0.36	-0.52	-0.35	-0.58	-0.18	-0.07		0.02		
10	1		100				L. Seri	7							
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	A. C.	77	THE PERSON		C. Property		1		P. L. Connection	4-14		1.555.20	11000000	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-			1 1 1 1 1 1 1			( D)				1000000		100000000000000000000000000000000000000	1000000	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1700	0.000		T 27 Table 1	1.7					1500		Address of the Control of the Contro	100,705,50	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		Midn	0.17	0.45	0.64	1.19	1.03	1.19	1.53	1.23	1.01	0.66	0.63	0.26	0.83
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							4 7								
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	6. 6	0.14	0.19	0.15	0.34	0.00	-0.06	-0.19	-0.05	0.27	0.32	0.14	0.07	0.11
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		7. 7	0.20	0.26	0.29	0.23	0.01	-0.06	-0.27	0.13	0.40	0.37	0.18	0.19	0.16
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-	8.8	0.23	0.35	0.30	0.31	0.05	0.07	-0.04	0.15	0.29	0.35	0.24	0.19	0.21
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		9. 9	3.00	12000	ALTERNATION CONTRACT		3 15 15 5 72 11	SACRETIC:		110-110	TANK REPORT			12 600 000 600	1000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		10.10	0.08	0.18	0.21	-0.21	-0.05	0.13	0.08	0.07	0.03		-31/10/11/11		C
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1						0 -		0 -	0 = 1			11/2	AIX-1	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		AND DESCRIPTION OF THE PARTY OF	1	1200	0.0000000000000000000000000000000000000	5.0000000000000000000000000000000000000	OH DE KNOT	1000			100 0 1000		1.30 4 100		C TO C C C
$ \begin{bmatrix} 6 \cdot 2 \cdot 6 & -0.14 & -0.21 & -0.39 & -0.47 & -0.56 & -0.60 & -0.73 & -0.57 & -0.45 & -0.21 & -0.29 & -0.18 & -0.40 \\ 7 \cdot 2 & -0.14 & -0.22 & -0.18 & -0.28 & -0.25 & -0.35 & -0.38 & -0.31 & -0.34 & -0.27 & -0.34 & -0.20 & -0.27 \\ 8 \cdot 2 & -0.16 & -0.22 & -0.33 & -0.57 & -0.53 & -0.61 & -0.65 & -0.57 & -0.63 & -0.42 & -0.34 & -0.23 & -0.44 \\ 8 \cdot 1 & -0.12 & -0.22 & -0.26 & -0.49 & -0.44 & -0.46 & -0.56 & -0.53 & -0.55 & -0.41 & -0.28 & -0.22 & -0.38 \\ 7 \cdot 1 & -0.10 & -0.23 & -0.11 & -0.20 & -0.16 & -0.20 & -0.29 & -0.27 & -0.26 & -0.28 & -0.18 & -0.21 \\ 9 \cdot 12 \cdot 3 \cdot 9 & -0.20 & -0.29 & -0.55 & -0.99 & -0.69 & -0.76 & -0.86 & -0.73 & -0.76 & -0.43 & -0.41 & -0.20 & -0.57 \\ 7 \cdot 2 \cdot 2(9) & -0.02 & 0.03 & -0.04 & -0.06 & -0.06 & -0.07 & -0.09 & -0.03 & -0.04 & 0.03 & -0.10 & -0.02 & -0.04 \\ \hline \end{tabular} $		the second second	1547.365	STATE OF THE PARTY	1-17/91	A CHARLES	A 40 C	1		3.5000.500	THE PERSON NAMED IN		CALL STREET	1000	1 1 1 1 1 1 1 1 1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					1000000	C. PERSON 18	10000	10 mm		93252 #1557	13-540-099-03		1 2 2 2 2 2	Company of the Compan	Free Comments
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		0. 2. 6	-0.14	-0.21	-0.39	-0.47	-0.56	-0.60	-0.73	-0.57	-0.45	-0.21	-0.29	-0.18	-0.40
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		7. 2	-0.14	-0.22	-0.18	-0.28	-0.25	-0.35	-0.38	-0.31	-0.34	-0.27	-0.34	-0.20	-0.27
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		8. 2	-0.16	-0.22	-0.33	-0.57	-0.53	-0.61	-0.65	-0.57	-0.63	-0.42	-0.34	-0.23	-0.44
$ \begin{vmatrix} 9.12.3.9 \\ 7. & 2.2(9) \end{vmatrix} \begin{vmatrix} -0.20 \\ -0.02 \end{vmatrix} \begin{vmatrix} -0.29 \\ 0.03 \end{vmatrix} \begin{vmatrix} -0.55 \\ -0.04 \end{vmatrix} \begin{vmatrix} -0.99 \\ -0.06 \end{vmatrix} \begin{vmatrix} -0.69 \\ -0.06 \end{vmatrix} \begin{vmatrix} -0.76 \\ -0.07 \end{vmatrix} \begin{vmatrix} -0.86 \\ -0.07 \end{vmatrix} \begin{vmatrix} -0.73 \\ -0.09 \end{vmatrix} \begin{vmatrix} -0.76 \\ -0.03 \end{vmatrix} \begin{vmatrix} -0.41 \\ -0.02 \end{vmatrix} \begin{vmatrix} -0.20 \\ -0.02 \end{vmatrix} \begin{vmatrix} -0.57 \\ -0.02 \end{vmatrix} \end{vmatrix} $		8. 1	THE PARTY OF		200 KGC	THE AREA	100000000000000000000000000000000000000			Commission of the Commission of the	7.453.500				-
7. 2.2(9) -0.02 0.03 -0.04 -0.06 -0.06 -0.07 -0.09 -0.03 -0.04 0.03 -0.10 -0.02 -0.04		7. 1		1000	950.875	1465 535	J. 250. / Sec. 1	1907 - 200		A STATE AND ADDRESS.	The second	1.1 Sept. 4-227	12.00		and the same of th
7. 2.2(9) -0.02 0.03 -0.04 -0.06 -0.06 -0.07 -0.09 -0.03 -0.04 0.03 -0.10 -0.02 -0.04		9.12.3.9	-0.20	-0.20	-0 55	_0.00	_0.60	-0 76	-0.90	-0.72	-0.76	_0.49	-0.47	_0 20	_0.57
													COLUMN	1000	
Dail.ext.   -0.12 -0.22 -0.13  0.09  0.05 -0.09  0.12 -0.04 -0.11 -0.18 -0.25 -0.18 -0.09								120							
	L	Dail. ext.	-0.12	-0.22	-0.13	0.09	0.05	-0.09	0.12	-0.04	-0.11	-0.18	-0.25	-0.18	-0.09

#### LXIII.

### Scotland. - Makerstoun. Lat. 55° 36' N. Long. 2° 31' W. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

												-	
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.67	0.88	1.24	2.30	2.00	2.25	2.10	1.98	1.95	0.88	0.46	0.24	1.41
1	0.76	0.92	1.37	2.52	2.04	2.43	2.44	2.24	2.15	0.88	0.46	0.16	1.53
2	0.78	1.08	1.37	2.70	2.33	2.54	2.57	2.38	2.26	1.06	0.60	0.18	1.65
3	0.76	1.06	1.48	2.79	2.55	2.65	2.79	2.56	2.35	1.57	0.60	0.29	1.79
4	0.67	1.01	1.66	2.96	2.51	2.43	2.70	2.56	2.48	1.20	0.68	0.40	1.77
5	0.78	0.92	1.77	2.88	2.06	1.96	2.21	2.44	2.46	1.40	0.60	0.44	1.66
6	0.60	0.85	1.73	2.25	1.31	1.12	1.35	1.78	2.22	1.31	0.66	0.51	1.31
7	0.51	0.99	1.26	1.43	0.48	0.32	0.46	0.91	1.24	1.26	0.66	0.44	0.83
8	0.53	0.79	0.46	0.36	-0.25	-0.51	-0.39	-0.09	0.00	0.62	0.66	0.40	0.22
9	0.33	0.08	-0.38	-0.79	-0.94	-1.11	-0.96	-1.02	-1.00	-0.16	0.08	0.22	-0.47
10	-0.22	-0.72	-1.12	-1.86	-1.52	-1.68	-1.59	-1.78	-1.92	-0.96	-0.47	-0.20	-1.17
11	-0.84	-1.21	-1.67	-2.55	-2.09	-2.26	-2.14	-2.33	-2.45	-1.63	-0.94	-0.62	-1.73
Noon.	-1.36	-1.61	-2.09	-3.06	-2.34	-2.48	-2.45	-2.73	-2.67	-2.03	-1.34	-0.93	-2.09
1	-1.71	-2.03	-2.27	-3.44	-2.69	-2.75	-2.48	-2.87	-3.03	-2.25	-1.56	-1.13	-2.35
2	-1.67	-2.05	-2.36	-3.57	-2.65	-2.57	-2.52	-2.93	-3.12	-2.20	-1.47	-0.96	-2.34
3	-1.29	-1.68	-2.32	-3.52	-2.65	-2.28	-2.54	-2.73	-2.85	-1.83	-0.96	-0.60	-2.10
4	-0.71	-1.30	-1.80	-3.05	-2.27	-1.95	-2.28	-2.47	-2.29	-1.23	-0.45	-0.16	-1.66
5	-0.13	-0.50	-1.20	-2.30	-1.76	-1.64	-1.81	-1.78	-1.49	-0.49	-0.07	-0.11	-1.11
6	0.18	-0.08	-0.40	-1.39	-0.98	-0.95	-1.34	-1.07	-0.60	-0.09	0.13	0.18	-0.55
7	0.29	0.15	0.08	-0.19	-0.18	-0.40	-0.59	-0.18	0.06	0.17	0.17	0.18	-0.04
8	0.31	0.37	0.46	0.52	0.62	0.36	0.35	0.56	0.46	0.40	0.28	0.18	0.41
9	0.29	0.52	0.73	1.21	1.15	1.00	0.95	1.09	0.95	0.64	0.37	0.24	0.76
10	0.27	0.64	0.95	1.74	1.46	1.56	1.48	1.58	1.33	0.73	0.46	0.31	1.04
11	0.22	0.79	1.06	2.08	1.77	1.94	1.70	1.89	1.51	0.73	0.40	0.36	1.20
Mean.	1.53	0.35	2.06	5.96	6.86	10.25	10.12	10.00	8.51	6.64	4.60	1.16	

#### LXIV.

IRELAND. — DUBLIN. Lat. 53° 23' N. Long. 6° 20' W. Gr. — Dove.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.M.1	0.58	0.53	1.56	2.18	2.53	2.76	2.18	2.22	1.64	1.16	0.53	0.36	1.52
3	0.80	0.71	1.64	2.40	2.89	3.11	2.53	2.40	1.87	1.42	0.67	0.49	1.74
5	0.93	0.98	1.64	2.49	2.31	2.18	2.18	2.53	1.87	1.73	0.76	0.58	1.68
7	0.84	0.93	1.38	0.58	-0.22	-0.89	-0.36	0.40	1.07	1.56	0.80	0.53	0.56
9	0.36	0.18	-0.31	-1.11	-1.24	-1.38	-1.10	-1.16	-0.76	-0.09	0.27	0.36	-0.50
11	-0.98	-0.07	-1.82	-2.40	-2.18	-2.09	-2.04	-2.27	-2.13	-1.91	-0.98	-0.71	-1.71
P.M.1	-1.60	-1.78	-2.67	-2.93	-2.62	-2.40	-2.27	-2.62	-2.67	-2.44	-1.56	-1.16	-2.23
3	-1.33	-1.47	-2.44	-2.84	-2.71	-2.31	-2.27	-2.49	-2.22	-2.04	-1.11	-0.67	-1.99
5	-0.44	0.44	-1.29	-1.82	-1.82	-1.87	-1.64	-1.73	-1.29	-0.84	-0.27	-0.18	-1.14
7	0.09	0.18	0.18	0.04	-0.27	-0.44	-0.27	-0.09	0.27	0.04	0.04	0.09	-0.01
9	0.22	0.31	0.76	1.20	1.29	1.24	1.20	1.16	0.93	0.58	0.36	0.18	0.79
11	0.36	0.40	1.07	1.73	1.96	2.04	1.87	1.64	1.42	0.84	0.44	0.22	1.17
Mean.	4.09	4.75	5.10	6.66	9.51	11.86	12.48	12.31	10.79	7.73	5.99	4.88	

#### LXV.

Russia. — Catharinenburg. Lat. 56° 50' N. Long. 60° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

				THE STATE OF		Degree	s of Re	aumur.					8	Market P
	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
-		0.50	0.07	3.04	1.05	0.00	9.00	0.51	0.40	1.00	0.00	0.45	0.05	1.00
N	Morn. 1	0.59	0.91	1.84	1.97	3.09	3.69	3.51	2.49	1.99	0.68	0.47	0.65	1.82
	2	0.58	0.89	2.09	2.41	3.52	4.15	3.76	2.93	2.27	0.84	0.42	0.67	2.04
	3	0.53	0.87	2.42	2.87	3.80	4.35	3.96	3.42	2.60	1.04	0.36	0.64	2.24
	4	0.48	0.89	2.80	3.21	3.82	4.17	4.01	3.78	2.89	1.23	0.35	0.61	2.35
	5	0.58	0.95	3.11	3.23	3.45	3.54	. 3.78	3.79	2.98	1.36	0.43	0.63	2.32
	6	0.54	1.00	3.15	2.83	2.67	2.49	3.18	3.30	2.74	1.36	0.55	0.72	2.04
	7	0.60	0.94	2.76	1.99	1.57	1.18	2.21	2.29	2.11	1.17	0.64	0.81	1.52
	8	0.56	0.71	1.90	0.84	0.31	0.17	0.98	0.94	1.16	0.80	0.60	0.80	0.79
		0.05	0.97	0.65	0.47	0.00	_1 25	_0.94	-0.48	0.05	0.28	0.37	0.61	-0.07
	9	0.37	0.27	0.65	-0.41	1000000	-1.35		-0.48	7-1	4.1	2000	S 75.75.164	-0.93
	10	-0.01	-0.33	-	71717		741			-1.03	100000000000000000000000000000000000000		E-2-0.044	
1	11		-0.97						1	-1.93		100		
1	Noon	-0.98	-1.47	-3.00	-2.83	-2.98	-3.13	-3.64	-3.03	-2.58	-1.34	-0.59	-0.90	-2.23
	1	-1.30	-1.75	-3.52	-3.04	-3.25	-3.35	-4.33	-3.25	-2.98	-1.62	-1.12	-1.32	-2.57
	2	100000	-1.77		-3.03			A. 5	-3.34	-3.16	-1.69	-1.13	-1.50	-2.69
	3	25 2 3 3 3 3 3 7 7	1 TO 100 TO	-3.39									-1.40	E-2017067781
	4			-2.96								-0.66	-1.10	-2.36
								11.72						
	5	130	-0.79	100000	-2.18			33.1	1	-2.57		Mark Tolland	-0.73	F 10.00
	6	-0.11	CONTROL	-1.77	7 10 10 10	- PANTED				-1.93	1	12/15/20/20 31	-0.39	
	7	0.11	1000	1	-0.92	F 305570			1	-1.12			-0.14	1-1
	8	0.22	0.17	0.36	-0.22	-0.42	-0.48	0.03	-0.53	-0.26	0.06	0.12	0.03	0.14
	9	0.30	0.42	0.32	0.42	0.53	0.56	1.28	0.43	0.52	0.26	0.22	0.15	0.45
	10	0.37	0.63		0.91	1.35	1.51	2.22	1.20	1.13	0.40		0.28	0.95
	11	0.36	1	-	1.29	2.03		2.84		1.52	0.48		0.43	1.30
1	Midn	0.55	0.89	1.62	1.61	2.59	1000	3.23	2.12	1.77	0.56		0.57	1.59
					9									
	6. 6	0.21	0.27	0.69	0.61	0.19	0.03	0.20	0.45	0.40	0.39	0.21	0.17	0.32
	7. 7	0.21	1	0.84	0.53		-0.17	0.20	0.43	100000000000000000000000000000000000000	0.39	0.33	0.33	0.37
	8. 8	0.39		0.77	0.31	10 Th 104	-0.33	0.51	A STATE OF		0.43	1000	0.41	0.32
	9. 9	0.33		0.49	0.01	1	-0.39	0.47	100000000000000000000000000000000000000	100	0.27	100000	0.38	0.19
	10.10	0.18	1000		1000	10000	-0.36				0.04			O PERSONAL PROPERTY OF THE PARTY OF THE PART
	10.10	0.10	0.13	0.00	-0.50	-0.23	-0.50	0.51	0.25	0.00	0.04	0.13	0.20	0.00
1	7. 2. 9	-0.16	-0.14	-0.18	-0.21	-0.44	-0.59	-0.43	-0.21	-0.18	-0.09	-0.09	-0.18	-0.20
	6. 2. 8	-0.20	-0.20	-0.28	-0.14	-0.39	-0.50	-0.52	-0.19	-0.23	-0.09	-0.15	-0.25	-0.26
	6. 2.10	-0.15	-0.05	0.14	0.24	0.20	0.17	0.21	0.39	0.24	0.02	0.08	-0.17	0.10
	6. 2. 6	-0.31	-0.40	-0.75	-0.60	-0.01	-1.15	-1.46	-0.81	-0.78	-0.30	-0.24	-0.39	-0.68
	7 0	0.00	0.40	0.40	0 -0	0.00	1 10	1 00	0.50	0.50	0.00	0.05	0.95	0.50
11	7. 2 8. 2			-0.43										
11		(1		-0.86										1
11	8. 1 7. 1	11	1	-0.81						-0.91			-0.26	
		0.35	0.41	-0.38	0.53	-0.84	-1.09	-1.00	-0.48	0.44	0.23	-0.24	-0.20	0.03
1 9	9.12.3.9	-0.38	-0.58	-1.36	-1.43	-1.70	-1.87	-1.90	-1.61	-1.30	-0.60	-0.31	-0.39	-1.12
	7. 2.2(9)	III TO THE REAL PROPERTY.	10000	-0.06	1	1	A Committee of the Comm		The second second		10.00	1	-0.10	1
1	Doil out	-0.20	_0 20		0.70	0.10	0.40	0.45	0.00	0.1**	0.15	_0.95		-0.17
L	Dail.ext.	11-0.39	-0.39	-0.24	0.10	0.18	0.40	-0.45	0.22	0.17	-0.17	-0.25	-0.35	-0.17

#### LXVI.

Russia. — Catharinenburg. Lat. 56° 50' N. Long. 60° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.42	1.07	1.70	2.12	2.64	3.06	2.93	2.16	1.96	0.89	0.47	0.47	1.66
1	0.52	1.19	2.00	2.40	3.11	3.51	3.41	2.49	2.31	1.08	0.51	0.50	1.92
2	0.52	1.25	2.23	2.82	3.49	3.90	3.86	2.76	2.58	0.99	0.54	0.52	2.12
3	0.55	1.41	2.53	3.05	3.73	4.15	4.11	3.03	2.83	1.47	0.58	0.54	2.33
4	0.63	1.52	2.75	3.26	3.74	3.92	4.28	3.22	3.06	1.61	0.68	0.58	2.44
5	0.68	1.67	2.85	3.24	3.27	3.35	3.66	3.14	3.22	1.67	0.71	0.61	2.34
6	0.73	1.76	3.06	2.24	2.27	1.99	2.47	2.45	3.04	1.69	0.82	0.64	1.93
7	0.81	1.76	2.59	1.61	0.89	0.61	1.02	1.37	2.27	1.53	0.85	0.65	1.33
8	0.88	1.51	1.46	0.34	-0.24	-0.53	-0.28	0.18	0.85	0.91	0.77	0.58	0.54
9	0.67	0.73	-0.06	-0.81	-1.09	-1.46	-1.45	-0.97	-0.57	-0.03	0.33	0.39	-0.36
10	0.13	-0.45	-1.45	-1.99	-1.94	-2.23	-2.35	-1.72	-1.68	-0.78	-0.22	-0.08	-1.23
11	-0.57	-1.44	-2.39	-2.62	-2.72	-2.93	-3.10	-2.54	-2.50	-1:46	-0.72	-0.71	-1.98
Noon.	-1.04	-2.13	-2.95	-3.09	-3.19	-3.38	-3.58	-2.99	-3.09	-1.73	-1.03	-1.19	-2.45
1	-1.39	-2.58	-3.27	-3.22	-3.28	-3.48	-3.57	-3.04	-3.32	-1.99	-1.25	-1.45	-2.68
2	-1.50	-2.74	-3.38	-3.26	-3.41	-3.59	-3.55	-3.02	-3.36	-2.02	-1.23	-1.39	-2.70
3	-1.28	-2.37	-3.18	-2.86	-3.14	-3.37	-3.40	-3.03	-3.48	-2.23	-1.11	-1.00	-2.5
4	-0.85	-1.97	-2.82	-2.65	-2.99	-3.05	-3.15	-2.83	-3.18	-1.61	-0.79	-0.61	-2.21
5	-0.50	-1.28	-2.20	-2.14	-2.60	-2.49	-2.67	-2.37	-2.48	-0.95	-0.47	-0.33	-1.71
6	-0.22	-0.74	-1.37	-1.46	-1.98	-1.98	-2.14	-1.66	-1.56	-0.56	-0.26	-0.11	-1.17
7	0.00	-0.25	-0.67	-0.59	-0.95	-1.17	-1.29	-0.79	-0.65	-0.22	-0.07	0.02	-0.55
8	0.10	0.08	-0.12	0.13	-0.04	-0.12	-0.16	0.11	0.07	0.06	0.06	0.11	0.02
9	0.17	0.40	0.44	0.65	0.85	0.96	0.83	0.84	0.67	0.36	0.16	0.26	0.55
10	0.24	0.65	0.94	1.13	1.53	1.88	1.67	1.39	1.25	0.53	0.27	0.39	0.99
11	0.34	0.86	1.34	1.58	2.13	2.51	2.36	1.81	1.65	0.74	0.40	0.56	1.36
Mean.	-10.76	-9.50	-5.83	0.47	6.31	12.08	14.53	10.61	6.32	1.41	-6.11	-11.68	

#### LXVII.

Russia. — St. Petersburg. Lat. 59° 56′ N. Long. 30° 18′ E. Gr. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.14	0.38	0.73	1.44	2.08	1.99	1.77	1.68	1.17	0.52	0.15	0.17	1.02
1	0.21	0.44	0.99	1.68	2.43	2.29	2.05	2.02	1.38	0.60	0.17	0.21	1.21
2	0.25	0.46	1.22	1.91	2.70	2.56	2.24	2.24	1.58	0.65	0.15	0.27	1.35
3	0.30	0.52	1.38	2.11	2.91	2.73	2.43	2.48	1.75	0.73	0.25	0.34	1.49
4	0.38	0.63	1.56	2.24	2.86	2.44	2.32	2.59	1.87	0.78	0.30	0.36	1.53
5	0.43	0.72	1.71	2.28	2.38	1.97	1.92	2.40	1.96	0.84	0.34	0.34	1.44
6	0.45	0.76	1.75	1.95	1.72	1.33	1.33	1.96	1.90	0.90	0.37	0.30	1.23
7	0.41	0.78	1.57	1.32	0.93	0.63	0.64	1.19	1.47	0.82	0.37	0.29	0.87
8	0.42	0.60	1.07	0.65	0.14	-0.04	0.05	0.42	0.81	0.57	0.32	0.25	0.44
9	0.35	0.40	0.40	-0.05	-0.59	-0.69	-0.56	-0.40	0.00	0.20	0.17	0.17	-0.05
10	0.13	-0.05	-0.19	-0.78	-1.30	-1.21	-1.12	-1.07	-0.71	-0.22	0.00	0.04	-0.54
11	-0.20	-0.48	-0.86	-1.42	-1.92	-1.71	-1.58	-1.64	-1.27	-0.61	-0.20	-0.14	-1.00

#### LXVII.

#### RUSSIA. - St. Petersburg, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-0.38	-0.90	-1.31	-1.93	-2.30	-1.99	-1.89	-2.10	-1.72	-0.94	-0.37	-0.30	-1.34
1	-0.63	-0.97	-1.62	-2.10	-2.41	-2.17	-2.03	-2.47	-2.26	-1.75	-0.64	-0.48	-1.6
2	-0.66	-1.04	-1.88	-2.36	-2.65	-2.32	-2.15	-2.60	-2.34	-1.29	-0.63	-0.58	-1.71
3	-0.55	-0.99	-1.94	-2.49	-2.90	-2.45	-2.29	-2.64	-2.31	-1.06	-0.46	-0.40	-1.71
4	-0.33	-0.83	-1.92	-2.65	-2.92	-2.60	-2.41	-2.80	-2.27	-0.86	-0.20	-0.31	-1.68
5	-0.25	-0.45	-1.53	-2.31	-2.48	-2.23	-2.06	-2.45	-1.76	-0.50	-0.16	-0.22	-1.37
6	-0.19	-0.26	-1.02	-1.43	-1.65	-1.41	-1.30	-1.41	-0.95	-0.25	-0.11	-0.14	-0.8
7	-0.18	-0.16	-0.55	-0.61	-0.74	-0.71	-0.63	-0.62	-0.35	-0.09	-0.05	-0.10	-0.4
8	-0.14	-0.03	-0.25	-0.03	0.06	-0.03	0.02	0.09	0.07	0.07	0.01	0.08	-0.0
9	-0.11	0.08	0.03	0.47	0.79	0.67	0.64	0.65	0.40	0.18	0.08	0.03	0.3
10	-0.03	0.17	0.24	0.84	1.22	1.25	1.18	1.05	0.66	0.33	0.08	0.02	0.58
11	0.06	0.30	0.50	1.17	1.76	1.65	1.45	1.40	0.91	0.45	0.11	0.11	0.8
Mean.	-7.41	-6.73	-3.56	1.10	7.01	11.33	13.39	13.58	8.43	3.61	-0.80	-3.75	

#### LXVIII.

Russia. — Helsingfors. Lat. 60° 10' N. Long. 24° 57' E. Gr. — Dove.

			11177		D	egrees of	Reaum	ur.			270		
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.06	0.47	1.28	1.61	1.61	2.01	1.65	1.36	0.83	0.37	0.18	0.20	0.97
1	0.13	0.49	1.48	1.87	1.94	2.44	1.90	1.68	1,03	0.45	0.15	0.21	1.15
2	0.16	0.52	1.64	2.07	2.21	2.84	2.17	1.98	1.21	0.55	0,18	0.18	1.31
3	0.23	0.67	1.84	2.21	2.58	3.04	2.45	2.23	1.35	0.65	0.23	0.15	1.4
4	0.35	0.64	1.91	2.37	2.68	2.77	2.42	2.49	1.48	0.62	0.28	0.23	1.55
5	0.38	0.77	1.98	2.34	2.28	2.21	2.05	2.41	1.63	0.67	0.33	0.10	1.43
6	0.38	0.92	2.01	1.74	1.31	1.31	1.33	1.81	1.63	0.75	0.33	0.03	1.13
7	0.41	0.99	1.78	1.14	0.58	0.51	0.55	1.11	1.28	0.73	0.36	0.01	0.79
8	0.43	0.99	1.04	0.17	-0.19	-0.36	-0.10	0.26	0.58	0.57	0.35	0.00	0.3
9	0.38	0.55	0.04	-0.73	-0.86	-0.83	-0.73	-0.56	-0.09	0.33	0.25	0.06	-0.18
10	0.08	-0.20	-0.89	-1.49	-1.39	-1.29	-1.23	-1.12	-0.65	-0.15	0.13	-0.07	-0.69
11	-0.19	-0.93	-1.19	-1.93	-1.76	-1.83	-1.65	-1.59	-1.05	-0.47	-0.19	-0.32	-1.09
Noon.	-0.72	-1.25	-2.36	-2.26	-1.82	-1.76	-1.80	-2.02	-1.67	-0.90	-0.59	-0.42	-1.4
1	-0.79	-1.50	-2.62	-2.46	-2.12	-2.06	-2.13	-2.26	-1.82	-1.08	-0.70	-0.45	-1.6
2	-0.74	-1.60	-2.62	-2.56	-2.19	-2.36	-2.28	-2.31	-1.85	-1.10	-0.64	-0.42	-1.7
3	-0.49	-1.33	-2.46	-2.37	-2.16	-2.49	-2.13	-2.17	-1.75	-0.95	-0.50	-0.22	-1.58
4	11	1	1	-1.89	-1.82	-2.16	-1.75	-1.84	-1.52	-0.77	-0.29	-0.02	-1.2
5	-0.12	-0.43	-1.56	-1.59	-1.49	-1.89	-1.48	-1.64	-1.20	-0.43	-0.17	0.03	-1.00
6	-0.04	-0.21	-0.79	-1.09	-1.09	-1.53	-1.15	-1.19	-0.72	-0.25	-0.09	-0.02	-0.68
7	0.03	0.07	-0.29	-0.49	-0.86	-0.96	-0.68	-0.64	-0.27	-0.13	-0.04	0.01	-0.38
8	0.08	0.20	0.01	0.14	-0.16	-0.36	-0.10	-0.14	0.05	-0.03	0.00	0.11	-0.02
9	0.10		0.44	0.64	0.44	0.37	0.55	0.28	0.23	0.05	0.06	0.13	0.29
10	0.08	1	0.74	1.04	0.94	1.04	1.02	0.71	0.43	0.13	0.10	0.18	0.56
11	0.01	0.42	1.01	1.37	1.34	1.54	1.37	1.06	0.63	0.27	0.18	0.15	0.78
Mean.	-5.02	-7.43	-3.89	-0.06	5.11	10.84	12.75	14.11	9.23	4.55	1.13	-3.42	

#### LXIX.

Russia. - Petersburg. Lat. 59° 56' N. Long. 30° 18' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degre	es of R	eaumur.		10 10			E.L.	
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.20	0.38	0.92	1.52	2.59	2.40	1.98	2.08	1.39	0.72	0.14	0.17	1.21
2	0.23	0.37	1.10	1.75	2.84	2.69	2.26	2.43	1.67	0.77	0.13	0.27	1.38
3	0.22	0.39	1.30	2.01	3.03	2.90	2.49	2.79		0.82	0.14	0.33	1000
4	0.21		1			1000	2.57	3.01	2.20			0.35	1
	0.21	0.20	1.40	2.10	0.00	2.01	2.01	0.01	2.20	0.00	0.10	0.00	1.02
5	0.26	0.50	1.59	2.17	2.79	2.60	2.37	2.92	2.25	0.95	0.20	0.35	1.58
6	0.37	-				and the same	1.88					0.34	
7	0.51	1		1 3 KM	1.27	1.13	1.15	1.70	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	O TOTAL OF	Ulilla	0.33	
8	0.59						0.34			0.72		0.31	0.56
0	0.00	0.40	0.55	0.00	0.41	0.24	0.04	0.13	1.01	0.12	0.10	0.51	0.50
9	0.53	0.23	0.47	-0.02	-0.47	-0.53	-0.40	-0.10	0.31	0.36	0.03	0.27	0.06
10	0.33	1			1000000	100000000000000000000000000000000000000	-	-0.86			1000	0.18	
II .						The Park Inches	12120	P. J. G. S.		THE CO.	The second		
11							7/01				-0.35		-0.86
Noon	-0.34	-0.73	-1.28	-1.02	-2.09	-1.83	-1.67	-2.01	-1.75	-0.99	-0.49	-0.15	-1.25
1	0.50	-0.92	-1.68	-2.01	-9 50	_9 90	7 00	-2.53	-2.29	-1.27	0 = 4	-0.32	7 57
				10000		1			1				
2		-0.95											-1.81
3	-0.61					Carlon half	and the last	-3.35				-0.48	
4	-0.45	-0.67	-1.75	-2.50	-3.36	-3.12	-2.68	-3.39	-2.65	-1.12	-0.18	-0.44	-1.86
_	0.00	0.44	1 44	0.70	0.77	0.00	0.40	9.00	0.70	0.00	0.00	0.00	7.07
5		-0.44						-3.02				-0.36	The second second
6	-0.15							-2.26				-0.26	
7		-0.02			- 24		The Property of the Land		-0.72			-0.19	-0.65
8	-0.13	0.13	-0.20	-0.10	-0.34	-0.31	-0.29	-0.20	-0.01	-0.12	0.19	-0.14	-0.13
	0.14	0.04	074	0.54	0.00	0.01	0.40	0.00	0 =0	0	0.70	0.70	0.00
9	-0.14	0.24	0.14	0.54	0.69	0.61	0.49	0.66	0.53	0.11		-0.12	0.33
10	-0.09	0.32	0.40	0.96	1.47	1.30	1.07	1.24	0.87	0.33	7.71	-0.09	0.66
11	0.02	0.37	0.59	1.20	2.00	1.77	1.45	1.58	1.05	0.50	0.17	-0.02	0.89
Midn	0.12	0.38	0.75	1.35	2.33	2.11	1.73	1.81	1.20	0.63	0.16	0.07	1.05
		3 3			F (4) 2-3		091		13/5				
	0.74	0.70	0.00	0 -				0.40			19		
6. 6	0.11	0.18	0.26		-0.12			0.10	0.28	0.18	0.17	0.04	0,10
7. 7	0.20	0.27	0.38	0.25	-0.05		-0,00	0.23	0.45	0.28	0.20	0.07	0.18
8.8	0.23	0.29	0.40	0.29	0.04	-0.04	0.03	0.29	0.50	0.30	0.18	0.09	0.22
9. 9	0.20	0.24	0.31	0.26	0.11	0.04	0.04	0.28	0.42	0.24	0.11	0.08	0.19
10.10	0.12	0.12	0.13	0.15	0.16	0.11	0.05	0.19	0.22	0.12	0.01	0.05	0.12
	1120-11		ELFES				660			323		HE DE	
7. 2. 9		-0.05	-0.13		-0.32		-0.22	-0.22		-0.11	-0.02	-0.08	-0.16
6. 2. 8	-0.15	-0.08	-0.18	-0.18	-0.35	-0.32	-0.24	-0.25	-0.21	-0.17	-0.02	-0.08	-0.19
6. 2.10	-0.13	-0.02	0.02	0.17	0.25	0.22	0.21	0.23	0.09	-0.02	-0.03	-0.06	0.08
6. 2. 6	-0.15	-0.20	-0.46	-0.69	-1.05	-0.97	-0.79	-0.94	-0.70	-0.33	-0.05	-0.12	-0.54
													N. S.
7. 2	-0.09	-0.20	-0.27	-0.49	-0.82	-0.75	-0.58	-0.66	-0.53	-0.22	-0.13	-0.06	-0.40
8. 2	-0.05	-0.25	-0.45	-0.83	-1.25	-1.19	-0.99	-1.11	-0.83	-0.32	-0.17	-0.07	-0.63
8. 1		-0.23										-0.01	-0.51
7. 1		-0.18											-0.28
	HIE.		1.227			7	2130					W. Ste	
9.12.3.9	-0.14	-0.28	-0.65	-0.91	-1.28	-1.18	-1.04	-1.20	-0.93	-0.46	-0.16	-0.12	-0.70
7. 2.2(9)	-0.11	0.02	-0.06		-0.07					-0.06		-0.09	1
DESCRIPTION OF	250	123	181				Mar Y			100 100	22 64		
Dail. ext.	-0.05	-0.19	-0.17	-0.17	-0.16	-0.11	-0.06	-0.19	-0.28	-0.19	-0.16	-0.07	-0.15
	1				-				-				

#### LXX.

Russia. — Helsingfors. Lat. 60° 10' N. Long. 24° 57' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

							aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	0.45	0.05	1.40	0.10	2.49	3.37	3.16	9.50	1 00	1.00	0.04	0.04	1 //2
Morn. 1	0.47	0.85 1.25	1.40	2.10 3.18	2.49	3.78	3.48	2.58	1.60 2.09	1.06 1.45	0.64	0.34	1.67 2.11
3	0.99	1.55	2.28	2.79	2.89	3.74	3.45	3.11	2.48	1.70	1.22	0.00	2.26
4	1.13	1.71	2.52	2.77	2.62	3.22	3.02	2.92	2.61	1.74	1.26	0.97	2.21
5	1.06	1.66	2.49	2.41	2.06	2.32	2.25	2.39	2.40	1.51	1.09	0.84	1.87
6	0.86	1.43	2.16	1.76	1.30	1.24	1.23	1.59	1.84	1.10	0.76	0.59	1.32
7	0.58	1.07	1.57	0.92	0.49	0.20	0.17	0.64	1.06	0.59	0.38	0.31	0.67
8	0.28	0.60	0.79	0.05	-0.26	-0.65	-0.78	-0.28	0.21	0.08	0.02	0.07	0.01
9	0.01	0.10	-0.05	-0.74	-0.87	-1.26	-1.51	-1.07	-0.58	-0.38	-0.27	-0.10	-0.56
10	-0.25	-0.42	-0.87	-1.35	-1.34	-1.65	-2.02	-1.68	-1.23	-0.77	-0.48	-0.22	-1.02
		-0.91			-1.70						-0.64		
Noon	-0.70	-1.29	-2.06	-2.10	-1.98	-2.16	-2.54	-2.43	-2.04	-1.30	-0.76	-0.43	-1.65
1	-0.86	-1.54	-2.36	-2.30	-2.19	-2.36	-2.65	-2.61	-2.23	-1.42	-0.85	-0.54	-1.83
2	-0.92	-1.60	-2.45	-2.37	-2.32	-2.51	-2.66	-2.66	-2.30	-1.43	-0.88	-0.61	-1.89
	AND PROPERTY.	-1.47	- DO	A CONTRACTOR	-2.31								1
4	-0.73	-1.20	-2.01	-2.10	-2.11	-2.42	-2.27	-2.26	-1.92	-1.05	-0.68	-0.49	-1.60
5  -	-0.52	-0.87	-1.56	-1.73	-1.77	-2.13	-1.85	-1.80	-1.48	-0.74	-0.48	-0.33	-1.27
6	-0.32	-0.57	-1.07	-1.25	-1.30	-1.71	-1.30	-1.24	-0.95	-0.44	-0.28	-0.18	-0.88
	-0.19	-0.38	-0.60	-0.72	-0.78	-1.20	-0.68	-0.62	-0.42	-0.22	-0.16	-0.11	-0.51
8	-0.15	-0.25	-0.20	-0.21	-0.24	-0.61	-0.04	-0.03	-0.00	-0.10	-0.12	-0.12	-0.17
9 .	-0.16	-0.18	0.10	0.26	0.29	0.07	0.61	0.52	0.31	-0.03	-0.12	-0.20	0.12
		-0.08	0.36	0.69	0.82	0.87	1.27	1.03	0.54	0.08	19.00		0.42
11	-0.06	0.12	0.63	1.13	1.40	1.75	1.95	1.54	0.79	0.29	0.02	-0.19	0.78
Midn	0.16	0.44	0.96	1.60	1.97	2.63	2.61	2.08	1.14	0.63	0.28	0.02	1.21
6. 6	0.27	0.43	0.55	0.26	-0.00	-0.24	-0.04	0.18	0.45	0.33	0.24	0.21	0.22
7. 7	0.20	0.35	0.49	0.10	-0.15	-0.50	-0.26	0.01	0.32	0.19	0.11	0.10	0.08
8. 8	0.07	0.18	.0.30	-0.08	-0.25	-0.63	-0.41	-0.16	0.11			-0.03	
11	-0.08	-0.04	0.03	-0.24	Later Control of	1000	-0.45	-0.28	-0.14	-0.21		-0.15	-0.22
10.10	-0.21	-0.25	-0.26	-0.33	-0.26	-0.39	-0.38	-0.33	-0.35	-0.35	-0.29	-0.24	-0.30
7. 2. 9	-0.17	-0.24	-0.26	-0.40	-0.51	-0.75	-0.63	-0.50	-0.31	-0.29	-0.21	-0.17	-0.37
6. 2. 8	-0.07	-0.14	-0.16	-0.27	-0.42	-0.63	-0.49	-0.37	-0.15	-0.14	-0.08	-0.05	-0.25
11	-0.07	-0.08	0.02		-0.07		3.7			-0.08	10000		
6. 2. 6	-0.13	-0.25	-0.45	-0.62	-0.77	-0.99	-0.91	-0.77	-0.47	-0.26	-0.13	-0.07	-0.49
7. 2	-0.17	-0.27	-0.44	-0.73	-0.92	-1.16	-1.25	-1.01	-0.62	-0.42	-0.25	-0.15	-0.62
8. 2	-0.32	-0.50			-1.29				-1.05	-0.68	-0.43	-0.27	-0.94
11	-0.29	-0.47	-0.79							-0.67			-0.91
7. 1	-0.14	-0.24	-0.40	-0.69	-0.85	-1.08	-1.24	-0.99	-0.59	-0.42	-0.24	-0.12	-0.58
9.12.3.9	-0.42	-0.71	-1.08	-1.22	-1.22	-1.48	-1.50	-1.38	-1.13	-0.75	-0.49	-0.33	-0.98
1 1 1	HEIGHTOUY				-0.31								
Dail.ext.	0.11	0.06	0.04	0.41	0.29	0.62	0.41	0.23	0.16	0.16	0.19	0.18	0.19

#### LXXI.

Norway. — Christiania. Lat. 59° 55' N. Long. 10° 43' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Morn. 1	Grand Co.				10000	Degree	es of Re	aumur.	1000			THE STATE	2400	
1.54   3	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
1.54   3			T	1		To the		7.5		122		When !		
3	Morn. 1	0.16	0.89	1.07	1.56	2.55	2.58	2.21	2.04	1.64	0.74	0.52	0.22	1.35
1.84	2	0.21	0.94	1.30	1.88	2.85	3.15	2.53	2.23	1.88	0.82	0.50	0.21	1.54
5   0.38   1.60   1.82   2.23   2.55   2.39   2.09   2.44   2.14   1.16   0.51   0.22   1.63   6   0.47   1.54   1.69   1.51   1.63   1.31   1.37   1.95   2.10   1.16   0.60   0.11   1.31   7   0.51   1.67   1.71   1.28   0.71   0.43   0.55   1.00   1.50   1.13   0.46   0.19   0.93   8   0.54   1.42   1.29   0.56   0.07   -0.32   -0.22   0.10   0.62   0.75   0.38   0.15   0.44   9   0.48   1.11   0.36   -0.06   -0.52   0.86   -0.78   -0.59   0.01   0.15   0.17   0.16   -0.03   10   0.24   0.27   -0.35   -0.67   -1.19   -1.57   -1.26   -1.23   -0.78   -0.48   -0.23   0.11   -0.59   11   -0.17   -0.69   -0.96   -1.88   -1.66   -2.05   -1.74   -1.67   -1.44   -1.00   -0.76   -0.20   -1.14   Noon   -0.67   -1.32   -1.48   -1.80   -2.17   -2.29   -2.02   -2.11   -2.02   -1.30   -1.06   -0.40   -1.55   1   -0.87   -1.90   -1.74   -2.22   -2.46   -2.50   -2.21   -2.35   -2.41   -1.59   -1.15   -0.42   -1.82   2   -1.04   -2.22   -1.95   -2.32   -2.46   -2.50   -2.21   -2.35   -2.41   -1.59   -1.15   -0.35   -1.90   3   -0.91   -2.29   -2.16   -2.26   -2.54   -2.47   -2.21   -2.50   -2.50   -1.58   -0.58   -0.53   -0.23   -0.88   4   -0.62   -2.00   -1.99   -2.11   -2.53   -2.29   -2.00   -2.32   -2.35   -1.33   -0.55   -0.12   -1.68   5   -0.35   -1.42   -1.58   -1.80   -2.20   -2.14   -1.87   -1.97   -1.80   -0.90   -0.23   -0.06   -1.36   6   -0.12   -1.10   -1.10   -1.27   -1.82   -1.70   -1.48   -1.48   -1.21   -0.52   -0.02   -0.03   -0.99   7   -0.01   -0.60   -0.65   -0.70   -1.35   -0.89   -0.89   -0.78   -0.57   -0.24   -0.11   -0.10   -0.58   8   0.12   -0.32   -0.20   -0.14   -0.44   -0.31   -0.30   -0.10   0.02   0.18   0.23   -0.13   -0.12   9   0.16   0.09   0.09   0.36   0.24   0.44   0.45   0.55   0.36   0.36   0.27   -0.05   0.28   10   0.27   0.34   0.36   0.70   0.93   1.20   1.06   1.08   0.81   0.58   0.33   -0.04   0.63   11   0.31   0.52   0.53   0.99   1.46   1.76   1.63   1.41   1.06   0.75   0.43   0.10   0.10   10   0.26   0.31   0.01   0.05   0.13   0.018   -0.10   0.06   0.02   0.05	3	0.27	1.17	1.51	2.03	3.23	3.28	2.64	2.41	2.03	0.94	0.49	0.28	1.69
6	4	0.32	1.49	1.67	2.12	3.21	3.05	2.62	2.60	2.07	1.06	0.55	0.30	1.84
6			S Laboratoria				1		1	1	Town.	100	St.	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			-				100000	0.00			C.C.		THE RESERVE	
8   0.54   1.42   1.29   0.56   0.07   -0.32   -0.22   0.10   0.62   0.75   0.38   0.15   0.44   9   0.48   1.11   0.36   -0.06   -0.52   -0.86   -0.78   -0.59   0.01   0.15   0.17   0.16   -0.03   10   0.24   0.27   -0.35   -0.67   -1.19   -1.57   -1.26   -1.23   -0.78   -0.48   -0.23   0.11   -0.59   11   -0.17   -0.69   -0.96   -1.38   -1.66   -2.05   -1.74   -1.67   -1.44   -1.00   -0.76   -0.20   -1.14   Noon   -0.67   -1.32   -1.48   -1.80   -2.17   -2.29   -2.02   -2.11   -2.02   -1.30   -1.06   -0.40   -1.55   1   -0.87   -1.90   -1.74   -2.22   -2.46   -2.50   -2.21   -2.35   -2.41   -1.59   -1.15   -0.42   -1.85   2   -1.04   -2.22   -1.95   -2.32   -2.46   -2.40   -2.20   -2.55   -2.54   -1.67   -1.15   -0.35   -1.90   3   -0.91   -2.29   -2.16   -2.26   -2.54   -2.47   -2.21   -2.50   -2.54   -1.67   -1.15   -0.35   -1.90   3   -0.91   -2.29   -2.16   -2.26   -2.54   -2.47   -2.21   -2.55   -2.55   -1.33   -0.55   -0.12   -1.68   4   -0.62   -2.00   -1.99   -2.11   -2.53   -2.29   -2.00   -2.32   -2.35   -1.33   -0.55   -0.12   -1.68   5   -0.35   -1.42   -1.58   -1.80   -2.20   -2.14   -1.87   -1.97   -1.80   -0.90   -0.23   -0.06   -1.36   6   -0.12   -1.10   -1.10   -1.27   -1.82   -1.70   -1.48   -1.48   -1.21   -0.52   -0.02   -0.03   -0.99   7   -0.01   -0.60   -0.65   -0.70   -1.35   -0.98   -0.89   -0.78   -0.57   -0.24   -0.11   -0.10   -0.58   8   0.12   -0.32   -0.20   -0.14   -0.44   -0.31   -0.30   -0.10   0.02   0.18   0.23   -0.13   -0.11   9   0.16   0.09   0.36   0.24   0.44   0.45   0.55   0.36   0.36   0.27   -0.05   0.28   10   0.27   0.34   0.36   0.70   0.93   1.20   1.06   1.08   0.81   0.58   0.35   -0.04   0.63   11   0.31   0.52   0.53   0.99   1.46   1.76   1.63   1.41   1.06   0.75   0.43   0.10   0.91   11   0.10   0.26   0.31   0.01   0.05   -0.18   -0.18   -0.10   -0.16   0.05   0.05   0.05   0.05   0.05   0.18   12   8   8   0.33   0.55   0.55   0.55   0.21   -0.19   -0.32   -0.26   0.00   0.32   0.47   0.31   0.01   0.16   0.25   0.35   0.05   0.05   0.05   0.05	CHECK AND DOG	1			100			19223736	The state of the state of			1000	BU ELV	
$\begin{array}{c} 9 \\ 10 \\ 0.24 \\ 0.27 \\ -0.35 \\ -0.66 \\ -0.52 \\ -0.86 \\ -0.7 \\ -1.19 \\ -1.57 \\ -1.26 \\ -1.23 \\ -1.06 \\ -0.78 \\ -0.78 \\ -0.78 \\ -0.48 \\ -0.48 \\ -0.23 \\ -0.11 \\ -0.17 \\ -0.69 \\ -0.96 \\ -1.38 \\ -1.80 \\ -2.17 \\ -2.29 \\ -2.02 \\ -2.11 \\ -2.02 \\ -2.11 \\ -2.02 \\ -1.30 \\ -$		1000			100	0.600			The same of	1000	I SECTION	STORES .	100	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	0.54	1.42	1.29	0.56	0.07	-0.32	-0.22	0.10	0.62	0.75	0.38	0.15	0.44
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	0.48	1.11	0.36	-0.06	-0.52	-0.86	-0.78	-0.59	0.01	0.15	0.17	0.16	-0.03
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			Cens			7	110000			Marie Contract	10.0	The second second		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		Maria Day			TO COL	1 9 5 1 3 1 4 1	100000000000000000000000000000000000000	DIFFEDOM NO.	6.0		10000	100000000000000000000000000000000000000		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	THE RESERVE OF THE PARTY OF THE	DOLLAR	0	1	1000	A 200 TO 100 TO	- C - C - C - C - C - C - C - C - C - C	The second second		100000	and the second of the second	P 400 100 1	CONTRACT TO STATE OF	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	-0.87	-1.90	-1.74	-2.22	-2.46	-2.50	-2.21	-2.35	-2.41	-1.59	-1.15	-0.42	-1.82
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			- 500	100	1.4.4.2.0		and the same		ALC: NO	1900 100	10000	57 Lb. 30	77.5	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	-0.91	-2.29	-2.16	-2.26	-2.54	-2.47	-2.21	-2.50	-2.50	-1.58	-0.88	-0.23	-1.88
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	-0.62	-2.00	-1.99	-2.11	-2.53	-2.29	-2.00	-2.32	-2.35	-1.33	-0.55	-0.12	-1.68
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	The state of		1		and the same			Lan e					The Labor	TIA
7											100000000000000000000000000000000000000	- C - C - C - C - C - C - C - C - C - C	TO 10000	
8       0.12       -0.32       -0.20       -0.14       -0.44       -0.31       -0.30       -0.10       0.02       0.18       0.23       -0.13       -0.12         9       0.16       0.09       0.09       0.36       0.24       0.44       0.45       0.55       0.36       0.36       0.27       -0.05       0.28         10       0.27       0.34       0.36       0.70       0.93       1.20       1.06       1.08       0.81       0.58       0.33       -0.04       0.63         11       0.31       0.52       0.53       0.99       1.46       1.76       1.63       1.41       1.06       0.75       0.43       0.10       0.91         Midn.       .       0.33       0.86       0.77       1.20       1.90       2.31       2.00       1.75       1.38       0.95       0.48       0.09       1.17         6. 6       0.18       0.22       0.30       0.27       -0.10       -0.20       -0.06       0.25       0.45       0.32       0.29       0.04       0.16         7. 7       0.25       0.54       0.53       0.29       -0.32       -0.16       0.11       0.47       0.45       <	100000000000000000000000000000000000000		The second	and the same of th	A CONTRACTOR OF THE PARTY OF TH	THE PERSON NAMED IN	- PEAUTY.	DAMES OF THE	Andrew Str.		4.00	Carlot and Carlot	THE RESERVE	
9		100000	0.00							and the		100	154 K.S.	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	0.12	-0.32	-0.20	-0.14	-0.44	-0.31	-0.30	-0.10	0.02	0.18	0.23	-0.13	-0.12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0	0.16	0.00	0.00	0.36	0.94	0.44	0.45	0.55	0.36	0.36	0.27	_0.05	0.28
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					THE REAL PROPERTY.	1200000			100				100000	
Midn         0.33         0.86         0.77         1.20         1.90         2.31         2.00         1.75         1.38         0.95         0.48         0.09         1.17           6. 6         0.18         0.22         0.30         0.27         -0.10         -0.20         -0.06         0.25         0.45         0.32         0.29         0.04         0.16           7. 7         0.25         0.54         0.53         0.29         -0.32         -0.28         -0.16         0.11         0.47         0.45         0.29         0.05         0.18           8. 8         0.33         0.55         0.55         0.21         -0.19         -0.32         -0.26         0.00         0.32         0.47         0.31         0.01         0.16           9. 9         0.32         0.60         0.23         0.15         -0.14         -0.21         -0.17         -0.02         0.19         0.26         0.22         0.06         0.12           10.10         0.26         0.31         0.01         0.05         -0.13         -0.18         -0.10         -0.08         0.02         0.05         0.05         0.02           6. 2. 8         -0.15         -0.33		- 11 - 1	1	70.00	2000	The second second					1 2 1 1 1 1 1 1 1	100 mm		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		A CONTRACTOR OF THE PARTY OF TH	100	1 -1 -1				. /	-	1000000	and the	A DECEMBER OF	40000	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Miun	0.00	0.00	, A	2.20					1.00		0110		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6. 6	0.18	0.22	0.30	0.27	-0.10	-0.20	-0.06	0.25	0.45	0.32	0.29	0.04	0.16
$\begin{array}{cccccccccccccccccccccccccccccccccccc$													- CO - 17 TO -	10000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				2 14 10				100000000000000000000000000000000000000		1	OF REAL PROPERTY.	150500000	State of the last	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		In Family				U. D. 140		4	-0.02		0.26	1 63 35		100
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Electrical Sections	Commence of the	0.31	0.01	0.05	-0.13	-0.18	-0.10	-0.08	0.02	0.05	0.05	0.04	0.02
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							1000				1	The same	1	1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						2000 2000		CONTRACTOR TOTAL	1 1 1 1 1 1 1 1 1 1 1 1	1000	TANKS IN			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	The state of the s		111111111111111111111111111111111111111	The state of the s	7 7 7 7 7 7 7			The second second	- Land		7 1000	17 - 25 - 20 10	1000	100
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			12 444 314								- A A S A S A S A S A S A S A S A S A S			The state of the s
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$									Shu S		Inc.			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								71 10.01	78	1	11.0	6		(2 As 197-197 A.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								THE R. LEWIS CO., LANSING		100000000000000000000000000000000000000	The second second		103 M. C. C. C. Y.	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1									- Bearing	The state of the s	Table 1999	
7. 2.2(9) -0.05 -0.09 -0.02 -0.08 -0.32 -0.27 -0.18 -0.10 -0.08 0.05 -0.04 -0.07 -0.11	7. 1	-0.18	-0.12	-0.02	-0.47	-0.88	-1.04	-0.82	-0.68	-0.46	-0.23	-0.35	-0.12	-0.50
7. 2.2(9) -0.05 -0.09 -0.02 -0.08 -0.32 -0.27 -0.18 -0.10 -0.08 0.05 -0.04 -0.07 -0.11	9.12.3.9	-0.56	-0.60	-0.80	-0.94	-1.25	-1.29	-1.14	-1.16	-1.04	-0.59	-0.38	-0.13	-0.82
Dail ext.   -0.25 -0.31 -0.17 -0.05   0.35   0.39   0.22   0.05 -0.20 -0.26 -0.28 -0.06 -0.05				C Didentil							700000	Della della	313/12/	
Date Office of the Control of the Co	Dail. ext.	-0.25	-0.31	-0.17	-0.05	0.35	0.39	0.22	0.05	-0.20	-0.26	-0.28	-0.06	-0.05

#### LXXII.

NORWAY. - DRONTHEIM. Lat. 63° 26' N. Long. 10° 25' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumut.

					Degree	s of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Name of the last		1000	100	9-78	-		718			13			VEN
Morn. 1	0.29	0.41	0.77	1.94	2.63	2.64	2.53	2.51	1.37	0.89	0.27	0.33	1.38
2	0.25	0.50	0.95	2.09	2.97	2.76	2.75	2.68	1.48	0.91	0.31	0.31	1.50
3	0.22	0.64	1.11	2.19	3.13	2.82	2.77	2.91	1.59	0.97	0.23	0.42	1.58
4	0.20	0.71	1.27	2.32	3.03	2.82	2.65	2.77	1.55	1.07	0.28	0.34	1.58
5	0.13	0.75	1.37	2.05	2.76	2.52	2.35	2.58	1.59	0.86	0.30	0.42	1.47
6	0.11	0.82	1.42	1.67	2.30	1.96	1.86	2.13	1.49	0.71	0.14	0.43	1.25
7	0.04	0.58	1.35	1.36	1.68	1.39	1.17	1.58	1.07	0.42	0.00	11-11	0.92
8	0.08	0.23	1.17	0.94	0.83	0.61	0.40	1.02	0.57		-0.02	0.36	0.52
		1									130		
9	0.00	7000	0.41			-0.03		0.22			-0.14	0.19	-0.02
10	-0.09	100						2,000,000,000	100000		-0.16	. VO 2 1911	-0.65
11		-0.78									-0.33		10000000
Noon	-0.59	-1.08	-1.35	-2.57	-2.81	-2.43	-2.77	-3.21	-2.05	-1.20	-0.38	-0.42	-1.75
1	-0.80	-1.22	-1.70	-2.66	-3.28	-3.25	-3 20	-3 30	-2 12	-1.14	-0.44	-0.42	-1.97
2	1 "		115000								-0.42		
3	1	-0.80		-2.22							-0.28		
4		13.3	- 175 Carlo				100	- 1			-0.16		1
		1700											2.10
5	-0.29	-0.36		-1.30	10000		Park 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	-1.09	-0.50	-0.06	-0.22	-1.15
6	-0.17			-0.90	-1.70	-1.84	-1.15	-1.27	-0.79	-0.51	0.08	-0.23	-0.78
7	0.09			-0.57	100	1.000			-0.32		0.09	-0.30	-0.43
8	0.27	0.17	-0.27	-0.20	-0.37	0.04	0.01	0.11	0.03	-0.02	0.17	-0.19	-0.02
9	0.45	0.37	0.00	0.16	0.50	0.41	0.66	0.51	0.43	0.22	0.05	-0.11	0.30
10	0.52	0.53	0.00	0.61	1.10	1.08	1.17	1.18	0.45	0.55	0.03	-0.06	0.65
11	0.47	0.50	0.43	0.90	1.61	1.63	1.48	1.67	1.02		0.13	0.02	0.88
Midn	0.45	0.49	0.63	1.27	1.92	2.07	1.88	2.13	1.28	1.14	0.19	0.02	1.12
			0.00		1.02		1.00		1.20	1	0.20	0.02	
				1		8	I ALC		4 30	10.45			-D = 1
6. 6	-0.03	0.36	0.34	0.39	0.30	0.06	0.36	0.43	0.35	0.10	0.11	0.10	0.24
7. 7	0.07	0.27	0.41	0.40	0.33	0.20	0.28	0.45	0.38	0.07	0.05	0.03	0.24
8. 8	0.18	0.20	0.45	0.37	0.23	0.33	0.21	0.57	0.30		0.08		0.25
9. 9	0.23	0.15	0.21	0.07	0.11	0.19	0.26	0.37		-0.04		0.04	0.14
10.10	0.22	0.03	0.05	-0.12	-0.10	0.08	-0.07	-0.02	-0.07	-0.02	-0.02	-0.02	0.00
7. 2. 9	-0.06	-0.07	-0.12	-0.31	-0.36	-0.51	-0.41	-0.42	-0.26	-0.15	-0.12	-0.07	-0.24
6. 2. 8	-0.10	100000			V				1	the second second	-0.04		
6. 2.10	-0.02	0.07		-0.06				-0.02			-0.05		
6. 2. 6	-0.25	0		1314			LAYS TO THE				-0.07		
7. 2	-0.32	-0.29			100000000000000000000000000000000000000				1 000	-	-0.21	1	100000000000000000000000000000000000000
8. 2	-0.30										-0.22		
8. 1											-0.23		
7. 1	-0.38	-0.32	-0.18	-0.65	-0.80	-0.93	-1.02	-0.91	-0.53	-0.36	-0.22	-0.03	-0.53
9.12.3.9	-0.16	-0.40	-0.62	-1.16	-1.46	-1.28	-1.33	-1.49	-0.89	-0.59	-0.19	-0.18	-0.87
7. 2.2(9)	0.07	1									-0.02		
	1	E LINE				12		1844 S			1900	24	
Dail. ext.	-0.14	-0.20	-0.14	-0.17	-0.08	-0.25	-0.22	-0.24	-0.35	-0.07	-0.07	-0.02	-0.16
7													

STRAIT OF KARA. Lat. 70° 37' N. Long. 57° 47' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

E STATE OF		155		40	Degre	es of Re	aumur.		0.05				
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	0.00	0.00		0.50	2.00	- 00		0.00	0.00	0.00	0.00	-	
Morn. 1	0.27	0.38	1.66	2.53	2.26	1.86	1.37	0.62	0.33	0.00		0.55	0.99
2	0.24	0.38	1.78	2.67	2.22	1.68	1.24	0.58	0.40	0.02	0.14	0.42	0.98
3	0.22	0.40	1.86	2.66	2.06	1.41	1.03	0.53	0.49	0.02	0.14	0.26	0.92
4	0.23	0.42	1.88	2.44	1.82	1.12	0.79	0.47	0.58	0.06	0.15	0.11	0.84
5	0.25	0.42	1.80	1.98	1.48	0.82	0.54	0.38	0.61	0.17	0.22	-0.00	0.72
6	0.27	0.33	1.55	1.30	1.01	0.49	0.25	0.26	0.58	0.29	0.36	-0.15	0.55
7	0.29	0.16	1.10	0.52	0.40	0.10	-0.05	0.10	0.42	0.35	0.52	-0.29	0.30
8	0.30	0.08	0.42	-0.27	-0.30		THE STATE OF	-0.07	0.27	0.32	0.64	-0.42	0.01
9	0.26	0.30	-0.43	-0.98	-1.01	-0.78	-0.66	-0.23	0.01	0.18	0.66	-0.54	-0.32
10		10000000	110000	100000	-7.00		3.6987250	-0.36	11100000000	0.02	N. Z. J. C. E. T.	-0.61	
11		-0.64		100000017	1100 1100				All Dollar All			-0.62	
Noon	123700	-0.70		-2.41	100000000000000000000000000000000000000	-1.62	1 1 1 1 1 1 1 1 1	1000	-0.72	-0.37		-0.54	1000
Noon	0.12	0.10	2.00	2.41	2.21	-1.02	1.04	0.00	0.12	0.57	0.10	-0.04	1.07
1	-0.31	-0.70	-2.70	-2.67	-2.26	-1.62	-1.03	-0.63	-0.81	-0.43	-0.13	-0.44	-1.14
-2	-0.49	-0.64	-2.52	-2.81	-2.11		-1.00	1000	-0.78	-0.36	-0.25	-0.31	-1.13
3	-0.60	1777	-2.10		11000	-1.40	100000	OF THE	-0.66	L. M. C. D.	-0.30	70 00	-1.03
4		-0.38	-1.54		-1.61		100 100		1 454 9 34	-0.10	THE WAY		-0.87
					1				THE STATE OF				
5	-0.58	-0.21	-0.98	-1.91	2000	-1.05		-0.59	-0.30	10000	-0.35	-0.04	-0.67
6	-0.46	-0.02	-0.47	-1.18	-0.90	-0.76		-0.38	-0.13	THE PARTY.	-0.41	0.06	-0.43
7	-0.26	0.14	-0.04	-0.37	-0.40	-0.35	-0.29	-0.09	0.06	0.08	-0.48	0.18	-0.15
8	-0.06	0.32	0.34	0.42	0.20	0.18	0.11	0.22	0.11	0.07	-0.52	0.33	0.14
	0.11	0.19	0.00	1.00	0.00	0.00	0.54	0.40	0.18	0.00	0.40	0.40	0.40
9	0.11	0.42	0.67	1.08	0.83	0.78	0.54 0.94	0.46	0.17	1112777	-0.49	0.48	0.43
10	0.22	0.46	0.98	1.59	1.42	1.31	0.000	0.77977.5	1200 500	A MARKET	-0.38	0.61	0.67
11	0.28	0.44	1.25	1.98	1.88	1.71	1.23	0.68	0.23	200	-0.20	0.66	0.85
Midn	0.29	0.40	1.48	2.29	2.16	1.90	1.38	0.66	0.27	0.01	-0.03	0.64	0.95
					17.50			125	A TANK	4.0	7.9	V.	
6. 6	0.10	0.16	0.54	0.06	0.06	-0.14	-0.17	-0.06	0.23	0.18	-0.03	-0.05	0.06
7. 7	0.02	0.15	0.53	0.08	-0.00	-0.13	-0.17	0.01	0.24	0.22	0.02	-0.06	0.08
8. 8	0.12	0.12	0.38	0.08	-0.05	-0.08	-0.12	0.08	0.19	0.20	0.06	-0.05	0.08
9. 9	0.19	0.06	0.12	0.05	-0.09	-0.00	-0.06	0.12	0.09	0.12	0.09	-0.03	0.05
10.10	0.20	-0.02	-0.17	0.01	-0.11	0.06	0.05	0.13	-0.04	0.04	0.09	-0.00	0.02
7 2 0	-0.03	0.09	-0.25	_0 40	-0.29	_0 99	_0.17	_0.05	-0.06	0.09	-0.07	_0.04	-0.13
7. 2. 9	100000		12500.711	3000	AR STATE	2000	100000	100000	100.000	-0.00		1010.7100.0	F301 7 3
6. 2. 8	-0.09		-0.21		ADLEDA .	100000	0.06	The second		-0.00	11 2 2 2 2 2 4 2 5	Children Children	-0.15
6. 2.10	-0.00		-0.00	0.03	0.11 $-0.67$	0.09 -0.60	100	-0.28		THE PARTY NAMED	11000	0.05	0.03
6. 2. 6	-0.23	-0.11	-0.48	-0.90	-0.07	-0.00	0.40	-0.20	-0.11	-0.00	-0.10	-0.13	0.34
7. 2		-0.24	3 9 5 5 5 5		-0.86				24/2018/31	7 10 10 10 10 10 10 10 10 10 10 10 10 10	1000000000	-0.30	1901,000
8. 2								-0.39			14034000	-0.37	100 000
8. 1	-0.01	-0.39		-1.47		-0.98	CLL CON TO	1,000000	-0.27	1000910	350000000	-0.43	A 100 CO
7. 1	-0.01	-0.27	-0.80	-1.08	-0.93	-0.76	-0.54	-0.27	-0.20	-0.04	0.20	-0.37	-0.42
9.12.3.9	-0.09	-0.28	-1.11	-1.27	-1.08	-0.76	-0.53	-0.27	-0.30	-0.09	-0.01	-0.20	0.50
7. 2.2(9)	0.01	0.09	TIME 1453	-0.03	91020000	0.03	0.01		-0.01	1200000	-0.18	0.09	0.01
North Park	-0.17	_0 19	-0.43	-0.07	-0.01	0.14	0.17	-0.04	-0.10	-0.04	0.07	0.09	-0.08
Dail. ext.	0.17	1.12	0.41	-0.07	-0.01	0.14	0.17	0.04	0.10	0.04	0.07	0.02	כטיי

#### LXXIV.

NOVAIA ZEMLIA. - MATOSCHKIN SCHAR. Lat. 73° - N. Long. 57° 20' E. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	es of Re	aumur.						THE PLAN
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
		0.70	0.10	7 00	2 40	7	1 10	0 70	7 00	0 40	0.74	0.77	0 70
Morn. 1	-0.22 -0.30	Entre A	0.46	1.63 1.34	2.42	1.70 1.54	1.18 1.20	0.73	0.88		-0.14 $-0.14$	-0.11 0.05	0.70
3	-0.31		0.70	1.15	1.89	1.26	1.11	0.80	0.62	100000	-0.14	0.03	0.61
4	-0.26	1	1.02	10	1.41	0.93	0.94	0.72	0.46	0.02		0.26	0.54
		1	All Land	TE II								17715	
5		-0.09	0.99	0.81	0.85	0.61	0.73	0.55	0.46	0.20	1	0.34	0.45
6 7		-0.09	0.86	0.63			0.47	0.30	0.56 0.58	0.26		0.41	0.34
8		-0.07 $-0.05$	0.62	0.09		-0.02 $-0.38$	1000000		0.38	0.18	1	0.45	0.16 -0.07
0	0.10	-0.00	0.04	-0.50	1.05	0.00	0.10	0.00	0.00	0.00	0.20	0.40	-0.07
9	0.10	-0.05	0.02		-1.65					-0.06		0.43	-0.33
10	0.07							-0.79					-0.61
11		-0.10					1 - V	-0.91	200	-0.14	1000		-0.79
Noon	0.05	-0.13	-0.78	-2.09	-2.67	-1.58	-1.08	-0.93	-1.46	-0.12	0.11	0.18	-0.88
1	0.06	-0.14	-0.93	-1.93	-2.58	-1.52	-1.06	-0.85	-1.32	-0.10	0.08	0.10	-0.85
2	0.09	1 1 1 1 1 1 1 1	1	-1.62				-0.70		-0.09		-0.02	7777
3	0.10	-0.11			-1.83			-0.52	-0.40	-0.07	-0.04	-0.11	-0.58
4	0.10	-0.07	-0.71	-0.80	-1.30	-0.78	-0.66	-0.32	-0.07	-0.02	-0.10	-0.20	-0.41
	0.70	0.00	0.50	0 = 1	0.00	0 **	0 54	0.14	0.00	0.10	0.10	0.00	0.00
5 6	0.10	1 2 2 1	-0.50 $-0.30$		TOTAL COLUMN	-0.57 -0.38	-0.54		-0.02 $-0.17$		-0.18 -0.20		
7	0.10	15.00	-0.30	0.30	0.46	-0.16		0.12	-0.17		-0.18		
8	0.12	1000	-0.09	0.70	1.04	- 1 mm - m	-0.11	0.21	2000000	1000	-0.14		0.13
												0.10	0.20
9	0.12		-0.06	1.24	1.59	0.56	0.14	0.30	-0.12		-0.10		0.31
10	0.08	0.19	-0.02	1.50	2.06	1.02	0.46	0.39	0.33	100	-0.08		0.47
11	-0.00	0.21	0.09	1.75	2.40	1.42	0.78	0.50	0.79		-0.08		0.61
Midn	-0.11	0.20	0.23	1.72	2.55	1.66	1.03	0.62	1.06	-0.39	-0.11	-0.22	0.69
	Photo:			Barby.	1 1					100			7 8 9
6. 6	0.04	0.04	0.28	0.19	0.06	-0.04	0.02	0.15	0.20	0.26	0.00	0.03	0.10
7. 7	0.08	0.01	0.23	0.20		-0.09		0.07	0.12	0.29	0.04	0.01	0.08
8.8	0.11	0.03	0.13	0.10		-0.12			0.01	0.26		-0.01	0.03
9. 9	0.11	0.05	-0.02	0.05	and the same of th	-0.11	The second second	-0.14	-0.06	0.15	0.07	-0.03	-0.01
10.10	0.08	0.07	-0.15	-0.14	-0.06	-0.07	-0.15	-0.20	-0.19	-0.01	0.05	-0.04	-0.07
7. 2. 9	0.09	-0.02	-0.13	-0.10	-0.36	-0.26	-0.21	-0.13	-0.14	0.15	0.06	-0.02	-0.09
6. 2. 8		-0.04								0.21	0.03	-0.03	-0.09
6. 2.10	A	-0.01						-0.00	-0.00	0.12	0.05	-0.02	0.03
6. 2. 6	0.05	-0.07	-0.13	-0.42	-0.72	-0.47	-0.31	-0.13	-0.17	0.14	0.01	0.01	-0.18
7. 2	0.08	-0.11	-0.17	-0.77	-1.33	-0.67	-0.30	-0.35	-0.16	0.05	0.14	0.22	-0.29
8. 2		-0.10			A CHEST SALE			C C 20 C 20 C 20 C	CONTRACT AND		0.14	- In the second	-0.40
8. 1		-0.10						-0.58		-0.02	0.17	0.28	-0.46
7. 1		-0.11						A Committee of the	The second of the last	0.04	0.17		-0.34
9.12.3.9		100	- W					100		0.0-	0.0-	0.00	0.08
7. 2.2(9)	0.09	0.04	-0.43 $-0.12$	C/9020144 (60)	-1.14	-		-0.43	San Land St.	0.03	0.05	-0.00	-0.37
1.2(0)	0.10	0.02	0.12	0.24	0.13	-0.06	-0.13	-0.02	-0.14	0.20	0.02	-0.14	0.01
Dail.ext.	-0.10	0.04	0.03	-0.17	-0.06	0.06	0.06	-0.07	-0.19	-0.02	0.03	-0.02	-0.09
									- 11				

#### LXXV.

NORWAY. - BOSSEKOP. Lat. 69° 58' N. Long. 22° E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	Sept.	Oct.	Nov.	Dec.	80 Days without Sun.
A.M. 2	-0.26	0.36	1.37		1.20	0.66	0.04	0.35	0.04
4	-0.11	0.30	1.78		1.01	0.53	-0.03	0.42	0.10
6	0.00	0.50	1.90		1.22	0.73	0.04	0.28	0.08
8	0.09	0.26	1.18	0.36	0.62	0.41	0.07	0.10	0.02
10	-0.13	-0.19	-1.09	-0.85	-1.01	-0.29	-0.15	-0.14	-0.19
Noon.	0.18	-0.79	-2.39	-1.29	-1.66	-1.05	-0.13	-0.09	-0.03
2	0.20	-1.02	-2.85	-1.22	-1.69	-1.02	-0.09	-0.34	-0.10
4	0.30	-0.11	-2.38	-0.82	-1.54	-0.50	0.09	-0.38	0.06
6	0.18	0.06	-0.57	-0.10	-0.27	-0.17	0.18	-0.23	0.09
8	0.12	0.16	0.46	0.70	0.39	0.09	0.14	-0.26	0.02
10	-0.34	0.21	1.19	1.44	0.79	0.13	-0.03	0.14	-0.10
12	-0.27	0.22	1.39	1.83	0.89	0.49	-0.13	0.17	-0.10
Mean.	-7.67	-6.39	-7.55	-0.77	5.91	-1.62	-6.55	-5.66	-7.66

LXXV'.

NORWAY. — BOSSEKOP. Lat. 69° 58' N. Long. 22° E. Greenw. Centigrade Degrees.

Hour.	Jan.	Feb.	March.	April.	Sept.	Oct.	Nov.	Dec.	80 Days without Sun.
A.M. 2	-0.32	0.45	1.71		1.50	0.82	0.05	0.44	0.05
4	-0.14	0.37	2.22		1.26	0.66	-0.04	0.52	0.12
6	0.00	0.62	2.37		1.52	0.91	0.05	0.35	0.10
8	0.11	0.32	1.47	0.45	0.77	0.51	0.09	0.12	0.02
10	-0.16	-0.24	-1.36	-1.06	-1.26	-0.36	-0.19	-0.17	-0.24
			de abij			miles.			- 31810
Noon.	0.22	-0.99	-2.98	-1.62	-2.07	-1.31	-0.16	-0.11	-0.04
2	0.25	-1.27	-3.56	-1.52	-2.11	-1.27	-0.11	-0.42	-0.12
4	0.37	-0.14	-2.97	-1.02	-1.92	-0.62	0.11	-0.47	0.07
6	0.22	0.07	-0.71	-0.12	-0.34	-0.21	0.22	-0.29	0.11
8	0.15	0.20	0.57	0.87	0.49	0.11	0.17	-0.32	0.02
10	-0.42	0.26	1.48	1.80	0.99	0.16	-0.04	0.17	-0.12
12	-0.34	0.27	1.73	2.29	1.11	0.61	-0.16	0.21	-0.12
Mean.	-9.59	-7.99	-9.44	-0.96	7.39	-2.02	-8.19	-7.07	-9.57

Panker or 1			10.10	all give			
			Marie .		NAME OF	Skills.	
	13.12						

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# HOURLY CORRECTIONS

FOR

# PERIODIC VARIATIONS.

AFRICA. - AUSTRALIA.

MOUNTLY CONTROLLORS

PREIODIC VARIATIONS.

ALIARTSUA - AUSTRA

#### LXXVI.

#### Africa. - St. Helena. Lat. 15° 55' S. Long. 5° 43' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.76	0.70	0.63	0.58	0.52	0.43	0.48	0.43	0.52	0.62	0.71	0.73	0.59
1	0.85	0.76	0.71	0.66	0.61	0.48	0.53	0.48	0.56	0.71	0.78	0.81	0.66
2	0.93	0.84	0.77	0.70	0.66	0.54	0.56	0.53	0.62	0.78	0.86	0.90	0.72
3	1.03	0.92	0.86	0.76	0.73	0.59	0.62	0.63	0.69	0.86	0.95	0.98	0.80
4	1.06	1.00	0.92	0.81	0.80	0.65	0.66	0.66	0.76	0.91	0.99	1.02	0.85
5	1.11	1.04	0.93	0.86	0.83	0.67	0.69	0.73	0.79	0.94	1.02	1.08	0.89
6	1.15	1.07	0.98	0.93	0.83	0.68	0.72	0.74	0.83	0.99	1.07	1.09	0.92
7	1.16	1.08	0.97	0.94	0.89	0.71	0.75	0.79	0.81	0.96	1.03	1.06	0.93
8	0.95	0.99	0.78	0.85	0.88	0.69	0.72	0.72	0.72	0.77	0.80	0.98	0.82
9	0.53	0.63	0.52	0.49	0.46	0.42	0.41	0.43	0.42	0.38	0.40	0.48	0.46
10	-0.05	0.06	-0.07	-0.04	-0.08	-0.04	-0.04	-0.02	-0.05	-0.17	-0.16	-0.09	-0.06
11	-0.62	-0.55	-0.49	-0.51	-0.47	-0.40	-0.40	-0.40	-0.55	-0.66	-0.67	-0.56	-0.52
Noon.	-1.14	-1.06	-0.95	-1.00	-0.96	-0.73	-0.76	-0.80	-0.92	-1.11	-1.12	-1.08	-0.97
1	-1.64	-1.46	-1.28	-1.31	-1.20	-1.04	-1.06	-1.12	-1.25	-1.45	-1.60	-1.52	-1.33
2	-1.81	-1.67	-1.48	-1.46	-1.32	-1.20	-1.26	-1.25	-1.42	-1.67	-1.80	-1.80	-1.51
3	-1.76	-1.78	-1.62	-1.50	-1.35	-1.18	-1.24	-1.31	-1.38	-1.64	-1.84	-1.82	-1.54
4	-1.69	-1.66	-1.54	-1.35	-1.24	-1.03	-1.12	-1.13	-1.20	-1.37	-1.64	-1.76	-1.39
5	-1.48	-1.38	-1.27	-1.06	-0.94	-0.78	-0.84	-0.86	-0.91	-0.99	-1.24	-1.38	-1.09
6	-0.92	-0.91	-0.83	-0.61	-0.47	-0.40	-0.44	-0.42	-0.43	-0.48	-0.66	-0.82	-0.62
7	-0.27	-0.33	-0.28	-0.11	-0.23	-0.03	-0.07	-0.03	0.01	0.02	-0.04	-0.18	-0.13
8	0.26	0.21	0.18	0.20	-0.12	0.17	0.13	0.15	0.23	0.29	0.32	0.30	0.19
9	0.47	0.44	0.34	0.34	0.14	0.26	0.23	0.25	0.32	0.26	0.48	0.48	0.33
10	0.60	0.55	0.48	0.44	0.41	0.32	0.33	0.32	0.38	0.49	0.56	0.58	0.46
11	0.69	0.64	0.55	0.51	0.45	0.39	0.38	0.38	0.46	0.55	0.64	0.67	0.53
Mean.	14.21	15.04	15.22	14.93	13.80	12.48	11.55	11.19	11.14	11.66	12.37	13.23	

#### LXXVII.

Africa.—Cape of Good Hope. Lat. 33° 56′ S. Long. 19° 39′ E. Gr.—Dove.

Degrees of Reaumur.

Hour	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	1.69	1.50	1.51	1.37	1.00	0.88	1.04	0.85	1.07	1.45	1.62	1.85	1.32
1	2.80	1.64	1.64	1.49	1.07	1.01	1.20	1.03	1.25	1.62	1.79	2.01	1.55
2	1.89	1.74	1.81	1.61	1.14	1.09	1.33	1.14	1.39	1.72	1.98	2.16	1.58
3	2.01	1.92	1.92	1.70	1.24	1.16	1.43	1.23	1.54	1.82	2.12	2.30	1.70
4	2.10	2.00	2.05	1.88	1.34	1.30	1.53	1.37	1.63	1.92	2.21	2.42	1.81
5	1.96	2.13	2.13	1.93	1.46	1.42	1.59	1.53	1.59	1.93	1.92	2.01	1.80
6	1.06	1.53	1.97	1.98	1.59	1.48	1.73	1.55	1.62	1.26	0.85	0.86	1.46
7	0.15	0.70	1.21	1.39	1.41	1.47	1.57	1.22	0.81	0.39	-0.02	-0.20	0.84
8	-0.53	-0.01	0.16	0.36	0.53	0.86	0.77	0.64	-0.06	-0.46	-0.67	-0.81	0.06
9	-1.10	-0.80	-0.76	-0.68	-0.39	-0.12	-0.24	-0.42	-0.82	-1.24	-1.25	-1.36	-0.77
10	-1.72	-1.65	-1.66	-1.48	-1.10	-0.90	-1.09	-1.08	-1.41	-1.82	-1.80	-1.90	-1.47
11	-2.23	-2.31	-2.37	-2.10	-1.64	-1.46	-1.72	-1.63	-1.85	-2.25	-2.24	-2.25	-2.00

#### LXXVII.

#### AFRICA. - CAPE OF GOOD HOPE, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-2.48	-2.72	-2.66	-2.56	-2.09	-1.92	-2.11	-1.88	-2.15	-2.45	-2.46	-2.52	-2.33
1	-2.54	-2.74	-2.95	-2.81	-2.20	-2.07	-2.33	-2.04	-2.23	-2.55	-2.48	-2.61	-2.46
2	-2.42	-2.54	-2.86	-2.79	-2.14	-2.06	-2.33	-1.97	-2.18	-2.44	-2.30	-2.44	-2.37
3	-2.16	-2.20	-2.51	-2.42	-1.84	-1.86	-2.13	-1.77	-1.82	-2.08	-2.01	-2.16	-2.08
4	-1.75	-1.70	-1.78	-1.75	-1.28	-1.28	-1.49	-1.32	-1.28	-1.52	-1.66	-1.90	-1.56
5	-1.21	-1.09	-1.03	-0.71	-0.61	-0.64	-0.76	-0.57	-0.56	-0.71	-1.05	-1.28	-0.85
0	0.10	0.70	0.70	0.00	0.00	0.00	0.00	0.75	0.00	0.00	0.01	0.75	0.70
6	-0.16	-0.13	-0.10	-0.03	-0.21	-0.29	-0.33	-0.17	0.00	0.20	-0.01	-0.15	
7	0.65	0.54	0.35	0.22	0.09	-0.05	-0.03	0.12	0.30	0.57	0.60	0.63	0.33
8	0.95	0.79	0.61	0.48	0.36	0.19	0.26	0.32	0.51	0.86	0.92	0.96	0.60
9	1.14	1.00	0.92	0.73	0.54	0.40	0.48	0.46	0.69	1.09	1.10	1.20	0.81
10	1.30	1.14	1.14	1.00	0.78	0.61	0.69	0.65	0.97	1.26	1.31	1.46	1.03
11	1.55	1.32	1.29	1.22	0.95	0.81	0.91	0.76	1.02	1.44	1.48	1.67	1.20
-	-			-									
Mean.	15.81	15.96	15.00	13.61	11.38	9.84	9.96	10.06	11.01	12.43	13.54	14.82	

#### LXXVIII.

Lat. 42° 53′ S. Long. 147° 21′ E. Gr. - Dove. Australia. — Hobarton.

	DALSUL)	(SUSPER	piene	THE PARTY	De	grees of	Reaum	ur.		100			
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	2.34	1.95	1.78	1.31	0.88	0.66	0.72	1.10	1.51	1.99	2.44	2.45	1.59
1	2.59	2.17	1.99	1.41	1.03	0.76	0.86	1.36	1.71	2.19	2.67	2.76	1.79
2	2.89	2.32	2.19	1.62	1.11	0.88	1.01	1.43	1.93	2.45	2.77	2.95	1.96
3	3.09	2.53	2.39	1.75	1.23	0.97	1.16	1.58	2.06	2.68	2.98	3.24	2.14
4	3.20	2.68	2.49	1.85	1.31	1.15	1.28	1.69	2.20	2.80	3.11	3.38	2.26
5	3.33	2.82	2.54	1.99	1.44	1.15	1.40	1.82	2.32	2.85	2.99	3.13	2.31
	0.00	2.59	0.04	0.11	7	7.00	1 50	7.07	0.04	0.00	0.04	2.24	2.14
6 7	2.62 1.48	1.75	2.64	2.11	1.55	1.29	1.50	1.91	2.34	2.60	2.24	1.03	1.61
8	0.27	0.68	2.10	2.00	1.60	1.37	1.50	1.90	1.84	0.41	0.01	-0.24	0.80
9	-0.88	1000	1.08	1.30	1.27	1.26	1.31	1.32	0.93		-1.13	-1.27	
10	-1.92	1	100000	0.24 $-0.85$	0.45 -0.46	0.60 $-0.18$	0.60 -0.21	0.44 -0.52	-0.21 $-1.21$	-0.70 $-1.68$	-2.10	-2.16	7-30 (PM)
11	-2.75			-0.89		-0.18		-0.52	-2.09		-2.10 $-2.89$		-2.02
11	-2.15	-2.54	-2.24	-1.78	-1.29	-0.90	-1.01	-1.55	-2.09	-2.54	-2.09	-2.00	2.02
Noon.	-3.51	-3.22	-3.03	-2.58	-2.00	-1.67	-1.67	-2.28	-2.70	-3.10	-3.43	-3.36	-2.71
1	-3.82	-3.52	-3.48	-2.95	-2.42	-2.08	-2.17	-2.73	-3.14	-3.48	-3.72	-3.67	-3.10
2	-3.91	-3.54	-3.63	-3.11	-2.53	-2.22	-2.38	-2.91	-3.25	-3.48	-3.67	-3.56	-3.18
3	-3.60	-3.36	-3.43	-2.87	-2.32	-2.02	-2.23	-2.71	-3.10	-3.32	-3.33	-3.45	-2.98
4	-3.20	-2.94	-2.92	-2.23	-1.69	-1.43	-1.73	-2.20	-2.53	-3.04	-3.12	-3.12	-2.51
5	-2.57	-2.22	-2.02	-1.35	-0.92	-0.73	-1.01	-1.37	-1.59	-2.02	-2.30	-2.56	-1.72
6	-1.38	-1.04	-0.81	-0.56	-0.36	_0.25	-0.48	-0.64	-0.65	-0.80	-1.01	-1.38	-1.78
7	-0.13	-0.20	-0.04		0.01	0.00	0.12	-0.13	0.01	0.05	0.20	-0.09	100
8	0.82	0.68	0.45	0.32	0.27	0.24	0.14	0.21	0.46	0.55	0.90	0.89	0.49
9	1.31	1.13	0.82	0.57	0.42	0.24	0.34	0.57	0.79	1.00	1.41	1.51	0.84
10	1.71	1.47	1.19	0.84	0.62	0.40	0.50	0.79	1.08	1.34	1.75	1.91	1.13
11	2.05		1.47	1.06	0.77	0.54	0.64	0.93	1.31	1.63	2.05	2.25	1.37
Mean.	13.38	13.96	11.96	9.41	7.69	5.93	5.21	6.24	7.97	9.39	11.38	12.95	

# CORRECTIONS FOR TEMPERATURE.

# MONTHLY AND YEARLY

CORRECTIONS FOR NON-PERIODIC VARIATIONS,

OR

# TABLES

FOR REDUCING THE MONTHLY AND YEARLY MEANS OF SINGLE YEARS
TO THE MEANS DERIVED FROM A SERIES OF YEARS.

# CONTRACTORS FOR TEMPERATURE

TENERT OF A TIMETOR

CORRECTIONS LOW KONTHUDIO AVERTIONS

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#### TABLES

FOR REDUCING THE MONTHLY AND YEARLY MEANS OF SINGLE YEARS TO THE MEANS DERIVED FROM A SERIES OF YEARS.

OBSERVATION shows that the monthly and annual mean temperature of a place somewhat varies from year to year. No law, however, has been as yet discovered as to the course of these oscillations. It follows that the means derived from observations carried on during a single year are but approximations to the true means. These last must be obtained from observations made for a series of years, during which these irregular variations become insensible by compensating each other; and it is obvious that their accuracy increases with the number of years which compose the series.

Professor Dove, having proved by his researches that these abnormal temperatures above and below the average of a whole month, or of a year, are apt to be felt simultaneously on extensive tracts of country, concluded that the means of a single year could be made available for obtaining the true means of the place, by being corrected for the non-periodic variations by means of normal stations in the same meteorological region, in which those elements had been more accurately determined by the observations of a long series of years. Comparing, namely, the means of a given year with the means derived from the whole series, we find a difference in + or -, which, applied, with reverse signs, to the means of the same year in the neighboring station to be corrected, will reduce, with a good degree of probability, the means of that particular year to the means which would have been obtained from a long series of years similar to that of the normal station.

The following tables, LXXIX. to XCVII., have been selected from those given by Dove in his five papers on the non-periodic variations of the atmospheric temperature, to be found in the *Memoirs of the Academy of Sciences of Berlin* for the years 1838, 1839, 1842, 1848, and 1853, to which we must refer for further details. They furnish normal stations for various latitudes; the columns contain the corrections for every month, viz. the differences, with *reverse* signs, between the monthly means in the year indicated in the first and last columns, and the means derived from the whole series, which are contained in the line at the bottom.

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#### LXXIX.

## Region of the Monsoons. - Madras.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

United States					De	51600 01	Keaum	ui.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1796	0.00	0.24	0.00	0.36	-0.10	-1.48	-1.16	-1.15	-0.31	-0.28	-0.47	-0.51	1796
1797			0.66	0.53	0.39	0.56	0.09	0.85		-0.33	0.16	-0.02	1797
1798	-0.13	1.12	0.40			0.39	0.53	-0.31	0.27	0.56		0.20	1798
1799	-0.13	-0.08	0.62	0.36	0.26	-0.06	-1.20	0.00	-0.36	0.38		0.25	1799
1800	0.40	0.41	0.57	1.20	-0.23	-0.50	-1.02	-0.40	-0.58	0.20	0.47	-0.60	1800
1801	0.44	0.01	1.77			-0.59	-0.67	0.63	-0.49	-0.02	-0.20	0.25	1801
1802	0.44	0.86	1.77	1.02	-0.36	0.65	0.58	-0.04	1.60	0.43	-0.02	-0.28	1802
1803	0.22	0.24	0.80	0.53	-0.32	0.08	0.18	0.80	0.80	0.38	0.33	0.65	1803
1804	1.64	1.48	0.75	1.38	0.70	0.70	1.24	0.00	0.58	0.38	0.91	0.29	1804
1805	0.27	0.41	0.66	-0.36	0.61	0.52	-0.76	-0.22	-0.27	-0.33	0.69	0.65	1805
1806	0.00	-0.39	-0.09	0.09	-0.41	-1.61	0.00	-0.13	1.07	0.47	0.96	0.12	1806
1807	0.22	-1.54	-3.20	-5.47	-1.79	0.48	1.20	-0.17	-0.09	-0.64	-0.20	0.78	1807
1813	0.80	0.37	0.13	0.96	1.12	-0.32	0.44	-0.22	-0.18	0.25	-0.38	-1.04	1813
1814	-0.36	-0.39	-0.58	0.04	-2.99	1.10	1.38	0.29	-0.22	0.07	-0.20	-0.37	1814
1815	-0.98	0.32	-0.67	2.00	1.55	-1.39	-0.98	0.27	0.31	-0.73	-0.91	-0.82	1815
1816	-1.09	-1.76	-1.56	-0.93	0.44	0.39	-0.44	-0.71	-0.67	-0.20	0.33	-0.51	1816
1817	-0.58		1		0.12		0.67	0.29	-0.71	-0.55	-0.96	0.52	1817
1818	0.22	0.32			1.41	0.65	-1.33	-2.00	-0.18	-0.55	-0.56	-0.37	1818
1819	-1.78	-1.28	-0.76	-0.13	0.48	0.88	0.44	0.98	-0.31	0.03	0.78	0.16	1819
1820	-0.67	-0.30	-0.85	0.58	-1.16	-0.32	0.18	0.23	-0.09	0.47	0.69	0.47	1820
1821	1.02	0.64	1.06	-1.51	0.26	0.08	0.58	0.94	-0.04	-0.02	0.20	0.20	1821
Means.	19.19	20.07	21.30	22.41	24.41	24.96	23.84	23.43	23.03	22.16	20.74	19.48	Means.
1822	-0.36	0.37	0.41	-0.28	0.07	-0.95	-0.76	0.72	-0.37	-0.70	-0.35	-0.19	1822
1823	0.31	0.37	-0.21	0.30	0.15	0.29	0.22	0.17	-0.60	0.72	0.27	0.97	1823
1824	0.71	0.59	0.27	0.52	-0.02	0.60	1.55	0.88	1.36	-0.93	0.14	0.26	1824
1825	-0.09	0.37	-0.21	0.12	0.24	-0.29	0.04	-0.36	0.03	0.32	0.59	-0.59	1825
1826	0.80	0.24	0.45	0.92	0.78	-1.17	0.04	-0.36	0.25	0.81	0.36	0.30	1826
1827	-0.09	-0.29	-0.17	0.17	-1.27	-0.46	-0.01	-0.09	-0.15	-0.13	0.54	0.08	1827
1828	1.07	0.51	-0.57	-0.59	-0.42	1000	-0.23	0.04	-0.60	-0.17	0.81	0.21	1828
1829	0.09	-	-0.35	0.08			-0.89	-0.01	0.16	0.54	0.23	0.12	1829
1830	-0.27	-0.74	0.01	-0.32	-2.73	-0.15	-0.36	-0.23	0.25	1.12	0.68	0.53	1830
1831	0.31	1.49	1.66	0.48	1.89	1.36	0.04	0.67	0.70	0.41	0.41	0.53	1831
1832	-0.49	-0.29	1.26	1.73	2.51	2.65	1.64	2.40	0.34	-0.25	0.46		1832
1833	0.36	0.91	-0.19	0.97	0.83	0.83	1.33	0.40	0.16	0.41	0.19	1.06	1833
1834	0.18	0.60	0.55	16.00	1.31	0.12	A	-0.18	-	-0.03	0.01	-0.01	1834
1835	-0.66			-1.07	-0.24		-0.67	-0.45		-0.74	-0.48		1835
1836	-0.75	-0.73	-1.41	-0.72	0.60	0.12	-0.58	-1.29	-0.24	0.15	-0.92	-1.03	1836
1837	-0.31	-0.02	0.06	-0.63	-1.17	-0.41	-0.40	-0.05	0.03	-0.34	-0.17	-0.85	1837
1838	-1.24	-0.69		0.04	-0.33	174200 000	0.75	-0.05	0.65	100	-0.57		1838
1839	0.36	-0.11	-0.12	-0.45	-0.15	-0.41	-0.49	-0.93	-0.68	0.68	-0.83	0.71	1839
1840	-0.13	-0.42	-0.70	0.17	0.29	0.25	-0.45	0.27	-0.77	0.19	-1.14	-0.32	1840
1841	0.05	-0.16	-0.17	-0.58	-1.17	-0.81	0.35	-0.71	0.74	-1.28	-0.34	-0.27	1841
1842	-0.09	-0.51	-0.08	-0.49	0.47	0.07	0.00	0.09	-0.86	-0.30	-0.30	-0.23	1842
1843	0.23	-0.02	-0.03	0.22	-1.53	-1.04	-0.22	0.44	0:16	-0.52	0.23	-0.32	1843
Means.	20.53	21.31	22.92	24.27	25.62	25.35	24.31	23.73	23.70	22.92	21.32	20.67	Means.

#### LXXX.

#### SICILY. - PALERMO.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

			100		De	grees of	Reaum	ır.			6	17 H. C.	
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	7.00
1791					-0.44		-0.52			2000		100	1791
1792	1.18	0.51	0.09	0.12	and the state of	1.12	1.00		-0.63	0.22	-0.83		1792
1793	-1.68	-0.38	-0.33		-2.04		-1.28		0.86		-0.25	0.44	1793
1794	-0.04	-0.69	-0.51	1	-0.79		-0.81	1	100000		-0.29	-0.47	1794
1795	-1.62	1.27	0.78	-0.10	0.12	-0.59	-1.12	-0.34	-0.72		-0.23	0.18	1795
7800	0.00	0.50	- 004	1 70	0.10	0.50	0.00	0.01	0.40		0.00	0.00	1800
1796	0.78	0.58	-0.84	100	-0.19	-0.59	1 1		0.40	1.11	0.00	0.98	1796
1797 1798	0.03	10000	-1.15 0.78		-0.24 $-0.99$	-0.70	-0.56 $0.72$	0.39	0.15	27.75.75	-0.12	0.16	1797 1798
1799	-1.75	1.38	0.78	0.64	10.63276	0.45	0.72	0.75	0.00	-1.00	1.97	0.31	1798
1800	2.27	2.96	0.69		0.63	-0.14	0.37	1000000	-0.58		-0.32 -0.18	0.40	1800
1000	2.21	2.00	0.03	2.40	0.00	-0.14	0.20	0.41	-0.50	0.02	-0.10	0.09	1000
1801	-0.11	0.76	1.45	0.24	-0.10	-0.16	1.26	-0.56	-0.07	1.04	1.04	1.64	1801
1802	0.09	1 19 19 19	0.47	-1.01		2.50	0.17	0.72	0.42	0.77	1.51	1.40	1802
1803	1.67	1	0.11		-1.08	0.66	0.04	0.52	0.31	-0.65	1.42	0.42	1803
1804	4.63	1111777	0.16	0.21	0.14	1.30	1.12	0.12	-0.14	0.31	1.22	1.40	1804
1805	0.80	1000	-0.68	-1.59	-1.59	1.21	-0.65	- AUTO- NO.			-1.85	-1.02	1805
2000				2.00	1.00		0.00	0.01	1.02	0.00	1.00	1.02	1000
1806	-1.15	0.64	-0.04	-0.50	0.41	0.10	-0.14	-0.85	-1.16	-0.43	-0.14	0.40	1806
1807	-1.06	0.16	0.34	-1.21	0.74	0.90	1.37	0.92	2.80	1.26	1.95	-0.07	1807
1808	-0.24	10000000	-0.86		-0.48	-0.43	0.88	0.04	2.42	-1.92	1150000	-2.31	1808
1809	0.87	-0.31	0.23	-0.50	-0.48	0.86	1.46		A TOTAL STATE OF	-1.67		-0.98	1809
1810	0.01	-0.27	2.49	0.28	0.50	-0.63	-0.54	-0.19	-0.29	-0.67	0.06	-0.91	1810
		114.83							TWO			1000	
1811	-0.15	0.69	-0.91	0.24	0.43	1.46	0.97	0.26	0.04	0.95	0.00	-0.76	1811
1812	-1.51	0.40	0.00	-0.39	-0.61	0.15	-1.32	-0.21	-0.69	-0.16	0.35	-0.18	1812
1813	-1.51	-1.02	-0.80	-0.52	0.79	0.32	-0.92	-1.25	-1.00	1.31	0.04	-1.18	1813
1814	0.54	-3.04	-0.88	0.04	-1.46	-0.59	-0.96	-0.56	-2.03	-0.49	-0.52	-0.42	1814
1815	-0.46	0.07	0.29	0.90	0.61	-0.63	-1.12	-2.01	-0.78	0.22	0.08	-0.78	1815
											the	-	
1816	-0.40		-0.71	-0.54	0.05	1000	- San	100000000000000000000000000000000000000	-0.80	-1.09	104177.01		1816
1817	-0.11		10000		• •		-0.39	TU 6/911	-0.34	0.11	-0.47	1 193	1817
1818	-0.66	0.87	• •	1.21	0.19	-1.10	TOTAL STREET	-0.45	0.24	-0.78	0.33	0.62	1818
1819	-1.02	0.18	0.72	0.97	-0.12	-0.21	-0.28	-0.34	Call Value	0.82	1.11	0.82	1819
1820	1.89	-0.11	-0.97	0.37	2.03	0.68	0.48	84.	• •		-0.65	0.29	1820
1821	1.00	-0.76	0.49	0.50	0.85	-0.74	-0.20	-0.21	0.51	-0.74	-0.72	0.69	1821
1821	1.92 -1.28	-0.76			0.68	2.97	-0.30	-100	1.88	3772-00		0.69	
1822	0.52	1.78	-0.53 $-0.80$	0.28	0.08	0.30	1.48 -0.36	1.46 0.35	-0.34	1.51 -0.76	0.06 -1.63	-0.53	1822 1823
1824	-0.91	0.42	-1.04	-1.01	1.25	-0.25	1000	1.86	0.13	1.51	0.64	0.51	1823
1825	-1.04	THE PARTY	-0.17	0.12	0.30	-0.45	-0.10	0.46	0.15		-0.05	1.67	1825
1020	1.04	1.02	0.17	0.12	0.00	0.20	0.10	0.40	0.00	1.00	0.00	1.07	1020
1826	-0.88	0.56	-0.29	-0.59	-1.08	-0.74	0.39	0.52	1.35	0.46	-0.87	-0.24	1826
1827	0.07	0.83	0.82	-0.51	0.18	-1.30	0.80	1.33	-0.73	C 100 100 100 100 100 100 100 100 100 10	-1.76		1827
1828	-0.16	0.20	0.23	0.29	1.99	1.28	2.48	1.10	0.74	-0.34		-0.37	1828
1829	0.79	-1.90	1.12	2.49	-0.09	-0.47	0.16	-0.12	0.41	-0.38	-0.35	100 SHALL 1	1829
1000								-					
Means.	8.35	8.27	9.40	11.52	14.35	17.12	19.25	19.48	17.60	14.78	11.69	9.44	Means.
The same of		1 10	4	36.43	61:17		II.	ROLL BEST	5133	47 7 3	THE PLANE	98 R	

## LXXXI.

## NORTH ITALY. - MILAN.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

-						DC	51005 01	Keaum	ui.					
	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	1763	° -1.32	° 1.58	-0.60	0.27	° -2.28	-0.79	0.68	° 1.11	° -1.11	° -1.69	0.56	° 1.02	1763
	1764	1.68	1.98	-0.70	-0.63	1.32	0.91	-0.12	-1.29	-1.21	-1.19	-0.26	1.52	1764
ı	1765	3.88	-0.92	0.60	0.47	-1.08	0.11	-2.62	-1.69	-0.11	0.11	0.24	-0.98	1765
4	1766	-3.42	-1.52	-0.40	0.57	0.02	1.31	-1.32	-0.19	-1.21	-0.49	2.14	-0.68	1766
	1767	-4.22	0.38	0.10	-0.93	-1.08	-1.19	0.78	-0.69	William.			-0.88	1767
									22/11			-IIR		
	1768	-0.82	-1.22	-1.50	0.37	-0.58	-2.19	0.68	0.51		IR.D-	0.64	-0.78	1768
	1769	1.88	-0.42	-0.50	-1.63	-0.48	1.01	-0.52	1.51		-2.19	1.24	0.62	1769
4	1770	-0.52	0.98	-0.60	-0.33	-0.58	0.81	-0.72	0.01	1.99	0.51	1.04	-0.68	1770
	1771	1.78	-0.52	-0.60		1.02	-0.19	0.68	1.51	0.49	-0.69	-1.06	The second second	1771
	1772	1.58	2.48	2.50	0.57		1.61	1.38	0.41	0.29	2.01	1.94	2.02	1772
													010,112	
	1773	1.58	-0.42	-0.80	-0.03	-0.48		-1.72	-1.29	0.69	1.61	0.34	1.82	1773
	1774	0.48	0.08	0.70	0.77		0.51	-0.12	1.31	-0.31	-1.09		-2.68	1774
	1775	0.38	2.08	1.60	0.47	To the late	0.71	0.78	-0.09	-0.31	-1.79	The same	-0.88	1775
	1776	-0.32	-0.02	1.30	0.97	100	0.11	0.48	0.41	-0.71	0.11		-1.18	1776
	1777	-1.52	-1.42	1.30	-0.23		-0.79	-1.22	0.51	0.19	0.41	1.24	March Committee	1777
							1,5							
	1778	0.38	0.08	-1.90	1.47	0.62	-0.29	0.98	0.81	-0.81	-0.09	0.64	1.72	1778
	1779	-3.52	1.98	0.00	1.07	1.72	-1.39	0.18	-0.19	1.59	1.81	-0.16	1.82	1779
	1780	-0.62	-1.92	2.70	-0.43	1.72	1.51	0.78	0.11	-0.51	1.81	-0.16	-1.08	1780
	1781	-0.12	0.38	1.90	1.47	0.22	0.01	1.78	0.41	0.39	-0.89	0.04	1.42	1781
	1782	2.18	-2.42	-0.70	-1.03	-1.08	1.21	2.08	0.91	-0.31	-1.79	14070	-0.58	1782
I	47.77					1			0.02	0.02	2	2.10	0.00	
	1783	0.98	1.18	-0.60	0.97	0.42	-0.99	1.08	-0.29	-0.31	1.51	0.24	-1.88	1783
	1784	0.48	-2.02	0.50	-2.03	2.62	2.11	1.38	0.61	1.49	-1.49		-1.18	1784
	1785	0.58	-1.12	-3.80	-1.23	0.72	1.21	0.68	0.61	2.69	0.41	0.74	2.02	1785
	1786	0.18	0.68	-0.90	0.87	0.72	0.81	-0.52	-0.89	1.09	-1.89	-0.36	1000	1786
	1787	-0.32	0.08	0.90	-0.03	-1.98	1.71	-0.02	1.61	0.09	0.81	0.84	1.72	1787
		401.			6.5	1.41								
	1788	2.78	1.08	2.30	1.37	-0.18	1.51	2.78	-0.39	0.99	0.21	-0.86	-2.88	1788
	1789	-1.72	0.98	-1.70	1.37	2.22	-0.79	0.28	0.11	0.29	0.31	-1.26	-2.38	1789
	1790	-0.12	1.48	-0.20	-1.73	1.62	0.71	-0.72	1.21	0.19	2.21	1.24	0.02	1790
	1791	2.48	1.08	1.20	1.87	-0.18	-0.49	0.58	1.51	0.09	-0.29	-0.46	1.92	1791
	1792	0.98	-0.12	1.30	1.87	-0.18	0.21	0.08	0.11	-0.41	0.71	0.54	-0.08	1792
			150			1100								
	1793	-1.22	-0.02	0.40	-1.43	-0.38	0.01	1.78	-0.29	2.49	1.31	1.44	2.22	1793
	1794	2.28	3.08	2.00	2.37	-0.08	0.81	1.78	0.21	-1.11	-0.49	1.84	-0.38	1794
	1795	-3.72	-3.12	-0.20	1.37	1.52	-0.79	-1.42	0.91	0.49	1.71	-0.16	1.52	1795
	1796	2.48	1.18	-1.70	-0.13	-0.28	-0.29	-0.12	0.71	1.39	0.41	1.24	-1.38	1796
	1797	0.78	0.18	-1.40	0.67	1.22	-1.59	1.18	2.51	1.09	-0.59	0.94	1.32	1797
	The state of the s							17.79	Syles I	15 118	8 18		-	
	1798	1.78	2.08	0.20	0.27	0.72	-0.09	0.48	0.51	0.29	-0.39	-0.86	-2.08	1798
-	1799	-3.22	0.88	0.60	-1.23	-0.98	-1.49	-0.62	0.41	1.39	0.51	-0.96	-1.18	1799
	1800	1.78	4.58	-1.10	2.67	1.32	-1.59	0.38	-0.09	0.49	0.01	1.24	-0.08	1800
	EDIST A				100		0.0	98-97	Wildley.	NE CE	\$2.E		10 /A	
	1801	1.38	1.08	1.50	0.77		-0.39	-0.62	-0.79	0.49	0.61	0.04	0.02	1801
1	1802	0.18	1.18	0.70	0.87	-0.08	1.71	0.28	2.21	1.09	2.81	1.04	1.52	1802
	1803	2.38	-3.82	0.30	1.47	-0.88	1.11	0.78	1.11	-0.91	-0.49	0.54	0.22	1803
L														

#### LXXXI.

## NORTH ITALY. - MILAN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Reaum	ur.	- 16			Sulphasy	
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
100	0	0	0	0	0	0	0	0	0	0	0	0	200
1804	100	1200	-0.60	100000000000000000000000000000000000000	The last time of	127	1	-0.39	THE REAL PROPERTY.	The second second	The second second	-0.18	1804
1805	-0.12	-0.02		-2.03	-0.78	0.21		The state of the s	The state of	Warm I was	-2.36	1 59 1	1805
1806	0.18	1.68		-1.53		1.01	No.	Laboret 1	1323 May 11 C. 1	1007.55	1.34	David Santa	1806
1807	0.58	0.28	1000	-1.33	1.32	0.21	1.18	1.71	POSTABILI	1.71		-0.08	1807
1808	-1.02	-1.62	-3.80	-1.23	1.62	-0.49	1.98	-0.69	0.39	-2.39	0.24	-2.08	1808
1000	0.40	1 00	7 40	0.00	1 00	0.57	0.50	0.01	0.53	0.10	0.00	0.00	1000
1809	0.48	1.98		-2.63	1.02	0.51	10000	0.21	1177 60 1	-0.19 1.11	-0.96	1.82	1809
1810 1811	0.08	-0.72 $1.48$	1.70	-0.23	0.22 1.82		and the second	-0.79 $-0.49$	1	2.21	0.34		1810 1811
1812	-3.32	-0.32	01-71		0.92	-0.29 1.01	A STATE OF THE PARTY OF THE PAR	THE RESERVE OF THE PARTY OF THE	500000000000000000000000000000000000000	0.11	-2.96	1000	1812
1813	-0.12	1.08	0.50	OT SEC	1.52	-0.99	THE THE BALL	-1.09	100000	LOCAL SECTION AND ADDRESS OF THE PARTY OF TH	-0.56		1813
1010	-0.12	1.00	0.50	1.07	1.02	-0.99	-2.12	-1.09	_1.11	0.21	-0.50	1.52	1019
1814	-0.12	-4.42	-1.40	0.77	-1.98	_1 00	-0.12	_1 00	-1.91	-0.69	1.04	1.82	1814
1815	-2.02	La Contraction	1.90	CARL AND A	1.22		-1.22	S I SHEY	CHC 2 (4.2)	THE REST	-1.26		1815
1816	-0.52	THE THEFT	-1.20	The second of	-0.58	-0.49	Manage.	-3.69	100000000000000000000000000000000000000	0.41	4.60000000	-1.88	1816
1817	-2.52	2.08	0.30	1000		0.21	COLUMN	-0.59	The same of	-1.89	C. Library D.	-0.18	1817
1818	0.48	3.34	0.70	and the same	1000	0.26	0.53	HILL SA	1000 000	0.48		-0.39	1818
1010	0.10	0.01	0.10	0.01	0.00	0.20	0.00	0.10	0.20	9.1	2.10	0.00	2010
1819	0.00	0.73	1.48	1.35	-0.02	-0.53	0.32	-0.50	0.48	0.46	0.93	0.30	1819
1820	-0.79	0.58	-0.56	1.60	THE COLUMN	-0.48	1000000	1.76		-0.30		-0.03	1820
1821	0.80	-0.18	-0.52	0.59	231127	-2.20		0.43	1	-0.29	0.78	0.35	1821
1822	1.81	1.28	2.10	0.99	1.05	3.31	0.53	0.26	1	0.66	1.38		1822
1823	-1.92	-0.25	-0.37	-0.55		-0.78	-0.60	0.53		0.11	-1.37	0.01	1823
1020		0.10	11,00		north l	lint	Herr	0.00	funt	51.0	10.8	10.1	
1824	1.01	1.49	-0.40	-0.85	-0.16	-1.57	1.33	0.90	0.71	0.23	1.25	2.07	1824
1825	1.39	0.62	-2.38	1.21		0.32	0.05	0.53		-0.81	0.82	3.92	1825
1826	-2.18	0.44	0.76	-0.72	-1.23	-0.09	0.18	1.55	0.71	1.48	-0.56	1.16	1826
1827	0.36	-1.72	1.12	0.73	0.46	-1.26	1.20	-0.60	-1.06	1.37	-1.46	0.25	1827
1828	1.38	-0.36	1.49	0.64	0.45	1.27	1.38	0.19	0.47	0.38	-0.81	0.60	1828
Taxin / s	THE LA	10,000	Tarl:		TOE.	178		120	THE PARTY	The state		1200	
1829	-0.04	-2.79	0.05	0.05	-0.03	0.23	0.22	-1.15	-0.89	-0.40	-1.68	-1.90	1829
1830	-3.72	-3.45	1.66	2.66	0.66	-0.33	1.71	1.02	-0.79	-0.81	0.99	0.60	1830
1831	0.38	-0.51	0.73	0.19	-1.12	-0.56	0.12	-1.05	-1.08	1.77	0.24	1.34	1831
1832	0.41	0.52	-0.21	-0.68	-2.07	-1.27	0.03	0.49	-1.15	-0.47	-0.41	-1.71	1832
1833	-0.47	1.18	-0.59	-1.23	2.00	0.37	-2.28	-2.77	-3.20	-1.36	0.14	1.37	1833
11 10 076		101120		HAN.	SEL SE	Part of	F.E.	E STATE	100	Black.			
1834	0.17		-0.19		The same of		-0.23			-0.79			1834
1835	1.03	73.34.56.1	(C) (C) (S) (A) (A) (A)		10 to	COLUMN TO THE REAL PROPERTY.		THE PARTY	-2.01			TRACTOR	1835
1836	-2.51	The Late of the la	-0.05		SUBSCE		-0.97	No.		-0.65	-2.16	111111111	1836
1837	-0.83	AL ROYAL TOWN		-2.41	The same of the same of	0.500 0.00	-1.29	0.37	THE RESERVE TO SECTION AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS	-1.93	1.133533.1	1000000	1837
1838	-2.16	-2.39	-0.72	-2.74	-0.98	-0.75	-0.78	-1.55	-1.58	-1.74	0.08	-0.80	1838
Mocas	0.75	200	-	10.00	24.00		10.00	10.0	11.00	70.00	-	0.00	Morra
Means.	0.52	2.82	6.40	10.03	14.08	17.09	18.92	18.39	15.31	10.79	5.76	2.08	Means.
1 0 D	COL.	18 4	DE L	Then	05.0	734.1	78.0	100-1	in the	All de	PER EN	104	
					Top a	THE PERSON	Papin.	166	Birn				100
		de Es			JUL I	HER	100	1	113	THE PARTY OF	9(-5)		
E PROOF		To the	33.3	To had	Total Miles	Sol a	B.C.A.	18	SYRAN	A Fami		Jan Bar	
1000	Carlo Indi	1	100	21.6	Service	Hilliam	TANKA	HE I	Sings.	Taly Bu	PARTS.		10000

## LXXXII.

## SWITZERLAND. - GENEVA.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						De	egrees o	f Reaum	ur.	1	N. DOT			SEAN LE
	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1	Exist	0	0	0	0	0	0	0	0	0	0	0	0	05/01/2/03
	1768	-0.86	-0.01	-2.38	-0.14	-0.61	-1.71	-0.92	-1.25	-1.42	0.99	0.77	0.08	1768
	1769	0.92	0.16	-1.05	0.13	-0.71	-1.57	-1.11	-1.43	-0.89	-3.00	1.62	0.61	1769
0	1770	-1.25	-1.30	-1.72	-2.40	-1.20	-1.34	-2.97	-1.24	0.49	-0.81	0.35	0.42	1770
	1771	0.53	-0.67	0.17	-2.68	0.34	-1.84	0.07	-1.45	-0.57	-0.17	-1.80	1.66	1771
1	1772	0.61	2.57	1.76	-0.41	-2.23	0.35	-0.72	-0.47	0.52	1.34	1.29	1.16	1772
	7 880	1 45	104	1 10	1.10	1.04	0.00	9.00	1 -0	0.10	000	0.70	7.07	1911
	1773	1.47	-1.84	-1.18		-1.64	NO THAT		100	1237 1 1504	1000		21911	1773
	1774	1.22	0.91	2.38	DATE THE	-0.94		3-ACTS 1599	0.42	12/25/2009	-1.45	120 20 20 20 20 20 20 20 20 20 20 20 20 2	COMM	1774
	1775	0.89	1.89	0.99	146673-111	-1.90			0-42/07/09/00	-0.02	-0.24	1000 100	-0.68	1775
	1776	-1.78	1.92	1.85	100000	-1.96	1	0.20	101.50	-1.50	0.26	The Carlotte	-0.09	1776
	1777	-0.41	-0.76	2.46	-1.23	-1.51	-0.38	-1.12	0.45	-0.41	1.27	0.21	-1.72	1777
	1778	0.03	-0.93	0.86	0.78	-0.09	-0.76	1.59	0.68	-1.85	0.32	0.76	1.85	1778
	1779	-3.43	-0.28	-0.14	1.70	0.97	1 1 1	1003 1100	-0.45	0.48	1.77	0.57	2.70	1779
	1780	-1.48	113000	2.35	-0.86	0.97	1	1	1.16	0.14	0.51	-1.02	-1.25	1780
	1781	0.96	1.09	0.37	2.15	1.78	0.28	-1.17	0.30	0.76	-0.47	1.69	2.97	1781
	1782	2.22	-3.74	-0.53		-1.76	0.18	-1.10	-0.72		-1.06	A	-2.04	1782
		92 337		0.00	0.00	20	0.10	1.10	02	0.0.	1.00	1.00	2.01	1102
	1783	2.01	1.68	-0.27	-0.71	-0.06	-1.13	1.75	-0.94	0.17	0.93	0.81	1.03	1783
	1784	-1.06	-2.03	-0.43	-2.51	1.73	1.69	0.84	-1.62	1.40	-1.87	-0.76	-3.38	1784
	1785	0.58	-3.26	-6.75	-5.48	-0.19	0.30	-0.33	-1.75	0.94	-0.40	0.11	0.42	1785
	1786	0.41	0.08	-1.62	0.69	-0.25	1.92	-0.99	-1.22	-0.59	-1.71	-0.69	0.19	1786
	1787	-1.99	-1.15	1.76	-0.30	-1.98	0.79	-0.70	0.21	-0.27	0.41	0.72	2.83	1787
	m setting				99	(Anna)	1 2 1 1 2		10 to	E LET		1000	1500	
	1788	1.01	2.06	2.19	1.04	1.13	1.04	1.61	-0.45	0.71	-0.83	A District of	-4.48	1788
	1789	-1.17	1.12	-1.97	1.19	1.71	-1.25	-0.80	-0.19	-0.57	-0.59	-1.59	-0.17	1789
	1790	0.36	0.75	0.99	-0.73	1.52	0.94	-1.10	0.63		1.95	1.13	0.78	1790
	1791	2.40	0.04	-0.02	2.86	0.61	1.04	0.98	2.30	0.98	0.72	-1.37	1.30	1791
1	1792	1.22	-0.28	2.11	1.81	-0.12	1.14	1.03	0.83	-0.09	1.37	0.86	0.45	1792
	1793	-0.52	1.05	1.77	0.08	-0.05	0.20	3.12	2.49	-0.12	1.24	0.61	1 10	1500
	1794	0.14	2.21	1.91	3.26	0.76	1.10	2.11	0.39	-0.12	-0.28	0.86	1.19 -1.75	1793
	1795	-4.85	0.37	0.26	1.76	1.32	1.34	-0.73	1.34	1.54	1.92	-0.96		1794
	1796	1.25	0.72	-2.15	-0.06	0.60	0.60	0.37	0.80	1.61	0.41	-0.14	1.11 -1.92	1795 1796
	1797	0.11	-1.41	-1.08	1.49	2.14	-1.28	2.21	1.28	0.71	-0.08	0.71	1.61	1797
	1798	0.53	-1.17	-1.02	0.83	1.00	1.29	0.45	0.81	0.48	-0.29	0.44	-0.96	1798
	1799	-1.57	1.71	-0.16	-1.73	-1.70	-1.16	-0.13	0.67	0.40	-0.40	-0.54	-2.59	1799
	1800	1.64	0.06	-1.66	2.43	2.40	-0.83	1.48	0.82	0.96	-1.55	0.63	-0.27	1800
														1000
	Means.	-0.43	0.75	3.08	7.19	11.21	14.03	15.44	14.85	11.49	7.32	3.34	0.57	Means.
						E3013				Sec. 1				
-	1796	2.27	0.07	-2.14	-0.25	A DESCRIPTION OF THE PERSON NAMED IN COLUMN TWO IN COLUMN	-0.64	-1.10	0.16	0.70	0.08	THE RESERVE	-1.70	1796
	1797	0.45	-0.85		0.97	100	-2.03	1.27	0.71	-0.48	-0.26	0.47	1.58	1797
	1798	0.68	-0.25	E397	0.96	-0.22	0.32	-0.64	-0.14	0.12	-0.08		-1.36	1798
	1799	-1.44	1.93	-0.26	-1.60	124	-0.49	-0.46	0.33	0.19	-0.26	-1.24		1799
-	1800	2.06	0.03	-1.53	2.88	1.66	-0.97	1.62	0.70	0.41	-1.16	0.67	-0.32	1800
	1801	1.81	0.13	1.43	0.74	0.43	-0.26	0.42	0.15	0.90	0.84	0.67	0.95	1801
	1802	-3.98	-0.38	0.94	1.18	0.53	1.66	-0.12	2.68	1.72	2.51	0.63	0.58	1802
	1803	-0.26	-2.58	0.24	2.05	-1.42	0.89	2.20	2.25	-0.79	-0.57	1.04	1.88	1803
	1904	4.58	-1.58	-0.19	0.30	1.50	2.02	0.04	0.47	0.59	0.22	1.36	-0.59	1804
L														

#### LXXXII.

## SWITZERLAND. — GENEVA (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.   Jan.   Feb.   March.   April   May.   June.   July.   Aug.   Sept.   Oct.   Nov.   Dec.   Year.			W/OP			De	grees of	Reaumi	ur.			194.1		Y-URANII
1806   -0.41   -0.23   -0.41   -1.35   -1.22   -0.49   -0.41   -0.73   0.18   -1.45   -2.19   -1.64   1805   1806   -1.10   0.24   -2.65   -1.47   1.42   0.43   2.66   3.03   -0.88   1.42   0.39   -2.48   1806   1809   -0.49   -3.14   -2.55   -1.57   1.14   -1.33   0.70   0.059   -0.14   -2.40   -0.28   -2.99   1808   1809   -2.23   1.95   0.19   -3.68   -0.06   0.12   -0.43   -0.32   -1.00   -1.05   -1.76   0.70   1809   -1.01   -1.04   -1.04   -1.05   -1.15   -1.19   1810   -3.14   -3.34   3.08   -0.28   0.29   -0.45   -0.14   -0.23   -0.44   0.70   2.21   0.71   -0.85   1811   1812   -3.92   1.40   -0.02   -1.54   0.27   0.02   -0.37   -0.69   -0.43   0.13   -1.80   -2.74   1812   1813   -1.74   1.51   -0.69   0.53   0.54   -0.84   -2.10   -1.02   -1.74   -0.87   0.95   2.34   1813   -1.32   -3.92   -1.44   0.96   -1.74   -0.26   0.37   -0.66   -1.74   -0.87   0.95   2.34   1813   -1.32   -3.92   -1.44   0.96   -1.74   -0.26   0.37   -0.66   -1.74   -0.87   0.95   2.34   1813   -0.13   -1.33   2.54   -0.48   -0.54   -1.41   -2.40   -2.14   -0.47   0.59   -1.05   -0.02   1816   1816   -0.13   -1.33   2.54   -0.48   -0.54   -1.41   -2.40   -2.14   -0.47   0.59   -0.05   -0.02   1816   1818   0.54   0.69   0.13   -0.08   -1.26   0.66   1.41   -0.41   -0.39   -0.92   1.06   -0.26   1818   1819   1.86   0.98   0.82   1.00   -0.21   -0.19   0.07   -0.34   0.42   0.07   -0.40   0.95   1819   1820   0.01   0.54   -1.24   2.07   0.39   -0.59   -0.55   0.77   0.55   -0.07   0.69   1.60   -2.32   1823   1.98   -1.14   -1.46   -0.25   -0.42   0.77   -1.19   -1.54   -1.17   0.62   0.66   0.24   0.99   -0.29   1.60   -2.32   1823   1.98   -1.16   -0.25   -0.10   -0.65   0.26   -0.40   -0.11   0.88   0.30   0.54   2.76   1825   1822   -0.07   -0.55   -0.09   1.69   -0.65   0.26   -0.40   -0.11   0.88   0.30   0.54   2.76   1825   1822   -0.07   -0.55   -0.09   1.69   -0.65   0.26   -0.40   -0.11   0.88   0.30   0.54   2.76   1825   1822   -0.85   -0.66   0.45   -0.85   -0.66   0.26   -0.40   -0.11   0.88   0.30   0.54	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1806		0	0											
1807	1805	-0.41	-0.23	-0.41	-1.35	-1.22	-0.49	-0.41	-0.73	0.18	-1.45	-2.19	-1.64	1805
1808	1806	3.23	1.83	0.12	-1.80	1.33	1.66	0.08	-0.39	0.11	1.10	1.34	2.42	1806
1809	1807	-1.10	0.24	-2.65	-1.47	1.42	0.43	2.66	3.03	-0.58	1.42	0.39	-2.48	1807
1810	1808	-0.49	-3.14	-2.58	-1.87	1.14	-1.33	0.70	0.59	-0.14	-2.40	-0.28	-2.99	1808
1810	1809	2.23	1.95	0.19	-3.68	-0.06	0.12	-0.43	-0.32	-1.00	-1.05	-1.76	0.70	1809
1811			4.112						71					That I
1812	1810	-3.14	-3.34	3.08	-0.28	0.29	-0.45	-1.01	-0.70	1.37	1.26	1.05	1.19	1810
1813	1811	-2.22	1.98	1.46	1.34	1.23	1.82	1.53	-0.14	0.70	2.21	0.71	-0.85	
1814	1812	-3.92	1.40	-0.02	-1.54	0.27	0.02	-0.37	-0.69	-0.43	0.13	-1.80	-2.74	1812
1815	1813	-1.74	1.51	-0.69	0.53	0.54	-0.84	-2.10	-1.02	-1.14	0.78	-0.49	0.32	1813
1816	1814	-1.32	-3.92	-1.44	0.96	-1.74	-0.26	0.37	-0.66	-1.74	-0.87	0.95	2.34	1814
1816		73/45/5	14.0	10.08	10)		284119		0.70	100		100	0.00	-075
1817			No. 50 (60 (60))	* W. T.	200	100000	100000	ALCOHOL: N		THE RESERVE OF THE PERSON NAMED IN	ASSESSED FOR	DEPO-1		CONDIC
1818		1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	41/	N. ACRES	1000		TAY TO		The second second	774	75798742	95/97		
1819	100000000000000000000000000000000000000	(0176)	OC 104 Sept 7.	Tree last	15/427-30	(NAME   1000)	PROPERTY 15 10 12	St. July 1000	110//00	100000000000000000000000000000000000000	10.7000	F 7 W 3 10		10000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7 - 100	100	313 E F 63	7 7 7 7 7 7 7 7	PARSON	1000	10 10 10 10 31	The state of the s	The same of	THE RESERVE AND ADDRESS.		- V12-1	100.00	The second second
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1819	1.86	0.98	0.82	1.00	-0.21	-0.19	0.07	-0.34	0.42	0.07	-0.40	0.95	1819
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1820	0.10	0.54	-1.24	2.07	0.39	-0.59	-0.65	0.84	-1.93	-0.31	-2.16	0.02	1820
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	- 59756 22200	1200000	Up XIII m			1000	100	-0.04 TO	85140275	THE PARTY OF		100	1.0	C1232 WALL
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-4573 7.5 ()	1000000		0.000	23.2.3.11.		RESTORT 174	270 1/1 1/19	PT OF WALL	1000		1 6473	C364V7	1-1-1-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	AND DOUBLE OF THE	10000		T A01, T 113	1100-120	91027311		THEN	10/25/72/03	White Co.	1 5001	200.00	708715	The state of the s
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	THE RESERVE OF THE PARTY OF THE	8	The state of the s	997.85-1111	9099551	The second		1000			11 1000 11	1000000	2000	
Means.         -0.42         1.87         4.70         8.79         13.45         15.81         17.67         17.66         14.70         9.73         5.23         1.27         Means.           1826         -3.23         1.12         1.47         0.34         -1.04         -0.06         0.90         2.57         1.22         0.95         -1.19         0.03         1826           1827         1.49         -2.15         1.02         1.29         0.90         -0.07         1.95         0.66         0.24         0.99         -2.02         2.56         1827           1828         2.82         1.06         0.70         0.81         1.22         0.89         0.59         -0.80         0.96         0.62         0.94         1828           1829         -0.85         -0.63         0.10         0.25         -0.06         -0.83         0.15         -0.89         -0.71         -1.52         -1.28         -3.87         1829           1830         -4.14         -1.74         1.20         2.70         0.57         -0.49         0.53         -0.01         -0.94         -0.86         0.46         -0.99         1830           1831         -1.10         0.46	100000000000000000000000000000000000000		PARTY IN	ALC: NO INC.	445	100000	300000000000000000000000000000000000000	13.55	100000000000000000000000000000000000000	The second second	1. h a 2.00 C 2.00 C	2 375		1-1-30 MIN
1826         -3.23         1.12         1.47         0.34         -1.04         -0.06         0.90         2.57         1.22         0.95         -1.19         0.03         1826           1827         1.49         -2.15         1.02         1.29         0.90         -0.07         1.95         0.66         0.24         0.99         -2.02         2.56         1827           1828         2.82         1.06         0.70         0.81         1.22         0.89         0.59         -0.80         0.86         0.96         0.62         0.94         1828           1829         -0.85         -0.63         0.10         0.25         -0.06         -0.83         0.15         -0.89         -0.71         -1.52         -1.28         -3.87         1829           1830         -4.14         -1.74         1.20         2.70         0.57         -0.49         0.53         -0.01         -0.86         0.46         -0.90         1830           1831         -1.10         0.46         1.67         1.54         0.53         -0.11         -0.02         -0.29         2.16         0.58         0.90         1831           1832         0.10         0.36         -0.55														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Means.	-0.42	1.87	4.70	8.79	13.45	15.81	17.67	17.66	14.70	9.73	5.23	1.27	Means.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	este title		BIBS.		MARIE .		E.A.				40-4	male	10.11	ALCOY.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		-3.23		TU 70 KL 1 SH				0.90	10.010.01		THE PARTY OF	111341.53	1.0	- 15 Ten 1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	100000000	1.49	-2.15	1.02	1.29	0.90	-0.07	1.95	Man Daniel	0.24	0.99	-2.02		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	70.00	2.82	1.06	0.70	0.81	1.22	0.89	0.59	ARREST TO S	0.86	0.96	NO. OF STREET		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1829	-0.85	-0.63	0.10	0.25	-0.06	-0.83	0.15	-0.89	-0.71	-1.52	-1.28	-3.87	1829
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1830	-4.14	-1.74	1.20	2.70	0.57	-0.49	0.53	-0.01	-0.94	-0.86	0.46	-0.90	1830
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1831	-1.10	0.46	1.67	1.54	0.53	-0.11	-0.02	-0.02	-0.29	2.16	0.58	0.90	1831
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	THE RESERVE AND	100000000000000000000000000000000000000	M. THE LAND					100		14	ALCOHOLD TO	111120000		ALC: NO SECURE AND ADDRESS OF THE PARTY OF T
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Charles and Control	Marie Control	And the second	Street in	1	Mary Thomas		And the second	Defendance of	A. V. W. V.		Walley VI		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	The state of the s	100	Marie III	DO. NO.	A PERSON NAMED IN	the result.		The state of the	125.00		and the second	ALCOHOLD IN	CO	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	The second second	the same	307,05111		12.5 THE R. P. LEWIS CO., LANSING	and the same of the same of	Section and the second		The second			4		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	MARKET !	2011-0		PLY by	All Black	BOOK	300	State of	0.418	1000	Milkey.	and sea	06,45	Mary 13
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	100000000000000000000000000000000000000					100000		A CHARLES	4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	100	OF SECTION	PANTAGE AND		The state of the state of the
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	THE REAL PROPERTY.	Marie Salar	Service 15	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10000	12 70 0	100 Pe 17 1	the same of the same	100 100 10	LOWER		STOCK HAR	L. Griss	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	The second second second	The same of	BOOK ALCOHOL	12.00	to the United			40.00	ALC: NO STATE OF	Address of the	The same of			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Lanca Control		LOCAL TA		The same of the		The second second		Editor Co			CO DO NO		
1842     -5.18     -2.84     0.56     -0.58     0.02     1.00     -0.19     0.78     -1.08     -2.18     -1.03     -0.71     1842       1843     1.50     2.22     -0.34     0.27     -1.60     -2.56     -2.35     -0.73     0.60     -0.24     0.25     -0.83     1843       1844	1840	2.60	0.02	-3.22	0.71	-0.10	-0.37	-2.32	-0.01	-0.56	-1.74	1.43	-3.14	1840
1842     -5.18     -2.84     0.56     -0.58     0.02     1.00     -0.19     0.78     -1.08     -2.18     -1.03     -0.71     1842       1843     1.50     2.22     -0.34     0.27     -1.60     -2.56     -2.35     -0.73     0.60     -0.24     0.25     -0.83     1843       1844	1841	0.45	-0.25	0.77	-0.69	1.82	-1.71	-1.98	-1.37	0.09	0.90	0.26	0.89	1841
1843     1.50     2.22     -0.34     0.27     -1.60     -2.56     -2.35     -0.73     0.60     -0.24     0.25     -0.83     1843       1844	1	1	-2.84		The state of the s	130 72 50	C)-43F CE	Co page 1	C. Same		-	1 10 10 10		CONTRACTOR OF STREET
1844	1843	1.50	2.22	-0.34	0.27	-1.60	The same of the same of	1	-0.73	0.60	-0.24	0.25		1843
1845 1.70 -3.33 -1.77 0.49 -1.98 0.47 0.06 -1.53 1.10 0.40 1.54 1.74 1845	CONTRACTOR OF THE PARTY OF THE		No. of Contract of	No.	100000	Maria Santa	N7 17 57 6	100000000000000000000000000000000000000		1000	1 - 100 miles	The same of		
		1.70		-1.77	0.49	-1.98	0.47			1.10	- NO.		1.74	
Means.   -0.72   0.98   4.16   7.03   10.77   13.61   14.96   14.58   11.84   7.98   3.98   1.30   Means.	White I	-			201	2 (1-2)			-		-	-		
	Means.	-0.72	0.98	4.16	7.03	10.77	13.61	14.96	14.58	11.84	7.98	3.98	1.30	Means.

#### LXXXIII.

# South Germany. - Vienna.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

	- 80V		district			De	grees of	Reaum	ur.	1				1000
Y	ear.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
		0	0	0	0	0	0	0	0	0	0	0	0	
1	775	-1.43	1.86	1.21	-2.35	-2.77	1.32	-0.41	1.29	0.84	0.26	0.29	-1.09	1775
1	776	-4.30	0.57	0.70	-1.11	-2.30	-0.42	-0.24	0.25	-1.42	-1.53	-1.32	-2.19	1776
1	777	-1.79	-1.24	0.32	-2.93	-0.22	-0.10	-1.17	0.57	-1.38	-0.53	0.35	-1.00	1777
1	778	1.92	-1.04	0.18	1.89	0.04	-0.43	1.18	0.95	-0.89	-0.54	0.87	3.61	1778
1	779	-1.75	3.15	2.27	3.05	1.24	-1.32	-1.35	-0.07	0.65	1.00	0.43	3.01	1779
1	780	-1.68	3.04	2.73	-1.38	-0.18	-0.92	-0.70	-0.48	-1.08	0.51	0.19	-1.99	1780
11	781	-0.87	0.05	0.77	0.86	0.25	1.44	-0.06	2.31	1.40	-0.45	1.84	0.34	1781
11	782	2.72	-2.63	0.60	-0.06	0.54	1.82	2.74	0.85	0.86	-0.76	-1.50	0.62	1782
11	783	3.59	4.12	-0.08	0.65	1.81	1.94	1.66	1.81	2.12	1.59	0.58	-2.56	1783
	784	-3.51	-1.87	-0.42	-1.36	1.69	0.86	0.47	0.49	1.98	-2.56	0.70	0.03	1784
		0.00	0.00	F (9)	204	0.67	1.48	_0.00	0.00	2.11	-0.55	0.41	0.17	1505
11	785	-0.73	-0.93	-5.63	-3.04		-1.47	-0.83	-0.86	-0.92	-2.11	-2.12	S. Co., 2011	1785
11	786	0.52	0.16	-0.04	1.84	LINES	0.25	-1.54	-1.85		1.10	0.93	0.60	1786
11	787	-0.39	1.47	0.65	-1.46	S STORES	1.11	-0.40	0.35	-0.78	-0.29	-1.39	2.82	1787
11	788	2.22	0.17	0.81	1000000	-0.36	1.18	2.28	-1.72 $-0.60$	1.00	0.77	0.73	-6.79	1788
1	789	-0.49	2.00	-2.43	1.19	2.15	-0.49	0.40	-0.60	0.37	0.77	0.73	0.21	1789
17	790	0.86	2.87	0.31	-1.11	1.20	1.56	-1.10	0.31	-0.83	-0.76	-0.43	2.09	1790
17	791	4.29	1.01	1.63	1.33	-0.44	-0.33	-0.37	0.67	-0.84	-0.40	-0.46	0.89	1791
17	792	0.56	-1.24	0.47	0.38	-0.96	0.62	0.38	0.26	-0.93	-1.11	-0.24	0.56	1792
17	793	-1.55	1.27	-1.00	-2.40	-1.23	-1.08	1.81	1.86	-0.07	1.13	0.64	1.99	1793
17	794	2.24	2.99	1.95	3.74	1.35	1.55	2.92	-0.75	-1.38	-0.19	0.33	-0.95	1794
1	795	-4.94	-1.29	0.23	1.81	-0.05	1.44	-1.95	0.31	-0.17	2.75	-1.00	2.28	1795
100	796	5.23	1.32	-2.73	-1.52	0.48	-0.04	0.14	0.58	1.96	0.84	-0.14	-1.48	1796
11	797	1.58	1.02	-0.71	2.10	2.94	0.68	1.95	2.17	2.01	1.23	0.54	1.11	1797
11	798	1.96	2.83	1.40	0.65	0.26	0.84	0.14	1.29	1.62	-0.47	-0.68	-3.68	1798
1	799	-5.34	-2.08	-0.83	-0.43	-0.45	-1.16	-0.58	1.00		0.45	0.58	-2.94	1799
		-		20,00	42.2	July 1	PER S	F(1,0)-	9030	COLLE	27.51	PACKET AND A SECOND	1.1	12.0
11	300	0.74	-0.19	-3.31	5.57	1.90	-1.45	-0.44	1.49	0.27	-0.40	1.57	0.10	1800
11	801	1.85	-0.21	2.47	0.80	1.83	1000	-1.18	-1.32	1.37	1.94	1.71	0.99	1801
11	802	-0.43	-1.34	0.89	0.73	-1.14	1.33	1.02	1.65	0.38	2.10	1.84	1.40	1802
11	803	-2.68	-3.46	-0.50	2.49	-1.59	-0.75	0.23	0.08	-2.12	-0.45	1.24	0.27	1803
1	804	3.42	-0.59	-2.44	0.05	0.29	-0.10	0.25	-0.51	0.80	0.48	-2.47	-2.40	1804
1	805	-0.48	-1.18	-1.28	-2.16	-1.85	-0.79	-1.26	-1.61	-0.04	-2.89	-2.19	0.24	1805
1	806	4.04	2.12	1.07	-2.07	1.84	-0.02	-0.16	-0.62	0.56	-0.80	1.60	3.48	1806
1	807	1.08	1.96	-1.54	-1.18	1.23	-0.34	1.25	4.74	0.17	1.37	1.96	0.46	1807
1	808	1.20	-0.51	-4.99	-1.20	1.42	0.15	1.30	1.80	1.13	-0.97	-0.32	-3.68	1808
1	809	-0.08	1.54	-1.13	-2.51	0.89	0.27	0.23	0.79	0.11	-1.31	-0.75	1.67	1809
1	810	-0.71	-0.03	2.03	-0.74	0.50	-1.65	0.82	0.15	2.26	-0.18	-0.09	2.01	1810
11	811	-3.58	-0.91	2.08	0.75	3.12	4.62	2.56	0.99	0.42	3.63	1.20	0.19	1811
11	812	-2.13	0.53	0.67		0.65		C 1 45 C	-	100000	The state of		1	1812
11	813	-1.84	2.07	-0.76	A STATE OF	0.36			1000	1	Marine Town	-0.24	0.68	1813
	814	-0.34	1000	-0.55	1	100000	1	0.66	The second	10000000	1	0.32	2.19	1814
1	815	-1.03	2.39	2.06	0.10	0.52	C.C.	-1.51	-1.29	-1.20	0.06	-1.07	-2.87	1815
11	816	1.84						100	-1.39	100 m 100 00	100000	-0.39	111111111111111111111111111111111111111	1816
11	817	3.24	1000			1.100	1400	17 61	-0.25	1000	MI K	1.09	W 1960 185	1817
11	1818	2.77				1000		100000000000000000000000000000000000000	1	0.41	0.84	0.60	1	1818
11	1819	1.22						1	-0.35		-0.12	0.51	The second second	Contract of
		11	,		1		1	1	1					

#### LXXXIII.

## South Germany. - Vienna (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

	March 1968	100-11		500 E	De	grees of	Reaum	ur.			7		
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1820	-2.47	0.36	-0.86	1.78	1.97		-0.96		1	0.16		-1.49	1820
1821	2.22	-1.56	-0.72	1.57	-0.81	-3.08	1000		0.51	-0.12	1.93	2.90	1821
1822	2.85	1.63	3.44	1.05	1.21	1.50	STATE OF THE STATE OF	-0.27	0.06	2.12	0.44	-0.27	1822
1823	-4.55	0.68	0.80	-0.29	0.42	The same		0.15	0.36	1.13	0.29	1.35	1823
1824	1.77	2.31	0.09	-0.72	-0.74	-0.60	-0.22	-0.53	1.36	0.60	1.56	4.00	1824
1825	3.15	0.50	-1.59	1.02	-0.14	-0.31	-0.72	-0.47	-0.62	-1.71	1.74	3.11	1825
1826	-3.65	-2.12	0.91	-0.12	-2.42	10100	1.34	2.06	0.69	0.89	-0.32	1.78	1826
1827	0.69	-2.92	1.61	1.65	1.33	1.19	1.67		-0.57	0.82	-3.48	0.83	1827
1828	0.19	-2.22	0.88	1.30	-0.16	0.21	0.00000	-1.49	100	-0.82	0.48	1.57	1828
1829	-1.66	-3.79	-1.87	-0.23	-2.26	-2.69	-0.32	-2.62	-0.31	-2.12	-3.62	-6.11	1829
1000	- 07	0.00		Villa I	0.00	and the same	20.00	0.01	- 01	- 00	0.00	-	1000
1830	-5.31	-3.23	-0.44	0.94	All the first state of	0.33	0.02	THE	-1.81	-1.68	0.76	1.13	1830
1831	-1.42	0.26	0.43	2.23	-0.90	CARROL .	0.33	-1.01	MEL AND ST	2.02	till a live	-0.04	1831
1832 1833	0.55	0.61	0.04	-0.16	-1.90	11,000	-1.29	0.32		0.04		-1.36	1832
1834	-3.35	2.33	0.24	-1.40	2.57	1.20	-2.26	-2.80	-1.22	-0.55	0.23	4.03	1833 1834
1094	4.67	0.32	-0.29	-1.17	2.24	1.65	2.61	1.26	2.85	-0.08	-0.89	1.25	1004
1835	1.71	1.46	0.46	-1.10	0.27	-0.07	0.92	0.19	0.09	-0.76	-3.77	-1.39	1835
1836	-0.08	0.29	3.84	0.00	-2.95	0.30	-0.48	-0.78	-0.89	0.91	-1.00	2.44	1836
1837	0.20	<b>-2.</b> 39	-1.96	-1.18	-2.57	-1.38	-2.96	0.84	-2.22	-0.82	-0.74	-0.95	1837
1838	-5.10	-4.14	-0.50	-2.44	-0.76	-0.74	-1.39	-2.29	-0.03	-1.75	-0.65	-0.84	1838
1839	1.12	0.73	-2.31	-3.85	-2.04	1.06	0.36		0.23	1.05	1.55	0.70	1839
1840	1.03	-0.88	-3.76	-0.55	-1.59	-1.05	-1.56	-1.94	-0.11	-2.03	2.09	-7.72	1840
1841	0.33	-3.24	0.65	0.93	2.19	-1.02	0.55	-1.10	0.24	2.04	0.28	2.27	1841
Means.	-1.22	0.63	3.85	8.66	13.31	15.72	17.14	16.77	13.25	8.51	3.67	0.39	Means.
			LXX	XIV.	Sour	тн С	ERMAI	му. —	RATI	SBON.			
1773	3.00	-0.28	-0.04	-0.28	0.25	0.34	-1.23	-0.60	0.47	1.20	1.06	2.35	1773
1774	1.63	0.85	2.17	1.97	-0.10	-0.17	-1.11	17.1	-1.29	-0.63	-2.98	-2.32	1774
1775	0.67	2.87	1.13	-2.41	-3.42	HALL THE	-1.91		-0.73	-2.19	-0.14	-0.64	1775
1776	-3.04	1.19											1776
THE BE 1				1)1 0		10	200	0.1			4.2	200	
1777	-1.47	-0.68	2.37	-1.29	-0.16	0.28	-1.02	1.24	0.01	1.07	1.31	-1.17	1777
1778	1.88	0.21	0.89	1.98	1.76	0.81	3.20	2.38	-1.33	-0.36	1.36	3.06	1778
1779 1780	-2.51	1.43	2.27	2.89	1.88	-0.34 1.30	-0.38 $0.64$	0.95 1.65	1.40 1.32	2.18 1.25	1.47 0.25	3.74 -0.75	1779 1780
1780	-0.83	-1.52	2.87 1.52	-0.92 1.88	0.87	1.52	0.64	2.36	2.45	-1.03	0.25	0.56	1780
	240			70.0	The state of	24	divisi.	3 7			111-11-3	TO BOTT	STATE OF
1782	2.46	-2.93	3.32	3.15	3.74	1.92	2.02	-0.28	0.80	-1.67	-2.72	-0.32	1782
1783	3.48	2.22	-0.95	0.26	0.93	0.92	1.73	0.45	0.13	1.00	EX. 25	-2.38	1783
1784	-4.07	-3.45	-1.69	-2.76	1.67	0.60	0.23	0.34	2.21	-2.46	0.36	-1.21	1784
1785	-1.20	-2.85	-6.49	-4.37	-1.08	-0.83	-1.42	-1.91	2.05	-0.77	0.28	0.10	1785
1786	0.66	0.04	-2.05	1.32	-1.54	1.28	-2.31	-1.85	-1.30	-1.93	-2.68	-0.18	1786
1787	-1.03	4.29	0.75	-1.53	-2.51	0.92	-1.31	0.36	0.07	1.78	0.89	2.06	1787
1788	1.86	-0.61	-0.30	-0.59	-0.35	0.88	1.66	-1.53	1.44	-0.20	-2.14	-8.30	1788
1789	-1.93	1.41	-2.90	0.64	1.62		-0.29	-0.28	-0.53	0.27	0.25	0.64	1789
1790	1.99	1.73	0.91	-1.21	1.20	1.42	-1.49	-0.08	-0.87	-0.37	-0.26	0.89	1790
1791	3.24	0.14	1.00	1.81	-0.76	-0.35	-0.35	1.14	-0.15	0.50	-2.43	0.84	1791
<u></u>													

## LXXXIV.

# South Germany. — Ratisbon (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

The same of			1000	- 10 -	De	grees of	reaum	uı.		W. In Inc.			
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1792	-0.57	-0.21	° 1.41	° 1.17	° -1.12	° 0.87	0.66	0.88	- -1.01	° 0.05	° 0.17	0.89	1792
1793	-1.17	1.26	0.53		0.0	-0.76	1.56	TO DESCRIPTION OF THE PERSON O	-0.47	1.87	10000	1.26	1793
1794	2.30		3.05	3.04	C 51 65	1.69	2.85	YALL DIN	-1.00	1.24		-0.78	1794
1795	-5.05			1795	-0.82	1.39	-2.22	0.29	1.08	3.11		2.26	1795
1796	4.26	1.59	-1.63	-0.77	C 2011	0.05	0.47	0.93	2.24	0.28	TENNIS P	-2.04	1796
1797	1.46	1.52	-0.17	2.09	CONTRACTOR OF THE PARTY OF THE	-0.72	2.14	1.73	0.75	0.06		1.59	1797
1798	1.88	1.94	0.18	1.02	0.66	1000	0.50	1.26	1.08		1 65	-2.69	1798
1799	-5.61	0.14		-1.87	9 1	-0.83		-2.86	-0.60				1799
1800	1.15	-0.63		4.66	CHECK !	-1.42	0.32	1.53	0.43	-0.69	1.30	0.63	1800
1801	2.72	0.10	10.76	0.76	16.5	-0.75	SUPPLY	0.13	1.15	1.60	- 10.3	0.81	1801
1802	-3.20	SCHOOL STREET	1	0.62	0.16	1.66	-0.04	2.80	0.73	2.40		0.71	1802
1803		The second second	-0.06		The second	1000	1.70	1.31	-0.96	- 7 - 1	1 1 1 1 1 1	0.93	1803
1804		20 C 15 C	-1.18	1000	1.17	0.88	0.29	-0.14	1.27	1.09		-738.0	1804
1805	-1.41		-0.34	Call of the 1	-1.76		-0.88	-1.60	0.74	-2.03		-0.21	1805
1806	4.22	2.45	13 mas	-2.24	2.47	Section 1	-0.49	0.15	0.86	0.04	100 110	3.58	1806
1807	1.19		-1.17		1.24	0.46	2.87	4.63	-0.94	1.58		1.54	1807
1808	1.08	3/7.534-	-2.79		100 TO 10	-0.45	1.61	1.19	0.33	THE REAL PROPERTY.	-0.23		1808
1809	0.33		-0.40	THE THE	0.71	Drait California	0.02	0.23	-0.31	-0.76		0.93	1809
1810	-1.72		1000	-0.63	- N. L	-1.00		0.17	2.72	0.52		1.89	1810
1811	-2.93	-0.16	2.09	1.48	2.23	2.85	1.75	0.24	0.43	2.24		-0.25	1811
1812	-1.33	1.05		CIL	1000	-1.15	A 100				-1.99		1812
1813	-3.03	0.99	111111111111111111111111111111111111111	,		-1.86	1777977	CONTRACT L		0.00			1813
1814	-1.37	-4.71	-2.93			-2.39							1814
1815	-1.30	1.05	1.18			-0.74	1000	10000		100000000000000000000000000000000000000			1815
1816	1.36	-1.83			COST.	-2.21		The state of	45.070	COLUMN TO	-1.49	-	1816
1817	2.51		-1.14	100000	1000000	Condition to the last	-1.79	3-43673		-3.22		-0.70	1817
1818	2.08	10000	-0.16	100 Per 1	1842-1	-0.02			23.003	-0.71	4	-2.08	1818
1819	1.49	0.60		THE REAL PROPERTY.	-0.76	0.529 July 1	-0.05	0.000	THE PASSING				1819
1820	-2.43	2000	-2.26		1200.000	-2.89		1000		-1.22	1	-1.66	1820
1821	1.17	-3.06	-1.51	0.99	-2.48	CONTRACT OF	OF REAL PROPERTY.	-1.18	-0.06	THE REAL PROPERTY.	Control of	2.53	1821
1822	2.21	0.63		0.26	Contract of			-0.87	1100	0.73	ALC: UNITED BY	-2.29	1822
1823	-4.17	0.86		-1.72	150 TEE T	-0.97	100000		10000000	0.02	WE 28 CO	1.05	1823
1824	0.92	0.38			1000000	1	-0.14	F 4 1 7 7 1 1 3	100	10000	1 1 1 1 1 1	1000	1824
1825	2.80	0.39	CONTRACTOR OF	1000000	0.93	1000	0.51	0.32	1.31	0.21	3.09	1 1 1 1 1 1	1825
1826	-3.57	-0.34	1.39	0.17	-1.04	1.05	1.99	3.61	1.61	1.38	00.034		1826
1827	0.09	100	1.00	1.31	1.20	1.05		-0.57	0.93	1.35			1827
1828	2.12		No. of the last	0.31	2 170	TO THE T	111.9.5	-2.47	111111111111111111111111111111111111111	100 Table 1	1 3 3 4 4	2.28	1828
1829	The state of the	-3.13	1	100000	-1.14	N 200 15 1	THE STATE OF THE S	-2.37	The STREET STREET	The Report of	PARTY AND ADDRESS OF THE PARTY AND ADDRESS OF	TO 14 1992	1829
1830	The state of the s	-3.61		1000	C. C. Diversit	-0.94	TOTAL AND	-1.28	17.77	P. Lander	G1755/110	-0.58	1830
1831	1991	-0.82	Prince	THE SALE	-0.48	-1.36	10000	COLUMN TO SERVICE	-58913V	2.40	Post and	0.26	1831
1832	0.77		1	1		1					-0.71	0.25	1832
1833	-3.05	HILLES	The second second	2000	2.29			-3.06	-2.01	-0.90	100000	3.95	1833
1834	5.52	-0.43	-0.25	-1.69	0.99	0.44	4.89	2.48	1.21	0.50	0.74	1.36	1834
Means.	-2.42	-0.09	3.09	7.55	11.94	13.72	14.88	14.62	11.69	7.11	2.22	-0.71	Means.
01/10	T	he numi	bers with	out sign	must b	e subtra	cted: th	ose with	the sig	n — mu	st be ado	led.	1

#### LXXXV.

## South Germany. - Stuttgard.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

			2-4			De	grees of	Reaumi	ur.			100		
Y	ear.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
		0	0	0	0	0	0	0	0	0	0	0	0	
1	792	0.64	-1.23	1.78	1.36	-1.12	-0.30	1.04	1.70	-0.70	1.30	-0.73	0.44	1792
1	793	-1.41	1.64	0.37	-1.36	-1.24	-0.31	2.52	1.84	-0.84	1.71	0.66	2.10	1793
1	794	2.02	3.72	2.76	3.26	0.41	1.30	2.75	0.12	-1.34	0.32	0.85	-1.72	1794
1	795	-4.88	0.36	0.65	2.81	0.64	1.43	-1.01	1.33	1.93	3.69	-0.49	3.76	1795
1	796	6.17	1.90	-2.51	-0.67	-0.32	0.10	-0.36	0.23	2.34	0.13	-0.87	-2.18	1796
-	1 44	11.6		72.3			A STATE	20						
-													- 00	
11	797	2.46	0.08		1.88		-1.30	2.86	1.01	1.04	0.36	1.82	PERSON TO	1797
11	798	0.65	1.44	0.69	1.16	0.66	1.21	0.14	0.66	1.36	0.53	0.33		1798
11	799	-3.46	1.77		-1.30			-0.98	0.32		1000	0.42		1799
-	800	3.03	-0.92	1000	4.56	1	-1.81	0.00	0.79	0.84	-0.37	1.61		1800
13	801	3.95	0.97	1.98	0.24	0.94	-0.54	0.91	1.42	2.32	2.89	1.30	1.46	1801
1			La Di											
1	802	-2.55	-0.02	0.80	2.13	0.23	1.53	-0.24	2.22	0.62	2.08	0.81	1.41	1802
11	803	-0.81	10000 221	100	1.49	-2.28	0.05	1.21	1.28	-	-0.90	0.46	1.36	1803
11	804		-0.98		-0.22	0.78		-0.35		100000000	0.74	0.56	-1.56	1804
11	805	A THE REST	-0.28	-0.60	100000000000000000000000000000000000000		-1.35		-1.44	Service and	-2.73	-2.47	0.06	1805
	806	-2.78	2.77	and the last	-1.99	Colombia Colombia	-0.27	W11.5	-0.59	-	0.03	1.67	4.85	1806
1	000	2.10	4.11	1.10	1.00	1.07	-0.21	-0.02	-0.00	-0.27	0.00	1.07	4.00	1000
	475 B	0.00	NO.	O.P.	Manage S	10,000	Lear h	836.0	is raily	P2-31-31			Mark A	
1	807	0.76	1.58	-2.43	-1.14	-1.02	-0.21	2.15	3.23	-0.74	1.71	1.37	-0.94	1807
1	808	1.95	-1.23	-3.55	-1.35	1.96	-0.98	0.54	0.77	-0.34	-1.49	-0.17	-4.02	1808
1	809	1.56	3.64	0.69	-2.58	0.84	-0.65	-0.36	0.16	0.30	-1.05	-1.65	2.12	1809
1	810	-1.56	-2.45	2.11	-4.12	-0.25	-0.95	-0.26	-0.48	2.08	0.09	1.44	0.97	1810
1	811	-3.01	0.49	2.31	0.97	1.41	1.41	0.75	-0.38	-0.04	3.02	1.28	-0.04	1811
		3/73							17.41					The one
	010	-2.36	1.00	-0.23	-3.17	0.64	0.00	1 05	1 17	-0.49	0.01	-2.28	4.01	1812
11	812	-2.30 $-2.25$	Marie Control	-0.23	0.53	1000	-1.45				THE RESERVE			1813
11	813	-2.25 $-1.96$		-3.67	1.09			No decided		-1.56	Contract to	0.69		1813
1	814	-1.90 $-1.92$	2000	St. Sand	0.39	1 2 2	-1.52 $-0.42$			ALC: NO.	1000	-2.30	- No. 197	1814
11	815	0.69	1.26 $-2.37$	-0.60			-0.42 $-2.63$				-0.17			1816
1	816	0.09	-2.37	-0.00	-0.00	-2.22	-2.05	-2.49	-2.34	-0.00	-0.17	-2.40	-0.82	1010
		118-3	SP D		-0-91		181	-		14-11				
1	817	3.31	1.47	-0.71	-3.71	-1.78	0.92	-1.54	-0.97	1.08	-3.25	1.01	-0.49	1817
1	818	2.67	0.40	0.41	1.33	-0.82	1.06	0.15	-0.91	-0.70	-0.91	1.62	-2.04	1818
1	819	-0.61	1.54	0.89	1.21	0.29	0.36	1.02	0.36	-0.92	-0.02	-0.95	1.16	1819
1	820	-1.64	-0.06	-2.16	1.31	-0.05	-1.91	-1.37	1.10	-1.84	-1.11	-2.81	-0.66	1820
1	821	2.13	-2.72	0.19	1.52	-1.98	-2.26	-1.97	0.15	0.77	-0.62	2.42	3.25	1821
	14/9		Sin I	No. 1		N. S.	10.74							
1	999	2.11	1.58	2.61	0 57	1.43	2.90	0.00	-0.85	_0.40	1 00	1.00	9.00	1000
11	822	Andrew Alle			0.51		A STATE OF THE PARTY OF			2011	1.33	1.82		1822
11	823	-2.76 $0.79$	1.25 0.79	100000	100 T Prof. 100 B	0.92	Control of the Control	-1.19	0.25 -0.39	-0.38 $0.68$	-1.03	-1.37	1.70	1823
11	824	1.92	-0.37	-0.89	1.85	0.27	-0.98 $0.26$	0.30	0.02	0.00	0.44 -0.64	2.52	3.81	1824
11	825 826	-4.81	1.06	1.16	0.19	10000	0.26	1.70	1.78	1.51	12 60 00	1.27 -1.07	2.74	1825
1	040	-4.01	1.00	1.10	0.19	-0.93	0.54	1.70	1.10	1.51	1.43	-1.07	0.54	1826
		TO SE	1	100						STA SE	THOU !	and the	C. C.	PER S
1	827	-0.49	-5.36	1.47	1.22	1.60	0.23	1.10	-0.45	0.08	0.67	-2.41	2.98	1827
1	828	3.10	-0.35	0.61	0.54	0.43	0.97	1.02	-1.10	0.07	-0.61	-0.17	1.19	1828
1	829	-2.45	-3.10	-0.58	0.46	-0.36	-0.61	0.45	-1.13	-1.50	-1.66	-2.88	-5.91	1829
1		-		-		-								

#### LXXXV.

#### South Germany. - Stuttgard (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1830	° -6.40	° -3.47	° 1.62	2.06	0.90	-0.38	0 1.05	0.00	0	0.89	0.90	0,74	1830
1831	-0.73		1.68			-0.09		-0.10	100			1.26	1831
1832	0.10		-0.64		1000	-0.59				-0.78		0.05	1832
1833	-2.56		-0.99	200					-1.35	-1.03	-0.13	177	1833
1834	5.05		-0.60	-1.87	2.16	1.33	2.74	0.90	1.73	-0.06	0.12	-0.27	1834
			10-1										1 XXI =
1835	1.53	1.20	-0.15	-0.90	-0.53	0.28	1.62	-0.21	0.60	-1.20	-3.22	-2.85	1835
1836		-1.27			-2.14		2000	0.46	-1.21		-0.01	1.04	1836
1837	0.90	111111111111111111111111111111111111111	-2.68	-2.84	-2.23	1.16	-1.19	C. C	-1.94	-0.60	-0.40	0.04	1837
1838	-4.43	-2.08	0.21	-2.32	-0.45	-0.03	-0.36	-0.90	0.64	-0.36	1.03	-1.34	1838
1839	0.78	-0.03	-1.31	-2.71	-1.07		7,000	-1.55	77.000	0.84	1.07	1.95	1839
											Teal		
1840	1.82	0.15	-2.90	1.36	0.29	0.16	-1.42	-0.23	-0.26	-2.39	1.10	-5.61	1840
1841		-1.98	2.09				1	-0.69					1841
1842	-1.50	-1.05	Annual London	-0.47	20.000	1.74		100			-1.82		1842
1843	2.07	1.54	0.15			-1.48			-0.15			0.23	1843
1844	0.31	-0.91	-0.30	N. 2. LO. 1	-1.01	75.5		-2.17	0.56	0.39	0.91	-3.18	1844
				-					-				
Means.	-0.80	1.64	3.97	7.80	11.87	14.03	15.48	15.02	12.05	8.05	4.11	1.25	Means.

#### LXXXVI. South Germany - Carlsruhe.

						Tron,	17.4	177		77 66	150.0		
1779	-3.98	1.18	1.26	2.19	1.14	-0.64	0.80	1.72	2.40	2.75	1.71	2.94	1779
1780	-2.23	-2.20	3.27	-1.17	0.52	0.41	0.27	1.39	0.18	0.83	0.00	-1.32	1780
1781	0.45	1.82	0.99	2.26	0.87	1.63	0.63	1.20	1.11	-0.94	-0.38	1.09	1781
1782	3.13	-3.95	-0.67	-1.10	-1.44	0.93	1.00	-1.62	-1.69	-2.08	-3.90	-1.07	1782
1783	3.33	1.35	-1.60	0.05	-0.14	0.47	1.69	-0.38	-0.71	-0.35	-1.04	-3.26	1783
	4)63		i mac	Toy all			THE PARTY NAMED IN	10,10	1,514	1790		A PARTY	- William
1784	-4.85	-3.17	-1.67	-2 72	0.49	-0.13	-0.48	-1.97	-0.63	-3.71	-0.71	-2.14	1784
1785			-5.49			100					-0.63		1785
1786	0.27	• •		F1117	-1.35		-1.77	1000		-1.97	41.51	-0.18	1786
1788				0.70	1.00						The same of	-8.65	1788
1789	-0.91		-3.15	OTHER DE		-1.49	1000	-0.14	40.0			0.91	1789
1.00	0.01	2	0.10		2.10	1.10	0.01	0.11			1124	0.01	1.00
	108.41					THE REAL PROPERTY.	200			CO. N.	1.05	81.01	
1798							0.20	0.39	0.59	0.55	0.14	-1.90	1798
1799	-3.09	0.92	-0.59	-1.15	-1.43	-0.70	-0.60	0.20	0.01	0.12	-0.12	-4.22	1799
1800	2.53	-1.60	-2.25	3.40	1.46	-2.10	-0.26	1.20	0.89	-0.43	-1.15	0.21	1800
1801	3.13	0.68	1.95	0.32	0.98	-0.98	-0.15	-0.49	0.76	0.98	1.17	2.21	1801
1802	-2.69	0.64	0.83	1.08	-0.60	1.37	-0.97	2.33	0.23	1.38	-0.38	0.53	1802
01874		N. Talle										3,T=1	
1803	-1.27	-2.92	-1.30	1.11	-2.75	-0.71	0.63	0.54	-2.37	-0.90	0.52	1.99	1803
1804	11		The second second	The same of the sa		-		-0.70		The state of the s	17 19 10 0	-2.05	1804
1805	11	1000	1	100000000000000000000000000000000000000	1000	3 44 1 3	TELESTIC 1	-1.17		M. Carrier	-2.92		1805
1806	4.11	1.89		-2.23	The second second	1700	136 mg	-0.35	TOTAL STREET	37.600	100	4.71	1806
	1/	1				1			1				

#### LXXXVI.

# South Germany. — Carlsruhe (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	egrees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1807	0.02	1.11	100000000000000000000000000000000000000	-1.34		-0.28	ATTENDED BY		-1.57			-0.53	1807
1808	1.38	-1.25	-3.54		2.40		1.94	0.96	2000	-1.28	-0.24	-3.75	1808
1809	1.24	3.25		-3.16		-1.22		-0.33		-1.36	-1.90	1.60	1809
1810	-3.19	-2.78	1.26	-0.17	100000000000000000000000000000000000000	-0.62	-0.65	1222	10000	-0.05	0.84	1.69	1810
1811	-2.40	1.17	2.79	1.65	2.32	1.55	. 0.78	-0.29	0.53	2.92	1.21	0.48	1811
200		-	4				19.5%	ME		I I		- 11	
1812	-2.09	1.47	-0.16	-2.96	0.83	-0.50	_1 53	-0.27	-0.24	1.33	-1.42	-3.80	1812
1813	-0.84	2.15	0.57	1.50	0.12	3.5 Pale 1	Secretary and	-1.78	11-11-11	0.27			1813
1814	-1.51	-3.24	-1.56	1.82	ACCOUNT OF	-1.66		-1.12		-0.68		2.67	1814
1815	-2.35	2.31	2.67	0.75	THE PROPERTY.	-0.57	1200		0.09	300 - 30 - 31	-1.99	-1.02	1815
1816	1.38	-2.00		0.27	100000000000000000000000000000000000000	-2.48					-2.14	0.17	1816
1010		2.00		0.21			1						2020
TO MERCOLLI	1.12-5	F.Jed.	0,6-0	£10,7	209	1	40		1356	Tell :	Top !	144	
1817	3.56	2.16			-1.63		-1.47			-2.82	1.78	0.13	1817
1818	2.91	1.12	0.59	1.53	-1.44	1.00	0.34	-1.01	O Lance	-0.63	1.49	-2.11	1818
1819	1.85	1.30	0.75	1.42	0.49	0.15	0.42	0.64		-0.15	-0.75	0.31	1819
1820	-1.09	0.55	-1.35	2.19	0.22	-2.16	-0.96	0.66	-1.20		-1.80	0.00	1820
1821	2.31	-1.59	0.73	1.78	-1.87	-2.01	-2.03	0.14	0.17	-0.68	2.72	3.52	1821
	4-00-6	0,541	M. Service	1177	407		14/12		1,18		11000	10.00	
1822	2.52	2.96	4.04	1.75	2.11	3.77	0.56	-0.14	0.46	1.19	2.66	-1.31	1822
1823	-2.23	2.20		-0.09	1.23		-1.14	0.87	0.24	-0.27	-0.11	2.95	1823
1824	1.39	1.98	THE RESERVE OF THE PERSON NAMED IN	-0.89	12.00		0.32	-0.22	1.04	0.66		4.09	1824
1825	1.92	0.28	-0.76	1.43	The same of	-0.41	0.85	0.49	1.15	0.15	1.51	3.05	1825
1826	-3.48	1.35	1.13	The second	-1.25	1.06	2.12	2.86	1.75		-0.21	0.93	1826
1010	0.10	1.00	1.10	0.20	1.20	2.00						0.00	2020
		dille.	-Olive		Tel A		1000					N N	
1827	-0.55	1	1.19	1.50	1.25	1.01	2.06	0.00	1.15		-2.01	2.85	1827
1828	3.18	0.41	1.17	0.82	0.74	1.19	0.91	-1.22	0.48		-0.33	1.85	1828
1829	-2.12	-2.33	-0.05	0.72	-0.04	0.21	0.50	-1.17			-1.88	-4.97	1829
1830	-5.83	-2.98	2.14	2.21	0.81	-0.22	0.86	-0.13	-1.01	-0.17	1.31	-0.32	1830
1831	-0.98	0.96	1.68	1.83	-0.50	-0.61	0.38	0.40	-0.81	3.26	0.30	1.64	1831
	L. Marsi						Was.	4111					LAUGE.
1832	0.10	-0.27	0.23	0.96	-0.88	-0.49	-0.01	1.02	-0.59	0.18	-0.68	0.95	1832
1833	-2.63	3.41	L. COMPA	-0.78		1.45		-2.23		-0.17	0.51	4.43	1833
1834	5.74	0.29	32.00	-1.12	1.87	1.12	2.76	1.35	1.82	0.53	0.79	0.29	1834
1835	1.77	1.74	1000	-0.90	-0.68	0.13	1.46	-0.17	-0.03	-0.83	-2.92	-2.23	1835
1836	0.43	-0.85		-0.66	1	0.47	0.21	0.47	1.67	0.82	0.66	1.56	1836
1,000			373	1	A ME		500	12	MAL	MATE I	22.7	3.00	MATE
	1.00	0.00		0.00	0.00	1.00	0.00	7.0	1.00	0.00	0	0	1000
1837	1.30	0.80		-2.33	THE RESERVE OF THE PERSON NAMED IN		-0.86	1.24	- C. (1) (2)	0.28	0.46	0.72	1837
1838	-4.35	-2.13	The second	-2.36	334	-0.21	1500 P	-1.20	0.44	-0.02	* TANK TO VALUE	-0.52	1838
1839	0.88	0.67		1 1 1 1 1 1 1 1	-0.54	2.28	0.16	-0.47	0.09	1.20	1.49	2.20	1839
1840	1.37	-0.69	-2.82	1.28	-0.51	0.23	-1.39	0.34	-0.22	-2.04	1.81	-5.32	1840
Means.	-0.17	1.95	4.39	8.31	12.40	14.43	15.80	15.41	12.60	8.30	4.16	1.35	Means.
1	To the	File	749	181.49	7 4 6	Percent.	100	100	Million !				
200	4.107	27/09-3	May !	M.D.R.	T. S. S.	14.4K	(Balana	HELL	SARAH SA	PERM	14 24	PARTY F	SVETS
T-68-874	17514	State :	Li has	BUNE	计学的	12.04	19,000	103/4	113/15	DAN'S THE	TERMS.		- HELL
1997	PARTY.	1,0	100	WAR	SHIRL SH	0.00	SAME.	DUCK	12,52	I head.	1 (2)	MICH	

#### LXXXVII.

## NORTH GERMANY. - BERLIN.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Since II				( and	De	grees of	Reaumi	ır.				-	
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1719	0 2.44	° 0.21	0 1.50	0.69	° 1.45	° 2.38	° 3.13	0	0.08	0.66	2.09	-1.02	1719
1719	2.27	0.40	-0.14	0.70	1.34	0.94	2.01	0.31	0.10	1.62	-0.03	1.47	1720
1721	2.38	-1.80	-0.14 $-1.53$	2.23	-0.91	1.21	-0.67	-0.17	0.10	0.40	1.69	0.07	1721
1721	1.50	-2.28	2.39	0.65	1.24	0.26	-0.38	-0.17 $-1.36$	-0.10	April 1	-0.58	-1.51	1728
1729	-3.18	-1.46	-3.57	-2.11	1.24	0.20	• •	1.50	0.10	• •	0.50		1729
1123	3.10	-1.40	-0.07	2.11	Y OF						nsval.	120.5	1123
1730	1.64	0.20	0.29	0.70	0.00	0.12	-0.62	-0.03	-0.69	-2.55	1.99	-0.48	1730
1731	-2.00	-1.78	-0.67	-1.67				-0.62	Annual Control of	1.85	0.67	0.26	1731
1732	-1.50	1.34	1.05	1.34	0.29	-1.54		-0.98	- MARY 13	1.14	-0.78	-3.99	1732
1733	2.69	2.54	0.86	1.59	-1.77	-2.71	-0.38	-0.97	-2.02	-0.53	0.21	2.46	1733
1734	0.40	2.51	1.86	0.55	-0.54	-1.26	-0.62	-0.93	-0.54	0.65	-2.85	-1.03	1734
1735	1.79	0.30	1.81	1.49	-0.87	-0.33	-1.38	-0.84	0.91	-1.01	-1.07	-0.17	1735
1736	-0.08	-0.92	-0.73	0.85	13 (-1)	-0.87		0.64	- 30	100	-0.09	1000	1736
1737	1.83	0.55	1.57	-1.36	0.77	0.11		-1.65	-0.10			-0.05	1737
1738	-0.55	0.55	1.11	1.54	-0.08	-0.42		-0.38	-0.05		-2.21	0.90	1738
1739	-0.17	2.06	1.11	-1.65		-0.96		-1.23			-5.35		1739
1.00	200	2000	-	1.00	wit i	0.00	111111	States	0.00	THE .	0.00	2.4.3	- social di
1740	-6.61	-6.54	-3.28	-3.45	-3.49	-1.70	-0.96	-0.62	1.62	-3.12	-2.35	-0.18	1740
1741	-0.93	1.88	-0.71	-1.38	-1.90	-1.59	0.17	-0.54	-0.20	1.22	1.77	-0.16	1741
1742	-1.23	1.08	-0.99	-2.16	-1.83	-0.72	-0.66	-1.26	-1.78	0.19	0.70	-3.22	1742
1743	1.32	0.99	-0.53	-1.94	0.28	1.05	-1.46	0.32	-0.50	-1.44	2.77	0.84	1743
1744	-1.98	-2.42	-0.09	2.33	0.10	-1.47	0.25	-0.60	0.94	2.10	1.25	-0.39	1644
1745	-1.92	-1.26	-0.10	0.20	0.73	1.01	0.01	0.17	0.10	1.15	2.17	-2.36	1745
1746	0.12	0.03		-0.39	0.43	0.000	1.41	-0.43	0.10	-1.06	0.00	1.89	1746
1747	-0.17	3.49	1000	0.70	-0.67		-0.33	0.18	1.43	0.43		1.04	1747
1748	-1.17	-1.70	1000	0.22	1.53		0.56	2.85	-0.14	0.00	1.79	3.19	1748
1749	2.28	0.47	-1.52	-0.14	1.58		0.39	1.64	0.33	0.05		1.28	1749
1750	1.19	3.22	3.87	1.26	0.30		1.97	1.56	0.26	-0.55		-0.06	1750
1751	-0.45		2.79	-0.86	3.59	2.39	1.78	3.12	0.42	-0.04			1751
Warne	-		180									_	Manne
Means.	-0.19	0.69	2.65	6.51	10.63	12.82	14.02	13.14	11.06	6.53	3.15	1.24	Means.
1755	-4.56	-6.47	100	0.54				-0.25				2.14	1755
1756	4.13	2.63		1.77	0.37	2.55		-0.35		1.62	1	-1.43	1756
1757	1.17	2.37	1.71	197	-0.39	1.47	3.25	0.22		-2.88	1.21		1757
1758	-2.57		0.13		1.08	A COLUMN	100	0.55		-0.97	0.16		1758
1759	3.26	1.79	1.18		-1.45		1.15		-0.45	1.09		1	1759
		48	12.00	1	1			1,21					te fail
1760	-0.56			0.34	VAL E	The state of the s	-0.29	0.03		100000	1 1 2 2 1 1 1	No. 11	1760
1761	0.97	1.65 -0.01		-0.01	1.55	DESCRIPTION OF	1	THE RESIDENCE	- 100	100000000000000000000000000000000000000	-0.12 $-0.32$		1761 1762
1762	-2.25		15-15 E. C. C.		NES 14522	The same	0.92	100000000000000000000000000000000000000	1			7500000	1762
1764	2.91				1000	The Later of	1			-0.63		1	1764
Maria C		1.00	0	1	11	1.04	1120		1	0.00	1.00	2.01	101
1765	1.64	-2.90	1.70	0.78	-2.50	-0.88	-1.92	1.12	-1.16	1.20	0.15	0.03	1765
1766	-0.10	-0.12	1.01	2.07	1	1	1		100000	-0.43	0.48	-0.26	1766
1767	-5.54	1.74	0.01	-1.58	-1.03	-1.65	-0.23	0.88	0.42	0.95	2.03	-1.75	1767
Ľ	"			-	<u> </u>		-		1	-	<del></del>		

#### LXXXVII.

## NORTH GERMANY. - BERLIN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

				5 92	De	grees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1768	o -3.52	0.98	° -1.28	° -0.11	° -0.68	-0.06	0.28	-0.08	° -1.03	° -0.48	0.54	0.47	1768
1769	1.22	-0.74	0.75		-1.01		-0.71	-1.07	0.58	-2.26	0.26	0.84	1769
1709	-0.20			0.14 $-1.09$	-0.11	THE PERSON	-0.71	-0.08	0.62	0.81	0.16	1.92	1770
			-3.16	Sec. 10. 20	J. S.	27.75 1		100	and the same	1000000	The state of the s	THE PLAN	No. of the last of
1771	-1.24	-3.28	-3.40	-3.27	2.04	Particular .		50 mm 3 mm	-0.46	0.76	I want	0.95	1771
1772	0.66	1.20	0.86	-0.86	-2.50			-0.41	0.60	1.62	1.89	1.38	1772
1773	2.50	-1.00	-0.61	0.49	1.37	-1.22	-0.85	0.06	0.57	1.89	-0.92	2.21	1773
Means.	-0.13	1.64	3.87	7.71	11.94	15.23	16.18	15.34	12.12	7.73	4.38	1.85	Means.
1774	1.50	2.26	2.29	1.56	-0.05	0.69	-1.56	-1.92	-1.61	0.71	-3.70	-0.75	1774
1775	0.95	3.20	2.53	-0.65	-0.72	3.26	1.88	1.61	2.00	1.23	-0.84	2.16	1775
1776	-5.55	2.42	2.10	100 CO TO TO TO	100 T 100 ET	1.19	1.21	0.32	0.12	-0.47	0.70	0.54	1776
1777	0.04	-1.67	0.67	-1.12	0.52	0.04	-0.60	-0.01	-1.71	0.23	2.23	0.75	1777
1778	-0.58	-1.72	1.09	1.98	0.67	0.30	1.02	0.66		-1.69	1000	3.84	1778
1779	0.33	3.82	2.99	2.39	0.61	-0.30	0.74	1.71	1.59	1.95	0.90	2.26	1779
1780	-1.06	-2.02	3.37	-1.27	0.72	0.24	0.45	0.99	-0.03	1.46			1780
1781	-0.44	0.53	2.05	1.85	1.19	1.97	2.02	2.56	1.60	-0.39	0.80	0.01	1781
1782	3.15	-2.86	-0.39	-0.87	0.33	1.78	1.52	0.21	1.75	-0.30	-1.13	0.78	1782
1783	3.19	3.67	-0.58	0.86	1.38	2.71	1.45	0.71	0.36	0.34	0.50		1783
AVENT.		8 18 1											100
1784	-3.97		-1.68		0.58	0.20		-1.35	0.02	3.77	201040	-0.94	1784
1785	0.47		-5.74	-2.54	-1.48	-0.84	TOO YOU		0.61			-1.42	1785
1786	1.81	-0.93	-2.32	1.60	-1.25	0.54		-1.26	-1.86	1000	-3.64		1786
1787	-0.29	1.38	2.05	-1.31	-0.77	0.99	and the second	-0.59	-0.17	1.32	0.69	2.07	1787
1788	2.46	-1.26	-1.47	0.10	0.45	1.64	1.64	-1.21	1.20	-0.35	-0.79	-8.64	1788
				e a la cons	LUL .	ESTA B						144	
1789	-1.93	1.46	-4.45	0.01	1.85	0.14	0.11	0.36	1.85	0.64	0.89	3.55	1789
1790	3.05	2.82	2.19	-1.67	1.70	0.58	1000	-0.54	-0.48		-0.30	1.92	1790
1791	3.91	1.52	1.47	1.74	-1.16	0.19	0.78	1.08			-0.89	1.35	1791
1792	0.53	-1.89	0.80	1.45	-0.81	0.83	1.59		-0.98		-0.01	1.14	1792
1793	-0.70	2.14	0.61	-0.68	-0.58	-1.34	1.68	0.22	-0.83	1.99	0.99	2.05	1793
1794	1.18	2.56	3.66	3.12	0.18	1.77	2.79	-0.59	-1.62	0.37	1.53	-2.14	1794
1795	-5.23	-0.36	-0.84	2.88	-1.78	2.10	-0.92	-0.37	1.27	3.36	0.10	3.14	1795
1796	6.51	0.68	-1.70	-0.34	-0.46	0.38	0.48	1.33	1.74	0.07	-0.60	-1.82	1796
1797	1.60	1.89	0.66	1.09	1.41	-0.23	1.55	1.26	2.02	0.55	-0.80	1.81	1797
1798	1.79	1.57	-0.07	1.29	0.76	1.20	0.38	0.92	1.24	-0.17	-0.45	-3.54	1798
1799	-2.97	-4.47	-1.65	-2.12	-2.27	-1.53	-1.05	-0.32	-0.65	-0.70	0.48	-4.41	1799
1800	-1.12		13.20	4.43	2.33		100	0.22	0.67		1.47	0.00	1800
1801	1.88	12 12 12 12 12	1.84	0.05	3.00	-1.37		-0.68	1.01	1.40	0.93	0.84	1801
1802	-1.00		1.65	0.45	-2.37	-1.01	-1.54	1.54	-0.08	3.04	0.78	1.81	1802
1803	-5.33	2.02	-0.16	2.84		-1.46	2.03	1.80		-0.45	0.68	-0.39	1803
	0.00	2.02	0.10		2.00	2.20		2.00	1.02	0.40	0.00	0.00	1000
1804	1.51	-1.48	-3.11	-1.06	1.04	-0.54	0.10	-0.73	1.17	-0.02	-2.40	-3.92	1804
1805		-1.94		-1.58		-1.53		The state of	Carlo Inches	-3.53	-2.58	1.24	1805
1806	3.02	0.94	0.19	-2.82		-2.26		-0.98	0.41	-0.12	1.47	4.14	1806
1807	1.62		-1.97	M. Harry				3.72			1.11	1.53	1807
2001	11 1.02	0.10	1.01	1.10	0.72	1.00	0.22	02	2.10	0.00	1.11	1.00	1001

#### LXXXVII.

## NORTH GERMANY. - BERLIN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees or	Reaum	ur.		-			
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1808	0.83	0	0	0	0	° -0.42	° 1.19	0.69	0 -0.54	-1.56	0	0	1808
	CONTRACTOR			-2.80		100000000000000000000000000000000000000	THE PAGE						
1809	-3.31	1.64	500000	-3.34	A. TOO	-0.89	100000000000000000000000000000000000000	0.36	1.00	-0.99	0.02	2.23	1809
1810	-0.99	-1.66	113714	-1.41	-1.88	-1.93	-0.05	-0.47	10000	-1.33		1.22	1810
1811	-2.93	-0.72	2.01		3.07	2.67	0.94			2.21	0.35	1.50	1811
1812	-1.14	-0.27	-1.05	-3.98	-1.20	-0.68	-2.37	-0.78	-1.81	1.14	-1.57	-5.52	1812
1813	-1.20	2.38	0.24	1.00	-0.73	-1.23	-1.27	-2.07	-0.82	-1.30	0.05	1.02	1813
1814	-2.12	-5.52	-2.78		-2.92	-1.99	1.02		-2.23	-1.21	0.55	1.26	1814
1815	-2.81	1.14	1.56		300	0.61	0.011000	The second second	1 7 1 1	0.42	13373	7520	1815
1816	0.95	-2.27	-0.68	1000	-2.68	-1.54			-1.64			-0.39	1816
1817	2.58	1.79		-3.86	0.70		-1.57	-0.55				100	1817
	2.00	- 1	0.10	0.00	0.10	1.01	1.0.	0.00	1.10		2.01	0111	101.
1818	2.54	0.19	1.56	0.53	0.22	0.95	0.72	-1.41	0.14	-0.58	-0.60	-0.89	1818
1819	2.51	1.57	1.59	0.85	1.00		1.42	1.60	0.81	-0.41		-2.61	1819
1820	-3.08	0.34	-0.02	1.52	0.91	-2.38	-2.08	1.23		0.99	1000	-1.88	1820
1821	1.52		0.14	3.28	-0.48		-1.51	-0.78	0.91	1.33		3.44	1821
10000						-				14.00			
Means.	-1.59	0.30	2.28	6.89	11.36	13.73	15.16	15.00	11.83	7.16	2.61	-0.32	Means.
		ST-	11.				100	older.	12.11				
1822	3.39	3.67	3.22	1.55	IN KALDAT		10.8	1.25	-1.24	1.36	100	-3.18	1822
1823	-7.56	-0.25	0.41	1 11 1200	-0.26	-0.78	-1.76	1.03	-0.34	0.66	1.01	1.12	1823
1824	3.67	2.45	0.29			-0.75	-0.56	-0.58	1.27	0.56	1.96	2.69	1824
1825	3.92	0.92	-2.26		-0.15	-1.10	-0.47	0.05	0.54	-0.12	1.30	2.03	1825
1826	-3.44	1.98	1.15	-0.19	-0.24	1.20	3.03	3.00	0.35	0.71	-0.33	0.49	1826
780	0.04			Flath.		4900	made.	TRACK!	1		1949	4	o birgu.
1827	0.25	-4.90	1.25	2.29	1.98	1.33		-0.04	1.09	0.83		1.16	1827
1828		-0.55	0.67	1.22	0.33	0.30		-0.71		-0.28	0.17	0.47	1828
1829		-2.67	-1.23	0.41	-0.29	0.12		THE RESERVE TO SERVE	-0.16	-1.62		-8.25	1829
1830	-4.21	-2.70	1.09	1.53	0.30	0.07	0.35	-0.26		-0.69	1.47	-1.79	1830
1831	-1.81	0.75	0.40	2.21	-0.94	-1.34	0.36	0.20	-1.22	1.77	-0.54	0.11	1831
1832	0.76	1.12	0.42	0.32	-1.43	-0.33	-2.40	0.22	-1.22	-0.35	-0.63	-0.24	1832
1833	-0.86	3.16	-0.18		3.46	1.33	-0.45	-3.12		-0.93	0.14	2.48	1833
1834	4.73	1.31	1.00	-0.68	1.82	1.23	3.65	2.34	0.74	-0.98	0.14	0.36	1834
1835	2.81	2.37	0.57	-0.91	-0.86	0.13	0.21	-0.59	1.22	-0.28	-2.71	-1.77	1835
1836	1.37	1.11	3.42	0.07	-2.55	0.13	-1.08	-0.39 $-1.49$	-1.06	1.00		0.26	1836
1000	1.07	1.11	0.42	0.07	2.00	0.20	1.00	1.40	1.00	1.00	-1.10	0.20	1000
1837	1.91	0.38	-1.98	-1.68	-1.49	-0.60	-1.11	1.20	-0.92	0.37	0.72	-0.87	1837
1838	-6.30	-3.63	0.42	-1.42	-0.24	0.35	-0.22	-1.78	1.27	-0.89	-1.14	-0.33	1838
1839	0.79	1.50	-1.98		0.58	0.95	0.77	-0.44	1.10	0.15		-1.49	1839
1840	-0.09	0.65	2000	-0.07	-0.03	0.16		-0.07	The second		-0.05		1840
1841	-0.01	-4.03	0.91	1.01	2.51		-1.10	-0.01	0.58	1.29	0.75	1.62	1841
Carrie 1	Engle-	3/000	regard	27,040	ESC.	ATECE	Trans.	2730	1.5	184 E-1	(HQCC)	313.34	
1842	-1.34	0.39	0.93	-1.52	0.75	-0.54	-0.84	3.13	0.42	-1.55	-2.82	0.71	1842
1843	2.40	2.45	-1.09	0.44	-2.01	-1.00	-0.41	1.17	-0.64	-0.66	1.42	1.96	1843
1844	1.00	-0.96	-1.50	0.48	0.56	-1.00	-2.35	-1.60	0.36	-0.24	0.56	2.41	1844
1845	1.65	-4.55	-6.24	0.28	-1.48	0.49	0.90	-0.94	-0.93	-0.18	1.26	0.33	1845
Means.	-1.90	-0.15	2.74	6.88	10.92	13.94	15.04	14.49	11.75	7.97	3.25	1.32	Means.
	1.00	0.10	2.14	0.00	10.32	10.74	10.04	14.40	11.79	1.51	3.40	1.02	

#### LXXXVIII.

#### DENMARK. — COPENHAGEN.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year						De	grees of	Keaum	ur.		7000			
1768	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	TWOP	0	0	0	0	0	0	0	0	0	0			120
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						LA ALTERNA	The same of the same of				13.6-20.00	COLUMN POR		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	The second second	1 10							PERSONAL PROPERTY.	7000		A COLUMN		A CONTRACTOR
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Transfer .	190 4	1 1 1 1 1 1		The same of		13.77	200		1777 to 12 73 miles	MARKET STATE	1101725	23.00	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ACC. WINDS TO	1000	100	325	The state of the s	The state of the s	The state of the s		The second second	1	17.755507	103100		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1771	-1.20	-2.18	-3.90	-3.14	0.27	1.50	70.55	-2.04	-0.90	0.03	-1.11	1.10	1771
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E JEST		7 2			1	N AN						A STATE	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1772	-0.88	-1.71	-2.53	-1.72	-1.94	-0.51	-0.56	-0.59	0.83	1.49	2.39	1.33	1772
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1.78	-0.46	0.35	0.33	0.83	-0.54	0.50	0.81	0.45	1.73	0.81	0.94	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1774	-2.37	0.34	0.87	0.83	-0.09	0.37	0.04	-0.65	-1.07	-0.31	-5.39	-2.55	1774
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1775	-0.51	1.79	1.72	0.21	-0.09	2.13	1.39	1.72	2.60	0.78	-1.97	0.71	1775
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1776	-5.22	1.18	1:49	0.73	-0.87	1.61	2.30	1.35	0.59	0.67	0.77	0.69	1776
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S. B. F.							MAR.		BLAT	6	1	No.	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1505	6, 10	10 2	AF IP	1.5		1	Marie .	37	140		No B		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	NR DR	700 900	7.31	The Party of the P	- CO. J.	1170	100000000000000000000000000000000000000	150-4	F-E-1921-195	mov-a	Control of the last		1000	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		no but	10000	10000000	C 18 3 1	Total Control			C180-11-1	The state of the state of	CELEBRAT I	125.00	GREAT !	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	100	100		4000	2.77	70	The second second		2000	.9	2 × (3)	W		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				1893-2511	0.000	000-00	S acres	4 - 7.	110000	A		1100 1100		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1786	0.13	0.06	-2.69	0.83	-1.08	1.48	-0.35	-0.41	-0.74	-1.21	-2.91	-0.04	1786
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	HEAL.			GW			Same Sale		Carlos S	1000	High	1	14	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1787	0.94	2.21	2.09	-0.20	0.07	0.01	0.06	-0.31	0.58	1.81	-0.40	0.26	1787
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			CONTRACTOR AND ADDRESS OF	THE R. LEWIS CO., LANSING, MICH.	FRANCES		STATE OF THE OWNER, TH	1000 1000	THE STATE OF THE PARTY OF	But Bu	400 000		-	1 4 4 1 1 1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	100000000000000000000000000000000000000	200	Sales Tall	2000	SHOET PRITTY	Mary Co.	Street, Street	100 000	F 12 TV	Parker Vision	0.00	Contract of	CONT. I	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	100		Salar Real	SEE SEAL	10000	750 E-2	200	41/4/16	P. W. Can	W. W. Chin		and the same of	The state of the	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					The state of the state of	1.77	-1.69	-0.89	0.42	0.21	1.19	1.78	1.20	1800
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1		125h		1000				Ve N				100	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		L. To		Boy !										
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1.28	0.75	March Street	1.44	The Secretary	141 P 247	Charles William		2000	and the latest	COLLEGE STATE OF	Section 1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1802	-0.56	1.04	1.90	1.000		CELLA ALL	100000	Carlotte Street	100000	Marie Marie	able to	ALCOHOLD .	1802
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 0 0 0		The second	251	100	The state of	CONTRACTOR OF	1000 TO 1000	The Country of the Co		The same of the sa	The Court of		100000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.00000			\$1.00 Date	The state of the s		THAT OF TH	DC+176/1	100 K ( 80)	04.44		The same	Carlo September	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1805	-1.79	-2.02	0.26	-1.03	-2.14	-3.46	-1.48	-1.03	0.77	-2.53	-0.56	0.77	1805
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			G 18 (	20,1	Pag				115.(					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1000	1 00	1 04	0.40	1 50	0.00	9 90	-1 70	_0.00	1 99	0.25	1 07	254	1000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					- T	THE RESERVE		The second second		TOTAL PROPERTY.		Mary Committee	Andrew Park	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			STATE OF THE PARTY OF	The second second		7940 21-1	100 000	Charles and "	A		200	10.00	-	Part of the latest and the latest an
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	- 7/2			ALC: UNKNOWN	Carlo Marie		The state of the s	4			Daniel Co.	Charles and the	1000	No real parts
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	A CONTRACTOR OF THE PARTY OF TH	100 140	ETTEL STORY	THE PARTY	The San Property					100000000000000000000000000000000000000	The contract of	Sales St.	100000000000000000000000000000000000000	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1010	0.00	0.20	0.00	1.13	2.03	1.01	0.01	0.23	0.01	0.10	0.22	0.10	1010
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		HE LOS	(C)		100	di we	TO DO	Sen en	العالم الم	E-gu	Contract of	1:90	Soyue,	12 15 2 2 10
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1811	-0.65	0.23	2.46	-0.71	1.75	0.96	2.07	-0.32	-0.26	1.28	1.12	1.07	1811
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				35.00			96. 3		MOCHELL IN	THE RESERVE OF THE PERSON NAMED IN			110	
1814   -3.81   -4.01   -2.15   0.28   -2.99   -1.97   0.13   -0.87   -1.05   -0.58   1.22   0.85   1814   1815   -0.67   1.47   1.82   0.30   -0.26   -1.26   -1.95   -0.81   -1.11   0.59   0.20   -0.66   1815			The second second						The second second	Programme 1				
1815   -0.67   1.47   1.82   0.30   -0.26   -1.26   -1.95   -0.81   -1.11   0.59   0.20   -0.66   1815	HITCH STREET					200	A 1000	FRANKE	HE LAND TO SERVICE	100		-		100
		1		Table 1	7 1 2 2 2 2	The state of	- 60-50		And the second	The state of the state of			1000	
1000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		HAR		3880		12 - S	ENTE	STALE.	A STATE	WEIL	Ser al	FINE	ES ONE	9 900
3030   0 WO 3 FO 0 OF 0 10 0 00 3 0W 0 10 3 00 0 00 0 00 0 00	A 180		Billion II		1	1		1	15	THE	1	Supply .	25 197	1-9/00/19
1816   0.72 - 1.56 - 0.05 - 0.49 - 2.69 - 1.87 - 0.49 - 1.86 - 0.89 - 0.72 - 0.95 - 0.31   1816	1816	0.72	-1.56	-0.05	-0.49	-2.69	-1.87	-0.49	-1.86	-0.89	-0.72	-0.95	-0.31	1816

#### LXXXVIII.

## DENMARK. - COPENHAGEN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

		TEVAL S			De	grees of	Reaum	ur.	1063		E. M. C.		STATE OF
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0 .	0	0	0	0	0	0	0	0	
1817	2.79	2.98	1.13	-1.10	-0.01	-1.04	-1.53	-1.38	0.62	-2.24	1.41	-1.71	1817
1818	1.99	1.73	2.40	-1.05	-0.05	0.97	1.29	-0.24	0.69	0.87	1.48	0.20	1818
1819	3.46	2.30	2.39	1.56	1.25	1.69	1.58	3.28	1.46	-0.79	-1.03	-1.26	1819
1820	-1.67	0.51	0.52	1.55	0.25	-1.16	-0.36	-0.33	-0.60	-0.64	-0.56	-0.87	1820
1821	0.36	0.16	0.24	2.24	-0.43	-1.77	-1.81	-0.86	0.67	1.62	1.68	2.47	1821
											2 2 3		
13/10/1	AV.	De la Contraction de la Contra	-		9-1-1	WAR.		RALES			F-14		
1822	2.56	3.82	3.64	2.28	1.59	0.87	0.24	-0.17	-0.64	1.52	2.63	0.56	1822
1823	-2.60	-0.08	0.70	-0.04	0.51	0.15	-0.94	0.41	0.47	1.02	1.88	1.74	1823
1824	3.65	2.36	0.97	0.91	0.14	1.22	-0.61	1.111.000	1.62	0.09	1.20	2.18	1824
1826					4.30	5.91	7.76	6.63				2.04	1826
1827	0.16	-2.30	0.59	2.14	1.44	1.93	0.09	-0.29	1.48	1.16	-1.20	2.30	1827
	THE STATE OF	ST.		N. Carlo	434	Marie I	D 13 . 14	1	Mag.	- 4 - 0.0			
ENERGE	A STATE OF	Marine Marine	177	dr.	P 47401	414	HE Y	11111		V		-	Pilos S
1828	-0.07	0.43	1.37	0.58	1.31	1.34	1.36			0.46	H. Charles	0.50	1828
1829	-1.14	-3.06	-0.95	-1.00	1.84		-0.23		0.03		-2.91	-3.60	1829
1830	-2.26	-2.85	1.39		-0.18	-0.86	2000	Contract of	-0.95	0.15	1.75	E277 22.04	1830
1831	-1.60	0.61	-0.16	1.87	0.31	0.85	2.52	1.700	-0.59	2.71	-0.65	1.91	1831
1832	1.52	1.73	1.55	1.84	-0.23	1.29	-0.94	-0.06	-0.98	0.60	-0.47	0.58	1832
			1977							Carl			
700			p1117.5			100		M 21	100	2000		Man 3	
1833	0.05	1.50			2.32	0.72		-2.27	0.08	0.63	0.77	1.32	1833
1834	2.26	1.71	2.23	0.90	11.15 30.71	0.72	3.60			-0.05	0.22	0.59	1834
1835	1.87	2.16		-0.02		1.17	1.03	The second	LOS MAN	-0.85			1835
1836	0.29	0.63	2.71	A 49 YO Y	-0.17	0.24	-0.89	-1.86		-0.48	15/11-20	0.09	1836
1837	0.17	0.54	-1.08	-1.50	-1.10	0.05	-0.21	0.60	-0.80	-0.06	-0.91	-0.75	1837
						P- 74	100	100000		9.5	Farls.	VP/A	
7000	0.00		0.00	0.00	0.00	0	0.00	200		- 00	0.01	0.05	7000
1838	1 100	WATER TO SERVICE AND ADDRESS OF THE PARTY OF	-0.56	The second second		- Co.	15/90/177		1000 0000			100000000000000000000000000000000000000	1838
1839		-0.38						1	-0.40	CONTRACTOR OF THE PARTY OF THE	-0.19		1839
1840	-0.63	25.0	-0.64	0.35	F- 6				-1.95	N W/T 0			1840
1841	1	-2.52	0.97	0.62	1/2-0.1323		INTERNATION OF THE PARTY OF THE	1	-0.71	The state of the state of		And the second	1841
1842	-0.26	1.43	2.05	0.61	1.78	-0.11	-0.99	2.73	0.31	-0.88	-1.57	2.36	1842
- A - A - A - A - A - A - A - A - A - A	TO LE									- Thirtie		1	
	O Dina						CALLED BY						
1843	1.82		-0.33	13.00	100	-0.25	- 1 2 h 2 m	The same of the sa	-0.20		0.86	2.99	1843
1844	0.07		-1.50	0.74	1.49				-0.62	10000		-1.43	1844
1845	1.24	-4.16	-4.45	0.54	-1.01	0.20	0.22	-0.86	-1.26	-1.04	1.28	0.59	1845
Manne		770.00		12/2				102 10		-	Wille		3/
Means.	-1.16	-0.80	0.55	4.45	8.98	12.45	13.81	13.50	10.86	7.05	3.12	0.68	Means.
1018		100		PO HAN	1 1 1 2 3		4	Blog.	11/19/2	MARKE	100	7	Marie Service
BY SEA		1111	APPENDI	District	CO C	10,114	198	1/15/20	PRESIDE	4	N/Salva	-414	
THE REAL PROPERTY.	F A	Te III	de de	De L	1307 303	7Willia	685/69	\$150 HE	\$277	ar g	de di	20/10	Callegan
or ally tell		100	60.0	Sept.	68.63	the sale	Paje.	No. 24	No.	28.19	F	Darile	199229
1986		195	1272	OR SL	AST I	BE10	fin is	192 F.	de l'	61.37	COLUMN TO SERVICE	127	AND THE REAL PROPERTY.
September 1			PR-FE	P to live	HAT.		TRUE.	CE.	Fig. G	CE E		17 -2	3/200
THE REAL PROPERTY.	1	05.69	34	28/1	ded-	AP.	54C)	13.50	1000	BALE.	10.00	19/63	in district
	1400		1	138	atols		137/2	Eagl		11 13 8	Et all		
THE E		mo.As	Bas I	2 1		213	THE A	To the last			31.8	-27	1000
		1000		AUTO	100				1		100		NO VICTOR

#### LXXXIX.

#### France. - Paris.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Reaum	ur.	142				
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1806	3.35	° 1.38	0.28	° -1.54	2.07	0.77	0.64	-0.38	0.53	-0.26	0 1.69	4.00	1806
1807	0.34	1.39	100000	-0.63	4 10 10 10 10 10 10 10 10 10 10 10 10 10	-0.52	1.94	2.34		1.15		-1.75	1807
1808	0.42	-1.42	-2.19	10000	400000000000000000000000000000000000000	-0.30	2.14	0.66		-1.74	0.58	-1.87	1808
1809	2.95	2.91	0.42		100	-1.38		-0.36	Victory and	-1.09	15/2 1/2	1.04	1809
1810	-2.90	-1.11	1000	-0.42		-0.06		-0.70	1.75	0.25	0.80	1.30	1810
1010	2.00	****	1.10		0.02	0.00			2		0.00	2.00	1010
1811	-1.83	2.31	1.90	1.58	2.14	0.25	0.44	-0.66	0.95	2.55	1.38	0.72	1811
1812	-0.32	1.63	-0.82	-1.92	0.88	-0.77	-0.96	-0.46	-0.17	0.51	-1.95	-3.71	1812
1813	-1.18	1.33	-0.23	0.71	0.48	-1.26	-1.12	-1.42	-1.38	0.29	-0.63	-0.47	1813
1814	-1.70	-3.37	-2.30	1.30	-1.67	-1.17	0.46	-0.91	-0.26	-1.22	-0.51	2.02	1814
1815	-1.98	2.39	2.29	0.36	0.18	-0.89	-0.93	-0.54	-0.11	0.77	-2.70	-1.34	1815
	55	1998.	27-70	111111	A STATE		25 211		ALC: Y	1074	264	100	Water!
1816	0.54	-1.69	-0.71	0.10	-1.40	-1.83	-2.53	-2.37	-1.26	0.29	-2.24	0.07	1816
1817	2.48	2.22	-0.20	-2.02	-1.70	0.61	-1.34	-1.66	0.99	-3.16	1.80	-1.12	1817
1818	1.94	-0.21	-0.15	1.20	-0.65	1.75	1.14	-0.18	0.05	0.38	1.98	-1.23	1818
1819	2.43	0.95	0.16	1.31	0.02	-0.85	0.30	0.78	0.58	-0.12	-1.66	-0.30	1819
1820	-2.02	-0.98	-1.42	1.20	-0.30	-1.37	-0.35	0.11	-1.19	-0.93	-1.30	-0.22	1820
			120016	Suit	Sand.		10 1 8 15	100					
1821	1.02	-2.58	0.54	1.34	-1.95	-2.05	-1.39	1.20	0.85	-0.14	2.70	3.10	1821
1822	1.96	1.52	2.62	1.01	1.72	3.26	0.09	0.42	0.18	1.72	1.82	-3.42	1822
1823	-1.79	0.88	-0.14	-0.62	0.50	-1.69	-1.23	0.46	0.00	-0.58	-0.84	1.58	1823
1824	0.61	0.68	-1.00	-0.54	-1.52	-0.61	-0.02	-0.17	0.89	0.54	2.30	2.74	1824
1825	1.23	0.06	-0.94	1.54	-0.22	-0.05	1.24	0.70	1.77	0.75	0.40	2.18	1825
		ASSESS,	E H			Travie	100.17		100	1 5 kg	PBI.		
1826	-2.77	1.73	0.56	0.27	-1.48	1.35	1.59	2.10	1.11	1.70	-1.08	1.72	1826
1827	-1.63	-4.14	1.14	1.14	0.18	-0.09	0.85	-0.43	0.46	1.52	-0.77	2.58	1827
1828	3.28	0.80	0.29	0.50	0.46	0.34	0.34	-0.74	0.74	-0.30	0.51	0.89	1828
1829	-3.16	-0.97	-0.75	-0.08	0.32	0.05	-0.10	-1.30	-1.53	-1.01	-1.64	-5.70	1829
1830	-3.42	-2.59	2.54	1.68	0.11	-0.82	0.16	-1.23	-1.50	-0.44	0.83	-0.82	1830
STATE OF	Back 1913		-		1000					0.00	n aid		
1831	0.13	1.53	1.85	1.30	SHEDOGIL!	-0.12	0.86	11 1 1 C 1 C 1 I	-0.35	37110 1 2	-0.10	1.50	1831
1832	-0.36	-0.59	-0.93	100000000000000000000000000000000000000	-1.05	0.22	0.68		-0.10	Service and a	-0.10	0.53	1832
1833	-1.73	2.34	-1.82	-0.38	2.54	1.06			-1.53	The second second	-0.61	3.46	1833
1834	4.34	-0.42	0.67	-0.70	1.59	0.70	1.25	0.69	1.24		-0.05	-0.02	1834
1835	1.35	1.69	-0.14	-0.38	-0.55	0.18	1.92	1.42	0.36	-0.92	-1.10	-2.84	1835
				M.A.		41117	Mary St		dian		(3 N)		No.
1836	0.55	-1.03	1.62	-1.02	-1.67	1.06	0.56	0.30	-1.24	-0.04	0.66	0.36	1836
1837	0.39	0.97	-3.26	-3.34	-2.79	1.14	-0.32	1.26	-0.84	0.04	-0.62	0.60	1837
1838	-5.21	-5.03	1	-2.52	T. 55 - 374	-0.68	-0.32	-0.42	-0.12	-0.04	0.74	-1.48	1838
1839	0.75	0.73	-0.62	-1.70	-0.71	1.62	-0.04	-0.86	0.00	-0.56	1.10	1.60	1839
1840	1.23	-0.47	-2.58	2.26	0.49	1.02	-1.08	0.98	-0.64	-1.40	0.99	-4.76	1840
		- 0		RES R	185 (80	THE STATE OF	PER	· ·	400	V began	0.00	NET B	3
1841	0.47	-1.35	1.94	0.42	2.25	_1 26	-1.68	-0.50	2.28	0.12	0.02	1.48	1841
1841	-2.65	0.33	1.94	0.42	0.00	The state of the s	110000000000000000000000000000000000000	3.18	HILL THAT	400000000000000000000000000000000000000	-1.10	0.36	1841
11	4140	-0.39	1.06					0.70	0.96	A. C.	0.54		The state of the s
1843 1844		-0.39	0.18				-1.12		0.30		0.34	0.60	1843
1044	0.03	-1.91	0.18	4.44	1.00	0.04	1.14	2.04	0.24	-0.00	0.20	-3.40	1844
Means.	1.53	3.35	5.33	7.90	11.50	13.66	14.96	14.89	12.52	9.00	5.41	2.92	Means.
	1.00	0.00	0.00	1.30	11.00	10.00	11.00	14.02	12.02	3.00	0.41	4.34	1

#### XC.

## Holland. — Zwanenburg.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	egrees of	Reaum	ur.	2				
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1743	0.60	0	-0.15	0	0,40	0 50	° -1.15	0 05	-0.22	-2.27	° 1.83	-0.23	1743
	-0.91		-0.74			-0.26		-1.23		0.39	0.66	0.23	1745
1744			-0.74 -0.70	100000000000000000000000000000000000000		1000000		-1.20	Wall-	-0.27	-0.50	300-10	
1745	0.15			,		200000000000000000000000000000000000000		7155 20	1244		100000000000000000000000000000000000000	-0.2377.53	1745
1746			-2.19			-0.62			-0.65 $0.34$	The same of the same	-2.80	1.02	1746
1747	-0.47	2.16	-2.29	-0.18	-0.52	0.92	-0.65	-0.21	0.34	-0.49	1.62	1.60	1747
1748	-0.24	-2.63	-4.14	-2.12	-0.31	1.45	0.08	0.39	-0.03	0.28	1.68	3.46	1748
1749	2.68	0.11	100000000000000000000000000000000000000	-0.52	1.11		1 1 1 1 1 1 1 1		-0.11	-0.35	-0.45	1.65	1749
1750	-0.34	2.60	14.000000	-0.06	1000	-0.10	0.97	-0.45	0.75	4000000	10.000	1500	1750
1751	1.09	-2.29	111111111111111111111111111111111111111	-0.60		-0.10	33736	-0.52	-1.19	-0.48	-1.31	0.33	1751
1752	1.71	-0.56			-1.10		1-10-	-0.09	THE REAL PROPERTY.	0.07	0.90	1.37	1752
1102	200	0.00	0.12	0.00	1.10	0.55	0.40	0.05	0.05	0.01	0.30	1.01	1.02
1753	-1.80	-0.11	1.34	0.01	-0.30	1.19	-0.34	-1.00	0.30	0.59	-0.88	0.67	1753
1754	0.64	-1.14	-2.23	-1.40	0.41	-0.49	-1.33	-0.16	-0.44	0.61	0.05	-0.36	1754
1755	-1.98	-3.19	-1.24	1.72	-1.37	1.89	-0.31	-1.33	-1.12	-0.08	-0.03	1.22	1755
1756	3.20	1.32	0.38	-1.57	-1.53	0.97	0.80	-0.50	0.74	-0.31	-1.13	-2.60	1756
1757	-2.22	-0.59	0.00	1.00	-1.01	-0.11	2.37	0.36	-0.21	-1.09	1.43	-0.09	1757
		PARTICIPATION OF THE PARTICIPA	T Troo		L. A.	CHILD IS				No.		1000	
7850	7.00	0.0=	0 17	0.00	7.05	0.00		0.00	0.75	0.01	A 01	0.00	
1758	-1.28	0.37	0.41	-0.39	1.95	0.29	-1.41	100	-0.17	0.21	0.05	0.36	1758
1759	2.86	2.13	1.49	No. of Contract of	-0.58	0.99	1.66	A 1 12 13	-0.07	1.05	-1.54		1759
1760	-1.64	-0.69	0.15	0.77	-0.22	1.31	-0.15	-0.40	1.14	0.28	1.08	2.67	1760
1761	1.78	1.90	2.37	0.47	0.92	0.86		1.16	0.67	-1.75	0.34	-1.59	1761
1762	2.10	0.09	-1.25	2.37	0.93	0.67	0.30	-1.31	-0.04	-1.98	-1.37	-2.02	1762
		0 70								misn.			
1763	-4.88	0.79	-0.34		-1.04	0.28		10 (0.10)	-0.56	A STATE OF THE PARTY OF	0.56	1.52	1763
1764	3.37	2.52	0.17	0.52	1.71	0.02	1.43	-0.32	- Date 27		-0.45	- 17 C - France	1764
1765	2.24	-2.13	2.30	1.62	0.27	1.22		0.85		1.24		-0.82	1765
1766	-0.22	-0.78	0.72	1.67	0.37	0.35	0.20	0.45	0.49	0.32	0.46	-0.68	1766
1767	-3.34	2.34	1.08	-0.63	-1.36	-0.94	-0.80	0.36	0.98	0.71	2.15	-1.33	1767
1768	-1.94	0.00	0.0=	0.00	0.00	0.54	0.05	0.00		0.00	0 =0	0.70	1 7 7 00
1768		0.93		-0.09		0.54	0.65	0.33	-1.27	-0.37	0.70	0.72	1768
	1.19	0.09	0.85	100000	-0.21	-0.53	0.53	-0.06	0.48	-1.71	0.58	1.43	1769
1770	1.45	0.92	-1.12	* 1	-0.15	-0.34	0.02	1.20	1.59	0.19	0.06	2.01	1770
1771 1772	-0.50	-1.44	121000	-2.59	1.72	0.26	The second second	-1.01	0.04	0.89	0.69	1.68	1771
1772	0.11	0.21	0.68	-0.50	-1.11	1.19	0.57	0.36	0.83	2.68	2.36	1.16	1772
1	0.00	0.7					The state of	The same	300	1100		The state of	0.00
1773	3.38	-0.57	1.36	0.81	0.35	0.31	The state of the s	1.17	100	1.79	1.51	1.76	1773
1774	0.58	1.62	2.18	1.30	0.08	0.96	1.12	0.51		1.23	-1.84	-0.45	1774
1775	1.31	3.40	2.12	1.04	-0.12	2.19	0.78	0.88	1.84	1.25	-1.53	1.65	1775
1776	-4.40	1.20	1.99	1.45	-0.85	1.11	1.56	0.47	-0.01	1.31	0.46	0.05	1776
1777	-0.23	-1.57	1.14	-0.56	0.15	-0.19	-0.07	0.88	0.60	0.73	1.97	-0.60	1777
3860	7.00	7	0.7				15,00		2010	50 8		110.15	146.3
1778	-1.26	1	-0.55	0.36	0.71	0.43		0.54		-2.02	1.08	2.90	1778
1779	-0.28	2.55	1.79	1.21	0.61	The same of the same of	0.60	1.51	1.27	1.61	0.19	0.53	1779
1780	-1.54	-0.56	2.68	-0.78	1.07	-0.51	-0.25	2.04	1.08	1.03	-0.07	-1.09	1780

#### XC.

# Holland. — Zwanenburg (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

	100				De	grees of	Reaum	ur.				1000	
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	3200
1781	-0.97	1.18		1.23		2.47	1.04	1.56		0.75		-0.39	1781
1782	2.88	-1.88	-0.56	-1.11	-1.09	0.77	0.34	-0.54	0.50	-0.93	2000	-0.89	1782
1783	2.39	2.13	The second second	1.24	10730	0.92	2.75	0.93	0.44	0.73	175-2010	-2.74	1783
1784	-3.26	-3.01	-2.04	-2.16		0.15		1250000	0.94	-2.30	0.000	-1.60	1784
1785	-0.06	-2.34	-3.32	-1.54	-0.96	-0.46	-0.01	-0.59	1.14	0.40	0.41	-1.70	1785
					1000			ENV			KIE	1	
1786	0.35	-0.08	-3.19	0.44	-0.59	0.72	-1.80	-0.75	-1.55	-1.49	-3.59	-0.23	1786
1787	-0.23	1.24	1.82	-0.90	-1.11	-0.11	-0.82	-0.56					1787
1788	2.20	-0.42	-1.15	0.24	0.58	1.05	0.87	-0.66	0.30	0.33	-0.73	-6.23	1788
1789	-2.66	0.98	-3.65	-1.64	0.56	-0.65	-0.58	-0.07	-0.40	-1.13	-1.10	1.84	1789
1790	2.20	2.51	1.53	-2.00	0.89	-0.72	-1.76	-1.25	-1.73	-0.86	-1.71	0.89	1790
									. 1994				
					7					0.00	0 ==0	0	
1791	2.74	1.29	1.23		-1.21				-0.74			-0.53	1791
1792	1.06	-0.38	0.03		-1.11	-0.93	-0.07		-1.53	-1.13	-0.14	1.05	1792
1793	0.52	1.59	0.03		-1.61	-1.70	0.67	The Control of the Co	-1.68	0.98	-0.17	1.60	1793
1794	-0.21	2.09	2.58	PARTIE A TOTAL	-0.76	-0.43	1.52	-0.87	-1.14	-0.54	0.41	-2.08	1794
1795	-4.52	-1.53	-0.92	0.85	-1.88	-0.18	-2.29	-0.08	1.51	2.39	0.37	2.87	1795
A SECOND	13.54	Marie	134.6			MEX.						311.6	
1796	4.72	1.76	-0.99	1.00	-0.63	-0.50	-0.91	0.02	0.64	-0.80	-0.46	-2.07	1796
1797	0.84	0.52	the state of the s	0.81	0.52	-1.18	1.38	0.01	-0.78	-0.60	0.32	1.59	1797
1798	1.45	1.73	0.31	1.22	0.11		-0.05	0.36	0.19	0.68	211 412	-3.49	1798
1799	-2.11	-2.00	-1.77	-2.19	-1.68	-1.83	100000	-1.08	-0.72	-0.63	0.59	-3.54	1799
1800	-0.65	-1.76		2.08	1.85	-2.10		0.04	0.50	0.02	1.12	-0.46	1800
									JI TA				ticus time
(日東西)	Take				73.5			17.38				VIII-	Sign
1801	1.97	-0.59	1.61	0.26		-1.43	The Sale	0.32	0.45	1.16	0.53	0.47	1801
1802	-0.75	0.24	0.56	0.55	and the same of	-0.28	-1.69	1.08	0.03	1.15	0.54	1.19	1802
1803	-3.04	-2.29	0.00	2.06		-0.92	1.43	0.75	-1.11	0.06	0.29	0.43	1803
1804	3.30	0.13	-0.92	-0.84	1.35	0.26	0.03	-0.20	1.57	0.62	-1.79	-2.84	1804
1805	-1.22	-0.36	-0.07	-0.56	-2.16	-1.97	-1.18	0.05	1.47	-2.00	-1.69	0.94	1805
A STATE OF		No.			142		Sana.		IN.	Water.			
1806	3.14	1.58	0.25	-1.95	1.79	-0.52	0.13	0.67	1.41	0.23	2.52	4.12	1806
1807	2.36	1.74	100000			-0.17	1.64	2.53		HEAD LOOK	-0.15	0.84	1807
1808	1.19	0.07		-2.02	1000	-0.46	2.62	1.64	0.24	-1.35		-1.50	1808
1809				-2.53		-1.03	-0.47	0.09		-1.32		0.68	1809
1810	-1.94	-1.39	-0.36	-0.41	-1.76	1 1554 (653)	0.05	-0.07	0.05.10	-0.63	-0.03	1.06	1810
1			115	1117		NEW Y	1750			N.V.	1111		N. THOMAS
THE P		Aug	1150		THE PARTY OF	100			DIA.	120.0			
1811	-2.75	0.55	1.41	1.16		1.53		-0.30		2.40	1.80	1.05	1811
1812	0.81	1.20	-1.21	-2.48	0.16	17 TO THE RES	1000	-0.56	A CHILDREN		-2.11	-4.00	1812
1813	-0.84	1.53	0.16	0.04	0.85			-0.91		-1.32	-0.76		1813
1814	-3.33	-4.20	-2.89	1.27	-2.01	-1.86	Total Control	-0.66		-1.44	-0.17	0.17	1814
1815	-2.69	0.96	2.23	0.59	0.59	-0.08	-1.63	-0.77	-0.54	0.07	-0.97	-1.90	1815
1816	0.52	-1.64	-0.78	-0.28	-1.48	-2.28	-1.31	-1.85	-1.14	-0.12	-2.06	-0.45	1816
1817	2.36	2.31	3 17 7 700	-2.12	10000000		-0.83			-3.16	1.83		1817
1818		-0.40	1 700 100	-0.21		1.69		-0.64			110000	-1.22	1818

#### HOLLAND. - ZWANENBURG (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1819	° 1.47	° 1.04	0.68	0.84	0.91	0.50	0.56	° 1.12	0.55	-0.79	。 -1.18	° -2.18	1819
1820		-1.49	10000	0.72		1917,5455	-1.06				12.4	September 14 miles	1820
1821	11	The same of	-0.16	1.66	-1.24	-1.91	-1.81	-0.14	0.72	0.20	1.72	2.08	1821
1822	2.64	1.93	2.26	0.40	1.53	1.65	0.24	-0.19	-0.88	0.74	1.99	-2.95	1822
1823	-6.29	-0.94	0.11	-1.19	0.44	-1.88	-0.89	0.12	-0.37	-0.66	0.90	1.65	1823
			1			PA							With the
1824	2.30	0.20	_0 22	_0.78	-0.47	-0.40	-0.19	0.00	1.03	0.36	1.52	2.59	1824
1825	2.63		-1.42	0.43	0.12		-0.04	Manne .		1.04	1.03	1.70	1825
1826	-2.57	0.97			-0.59	1	1300 300	The state of		1.95			1826
1827		-3.83	1	0.93		-0.24		-0.55		100	-0.91	2.79	1827
1828		-0.75	1.05	0.43				-0.64	1122		-0.18	1.96	1828
			2.00										
1829	-3.35	-2.47	-1.43	-0.45	0.10	-0.37	-0.42	-1.35	-1.52	-0.43	-1.61	-5.77	1829
1830	-2.70	-4.01	0.50	0.75	0.13	-1.45	0.59	-1.17	-1.45	0.34	1.00	-1.80	1830
1831	-1.07	0.04	1.24	1.61	-0.10	-0.09	0.90	0.66	-0.14	3.16	0.66	1.72	1831
1832	-0.77	-1.34	-0.43	0.55	-1.49	-0.07	-1.74	-0.12	-0.64	0.48	-1.37	0.72	1832
1833	-2.12	1.33	-1.62	-0.68	2.22	0.92	-0.48	-2.08	-0.99	0.11	0.44	3.07	1833
1834	4.21	0.40	1.15	-0.87	1.31	0.87	1.80	1.00	0.86	0.68	-0.31	1.42	1834
1835	1.21	1.81	0.47	-0.76	-1.09	0.92	0.47	0.07	-0.22	-0.77	-1.44	-0.44	1835
	-				-		-		1007	17-11		-	
Means.	0.99	3.14	3.86	6.80	10.12	12.45	13.97	14.13	12.30	8.61	4.84	2.16	Mean

## XCI. ENGLAND. - LONDON.

-										-	150000			
179	4	-0.96	2.72	1.23	1.64	-0.99	-0.43	1.83	-0.38	-1.35	-0.61	0.36	-1.10	1794
179	5	-5.04	-2.08	-1.26	-0.23	-0.46	-1.98	-0.04	0.11	1.76	1.61	-0.88	2.46	1795
179	6	4.42	0.50	-1.00	1.10	-1.26	-1.00	-1.28	-0.51	1.23	-1.45	-0.97	-3.76	1796
179	7	-0.01	-1.44	-1.51	-0.45	-0.70	-1.56	0.62	-0.82	-0.97	-1.34	-0.44	0.93	1797
179	18	-3.44	-0.28	-0.12	1.41	0.44	1.31	-0.10	0.88	-0.11	0.09	-1.24	-2.39	1798
			-214	-1008				ROE.		124	ALB P	TOTAL		
1776		1.00	1 00		104	7.00	104	0.50	7.10	7.10	1.00	0.10	0.50	7800
179	9	-1.00	-1.05	-1.74	-1.94	-1.39	-1.34	-0.79	-1.40	-1.19	-1.02	0.13	-2.79	1799
180	00	0.59	-2.04	-1.70	1.14	0.66	-1.37	0.66	1.23	0.42	-0.86	-0.15	-0.24	1800
180	)1	1.64	-0.08	1.26	-0.35	-0.10	-0.09	-0.48	0.76	0.88	0.33	-1.08	-1.37	1801
180	)2	-1.21	0.11	-0.04	1.14	-1.50	-0.66	-2.20	1.74	0.49	0.23	-0.89	-0.56	1802
180	93	-0.92	-1.03	0.51	0.88	-1.12	-0.89	0.97	0.41	-1.77	-0.40	-0.31	0.98	1803
1					1450	114	1384	1100	- 26	1169	ALC:	Best	15.0	
180	14	3.39	-0.73	0.00	0.00	1 00	7.00		0.00	1.10	0.00	0.00	1 50	1004
1			7 5 6 1 6	0.00	-0.95	1.80	1.07	-0.57	-0.20	1.16	0.66	0.08	-1.52	1804
180	05	-0.52	0.04	0.34	-0.20	-1.38	-1.49	-0.89	0.60	1.15	-1.06	-1.17	0.08	1805
180	96	2.27	1.27	-0.23	-1.21	1.00	0.64	-0.06	0.38	0.16	0.54	2.11	3.64	1806
180	07	0.64	0.54	-1.80	-0.14	1.05	-0.34	1.07	1.36	-1.61	1.44	-1.60	-1.19	1807
180	08	0.64	-1.01	-1.80	-1.43	1.99	0.02	1.87	0.82	-0.55	-1.76	0.58	-1.32	1808
18	09	-0.11	2.36	0.65	-2.05	1.23	-0.38	-0.75	-1.09	-0.24	-0.08	-1.33	0.72	1809
										1				

### XCI.

## England. — London (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.   Jan.   Feb.   March.   April.   May.   June.   July.   Aug.   Sept.   Oct.   Nov.   Dec.   Year.		111111111111111111111111111111111111111		1771		De	grees or	Reaumu	11.					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1810		0.01	0.38	0.12		0.20							1810
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	The second second			S NAME OF THE OWNER, WHEN							7 (6.6)	Address of the last		A Company
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			and the same	1000000	The state of the state of			N. S. Control of the	0.2020/55/	IN PARTIES.	Sandan .	Control of the last	130000	Toronto and
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							The section of				100000000	State of the Control	Property and the	The second second
1815	1 Commence	1	-000	Land Street		The state of the s	1000000	The second second	March 2017		The second second	The state of the state of		The second second second
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.00			-						DE GY			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		-				1100	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		morn	4				Sens
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Listania de la composición della composición del			THE ALL		Committee of	W201001			1000		the state of the s		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	and the same of th			7 1 1 1 1 1 1		20 00	1000		712000000000	Total Design	Parket Age 1	Laborate Street		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	March Street, St.	The second of		The state of		The State of the S			The same of the same of	The same of the same of	The state of the last of		Contract to	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	the Country of	THE PARTY OF		100				Later Later		A . The state of		Donney.	THE WAR	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1819	2.29	0.85	1.36	1.37	0.88	-0.69	0.36	1.58	0.70	3.08	-0.75	-C.74	1819
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			2 .09	17.6			Property.	U.S.	77.6	010	S.L.	9/50	199	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1820	-1.44	-0.66	0.25	1.68	-0.01	-0.74	-0.71	-1.18	-0.99	-0.96	-0.22	0.59	1820
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	A 44 CHAIN	J. St. 184 .		The second	Date of the Party	12mm (2mm / 1951 / 10	Contract of the	Sept. 18.	Lucian Library	1410 W	1. 7. N. W.		The State of the last of the l
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	V ALCOHOL .	Samuel Co.	THE STREET	A 10 Mar.		Livery Dr.	731-10 PL-	1400000	There's May		100 20	The Plant	A 100 CO.	A CONTRACTOR OF THE PARTY OF TH
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			0.19					0.14	0.78	0.39	-0.56	0.54	0.55	1823
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	0.78	2.41	-0.73	-0.94	-1.48	-1.40	0.00	-0.29	0.48	-0.03	1.38	1.08	1824
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		WILE T		HELVI.				THE REAL PROPERTY.				52,706	1020-75	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1000	100						1000	0.00		0.00	001	0.70	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	The same of	17/20 55-04		100 St. 100 Land		0. T. D. S. B.		19800 100	The Mary Street	10 May 1-17 Co.	ARRY CL.	330-01-00-1	1 200 100	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										Self Self				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1000000			1			I Talendaria	100000				1000000	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					200	O TO SHEET TO A	10 Table 10	The same of the sa				177		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1829	-1.76	-0.24	-1.08	-0.85	0.50	0.35	-0.48	-1.22	-1.41	-1.16	-1.60	-3.14	1829
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						THE ST					91-1-1		ELLIN D	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1830	-2.31	-2.17	1.98	1.15	-1.39	-1.09	0.65	-1.09	-1.37	0.32	0.63	-2.12	1830
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								1.49	1.29	-0.04	2.39	-0.08	1.21	1831
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1832	0.13	-0.86	-0.42	0.35	-0.70	0.57	-0.20	0.18	-0.06	0.52	0.47	1.08	1832
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1833	-0.64	1.45	-1.68	-0.10	2.72	0.66	-0.13	-1.31	-1.41	0.24	0.16	2.21	1833
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1834	3.73	0.48	1.16	-0.48	1.59	1.20	1.29	0.76	0.70	0.10	0.45	0.35	1834
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Y											337 1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1005	0.00	0.07	0.00	0.00	0.30	0.00	0.00	1 00	0.97	0.00	0.00	1 00	1005
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	No. of the last of			A.A. Taranta						140 - 3000		100000000000000000000000000000000000000	1000	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	St.								1					The Particular Control
1840     1.27     -0.50     -1.97     -0.01     0.14     1.02     -0.77     0.73     -1.10     -1.32     0.60     -2.41     1840       1841     -0.38     -1.41     2.58     0.61     2.08     2.17     -1.02     -0.02     0.16     -0.01     0.40     1.06     1841       1842     -1.02     0.81     1.47     -0.43     0.59     2.84     0.18     2.11     0.19     -1.70     0.36     2.50     1842	2 / 7 / Mar 27 1			COLUMN TO STATE OF THE PARTY OF	The state of the s				A CONTRACTOR				C	CONTRACTOR OF THE
1840				The state of					1					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1839	0.73	0.14	-1.08	-2.48	-1.24	0.06	U.50	0.73	-1.00	-0.52	0.07	-0.21	1839
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	A STATE OF			1200	1			10/20		1000		1112		
1842 -1.02 0.81 1.47 -0.43 0.59 2.84 0.18 2.11 0.19 -1.70 0.36 2.50 1842	1840			-1.97	-0.01	0.14	1.02	-0.77	0.73	-1.10	-1.32	0.60	-2.41	1840
1842 -1.02 0.81 1.47 -0.43 0.59 2.84 0.18 2.11 0.19 -1.70 0.36 2.50 1842	1841	-0.38	-1.41	2.58	0.61	2.08	2.17	-1.02	-0.02	0.16	-0.01	0.40	1.06	1841
Means. 2.38 3.81 5.00 7.30 10.46 12.92 14.26 14.07 12.06 8.88 5.51 3.81 Means.	1842			1.47	-0.43	0.59	2.84	0.18	2.11	0.19	-1.70	0.36	2.50	1842
Means. 2.38 3.81 5.00 7.30 10.46 12.92 14.26 14.07 12.06 8.88 5.51 3.81 Means.	Manne		-		1000						-			Mann
	Means.	2.38	3.81	5.00	7.30	10.46	12.92	14.26	14.07	12.06	8.88	5.51	3.81	Means.
			11.7			1								
					134	TEN V		100	THE P				184 T.C.	
					Table 1						Teeter.	585	TATA	
			1		VA-74			1000	10 10	1000		818		

### XCII.

### SCOTLAND. - KINFAUNS CASTLE.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

	The same				-	De	egrees of	Reaum	ur.		Marie Co			
	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	1814	0 -4.71	° -1.63	° -1.73	0.56	° -2.46	° -2.36	-0.60	。 -1.12	° -0.34	° -1.16	° -1.61	° -1.46	1814
	1815	-1.69	1.13	0.16	-0.03	0.95	0.24	-0.12	0.23	0.27	0.74	1000	-2.47	1815
	1816	-0.24	-1.60	-1.49	-1.58	-0.74			-0.53	-0.99	-0.24	-1.12		1816
	1817	1.60	1.29	-0.44	0.33	-1.12	0.80		-1.11	0.18	-2.22	1.78	-1.38	1817
	1818	0.51	-1.03	-1.41	-1.59	1.03	1.43	0.85	-0.22	-0.15	2.34	2.54	0.25	1818
	1819	0.85	-0.88	0.67	-0.20	-0.36		0.07	2.00	0.30	-0.32	-2.35	-2.60	1819
	1820	-2.43	0.95	0.33	1.10	0.20		0.39	-0.26	-0.36	-1.20	0.15	0.36	1820
	1821	0.55	0.97	0.26	1.12	-1.09		-0.01	0.84	1.44	0.83	0.38	0.73	1821
	1822	1.85	1.28	1.08	0.79	0.97		0.50	0.26	-0.81	0.48	1.38	-0.61	1822
	1823	-0.91	-1.69	-0.16	-0.60	0.63		-0.92	-0.85		-0.56	2.02	-0.04	1823
	1824	2.64	1.20	-0.56	0.39	0.18	0.26	0.43	0.03	0.24	-2.16		0.35	1824
	1825	1.94	0.84	0.45	0.82	-0.09	0.31	1.59	1.53	1.85	1.79		0.80	1825
	1827	0.68	-0.77	0.02	0.73	0.51	0.38	0.16	0.37	1.48	2.48	HACT'S	2.23	1827
	1828 1829	2.50 -0.38	1.44 0.96	1.63 0.42	0.69 $-0.48$	1.20 0.87	1.23 1.00	0.93 -0.12	1.03 -0.44	1.23 -1.02	1.10 0.34		2.73 0.02	1828 1829
	1830	0.40	-0.22	2.07	0.87	0.60	-0.63	0.50	-1.13	0.11	1.33	0.92	-0.89	1830
	1832	1.91	1.27	0.92	1.22	-0.19	0.50	0.30	0.93	1.35	1.53	-0.56	0.40	1832
	1833	-1.40	0.51	-0.41	0.32	2.79		377	-0.98	-0.24	0.53	0.12	0.40	1833
	1834	2.23	0.97	1.05	100000000000000000000000000000000000000	1.01	0.59	0.67	0.34	0.24	-	0.12	4 4 4 4 4	1834
				100000000000000000000000000000000000000	0.51		0.53	0.93	12000	1/04/9/04	0.49	THE PLANT	0.57	6500
	1835 1836	0.59	0.72 -0.67	-0.08 -0.70	0.23 -0.81	-0.58 0.10	0.20 -0.54	-0.17	1.09 -1.09	-0.10 $-1.67$	-1.10 -0.86	-0.31 $-0.94$	-0.34 -0.05	1835 1836
	1837	-0.07	0.20	-2.26	-0.81 $-2.35$	F 1 2 2 2 2 2 2	-0.04 -0.05	-1.16 $0.52$	-1.09	100	0.23		1.74	1837
	1838	-2.58	-4.61	-2.20 $-0.83$	-2.55 $-1.44$	ATT OF			-0.24	-0.53	-0.55	2.73	0.48	1838
	1839	-0.90	-0.79	-0.53 $-1.56$		-1.18	-1.03	-0.04 $-0.34$	-0.24 $-0.79$	-0.64		0.11	-0.35	1839
	1840	0.65	-0.19 $-0.26$	-0.07	-1.24 $1.00$	400 -03		-0.34 $-1.30$	0.21	-1.29	-0.17 $-0.63$	-0.17	-0.58	1840
	1841	-2.19	-0.09	2.25	-0.28	0.51	-1.07	-0.83	-0.20	0.51	-1.52	-1.94	-0.49	1841
	1842	-1.17	0.49	0.35	-0.07	0.48		-0.83	1.24	0.32	-1.52	-0.81	1.81	1842
	Means.	1.77	2.74	3.87	5.71	8.13	10.58	11.76	11.28	9.52	6.72	4.35	2.96	Means.
	71				TOTAL				m	0			NATE:	
			11/4		XCII	l. F	INLAN	ID. —	Torn	VEA.	Prys			
	1801							(i.e.	1.4	.,.		-0.01	-1.67	1801
	1802	-0.57	-0.17	-0.15	0.10	-2.88	-0.66	-2.03	-1.60		1.30	N. S. C. C. C.	-4.06	1802
	1803	100000	-0.90	-0.13	1.57	1.69		-0.58		-0.90	1.18	0.71	-3.67	1803
	1804	-2.50	-4.82	-2.34	1.99	1.50	-0.97	0.78	-0.70	-0.21	1.19	1.46	-4.01	1804
	1805	13.00	-2.94	-1.15	-0.79	DECEMBER 1	-2.90	2000	0.62		-4.62	I TOTAL		1805
1	1806	2.91	1.91	-0.03	2.02	1.00	-1.18	-1.90	2.00	1.20	0.13	-0.97	0.74	1806
1	1807	-3.40	1.94	-1.25	-2.57	-1.93	-0.61	0.34	0.89	-1.41	-2.30	-0.20	-0.92	1807
	1808	1.80	100	0.19	-2.31	1.14	2.65	0.58	-0.11	-0.51	3.53	2.24	-3.74	1808
	1809	-7.19	Are the	-2.74	-3.78	-1.91	1777	-0.50	12.700 6.75	-0.34	-0.25	- 17 7 6 7	8.07	1809
	1810	-2.18	-2.36	-2.41	-2.45	-6.45	WELL A	-2.13	11 7 5	-1.34	-1.23	-4.13	-2.20	1810
	1811	2.98	-2.74	3.64	-2.04	-0.69	0.42	-0.91	-2.66	-1.05	-1.90	T-4.505 TH	-2.06	1811
	1812	1.18	1.85		-1.39	0.55		-2.53	-1.20	2 420 4		-4.18	100000000000000000000000000000000000000	1812
	1813	1.32	1.15	1.70	1.88	-0.71	-1.58	1.87	0.08	1.88	-2.89	3.65	-1.43	1813

## XCIII.

## FINLAND. - TORNEA (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.   Jan.   Feb.   March   April.   May.   June.   July.   Aug.   Sept.   Oct.   Nov.   Dec.   Year.
1814
1815
1816
1817
1818
1819
1820
1821
1822
1823
1824
1825
1826
1827
1828
1829
1830
1830
1832   5.26   8.25   3.64   2.92   0.10   0.51   -1.11   -1.22   -3.67   2.86     1832
Means   -12.55   -10.76   -7.19   -1.62   4.01   10.59   13.05   10.81   6.22   0.26   -6.27   -10.32   Means
XCIV. North America. — Albany, N. Y.  Degrees of Reaumur.  1826   1.92   2.44   1.65   -1.02   3.23   1.07   0.72   1.09   1.57   1.46   0.81   0.35   1826   1827   -2.91   1.07   1.15   1.62   -0.02   0.05   0.55   0.08   0.43   1.14   -1.72   0.77   1827   1828   2.80   4.52   2.10   -0.88   0.76   2.66   -0.41   1.33   0.35   -0.31   0.76   3.17   1828
Degrees of Resumur.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$
1 1000   0 01 0 01 0 10 0 10 0 0 0 1 11 0 0 0 0
1829   -0.21   -2.27   -0.87   0.12   2.09   0.03   -1.54   -0.42   -1.93   0.92   0.50   3.63   1829
1830   0.28   -0.11   1.41   3.64   -0.21   -0.92   0.81   0.27   0.19   1.42   3.83   4.71   1830
1831  -1.30  -1.03   2.77   1.89   1.07   2.11   0.32   1.01   1.00   1.52   0.63   -4.94   1831
1832   0.18   -0.87   0.16   -1.29   -1.35   0.19   -0.34   -0.31   0.53   0.67   1.15   0.76   1832
1833   2.34   -1.34   -1.15   1.75   1.55   -2.35   -1.06   -1.47   -0.55   -0.55   -0.61   0.18   1833
1834   -1.18   3.73   0.67   0.68   -0.05   -1.12   1.59   -0.03   0.27   -1.31   -0.36   -1.13   1834
1835   -1.06   -1.50   -0.98   -1.59   -0.57   -0.34   -0.43   -0.90   -2.14   1.45   0.31   -3.06   1835
1836   -0.35   -3.89   -3.48   -2.27   -0.95   -1.30   0.20   -2.39   -0.39   -3.06   -0.62   -0.92   1836
1837   -3.40   -0.72   -1.94   -2.02   -1.23   0.07   -0.95   -0.98   -0.60   -0.89   0.33   -0.49   1837
1838   3.34   -4.01   0.97   -3.07   -1.26   1.78   0.31   0.27   0.36   -0.68   -1.47   -2.11   1838
1839   -0.25   1.62   0.14   0.79   -0.79   -1.79   0.15   -0.14   0.41   0.99   -0.94   -0.19   1839
1840   -3.32   3.14   0.60   1.32   0.96   -0.14   0.94   0.81   -0.91   0.28   0.28   -1.26   1840
1841   1.95   -0.72   -1.19   -2.58   -1.13   1.90   0.   1.23   0.88   -1.72   -0.49   0.86   1841
1842 2.03 3.15 2.06 0.62 -1.96 -0.98 0.28 0.13 -1.09 -0.12 -1.00 -1.69 1842
1843   2.65   -3.06   -4.26   -0.62   -0.62   -0.64   -0.55   0.64   0.85   -1.24   -1.11   0.93   1843
1844   -3.74   -0.15   0.27   2.97   0.47   -0.29   -0.60   -0.19   0.72   0.02   -0.20   0.47   1844
Means3.58 -3.08 1.28 7.04 12.33 16.02 17.80 16.86 13.06 7.64 2.70 -1.65 Means

### XCV.

### NORTH AMERICA. - SALEM, MASS.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.   Jan.   Feb.   March   April   May.   June.   July.   Aug.   Sept.   Oct.   Nov.   Dec.   Year.	-	No.					D	egrees of	Reaum	ur.	31.55 %				
1787		Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.	Year.
1788			0	0		0		0	0	0	0	0	0	0	
1789		1787	0.40					10000	-1.53	-0.28	-1.13	-1.00	0.58	0.07	1787
1790		1788	-1.38	-2.15	-0.32	-0.47	11/1/10/10	-1.39	0.14	-0.17	0.87	-1.00	2.03	-1.60	1788
1791		1789	0.17	-2.81	100	100 000		A. P. S. S. S.	-0.31	0.05	-0.47	-2.56	0.47	1.18	1789
1792		1790	1.17	-1.04	-1.32	-1.47	-0.50	-0.50	-0.75	-1.50	-1.02	-0.56	-0.97	-2.82	1790
1793		1791	0.17	-1.48	0.90	.0.64	1.50	1.16	-0.08	0.16	-0.69	-2.23	-0.42	0.07	1791
1793		7800	004	0.00	7 70	0.00	7 07	004	0.04	0.00	1 00		0.00	1 10	7800
1794		HIELD IN			100		100000				YORK MA			100	The second second
1795					1						Control of				
1796						0.5		-						0.3000	The second second
1797	ı							14 0 1		of Section 1	1	HERE SALES	A Common	2000	
1798		1790	1.10	0.12	-0.57	1.17	-0.11	0.40	0.59	0.80	-0.06	-0.55	-1.20	-3.02	1790
1798		1797	-1.15	2.24	0.55	-0.26	-1.25	0.41	1.40	-0.45	-0.64	-0.83	-1.72	-2.52	1797
1799			11		L LODGE	100011							A CONTRACTOR	1 3 San 1995	
1800															The state of the s
1801				2007	1 2 3 3 5	The state of	1000000		100 15 17		1		100000	1000	The state of the
1802   3.79   -0.16   0.76   0.31   -1.34   0.13   0.13   0.88   1.19   1.87   1.23   1.19   1803   1.804   -0.48   0.08   -0.48   -0.98   1.55   0.20   -0.25   -0.44   0.28   -1.05   0.16   -1.76   1804   1805   -1.46   1.02   1.92   1.45   0.91   0.11   1.40   0.82   1.23   -0.52   0.13   3.24   1805   1806   0.48   1.60   -1.83   -2.28   -0.44   -0.19   -1.12   -0.77   -0.52   -0.44   0.15   -0.06   1806   1807   -1.05   -1.13   -1.30   -0.31   -0.80   -0.62   0.05   0.00   -1.08   0.22   -0.65   2.45   1807   1808   0.13   1.41   1.55   0.37   -0.74   0.04   -0.15   -0.86   0.54   -0.72   0.69   0.72   1808   1809   -1.15   -1.73   -1.36   0.31   -0.24   -0.42   -1.90   -0.76   -0.95   3.00   -2.19   2.04   1809   1810   0.11   0.95   -0.68   0.70   0.84   0.04   -0.93   -0.39   0.46   -0.12   -0.24   -0.34   1811   1812   -1.51   -1.16   -2.68   -1.05   -3.22   -2.04   -2.13   -1.64   -2.07   -0.30   -0.90   -0.73   1812   1813   -1.09   -0.34   -2.55   0.08   -1.46   -0.95   -1.17   0.44   1.02   -0.62   0.83   -0.70   1813   1814   -0.73   0.80   -0.51   1.08   0.76   -1.58   -0.30   -0.94   -0.57   -0.07   0.39   -1.78   1814   1815   -0.93   -1.98   0.28   -1.47   -1.49   -0.16   1.12   -1.82   -0.50   -0.69   1.07   -0.45   1815   1816   -0.16   0.07   -2.14   -0.44   -1.36   -2.36   -2.49   -1.31   -1.77   0.17   1.79   0.31   1816   1817   -0.71   -3.48   -1.43   -0.73   -0.44   -1.65   -0.52   -0.76   0.18   -0.70   0.78   0.86   1817   1818   -0.51   -3.56   0.14   -2.31   -0.42   1.17   0.85   -0.01   -0.84   0.61   1.92   -1.94   1818   1820   -1.51   1.00   -0.22   -0.07   -0.23   0.51   1.95   0.26   1.52   -0.17   -0.98   -2.49   1820   1.821   -2.75   1.50   -0.80   -0.97   -0.37   0.36   -1.08   0.83   -0.11   -0.05   0.42   -1.31   1821   1822   -1.60   -0.50   1.64   -0.87   1.77   0.09   0.44   0.06   1.84   0.75   0.96   0.12   1822   1823   0.37   -1.99   0.99   0.20   -1.19   -0.42   -0.19   0.35   -1.63   -0.58   -1.72   0.52   1823   1824   2.28   0.47   -0.11   0.62   -0.84   -0.		1801	0.40	0.46	1.51	at the last	The same of	- TH SOLE !	1000		1	- 11 11 -	- 100000	345 100	
1803					16-1-3	on no			in the same				-115		
1804		THE RESERVE	1 1 1 1 1 1 1	the second	THE PROPERTY.		100 P 100	The state of the s		110 4 71	C. P. C.	100			
1805		Committee of the			100,700	- Str. Brown	DESCRIPTION OF	9 30 100 1	50 LT-1	100000000000000000000000000000000000000		YELDSII.		77 20 200	The second of the
1806						POST-OFFICIAL	100000000000000000000000000000000000000	C SO BOAR		N 10-0795 A D		M 350 4 MOTE 1		- XX 105.11	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	000000000000000000000000000000000000000		The second					CANADA I	DATE TO SERVICE			1.000		
1808		1806	0.48	1.60	-1.83	<b>-2.2</b> 8	-0.44	-0.19	-1.12	-0.77	-0.52	-0.04	0.15	-0.06	1806
1808	1	1807	-1.05	-1.13	-1.30	-0.31	-0.80	-0.62	0.05	0.00	-1.08	0.22	-0.65	2.45	1807
1809		0		25				1.111-0.00	L 173 4092 11						
1810					F 1 ( 5 F 1)	7 17.51	1.11	12/20/20/20	LOSSIC PA	27 0	11/11/01	W 25 / 2 m			
1811					CONTRACTOR OF THE PARTY OF THE		100	16.90,90		35	100		70000		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1811	0.30	0.14	1.69	4	1113-113			-	77 675				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			1				2.7	51.3		1000		STATE	1	1000	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		ALCOHOL: NO		SEC. 531	The Street	00311		TO STAR		11/2/2017	CONT. PORT		COLUMN TO STATE OF THE PARTY OF	1118	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				DPL (SCA)	O D. HOLD	235,596	SALITHMAN	S. P. C. T. Street	125 47	4452, 17	The state of	TTOTAL	1000	7.12	
1816		COST TO THE		T. A	0.570 870	2530,43274	40.00	1.05 .5311.	1.71 .27.00	12. T. J. Liber	20-10-	A STATE OF THE PARTY OF	DE SYSTEM		10. 10.000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-														
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1816	-0.16	0.07	-2.14	-0.44	-1.36	-2.36	-2.49	-1.31	-1.77	0.17	1.79	0.31	1816
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1817	-0.71	-3.48	-1.43	-0.73	-0.44	-1.65	-0.52	-0.76	0.18	-0.70	0.78	0.68	1817
1819		A ELASTIC P			77,1	the transfer of the same of	ALTERNATION OF			CO. 07. 1	C-1346.	ALC: LABOR TO	W-000-00	27/12/1	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-	A COLUMN				1967	11.73(1).73(1)	CEXC		110/00/07	1372-1231	3-18+30.5	31.5.57	D 30/3.77	500607000
1821		1820	-1.51	1000	00000	0.1512.46	0.750, 3.225	0.733.55	000-025	430000	200	E-813/5/200		1000	100000000000000000000000000000000000000
1822     -1.60     -0.50     1.64     -0.87     1.77     0.09     0.44     0.06     1.84     0.75     0.96     0.12     1822       1823     0.37     -1.99     -0.99     0.20     -1.19     -0.42     -0.19     0.35     -1.63     -0.58     -1.72     0.52     1823       1824     2.28     0.47     -0.11     0.62     -0.84     -0.59     -0.14     -1.08     0.12     0.21     -0.61     1.43     1824       1825     1.30     1.27     2.16     1.49     0.69     1.74     2.36     -0.12     -1.05     0.70     -0.14     0.62     1825       1826     0.96     1.11     0.10     -1.05     2.95     0.04     1.56     -0.13     0.78     0.23     0.19     0.55     1826       1827     -1.49     0.52     0.64     1.56     -0.03     -0.60     -0.35     -0.82     -0.28     1.13     -2.74     0.01     1827       1828     2.42     4.05     1.10     -0.97     -0.68     1.06     0.36     0.96     0.37     -0.19     1.17     2.04     1828		1821	-2.75					Service Co. To.	100000	1 march 1	Section Co.	0.00	77 - 6 VIII	Section 1971	
1823     0.37     -1.99     -0.99     0.20     -1.19     -0.42     -0.19     0.35     -1.63     -0.58     -1.72     0.52     1823       1824     2.28     0.47     -0.11     0.62     -0.84     -0.59     -0.14     -1.08     0.12     0.21     -0.61     1.43     1824       1825     1.30     1.27     2.16     1.49     0.69     1.74     2.36     -0.12     -1.05     0.70     -0.14     0.62     1825       1826     0.96     1.11     0.10     -1.05     2.95     0.04     1.56     -0.13     0.78     0.23     0.19     0.55     1826       1827     -1.49     0.52     0.64     1.56     -0.03     -0.60     -0.35     -0.82     -0.28     1.13     -2.74     0.01     1827       1828     2.42     4.05     1.10     -0.97     -0.68     1.06     0.36     0.96     0.37     -0.19     1.17     2.04     1828		1000	1 00	0.70	59 JIL.	0.0	DE AUT	06,56	79.00	BULL -	EALALA	A HELL	12.94	DE THE	045811
1824     2.28     0.47     -0.11     0.62     -0.84     -0.59     -0.14     -1.08     0.12     0.21     -0.61     1.43     1824       1825     1.30     1.27     2.16     1.49     0.69     1.74     2.36     -0.12     -1.05     0.70     -0.14     0.62     1825       1826     0.96     1.11     0.10     -1.05     2.95     0.04     1.56     -0.13     0.78     0.23     0.19     0.55     1826       1827     -1.49     0.52     0.64     1.56     -0.03     -0.60     -0.35     -0.82     -0.28     1.13     -2.74     0.01     1827       1828     2.42     4.05     1.10     -0.97     -0.68     1.06     0.36     0.96     0.37     -0.19     1.17     2.04					414 7 17 77	140047073113	TATE OF THE PARTY OF		100000	2354 F.	P. 10 C. 10	4.44444	9 34 9 3	10000	
1825     1.30     1.27     2.16     1.49     0.69     1.74     2.36     -0.12     -1.05     0.70     -0.14     0.62     1825       1826     0.96     1.11     0.10     -1.05     2.95     0.04     1.56     -0.13     0.78     0.23     0.19     0.55     1826       1827     -1.49     0.52     0.64     1.56     -0.03     -0.60     -0.35     -0.82     -0.28     1.13     -2.74     0.01     1827       1828     2.42     4.05     1.10     -0.97     -0.68     1.06     0.36     0.96     0.37     -0.19     1.17     2.04     1828		A BESTALL - D	N.J. H.L.		TH-10	A 22 - 12 - 1	N. W. P. S.	- N J. C.	A 1 3 3 - 1	1273 200	111111111111111111111111111111111111111	200	1-1-3-1	276 12	
1826     0.96     1.11     0.10     -1.05     2.95     0.04     1.56     -0.13     0.78     0.23     0.19     0.55     1826       1827     -1.49     0.52     0.64     1.56     -0.03     -0.60     -0.35     -0.82     -0.28     1.13     -2.74     0.01     1827       1828     2.42     4.05     1.10     -0.97     -0.68     1.06     0.36     0.96     0.37     -0.19     1.17     2.04       Moore		POPPER DE LA	The state of		1500000	0.00	7.7035	3 (45470.77)	SECRETARY 21	100000000000000000000000000000000000000	THE REAL PROPERTY.	DUNEST	- NO. W.	1 CONTROL	1 1 1 1 1 1 1 1 1
1827		Mary Police To a					ALCOHOL: NO. 1	-/ 200	100 100	Allen days	Contract of the	the second second	Also study	20.20	The same of the sa
1828 2.42 4.05 1.10 -0.97 -0.68 1.06 0.36 0.96 0.37 -0.19 1.17 2.04 1828		1020	. 0.50	1.11	0.10	-1.05	2.95	0.04	1.56	-0.13	0.78	0.23	0.19	0.55	1820
1828 2.42 4.05 1.10 -0.97 -0.68 1.06 0.36 0.96 0.37 -0.19 1.17 2.04 1828	1	1827	-1.49	0.52	0.64	1.56	-0.03	-0.60	-0.35	-0.82	-0.28	1.13	-2.74	0.01	1827
Means2.84 -1.85 1.54 6.36 11.05 15.61 17.97 17.17 13.80 8.56 3.53 -0.63 Means.		1828	2.42	4.05	1.10		TO TO A COLUMN	1000	70 ISIN	The state of the same	12 To 10 To	Larray Fred	27774	The second second	
-2.84   -1.85   1.54   6.36   11.05   15.61   17.97   17.17   13.80   8.56   3.53   -0.63   Means.		Means	0.01	7.05											Maria
		means.	-z.84	-1.85	1.54	6.36	11.05	15.61	17.97	17.17	13.80	8.56	3.53	-0.63	Means.

#### XCVI.

### ICELAND. — REIKIAVIK.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
0	0	0	0	0	0	0	0	0	0	0	0	
1.80	-0.56	0.40	2.09	-0.60	0.06	2.44	1.76	0.84	-1.50	0.18	-0.86	1823
-0.32	0.61	-0.05	2.16	2.95	4.63	3.12	1.53	-0.73	-2.37	-3.64	-3.99	1824
-1.07	-0.40	3.04	0.98	0.50	0.33	1.70	0.66	2.34	1.68	-0.81	-0.92	1825
-0.19	2.84	2.15	-0.79	1.58	-1.10	-0.75	-0.18	1.24	1.12	0.36	1.17	1826
-0.72	1.93	-3.80	-0.86	0.67	0.86	0.14	1.73	0.64	2.29	2.26	0.88	1827
		TO DW									EVIN	
1.98	2.48	1.54	1.29	2.37	0.53	3.15	3.98	3.07	3.26	0.94	2.77	1828
1.02	-0.09	0.20	0.56	0.79	0.26	1.21	2.21	-0.20	-1.16	0.03	1.86	1829
1.89	-0.58	-1.22	-0.72	2.44	0.52	-0.80	10 10 10 10 10 10 10 10 10 10 10 10 10 1		2.09	-0.35	-2.60	1830
0.28	-0.95	2.58	1.39						0.95	-0.76	1.45	1831
1	11.00		100		1000					10000		
					DAY OF					-	Land.	
	3 3	12.50	Topic.	de di	mega				95 / 34		Sugration of	1832
1.41	-0.13	1.93	-0.21	-0.57	-0.40	-1.96	-2.14	-1.22	-0.79	0.31	-1.64	1833
-0.43	0.10	0.73	0.14	-1.35	-1.99	-1.81	-2.41	-1.44	-1.13	0.22	2.76	1834
-4.08	-1.92	-1.55	-1.32	-2.35	-1.97	-1.62	-0.38	-0.64	-2.41	1.58	1.30	1835
-1.86	-3.24	-2.00	-3.01	-0.37	-0.94	-0.59	-2.68	-1.80	-1.67	-1.52	-1.95	1836
-0.42	0.43	-2.23	-1.91	-2.07	-0.32	0.40						1837
-1.00	-1.60	-1.07	1.84	5.54	8.67	10.78	9.27	6.42	2.19	-0.60	-1.15	Means.
	1.80 -0.32 -1.07 -0.19 -0.72 1.98 1.02 1.89 0.28 0.71 1.41 -0.43 -4.08 -1.86 -0.42	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					

## XCVII. GREENLAND. — GODTHAAB.

							- X						
1796			*							-2.52	1.51	2.19	1796
1797	0.91	-2.08	-0.73	-1.96	1.14	0.27	1.40	1.31	0.77	1.02	2.22	0.87	1797
1798	-1.30	0.53	3.98	0.08	0.37	-0.39	0.39	0.07	-0.37	-0.67	0.83	-0.08	1798
1799	-0.40	3.08	-1.87	0.47	0.37	-0.71	-0.47	-0.72	0.62	-0.43	-0.91	4.72	1799
1800	2.75	0.22	2.32	-0.68	1.52	1.05	0.35	0.88	-0.42	0.48	0.05	0.07	1800
1801	-0.86	2.63	0.00	-1.00	-2.86	-1.61	0.89	0.92	-0.39	0.19	0.22	1.94	1801
1802	1.85	-2.99		-2.68						all to			1802
1816							0.09	-0.98	-0.12	-0.15	-0.01	100000000000000000000000000000000000000	1816
1817	-1.55	-2.46	-4.17	0.37	-1.32	-0.79	-1.63	-0.28	-0.41	-1.65	-0.52	-1.73	1817
1818	-5.58	-5.13	-4.00	2.56	-0.90	-0.84	0.52	0.15	-0.71	-1.97	-1.82	-0.42	1818
		444	711	1.11					1448		W. Bl		
1819	-2.74	0.94	-0.35	0.98	000000000000000000000000000000000000000	1	-3.78	-2.29	-2.30	1.78	1.38	3.15	1819
1820	4.16	0.14	0.35	-2.15	0.97	0.66	-0.96	-1.57	-0.72	-0.06	1.60	1.19	1820
1821	0.04	0.42	1.30	1.00	-0.07	0.68							1821
1841									0.45	0.14	-0.27	0.23	1841
1842	1.13	-1.15	-1.12	1.56	2.03	0.37	0.89	0.34	1.39	1.95	-0.37	-1.37	1842
1843	0.11	4.74	4.65	2.18	1.18	1.16	1.52	0.72	1.57	1.66	-2.89	-3.93	1843
1844	-0.13		-0.51		-1.29	0.79	0.78			1000	-1.08		1844
1845	1.54	0.76	3.98		1000	0.32		4.	• •	• •	-1.00		1845
Means.	-8.72	-8.64	-7.29	-4.44	0.07	3.15	4.41	3.93	1.62	-0.96	-4.47	-6.45	Means.

II Separate										Es.	
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		がある。		(日本)							

## CORRECTIONS

FOR

## FORCE OF VAPOR AND RELATIVE HUMIDITY.

## HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OR

### TABLES

FOR REDUCING THE MEANS OF THE OBSERVATIONS TAKEN AT ANY HOUR OF THE DAY TO THE TRUE MEAN FORCE OF VAPOR AND RELATIVE HUMIDITY OF THE DAY, OF THE MONTH, AND OF THE YEAR.

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HOERIN CORRECTIONS FOR PERSONS VARIATIONS,

## au Iur

#### XCVIII.

England. - Greenwich. Lat. 51° 29' N.; Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours, to obtain the true Mean Force of Vapor for the respective Months. (GLAISHER.)

English Inches.

Hours. Jan. Feb. March. April. May. June. July. Aug. Sept. Oct. Nov.	-   - 15
Total April 12091 Suite Suit Suite S	Dec. Mean
Inch.	Inch. Inch.
Midn006 .006 .008 .017 .026 .031 .028 .025 .024 .018 .010	.009 .01
1 .011 .008 .010 .021 .028 .037 .031 .031 .030 .020 .012	.010 .02
2 .015 .010 .011 .024 .031 .043 .036 .035 .035 .021 .015	.010 .02
3 .015 .011 .013 .027 .032 .048 .038 .039 .037 .023 .017	.011 .02
4 .015 .013 .015 .029 .031 .047 .037 .040 .040 .025 .019	.011 .02
5 .015 .014 .016 .029 .027 .037 .031 .038 .040 .023 .021	.011 .02
6 .014 .015 .016 .025 .019 .022 .019 .029 .033 .021 .021	.010 .02
7   .013   .014   .014   .016   .007   .008   .007   .014   .022   .018   .018	.009 .01
1010 1011 1011 1000 1001 1011 1011 1010	.000
8   .010   .010   .005  005  004  004   .000   .010   .011   .012	.007 .00
9 .007 .006 .005 .005016015014012005 .005 .005	.00500
10   .002   .000  003  013  024  027  019  021  019  005  004	.00101
THE STATE OF THE PROPERTY OF T	00401
11 .004003007020020030023027027003010	00-1
Noon  007  009  012  026  030  042  029  030  030  015  017   -	00702
1  008  013  013  027  030  045  033  032  030  018  019	
2  007  015  013  027  028  043  034  034  029  017  020	
1020 1020 1020 1020	00802
0007012020020030031027011010	00502.
4  007  010  010  020  021  035  028  027  021  009  010   -	00701
5  004  006  006  014  015  025  021  020  017  006  005   -	1
	00300
	001002
1001 1001 1001 1001 1001 1001 1001 1000 1000	.001
8 .000 .001 .004 .005 .005 .005 .004 .004 .004 .005 .006	.001 .004
9 .000 .003 .005 .007 .013 .015 .010 .010 .008 .008 .008	.004 .00
	.005 .011
	.006 .014
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6. 6   .006   .005   .007   .009   .005   .003   .001   .007   .012   .008   .010	.004 .006
7. 7   .006 .006 .008 .009 .001 .000 .000 .004 .009 .011 .011	.004 .003
	.004 .003
	Sealing Street
9. 9   .003 .004 .005 .006002 .000002001 .002 .006 .007	.004 .003
10.10   .001 .002 .002002003002001003003 .003 .002	.003 .000
	.002001
	111 532
6. 2. 8   .002 .000 .002 .001001005004000 .003 .003 .002	.001 .000
6. 2.10   .003 .001 .003 .003 .002 .001 .001 .003 .006 .005 .003	.002 .003
	.000003
7. 2   .003  000   .000  005  011  017  014  010  003   .000  001	.000008
8. 2   .001  002  001  011  017  023  019  017  009  003  004   -	.000009
	.000009
7. 1   .002   .000   .000  005  012  018  013  009  004  000  000	.000005
9.12.3.9  002  003  003  010  015  020  016  016  013  004  005	.001009

#### XCIX.

## England. - Greenwich. Lat. 51° 29' N.; Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours to obtain the true Mean *Humidity* for the respective Months. (GLAISHER.)

Thousandths.

1				120		housand	U119.	- 6					
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
				005				000	000	0.00	0-0	-	
Midn		1		095						122/10/10	1 10 10 10 10 10		
1	.002			106						Delta della	009	All Shirts of	100
2	.004	75		116		125			085				
3	003	033	067	123	113	132	116	117	091	070	020	019	075
4	013	036	068	126	114	138	120	123	097	075	030	024	080
5	019			125		139				077		024	
6	021	2000		112		107					033		
7		030		080		065		1		058			052
8	020	020	035	065	024	015	005	020	047	037	021	018	027
9	017	007	003	034	.018	.035	.041	.030	.000	009	008	007	.003
10	004	.009	.031	015	.051	.078	.080	.070	.042	.025	.008	.008	.032
11	.011	.028	.060	.022	.083	.100	.104	.102	.082	.060	.027	.022	.058
77				000						000	0.10		000
Noon	.031	.045	.084	.070	.110	.123	.114	.127	.115	.088	.040	.033	.082
1 2	.054	.058	.100	.132	.126	.137	.119	.142	.131	.109	.050	.046	.100
3	.059	.065	.106	.151	.125	.135	.123	.145	.132	.113	.054	.048	.105
	•040	.005	.104	.147	.110	.120	.121	.190	.120	.100	.041	.000	.090
4	.036	.053	.087	.128	.108	.113	.111	.120	.103	.089	.032	.024	.084
5	.021	.032	.063	.110	.091	.099	.095	.100	.071	.055	.018	.013	.064
6	.007	.009	.038	.088	.074	.078	.062	.071	.044	.030	.005	.004	.042
7	005	010	.010	.059	.052	.049	.025	.036	.009	.007	005	003	.019
	15 4.6				N TY								
8	014	023	010	.020	.022	1000	015				012	12	004
9	016	029	032	030	018	025	040	038					
10	019	100000000	048	The Carlotte	050			067		100000000000000000000000000000000000000	020		
11	018	036	060	080	075	085	080	085	071	048	020	009	055
	100	fel-h											
6. 6	007	012	012	012	005	015	017	018	027	020	014	011	015
7. 7	012		023				C 10 1 7 1 4	012					
8.8		021		022		War and the	The Control of the	A STATE			1000	011	
				E P			N. Page	1	1	fi no		Tent	-
9. 9	016	018	018	032	.000	.005	.000	004	020			007	
10.10	011	010	009	037	.000	.009	.006	.001	008	007	006	.000	006
7. 2. 9	.008	.002	.006	.014	.016	.015	.009	.015	.004	.010	.002	.005	.009
600	000	000	0.1.1			0.00	20.	0.00	07.0	070	000	000	070
6. 2. 8	.008	.003	.011	.019	.021	.013	.004	.013	.016	.010	.003	.006	.010
6. 2. 6	006	.000	002	006	003	010	014	009	008 .026	.001	.000	.005	003
0. 2. 0	.015	.013	.027	.042	.038	.035	.029	.036	.020	.024	.009	.009	.020
7. 2	.019	.017	.026	.036	.033	.035	.034	.042	.026	.027	.012	.011	.026
8. 2	.019	.022	.036	.043	.050	.060	.059	.062	.042	.038	.016	.015	.039
8. 1	.017	.019	.032	.034	.051	.061	.057	.061	.042	.036	.014	.014	.037
7. 1	.017	.014	.023	.026	.033	.036	.032	.041	.025	.026	.009	.010	.024
0.10.00	077	070	0.00									0-	000
9.12.3.9	.011	018	.038	.038	.032	.064	.059	.064	.050	.040	.016	.014	.037

## METEOROLOGICAL TABLES.

VI.

MISCELLANEOUS TABLES,

· USEFUL IN

TERRESTRIAL PHYSICS AND METEOROLOGY.

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PROTOGRAPH COME PRESENT TATAL PROPERTY

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## POSITIONS OF THE PRINCIPAL OBSERVATORIES.

[From the American Nautical Almanac.]

(North Latitudes and West Longitudes are considered as positive.)

Place.	Latitude.	Longitude from Washington in Time.	Longitude from Washington in Arc.	Longitude from Greenwich in Arc.
Åbo,	+60 26 56.8	h. m. s. - 6 37 20.0	260 40 0.6	337 42 48.6
Altona,	53 32 45.3	5 47 57.4	273 0 39.8	350 3 27.8
Athens,	37 58 20	6 43 6.4	259 13 24.2	336 16 12.2
Berlin,	52 30 16.7	6 1 46.1	269 33 28.1	346 36 16.1
Bilk,	51 12 25	5 35 16.1	276 10 58.1	353 13 46.1
Dia,	01 12 20	0 00 10.1	210 10 00.1	000 10 40.1
Bonn,	50 43 45.0	5 36 35.7	275 51 5.1	352 53 53.1
Breslau,	51 6 56.0	6 16 21.2	265 54 42.0	342 57 30.0
Brussels,	50 51 10.7	5 25 38.8	278 35 18.0	355 38 6.0
Cambridge (Eng.),	52 12 51.8	5 8 34.7	282 51 18.9	359 54 6.9
Cambridge (Mass.),	+42 22 48.6	0 23 41.5	354 4 36.9	71 7 24.9
		A STATE OF THE REAL PROPERTY.		
Cape of Good Hope,	-33 56 3	6 22 7.2	264 28 12.3	341 31 0.3
Christiania,	+59 54 43.7	- 5 51 6.0	272 13 30.6	349 16 18.6
Cincinnati,	39 5 54	+ 0 29 46.9	7 26 42.8	84 29 30.8
Copenhagen,	55 40 53.0	- 5 58 30.5	270 22 22.5	347 25 10.5
Cracow,	50 3 50.0	6 28 2.4	262 59 23.4	340 2 11.4
Dorpat,	58 22 47.1	6 55 5.8	256 13 33.6	333 16 21.6
Dublin,	53 23 13	4 42 49.2	289 17 42.0	6 20 30.0
Durham,	54 46 6.4	5 1 53.2	284 31 42.0	1 34 30.0
Edinburgh,	55 57 23.2	4 55 28.2	286 7 57.0	3 10 45.0
Florence,	43 46 40.8	5 53 12.9	271 41 47.1	348 44 35.1
		A THE STREET		
Geneva,	46 11 58.8	- 5 32 48.9	276 47 46.8	353 50 34.8
Georgetown,	38 54 26.1	+ 0 0 6.2	0 1 33.0	77 4 21.0
Göttingen,	51 31 47.9	- 5 47 57.3	273 0 40.5	350 3 28.5
Gotha,	50 56 5.2	5 51 6.9	272 13 17.1	349 16 5.1
Greenwich,	51 28 38.2	5 8 11.2	282 57 12.0	0 0 0
Hamburg,	53 33 7	- 5 48 4.8	272 58 48.6	350 1 36.6
Hudson,	41 14 42.6	+ 0 17 32.1	4 23 0.9	81 25 48.9
Kasan,	55 47 23.1	- 8 24 43.1	233 49 13.1	310 52 1.1
Königsberg,	54 42 50.4	6 30 11.6	262 27 6.6	339 29 54.6
Kremsmünster,	48 3 23.8	6 4 44.6	268 48 50.7	345 51 38.7
Leipsic,	51 20 20.7	5 57 39.7	270 35 4.5	347 37 52.5
Leipsic, Leyden,	52 9 28.2	5 26 8.6	278 27 50.6	355 30 38.6
Liverpool,	53 24 47.7	4 56 11.1	285 57 13.7	3 0 1.7
London,	51 31 29.8	5 7 34.1	283 6 28.5	0 9 16.5
Madras,	+13 4 9.2	-10 29 8.2	202 42 57.0	279 45 45.0
L'Italian,	10 4 3.2	10 23 0.2	204 42 01.0	2.0 30 30.0

Place.	La	titu	le.	from V	rgitu Vash Tim	ington		ı W	Vash Arc	ington	from G	reen Arc.	wich i
Mannheim,	+49	29	12.9	h.		2.7	27	0	29	19.5	351		7.5
Markree,	54	10	31.7	4	34	22.8	29	1	24	18.0	8	27	6.0
Marseilles,	43	17	49	5	29	40.2	27	7	34	57.2	354	37	45.2
Milan,	45	28	0.7	5	44	57.8	27	3	45	32.4	350	48	20.4
Modena,	44	38	52.8	5	51	55.2	27	2	1	12.5	349	4	0.5
Moscow,	55	45	19.8	7	38	28.5	2	15	22	52.7	322	25	40.7
Munich,	48	8	45	5	54	37.6	2	71	20	35.4	348	23	23.4
Naples,	40	51	46.6	6	100	12.1	20	8	41	58.1	345	44	46.1
Olmütz,	49	35	40.0	6	17	11.3	20	35	42	10.5	342	44	58.5
Oxford,	51	45	36.0	5	3	8.6	28	34	12	51.0	1	15	39.0
Padua,	45	24	2.5	5	55	40.2	23	1	4	56.6	348	7	44.6
Palermo,	+38	6	44	-6	1	36.7	26	9	35	50.1	346	38	38.1
Paramatta,	-33	48	49.8	+8	47	42.6	18	1	55	38.3	208	58	26.3
Paris,	+48	50	13.2	-5	17	32.7	28	0	36	50.1	357	39	38.1
St. Petersburg,	59	56	29.7	7	9	24.7	28	2	38	49.8	329	41	37.8
Philadelphia,	39	57	7.5	0	7	33.6	35	8	6	35.4	75	9	23.4
Prague,	50	5	18.5	6	5	53.2	26	8	31	42.6	345	34	30.6
Pulkowa,	59	46	18.7	7	9	29.9	25	2	37	31.9	329	40	19.9
Rome,	41	53	54	5	58	5.9	27	0	28	31.5	347	31	19.5
San Fernando,	+36	27	45	4	43	22.1	28	9	9	29.1	6	12	17.1
Santiago,	-33	26	24.8	0	25	52.3	35	3	31	55.5	70	34	43.5
Senftenberg,	+50	5	10.1	6	14	1.1	26	6	29	43.1	343	32	31.1
Vienna,	48	12	35.5	6	13	43.7	26	6	34	4.1	343	36	52.1
Washington,	200		39.3	0	0	0		0	0	0	77	2	48.0
Wilna,	+54	40	59.1	-6	49	23.0	25	7	39	15.5	334	42	3.5

II. TO CONVERT PARTS OF THE EQUATOR IN ARC INTO SIDEREAL TIME, OR TO CONVERT TERRESTRIAL LONGITUDE IN ARC INTO TIME.

					D	EGREES.					
Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.
0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.
1	0 4	41	2 44	81	5 24	121	8 4	161	10 44	201	13 24
2	0 8	42	2 48	82	5 28	122	8 8	162	10 48	202	13 28
3 4	0 12 0 16	43	2 52 2 56	83	5 32 5 36	123 124	8 12 8 16	163 164	10 52 10 56	203	13 32
5	0 20	45	3 0	85	5 40	125	8 20	165	11 0	204	13 36 13 40
	20	10			10		20	200		200	10 40
6	0 24	46	3 4	86	5 44	126	8 24	166	11 4	206	13 44
7	0 28	47	3 8	87	5 48	127	8 28	167	11 8	207	13 48
8	0 32	48	3 12	88	5 52	128	8 32	168	11 12	208	13 52
9 10	0 36 0 40	49 50	3 16 3 20	89 90	5 56 6 0	129 130	8 36 8 40	169 170	11 16 11 20	209	13 56 14 0
10	0 40	30	3 20	30	0 0	150	0 40	170	11 20	210	14 0
11	0 44	51	3 24	91	6 4	131	8 44	171	11 24	211	14 4
12	0 48	52	3 28	92	6 8	132	8 48	172	11 28	212	14 8
13	0 52	53	3 32	93	6 12	133	8 52	173	11 32	213	14 12
14	0 56	54	3 36	94	6 16	134	8 56	174	11 36	214	14 16
15	1 0	55	3 40	95	6 20	135	9 0	175	11 40	215	14 20
16	1 4	56	3 44	96	6 24	136	9 4	176	11 44	216	14 24
17	1 8	57	3 48	97	6 28	137	9 8	177	11 48	217	14 28
18	1 12	58	3 52	98	6 32	138	9 12	178	11 52	218	14 32
19	1 16	59	3 56	99	6 36	139	9 16	179	11 56	219	14 36
20	1 20	60	4 0	100	6 40	140	9 20	180	12 0	220	14 40
21	1 24	61	4 4	101	6 44	141	9 24	181	12 4	221	14 44
22	1 28	62	4 8	102	6 48	142	9 28	182	12 8	222	14 48
23	1 32	63	4 12	103	6 52	143	9 32	183	12 12	223	14 52
24	1 36	64	4 16	104	6 56	144	9 36	184	12 16	224	14 56
25	1 40	65	4 20	105	7 0	145	9 40	185	12 20	225	15 0
26	1 44	66	4 24	106	7 4	146	9 44	186	12 24	226	15 4
27	1 48	67	4 28	107	7 8	147	9 48	187	12 28	227	15 8
28	1 52	68	4 32	108	7 12	148	9 52	188	12 32	228	15 42
29	1 56	69	4 36	109	7 16	149	9 56	189	12 36	229	15 16
30	2 0	70	4 40	110	7 20	150	10 0	190	12 40	230	15 20
31	2 4	71	4 44	111	7 24	151	10 4	191	12 44	231	15 24
32	2 8	72	4 48	112	7 28	152	10 8	192	12 48	232	15 28
33	2 12	73	4 52	113	7 32	153	10 12	193	12 52	233	15 32
34	2 16	74	4 56	114	7 36	154	10 16	194	12 56	234	15 36
35	2 20	75	5 0	115	7 40	155	10 20	195	13 0	235	15 40
36	2 24	76	5 4	116	7 44	156	10 24	196	13 4	236	15 44
37	2 28	77	5 8	117	7 48	157	10 24	197	13 4	237	15 48
38	2 32	78	5 12	118	7 52	158	10 32	198	13 12	238	15 52
39	2 36	79	5 16	119	7 56	159	10 36	199	13 16	239	15 56
40	2 40	80	5 20	120	8 0	160	10 40	200	13 20	240	16 0

TO CONVERT PARTS OF THE EQUATOR IN ARC INTO SIDEREAL TIME, OR 2 TO CONVERT TERRESTRIAL LONGITUDE IN ARC INTO TIME.

		32.XI	s		DEGE	LEES.					
Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.
0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.
241	16 4	261	17 24	281	18 44	301	20 4	321	21 24	341	22 44
242	16 8	262	17 28	282	18 48	302	20 8	322	21 28	342	22 48
243	16 12	263	17 32	283	18 52	303	20 12	323	21 32	343	22 52
244	16 16 16 20	264	17 36 17 40	284	18 56 19 0	304	20 16 20 20	324 325	21 36 21 40	344	22 56 23 0
245	16 20	265	17 40	285	19 0	305	20 20	323	21 40	345	25 0
246	16 24	266	17 44	286	19 4	306	20 24	326	21 44	346	23 4
247	16 28	267	17 48	287	19 8	307	20 28	327	21 48	347	23 8
248	16 32	268	17 52	288	19 12	308	20 32	328	21 52	348	23 12
249	16 36	269	17 56	289	19 16	309	20 36	329	21 56	349	23 16
250	16 40	270	18 0	290	19 20	310	20 40	330	22 0	350	23 20
251	16 44	271	18 4	291	19 24	311	20 44	331	22 4	351	23 24
252	16 48	272	18 8	292	19 28	312	20 48	332	22 8	352	23 28
253	16 52	273	18 12	293	19 32	313	20 52	333	22 12	353	23 32
254	16 56	274	18 16	294	19 36	314	20 56	334	22 16	354	23 36
255	17 0	275	18 20	295	19 40	315	21 0	335	22 20	355	23 40
256	17 4	276	18 24	296	19 44	316	21 4	336	22 24	356	23 44
257	17 8	277	18 28	297	19 48	317	21 8	337	22 28	357	23 48
258	17 12	278	18 32	298	19 52	318	21 12	338	22 32	358	23 52
259	17 16	279	18 36	299	19 56	319	21 16	339	22 36	359	23 56
260	17 20	280	18 40	300	20 0	320	21 20	340	22 40	360	24 0
					Min	UTES.		-			
1	m. s.	11	m. s.	01	m. s.	27	m. s.	17	m. s.	/	m. s.
1 2	0 4 0 8	11 12	0 44 0 48	21 22	1 24 1 28	31 32	2 4 2 8	41 42	2 44 2 48	51 52	3 24 3 28
3	0 12	13	0 52	23	1 32	33	2 12	43	2 52	53	3 32
4	0 16	14	0 56	24	1 36	34	2 16	44	2 56	54	3 36
5	0 20	15	1 0	25	1 40	35	2 20	45	3 0	55	3 40
6	0 24	16	1 4	26	1 44	36	2 24	46	3 4	56	3 44
7	0 28	17	1 8	27	1 48	37	2 28	47	3 8	57	3 48
8	0 32	18	1 12	28	1 52	38	2 32	48	3 12	58	3 52
9	0 36	19	1 16	29	1 56	39	2 36	49	3 16	59	3 56
10	0 40	20	1 20	30	2 0	40	2 40	50	3 20	60	4 0
		1		1.50		ONDS.	1002.0	4		1000	
1	0.067	11	s. 0.733	21	s. 1.400	31	2.067	41	s. 2.733	51	s. 3.400
2	0.133	12	0.800	22	1.467	32	2.133	42	2.800	52	3.467
3	0.200	13	0.867	23	1.533	33	2.200	43	2.867	53	3.533
4	0.267	14	0.933	24	1.600	34	2.267	44	2.933	54	3.600
5	0.333	15	1.000	25	1.667	35	2.333	45	3.000	55	3.667
6	0.400	16	1.067	26	1.733	36	2.400	46	3.067	56	3.733
7	0.467	17	1.133	27	1.800	37	2.467	47	3.133	57	3.800
8	0.533	18	1.200	28	1.867	38	2.533	48	3.200	58	3.867
9	0.600	19	1.267	29	1.933	39	2.600	49	3.267	59	3.933
10	0.667	20	1.333	30	2.000	40	2.667	50	3.333	60	4.000

III. TO CONVERT SIDEREAL TIME INTO PARTS OF THE EQUATOR IN ARC, OR TO CONVERT TIME INTO TERRESTRIAL LONGITUDE IN ARC.

					Hot	JRS.				HE H	
Time.	Arc.	Time.	Arc	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.
h.	0	h.	0	h.	0	h.	0	h.	0	h.	0
1	15	5	75	9	135	13	195	17	255	21	315
2	30	6	90	10	150	14	210	18	270	22	330
3	45	7	105	11	165	15	225	19	285	23	345
4	60	8	120	12	180	16	240	20	300	24	360
har de	ter Thorn	102 E	500	168	Min	UTES.			11 54	AUG N	
m.	0 /	m.	0 /	m.	0 /	m.	0 /	m.	0 /	m.	0 /
1	0 15	11	2 45	21	5 15	31	7 45	41	10 15	51	12 45
2	0 30	12	3 0	22	5 30	32	8 0	42	10 30	52	13 0
3	0 45	13	3 15	23	5 45	33	8 15	43	10 45	53	13 15
4	1 0	14	3 30	24	6 0	34	8 30	44	11 0	54	13 30
5	1 15	15	3 45	25	6 15	35	8 45	45	11 15	55	13 45
6	1 30	16	4 0	26	6 30	36	9 0	46	11 30	56	14 0
7	1 45	17	4 15	27	6 45	37	9 15	47	11 45	57	14 15
8	2 0	18	4 30	28	7 0	38	9 30	48	12 0	58	14 30
9	2 15	19	4 45	29	7 15	39	9 45	49	12 15	59	14 45
10	2 30	20	5 0	30	7 30	40	10 0	50	12 30	60	15 0
				(1	SEC	onds.		II .			
s. 1	0 15	s. 11	2 45	8. 21	5 15	8. 31	7 45	s. 41	10 15	51	12 45
2	0 30	12	3 0	22	5 30	32	8 0	42	10 30	52	13 0
3	0 45	13	3 15	23	5 45	33	8 15	43	10 45	53	13 15
4	1 0	14	3 30	24	6 0	34	8 30	44	11 0	54	13 30
5	1 15	15	3 45	25	6 15	35	8 45	45	11 15	55	13 45
6	1 30	16	4 0	26	6 30	36	9 0	46	11 30	56	14 0
7	1 45	17	4 15	27	6 45	37	9 15	47	11 45	57	14 15
8	2 0	18	4 30	28	7 0	38	9 30	48	12 0	58	14 30
9	2 15	19	4 45	29	7 15	39	9 45	49	12 15	59	14 45
10	2 30	20	5 0	30	7 30	40	10 0	50	12 30	60	15 (
		11.54	d relin	1 (18)	Tenths of	F SECON	IDS.	11		7	6, 10, 6
s.	"	8.	"	s.	1 "	s.	"	S.	"	s.	"
0.01	0.15	0.18	2.70	0.35	5.25	0.52	7.80	0.69	10.35	0.86	12.90
0.02	0.30	0.19	2.85	0.36	5.40	0.53	7.95	0.70	10.50	0.87	13.05
0.03	0.45	0.20	3.00	0.37	5.55	0.54	8.10	0.71	10.65	0.88	13.20
0.04	0.60	0.21	3.15	0.38	5.70	0.55	8.25	0.72	10.80	0.89	13.35
0.05	0.75	0.22	3.30	0.39	5.85	0.56	8.40	0.73	10.95	0.90	13.50
0.06	0.90	0.23	3.45	0.40	6.00	0.57	8.55	0.74	11.10	0.91	13.65
0.07	1.05	0.24	3.60	0.41	6.15	0.58	8.70	0.75	11.25	0.92	13.80
0.08	1.20	0.25	3.75	0.42	6.30	0.59	8.85	0.76	11.40	0.93	13.95
0.09	1.35	0.26	3.90	0.43	6.45	0.60	9.00	0.77	11.55	0.94	14.10
0.10	1.50	0.27	4.05	0.44	6.60	0.61	9.15	0.78	11.70	0.95	14.25
0.11	1.65	0.28	4.20	0.45	6.75	0.62	9.30	0.79	11.85	0.96	14.40
0.12	1.80	0.29	4.35	0.46	6.90	0.63	9.45	0.80	12.00	0.97	14.55
0.13	1.95	0.30	4.50	0.47	7.05	0.64	9.60	0.81	12.15	0.98	14.70
0.14		0.31	4.65	0.48	7.20	0.65	9.75	0.82	12.30	0.99	14.85
0.15	2.25	0.32	4.80	0.49	7.35	0.66	9.90	0.83	12.45 12.60	1.00	15.00
				0.50	7.50	0.67	10.05				

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# IV. FOR CONVERTING SIDEREAL TIME INTO MEAN SOLAR TIME, AND MEAN TIME INTO SIDEREAL TIME.

	HOURS	8.			MINU	ITES.		4		SECO	NDS.	
Hours	Mean Time.	Sidereal Time.	Min- utes.	Mean Time.	Sidereal Time.	Min- utes.	Mean Time.	Sidereal Time.	Sec- onds.	Mean or Sidereal Time.	Sec- onds.	Mean or Sidere Time
10.0	m 8.	m. s.		8.	8.		8.	8.		8.	-	8.
1	0 9.83	0 9.86	1	0.16	0.16	31	5.08	5.09	1	0.00	31	0.09
2	0 19.66	0 19.71	2	0.33	0.33	32	5.24	5.26	2	0.01	32	0.09
3	0 29.49	0 29.57	3	0.49	0.49	33	5.41	5.42	3	0.01	33	0.09
4	0 39.32	0 39.43	4	0.66	0.66	34	5.57	5.59	4	0.01	34	0.09
5	0 49.15	0 49.28	5	0.82	0.82	35	5.75	5.75	5	0.01	35	0.10
6	0 58.98	0 59.14	6	0.98	0.99	36	5.90	5.91	6	0.02	36	0.10
7	1 8.81	1 9.00	7	1.15	1.15	37	6.06	6.08	7	0.02	37	0.10
8	1 18.64	1 18.85	8	1.31	1.31	38	6.23	6.24	8	0.02	38	0.10
9	1 28.47	1 28.71	9	1.47	1.48	39	6.39	6.41	9	0.03	39	0.11
10	1 38.30	1 38.57	10	1.64	1.64	40	6.55	6.57	10	0.03	40	0.11
11	1 48.13	1 48.42	11	1.80	1.81	41	6.72	6.74	11	0.03	41	0.11
12	1 57.96	1 58.28	12	1.97	1.97	42	6.88	6.90	12	0.03	42	0.12
13	2 7.78	2 8.13	13	2 13	2.14	43	7.05	7.06	13	0.04	43	0.12
14	2 17.61	2 17.99	14	2.29	2.30	44	7.21	7.23	14	0.04	44	0.12
15	2 27.44	2 27.85	15	2.46	2.46	45	7.37	7.39	15	0.04	45	0.12
16	2 37.27	2 37.70	16	2.62	2.63	46	7.54	7.56	16	0.04	46	0.13
17	2 47.10	2 47.56	17	2.79	2.79	47	7.70	7.72	17	0.05	47	0.13
18	2 56.93	2 57.42	18	2.95	2.96	48	7.86	7.89	18	0.05	48	0.13
19	3 6.76	3 7.27	19	3.11	3.12	49	8.03	8.05	19	0.05	49	0.13
20	3 16.59	3 17.13	20	3.28	3.29	50	8.19	8.21	20	0.06	50	0.1
21	3 26.42	3 26.99	21	3.44	3.45	51	8.36	8.38	21	0.06	51	0.14
22	3 36.25	3 36.84	22	3.60	3.61	52	8.52	8.54	22	0.06	52	0.14
23	3 46.08	3 46.70	23	3.77	3.79	53	8.68	8.71	23	0.06	53	0.18
24	3 55.91	3 56.56	24	3.93	3.94	54	8.85	8.87	24	0.07	54	0.1
25	4 5.74	4 6.41	25	4.10	4.11	55	9.01	9.04	25	0.07	55	0.18
26	4 15.57	4 16.27	26	4.26	4.27	56	9.17	9.20	26	0.07	56	0.15
27	4 25.40	4 26.13	27	4.42	4.43	57	9.34	9.36	27	0.07	57	0.16
28	4 35.23	4 35.98	28	4.59	4.60	58	9.50	9.53	28	0.08	58	0.16
29	4 45.06 4 54.89	4 45.84	29 30	4.75	4.76	59 60	9.67	9.69	29	0.08	59	0.16
90	4 94.09	4 90.09	90	4.04	4.95	00	9.53	9.86	30	0.08	60	0.16

# CORRECTION OF THE TIME OBTAINED BY OBSERVATION OF THE SUN, IN ORDER TO HAVE THE TRUE TIME OF THE CLOCK.

Day of	Jan.	Feb.	Mar.	Apr.	Apr.	May.	June.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Dec.	Day of
Month.	Add.	Add.	Add.	Add.	Subt.	Subt.	Subt.	Add.	Add.	Add.	Subt.	Subt.	Subt.	Subt.	Add.	Month.
1000	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	
1	4	14	13	4		3	3		3	6	0	10	16	11		1
2	4	14	12	4		3	2		4	6	0	11	16	10		2
3	5	14	12	3		3	2		4	6	1	11	16	10		3
4	5	14	12	3		3	2		4	6	1	11	16	10		4
5	6	14	12	3		4	2		4	6	1	12	16	9		5
6	6	14	12	2		4	2		4	6	2	12	16	9		6
7	7	14	11	2		4	2		4	5	2	12	16	8		7
8	7	15	11	2		4	1		5	5	2	12	16	8		8
9	8	15	11	2		4	1		5	5	3	13	16	7		9
10	8	15	11	1		4	1		5	5	3	13	16	7		10
11	9	15	10	1		4	1		5	5	3	13	16	6		11
12	9	15	10	1		4	1		5	5	4	13	16	6		12
13	9	15	10	1		4	0		5	5	4	14	16	5		13
14	10	14	9	0		4	0		5	4	5	14	15	5		14
15	10	14	9	0		4	0		6	4	5	14	15	4		15
16	10	14	9	0		4	0		6	4	5	14	15	4		16
17	11	14	9	0		4	0		6	4	6	15	15	3		17
18	11	14	8		1	4		1	6	4	6	15	15	3		18
19	11	14	8		1	4		1	6	3	6	15	14	2		19
20	11	14	8		1	4		1	6	3	7	15	14	2		20
21	12	14	7		1	4		1	6	3	7	15	14	1		21
22	12	14	7		2	4		2	6	3	7	15	14	1		22
23	12	14	7		2	4		2	6	2	8	16	13	0		23
24	12	13	6		2	3		2	6	2	8	16	13	0		24
25	13	13	6		2	3		2	6	2	8	16	13	0	• •	25
26	13	13	6		2	3		2	6	2	9	16	12		1	26
27	13	13	5		2	3		3	6	1	9	16	12		1	27
28	13	13	5		3	3		3	6	1	9	16	12		2	28
29	14	13	5		3	3		3	6	1	10	16	11		2	29
30	14		4		3	3		3	6	0	10	16	11-		3	30
31	14		4			3			6	0		16			3	31

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#### TABLE FOR COMPUTING TERRESTRIAL SURFACES.

The tables under No. VI. were published by Delcros in the Annuaire Météorologique de la France pour 1850, p. 65 et seq.

The formula from which they have been computed reads as follows: -

$$S = \frac{ab\pi}{90} \begin{cases} \sin\frac{1}{2}\phi\cos\left(L + \frac{1}{2}\phi\right) \\ -\frac{1}{3}\left[2\cdot\left(\frac{a-b}{a+b}\right) + \left(\frac{a-b}{a+b}\right)^{2}\right]\sin\left(\phi + \frac{1}{2}\phi\right)\cos\left[3L + (\phi + \frac{1}{2}\phi)\right] \\ +\frac{1}{5}\left[3\cdot\left(\frac{a-b}{a+b}\right)^{2} + \left(\frac{a-b}{a+b}\right)^{3}\right]\sin\left(2\phi + \frac{1}{2}\phi\right)\cos\left[5L + (2\phi + \frac{1}{2}\phi)\right] \\ -\text{etc.}; \end{cases}$$

in which  $a=\frac{1}{2}$  great axis of the globe;  $b=\frac{1}{2}$  small axis; L= the latitude of the lower limit of a quadrilateral surface; L'= the latitude of the upper limit of the same;  $\phi=L'-L$ ; S= the area of a quadrilateral surface of one degree in longitude;  $\pi=$  the ratio of the circumference to the diameter.

Substituting the numerical values, the quarter of the meridian being = 10,000,724 legal metres; the  $\frac{1}{2}$  great axis, or a, = 6,376,989 metres; the  $\frac{1}{2}$  small axis, or b, = 6,356,323 metres; the ratio of the axis  $\frac{1}{300,64}$ ; and making  $\phi = 1^{\circ}$  nonagesimal, the

formula becomes,

$$\mathbf{S} = \left\{ \begin{array}{l} 224.996360 \; \cos \left( \; \mathbf{L} + \mathbf{0}^{\circ} \; \mathbf{30'} \right) \\ -0.730851 \; \cos \left( 3 \; \mathbf{L} + \mathbf{1}^{\circ} \; \mathbf{30'} \right) \\ +0.001784 \; \cos \left( 5 \; \mathbf{L} + \mathbf{2}^{\circ} \; \mathbf{30'} \right) \\ -0.000004 \; \cos \left( 7 \; \mathbf{L} + \mathbf{3}^{\circ} \; \mathbf{30'} \right) \\ + \; \text{etc.} \end{array} \right.$$

The first three terms of the formula give the results with sufficient accuracy.

In order to avoid too large a number of figures, the results are given in square miles, the linear base of which is a mile equal to  $\frac{1}{15}$  of the mean degree of the meridian. That mile is thus  $=\left(\frac{10000724}{90\times15}\right)=7407.942$  metres. In order to convert the results into new geographical miles, of which  $60=1^\circ$ , multiply by 16,  $\log=1.2041200$ ; into common French leagues,  $25=1^\circ$ , multiply by 2.777778,  $\log=0.4436975$ ; into nautical leagues,  $20=1^\circ$ , multiply by 1.777778,  $\log=0.2498775$ ; into English statute miles,  $69.163=1^\circ$ , by 21.711034,  $\log=1.3366868$ .

#### USE OF THE TABLES.

Table I., which gives the number of square miles contained in the quadrilateral surfaces of one degree in latitude and longitude, successively from the equator to the pole, will be more frequently used. Table II. has been computed for maps on a smaller scale; and Tables III. and IV. for maps of very small scale, covering large areas, in which surfaces of one degree could not be estimated with sufficient accuracy. If the scale is large enough to have the minutes traced on, then Table V. is to be used.

For computing a surface by Table I., which may serve as an example for all the others, find first the lowest parallel circle which crosses, on the map, the surface to be estimated; suppose it is 40° lat. N., and the zone within 40° and 41° lat. N. contains four integral degrees of longitude, that is, four surfaces of one degree each way; then in the first column of the table, on the line beginning with latitude 40°, and in the vertical column headed 4, take the value of these four surfaces, viz. 685.88. Then take likewise the value of the number of surfaces between 41° and 42° lat. N., and so on. The fractional parts left outside of the integral degrees are best estimated, with the compass, in decimals, the values of which can be found in the columns of the multiples, by properly moving the decimal point to the left. Having taken them in that way, and summing them up with all the integral surfaces, we obtain the total surface required.

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TABLE I. QUADRILATERAL SURFACES OF 1 DEGREE IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Lim:	iting			Multiples	of these Qu	adrilateral S	Surfaces from	m 1 to 9.		
LATIT	UDES.			In an			1		KE HIVE	N THEOLOGY
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	1	224.259	448.52	672.78	897.04	1121.29	1345.55	1569.81	1794.07	2018.33
1	2	224.192	448.38	672.58	896.77	1120.96	1345.15	1569.35	1793.54	2017.73
2	3	224.059	448.12	672.18	896.24	1120.30	1344.36	1568.42	1792.47	2016.53
3	4	223.860	447.72	671.58	895.44	1119.30	1343.16	1567.02	1790.88	2014.74
4	5	223.594	447.19	670.78	894.37	1117.97	1341.56	1565.16	1788.75	2012.34
5	6	223.261	446.52	669.78	893.05	1116.31	1339.57	1562.83	1786.09	2009.35
6	7	222.863	445.73	668.59	891.45	1114.31	1337.18	1560.04	1782.90	2005.76
7	8	222.398	444.80	667.19	889.59	1111.99	1334.39	1556.78	1779.18	2001.58
8	9	221.867	443.73	665.60	887.47	1109.33	1331.20	1553.07	1774.93	1996.80
9	10	221.270	442.54	663.81	885.08	1106.35	1327.62	1548.89	1770.16	1991.43
10	11	220.607	441.21	661.82	882.43	1103.03	1323.64	1544.25	1764.85	1985.46
11	12	219.878	439.76	659.63	879.51	1099.39	1319.27	1539.15	1759.02	1978.90
12	13	219.084	433.17	657.25	876.34	1095.42	1314.50	1533.59	1752.67	1971.76
13	14	218.225	436.45	654.67	872.90	1091.12	1309.35	1527.57	1745.80	1964.05
14	15	217.300	434.60	651.90	869.20	1086.50	1303.80	1521.10	1738.40	1955.70
15	16	216.311	432.62	648.93	865.24	1081.55	1297.86	1514.17	1730.48	1946.80
16	17	215.257	432.02	645.77	861.03	1076.28	1291.54	1506.80	1730.48	1937.3
17	18	214.138	428.28	642.41	856.55	1070.28	1284.83	1498.97	1713.10	1927.2
18	19	212.955	425.25	638.87	851.82	1064.78	1277.73	1490.69	1703.64	1916.6
19	20	211.709	423.42	636.13	846.84	1058.54	1270.25	1481.96	1693.67	1905.38
		100000		15,000,20		REAL FOR		4.10	31 10 55	
20	21	210.399	420.80	631.20	841.59	1051.99	1262.39	1472.79	1683.19	1893.5
21	22	209.025	418.05	627.08	836.10	1045.13	1254.15	1463.18	1672.20	1881.2
22 23	23 24	207.589	415.18	622.77	830.36	1037.95	1245.54	1453.12	1660.71	1868.30
24		206.090	412.18	618.27	824.36	1030.45	1236.54	1442.63	1648.72	1854.8
	25	204.529	409.06	613.59	818.12	1022.65	1227.18	1431.71	1636.24	1840.7
25	26	202.907	405.81	608.72	811.63	1014.53	1217.44	1420.35	1623.25	1826.1
26	27	201.223	402.45	603.67	804.89	1006.11	1207.34	1408.56	1609.78	1811.00
27	28	199.477	398.95	598.43	797.91	997.39	1196.86	1396.34	1595.82	1795.3
28	29	197.672	395.34	593.02	790.69	988.36	1186.03	1383.70	1581.38	1779.0
29	30	195.806	391.61	587.42	783.23	979.03	1174.84	1370.64	1566.45	1762.20
30	31	193.881	387.76	581.64	775.52	969.40	1163.29	1357.17	1551.05	1744.9
31	32	191.897	383.79	575.69	767.59	959.48	1151.38	1343.28	1535.17	1727.0
32	33	189.854	379.71	569.56	759.41	949.27	1139.12	1328.98	1518.83	1708.6
33	34	187.753	375.51	563.26	750.01	938.76	1126.52	1314.27	1502.02	1689.7
34	35	185.594	371.19	556.78	742.38	927.97	1113.57	1299.16	1484.75	1670.3
35	36	183.379	366.76	550.14	733.52	916.89	1100.27	1283.65	1467.03	1650.4
36	37	181.107	362.21	543.32	724.43	905.53	1086.64	1267.75	1448.86	1629.9
37	38	178.780	357.56	536.34	715.12	893.90	1072.68	1251.46	1430.24	1609.0
38	39	176.397	352.79	529.19	705.59	881.98	1058.38	1234.78	1411.18	1587.5
39	40	173.960	347.92	521.88	695.84	869.80	1043.76	1217.72	1391.68	1565.6
40	41	171.469	342.94	514.41	685.88	857.34	1028.81	1200.28	1371.75	1543.2
41	42	168.925	337.85	506.77	675.70	844.62	1013.55	1182.47	1351.40	1520.2
42	43	166.328	332.66	498.98	665.31	831.64	997.97	1164.30	1330.62	1496.9
43	44	163.680	327.36	491.04	654.72	818.40	982.08	1145.76	1309.44	1473.1
44	45	160.980	321.96	482.94	643.92	804.90	965.88	1126.86	1287.84	1448.8

TABLE I. (Continued.) QUADRILATERAL SURFACES OF 1 DEGREE IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

								CU PULL		
LATI'	iting TUDES.		***	Multiples	of these Qu	adrilateral i	Surfaces fro	m 1 to 9.		
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.
45	46	158.231	316.46	474.69	632.92	791.15	949.39	1107.62	1265.85	1424.08
46	47	155.432	310.86	466.30	621.73	777.16	932.59	1088.02	1243.46	1398.89
47	48	152.584	305.17	457.75	610.34	762.92	915.51	1068.09	1220.67	1373.26
48	49	149.689	299.38	449.07	598.75	748.44	899.13	1047.82	1197.51	1347.20
49	50	146.746	293.49	440.24	586.98	733.73	880.48	1027.22	1173.97	1320.71
50	51	143.757	287.51	431.27	575.03	718.78	862.54	1006.30	1150.06	1293.81
51	52	140.723	281.45	422.17	562.89	703.61	844.34	985.06	1125.78	1266.51
52	53	137.644	275.29	412.93	550.58	688.22	825.86	963.51	1101.15	1238.80
53	54	134.522	269.04	403.57	538.09	672.61	807.13	941.65	1076.17	1210.70
54	55	131.357	262.71	394.07	525.43	656.78	788.14	919.50	1050.86	1182.21
55	56	128.150	256.30	384.45	512.60	640.75	768.90	897.05	1025.20	1153.35
56	57	124.903	249.81	374.71	499.61	624.51	749.42	874.32	999.22	1124.13
57	58	121.616	243.23	364.85	486.46	608.08	729.69	851.31	972.92	1094.54
58	59	118.289	236.58	354.87	473.16	591.45	709.74	828.03	946.32	1064.61
59	60	114.926	229.85	344.78	459.70	574.63	689.55	804.48	919.41	1034.33
60	61	111.525	223.05	334.58	446.10	557.63	669.15	780.68	892.20	1003.73
61	62	108.089	216.18	324.27	432.35	540.44	648.53	756.62	864.71	972.80
62	63	104.618	209.24	313.85	418.47	523.09	627.71	732.32	836.94	941.56
63	64	101.113	202.23	303.34	404.45	505.56	606.68	707.79	808.90	910.02
64	65	97.575	195.15	292.73	390.30	487.88	585.45	683.03	780.60	878.18
65	66	94.007	188.01	282.02	376.03	470.03	564.04	658.05	752.05	846.06
66	67	90.408	180.82	271.22	361.63	452.04	542.45	632.85	723.26	813.67
67	68	86.779	173.56	260.34	347.12	433.90	520.68	607.46	694.23	781.01
68	69	83.123	166.25	249.37	332.49	415.61	498.74	581.86	664.98	748.11
69	70	79.439	158.88	238.32	317.76	397.20	476.64	556.08	635.52	714.95
70	71	75.730	151.46	227.19	302.92	378.65	454.38	530.11	605.84	681.57
71	72	71.996	143.99	215.99	287.99	359.98	431.98	503.98	575.97	647.97
72	73	68.239	136.48	204.72	272.96	341.20	409.44	477.68	545.91	614.15
73	74	64.460	128.92	193.38	257.84	322.30	386.76	451.22	515.68	580.14
74	75	60.659	121.32	184.98	242.64	303.30	363.96	424.62	485.28	545.94
75	76	56.839	113.68	170.52	227.36	284.20	341.04	397.88	454.72	511.55
76	77	53.001	106.00	159.00	212.00	265.00	318.00	371.00	424.00	477.01
77	78	49.145	98.29	147.43	196.58	245.72	294.87	344.01	393.16	442.30
78	79 80	45.272	90.54	135.82 124.16	181.09 165.54	226.36 206.93	271.63 248.31	316.91 289.70	362.18 331.08	407.45 372.47
80	81	37.485	74.97	112.46	149.94	187.43	224.91	262.40	299.88	337.37
1 1 1 1 1 1 1 1 1 1		Action Williams			134.29	TO SECTION AND ADDRESS.				100000000000000000000000000000000000000
81	82	33.572	67.14	100.72		167.86	201.43	235.01	268.58	302.15
82	83	29.649	59.30	88.95	118.59	148.24	177.89	207.54	237.19	266.84
83	84 85	25.715	51.43	77.15 65.32	102.86 87.09	128.58 108.87	154.29 130.64	180.01 152.41	205.72 174.19	231.44 195.96
85	86	17.824	35.65	53.47	71.30	89.12	106.95	124.77	142.59	160.42
86	87	13.869	27.74	41.61	55.48	69.35	83.22	97.09	110.96	124.82
87	88	9.910	19.82	29.73	39.64	49.55	59.46	69.37	79.28	89.19
88	89	5.947	11.89	17.84	23.79	29.74	35.68	41.63	47.58	53.53
89	90	1.983	3.97	5.95	7.93	9.91	11.90	13.88	15.86	17.84
00	1 00	1.000	0.01	0.00	1.00	0.01	11.00,	10.00	10.00	24079

TABLE II. QUADRILATERAL SURFACES OF 2 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Th.   Sup.     1.     2.   3.   4.   5.   6.   7.   8.	
2         4         895.838         1791.68         2697.51         3583.35         4479.19         5375.03         6270.57         7166.7           4         6         899.510         1787.42         2681.13         3574.84         4465.55         5362.26         6255.97         7149.6           6         8         890.520         1781.04         2671.56         3562.08         4452.60         5343.12         6233.64         7124.1           10         12         880.969         1761.94         2642.91         3523.88         4404.85         5285.82         6166.79         7047.7           12         14         874.617         1749.23         2623.85         3498.47         4373.09         5247.70         6122.32         6996.9           14         16         855.789         1717.58         256.37         3485.16         2501.15         500.55         5987.7         6122.32         6996.9           14         16         18         855.789         1717.55         256.37         3485.16         2499.95         5152.74         611.52         870.31           18         20         849.328         1696.6         2547.98         3397.31         4246.64         5995.97	9.
2         4         895.838         1791.68         2687.51         3582.35         4479.19         5375.03         6270.87         7166.7           4         6         8893.510         1787.42         2681.13         3574.84         4468.55         5362.26         6255.97         7149.66           8         10         886.272         1772.54         2658.82         3545.09         4431.36         5341.26         6233.46         7124.11           10         12         880.969         1761.94         2642.91         3523.88         4404.85         5285.82         6166.79         7047.77           16         18         874.617         749.23         2623.85         3498.47         4378.09         5247.70         6122.23         8996.9           16         18         855.789         1717.58         2576.37         3495.16         4293.95         5182.74         6011.52         6996.9           20         22         838.848         1677.70         2516.54         3355.39         4194.24         5033.09         5871.94         6710.7           22         24         26         18         11.400         1602.92         2482.03         3390.44         436.50         4964.16	8072.1
6         8         890.520         1781.04         2671.56         3562.08         4452.60         5343.12         6233.64         7124.11           8         10         886.272         1772.54         2658.82         3545.09         4431.36         5317.63         6208.91         7090.11           10         12         880.969         1761.94         2642.91         3523.88         4404.85         5285.32         6166.79         7047.7           12         14         874.617         1749.23         2623.85         3498.47         4373.09         5247.70         6122.32         6996.99           16         18         858.789         1717.58         2576.37         3435.16         4293.95         5152.74         6011.52         6870.3           18         20         849.828         1698.66         2547.98         3397.31         4246.64         5099.97         5945.30         6794.6           20         22         835.848         1677.70         216.54         3355.39         4194.24         5033.09         5871.94         6710.7           22         24         26         81.400         1602.80         2404.20         3205.60         4007.00         4808.40         5609.80 </td <td>8062.5</td>	8062.5
8         10         886.272         1772.54         2658.82         3545.09         4431.36         5317.63         6203.91         7090.1           10         12         880.969         1761.94         2642.91         3523.88         4404.85         5285.82         6166.79         7047.77           14         16         867.221         1734.44         2601.66         3468.88         4336.11         5203.33         6070.55         6937.7         6122.92         6996.9         18         20         849.328         1698.66         2547.98         3397.31         4246.64         5095.97         5945.30         6794.6           20         22         838.848         1677.70         2516.54         3355.39         4194.24         5033.09         5871.94         6710.77           24         26         814.872         1629.74         2444.62         3255.49         4074.36         4899.23         5704.11         6518.9           26         28         811.400         1602.80         2404.20         3205.60         4007.00         4808.23         5704.11         6518.9           28         30         766.956         1573.91         2360.87         3147.83         3934.78         4721.74	8043.3
10         12         880.969         1761.94         2642.91         3523.88         4404.85         5285.82         6166.79         7047.7           12         14         874.617         1749.23         2623.85         3498.47         4373.09         5247.70         6122.32         6996.9           16         18         867.878         1717.58         2576.37         3435.16         4293.95         5152.74         6011.52         6870.3           18         20         849.328         1698.66         2547.98         3397.31         4246.64         5095.97         5945.30         6791.5         6870.3           20         22         838.848         1677.70         2516.54         3355.39         4194.24         5033.09         5871.94         6710.71           24         26         814.872         1629.74         2444.62         3259.49         4074.36         4898.23         5704.11         6711.51         6618.8           25         30         786.956         1573.91         2360.87         3147.83         3934.73         4721.74         550.69         6295.6           30         32         771.555         1543.11         2314.67         3086.22         3857.78         462	8014.6
12         14         874.617         1749.23         2623.85         3498.47         4378.09         5247.70         6122.32         6996.9           14         16         867.221         1734.44         2601.66         3468.88         4336.11         5203.33         6070.55         6937.7           16         18         858.789         1717.58         2576.37         3435.16         4299.95         5152.74         6011.52         6870.3           18         20         849.328         1698.66         2547.98         3397.31         4246.64         5095.97         5945.30         6794.6           20         22         838.848         1677.70         2516.54         3355.39         4194.24         5033.09         5871.94         6710.77           22         24         826         814.872         1629.74         2444.62         3259.49         4074.36         4889.23         5704.11         6618.8           24         26         814.800         1602.80         2404.20         3205.60         4007.00         4808.40         5608.06         6295.6           23         74         755.51         1543.11         2314.67         3086.22         3857.78         4629.33         5400.8	7976.4
14         16         867.221         1734.44         2601.66         3468.88         4336.11         5203.33         6070.55         6937.7           16         18         558.789         1717.55         2576.37         3435.16         4293.95         5152.74         6011.52         6870.3           18         20         849.328         1698.66         2547.98         3397.31         4246.64         5095.97         5945.30         6794.6         6701.7           20         22         838.848         1677.70         2516.54         3355.39         4194.24         5033.09         5871.94         6710.71           22         24         26         814.872         1629.74         2444.62         3259.49         4074.36         4889.23         5704.11         6518.9           26         28         811.400         1602.80         2404.20         3205.60         4007.00         4808.40         560.80         6295.6           30         32         771.555         1543.11         2314.67         3086.22         3857.78         4629.33         5400.89         6172.4           4         36         73.946         1475.99         2213.84         2951.78         3689.73         4421.68 <td>7928.7</td>	7928.7
16         18         858.789         1717.58         2576.37         3435.16         4293.95         5152.74         6011.52         6870.3           18         20         849.328         1698.66         2547.98         3397.31         4246.64         5095.97         5945.30         6794.6           20         22         838.848         1677.70         2516.54         3355.39         4194.24         5033.09         5871.94         6710.72           24         26         814.872         1629.74         2444.62         3259.49         4074.36         4889.23         5704.11         6518.9           26         28         811.400         1602.80         2404.20         3205.60         4007.00         4808.40         5609.80         6411.2           28         30         786.956         1573.91         2360.87         3147.83         3934.78         4721.74         5508.69         6295.6           30         32         771.555         1543.11         2314.67         3086.22         3857.78         4629.33         5400.89         6172.4           34         36         735.213         1510.43         2265.64         3020.85         377.60         4531.28         5286.49         60	7871.5
18         20         849.328         1698.66         2547.98         3397.31         4246.64         5095.97         5945.30         6794.6           20         22         838.848         1677.70         2516.54         3355.39         4194.24         5033.09         5871.94         6710.71           24         26         814.872         1629.74         2444.62         3259.49         4074.36         4889.23         5704.11         6518.9           26         28         811.400         1602.80         2404.20         3205.60         4007.00         4808.40         5609.80         6411.2           28         30         786.956         1573.91         2360.87         3147.83         3934.78         4721.74         5508.69         6295.6           30         32         771.555         1543.11         2314.67         3086.22         3857.78         4629.33         5400.89         6172.4           34         36         737.946         1475.89         2213.84         2951.78         3689.73         4427.68         5165.62         5903.5           36         35         719.773         1439.55         2159.32         2879.09         3598.87         4318.64         508.41         57	7804.9
20         22         838.848         1677.70         2516.54         3355.39         4194.24         5033.09         5871.94         6710.71           22         24         827.359         1654.72         2482.08         3309.44         4136.80         4964.16         5791.51         6618.8           24         26         814.872         1629.74         2444.62         3259.49         4074.36         4889.23         5704.11         6518.9           26         28         811.400         1602.80         2404.20         3205.60         4007.00         4808.40         5609.80         6411.2           30         32         771.555         1543.11         2314.67         3086.22         3857.78         4629.33         5400.89         6174.73           34         36         787.946         1475.89         22118.84         2951.78         3689.73         4427.68         5165.65         5903.5           36         38         719.773         1439.55         2159.32         2879.09         3598.87         4318.64         5038.41         5758.12           36         38         70.707.13         1401.43         2102.14         2802.85         3503.57         4204.28         4904.99	7729.1
22         24         827.359         1654.72         2482.08         3309.44         4136.80         4964.16         5791.51         6618.8           24         26         814.872         1629.74         2444.62         3259.49         4074.36         4889.23         5704.11         6518.9           26         28         811.400         1602.80         2404.20         3259.49         4074.36         4889.23         5704.11         6518.9           30         786.956         1573.91         2360.87         314.783         3934.78         4721.74         5508.69         6295.6           30         32         771.555         1543.11         2314.67         3086.22         3857.78         4629.33         5400.89         6172.4           34         36         737.946         1475.89         2213.84         2951.78         3698.73         3427.68         5165.62         5903.5           36         38         719.773         1439.55         2159.32         2879.09         3598.87         4318.64         5088.41         5788.1           38         40         700.713         1401.43         2102.14         2802.85         3503.57         4204.28         4904.99         5605.7	7643.9
22         24         827.359         1654.72         2482.08         3309.44         4136.80         4964.16         5791.51         6618.8           24         26         814.872         1622.974         2444.62         3259.49         4074.36         4889.23         5704.11         6518.9           26         28         811.400         1602.80         2404.20         3205.60         4007.00         4808.40         5609.80         6411.2           28         30         786.956         1573.91         2360.87         3147.83         3934.78         4721.74         5508.69         6295.6           30         32         771.555         1543.11         2314.67         3086.22         3857.78         4629.33         5400.89         6174.73           34         36         787.946         1475.89         2213.84         2951.78         3689.73         4427.68         5165.65         5903.5           36         38         719.773         1439.55         2159.32         2879.09         3598.87         4318.64         5083.41         5758.12           38         40         700.713         1401.43         2102.14         2802.85         3503.57         4204.28         4904.99 <th< td=""><td>7549.6</td></th<>	7549.6
24         26         814.872         1629.74         2444.62         3259.49         4074.36         4889.23         5704.11         6518.9           26         28         811.400         1602.80         2404.20         3205.60         4007.00         4808.40         5609.80         6411.2           28         30         786.956         1573.91         2360.87         3147.83         3934.78         4721.74         5508.69         6295.6           30         32         771.555         1548.11         2314.67         3086.22         3857.78         4629.33         5400.89         6172.4           31         36         737.946         1475.89         2213.84         2951.78         3689.73         4427.65         5165.62         5903.5           38         40         700.713         1401.43         2102.14         2802.85         3503.57         4204.28         4904.99         5605.7           40         42         680.787         1361.57         2042.36         2723.15         3403.93         4084.72         4765.51         5446.2           42         44         660.016         1320.03         1980.05         2640.06         3300.08         3960.09         4620.11         52	
26         28         811.400         1602.80         2404.20         3205.60         4007.00         4808.40         5609.80         6411.2           28         30         786.956         1573.91         2360.87         3147.83         3934.78         4721.74         5508.69         6295.6           30         32         771.555         1543.11         2314.67         3086.22         3857.78         4629.33         5400.89         6172.4           34         36         737.946         1475.89         2213.84         2951.78         3689.73         4427.68         5165.62         5903.5           36         38         719.773         1439.55         2159.32         2879.09         3598.87         4318.64         5038.41         5758.13           40         42         680.787         1361.57         2042.36         2723.15         3403.93         4084.72         4765.51         5446.2           42         44         660.016         1320.03         1980.05         2640.06         3000.08         3960.09         4620.11         5280.1           44         46         638.423         1276.85         1915.27         2553.69         3192.11         3530.54         4468.96         5	200
28         30         786.956         1573.91         2360.87         3147.83         3934.78         4721.74         5508.69         6295.6           30         32         771.555         1543.11         2314.67         3086.22         3857.78         4629.33         5400.89         6172.4           32         34         755.213         1510.43         2265.64         3020.85         3776.06         4531.28         5286.49         6041.7           34         36         737.946         1475.89         2213.84         2951.78         3689.73         4427.68         5165.62         5903.5           38         40         700.713         1401.43         2102.14         2802.85         303.57         4204.28         4904.99         5605.7           40         42         680.787         1361.57         2042.36         2723.15         3403.93         4084.72         4765.51         5466.2           42         44         660.016         1320.03         1980.05         2640.06         3000.08         3960.09         4620.11         5280.1           44         46         63.8423         1276.85         1915.27         2553.69         3192.11         3530.54         4468.96         510	
30         32         771.555         1548.11         2314.67         3086.22         3857.78         4629.33         5400.89         6172.4           32         34         755.213         1510.43         2265.64         3020.85         3776.06         4531.28         5286.49         6041.7           34         36         737.946         1475.89         2213.84         2951.78         3689.73         4427.68         5165.62         5903.57           38         40         700.713         1401.43         2102.14         2802.85         3503.57         4204.28         4904.99         5605.7           40         42         680.787         1361.57         2042.36         2723.15         3403.93         4084.72         4765.51         5446.2           44         46         638.423         1276.85         1915.27         2553.69         3192.11         3830.54         4468.96         5107.3           48         50         592.869         1185.74         1778.61         2371.48         2964.34         3557.21         4150.08         4742.9           50         .52         568.960         1137.92         1706.88         2275.84         2844.80         3413.76         3982.72	1000
32         34         755.213         1510.43         2265.64         3020.85         3776.06         4531.28         5286.49         6041.7           34         36         737.946         1475.89         2213.84         2951.78         3689.73         4427.68         5165.62         5903.5           36         38         719.773         1439.55         2159.32         2879.09         3598.87         4318.64         5038.41         5758.13           38         40         700.713         1401.43         2102.14         2802.85         3503.57         4204.28         4904.99         5605.7           40         42         680.787         1361.57         2042.36         2723.15         3403.93         4084.72         4765.51         5446.2           44         46         638.423         1276.85         1915.27         2553.69         3192.11         3830.54         4468.96         5107.3           48         50         592.869         1185.74         1778.61         2371.43         2964.34         3557.21         4150.08         4742.9           50         .52         568.960         1137.92         1706.88         2275.84         2844.80         3413.76         3982.72	6944.0
34         36         737.946         1475.89         2213.84         2951.78         3689.73         4427.68         5165.62         5903.5           36         38         719.773         1439.55         2159.32         2879.09         3598.87         4318.64         5038.41         5758.19           38         40         700.713         1401.43         2102.14         2802.85         3503.57         4204.28         4904.99         5605.7           40         42         680.787         1361.57         2042.36         2723.15         3403.93         4084.72         4765.51         5446.2           42         44         660.016         1320.03         1980.05         2640.06         3300.08         3960.09         4620.11         5280.1           44         46         638.423         1276.85         1915.27         2553.69         3192.11         3830.54         4468.96         51073.3           48         50         592.869         1185.74         1778.61         2371.48         2964.34         3557.21         4150.08         4742.9           50         .52         568.960         1137.92         1706.88         2275.84         2844.80         3413.76         3982.72 <td< td=""><td></td></td<>	
36         38         719.773         1439.55         2159.32         2879.09         3598.87         4318.64         5038.41         5758.1           38         40         700.713         1401.43         2102.14         2802.85         3503.57         4204.28         4904.99         5605.7           40         42         680.787         1361.57         2042.36         2723.15         3403.93         4084.72         4765.51         5446.2           42         44         660.016         1320.03         1980.05         2640.06         3300.08         3960.09         4620.11         5280.1           44         46         638.423         1276.85         1915.27         2553.69         3192.11         3830.54         4468.96         5107.3           46         48         616.032         1232.06         1848.10         2464.13         3080.16         3696.19         4812.23         4928.2           48         50         592.869         1187.92         1706.88         2275.84         2844.80         3413.76         3982.72         4551.66           52         54         544.332         1088.66         1632.99         2177.33         2721.66         3265.99         3810.32         4	
38         40         700.713         1401.43         2102.14         2802.85         3503.57         4204.28         4904.99         5605.7           40         42         680.787         1361.57         2042.36         2723.15         3403.93         4084.72         4765.51         5446.2           42         44         660.016         1320.03         1980.05         2640.06         3300.08         3960.09         4620.11         5280.1           44         46         638.423         1276.85         1915.27         2553.69         3192.11         3830.54         4468.96         5107.3           46         48         616.032         1232.06         1848.10         2464.13         3080.16         3696.19         4812.23         4928.2           48         50         592.869         1185.74         1778.61         2371.48         2964.34         3557.21         4150.08         4742.9           50         .52         568.960         1137.92         1706.88         2275.84         2844.80         3413.76         3982.72         4551.66           51         54         544.332         1088.66         1632.99         2177.33         2721.66         3265.99         3810.32	
40         42         680.787         1361.57         2042.36         2723.15         3403.93         4084.72         4765.51         5446.2           42         44         660.016         1320.03         1980.05         2640.06         3300.08         3960.09         4620.11         5280.1           44         46         638.423         1276.85         1915.27         2553.69         3192.11         3830.54         4468.96         5107.3           46         48         616.032         1232.06         1848.10         2464.13         3080.16         3696.19         4312.23         4928.2           48         50         592.869         1185.74         1778.61         2371.48         2964.34         3557.21         4150.08         4742.9           50         .52         568.960         1137.92         1706.88         2275.84         2844.80         3413.76         3982.72         4551.66           52         54         544.332         1088.66         1632.99         2177.33         2721.66         3265.99         3810.32         4354.6           54         56         519.014         1038.03         1557.04         2076.06         2595.07         3114.09         3633.10	6306.4
42         44         660.016         1320.03         1980.05         2640.06         3300.08         3960.09         4620.11         5280.11         5280.11         5280.11         5280.11         5280.11         5280.11         5280.11         5280.11         5280.11         3830.54         4468.96         5107.3         46         48         616.032         1232.06         1848.10         2464.13         3080.16         3696.19         4312.23         4928.2         48         50         592.869         1185.74         1778.61         2371.48         2964.34         3557.21         4150.08         4742.9         50         .52         568.960         1137.92         1706.88         2275.84         2844.80         3413.76         3982.72         4551.66         52         54         544.332         1088.66         1632.99         2177.33         2721.66         3265.99         3810.32         4354.66         54         56         519.014         1038.03         1557.04         2076.06         2595.07         3114.09         3633.10         4152.1         4551.66         58         493.037         986.07         1479.11         1972.15         2465.18         2958.22         3451.26         3944.22         58         60         466.430         93	6127.0
44         46         638.423         1276.85         1915.27         2553.69         3192.11         3830.54         4468.96         5107.3           46         48         616.032         1232.06         1848.10         2464.13         3080.16         3696.19         4312.23         4928.2           48         50         592.869         1185.74         1778.61         2371.48         2964.34         3557.21         4150.08         4742.9           50         .52         568.960         1137.92         1706.88         2275.84         2844.80         3413.76         3982.72         4551.63           52         54         544.332         1088.66         1632.99         2177.33         2721.66         3265.99         3810.32         4354.63           54         56         519.014         1038.03         1557.04         2076.06         2595.07         3114.09         3633.10         4152.1           56         58         493.037         986.07         1479.11         1972.15         2465.18         2958.22         3451.26         3944.22           58         60         466.430         932.86         13199.29         1865.72         2332.15         2798.58         3265.01 <td< td=""><td>1 - 1</td></td<>	1 - 1
46         48         616.032         1232.06         1848.10         2464.13         3080.16         3696.19         4312.23         4928.2           48         50         592.869         1185.74         1778.61         2371.48         2964.34         3557.21         4150.08         4742.9           50         .52         568.960         1137.92         1706.88         2275.84         2844.80         3413.76         3982.72         4551.66           52         54         544.332         1088.66         1632.99         2177.33         2721.66         3265.99         3810.32         4354.66           54         56         519.014         1038.03         1557.04         2076.06         2595.07         3114.09         3633.10         4152.1           56         58         493.037         986.07         1479.11         1972.15         2465.18         2958.22         3451.26         3944.2           58         60         466.430         932.86         1399.29         1865.72         2332.15         2798.58         3265.01         3731.4           60         62         439.228         878.46         1317.68         1756.91         2196.14         2635.37         3074.59         35	1
48         50         592.869         1185.74         1778.61         2371.48         2964.34         3557.21         4150.08         4742.9           50         .52         568.960         1137.92         1706.88         2275.84         2844.80         3413.76         3982.72         4551.66           52         54         544.332         1088.66         1632.99         2177.33         2721.66         3265.99         3810.32         4354.66           54         56         519.014         1038.03         1557.04         2076.06         2595.07         3114.09         3633.10         4152.1           56         58         493.037         986.07         1479.11         1972.15         2465.18         2958.22         3451.26         3944.21           58         60         466.430         932.86         1399.29         1865.72         2332.15         2798.58         3265.01         3731.4           60         62         439.228         878.46         1317.68         1756.91         2196.14         2635.37         3074.59         3513.83           62         64         411.461         822.92         1234.38         1645.84         2057.30         2468.76         2880.23         3	100000000000000000000000000000000000000
50         -52         568.960         1137.92         1706.88         2275.84         2844.80         3413.76         3982.72         4551.66           52         54         544.332         1088.66         1632.99         2177.33         2721.66         3265.99         3810.32         4354.66           54         56         519.014         1038.03         1557.04         2076.06         2595.07         3114.09         3633.10         4152.1           56         58         493.037         986.07         1479.11         1972.15         2465.18         2958.22         3451.26         3944.25           58         60         466.430         932.86         1399.29         1865.72         2332.15         2798.58         3265.01         3731.4           60         62         439.228         878.46         1317.68         1756.91         2196.14         2635.37         3074.59         3513.8           62         64         411.461         822.92         1234.38         1645.84         2057.30         2468.76         2880.23         3291.63           64         66         354.374         708.75         1063.12         1417.50         1771.87         2126.24         2480.62         28	
52         54         544.332         1088.66         1682.99         2177.33         2721.66         3265.99         3810.32         4354.66           54         56         519.014         1038.03         1557.04         2076.06         2595.07         3114.09         3633.10         4152.1°           56         58         493.037         986.07         1479.11         1972.15         2465.18         2958.22         3451.26         3944.2°           58         60         466.430         932.86         1399.29         1865.72         2332.15         2798.58         3265.01         3731.4           60         62         439.228         878.46         1317.68         1756.91         2196.14         2635.37         3074.59         3513.8°           62         64         411.461         822.92         1234.38         1645.84         2057.30         2468.76         2880.23         3291.6°           64         66         383.164         766.33         1149.49         1532.66         1915.82         2298.99         2682.15         3065.3°           68         70         325.124         650.25         975.37         1300.50         1625.62         1950.75         2275.87         260	5120.6
54         56         519.014         1038.03         1557.04         2076.06         2595.07         3114.09         3633.10         4152.1           56         58         493.037         986.07         1479.11         1972.15         2465.18         2958.22         3451.26         3944.2           58         60         466.430         932.86         1399.29         1865.72         2332.15         2798.58         3265.01         3731.4           60         62         439.228         878.46         1317.68         1756.91         2196.14         2635.37         3074.59         3513.8           62         64         411.461         822.92         1234.38         1645.84         2057.30         2468.76         2880.23         3291.63           64         66         383.164         766.33         1149.49         1532.66         1915.82         2298.99         2682.15         3065.33           66         68         354.374         708.75         1063.12         1417.50         1771.87         2126.24         2480.62         2834.99           70         72         295.453         590.91         886.36         1181.81         1477.27         1772.72         2068.17         2363.63	4898.9
56         58         493.037         986.07         1479.11         1972.15         2465.18         2958.22         3451.26         3944.2           58         60         466.430         932.86         1399.29         1865.72         2332.15         2798.58         3265.01         3731.4           60         62         439.228         878.46         1317.68         1756.91         2196.14         2635.37         3074.59         3513.83           62         64         411.461         822.92         1234.38         1645.84         2057.30         2468.76         2880.23         3291.63           64         66         383.164         766.33         1149.49         1532.66         1915.82         2298.99         2682.15         3065.31           66         68         354.374         708.75         1063.12         1417.50         1771.87         2126.24         2480.62         2834.91           68         70         325.124         650.25         975.37         1300.50         1625.62         1950.75         2275.87         2601.00           70         72         295.453         590.91         886.36         1181.81         1477.27         1772.72         2068.17         2363.63	4 - 2 - 2 - 2 - 3
58         60         466.430         932.86         1399.29         1865.72         2332.15         2798.58         3265.01         3731.4           60         62         439.228         878.46         1317.68         1756.91         2196.14         2635.37         3074.59         3513.8           62         64         411.461         822.92         1234.38         1645.84         2057.30         2468.76         2880.23         3291.61           64         66         383.164         766.33         1149.49         1532.66         1915.82         2298.99         2682.15         3065.33           66         68         354.374         708.75         1063.12         1417.50         1771.87         2126.24         2480.62         2834.93           68         70         325.124         650.25         975.37         1300.50         1625.62         1950.75         2275.87         2601.00           70         72         295.453         590.91         886.36         1181.81         1477.27         1772.72         2068.17         2363.63           72         74         265.398         530.80         796.20         1061.59         1326.99         1592.39         1857.79         2123.19<	4671.1
60         62         439.228         878.46         1317.68         1756.91         2196.14         2635.37         3074.59         3513.8           62         64         411.461         822.92         1234.38         1645.84         2057.30         2468.76         2880.23         3291.61           64         66         383.164         766.33         1149.49         1532.66         1915.82         2298.99         2682.15         3065.33           66         68         354.374         708.75         1063.12         1417.50         1771.87         2126.24         2480.62         2834.93           68         70         325.124         650.25         975.37         1300.50         1625.62         1950.75         2275.87         2601.00           70         72         295.453         590.91         886.36         1181.81         1477.27         1772.72         2068.17         2363.63           72         74         265.398         530.80         796.20         1061.59         1326.99         1592.39         1857.79         2123.19           74         76         234.998         469.99         704.99         939.99         1174.99         1409.99         1644.98         1879.99 </td <td>100000</td>	100000
62         64         411.461         822.92         1234.38         1645.84         2057.30         2468.76         2880.23         3291.66           64         66         383.164         766.33         1149.49         1532.66         1915.82         2298.99         2682.15         3065.33           66         68         354.374         708.75         1063.12         1417.50         1771.87         2126.24         2480.62         2834.99           68         70         325.124         650.25         975.37         1300.50         1625.62         1950.75         2275.87         2601.00           70         72         295.453         590.91         886.36         1181.81         1477.27         1772.72         2068.17         2363.63           72         74         265.398         530.80         796.20         1061.59         1326.99         1592.39         1857.79         2123.19           74         76         234.998         469.99         704.99         939.99         1174.99         1409.99         1644.98         1879.99           76         78         204.290         408.58         612.87         817.16         1021.45         1225.74         1430.03         1634.33 <td></td>	
64         66         383.164         766.33         1149.49         1532.66         1915.82         2298.99         2682.15         3065.33           66         68         354.374         708.75         1063.12         1417.50         1771.87         2126.24         2480.62         2834.93           68         70         325.124         650.25         975.37         1300.50         1625.62         1950.75         2275.87         2601.00           70         72         295.453         590.91         886.36         1181.81         1477.27         1772.72         2068.17         2363.63           72         74         265.398         530.80         796.20         1061.59         1326.99         1592.39         1857.79         2123.19           74         76         234.998         469.99         704.99         939.99         1174.99         1409.99         1644.98         1879.99           76         78         204.290         408.58         612.87         817.16         1021.45         1225.74         1430.03         1634.33           78         80         173.316         346.63         519.95         693.26         866.58         1039.90         1213.21         1386.53	3953.0 3703.1
66         68         354.374         708.75         1063.12         1417.50         1771.87         2126.24         2480.62         2834.99           68         70         325.124         650.25         975.37         1300.50         1625.62         1950.75         2275.87         2601.00           70         72         295.453         590.91         886.36         1181.81         1477.27         1772.72         2068.17         2363.66           72         74         265.398         530.80         796.20         1061.59         1326.99         1592.39         1857.79         2123.19           74         76         234.998         469.99         704.99         939.99         1174.99         1409.99         1644.98         1879.99           78         80         173.316         346.63         519.95         693.26         866.58         1039.90         1213.21         1386.51           80         82         142.115         284.23         426.34         568.46         710.57         852.69         994.80         1136.93           82         84         110.728         221.46         332.18         442.91         553.64         664.37         775.09         885.83	
68         70         325.124         650.25         975.37         1300.50         1625.62         1950.75         2275.87         2601.00           70         72         295.453         590.91         886.36         1181.81         1477.27         1772.72         2068.17         2363.66           72         74         265.398         530.80         796.20         1061.59         1326.99         1592.39         1857.79         2123.19           74         76         234.998         469.99         704.99         939.99         1174.99         1409.99         1644.98         1879.99           78         80         173.316         346.63         519.95         693.26         866.58         1039.90         1213.21         1386.51           80         82         142.115         284.23         426.34         568.46         710.57         852.69         994.80         1136.93           82         84         110.728         221.46         332.18         442.91         553.64         664.37         775.09         885.83           84         86         79.195         168.39         237.59         316.78         395.98         475.17         554.37         633.50 <t< td=""><td>3448.4</td></t<>	3448.4
70         72         295.453         590.91         886.36         1181.81         1477.27         1772.72         2068.17         2363.66           72         74         265.398         530.80         796.20         1061.59         1326.99         1592.39         1857.79         2123.19           74         76         234.998         469.99         704.99         939.99         1174.99         1409.99         1644.98         1879.99           76         78         204.290         408.58         612.87         817.16         1021.45         1225.74         1430.03         1634.33           78         80         173.316         346.63         519.95         693.26         866.58         1039.90         1213.21         1386.55           80         82         142.115         284.23         426.34         568.46         710.57         852.69         994.80         1136.93           82         84         110.728         221.46         332.18         442.91         553.64         664.37         775.09         885.83           84         86         79.195         168.39         237.59         316.78         395.98         475.17         554.37         633.50 <tr< td=""><td>2926.1</td></tr<>	2926.1
72         74         265.398         530.80         796.20         1061.59         1326.99         1592.39         1857.79         2123.19           74         76         234.998         469.99         704.99         939.99         1174.99         1409.99         1644.98         1879.99           76         78         204.290         408.58         612.87         817.16         1021.45         1225.74         1430.03         1634.33           78         80         173.316         346.63         519.95         693.26         866.58         1039.90         1213.21         1386.53           80         82         142.115         284.23         426.34         568.46         710.57         852.69         994.80         1136.99           82         84         110.728         221.46         332.18         442.91         553.64         664.37         775.09         885.89           84         86         79.195         168.39         237.59         316.78         395.98         475.17         554.37         633.54           86         88         47.559         95.12         142.68         190.24         237.79         285.35         332.91         380.47	THE RES
74         76         234.998         469.99         704.99         939.99         1174.99         1409.99         1644.98         1879.96           76         78         204.290         408.58         612.87         817.16         1021.45         1225.74         1430.03         1634.33           78         80         173.316         346.63         519.95         693.26         866.58         1039.90         1213.21         1386.53           80         82         142.115         284.23         426.34         568.46         710.57         852.69         994.80         1136.93           82         84         110.728         221.46         332.18         442.91         553.64         664.37         775.09         885.83           84         86         79.195         168.39         237.59         316.78         395.98         475.17         554.37         633.50           86         88         47.559         95.12         142.68         190.24         237.79         285.35         332.91         380.47	2659.0
76         78         204.290         408.58         612.87         817.16         1021.45         1225.74         1430.03         1634.33           78         80         173.316         346.63         519.95         693.26         866.58         1039.90         1213.21         1386.53           80         82         142.115         284.23         426.34         568.46         710.57         852.69         994.80         1136.93           82         84         110.728         221.46         332.18         442.91         553.64         664.37         775.09         885.83           84         86         79.195         168.39         237.59         316.78         395.98         475.17         554.37         633.50           86         88         47.559         95.12         142.68         190.24         237.79         285.35         332.91         380.47	2388.5
78         80         173.316         346.63         519.95         693.26         866.58         1039.90         1213.21         1386.53           80         82         142.115         284.23         426.34         568.46         710.57         852.69         994.80         1136.93           82         84         110.728         221.46         332.18         442.91         553.64         664.37         775.09         885.83           84         86         79.195         168.39         237.59         316.78         395.98         475.17         554.37         633.56           86         88         47.559         95.12         142.68         190.24         237.79         285.35         332.91         380.47	1838.6
80     82     142.115     284.23     426.34     568.46     710.57     852.69     994.80     1136.93       82     84     110.728     221.46     332.18     442.91     553.64     664.37     775.09     885.83       84     86     79.195     168.39     237.59     316.78     395.98     475.17     554.37     633.50       86     88     47.559     95.12     142.68     190.24     237.79     285.35     332.91     380.47	1559.8
82     84     110.728     221.46     332.18     442.91     553.64     664.37     775.09     885.83       84     86     79.195     168.39     237.59     316.78     395.98     475.17     554.37     633.50       86     88     47.559     95.12     142.68     190.24     237.79     285.35     332.91     380.47	
84     86     79.195     168.39     237.59     316.78     395.98     475.17     554.37     633.51       86     88     47.559     95.12     142.68     190.24     237.79     285.35     332.91     380.47	1279.0
86 88 47.559 95.12 142.68 190.24 237.79 285.35 332.91 380.47	996.5
2200 20021 2000 00201 00001	428.0
88 90   15.860   31.72   47.58   63.44   79.30   95.16   111.02   126.88	142.7

TABLE III. QUADRILATERAL SURFACES OF 5 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi LATIT	ting UDES.			Multiple	es of these (	Quadrilatera	l Surfaces fro	om 1 to 9.		
Inf.	Sup.	1.	2.	3.	.4.	5.	6.	7.	8.	9.
0	5	5599.821	11199.64	16799.46	22399.29	27999.11	33598.93	39198.75	44798.57	50398.39
5	10	5558.288	11116.58	16674.87	22233.15	27791.44	33349.73	38908.02	44466.31	50024.60
10	15	5475.466	10950.93	16426.40	21901.87	27377.33	32852.80	38328.27	43803.73	49279.20
15	20	5351.846	10703.69	16055.54	21407.39	26759.23	32111.08	37462.93	42814.77	48166.62
20	25	5188.165	10376.33	15564.49	20752.66	25940.82	31128.99	36317.15	41505.32	46693.48
	144							S STATE OF	STATE OF	
25	30	4985.425	9970.85	14956.27	19941.70	24927.12	29912.55	34897.97	39883.40	44868.82
30	35	4744.891	9485.78	14234.67	18979.57	23724.46	28469.35	33214.24	37959.13	42704.02
35	40	4468.110	8936-22	13404.33	17872.44	22340.55	26808.66	31276.77	35744.88	40212.99
40	45	4156.909	8313.82	12470.73	16627.64	20784.54	24941.45	29098.36	33255.27	37412.18
45	50	3813.408	7626-82	11440.22	15253.63	19067.04	22880.45	26693.86	30507.26	34320.67
									1	
50	55	3440.013	6880.03	10320.04	13760.05	17200.06	20640.08	24080.09	27520.10	30960.12
55	60	3039.419	6078.84	9118.26	12157.68	15197.09	18236.51	21275.93	24315.35	27354.77
60	65	2614.598	5229.20	7843.80	10458.39	13072.99	15687.59	18302.19	20916.79	23531.39
65	70	2168.779	4337.56	6506.34	8675.12	10843.89	13012.67	15181.45	17350.23	19519.01
70	75	1705.427	3410.85	5116.28	6821.71	8527-13	10232.56	11937.99	13643.42	15348-84
75	80	1228.213	2456.43	3684.64	4912.85	6141.07	7369.28	8597.49	9825.71	11053.92
80	85	740.973	1481.95	2222.92		AT CAMPAGE	4445.84	5186.81	5927.78	6668.76
85	90	247.668	495.34	743.00	990.67	1238.34	1486.01	1733.68	1981.34	2229.01

FABLE IV. QUADRILATERAL SURFACES OF 10 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi ATIT	ting UDES.			Multiple	es of these	Quadrilateral	Surfaces fro	m 1 to 9.		
inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	s.	9.
0	10	22316.220	44632.44	66948.66	89264.88	111581.10	133897.32	156213.54	178529.76	200845.98
10	20	21654.626	43309.25	64963.88	86618.50	108273.13	129927.76	151582.38	173237.01	194891.63
20	30	20347.180	40694.36	61041.54	81388.72	101735.90	122083.08	142430.26	162777.44	183124.62
30	40	18426.004	36852.01	55278.01	73704.02	92130.02	110556.02	128982.03	147408.03	165834.04
40	50	15940.634	31881.27	47821.90	63762.54	79703.17	95643.80	111584.44	127525.07	143465.71
50	60	12958.864	25917.73	38876.59	51835.46	64794.32	77753.18	90712.05	103670.91	116629.78
60	70	9566.755	19133.51	28700.26	38267.02	47833.77	57400.53	66967.28	76534.04	86100.79
70	80	5867.281	11734.56	17601.84	23469.12	29336.40	35203.69	41070.97	46938.25	52805.53
80	90	1977.282	3954.56	5931.85	7909.13	9886.41	11863.69	13840.97	15818-26	17795.54

TABLE V. Mean Quadrilateral Surfaces of 1, 10, 20, and 30 Minutes in Latitude and in Longitude deduced from each Quadrilateral of 1 Degree in Table I.

Limi LATIT	UDES.	Mean Su		asuring in ongitude.	Latitude	Limi LATIT	iting TUDES.	Mean Su	rfaces mea and in L	asuring in longitude.	Latitude
Inf.	Sup.	1/.	10%	201.	30%	Inf.	Sup.	1'.	10'.	20'.	30%
0	1	0.0623	6.229	24.918	56.065	45	46	0.0440	4.395	17.581	39.558
1	2	0.0623	6.228	24.910	56.048	46	47	0.0432	4.318	17.270	38.858
2	3	0.0622	6.224	24.895	56.015	47	48	0.0424	4.238	16.954	38:146
3	4	0.0622	6.218	24.873	55.965	48	49	0.0416	4.158	16.632	37.422
4	5	0.0621	6.211	24.844	55.898	49	50	0.0408	4.076	16.305	36.68
5	6	0.0620	6.202	24.807	55.815	50	51	0.0399	3.993	15.973	35.93
6	7	0.0619	6.191	24.763	55.716	51	52	0.0391	3.909	15.636	35.18
7	8	0.0618	6.178	24.711	55.599	52	53	0.0382	3.823	15.294	34.41
8	9	0.0616	6.163	24.652	55.467	53	54	0.0374	3.737	14.947	33.63
9	10	0.0615	6.146	24.586	55.317	54	55	0.0365	3.649	14.595	32.83
10	11	0.0613	6.128	24.512	55.152	55	56	0.0356	3.560	14.239	32.03
11	12	0.0611	6.108	24.431	54.970	56	57	0.0347	3.470	13.878	31.22
12	13	0.0609	6.086	24.343	54.771	57	58	0.0338	3.378	13.513	30.40
13	14	0.0606	6.062	24.247	54.556	58	59	0.0329	3.286	13.143	29.57
14	15	0.0604	6.036	24.144	54.325	59	60	0.0319	3.192	12.770	28.73
15	16	0.0601	6.009	24.035	54.078	60	61	0.0310	3.098	12.392	27.88
16	17	0.0598	5.979	23.917	53.814	61	62	0.0300	3.002	12.010	27.02
17	18	0.0595	5.948	23.793	53.534	62	63	0.0291	2.906	11.624	26.15
18	19	0.0592	5.915	23.662	53.239	63	64	0.0281	2.809	11.235	25.27
19	20	0.0588	5.881	23.523	52.927	64	65	0.0271	2.710	10.842	24.39
20	21	0.0584	5.844	23.378	52.600	65	66	0.0261	2.611	10.445	23.50
21	22	0.0581	5.806	23.225	52.256	66	67	0.0251	2.511	10.045	22.60
22	23	0.0577	5.766	23.065	51.897	67	68	0.0241	2.411	9.642	21.69
23	24	0.0572	5.725	22.899	51.523	68	69	0.0231	2.309	9.236	20.78
24	25	0.0568	5.681	22.725	51.132	69	70	0.0221	2.207	8.827	19.86
25	26	0.0564	5.636	22.545	50.727	70	71	0.0210	2.104	8.414	18.93
26	27	0.0559	5.590	22.358	50.306	71	72	0.0200	2.000	8.000	17.99
27	28	0.0554	5.541	22.164	49.869	72	73	0.0190	1.896	7.582	17.06
28	29	0.0549	5.491	21.964	49.418	73	74	0.0179	1.791	7.162	16.11
29	30	0.0544	5.439	21.756	48.952	74	75	0.0168	1.685	6.740	15.16
30	31	0.0539	5.386	21.542	48.470	75	76	0.0158	1.579	6.315	14.21
31	32	0.0533	5.330	21.322	47.974	76	77	0.0147	1.472	5.889	13.25
32	33	0.0527	5.274	21.095	47.463	77	78	0.0137	1.365	5.461	12.28
33	34	0.0522	5.215	20.861	46.938	78	79	0.0126	1.258	5.030	11.31
34	35	0.0516	5.155	20.622	46.399	79	80	0.0115	1.150	4.598	10.34
35	36	0.0509	5.094	20.375	45.845	80	81	0.0104	1.041	4.165	9.37
36	37	0.0503	5.031	20.123	45.277	81	82	0.0093	0.933	3.730	8.39
37	38	0.0497	4.966	19.864	44.695	82	83	0:0082	0.824	3.294	7.41
38	39	0.0490	4.900	19.600	44.099	83	84	0.0071	0.714	2.857	6.42
39	40	0.0483	4.832	19.329	43.490	84	85	0.0060	0.605	2.419	5.44
40	41	0.0476	4.763	19.052	42.867	85	86	0.0049	0.495	1.980	4.45
41	42	0.0469	4.692	18.769	42.231	86	87	0.0039	0.385	1.541	3.46
42	43	0.0462	4.620	18.481	41.582	87	88	0.0028	0.275	1.101	2.47
43	44	0.0455	4.547	18.187	40.920	88	89	0.0017	0.165	0.661	1.48
44	45	0.0447	4.472	17.887	40.245	89	90	0.0006	0.055	0.220	0.49

#### ERRATA IN THE FIRST EDITION.

- A, page 7, line below the title, instead of  $(32 + \frac{4}{5}x^{\circ})$  read  $(32 + \frac{9}{5}x^{\circ})$ .
- A, " 21, on the line beginning with 30, in the last four columns,

100.75 100.97 101.20 instead of 101.42 101.07 101.30 101.52. read 100 85

- 7, on the line beginning with 23°, second column, instead of 20.410, read 20.888. B,
- 66 23, on the line beginning with 12°, third column, instead of 5.87, read 5.37. В,
- B. 30-32, at the head of each first column, Temperature of the Air, add "in Centigrade degrees."
- 40, Table II., first part, on the line beginning with 60, column headed 7, instead of 24.11,01, В, read 24.9,01.
- 66 Table II., first part, on the line beginning with 70, column headed 5, instead of 27.4,47, B, read 27.8,47; and column headed 8, instead of 28.11,77, read 28.9,77.
- В, " Table II., second part, on the line beginning with 70, column headed 5, instead of 328.47, read 332.47.
- 41, Table III., line beginning with 20, the five last columns, B. 73.70, instead of 63.54 66.08 68.62 71.16 63.50 66.04 68.58 71.12 73.66. read
- B. " Table III, line beginning with 200, column headed 3, instead of 515.11, read 515.61.
- 42, Table V., line beginning with 180, column headed 7, instead of 516.21, read 506.21. B.
- В, 43, Table VI., first part, on line beginning with 70, column headed 2, instead of 76.635, read 76.735.
- B, Table VI., second part, on line beginning with 7, the last eight columns, instead of 0.6483 0.6572 0 6661 0.6750 0.6839 0.6927 0.7016 0.7105. 0.6395 0.6483 0.6572 0.6661 0.6750 0.6839 0.6927
- 43, Table VI., second part, on line beginning with 12, column headed 5, instead of 1.1018, В, read 1.1102.
- C, 11, on line beginning with 26.5 inches, column headed 6, instead of 674.41, read 674.61.
- 66 C, " on line of 27.1 inches, column headed 1, instead of 688.38, read 688.58.
- C, 12, on line of 30.5 inches, column headed 2, instead of 778.20, read 775.19.
- C, 66 39 and 41, at the head of table, instead of "Tenths of Degrees," read "English Inches."
- 66 28, 29, and 30, head of page, instead of "Tenths of a Degree," read "Hundredths of a Degree." D,
- D, 35, note at the bottom, instead of "Geology," read "Geodesy."
- D, 66 36, on line beginning with 160, columns headed 8 and 9, instead of 550.19 and 553.47, read 551.19 and 554.47.
- D, 36, on line beginning with 260, columns headed 2, 3, 5, and 6,

66

66

- 882.72, instead of 860.59 863.87 879.43 read 859.60 862.88 869.44 872.72.
- D, 37, on line beginning with 620, column headed 4, instead of 2048.28, read 2047.28.
- " D, 66 66 66 66 770, 0, 2526.39. 2526.29.
- " D. 38. 880. 5, 2903.69, 2903.60.
- D. 66 66 40 890, .. 6, 2939.79. 2939.69.
- " " 66 D, 3069.64, 930, 5, 3067.64.

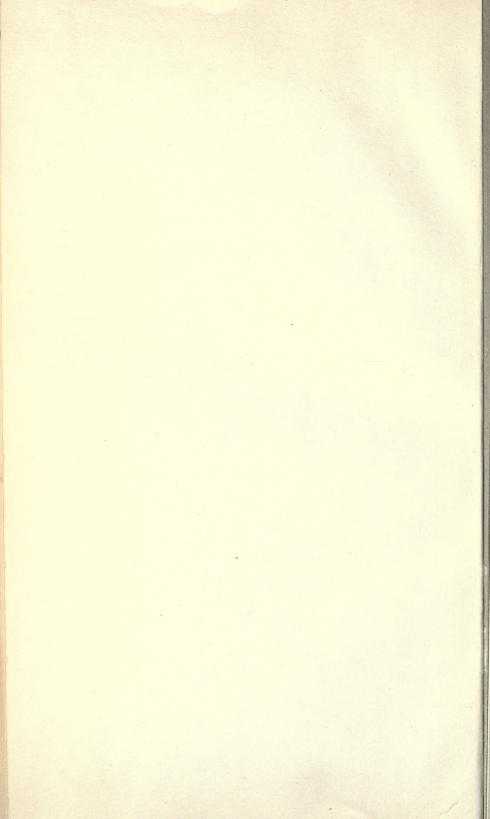
66

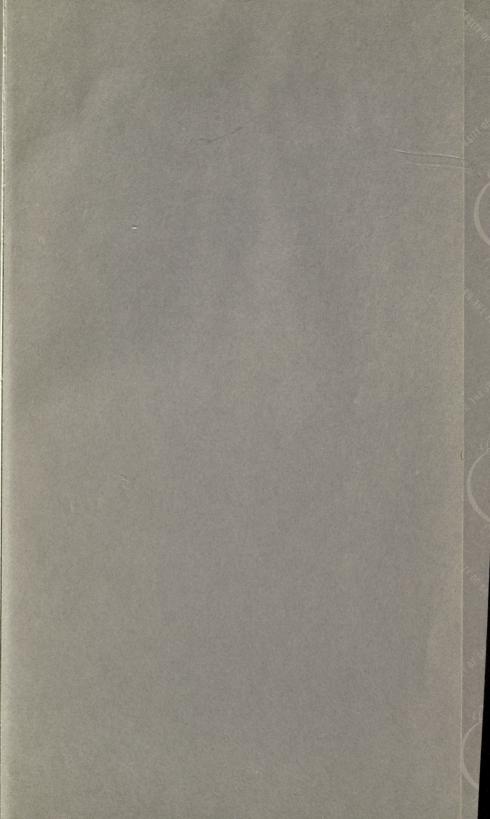
66

- D, 4, 990. 3261.71, 3261.21.
- 66 66 66 66 D, 3264.59. 3264.49. 990. 5, D. 39, on line beginning with 1380, columns headed 3, 4, 5, 6, 7, 8,
- instead of 4537.28 4540.56 4543.85 4547.13 4550.41 4553.69, 4537.48 4540.76 read 4544.05 4547.33 455061
- D, 40, on line beginning with 1610, column headed 5, instead of 5292.65, read 5298.65.
- 44, Table X., on line beginning with 3, column headed 6, instead of 21.0205, read 23.0205. D,
- D, 45, Table XII., on line beginning with column 0, column headed 5, instead of 0.83333, read 0.08333.

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