

DEPARTMENT OF COMMERCE
BUREAU OF STANDARDS
George K. Burgess, Director

CIRCULAR OF THE BUREAU OF STANDARDS, No. 101

PHYSICAL PROPERTIES OF MATERIALS

I. STRENGTHS AND RELATED PROPERTIES OF METALS AND WOOD

(Second Edition)

April 23, 1924



PRICE, 40 CENTS

Sold only by the Superintendent of Documents, Government Printing Office
Washington, D. C.

WASHINGTON
GOVERNMENT PRINTING OFFICE
1924



Scientific and Technical Laboratories of the Bureau of Standards.

Investigations on the physical properties of metals and woods are made in the industrial laboratories shown in the upper left of this illustration.

DEPARTMENT OF COMMERCE
BUREAU OF STANDARDS
George K. Burgess, Director

CIRCULAR OF THE BUREAU OF STANDARDS, No. 101

PHYSICAL PROPERTIES OF MATERIALS

I. STRENGTHS AND RELATED PROPERTIES OF METALS AND WOOD

(Second Edition)

April 23, 1924



PRICE, 40 CENTS

Sold only by the Superintendent of Documents, Government Printing Office
Washington, D. C.

WASHINGTON
GOVERNMENT PRINTING OFFICE

1924

PHYSICAL PROPERTIES OF MATERIALS.

I. STRENGTH AND RELATED PROPERTIES OF METALS AND WOOD.

ABSTRACT.

This circular contains the values for tensile, compressive, and shearing strengths; ductility; modulus of elasticity; and other related properties of pure metals and their alloys and of wood. In addition to these the properties of metals at elevated temperatures, their fatigue and impact properties, and the effect of heat treatment and cold working are given.

Other properties and uses of less commonly used metals are described briefly. Graphical representation is used in many cases to show the change of the properties of a material with changing conditions. References to the sources are given for all values in this circular.

CONTENTS.

	Page.
I. Introduction	8
II. Scope of the work	8
III. Sources of included data	8
IV. Acknowledgments	9
V. Test specimens and conditions	9
VI. Definitions	9
1. Proportional limit	9
2. Elastic limit	11
3. Yield point	11
4. Tensile, compressive, or shearing strength	11
5. Modulus of rupture	11
6. Torsional strength (or modulus of rupture in torsion)	11
7. Elongation	12
8. Reduction	12
9. Poisson's ratio	12
10. Modulus of elasticity in tension or compression	12
11. Modulus of elasticity in shear	12
12. Brinell hardness number	12
13. Shore scleroscope hardness	13
14. Erichsen value	13
15. Bend test	13
16. Impact value	13
17. Fatigue resistance	14
18. Resilience	14
19. Ductile materials	14
20. Plastic materials	14
21. Malleable materials	14
22. Brittle materials	14
23. Stiff materials	14
24. Flexible materials	15
25. Tough materials	15
26. Soft materials	15
27. Hard materials	15
VII. Texts on strength of materials	15
VIII. Physical properties of metals (Tables 1 to 42)	16
IX. Nomenclature of copper alloys	37

	Page.
X. Iron and steel specifications	77
XI. Alloy steels	101
XII. Fatigue properties of steel	139
XIII. Manila rope	169
XIV. Wood	170
List of references	194
Index	199

TABLES.

Table 1.—Tensile and thermal properties of metals.	16
Table 2.—Tensile properties of sheet aluminum	18
Table 3.—Ductility and hardness of sheet aluminum	18
Table 4.—Tensile requirements of soft and annealed copper wire.	35
Table 5.—Tensile requirements of medium hard-drawn copper wire	35
Table 6.—Tensile requirements of hard-drawn and hard-rolled copper wire.	36
Table 7.—Tensile requirements of copper plates.	36
Table 8.—Tensile requirements of rolled copper	36
Table 9.—Classification of ferrous metals in principal European languages.	74
Table 10.—Properties of semisteel.	85
Table 11.—Tensile strength of commercial steel music wire.	98
Table 12.—Properties of high tensile steel wire.	98
Table 13.—Tensile requirements of steel wire rope	99
Table 14.—Tensile strength of steel wire rope.	101
Table 15.—Effect of heat treatment on properties of chromium steels.	105
Table 16.—Correlation between the tensile strength of steel and its hardness.	136
Table 17.—Impact properties of some metals.	137
Table 18.—Impact properties of carbon steels.	137
Table 19.—Effect of low temperatures on hardness and impact resistance of metals.	138
Table 20.—Effect of temperature on the impact resistance of annealed steels (chemical composition of tested steels).	139
Table 21.—Fatigue properties of manganese and aluminum bronze (chemical composition of tested samples).	139
Table 22.—Fatigue properties of carbon and alloy steels (chemical composition and heat treatment of tested steels).	142
Table 23.—Effect of high temperature on the tensile properties of cast iron (chemical composition of tested materials).	145
Table 24.—Effect of high temperature on the tensile strength of cast iron.	146
Table 25.—Effect of repeated heating and cooling on tensile strength of cast iron.	146
Table 26.—Effect of temperature on the tensile properties of some metals (chemical composition of tested metals).	146
Table 27.—Effect of temperature on torsional properties of some metals (chemical composition of tested metals).	148
Table 28.—Effect of temperature on the tensile properties of some metals.	149
Table 29.—Effect of temperature on the tensile strength of high-speed steel.	151
Table 30.—Flow of steels under constant load at high temperatures.	151
Table 31.—Flow of steels under constant load at high temperatures (chemical composition and heat treatment of tested steels).	152
Table 32.—Tensile strength of steels at elevated temperatures under rapidly applied load.	159
Table 33.—Tensile properties of molybdenum wire at high temperatures.	160
Table 34.—Tensile properties of nickel wire at high temperatures.	161
Table 35.—Compression tests of some steels at high temperatures (chemical composition of tested steels).	161
Table 36.—Compression tests of white metal bearing alloys at elevated temperatures	165
Table 37.—Chemical composition of white-metal bearing alloys.	165
Table 38.—Tensile properties of some bearing alloys at elevated temperature	165

	Page.
Table 39.—Elasticity at high temperatures (chemical composition of tested metals).....	165
Table 40.—Elasticity at low temperatures.....	167
Table 41.—Effect of temperature on modulus of elasticity of annealed metals.....	167
Table 42.—Effect of annealing temperature on elastic properties of cold-rolled brass tubes..	168
Table 43.—Weight and strength of manila rope.....	169
Table 44.—Strength of manila rope.....	169
Table 45.—Results of tests on 126 species of wood tested in a green condition.....	172
Table 46.—Results of tests on 126 species of wood tested in an air-dry condition.....	184
Table 47.—Approximate figures for change of properties of woods with change of moisture content.....	194

ILLUSTRATIONS.

Fig. 1.—Standard specimens used and recommended by the structural and engineering mechanics section, Bureau of Standards.....	10
Fig. 2.—Effect of temperature on the tensile properties of aluminum.....	18
Fig. 3.—The tensile properties of aluminum-copper sand-cast alloys.....	30
Fig. 4.—The tensile properties of aluminum-copper chill-cast alloys.....	30
Fig. 5.—The tensile properties of aluminum-copper alloys in the form of sheet 0.05-inch (1.27 mm) thick.....	30
Fig. 6.—The tensile properties of aluminum-copper alloys; 1¼-inch (31.7 mm) diameter bars hot rolled from 3-inch (76.2 mm) ingots.....	30
Fig. 7.—Variation of the tensile properties of duralumin with temperature.....	30
Fig. 8.—Effect of annealing on the tensile properties of duralumin.....	30
Fig. 9.—Effect of cold working on the tensile properties of duralumin.....	31
Fig. 10.—The tensile properties of aluminum-zinc sand-cast alloys.....	31
Fig. 11.—The tensile properties of aluminum-zinc chill-cast alloys.....	31
Fig. 12.—The tensile properties of aluminum-zinc alloys; 1¼-inch (31.7 mm) diameter bars hot rolled from 3-inch (76.2 mm) ingots.....	31
Fig. 13.—Effect of high temperatures on the tensile properties of copper.....	31
Fig. 14.—Fatigue properties of aluminum and manganese bronzes.....	37
Fig. 15.—Correlation between the heat treatment and the tensile properties of nickel-silvers..	66
Fig. 16.—Correlation between the heat treatment and the tensile properties of nickel-silvers..	67
Fig. 17.—Effect of drawing temperature on the tensile properties of steel.....	79
Fig. 18.—Effect of drawing temperature on the tensile properties of steel.....	80
Fig. 19.—Effect of drawing temperature on the tensile properties of steel.....	80
Fig. 20.—Effect of drawing temperature on the tensile properties of steel.....	81
Fig. 21.—Effect of drawing temperature on the tensile properties of steel.....	81
Fig. 22.—Effect of drawing temperature on the tensile properties of steel.....	82
Fig. 23.—Effect of drawing temperature on the tensile properties of steel.....	82
Fig. 24.—Effect of drawing temperature on the tensile properties of steel.....	83
Fig. 25.—Effect of drawing temperature on the tensile properties of steel.....	83
Fig. 26.—Effect of carbon content on the strength of Bessemer steel.....	93
Fig. 27.—Effect of carbon content on the mechanical properties of hot rolled and annealed steel.....	93
Fig. 28.—Effect of drawing temperature on the tensile properties of stainless steel.....	110
Fig. 29.—Effect of drawing temperature on the tensile properties of chrome-vanadium steel..	110
Fig. 30.—Effect of drawing temperature on the tensile properties of chrome-nickel steel....	111
Fig. 31.—Effect of drawing temperature on the tensile properties of nickel steel.....	111
Fig. 32.—Effect of drawing temperature on the tensile properties of tungsten steel.....	120
Fig. 33.—Fatigue properties of carbon and alloy steels.....	140
Fig. 34.—Fatigue properties of carbon and alloy steels compared with other properties.....	140
Fig. 35.—Fatigue properties of carbon and alloy steels compared with other properties.....	141
Fig. 36.—Correlation between the endurance limit and other properties of steels.....	143
Fig. 37.—Correlation between the endurance limit and the tensile properties of steels.....	144

	Page.
Fig. 38.—Tensile properties of cold-rolled boiler plate at elevated temperatures.....	147
Fig. 39.—Tensile properties of hot-rolled boiler plate at elevated temperatures.....	147
Fig. 40.—Tensile properties of cold, hot, and blue rolled boiler plate at elevated temperatures as determined on specimens cut across the direction of rolling.....	148
Fig. 41.—Tensile properties at elevated temperatures of 0.38 per cent carbon steel.....	150
Fig. 42.—Tensile properties at elevated temperatures of chromium-vanadium steel.....	150
Fig. 43.—Tensile properties at elevated temperatures of nickel-chromium steel.....	152
Fig. 44.—Tensile properties at elevated temperatures of 3/4 per cent nickel steel.....	153
Fig. 45.—Tensile properties of Monel metal and nickel at high temperatures.....	153
Fig. 46.—Variation of tensile properties of rolled zinc, with temperature.....	153
Fig. 47.—Effect of temperature on tensile properties of some metals.....	154
Fig. 48.—Effect of temperature on torsional properties of some metals.....	155
Fig. 49.—Effect of temperature on the tensile properties of nickel, zinc, magnesium, tin, cadmium, and lead.....	156
Fig. 50.—Effect of high temperature on the tensile properties of steels.....	157
Fig. 51.—Effect of high temperature on the tensile properties of steels.....	158
Fig. 52.—Compression tests of wrought iron at elevated temperatures.....	162
Fig. 53.—Compression tests of 0.10 per cent carbon steel at elevated temperatures.....	162
Fig. 54.—Compression tests of 0.32 per cent carbon steel at elevated temperatures.....	163
Fig. 55.—Compression tests of 0.95 per cent carbon steel at elevated temperatures.....	163
Fig. 56.—Compression tests of chrome-nickel steel at elevated temperatures.....	164
Fig. 57.—Compression tests of chrome-nickel steel at elevated temperatures.....	164
Fig. 58.—Effect of temperature on the modulus of elasticity in shear.....	166
Fig. 59.—Effect of temperature on the modulus of elasticity in shear.....	166
Fig. 60.—Effect of temperature on the impact resistance of annealed steels.....	167

LIST OF ABBREVIATIONS USED IN THIS CIRCULAR.

Tensile strength.....	tns. str.	Feet.....	ft.
Elastic limit.....	el. lim.	Inches.....	in.
Proportional limit.....	pro. lim.	Meter.....	m
Yield point.....	ylt. pnt.	Centimeter.....	cm
Elongation.....	elong.	Millimeter.....	mm
Reduction.....	red.	Square inch.....	in. ²
Brinell hardness.....	Bhn.	Square centimeter.....	cm ²
Scleroscope hardness.....	scl.	Square millimeter.....	mm ²
Compression.....	comp.	Inch-pound.....	in.-lb.
Transverse.....	trv.	Kilogram meter.....	kgm
Torsion.....	tor.	Cubic inch.....	in. ³
Rupture.....	rupt.	Cubic centimeter.....	cm ³
Impact.....	imp.	Revolutions per minute.....	r. p. m.
Modulus of elasticity.....	mod. el.	Thousand.....	th.
Heat treatment.....	ht. tr.	Degrees (temperature).....	°
Pounds.....	lb.	Centigrade.....	C.
Grains.....	gr	Fahrenheit.....	F.
Kilogram.....	kg	Average.....	avg.
Gram.....	g		

LIST OF CONVERSION FACTORS USED IN THIS CIRCULAR.

1 m = 3.281 ft.	1 kg/m ³ = 0.06243 lb./ft. ³
1 cm = 0.3937 in.	1 kg/cm ³ = 14.223 in. lb./in. ³
1 kg = 2.2046 lb.	
1 kg/mm ² = 1,422.3 lb./in. ²	η° C. = $\left(\frac{9}{5}\eta + 32\right)$ ° F
1 kgm = 7.233 ft.-lb.	

Chemical Symbols.

Smithsonian Physical Tables, 7th ed., 1920.]

Substance:	Symbol.	Substance—Continued.	Symbol.
Aluminum.....	Al	Manganese.....	Mn
Antimony.....	Sb	Mercury.....	Hg
Argon.....	A	Molybdenum.....	Mo
Arsenic.....	As	Neodymium.....	Nd
Barium.....	Ba	Neon.....	Ne
Bismuth.....	Bi	Nickel.....	Ni
Boron.....	B	Niton.....	Nt
Bromine.....	Br	Nitrogen.....	N
Cadmium.....	Cd	Osmium.....	Os
Caesium.....	Cs	Oxygen.....	O
Calcium.....	Ca	Palladium.....	Pd
Carbon.....	C	Phosphorus.....	P
Cerium.....	Ce	Platinum.....	Pt
Chlorine.....	Cl	Potassium.....	K
Chromium.....	Cr	Praseodymium.....	Pr
Cobalt.....	Co	Radium.....	Ra
Columbium.....	Cb	Rhodium.....	Rh
Copper.....	Cu	Rubidium.....	Rb
Dysprosium.....	Dy	Ruthenium.....	Ru
Erbium.....	Er	Samarium.....	Sa
Europium.....	Eu	Scandium.....	Sc
Fluorine.....	F	Selenium.....	Se
Gadolinium.....	Gd	Silicon.....	Si
Gallium.....	Ga	Silver.....	Ag
Germanium.....	Ge	Sodium.....	Na
Glucinum.....	Gl	Strontium.....	Sr
Gold.....	Au	Sulphur.....	S
Hafnium.....	Hf	Tantalum.....	Ta
Helium.....	He	Tellurium.....	Te
Holmium.....	Ho	Terbium.....	Tb
Hydrogen.....	H	Thallium.....	Tl
Indium.....	In	Thorium.....	Th
Iodine.....	I	Thulium.....	Tm
Iridium.....	Ir	Tin.....	Sn
Iron.....	Fe	Titanium.....	Ti
Krypton.....	Kr	Tungsten.....	W
Lanthanum.....	La	Uranium.....	U
Lead.....	Pb	Vanadium.....	V
Lithium.....	Li	Xenon.....	Xe
Lutecium.....	Lu	Ytterbium.....	Yb
Magnesium.....	Mg	Yttrium.....	Yt
		Zinc.....	Zn
		Zirconium.....	Zr

I. INTRODUCTION.

The compilation of the information contained in this circular was begun in response to a request in 1920 from the Smithsonian Institution for the assistance of the Bureau of Standards in the revision of the Smithsonian Physical Tables.

Due to the frequent requests for information on the physical properties of materials received at the Bureau of Standards, many of which could be answered by referring to the tables prepared for the Smithsonian Institution, they were published as Physical Properties of Materials, Circular No. 101, of the Bureau of Standards.

The first edition was compiled by H. A. Anderson, assistant engineer physicist. The unprecedented number of requests for the first edition, which soon exhausted the supply, led to the preparation of this edition.

In response to the request printed on the cover of the first edition of this circular for constructive criticism, many letters have been received from engineers in testing laboratories, manufacturing concerns, engineering offices, and technical societies and institutions. It was evident from these letters that the writers believed that a publication of this kind is greatly needed, as the data contained in it had not previously been easily accessible. In so far as possible all the suggested improvements have been made in this edition.

II. SCOPE OF THE WORK.

This edition, which has been enlarged to about four times the size of the first, includes the additional material which has appeared in the technical literature during the past few years, and, by enlarging its scope, it includes the properties of metals at elevated temperatures, their fatigue and impact resistance, as well as other useful data.

The physical properties of wood, obtained by the Forest Products Laboratory, have also been included.

In many cases graphical representation has been used to show the effect of heat treatment, temperature, and other factors on the property of a material. Often these graphs are reproduced with little alteration from the original source. Values may be read from these curves with an accuracy sufficient for the practical use of the curves. All values are given in both metric and English systems.

III. SOURCES OF INCLUDED DATA.

The data were gathered from three sources: (1) Experimental data published in the technical periodicals and engineering handbooks; (2) specifications prepared by the technical societies and Government departments; and (3) unpublished experimental data of the Bureau of Standards and those obtained from the manufacturers of the material.

The strengths and related properties of most engineering materials vary between wide limits; any value assigned to a material represents a materials engineer's opinion as the most probable value that can be obtained under given circumstances. These values should be looked upon as representative of material rather than as characterizing a single specimen.

The compiler has undertaken to select reliable sources of information; he has tried to conscientiously reproduce with accuracy the values given and the opinions expressed in the original source, reference to which is given in all cases in this circular.

IV. ACKNOWLEDGMENTS.

This edition was compiled and the charts drawn by S. N. Petrenko, associate mechanical engineer. Credit is due H. L. Whittemore, under whose supervision the work was done, and to all those who have assisted in putting the data in its present form.

V. TEST SPECIMENS AND CONDITIONS.

In general, test specimens used in the determination of the tabulated data were in conformity with the recommendations of the American Society for Testing Materials.¹ As a rule, tensile specimens were of 12.8 mm, or 0.505 inch diameter, and 50.8 mm, or 2 inches gauge length. The sizes of compressive and transverse specimens are usually shown accompanying the tables. Figure 1 shows the test specimens used and recommended by this bureau.

All data shown in these tables were determined at ordinary room temperature, averaging 20° C. (68° F.) unless otherwise stated.

VI. DEFINITIONS.

The following definitions represent the practice of the bureau in reporting data on physical properties of engineering materials and also govern the use of the terms in this circular. In tensile and compressive tests the stresses are computed on the basis of the original cross-sectional area of the specimen; in transverse and torsional tests the stress in the extreme fiber is computed from the flexural and torsional formulas.

Definitions of mechanical properties of materials and methods of testing in use at the bureau are in general conformity with the standard methods for testing of the American Society for Testing Materials.²

1. PROPORTIONAL LIMIT.

Stress at which the deformation ceases to be proportional to the load as determined by strainometer (extensometer for tension, compressometer for compression, and deflectometer for transverse tests, value being read from plotted results).

¹ A. S. T. M. Standards Handbook; 1921; and triennially thereafter, especially Standard methods for testing, p. 841.

² A. S. T. M. Standards, pp. 841-852; 1921.

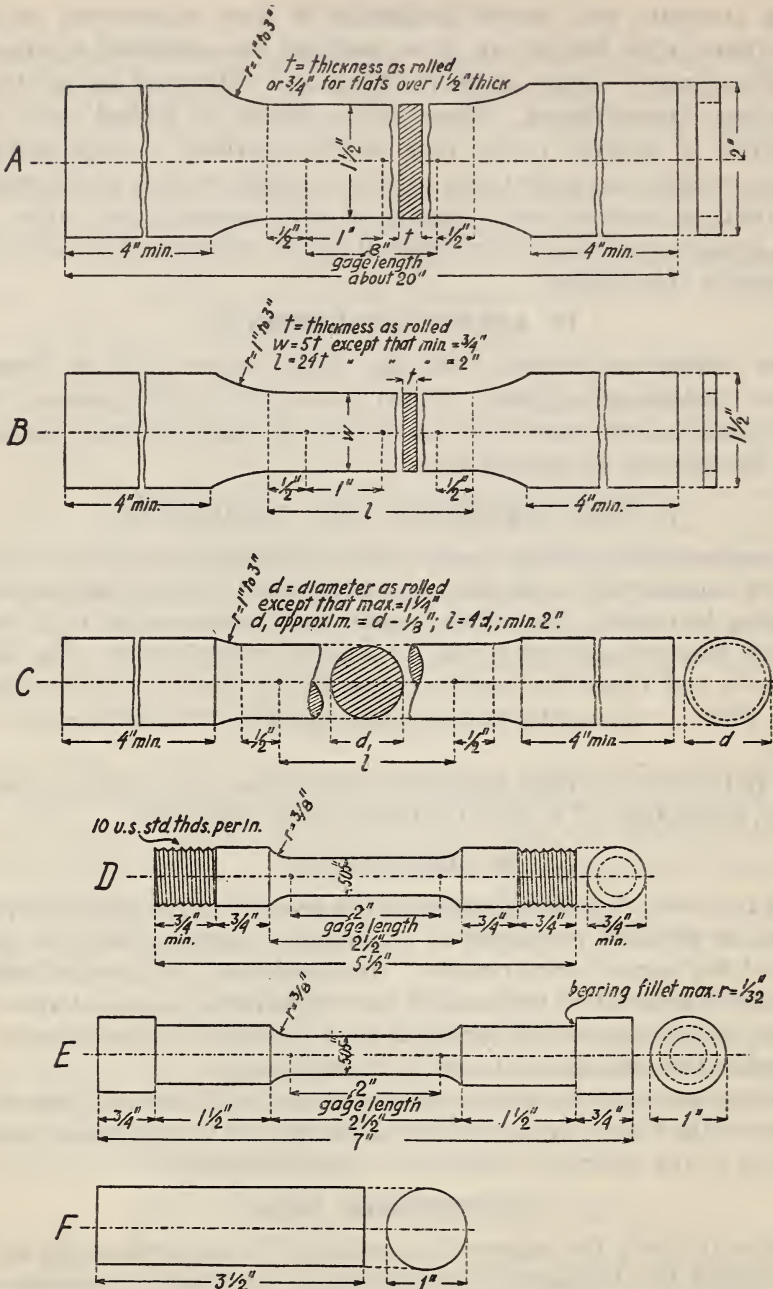


FIG. 1.—Standard specimens used and recommended by structural and engineering mechanics section, Bureau of Standards.

A, tension, flat, for wedge grips, for rolled plates over $\frac{1}{4}$ in. (6.35 mm) thick; B, tension, flat, $\frac{1}{4}$ in. (6.35 mm) thick or less; C, tension, round, for wedge grips, for rolled rods and bars; D, tension, round, for accurate tests, except determination of modulus of elasticity; E, tension, round (preferable form) for accurate tests, except determination of modulus of elasticity; F, compression, round, for all determinations except modulus of elasticity.

2. ELASTIC LIMIT.

In tensile and compressive tests: The stress at which the initial permanent elongation or shortening of the gauge length occurs, as shown by an instrument of high precision (determined from set readings with extensometer or compressometer). In transverse tests: The extreme fiber stress at which the initial appreciable permanent deflection occurs as determined with deflectometer.

Tests are rarely made to determine the elastic limit, since such tests involve repeated application and release of load and require considerable time. For practical purposes the elastic limit may be regarded as equal to the proportional limit.

3. YIELD POINT.

Stress at which marked increase in deformation of specimen occurs without increase in load as determined usually by drop of beam or with dividers for tensile, compressive, or transverse tests. (Reported for all tests of ductile materials.)

4. TENSILE, COMPRESSIVE, OR SHEARING STRENGTH.

Maximum stress developed in the material during test, load being referred to the original cross section.

5. MODULUS OF RUPTURE.

Maximum stress in the extreme fiber of a beam tested to rupture, as computed by the empirical application of the flexural formula to stresses above the transverse proportional limit. For simple rectangular beam with concentrated center load it equals

$$\frac{1.5 \times \text{load} \times \text{span}}{\text{area} \times \text{depth}}$$

6. TORSIONAL STRENGTH (OR MODULUS OF RUPTURE IN TORSION).

Maximum stress in the extreme fiber of a specimen tested to rupture as computed by the empirical application of the torsional formula to stresses above the torsional proportional limit. For a round specimen it equals

$$S = \frac{5.1 \times \text{twisting moment}}{\text{diameter}^3}$$

In ductile materials the stress at rupture may be considered uniformly distributed over the cross-sectional area and the above formula assumes the form

$$S = \frac{3.82 \times \text{twisting moment}}{\text{diameter}^3}$$

7. ELONGATION.

The percentage of elongation is found by dividing the increase of length after rupture by the original gauge length. The percentage of elongation depends on the gauge length. The elongation indicates the ductility of the material.

8. REDUCTION.

The percentage of reduction is found as the ratio of the difference between the original and broken area of cross section to the original area. Reduction of area indicates generally the ductility of material.³

9. POISSON'S RATIO.

The ratio of lateral contraction per unit of diameter to longitudinal extension per unit of length of a bar under terminal tension within the elastic limit of material.

10. MODULUS OF ELASTICITY IN TENSION OR COMPRESSION.⁴

Ratio of stress within the proportional limit to the corresponding strain as determined with a precise extensometer. Accurate determinations of the modulus of elasticity are made with a gauge length at least 8 in. (203.2 mm) in length.

11. MODULUS OF ELASTICITY IN SHEAR.⁵

Ratio of stress within the proportional limit to the corresponding angular strain (in radians). The following theoretical relation exists between the modulus of elasticity in shear and the modulus of elasticity

$$G = \frac{E}{2(1 + \lambda)},$$

where G is the modulus of elasticity in shear, E modulus of elasticity, and λ Poisson's ratio.

It is difficult to make a direct experimental determination of G on account of the presence of other stresses. It is usually determined by the torsion of a round bar.

12. BRINELL HARDNESS NUMBER.

Ratio of load on a sphere used to indent the material to be tested to the area of the spherical indentation produced. The standard sphere used is a 10 mm diameter hardened steel ball. The loads used are 3,000 kg (6,615 pounds) for steel and 500 kg (1,102 pounds) for softer metals, and the time of application of load is 30 seconds. Values shown in the tables are based

³ Some authors consider the reduction of area as a measure of toughness.

⁴ Generally known as Young's modulus (is called in this circular modulus of elasticity).

⁵ Often called the modulus of rigidity.

on spherical areas computed in the main from measurements of the diameters of the spherical indentations, by the following formula:

$$\text{Bhn} = \frac{P}{\pi t D} = \frac{P}{\pi D \left(\frac{D}{2} - \sqrt{\frac{D^2}{4} - \frac{d^2}{4}} \right)}$$

P = load in kg, t = depth of indentation, D = diameter of ball, and d = diameter of indentation, all lengths being expressed in millimeters. Brinell hardness values have a certain relation to tensile strength, and hardness determinations may be used to determine tensile strengths approximately by employing the proper conversion factor for the material under consideration. See Table 16. (Data after Abbott.)

13. SHORE SCLEROSCOPE HARDNESS.

Height of rebound of a diamond-pointed hammer falling on the object from a fixed height through a tube under the acceleration due to its own weight. The hardness is measured on an empirical scale on which the average hardness of martensitic high-carbon steel equals 100. On very soft metals a "magnifier" hammer is used in place of the commonly used "universal" hammer, and values may be converted to the corresponding "universal" value by multiplying the reading by 4/7. The scleroscope hardness, when properly determined, is considered an index of the tensile strength of the metal tested.

14. ERICHSEN VALUE.

Index of forming qualities of sheet metal. The test is conducted by supporting the sheet on a circular ring and deforming it at the center of the ring by a spherical-pointed tool. The depth of impression (or cup), in millimeters, required to obtain fracture is the Erichsen value for the metal. Erichsen standard values for trade qualities of soft metal sheets, corresponding to various sheet thicknesses, are furnished by the manufacturer of the machine.⁶

15. BEND TEST.

Angle through which the material can be bent without fracture or the number of bendings around a predetermined diameter is recorded. In some cases a minimum diameter around which the test piece can be bent through a certain angle is determined. Very valuable test indicating the ductility of malleable metals.

16. IMPACT VALUE.

Indicates the shock-resisting qualities of material. Is of particular value in ascertaining the influence of heat treatment. Impact value depends on the form of the specimen.⁷ The data in this circular are given (unless

⁶ Proc. A. S. T. M., 17 (2), p. 200; 1917.

⁷ For the description of impact testing machines and specimens used by various investigators see H. I. Whittemore, Bibliography on impact testing, Proc. A. S. T. M.; 1922.

otherwise stated) for standard international Charpy specimen, 10 by 10 by 40 mm (0.394 by 0.394 by 1.575 inches, the last value being the distance between the supports).

17. FATIGUE RESISTANCE.

Resistance of material to a load, which is applied and removed in whole or in part many times and at short intervals. Fatigue resistance is a very valuable property of materials. Some engine parts are subjected to a very high number of reversals of stress during the life of the machine.

Numerical values for fatigue resistance may be given in two ways: (1) The "stress" at which a specimen endures a definite number of cycles of stress; (2) The "endurance limit," if such exists; that is, the maximum stress which the specimen will endure for any number of repetitions.⁸

18. RESILIENCE.

The potential energy of deformation of a body. The resilient materials are those which are capable of absorbing elastically a large amount of work done by the applied load. The resilience depends upon the elastic limit of material and upon its modulus of elasticity (in tension or in shear).

19. DUCTILE MATERIALS.

Ductile materials are those which are capable of undergoing considerable permanent deformation while subjected to tensile stresses.

20. PLASTIC MATERIALS.

Plastic materials are those which are capable of undergoing considerable permanent deformation under compressive stresses.

21. MALLEABLE MATERIALS.

Malleable materials are those which can be hammered into thin sheets without rupture.

22. BRITTLE MATERIALS.

Brittle materials are those which show little permanent deformation when stressed to rupture.

23. STIFF MATERIALS.

Stiff materials are those which have a high modulus of elasticity or a high modulus of elasticity in shear. They deform little, if subjected to stresses not exceeding the elastic limit.

⁸ Description of fatigue testing machines may be found in the following publications: (1) McAdam, jr., *Alternating torsion machine*, *Iron Age*, 100; 1917; (2) McAdam, jr., *Impact endurance testing machine*, *Jour. Am. Soc. Nav. Eng.*, November, 1917; (3) Arnold, *Alternating testing machine*, *Proc. Inst. Mech. Eng.*, pt. 3; 1904; (4) Farmer, *Rotating beam testing machine*, *Proc. A. S. T. M.*; 1919; (5) Landgraf Turner, *Alternating stress machine*, *Am. Mach. Apr.* 22, 1919; (6) Upton Lewis, *Am. Mach.*, October, 1912; (7) Stanton, *Alternating stress machine*, *Proc. Inst. Civ. Eng.*, 166; (8) Stromeier, *Alternating torsion machine*, *Proc. Roy. Soc. A.*, 90; 1914; (9) Koppers, *Wisconsin rotating beam machine*, *Univ. Ill., Eng. Exp. Sta. Bul. No. 120*; (10) Smith, *Alternating tension and compression machine*, *Engineering*, 88, p. 105; (11) Olsen-Foster, *Reversed torsion testing machine*, *Univ. Ill. Eng. Exp. Sta. Bul. No. 120*; (12) White-Souther, *Chem. and Met. Eng.*, December, 1921; (13) Haigh, *Alternating testing machine*, *Engineering*, November, 1912; and (14) Olsen, *Vibrating testing machine*, *Electr. Rev.*, April, 1908.

24. FLEXIBLE MATERIALS.

Flexible materials are those which have a low modulus of elasticity or a low modulus of elasticity in shear. They can be deformed considerably by bending, twisting, etc., within the elastic limit of material.

25. TOUGH MATERIALS.

Tough materials are those which will withstand heavy shocks or will absorb a large amount of energy.

26. SOFT MATERIALS.⁹

Soft materials are those which offer little resistance to indenting or scratching.

27. HARD MATERIALS.⁹

Hard materials are those which offer great resistance to indenting or scratching.

VII. TEXTS ON STRENGTH OF MATERIALS.

For an interpretation of the physical significance of the elastic limit, proportional limit, yield point, and other properties, reference may be made to any good text on mechanics of materials, including the following:

- Andrews, The strength of materials; 1916. Van Nostrand & Co., New York.
Boyd, Strength of materials; 1917. McGraw-Hill Book Co., New York.
Burr, The elasticity and resistance of the materials of engineering; 1915. John Wiley & Sons, New York.
Ewing, Strength of materials; 1906. Putnam Co., London.
Goodman, Mechanics applied to engineering; 1899. Longmans, Green & Co., London.
Johnson, Materials of construction; 1918. John Wiley & Sons, New York.
Lanza, Applied mechanics; 1910. John Wiley & Sons, New York.
Merriman, Mechanics of materials; 1915. John Wiley & Sons, New York
Mills, Materials of construction; 1922. John Wiley & Sons, New York.
Moore, Materials of engineering; 1917. McGraw-Hill Book Co., New York
Morley, Strength of materials; 1920. Longmans, Green & Co., London.
Murdock, Strength of materials; 1911. John Wiley & Sons, New York.
Slocum, Resistance of materials; 1914. Ginn & Co., Boston.
Unwin, The testing of materials of construction; 1910. Longmans, Green & Co., London.
Love, A treatise on the mathematical theory of elasticity; 1906. Cambridge, University Press.
Fuller and Johnston, Strength of materials; 1919. J. Wiley & Sons, New York.
Martens, Handbook of testing materials; 1899. J. Wiley & Sons, New York.
Bach, Elasticität und festigkeit; 1922. Berlin.
Lorenz, Technische elasticitätslehre; 1913. München.
Föppl, Vorlesungen über technischen mechanik; 1900-1912. Leipzig.
Record, Mechanical properties of wood; 1914. New York.
Bulletin No. 556, Forest Service, U. S. Department of Agriculture; 1917.

⁹ "Soft" and "hard" are indefinite terms which acquire a definite relative meaning when a definite hardness test is specified.

VIII. PHYSICAL PROPERTIES OF METALS.
TABLE 1.—Tensile and Thermal Properties of Metals.

Material and composition.	Condition.	Specific gravity.	Tensile properties						Elongation in 50.8 mm or 2 inches.	Hardness number.	Thermal properties.			Reference.			
			Metric kg./mm. ²		English lb./in. ²		Reduction of area.	Brinell.			Melting point.	Linear coefficient of expansion $\times 10^6$ (per 1°C.).	Casting shrinkage.				
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.									Yield point.	Tensile strength.	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Aluminum 1: Pure— Al, 99.0 or better.	Sand cast at 700°C. (1,292° F.). Sheet annealed; all gauges 1/4 in. (6.35 mm) or less. Sheet, full hard. Bars and wire, full hard. Cast, 1 in. (25.4 mm) diameter. Cast, chill shaped sand. Rolled, 13/16 in. (20.6 mm) diameter. Rolled hard (sheet). Sheet, 0.08 in. (2.03 mm) soft. Drawn, 13/16 in. (20.6 mm) diameter.	2.11 2.11	2.11 2.11	8.4-9.1 8.4-9.8	3,000 3,000	12,000-13,000 12,000-14,000	5,150 5,600 14,600	11,700 11,000 16,100	37 24 30.5	Per ct. 30-35 20-35	Per ct. 35-40 50-75	21-24 22-26	6-9 4-6	°C.	23.0	mm/m in./ft.	(1) (1) (1) (110) (110) (110) (110) (110) (110)
Aluminum 2: Full, 99.3	Normalized, mechanically worked and annealed at 400°C. (752° F.). Cast, sand	2.70	2.70	8.8-10.6	8,000-9,000	12,500-15,000	8,500	11,000-13,000	10-40	20-30	4 23-28	6 4-6	659 (1,218 F.)				(168) (168)

(Properties vary with the gauge.)

Cast, chill.....	6.3	8.4-9.8	9,000	12,000-14,000	15-25				(168)
Sheet, annealed.....	5.6-6.3	8.4-10.6	8,000-9,000	12,000-15,000	12-35	20-30			(168)
Sheet, half hard.....	6.3-8.4	12.7-15.5	9,000-12,000	18,000-22,000	5-12	20-30	13-15		(168)
Sheet, hard.....	8.4-10.6	15.5-17.6	12,000-15,000	22,000-25,000	1-7	20-30			(168)
Bars, hard.....	8.4-10.6	17.6-21.6	12,000-15,000	25,000-35,000		30-40			(168)
Wire, hard.....	11.2-23.2	17.6-38.7	12,000-35,000	22,000-55,000		40-50			(168)
Aluminum ⁶									(11)
Cast.....									(11)
Rolled.....									(11)

¹ Average value for modulus of elasticity 7,030 kg/mm², or 10,000,000 lb./in.². No values for heat treated Al are given, as pure Al is not improved by heat treatment.

² Smithsonian Physical Tables, 7th edition; 1920.

³ The mean value of modulus of elasticity for bars and wire is given by Britlee at 17° C. (62.6° F.), 6,000 kg/mm² (9,810,000 lb./in.²). Landolt-Bornstein tables (1912) give for modulus of elasticity 6,300-7,500 kg/mm² (8,960,000-10,670,000 lb./in.²). K. Koch and C. Danneker (see Fig. 58) give for modulus of elasticity in shear at 20° C. (68° F.), 750 kg/mm² (3,870,000 lb./in.²). According to Winkelmann's Handbuch der Physik, 1, 1, 1908; modulus of elasticity of cast aluminum 6,570 kg/mm² (9,340,000 lb./in.²); modulus of elasticity of drawn aluminum 7,540 kg/mm² (10,725,000 lb./in.²); modulus of elasticity in shear of cast aluminum 2,480 kg/mm² (3,670,000 lb./in.²). Poisson's ratio (Cardant) is 0.63. Average ultimate compressive strength of cast aluminum (Eilmendorf) 47.1 kg/mm² (67,000 lb./in.²). Eilmendorf gives the following formula for alternating stress of cast aluminum of tensile strength averaging 10.6 kg/mm² (15,000 lb./in.²): $S = 43,000 \times R^{-0.113}$, where S = fiber stress in lb./in.² and R = number of reversals to rupture (White-Souther machine).

Ericksen values:

B. & S. gauge. 28 24 20 16 12

Depth of cup mm 5.5-7.5 7.0-8.0 7.5-9.0 9.0-10.5 10.5-12.0.

⁴ 500 kg (1,102 lb.) load.

⁵ Magnifying hammer.

⁶ Shearing strength: Cast 8.4 kg/mm² (12,000 lb./in.²); rolled 11.3 kg/mm² (16,000 lb./in.²).

TABLE 2.—Tensile Requirements of Sheet Aluminum—Specification Values.

[Sheet: A. S. T. M., B25-19 T. Al min., 99.0; minimum strengths and elongation.]

Gauge (B. & S.).	Thickness.		Temper number.	Hardness.	Tensile strength.		Elongation in 50.8 mm (2 in.).
	mm	in.			kg/mm ²	lb./in. ²	
12-16, inclusive.....	2.052-1.290	0.0808-0.0508	1	Soft, annealed.....	8.8	12,500	Per cent. 30.0
			2	Half hard.....	12.7	18,000	7.0
			3	Hard.....	15.5	22,000	4.0
17-22, inclusive.....	1.152- .643	.0453- .0253	1	Soft, annealed.....	8.8	12,500	20.0
			2	Half hard.....	12.7	18,000	5.0
			3	Hard.....	17.6	25,000	2.0
23-26, inclusive.....	.574- .404	.0226- .0159	1	Soft, annealed.....	8.8	12,500	10.0
			2	Half hard.....	12.7	18,000	5.0
			3	Hard.....	21.1	30,000	2.0

¹ Sheets of temper No. 1 to withstand being bent double in any direction and hammered flat.
² Sheets of temper No. 2 to bend 180° about radius equal to thickness without cracking.

NOTE.—Tensile test specimen to be taken parallel to the direction of cold-rolling of the sheet.

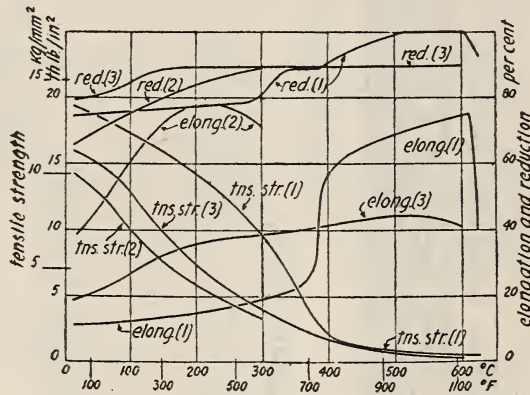


FIG. 2.—Effect of temperature on the tensile properties of aluminum.

Curves (1) for rolled unannealed sample of 99.56 per cent aluminum 6.3 mm (1/4 in.) round bars; G. D. Bengough, J. Inst. Met., 7, p. 123; 1912.

Curves (2) for annealed sample sheet, 8 mm (0.315 in.) thick; R. Baumann, Mitteilungen über Forschungsarbeiten auf dem Gebiete des Ingenieurwesens, No. 112, p. 23; 1911.

Curves (3) for a sample annealed at 350° C. (662° F.) 8 mm (0.315 in.) round bars. P. Ludwik, Zeitschrift des Vereines Deutscher Ingenieure, August 14, p. 657; 1915.

TABLE 3.—Ductility and Hardness of Sheet Aluminum—Experimental Results.

[Aluminum sheet, Grade A (Al min., 99.0). From tests on No. 18 B. & S. gauge, sheet rolled from 6.3 mm, or 0.25 in., slab, Iron Age, vol. 101, p. 950; 1918.]

Heat treatment, annealed.	Thickness.		Erichsen value, depth of cup.	Scleroscope hardness.
	mm	in.		
None (as rolled).....	1.08	0.0425	6.83	14.0
At 200° C. (392° F.), 2 hours.....	1.09	.0429	8.39	10.0
At 300° C. (572° F.), 2 hours.....	1.07	.0422	10.17	4.5
At 400° C. (752° F.), 2 hours.....	1.08	.0425	10.10	4.5
At 200° C. (392° F.), 30 min.....	1.07	.0422	7.97	11.8
At 400° C. (752° F.), 30 min.....	1.08	.0425	9.83	4.5

Copper, iron ⁵ — Cu, 0.89; Fe, 0.52; Si, 0.33; Mn, 0.32; Al, balance.	Wire, for rivets, as received.	21.3	25.2	30,200	35,800	6.0				(133)
	Wire, for rivets, quenched and aged.	12.9	17.3	18,400	24,600	20.0				(133)
Copper, iron, inc. nickel ⁶ ; (major metal). ⁴ Copper, iron, aluminum, magnesium, Al, 95.2; Cu, 4.2; Mg, 0.6.	Cast bars.....		21.1		30,000					(99)
	Cast at 700° C. (1,292° F.).		9.6—	4,500—	13,600—	2—0	0.5—0	74	17—18	(169)
	Annealed, 500° C. (932° F.).		13.3	6,500	18,900					(169)
			17.5	6,500	24,900		1	80	21	(168)
	Cast, sand.....	7.3	9.7	10,400	13,800	5				(168)
	Cast, chill.....	8.7	13.4	12,400	19,100	6				(168)
	Cast sand.....	10.5	12.7	14,900	18,100	5				(168)
	Cast, chill.....	12.3	15.7	17,500	22,400	5				(168)
	Cast, sand.....	2.3	2.3	3,200	3,200	2.5				(168)
	Cast, chill.....	10.1	13.1	14,300	18,600	3.5				(168)
Copper, manga- nese (alloy No. 11)— Al, .96; Cu, 2.89; Mn, 0.94.	Cast, sand.....	9.4	11.7	13,400	16,700	5.0				(168)
	Cast, chill.....	11.4	19.0	16,200	27,000	13.5				(168)
	Hot rolled to 1½ in (38.6 mm),	13.9	24.8	19,700	35,300	20.0	32.8			(168)
	Hot rolled to 1¼ in. (20.6 mm).	20.1	26.0	28,600	37,000	15.0	38.0			(168)
Copper, manga- nese ⁶ — Al, .97; Cu, 1.5; Mn, 1.1 ⁷	Cast sand.....		14.1		20,000	12.0				(169)
	Forged.....		19.5	19,500	27,800	12.0	47.0			(169)

² Used for general castings.
³ For castings for use at high temperatures.
⁴ For pressure castings.
⁵ Shearing strength: Wire as received avg., 13.9 kg/mm² (19,800 lb./in.²); wire quenched and aged, 11.2 kg/mm² (15,900 lb./in.²).
 It was concluded from this investigation that the use of very soft rivets, consisting of nearly pure aluminum, does not appear to be necessary, since perfectly satisfactory joints can be made using cold-drawn and annealed wire of 3/20 alloy (Cu, 3; Zn, 20; Al, 77) or duralumin wire (see those materials), and since last two materials gave much higher shearing strength they are preferable.
⁶ White metal can be cast, rolled in sheets, spun, and welded; can be easily machined. The castings have fine homogeneous structure and are very tough. Heat treatment increases tensile strength of cast bars to 38.7 kg/mm² (55,000 lb./in.²). The metal does not corrode nor tarnish and takes high polish. The only acid which shows an ill effect is hydrochloric acid.
⁷ Bureau of Standards analysis showed: Cu, 2.96; Si, 0.37; Fe, 1.96; Zn, 0.43; Ni, 0.37; Mn, 0.30; Mg, 0.05; Al, balance.
⁸ Specification values, aluminum castings, U. S. Navy, 49 Al, July 1, 1915: Aluminum, min., .94; Cu, max., .6; Mn, max., .3; Fe, max., .05; Si, max., .05. Minimum tensile strength, 12.7 kg/mm² (18,000 lb./in.²), with 8.0 per cent elongation in 2 inches (50.8 mm).
⁹ Naval Gun Factory.

Cu, 3.5-4.5; Mn, 0.4-1.0; Mg, 0.2-0.75; Al and top, balance.	Annealed. Rolled, 70 per cent reduction. Rolled and heat treated. Rolled after heat treatment.	8.4-10.5 21.1-24.6 12.7-15.5 21.1-31.6	19.7-24.6 31.6-36.9 36.9-42.2 42.2-52.7	12,000-15,000 15,000-30,000 35,000-47,000 52,500-60,000 45,000-75,000	28,000-35,000 45,000-47,000 52,500-60,000 60,000-75,000	15-18 2.0-2.5 16-20 1-15	25-30 5-8 20-25 15-20	53-58 85-90 85-100 110-150	18-28 35-40 30-40 35-50	(1) (1) (1) (1)
Copper, nickel, magnesium alloy ⁽¹⁰⁾ is— Cu, 4; Ni, 2; Mg, 1.5; Al, balance.	Cast, chill. 7/8 in. (22.3 mm) diam, rod hot rolled. 7/8 in. (22.3 mm) diam, rod cold rolled from 1 1/4 in. (31.7 mm) in. quenched 530° C. (986° F.) aged. 0.05 in. (1.27 mm) sheet hot rolled quenched 530° C. (986° F.) aged. 0.018 in. (0.46 mm) sheet quenched 530° C. (986° F.) aged.	2.8 18.9 12.1 15.5	18.9 24.0 27.1 33.0	26,900-39,400 34,100 38,500 47,000	26,900-39,400 34,100 38,500 47,000	6.5 20.0 25.0 17.0	30.0 34.0 19.0	(134) (134) (134) (134)		

¹⁰ Most remarkable light alloy of Al. Discovered by Wilm in 1903-1911. Chemical composition Cu, 3.5-5.5; Mn, 0.5-0.8; Mg, 0.5; Al, balance. Can be readily rolled and forged. Quenching from 400-520° C. (752-968° F.) increases hardness very little, but upon aging for several days both hardness and ductility are increased from 15 to 50 per cent. Duralumin is remarkably resistant to corrosion in hardened state. Can be welded, but the joint is weaker than original material. The density of duralumin varies from 2.75 to 2.84. Modulus of elasticity, 7,030 kg/mm² (10,000,000 lb./in.²). (P. Merica Chem. and Met. Eng., Sept. 15, 1918.)

¹¹ Most advantageous heat treatment: Water quenching at 475° C. (887° F.). The following results were obtained by Dr. Sauvieur:

Treatment.	When tested.	Elastic limit.		Tensile strength.		Elongation 4 inches (101.6 mm).		Reduction of area.	
		kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	Per cent.	Per cent.	Per cent.	Per cent.
None. Heated to 475° C. (887° F.) in salt bath and quenched in water.	Immediately.	30.2	43,000	38.4	54,600	17	21	21	21
		18.7	26,600	29.0	41,300	22.2	24	24	24
		21.7	30,800	37.5	53,200	23.4	25	25	25
		23.6	33,600	39.1	55,600	21.6	27	27	27
	After 24 hours	23.6	33,600	39.9	56,700	22.5	27	27	27
	After 48 hours	25.2	35,800	39.1	55,600	23	25	25	25
	After 1 week								
	After 1 month								

¹² Shearing strength, 25.9 kg/mm² (36,800 lb./in.²). Riveted joints showed no tendency to cracking or deterioration in the course of many months. Owing to their higher strength compare favorably with rivets made of softer alloys.

¹³ Tensile strength at 250° C. (482° F.), 17.3 kg/mm² or 24,600 lb./in.²; tensile strength at 350° C. (662° F.), 7.9 kg/mm² or 11,200 lb./in.²; elongation in 2 inches (50.8 mm), at 350° C. (662° F.), 15 per cent. Alloy is, though weaker than other alloys at ordinary temperatures has superior tensile strength at elevated temperatures as well as higher resistance to alternating stress. It is immune from "season cracking" and possesses remarkable resistance to corrosion.

Silicon (silu- min) ³⁰	{ 2.5- 2.65 }	20.0	28,400	5-10	60			(211)
Silver (argen- ta) ³¹								(112)
Tungsten (par- thium) ³²								(44)
Zinc.....								(168)
Al, Zn; various proportions (see fig. 10.) ³³								(98)
Zinc (alzene) ³⁴	3.8	16.9	24,000	0				(105)
Zinc, copper ³⁴	2.88	17.4	24,700	6.2				(105)
Al, 89; Zn, 10; Cu, 1.....	2.91	17.8	25,380	4.0				(105)
Al, 88; Zn, 10; Cu, 2.....	2.85	14.7	20,860	5.7				(105)
Al, 92; Zn, 5; Cu, 3.....								(169)
Al, 88.6; Zn, 8.4; Cu, 3, Annealed 500° C. (932° F.).....	4.7	18.5	6,700	8.0	7.5	50	10	(169)
Al, 81.1; Zn, 15.9; Cu, 3, Cast at 700° C. (1,292° F.).....	4.4	20.2	6,200	8.0	7.5	50	10	(169)
Al, 81.1; Zn, 15.9; Cu, 3, Annealed 500° C. (932° F.).....	3.09	24.7	14,000	2.0	2.0	74	15	(169)
Al, 81.0; Zn, 12.5-14.5; Cu, 2.25-3.25; Si, Fe, Mn, Sn, max. 1.7; other imp., none.....	3.0	29.0	14,000	4.0	4.0	70	15	(169)
Zinc, copper (al, Cu) ³⁵		17.6- 21.1	25,000- 30,000	More than 1.0				(145)
Zn, 12.5-14.5; Cu, 2.5-3; Al, balance.....	3.0	27 17.3	27 24,600	27 4				(134)

³⁰ Has advantage over other aluminum alloys at high temperature. Brinell hardness 60 at 500 kg (1,102 lb.) load, 10 mm ball at room temperature and 20-25 at 350° C. (662° F.). Wet steam does not appreciably attack aluminum. Somewhat less resistant than pure aluminum to attack by dilute nitric acid (25 per cent) or other strong acids. Conducts heat better than other known alloys of aluminum.

³¹ Alloy of aluminum and silver. Fine white color; good casting properties; rolls and machines well, and takes good polish.

³² Alloy of aluminum and tungsten. Used in France in automobile construction because of its lightness and strength.

³³ Good for casting; resists corrosion well; takes good polish, used in automobile industry.

³⁴ Alloys containing 5 per cent and over of zinc are subject to an "aging" phenomenon which results in an increase in tensile strength and a decrease in elongation. Alloys of 5 per cent or more of zinc are not adapted for parts subjected to high temperature.

³⁵ Tested without machining off the skin. Tensile strength of "L 5" increases considerably on aging. Tensile strength of chill bar 1 inch (25.4 mm) diameter increases 30 per cent in 10 months. Tensile strength falls off rapidly as the temperature increases. Tensile strength at normal temperature=22.0 kg/mm² (31,200 lb./in.²). Tensile strength at 250° C. (482° F.)=6.3 kg/mm² (9,000 lb./in.²). Tensile strength at 350° C. (662° F.)=2.4 kg/mm² (3,400 lb./in.²).

³⁶ Specification values.

0.10 in. (2.54 mm) sheet hot-rolled, 100 ft. or 16 ft. long, 200° C. (392° F.),	19.3	35.0	27,550	49,700	24-28				(134)
0.063 in. (1.6 mm) diam. wire as received.		43.8	62,200		31.8				(134)
0.063 in. (1.6 mm) diam. wire annealed at 250° C. (482° F.).		32.6	46,300		31.14				(134)
Antimony: #1								630 (1,166° F.)	84 11.5 (98)
Antimony: #2 Sb, 99.45; As, Fe.		1.08	1,540					84 271 (520° F.)	84 13.46 (130)
Bismuth: #6 Bi.....	9.8							2,000-2,500 (3,632-4,532° F.)	(2)
Boron: #7 B.....								321 (610° F.)	84 30.7 (138)
Cadmium: #8 Cd.....	818.64								

²⁸ Corroded strongly even by a weak saline solution and ultimately undergoes a complete disintegration.
²⁹ Shearing strength, 26.8 kg/mm² (38,100 lb./in.²). Riveted joints showed no tendency to cracking or deterioration in the course of many months. Owing to their higher strength they compare favorably with rivets made of softer alloys.
³⁰ Shearing strength, 35.4 kg./mm.² (50,400 lb./in.²). Notched bar tests at 86 and 185° below 0° F. (112 and 301° below 0° F.) showed no embrittling action of the intense cold.
³¹ In 4 in. (101.6 mm).
³² Silver white crystalline brittle metal. Used in bearing metals and as type metal (expands on solidification).
³³ Vacuo distilled, 6.62; ditto-compressed, 6.69; amorphous, 6.22 (Smithsonian Physical Tables, 1920).
³⁴ Smithsonian Physical Tables, 7th edition, 1920.
³⁵ Modulus of elasticity, 7,950 kg/mm² (11,300,000 lb./in.²); modulus of elasticity in shear, 2,020 kg/mm² (2,870,000 lb./in.²). These results were obtained from bending tests and due to the anisotropic nature of wire can be used for calculation of bending stresses only.
³⁶ Has lustrous appearance like antimony; is very brittle; not altered in cold air, but on heating forms oxide; forms easily fusible alloys suitable for reproduction of woodcuts, for fusible valves and wires.

Melting Points of Some Bismuth Alloys.

Name of alloy.	Chemical composition, parts—				Melting point.	
	Bi	Pb	Sn	Cd	°C.	°F.
Wood's metal.....	5	8	4	3	68	154
Rose's metal.....	9	8	3	3	79	174
Newport's alloy.....	18	3	94.5	202
Lipowitz's alloy.....	13	8	8	3	70	158

Landolt Börnstein tables (1912) give for the modulus of elasticity of cast Bi 3,200 kg/mm² (4,550,000 lb./in.²) and for the modulus of elasticity in shear 1,200 to 1,400 kg/mm² (1,710,000 to 1,990,000 lb./in.²). Poisson's ratio of Bismuth 0.33. Poisson's ratio of Wood's metal, 0.49. Winkelman's Handbuch der Physik, 1908, I (1), gives for modulus of elasticity in shear of Wood's metal, 846 kg/mm² (1,190,000 lb./in.²). Poisson's ratio of Rose's metal, 0.47 and that of Lipowitz's alloy, 0.45.
³⁷ Hardness of fused boron inferior only to diamond. Most interesting property; enormous (2,000,000 times) increase of electrical conductivity at red heat.
³⁸ 1 per cent of Cd in brasses with 66-70 per cent copper has no appreciable effect. Cd content more than 1 per cent has a detrimental effect, especially on resilience. Landolt Börnstein tables (1912) give for modulus of elasticity 5,000 to 7,000 kg/mm² (7,100,000 to 9,900,000 lb./in.²) and the modulus of elasticity in shear 1,000 to 2,500 kg/mm² (1,420,000 to 3,500,000 lb./in.²). Poisson's ratio, 0.36. According to Winkelman's Handbuch der Physik, 1908, I (1), modulus of elasticity of cast Cd, 7,070 kg/mm² (10,050,000 lb./in.²) and modulus of elasticity in shear, 2,450 kg/mm² (3,480,000 lb./in.²).
³⁹ Landolt Börnstein tables, 1912.

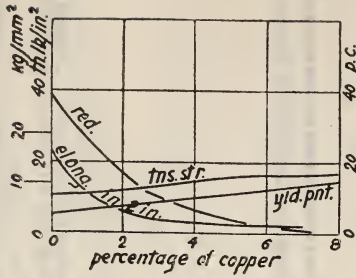


FIG. 3.—Tensile properties of aluminum-copper sand-cast alloys.

H. C. Carpenter and C. A. Edwards, 8th report to the alloys research committee of the Inst. Mech. Eng.; 1907.

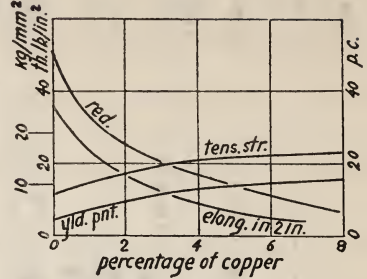


FIG. 4.—The tensile properties of aluminum-copper chill-cast alloys.

H. C. Carpenter and C. A. Edwards, 8th report to the alloys research committee of the Inst. Mech. Eng.; 1907.

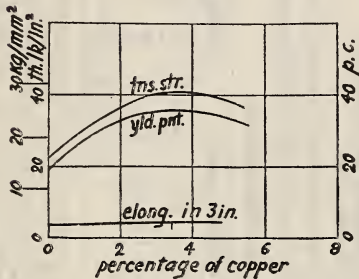


FIG. 5.—The tensile properties of aluminum-copper alloys in the form of sheet 0.05 in. (1.27 mm) thick.

The ingots were cast $\frac{5}{8}$ in. (15.9 mm) thick, hot rolled to $\frac{3}{8}$ in. (9.52 mm), cold rolled to $\frac{1}{4}$ in. (6.35 mm), annealed, cold rolled to 0.1 in. (2.54 mm), annealed, cold rolled to 0.05 in. (1.27 mm). H. C. Carpenter and C. A. Edwards, 8th report to the alloys research committee of the Inst. Mech. Eng.; 1907.

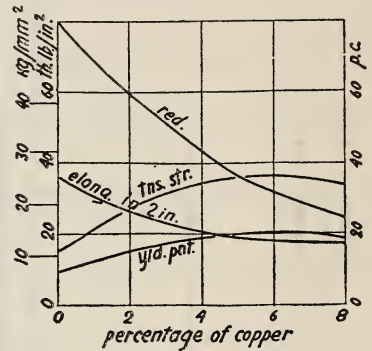


FIG. 6.—The tensile properties of aluminum-copper alloys $1\frac{1}{4}$ in. (31.7 mm) diameter bars hot rolled from 3 in. (76.2 mm) ingots.

H. C. Carpenter and C. A. Edwards, 8th report to the alloys research committee of the Inst. Mech. Eng.; 1907.

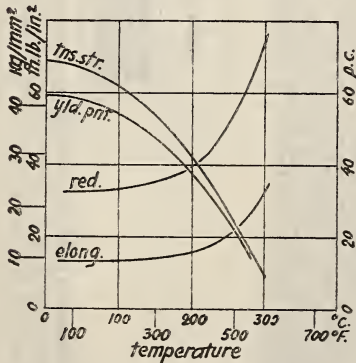


FIG. 7.—Variation of the tensile properties of duralumin with temperature.

L. M. Cohn, Elektrotechnik und Maschinenbau, 30, pp. 809, 829; 1912; and Duralumin, Ver. z. Ford. d. Gewerbebeisess, 89, p. 643; 1910.

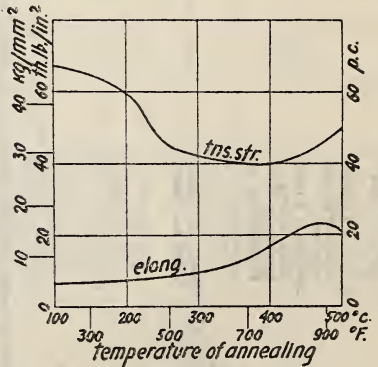


FIG. 8.—Effect of annealing on the tensile properties of duralumin.

L. M. Cohn, Duralumin, Elektrotechnik und Maschinenbau, 30, pp. 809, 829; 1912; and Duralumin, Ver. z. Ford. d. Gewerbebeisess, 89, p. 643; 1910.

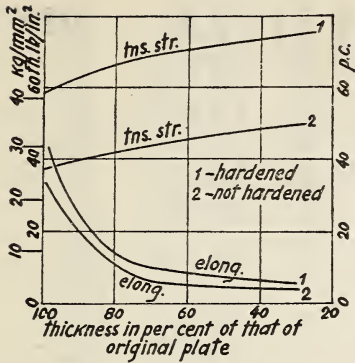


FIG. 9.—Effect of cold working on the tensile properties of duralumin.

Samples cold rolled from a thickness of 7 mm (0.276 in.). L. M. Cohn, Duralumin, *Elektrotechnik und Maschinenbau*, 80, pp. 800, 829; 1912; and Duralumin, *Ver. z. Ford. d. Gewerbetreibenden*, 89, p. 643; 1910.

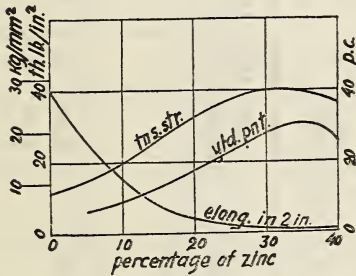


FIG. 11.—The tensile properties of aluminum-zinc chill-cast alloys.

W. Rosenhain and L. Archbutt, 10th report to the alloys research committee, *Inst. Mech. Eng.*; 1912.

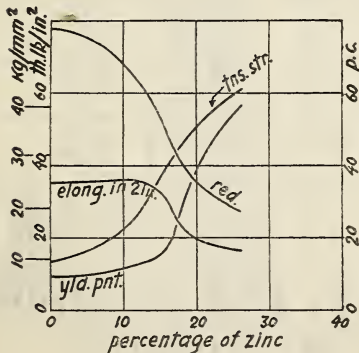


FIG. 12.—The tensile properties of aluminum-zinc alloys; $1\frac{1}{4}$ in. (31.7 mm), diameter bars hot rolled from 3 in. (76.2 mm) ingots.

W. Rosenhain and L. Archbutt, 10th report to the alloys research committee, *Inst. Mech. Eng.*; 1912.

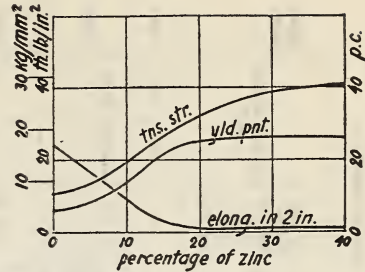


FIG. 10.—The tensile properties of aluminum-zinc sand-cast alloys.

W. Rosenhain and L. Archbutt, 10th report to the alloys research committee, *Inst. Mech. Eng.*; 1912.

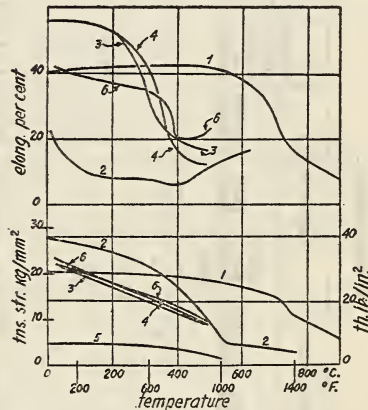


FIG. 13.—Effect of high temperatures on the tensile properties of copper.

1. Annealed electrolytic copper; rate of loading $1,120 \text{ lb./in.}^2$ (0.79 kg/mm^2) per minute, tested in air. (G. D. Bengough and D. Hanson, *Jour. Inst. Met.*, 12, p. 56; 1914.)
2. Rolled arsenical copper; rate of loading $1,120 \text{ lb./in.}^2$ (0.79 kg/mm^2) per minute, tested in CO_2 . (G. D. Bengough and D. Hanson, *Jour. Inst. Met.*, 12, p. 56; 1914.)
3. Annealed electrolytic copper, tested in air. (A. K. Huntington, *Jour. Inst. Met.*, 8, p. 126; 1912.)
4. Arsenical copper, tested in air. (A. K. Huntington, *Jour. Inst. Met.*, 12, p. 234; 1914.)
5. Yield point for electrolytic copper. (B. S. Circular No. 73, p. 41; 1918.)
6. "Pure" copper, Le Chatelier, *Congrès des Méthodés d'Essais*, Paris; 1912.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.								Hardness number.		Thermal properties.			Reference.	
			Metric kg./mm. ²				English lb./in. ²				Brinell.	Sclero-scope.	Melting point.	Linear coefficient of expansion ×10 ⁶ (per 1° C.).	Casting shrinkage.		
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.	Yield point.	Tensile strength.	Elongation in 50.8mm or 2 inches.	Reduction of area.							
1	2	8	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Cerium: Ce.....		7.02											°C. (1,184° F.)		mm/m	in./ft.	(138)
Chromium: Cr.....		7.19-7.73											°C. (2,933° F.)				(138)
Cobalt, (pure): ⁴⁰ Co.....	Cast.....	8.79		(4)	24.2		(4)	34,400	Less than 1.0	Per ct.			1,478 (2,692° F.)	43 12.36			(91)
	Annealed.....	8.81		(4)	26.0		(4)	36,980	Less than 1.0	Per ct.							(91)
(Commercial) (Imp. Fe, Si, C) ⁴¹	Wire.....	8.93			63.3			About 90,000	4.7	Per ct.							(91)
Co, 97-99; C, 0.062. C, 0.25.....	Cast.....				42.0			59,700	About 8.0	About 7.0							(91)
	do.....				43.5			61,900	About 25.0	About 29.0							(91)
Chromium (steel), ⁴² C, 22.5; Mn, 10.8; P, 3.15; S, 0.015; Zn; C, 0.9; Si, 0.8 Copper: ⁴³ Electrolytic— Cu, 99.9.....	do.....		59.8		77.3	85,000		110,000				512					(5)
	Wire.....				26.7	8,500		38,000	50	50		40					(113)
	Annealed at 500° C. (932° F.) Not annealed (96 per cent reduction). ⁴⁷				47.4			67,400	0.8	64.5							(109, 170, 109, 170)

Annealed at 750° C. (1,382° F.) after drawing cold, ⁴⁷	21.9	31,200	24.5	76.0	(109, 170)
Drawn hot (64 per cent reduction). ⁴⁸	32.9	46,800	4.3	70.5	(109, 170)

⁴¹ See foot note 34, p. 20.
⁴² Compressive strength. Cast 82.3 kg/mm² (12,150 lb./in.²); annealed, 82.3 kg/mm² (117,200 lb./in.²). Compressive yield point: Cast 29.6 kg/mm² (42,200 lb./in.²); annealed 39.5 kg/mm² (56,100 lb./in.²). Cobalt is readily machined but brittle. Special treatment is necessary to render pure cast cobalt amenable to working.

⁴³ Under load of 1,500 kg (3,500 lb.).
⁴⁴ Smithsonian Physical Tables, 7th edition, 1920.
⁴⁵ Compressive strength—C about 0.18; Cast, 125.1 kg/mm² (178,000 lb./in.²); annealed 104.1 kg/mm² (148,000 lb./in.²). Compressive yield point—C, about 0.18; Cast, 36.6 kg/mm² (52,100 lb./in.²); annealed, 42.9 kg/mm² (61,000 lb./in.²). Commercial Co containing C may be readily swaged down from cast bars to wire. Addition of C gives toughness. ⁴⁶ Produced in 1890. Considerable hardness and toughness. Most important property, ability to maintain a cutting edge at a high speed, even at a full, red heat. Can not be forged and can only be reduced to the desired form by casting in the form of bars, which are afterwards ground.
⁴⁷ Tests made under working conditions on stranded cables of hard-drawn wire gage. Modulus of elasticity of 7-strand cable 14,200 kg/mm² (20,000,000 lb./in.²); modulus of elasticity of 10-strand cable 12,300 kg/mm² (17,500,000 lb./in.²); modulus of elasticity of 37-strand cable 10,900 kg/mm² (15,500,000 lb./in.²); 14,950 kg/mm² (20,000,000 lb./in.²) was suggested as suitable working value for solid wire.

Properties of Bare Copper Cables.

[Results of Tests Made at the Massachusetts Institute of Technology in 1912; Pender, Handbook for Electrical Engineers, 1914, p. 1880. The cables were given Preliminary Stretch Before Readings were Taken.]

Cables designation.	Number of wires in cables.	Pitch of layers.				Elastic limit.		Tensile strength.		Modulus of elasticity.	
		First layer.		Second layer.		kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²
		mm	in.	mm	in.						
A.....	7	114.3	4.5	15.5	22,900	37.6	53,300	11,680	16,600,000
B.....	19	177.8	7	127.0	5	15.0	21,300	42.0	59,800	11,470	16,300,000
C.....	19	228.6	9	114.3	4.5	16.0	23,000	39.4	55,000	11,600	16,500,000
D.....	19	228.6	9	228.6	9	17.8	25,000	37.9	52,800	11,570	16,500,000
E.....	19	114.3	4.5	76.2	3	17.8	25,300	37.9	53,800	9,570	13,600,000

Properties of Component Wires of Above Cables.

Wires from cables.	Diameter of wires.		Elastic limit.		Tensile strength.		Modulus of elasticity.	
	mm	in.	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²
A.....	3.17	0.125	19.0	27,000	44.2	62,800	16,900,000	16,900,000
B.....	3.17	.125	19.0	27,000	43.5	61,900	13,300,000	18,900,000
C.....	3.17	.125	18.3	26,000	43.4	61,800	11,680,000	16,600,000
D.....	3.17	.125	18.3	26,000	41.7	59,300	12,320,000	17,500,000

⁴⁷ Wire drawn cold from 0.125 to 0.025 inch (3.18 to 0.64 mm).

⁴⁸ Wire drawn at 150° C. (303° F.) from 0.031 to 0.025 inch (0.79 to 0.64 mm).

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.				Thermal properties.			Reference.	
			Metric kg./mm. ²			English lb./in. ²			Reduction in elongation of 50.8 mm or 2 inches.	Brinell.	Sclero-scope.	Melting point.	Linear coefficient of expansion ×10 ⁶ (per 1° C.)	Casting shrinkage.			
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.	Yield point.	Tensile strength.							Per cent.		Per cent.
1	2	8	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Copper (pure) ⁴⁹ .																	
Pure—																	
Cu, min. 99.5.	Soft, sheet 0.005–0.031 in. (0.13–0.79 mm).				26.0				max. 37,000	min. 20.0							(146)
	Soft, sheet 0.032–0.375 in. (0.81–9.51 mm).				25.3				max. 36,000	min. 25.0							(146)
	Hard, sheet 0.072–0.375 in. (1.83–9.51 mm).				28.1				min. 40,000	min. 8.0							(146)
	Hard, sheet, over 0.375 in. (9.51 mm).				26.4				min. 37,500	min. 15.0							(146)
Cu, 99.9 ⁵⁰ .	Normalized ⁵¹ .	8.89			21.1–28.1				30,000–40,000	40–60							(170)
Commercial—									17,600–25,000	60							(168, 170)
Cu, 99.6.	Cast.	8.89	7.0	14.1	35.2	20,000			50,000	8							(170)
	Normalized ⁵¹ .																
	Rolled, hard (40 per cent reduction).	8.89			24.6				35,000	50							(170)
	Annealed at 500° C. (932° F.).	8.90			35.2	37,000			50,000	9							(170)
	Drawn, cold (50 per cent reduction).		26.0														(170)

⁴⁹ According to Winkelman's Handbuch der Physik, 1908, 1, 1.—: Modulus of elasticity of cast copper, 10,800 kg/mm² (15,350,000 lb./in.²); modulus of elasticity of annealed copper, 10,520 kg/mm² (14,950,000 lb./in.²); modulus of elasticity of drawn copper, 12,140 kg/mm² (17,250,000 lb./in.²); modulus of elasticity in shear of cast copper, 4,780 kg/mm² (6,790,000 lb./in.²); modulus of elasticity of copper (electrolytic), 12,200 kg/mm² (17,350,000 lb./in.²); modulus of elasticity of drawn copper, 4,200 kg/mm² (5,950,000 lb./in.²).
⁵⁰ Modulus of elasticity of copper (electrolytic), 12,200 kg/mm² (17,350,000 lb./in.²); modulus of elasticity of cast copper, 7,700 kg/mm² (11,000,000 lb./in.²). According to American Steel & Wire Co. (1923) modulus of elasticity of hard-drawn copper is 18,000,000 lb./in.²; modulus of elasticity of cast copper, 7,700 kg/mm² (11,000,000 lb./in.²); modulus of elasticity of drawn copper, 12,400 kg/mm² (17,600,000 lb./in.²); modulus of elasticity of annealed copper, 12,900 kg/mm² (18,000,000 lb./in.²); modulus of elasticity of cast copper, 7,700 kg/mm² (11,000,000 lb./in.²).
 Modulus of elasticity in shear of cast copper, 4,240 kg/mm² (6,030,000 lb./in.²); Poisson's ratio, 0.33. Shear strength—tensile strength and varies in annealed or cast condition from 15.5 to 25.3 kg/mm² (22,000 to 36,000 lb./in.²). Compression—copper of good quality does not fail in compression test by fracture, it merely yields indefinitely. Cast-copper annealed cylinders 0.625-inch (15.8 mm) diameter and 2 inches (50.8 mm) long: shortened 5 per cent at 22.0 kg/mm² (31,300 lb./in.²); shortened 10 per cent at 28.9 kg/mm² (41,200 lb./in.²); shortened 20 per cent at 39.0 kg/mm² (55,400 lb./in.²).
⁵¹ Pure copper may best be normalized by casting, rolling, and drawing, followed by annealing at 500° C. (932° F.).
⁵² Not determinable.
⁵³ Bhn. of annealed or cast copper is 30–40 (500 kg (1,102 lb.) 10 mm ball). When hardened by cold work, Bhn. may become as high as 100.
⁵⁴ Coefficient of expansion (16.47+0.0045)10⁻⁶ where t=degrees Centigrade.

TABLE 4.—Tensile Requirements of Soft or Annealed Copper Wire.

[A. S. T. M. specification B 3-15.]

Diameter.		Tensile strength.		Elongation (minimum) in 254 mm (10 in.).
mm	in.	kg/mm ²	lb./in. ²	
11.70-7.37	0.460-0.290	25.3	36,000	35
7.34-2.62	.289-.103	26.0	37,000	30
2.59-.53	.102-.021	27.1	38,500	25
.51-.08	.020-.003	28.2	40,000	20

TABLE 5.—Tensile Requirements of Medium Hard-Drawn Copper Wire.

[A. S. T. M. specification B 2-15.]

Diameter.		A. W. G. (No.).	Tensile strength.				Elongation (minimum).
mm	in.		Minimum.		Maximum.		
		kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	Per cent in 254 mm (10 in.).	
11.68	0.460	0000	29.5	42,000	34.4	49,000	3.75
10.40	.410	000	30.2	43,000	35.1	50,000	3.6
9.27	.365	00	30.9	44,000	35.8	51,000	3.25
8.25	.325	0	31.6	45,000	36.5	52,000	3.0
7.35	.289	1	32.3	46,000	37.2	53,000	2.75
6.54	.258	2	33.0	47,000	37.9	54,000	2.5
5.83	.229	3	33.7	48,000	38.7	55,000	2.25
							Per cent in 1,524 mm (60 in.).
5.19	.204	4	34.0	48,330	38.9	55,330	1.25
4.62	.182	5	34.2	48,660	39.1	55,660	1.20
4.12	.162	6	34.4	49,000	39.4	56,000	1.15
3.66	.144	7	34.7	49,330	39.6	56,330	1.11
3.26	.128	8	34.9	49,660	39.8	56,660	1.08
2.91	.114	9	35.1	50,000	40.1	57,000	1.06
2.59	.102	10	35.4	50,330	40.3	57,330	1.04
2.31	.091	11	35.6	50,660	40.5	57,660	1.02
2.05	.081	12	35.8	51,000	40.8	58,000	1.00
1.83	.072	13	36.0	51,330	41.0	58,330	.98
1.63	.064	14	36.3	51,660	41.2	58,660	.96
1.45	.057	15	36.5	52,000	41.5	59,000	.94
1.29	.051	16	36.8	52,330	41.7	59,330	.92
1.15	.045	17	37.0	52,660	41.9	59,660	.90
1.02	.040	18	37.2	53,000	42.2	60,000	.88

Proportional limit of medium hard-drawn copper wire averages 50 per cent of tensile strength required in these specifications.

TABLE 6.—Tensile Requirements of Hard-Drawn and Hard-Rolled Copper Wire—Specification Values.

[Specific gravity, 8.89 at 20° C. (68° F.). For copper wire and for hard-drawn and hard-rolled flat copper of thicknesses corresponding to diameters of wire. (A. S. T. M., B 1-15.)]

Diameter.		A. W. G. No.	Minimum tensile strength.		Minimum elongation.
mm	in.		kg/mm ²	lb./in. ²	
11.68	0.460	0000	34.5	49,000	Per cent in 254 mm (10 in.).
10.40	.410	0000	35.9	51,000	3.75
9.27	.365	00	37.1	52,800	3.25
8.25	.325	0	38.3	54,500	2.80
					2.40
7.35	.289	1	39.4	56,100	2.17
6.54	.258	2	40.5	57,600	1.98
5.83	.229	3	41.5	59,000	1.79
					Per cent in 1,524 mm (60 in.).
5.19	.204	4	42.2	60,100	1.24
4.62	.182	5	43.0	61,200	1.18
4.12	.162	6	43.7	62,100	1.14
3.66	.144	7	44.3	63,000	1.09
3.26	.128	8	44.8	63,700	1.06
2.91	.114	9	45.2	64,300	1.02
2.59	.102	10	45.9	64,900	1.00
2.31	.091	11	46.0	65,400	.97
2.05	.081	12	46.2	65,700	.95
1.83	.072	13	46.3	65,900	.92
1.63	.064	14	46.5	66,200	.90
1.45	.057	15	46.7	66,400	.89
1.29	.051	16	46.8	66,600	.87
1.15	.045	17	47.0	66,800	.86
1.02	.040	18	47.1	67,000	.85

Proportional limit of hard-drawn copper wire averages 55 per cent of tensile strength required in these specifications for four largest-sized wires in table, and 60 per cent of tensile strength for smaller sizes.

TABLE 7.—Tensile Requirements of Copper Plates.

[A. S. T. M. specification B 11-18.]

Analysis.	Tensile strength.		Elongation in 203.2 mm (8 in.).
	kg/mm ²	lb./in. ²	Per cent.
Copper, arsenical, As, 0.25-0.50; impurities, max, 0.12.....	21.8	31,000	35
Copper, nonarsenical, impurities, max., 0.12.....	21.1	30,000	30

TABLE 8.—Tensile Requirements of Rolled Copper—Specification Values.

[U. S. Navy Department, 47C2b, minimums for rolled copper, Cu, min. 99.5.]

Description.	Temper.	Thickness.	Tensile strength.		Elongation in 50.8 mm (2 in.).
			kg/mm ²	lb./in. ²	Per cent.
Rods, bars, and shapes ¹	Soft.....		21.1	30,000	25
	Hard.....	To 9.5 mm (3/8 in.), inclusive.....	35.2	50,000	10
do.....	9.5 to 25.4 mm (1 in.).....	31.6	45,000	12
do.....	25.4 to 50.8 mm (2 in.).....	28.1	40,000	15
do.....	Over 50.8 mm (2 in.).....	24.6	35,000	20
Sheets and plates.....	Soft.....		21.1-28.1	30,000-40,000	25
	Hard.....		24.6	35,000	18

¹ Hammer test: Bars shall stand hammering hot to a fine point. Bending test: Bars shall stand bending cold through 130° to radius equal to diameter or thickness of test bar.

IX. NOMENCLATURE OF COPPER ALLOYS.

The general system of nomenclature employed has been to denominate (a) all simple copper-zinc alloys as *brasses*; (b) all simple copper-tin alloys as *bronzes*; and (c) three or more metal alloys composed primarily of either of these two combinations as *alloy brasses* or *bronzes*, as, for example, "Zinc bronze" for U. S. Government composition "G," Cu, 88 per cent; Sn, 10 per cent; Zn, 2 per cent. Alloys of the third type noted above, together with other alloys composed mainly of copper, have been called *copper alloys*, with the alloying elements other than minor impurities listed as modifying copper in the order of their relative percentages. In some instances the scientific name used to denote an alloy is based upon the deoxidizer used in its preparation, which may appear either as a minor element of its composition or not at all, as, for example, phosphor bronze. Commercial names are shown below the scientific names. In some cases a commercial name is used for alloys of widely varying composition.

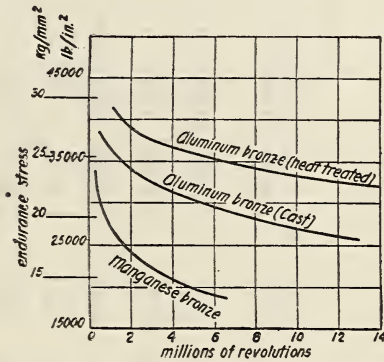


FIG. 14.—Fatigue properties of aluminum and manganese bronzes.

W. M. Corse and G. F. Comstock, Proc. A. S. T. M., 162, p. 117; 1916.

The tests were made in White-Souther machine. For chemical composition and other physical properties of tested metals see Table 21.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Elongation in 50.8 mm or 2 inches.	Reduction of area.	Hardness number.			Thermal properties.			Reference.		
			Metric kg/mm ²		English lb./in. ²		Proportional limit.	Yield point.			Tensile strength.	Brinell.	Scleroscope.	Melting point.	Linear coefficient of expansion $\times 10^6$ (per 1° C.).	Casting shrinkage.			
			Yield point.	Tensile strength.	Proportional limit.	Yield point.												Tensile strength.	
Copper: Aluminum (aluminum bronze) Cu, 92.5; Al, 7.2. Cu, 90.1; Al, 9.9.	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18		
			6.7	37.6	50.0	9,600	25,300	33,500	9.0	72.9	81	19	°C.	mm/m	in./ft.				
			17.8	50.0	25,300	29,800	71,000	21.7											(109)
			21.0	50.0	29,800		71,000												(164)
			35.3	78.7	50,200		112,000	3.0											(40)
			19.5	58.2	27,800		82,700	30.5											(40)
			26.0	41.6	37,000		59,100	5.0											(40)
			27.8	60.8	39,600		86,400	22.0											(40)
			21.5	55.2	30,500		78,500	31.5				30.5							(40)
			23.3	60.0	33,200		85,300	28.8				30.8							(40)
			24.8	45.0	35,200		63,900	6.5				10.2							(40)
			41.3	71.7	58,700		101,900	11.0				16.8							(40)
			63.7	69.2	90,500		98,400	13.4				22.2							(40)
16.9	49.3	24,000		70,100	20.5				20							(114)			
13.9	51.1	19,800		72,700	25.3				20							(169)			
23.3	60.0	35,200		83,500	21.7				22.4							(169)			
Cu, 90; Al, 10. ³ Cu, 90; Al, 10. ³	Casting sand.	7.5 7.5	13.9 23.3	16.9 60.0	49.3 35,200	24,000 90,500	58,700 98,400	101,900 98,400	11.0 13.4	16.8 22.2	20 20	90-100 102-106	18.3	0.22					

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific grav-ity.	Tensile properties.						Hardness num-ber.			Thermal properties.				Refer-ence.	
			Metric kg./mm ²			English lb./in. ²			Elonga-tion in 50.8 mm or 2 inches.	Reduc-tion of area.	Brinell.	Melting point.	Linear coeffi-cient of expan-sion $\times 10^6$ (per 1°C.)	Casting shrink-age.			
			Pro-portion- al limit.	Yield point.	Tensile strength.	Pro-portion- al limit.	Yield point.	Tensile strength.									
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Copper—Contd. Aluminum, iron bronze)— Cu, 88.5; Al, 10.5; Fe, 1.0.			14.1 28.1		54.1 64.7	20,000 40,000		77,000 92,000	24.5 14.0	25.0 18.5	100 140						(169) (169)
Cu, 89; Al, 10; Fe, 1.9 Cu, 89; Al, 10; Fe, 1.11 Cu, 87.0; Al, 9.8; Fe, 3.14; ¹² Cu, 85.6; Al, 10.81; Fe, 3.57. Aluminum, iron (Silliman bronze)— Cu, 86.4; Al, 9.7; Fe, 3.9. Aluminum, tin, iron (alu- min bronze) ¹³ . Cu, 90.4; Al, 8.9; Sn, 0.4; Fe, 0.2; Cu, 90.4; Al, 8.8; Sn, 0.1; Fe, 0.4; Pb, 0.2; ¹⁴ Aluminum, tin— Cu, 88.5; Al, 10.4; Sn, 1.2.	Cast, sand, Quenched, 850° C. (1,562° F.); drawn, 700° C. (1,292° F.)	7.5 7.5 7.71 7.58	16.2- 19.7 16.9	45.7- 56.3 54.2	23,000- 28,000 24,000	65,000- 80,000 77,000	20-30 24	21-29 25	10.92- 100 95-105			°C.		18.3 18.3	0.22 .22	(45) (114) (46) (46)	
	Wrought. Cast.		9.84 8.1	59.3 55.4	14,000 11,500		84,400 78,850	11.5 14.5	29.2								(175) (175)
			8.9	43.5	12,700		61,900	27.0	29.2								(177)
			10.2	39.0	14,500		55,500	27.5	34.7								(177)
	Cast, chill.		25.8	47.8	36,700		68,000	4.4	5.6	189	32						(83)

Cu, 94.98; Ni, 0; Al, 5.02; Ni, 0.94; Al, 5.10; Cu, 92.68; Ni, 2.38; Al, 4.94; Cu, 89.84; Ni, 4.84; Al, 5.32; Cu, 87.48; Ni, 7.31; Al, 5.21. Nickel(Benedict nickel) ^{19a} —Cu, 84-86; Ni, remainder.	8.2	34.9	49,600	82.5	78.9	(115)
Nickel, aluminum ^{19b} —Cu, 82.1; Ni, 14.6; Al, 2.5; Zn, 0.7.	8.3	35.9	51,000	94.6	76.1	(115)
	8.7	36.2	51,400	90.2	71.0	(115)
	14.8	40.2	57,200	70.0	60.2	(115)
	37.8	61.4	87,400	25.6	26.8	(115)
Forged.....	48.0	90.0	68,400	10.0	12.0	(190)
			128,000			(84)

¹⁸ Modulus of elasticity, 10,720 kg/mm² (15,250,000 lb./in.²)
¹⁹ Compressive proportional limit, 1.0 kg/mm² (2,750 lb./in.²); compressive strength, 19.7 kg/mm² (8,000 lb./in.²); compression, per cent of original length, .25.
²⁰ Compressive proportional limit, 5.1 kg/mm² (1,200 lb./in.²); compressive strength, 32.8 kg/mm² (40,700 lb./in.²); modulus of elasticity, 5,620 kg/mm² (8,000,000 lb./in.²); in compression, 4,560 kg/mm² (6,200,000 lb./in.²).
²¹ Valuable property—an extremely low temperature coefficient of electrical resistance.
²² Chemical composition according to various authors.

	Cu	Mn	Ni	Fe
Fuessner and Linden.	84	12	4
Liddell.	82.12	15.02	2.29	0.57
Analysis of manganin bar made from old German stock.	82.62	12.82	3.78	.72

²³ Landolt Börnstein Physical Tables (1912) give for modulus of elasticity, 12,600 kg/mm² (17,900,000 lb./in.²); modulus of elasticity in shear, 4,700 kg/mm² (6,680,000 lb./in.²) and Poisson's ratio 0.33.
²⁴ Landolt Börnstein Physical Tables (1912) give for modulus of elasticity 16,600 kg/mm² (23,600,000 lb./in.²); modulus of elasticity in shear, 6,200 kg/mm² (8,820,000 lb./in.²) and Poisson's ratio 0.33.
²⁵ Nickel alloys are often used for the construction of turbine blading (resistance to heat and steam action). The following compositions are in commercial use in Great Britain:

Components.	Alloy A.	Alloy B.	Alloy C.
Cu.....	82.07	79.63	79.0
Al.....	2.54	9.77	11.5
Ni.....	14.64	4.13	5.0
Mn.....	Nil.	.94	Nil.
Zn.....	Nil.	.68	Nil.
Fe.....	Trace.	4.80	4.5
Si.....	.04	.14

²⁶ Suitable for tubes for condenser distillers and feed-water heaters.
²⁷ Modulus of elasticity, 14,900 kg/mm² (21,150,000 lb./in.²).

max. 0.5; Al, none; other imp., max. 0.1/2	8.4	17.6	12,000	25,000	Min. 8				(150)
Tin, 16.4-86.0; Cu, 83.0-86.0; Sn, 4.5-6.0; Pb, 8.0-10.0; Zn, max. 2.0; imp., max. 0.25.									
Tin, lead (bronze bearing metal) ²⁸ ;									
al) ²⁸ ;									
Cu, 85; Sn, 10; Pb, 5.	19.7			28,000	12.5		88 60		20.8 .25 (14)
Cu, 80; Sn, 10; Pb, 10.	17.6			25,000	8.0		88 55		20.8 .25 (14)
Cu, 77; Sn, 8; Pb, 15.	14.1			20,000	10.0		88 48		20.8 .25 (14)
Cu, 73; Sn, 7; Pb, 20.	12.7			18,000	7.0		88 45		20.8 .25 (14)
Cu, 70; Sn, 5; Pb, 25.	10.5			15,000	5.0		88 40		20.8 .25 (14)
Tin, lead, phosphorus—									
Cu, 80; Sn, 10; Pb, 10; P, tr.	9.1	11.3	16,000	30,000	6.0	3.5	65	12	(169)
Cast	21.1								

²⁸ Compressive strengths: Cu, 97; Sn, 2.3, 23.9 kg/mm² (34,000 lb./in.²); Cu, 60; Sn, 10, 39.5 kg/mm² (56,000 lb./in.²); Cu, 80; Sn, 20, 88.0 kg/mm² (128,000 lb./in.²); Cu, 70; Sn, 10, 165.5 kg/mm² (239,000 lb./in.²). Minimum compressive elastic limit (specification value): A, S, T, M, B, 27-18 T for cylinders 1 in.² (64.5 mm²) area and 1 in. (25.4 mm) long, of Cu, 10 lb./in.² to 15.00 kg/mm² (2,400 lb./in.²) and equals to load required to produce 0.01 per cent set. Average modulus of elasticity of bronzes varies from 7,030 kg/mm² (10,000,000 lb./in.²) according to Winkelman's Handbuch der Physik, 1908, 1, 1, modulus of elasticity of cast bronze (Cu, 88; Sn, 12) 10,600 kg/mm² (15,070,000 lb./in.²); and modulus of elasticity in shear (Cu, 88; Sn, 12) 4,060 kg/mm² (5,770,000 lb./in.²).

²⁹ Compressive proportional limit, 15.5 kg/mm² (22,000 lb./in.²).

³⁰ Compressive proportional limit, 10.5 kg/mm² (15,000 lb./in.²) and 28 per cent set for 70.3 kg/mm² (100,000 lb./in.²).

³¹ Combines strength with fair machining qualities. Good for bushings subjected to severe working conditions.

³² Suitable alloy for bronze-backed bearings.

³³ Compressive elastic limit was taken as the load producing a compression of 0.001 in. (0.025 mm) in the specimen of 1 in.² (64.6 mm²) sectional area and 1 in. (25.4 mm) high.

Composition.		Compressive elastic limit.	
Cu	Pb	kg/mm ²	lb./in. ²
85	10	12.7	18,000
80	10	10.5	15,000
77	8	8.4	12,000
73	7	7.7	11,000
70	5	7.0	10,000

³⁴ 500 kg (1,102 lb.) load.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.			Thermal properties.			Reference.			
			Metric kg/mm ²		English lb./in. ²		Elongation in 50.8 mm or 2 inches.	Reduction of area.	Brinell.	Scleroscope.	Melting point.	Linear coefficient of expansion $\times 10^6$ (per 1°C.)	Casting shrinkage.					
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.								Yield point.		Tensile strength.		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	
Copper—Contd. Tin, lead, phosphorus (phosphor bronze) #1— Cu, 78.5-81.5; Sn, 9.0-11.0; Pb, 9.0-11.0; Z, 0.05-0.25; Zn, max. 0.75; other 1 in P, max. 0.25; Tin, lead, zinc Cu, 76.5-88; Pb, 13; Zn, 4. Tin, lead, zinc #2— Cu, 81; Sn, 7; Pb, 9; Zn, 3. Cu, 88; Sn, 8; Pb, 2; Zn, 2. Tin, lead, zinc, phosphorus— Cu, 73.2; Sn, 11.3; Pb, 12.0; Zn, 2.5; P, 1. Tin, lead, zinc (red brass) #1— Cu, 83.0-86.0; Sn, 4.5-5.5; Pb, 4.5-5.5; Zn, 4.5-5.5; Fe, max. 0.35; Sb, max. 0.25; Al, none. Tin, lead, zinc (car journal bearings) #1— Cu, 93; Sn, 5; C, 30; Sn, 5; Pb, 3.	Cast	8.4	17.6	13.8	13.4-14.1	18.8	19,600	25,800	11.0	11.5	8	8	11.5	11.5	11.5	11.5	(151)	
	do		10.5	21.4	15,000	30,400	4.0	3.3	11	11	11	11	11	11	11	11	11	(169)
	do		8.4	19.0	12,000	27,000	min. 16	16	16	16	16	16	16	16	16	16	16	(152)
	do		29.4	28.5	41,800	40,500	34.5	34.5	23	15	23	15	23	15	23	15	23	(7)
	do		28.5	28.5	40,500	40,500	34.5	34.5	15	23	15	23	15	23	15	23	15	(7)

Cu, 90; Sn, 10do..... 39,000 15 23
 Cu, 85; Sn, 5do..... 38,100 36 14
 Pb, 5; Zn, 5do..... 27.4
do..... 26.8
 # This metal is an excellent composition for use where antifriction qualities are desired, standing up exceedingly well under heavy loads and severe usage.
 38 Compressive strength, 54.2 kg/mm² (77,600 lb./in.²).
 39 Compressive proportional limit, 8.8 to 9.1 kg/mm² (12,500 to 13,000 lb./in.²) and 3.4 to 3.5 per cent set for 70.3 kg/mm² (100,000 lb./in.²).
 40 Compressive strength, 49.3 kg/mm² (70,500 lb./in.²).
 41 Frictioning tests satisfactory.
 42 Compressive strength, 11.9 kg/mm² (17,100 lb./in.²).
 43 Chemical analysis: (1) The lowest per cent of copper to be used, 65; (2) it is desirable to have not more than 5 per cent of tin; (3) it is desirable to increase the percentage of lead rather than zinc; and (4) alloys having 5 per cent of tin, up to 20 per cent of lead and up to 5 per cent of zinc may be satisfactory for car journal bearings.
 Compressive strength of bearing alloys.

Chemical composition (per cent).				Compressive pro- portional limit.		Chemical composition (per cent).				Compressive pro- portional limit.		Com- pression under load of 100,000 lb./in. ² (70.3 kg/mm ²).	
Cu	Sn	Pb	Zn	kg/mm ²	lb./in. ²	Cu	Sn	Pb	Zn	kg/mm ²	lb./in. ²	Per cent.	Per cent.
95	5	0	0	12.7	18,000	75	5	10	10	13.4	19,000	32	32
90	5	0	0	13.4	19,000	75	5	20	0	10.5	15,000	19.5	19.5
90	10	0	0	17.6	25,000	75	10	5	10	19.0	27,000	22	22
85	5	5	5	12.7	18,000	75	10	10	5	20.0	28,500	32	32
85	5	10	0	12.7	18,000	75	10	15	0	16.2	23,000	32	32
85	10	5	0	15.5	22,000	70	5	25	0	11.6	16,500	30	30
80	5	5	10	12.7	18,000	70	5	10	15	13.0	18,500	30	30
80	5	10	5	11.3	16,000	70	5	20	5	12.3	17,500	30	30
80	5	15	0	11.3	16,000	70	10	20	0	14.8	21,000	30	30
80	10	5	5	19.0	27,000	70	10	5	15	28.1	40,000	17	17
80	10	0	0	16.2	23,000	70	10	15	5	18.3	26,000	17	17
75	5	5	15	12.0	17,000	65	5	10	10	20.4	29,000	17	17
75	5	15	5	13.0	18,500	65	5	30	0	10.5	15,000	17	17

Wearing test of some bearing alloys.
 [Total number of revolutions 100,000 (525 r. p. m.), Pressure 1,000 lb./in.² (0.70 kg/mm²).]

Chemical composition (per cent).				Temperature above room.			Wear.	
Cu	Sn	Pb	Zn	°C.	°F.	g.	ft.	
85.76	14.90	28	82	0.2800	0.0181	
95.01	4.95	29	84	0.0766	0.0049	
90.82	4.62	4.82	29	84	0.0542	0.0035	
81.27	5.17	14.14	32	90	0.0327	0.0021	
68.71	5.24	26.67	32	90	0.0204	0.0013	
85.12	4.65	10.64	31	88	0.0380	0.0025	
79.84	4.71	10.30	5.44	37	99	0.0466	0.0030	
74.28	4.68	10.51	11.04	38	100	0.0846	0.0055	

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.			Thermal properties.			Reference.		
			Metric kg/mm ²		English lb./in. ²		Elongation in 50.8 mm or 2 inches.	Reduction of area.	Brinell.	Sclero-scope.	Melting point.	Linear coefficient of expansion $\times 10^6$ (per 1°C.).	Casting shrinkage.				
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.								Yield point.		Tensile strength.	
1	2	8	4	5	6	7	8	9	10	11	12	18	14	15	16	17	18
Copper—Contd. Tin, lead, zinc (car journal bearings)— Continued.										Per ct.			°C.		mm/m	in./ft.	(7)
Cu, 85; Sn, 5; Pb, 10.	Cast.....				22.0					19.5							(7)
Cu, 85; Sn, 10; Pb, 5.do.				23.0					9.5							(7)
Cu, 80; Sn, 5; Pb, 5; Zn, 10.do.				19.8					15							(7)
Cu, 80; Sn, 5; Pb, 10; Zn, 5.do.				24.4					23							(7)
Cu, 80; Sn, 5; Pb, 5.do.				16.4					15.5							(7)
Cu, 80; Sn, 10; Pb, 5; Zn, 5.do.				23.6					3.5							(7)
Cu, 80; Sn, 10; Pb, 10.do.				22.4					8.5							(7)
Cu, 75; Sn, 5; Pb, 5; Zn, 15.do.				19.0					10							(7)
Cu, 75; Sn, 5; Pb, 15; Zn, 5.do.				22.0					19							(7)
Cu, 75; Sn, 5; Pb, 10; Zn.do.				21.0					13							(7)
Cu, 75; Sn, 5; Pb, 20.do.				16.4					15.5							(7)
Cu, 75; Sn, 10; Pb, 5; Zn, 10.do.				17.2					1.0							(7)
Cu, 75; Sn, 10; Pb, 10; Zn, 5.do.				22.0					2.5							(7)
Cu, 75; Sn, 10; Pb, 15.do.				19.0					6							(7)
Cu, 70; Sn, 5; Pb, 25.do.				17.4					14							(7)
Pb, 10; Zn, 15.do.				20.0					10							(7)

Cu, 70; Sn, 5; Pb, 20; Zn, 5; do.	19.8	28, 100	20	15	(7)
Cu, 70; Sn, 10; Pb, 20; do.	19.0	27, 000	6	19	(7)
Cu, 70; Sn, 10; Pb, 5; Zn, 13; do.	19.3	27, 500	1.5	28	(7)
Cu, 70; Sn, 10; Pb, 10; Zn, 10; do.	19.8	28, 100	1.5	23	(7)
Cu, 70; Sn, 5; Pb, 5; Zn, 5; do.	21.1	30, 000	4.7	22	(7)
Cu, 65; Sn, 5; Pb, 10; do.	13.9	19, 800	12	10	(7)
Tin, nickel, zinc (nickel bronze) ^{4c}	9.1	13, 000	31.8	28.0	(180)
Cu, 88; Sn, 5; Ni, 5; Zn, 2; Cu, 89; Sn, 4; Ni, 4; Zn, 3.4 ^{4d}	8.1	11, 500	31.2	31.2	(180)
Tin, phosphorus (phosphor bronze) ^{4c}	91.4	min. 130, 000			(153)
Sn, 4.0-6.0; P, 0.0625 in. (1.59 mm), Spring wire max. 0.2; Fe, 0.0625-0.125 in. max. 0.1; Pb, max. 0.1; Cu, remainder.	84.3	min. 120, 000			(153)
Spring wire (1.59-3.17 mm), Spring wire 0.125-0.250 in. (3.17-6.34 mm), Spring wire 0.250-0.375 in. (6.34-9.51 mm).	77.3	min. 110, 000			(153)
Tin, phosphorus (phosphor bronze) ^{4c}	70.3	min. 100, 000			(153)
Sn, 95; Sn, 4.9; P, 0.1.	45.7	65, 000	30.0	37	(169)
Tin, phosphor- us—80; Sn, 10.5; P, 0.5.	21.8	31, 000- 35, 000	6-10	72-77	(164)
Tin, phosphorus (phosphor gear bronze) ^{4c}	24.6	min. 20, 000	min. 10		(154)
Cu, 88.0-90.0; Sn, 10.0-12.0; P, 0.1-0.3; Pb, Zn, and other imp., max. 0.5.	24.6	min. 35, 000			(154)

^{4b} Modulus of elasticity, 12,200 kg/mm² (17,300,000 lb./in.²).

^{4c} Modulus of elasticity, 10,500 kg/mm² (14,900,000 lb./in.²).

^{4d} The wire shall be capable of being bent through an angle of 180° flat back on itself without fracture on the outside of the bent portion.

^{4e} Cu, 80; Sn, 20; P max. 1; cast. Compressive proportional limit, 17.6 to 28.1, kg/mm² or 35,000 to 40,000 lb./in.² and 6 to 10 per cent set for 70.3 kg/mm² (100,000 lb./in.²) load.

^{4f} Very hard bronze; may be used for gears and worm wheels.

Tin, zinc, lead— Cu, 83; Sn, 14; Zn, 2; Pb, 1	10.5— 13.4	16.2— 19.0	15,000— 19,000	23,000— 27,000	4-0.5	4-0.5	20-24		(164)
Tin, zinc, lead (U.S.N. valve bronze) ⁶⁰ — Cu, 87; Sn, 7; Zn, 5; Pb, 1	13.2	24.8	18,700	35,300	23.2	24.9			(169)
Tin, zinc, lead a— Cu, 90; Sn, 6.5; Zn, 2; Pb, 1.5	12.7— 15.5	23.9— 28.1	18,000— 22,000	34,000— 40,000	33-25	34-26	50-60		(164)
Cu, 85; Sn, 5; Zn, 5; Pb, 5 ⁶⁰	10.5— 13.4	19.0— 23.2	15,000— 19,000	27,000— 33,000	20-16	20-15	50-63		(164)
Cu, 88; Sn, 8; Zn, 2; Pb, 2	11.8— 26.0	21.8— 26.0	19,000— 26,000	31,000— 37,000	20-16		57-59		(164)
Tin, zinc (Gov. bronze or U. S. N. gun bronze or ad- miralty gun metal) ⁶⁰ — Cu, 83; Sn, 10; Zn, 2	8.7	33.8	18,000	48,000	50		64 70	10.8	0.13 (116)
Tin, zinc (gun metal) ⁶⁰ — Cu, 80; Sn, 11; Zn, 8; Fe, max. 0.02; Pb, max. 0.20	10.5	21.1	15,000	30,000	min. 15.0				(193)

⁵⁹ The opinion of various investigators regarding the effect of lead varies: F. Johnson (small chill casting), "Pb does not affect seriously mechanical properties, except shock resistance." H. Primrose (chill casting), "It has even been claimed that 0.5 per cent Pb improves alloy, but it is very doubtful." W. Ramsay, "Even 0.5 per cent Pb reduces tensile strength materially." A. Seaton, "Pb is really a good friend and not an enemy." R. Rolfe, conclusion derived from this investigation, "The proportion of lead may be with advantage increased up to 1 per cent."

³⁸ Stanton Impact test; energy to fracture.

Lead content.	Sand cast.		Chill cast.	
	kgm	ft. lb.	kgm	ft. lb.
0.7	6.7	171	4.2	30
1.36	30.0	217	2.4	17
1.46	14.2	103	4.3	31
1.68	8.2	59	3.5	25

⁶⁰ This alloy is suitable wherever a strong, general utility bronze is required. It may be used for severe working conditions where heavy pressures obtain, as in gears and bearings. U. S. Navy specification 4658B, June 1, 1922: Cu, min. 87; Sn, min. 7; Pb, max. 1.0; Fe, max. 0.06; Zn, remainder. Compressive proportional limit 9.1 kg/mm² (13,000 lb./in.²) with 34 per cent set for 70.3 kg/mm² (100,000 lb./in.²) load. Compressive proportional limit 8.4 kg/mm² (12,000 lb./in.²) with 36 per cent set for 70.3 kg/mm² (100,000 lb./in.²) load. Impurities present in the alloy: Fe, not exceeding 0.10 per cent; S, not exceeding 0.05 per cent; Pb, not exceeding 0.50 per cent (improves machining qualities). Al and Sb are not allowed even in small quantities. ⁶¹ 500 kg (1,102 lb.) load, 10 mm ball.

0.410 in. (10.4 mm), 60 per cent conductivity wire, 0.365 in. (9.27 mm).	43.3	61,600	66,300	(15)
60 per cent conductivity wire, 0.325 in. (8.25 mm).	46.6	min.	100,000	(15)
Spring wire	70.3	min.	100,000	(156)
do.	70.3	min.	100,000	(156)
Zinc (brass) ^{67, 68} Grade A: Cu, 70.0-74.0; Pb, max. 0.1; Fe, max. 0.06; Zn, remainder. ⁶⁹ Grade B: Cu, 64.0-68.0; Pb, max. 0.1; Fe, max. 0.07; Zn, remainder. Zinc (low brass)— Cu, 80; Zn, 20.	24.6 52.7 29.5	35,000 75,000 42,000	31 5 50	(169) (169) (169)
Cast, sand	24.6	35,000	31	(169)
Rolled, hard	52.7	75,000	5	(169)
Rolled, soft	29.5	42,000	50	(169)
Zinc (brass)— Cu, 70; Zn, 30. Cu, 66; Zn, 34 (standard sheet).	28.1 42.2 33.7	40,000 60,000 48,000	35 5 50	(169) (169) (169)
Cast, sand	28.1	40,000	35	(169)
Rolled, hard	42.2	60,000	5	(169)
Rolled, soft	33.7	48,000	50	(169)

⁶⁶ The material is suitable for fittings exposed to the action of salt water, for gears, driving and main nuts of steering gears, and castings for other parts which require strength combined with good bearing qualities and incorrodibility.
⁶⁷ In 10 in. (25.4 mm).
⁶⁸ Modulus of elasticity of brass: Annealed, 9.840 kg/mm² (14,000,000 lb./in.²), Carnegie Steel Co. Pocketbook, 1923. Cast, 8.000-10.000 kg/mm² (11,400,000-14,000,000 lb./in.²), Lendell-Bornstein, Phys.-Chem. Tabellen, Berlin, 1912. Cast, 9.630 kg/mm² (13,700,000 lb./in.²), Proc. Inst. Mech. Eng., 1912, p. 1155. Drawn, 9.400 kg/mm² (13,350,000 lb./in.²), Smithsonian Physical Tables, 1918.

Compressive strength of brass:

Cu	Zn	Cast	
		kg/mm ²	lb./in. ²
90	10	21.1	30,000
80	20	27.4	39,000
70	30	42.2	60,000
60	40	52.7	75,000
50	50	77.3	110,000

Erichsen values for brass: Soft slab, 1.3 mm or 0.05 in. thick; no rolling; depth of impression in standard sheet, 13.9 mm. Cu, 70; Zn, 30; hard sheet, 1.3 mm or 0.05 in. thick; rolled; 38 per cent reduction; depth of impression, 7.4 mm. Cu, 70; Zn, 30; hard sheet, 0.5 mm or 0.020 in. thick; rolled; 60 per cent reduction; depth of impression 3.8 mm. Shearing strength: Brass, cast, 25.3 kg/mm² (36,000 lb./in.²). (Frye, Civ. Eng. Pocketbook, p. 496; 1918.)
⁶⁹ Modulus of elasticity, 10,800 kg/mm² (15,400,000 lb./in.²); modulus of elasticity in shear, 3,660 kg/mm² (5,200,000 lb./in.²); Poisson's ratio, 0.327 (Love, "The mathematical theory of elasticity," 1906).

⁶⁹ The wire should be capable of being bent through an angle of 180° around a wire of the same diameter without breaking.

⁷⁰ Grade A, for use where the requirements are especially severe.

⁷¹ Am. Soc. Test. Mat. specification B 19-19 requires Bhn. of 51-65 at 500 kg (1,102 lb.) load for 70-30 annealed sheet brass.

Cu, 50.19; Zn, 49.81.	9.45 3.6	13.9 24.9	13,400 5,150	19,700 35,400 min. 77 27.5	1.0 5.0 5.5	⁷⁶ 108 ⁷⁶ 117	(117) (117)
Sheet thinner than 0.080 in. (2.03 mm), quarter hard.	31.6			min. 52,500		75-95	(158)
Sheet thinner than 0.080 in. (2.03 mm), half hard.	36.9			min. 77 15.0		95-115	(158)
Sheet thinner than 0.080 in. (2.03 mm), hard.	47.4			min. 67,500		130-150	(158)
Sheet thinner than 0.080 in. (2.03 mm), extra hard.	56.2			min. 80,000		150-170	(158)
Sheet thinner than 0.080 in. (2.03 mm), spring.	61.5			min. 87,500		160-180	(158)
Sheet thinner than 0.080 in. (2.03 mm), light anneal.	31.6			min. 45,000		65-75	(158)
Sheet thinner than 0.080 in. (2.03 mm), drawing anneal.	29.5			min. 42,000		55-65	(158)
Sheet thinner than 0.080 in. (2.03 mm), soft drawing anneal.	28.1			min. 40,000		47-55	(158)
Cast, sand.	20.4			29,000	22		(169)
Rolled, hard.	38.7			55,000	5	60	(169)
Rolled, soft.	26.0	8.7		37,000	40	70 47 10	(169)

Zinc (red metal) —

Cu, 90; Zn, 10.

Zinc (brazing metal) ⁷⁵ —

Cu, 84-86; Fe, max. 0.06; Pb, max. 0.3; Zn, remainder.

⁷² A pin having a taper of 1 to 8 shall be driven into one end of a tube until the diameter is increased 15 per cent. The tube shall withstand this test without showing cracks, splits, or other defects.

⁷³ Muntz metal should not be annealed at temperatures between 750 and 800° C. (1,382 and 1,472° F.), as this is a danger range, but it may be heated above 600° C. (1,112° F.) without destroying its good qualities.

⁷⁴ Shall be bent cold through 120° to a radius equal to the diameter or thickness without signs of cracking or failure. Suitable for bolts and nuts not subject to action of salt water for sheathing bottoms of wooden boats, etc.

⁷⁵ Winkelman's Handbuch der Physik, 1908, I, 1, gives for 60/40 cast brass the modulus of elasticity 9,220 kg/mm² (13,100,000 lb./in.²) and modulus of elasticity in shear 3,390 kg/mm² (4,820,000 lb./in.²).

⁷⁶ 10 mm ball and 1,000 kg (2,204 lb.) load.

⁷⁷ In very thin sheets, on account of the difficulties in testing, the elongation may be considerably less than the values given above.

⁷⁸ Suitable for all flanges for copper pipe and other fittings that are to be brazed.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.				Thermal properties.			Reference.	
			Metric kg./mm. ²		English lb./in. ²		Elongation in 50.8 mm or 2 inches.	Reduction of area.	Brinell.	Sclero-scope.	Melting point.	Linear coefficient of expansion × 10 ⁶ (per 1 °C.).	Casting shrinkage.				
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.								Yield point.	Tensile strength.		
1	2	8	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Copper—Contd.																	
Zinc, aluminum— Cu, 70.5; Zn, 26.4; Al, 3.1.			13.4		33.0	19,000		47,000	Per ct. 50.0				°C.		mm/m	in./ft.	(169)
Cu, 62.9; Zn, 33.3; Al, 3.8.					56.2			80,000									(169)
Cu, 57; Zn, 42; Al, 1.	Cast.				40.0			57,000	50.0								(169)
Cu, 55; Zn, 41; Al, 4.					60.0			85,400	16.5								(169)
Zinc, aluminum (aluminum brass)—																	
Cu, 69.79; Zn, 26.67; Al, 3.54.	Cast.			21.4	46.1			30,450	26.0	27.6	79 104						(117)
Cu, 69.13; Zn, 26.32; Al, 4.55.	Forged			36.8	58.4			52,400	34.0	41.9	79 143						(117)
Cu, 69.42; Zn, 24.66; Al, 2.90.	Cast.			27.7	50.2			39,400	8.0	11.7	79 134						(117)
Cu, 59.8; Zn, 38.56; Al, 2.18.	Forged			44.2	60.8			45,500	17.0	20.0	79 143						(117)
Cu, 59.85; Zn, 37.13; Al, 3.02.	Cast.			51.2	66.5			62,900	3.0	1.5	79 185						(117)
Iron, vanadium (victor bronzes) ^{90a} —				50.4	59.8			72,800	6.0	8.4	79 193						(117)
Cu, 58.4; Zn, 38.5; Fe, 1.0; V, 0.03.	Cast.			25.2	49.3			33,350	30.0	33.5	79 114						(117)
Iron—				18.2	25.2			23,800	11.0	14.6	79 104						(117)
Cu, 59.45; Zn, 35.85; Al, 0.98; Mn, 3.49; Fe, 0.22; P, 0.01.	Cast.			35.1	58.0			32,700	16.0	21.5	79 128						(117)
	Forged			29.9	63.5			50,000	18.5	24.5	79 159						(117)
Zinc, aluminum, iron, vanadium (victor bronzes) ^{90a} —								42,600	24.5	30.6	79 134						(117)
Cu, 58.6; Zn, 38.5; Al, 1.5; Fe, 1.0; V, 0.03.	Cold, drawn.		56.2		64.6	80,000			11.5	29.0							(169)
Zinc, aluminum, manganese, iron—																	
Cu, 59.45; Zn, 35.85; Al, 0.98; Mn, 3.49; Fe, 0.22; P, 0.01.	Cast.			21.1	50.1			30,000	25.0	24.6	81 114						(118)
	Forged			32.6	55.3			46,300	36.0	47.2	81 134						(118)

Cu, 59.45; Zn, 36.6; Al, 1.56; Mn, 1.97; Fe, 0.40; P, 0.02.	26.8 27.1	56.5 58.3	38,100 38,500	80,400 82,800	22.0 28.0	20.0 30.6	81,138 81,148	(118) (118)
Cu, 58.15; Zn, 35.18; Al, 2.24; Mn, 4.10; Fe, 0.25; Pb, 0.08.	37.6 39.1	63.8 68.4	53,500 55,600	90,700 97,300	14.0 18.5	15.0 21.5	81,165 81,159	(118) (118)
Cu, 57.23; Zn, 37.9; Al, 2.59; Mn, 2.08; Fe, 0.20.	30.6 32.3	65.2 67.1	43,400 45,900	92,800 95,400	18.0 24.0	20.0 24.5	81,165 81,159	(118) (118)
Zinc, aluminum, manganese, iron (tensile) ⁸²								
Cu, 64; Zn, 29; Al, 3.1; Mn, 2.5; Fe, 1.2.	21.1	68.9	30,000	98,000	16.0	17.0	130	(169)
Zinc, aluminum, manganese, vanadium—metal ⁸²								
Cu, 58.6; Zn, 38.5; Al, 1.5; Mn, 0.5; V, 0.03.	35.6	57.2	50,600	81,400	12.0	14.0		(169)
Zinc, iron, tin, aluminum, manganese, manganese bronze ⁸³								
Cu, 55.7; Zn, 42.4; Fe, 1.8; Sn, 0.8.	8.4	42.5 53.6 58.5	60,500 76,200 83,100					(125) (125) (125)
Zinc, iron, tin, aluminum, manganese, iron—metal ⁸²								
Cu, 56.2; Zn, 41; Fe, 1; Sn, 1; Al, 0.5; Mn, 0.5.	23.2	49.2	33,000	70,000	22-35	25.0	104-119	(164)
Zinc, iron—metal ⁸²								
Cu, 58.96; Zn, 41.04.	13.9 14.2	39.2 40.9	19,700 20,200	55,700 58,200	45.0 47.5	49.7 62.0	81,90 81,90	(119) (119)
Cu, 59.37; Zn, 39.68; Fe, 0.95.	14.8	42.2	21,000	60,000	44.0	44.6	81,90	(119)
Cu, 59.04; Zn, 38.95.	21.9	45.3	31,100	64,500	44.0	63.7	81,107	(119)
1.56; Pb, 0.45.	17.3	42.2	24,600	60,000	33.0	30.6	81,85	(119)
Cu, 59.12; Zn, 38.36; Fe, 2.52.	21.4	43.4	30,400	61,800	43.0	59.3	81,98	(119)
	15.7 24.9	41.7 44.5	22,400 35,400	59,300 63,400	46.0 39.0	49.7 54.6	81,92 81,110	(119) (119)

⁷⁹ 10 mm ball, 1,000 kg (2,204 lb.) load.
⁸⁰ Specification values, U. S. Navy 49 B1b, Jan. 3, 1976: Vanadium bronze castings: Cu, min. 61; Zn, 38; Sn, max. 1 (including V), min. values. Proportional limit, 15.8 kg/mm² (42,500 lb./in.²); tensile strength, 38.7 kg/mm² (85,000 lb./in.²), with 25 per cent elongation.

⁸¹ 10 mm ball and 1,000 kg (2,204 lb.) load.

⁸² Cu, 67; Zn, 24; Al, 4.4; Mn, 3.8; P, 0.01; compressive proportional limit 42.3 kg/mm² (90,000 lb./in.²) and 1.33 per cent set for 70.3 kg/mm² (100,000 lb./in.²) load.

⁸³ Compressive proportional limit 19.8 to 20.0 kg/mm² (47,500 to 48,500 lb./in.²).

Zinc, iron (delta metal)	Cast, sand	31.7	45,000	10.0					(126)
Cu, 57; Zn, 42; Fe, 1.	Rolled, hard	42.2	60,000	17.0					(126)
Zinc, iron (delta metal) ³⁶	Cast	31.7	45,000	10.0					(98)
Cu, 60; Zn, 36; Fe, 1 (-); Sn, 2 (1-5).	Rolled	43.2	70,000	17.0					(98)
	Wire	84.4	90,000-120,000						(98)
Zinc, iron - Cu, 65; Zn, 30; Fe, 5.5	Rolled, hard	45.7	65,000						(103)
Zinc, iron, manganese - Cu, 60; Zn, 38.5; Fe, 1; Mn, 4.	Cast	49.2	35,000	25					(169)
Zinc, iron, manganese (manganese bronze) ³⁷	Rolled	63.2	45,000	25					(169)
Cu, 55.5; Zn, 41.3; Fe, 0.95; Mn, 0.87; Al, Sn, Pb.	Cast	50.5	60,700	21.6					(120)
Zinc, iron, tin, aluminum (manganese bronze)	do	50.7-59.1	72,000-84,000	35-22	109-119				(164)
Cu, 56; Zn, 41.5; Fe, 1; Sn, 0.75; Al, 0.5.									
Zinc, iron, tin, aluminum, manganese (manganese bronze) ³⁸	do	49.7	31,000	26					(90)
Cu, 57.0 ³⁸ ; Zn, 41.0; Sn, 0.80; Fe, 0.55; Al, 0.3.									
Zinc, lead (cast-lead brass)	do	23.2-27.5	33,000-39,000	30-26	35-30				(169)
Cu, 60-63.5; Zn, 35-33.5; Pb, 5.3.	Sheet, annealed	29.5	42,000	50					(169)
	Sheet, hard	42.9	61,000	30					(169)

³¹ First values are for longitudinal specimens; second for transverse specimens.

³² Malleable at red heat and can be hammered, rolled, or drawn into fine wire. Addition of Fe increases strength. Aichi's metal is about 50 per cent stronger than brass of the same composition but without Fe. At 200° F. (93° C.) tensile strength equals 31.6 kg/mm² (45,000 lb./in.²); at 500° F. (260° C.) tensile strength equals 21.1 kg/mm² (30,000 lb./in.²); at 900° F. (482° C.) tensile strength equals 7.0 kg/mm² (10,000 lb./in.²).

³³ Has great strength and toughness, gives good castings; can be rolled and forged hot; stands a fair amount of drawing and hammering when cold; when exposed to atmosphere tarnishes less than brass; takes high polish. According to Winkelmann's Handbuch der Physik, 1908, I, p. 557, the modulus of elasticity is 11,700 kg/mm² (16,600,000 lb./in.²).

³⁴ Scrap metal was used.

³⁵ The effect of various components: Sn increases tensile strength and raises yield point. More than 0.8 per cent of tin lowers ductility. Ordinarily the content of tin is 0.75 per cent; Fe increases tensile strength and raises yield point. Makes the grain smaller. Amount of iron usually about 0.7 per cent; Al is added to obtain fluidity in pouring; 0.3-0.5 per cent is considered sufficient; Mn increases hardness and strength; is added for deoxidizing. 0.3 per cent is sufficient; Pb weakens alloy, maximum permissible amount 0.2 per cent.

³⁶ Average of nine determinations.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.				Thermal properties.			Reference.		
			Metric kg./mm ²		English lb./in. ²		Elongation in 50.8 mm or 2 inches.	Reduction of area.	Brinell.	Sclero-scope.	Melting point.	Linear coefficient of expansion $\times 10^6$ (per 1° C.).	Coating shrinkage.					
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.								Yield point.	Tensile strength.			
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	
Copper—Contd.																		
Zinc, lead, tin (yellow brass) ⁹⁶ —																		
Cu, 62.0-65.0; Zn, 31.0-36.0; Pb, 2.0-4.0; Sn, max. 1.0; Fe, max. 0.5; Al, none; other imp., 0.25.	Cast			8.4	17.6													(159)
Cu, 70; Sn, 27; Pb, 2; Sn, 1.	do		7.4		20.7	10,500			29,500	25.0	53							(164)
Zinc, lead, brass ⁹⁷ (red)	do	8.6	11.3		21.1	16,000			30,000	17.0		7.0						(103)
Cu, 83; Zn, 7; Pb, 6; Sn, 4.	do																	
Copper, zinc, lead, tin—	do	8.87	8.4		18.6	12,000			26,500	23.0								(169)
Cu, 78; Zn, 9.5; Pb, 10; Sn, 2.	do																	
Zinc, manganese (manganese bronze) ⁹⁸ —																		
Cu, 58; Zn, 39; Mn, 0.05; Sn; Fe; Al; Pb.	Cast, sand			21.1-24.6	49.2-52.7	30,000-35,000	30,000-35,000	70,000-75,000	30-22	32-25	109-119	18-19						(169)
	Cast, chill			22.5-26.0	52.7-56.2	32,000-37,000	32,000-37,000	75,000-80,000	32-25	34-28	119-130	18-22						(169)
Zinc, tin, iron, aluminum, manganese (manganese bronze) ⁹⁹ —																		
Cu, 53.72; Zn, 39.05; Sn, 0.79; Fe, 1.06; Mn, 0.04; Al, 0.07; Pb, 0.12.	Cast, sand	8.4		49.2-52.7	49.2-52.7	70,000-75,000	70,000-75,000	70,000-75,000	22-30	109-119					20.8	0.25		(111)
	Cast, chill			52.7-56.2	52.7-56.2	75,000-80,000	75,000-80,000	75,000-80,000	25-32	119-130					20.8	.25		(111)

Zinc, manganese (manganese bronze) ⁸⁰ — Cu, 56-60; Zn, 37-42; Fe, Sn; Mn.	21.1 56.2	42.2 70.3	30,000 80,000	60,000 100,000	8-10 12-15			(98) (98)
Zinc, manganese— Cu, 60; Zn, 39; Mn, Ir.	8.3 31.6	52.7	45,000	75,000	25	28	30	(169)
Zinc, manganese, tin, aluminum (manganese bronze)— Cu, 55-57; Zn, 38-42; Mn, 0-1.5; Al, 0-3.50; Fe, 0-1.50; Pb, 0-2.0; 0-0.2.		45.7		65,000	20			(197)
Zinc, manganese (manganese bronze) ⁸⁰ — Cu, 53.0-62.0; Zn, 38.0-47.0; Pb, max 0.15.	21.1	42.2 49.2	30,000 min.	60,000 min. 70,000	15 20			(160) (160)
Zinc, manganese, aluminum, lead, (manganese bronze)— Cu, 53-62; Zn, 36-54; Al, 0.05-0.5; Pb, max 0.15.		49.2		70,000	20.0			(16)
Zinc, manganese, iron, silicon— Cu, 56.95; Zn, 39.72; Mn, 1.01; Fe, 0.24; Si, 0.08.	15.9 15.9	39.5 41.1	22,600 22,600	56,200 58,500	51.0 47.0	49.7 57.0	** 80	(119) (119)
Cu, 58.42; Zn, 39.8; Mn, 1.48; Fe, 0.25; Cu, 58.42; Zn, 39.23; Mn, 2.0; Fe, 0.26; Si, 0.05.	14.0	40.9	19,900	58,200	49.0	61.5	** 90	(119)
.....do.....	14.3	42.3	20,400	60,200	45.0	52.7	** 90	(119)

⁸⁰ Good machining properties.
⁸¹ Compressive strength 54.5 kg/mm² (77,500 lb./in.²).—Philadelphia & Reading Railway Co. letter to U. S. Bureau of Standards Apr. 25, 1917.
⁸² Modulus of elasticity, sand cast 9,840 kg/mm² (14,000,000 lb./in.²).
⁸³ Specification values: U. S. Navy 46B16-a, cast, minimums, tensile strength 49.2 kg/mm² (70,000 lb./in.²) with 40 per cent elongation in 2 in. (50.8 mm); U. S. Navy 46B15a, rolled, minimums, proportional limit 24.6 kg/mm² (35,000 lb./in.²), tensile strength 49.2 kg/mm² (70,000 lb./in.²) with 30 per cent elongation in 2 in. (50.8 mm); Cu, 57-66; Zn, 42-37; Fe, max 2.0; Sn, 0.5-1.5 (2.9 per cent increase in values for thicknesses of 1 in. (25.4 mm) and under).
⁸⁴ Compressive strength of cast bronze is 91.4 kg/mm² (130,000 lb./in.²). Very ductile and may be bent hot or cold. Not easily corroded. Used in machinery where corrosion may occur.
⁸⁵ This metal may be hardened by the addition of small amounts of Sn, Fe, Mn, Al, or a combination of these metals. Used where strength and toughness are required.
⁸⁶ 10 mm Ball and 1,000 kg (2,205 lb.) load.

Cu, 61.6; Zn, 19.9; Ni, 22.4; 9.8; Ni, 28.0; Cu, 65.82; Ni, 6.17; Fe, 0.23; Mn, 0.06; Pb, 1.27; Zn, balance.	8.71	13.4	27.1	19,100	38,500	24.5	26.7	86	(85, 86, 87)
do.	8.74	13.8	31.1	19,600	44,200	32.0	36.7	69	(85, 86, 87)
Cold rolled, mill annealed.	18.7	37.8	37.8	26,600	53,700	55.2	61.2	65	(47)
Cold rolled, 28.3 per cent reduction.	47.7	47.7	52.2	67,700	74,200	14.2	45.9	140	(47)
Cold rolled, 46.3 per cent reduction.	64.7	64.7	64.7	92,000	92,000	5.0	34.7	161	(47)
Cold rolled, 74.5 per cent reduction.	75.8	75.8	75.8	107,800	107,800	2.2	18.0	175	(47)
Cu, 64.68; Ni, 6.73; Fe, 0.19; Mn, 0.06; Zn, balance.	17.4	47.4	37.8	24,700	53,800	64.5	65.7	65	(47)
Cold rolled, mill annealed.	47.4	47.4	50.2	67,400	71,400	23.7	53.1	132	(47)
Cold rolled, 24.6 per cent reduction.	67.8	67.8	67.8	96,400	96,400	4.7	34.1	170	(47)
Cold rolled, 49.8 per cent reduction.	78.9	78.9	78.9	112,300	112,300	2.5	26.5	176	(47)
Cold rolled, 75.4 per cent reduction.									

⁸⁷ Can be rolled and worked both hot and cold.

⁸⁸ The alloy can be hot worked.

⁸⁹ Used for parts requiring a metallic-white finish.

¹ Modulus of elasticity 11,450-13,300 kg/mm² (16,300,000-18,900,000 lb./in.²).

² The correlation between the heat treatment of nickel-silvers and their mechanical properties is shown in Figures 15 and 16. The chemical composition of the three alloys tested is given in the table below.

Copper.....	59.26	59.72	60.20	Manganese.....	Trace.	Trace.	Trace.
Nickel.....	10.65	15.91	19.29	Sulphur.....	0.039	0.055	0.052
Lead.....	Nil	Nil	.09	Carbon.....	116	.185	.185
Iron.....	.39	.46	.47	Zinc.....	Balance.	Balance.	Balance.

³ The commercial nickel-silvers have small amount of lead (less than 0.5 per cent) and iron (about 0.30 per cent); total amount of impurities, less than 1 per cent. An addition of manganese (about 0.25 per cent) increases ductility without loss of strength.

Compression at 157.5 kg/mm² (224,000 lb./in.²).

Alloy.		Com- pression.
Cu	Ni	Zn
60.6	7.6	31.7
61.8	16.4	21.7
61.6	22.4	15.9
61.2	28.6	9.8
		Per cent.
		57.2
		56.2
		57.8
		55.0

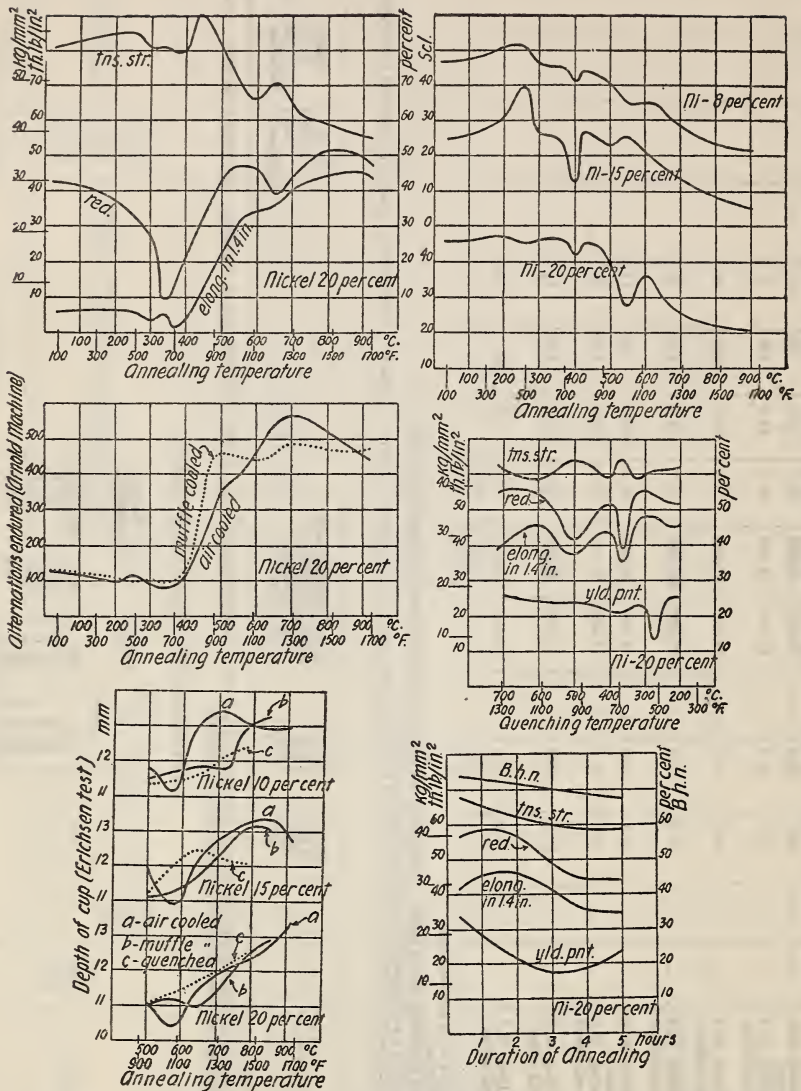


FIG. 15.—Correlation between the heat treatment and the tensile properties of nickel-silvers.

F. C. Thompson, Jour. Inst. Met., 15, p. 230; 1916; 17, p. 119; 1917; 27, p. 227; 1922. For chemical composition see Table 7.

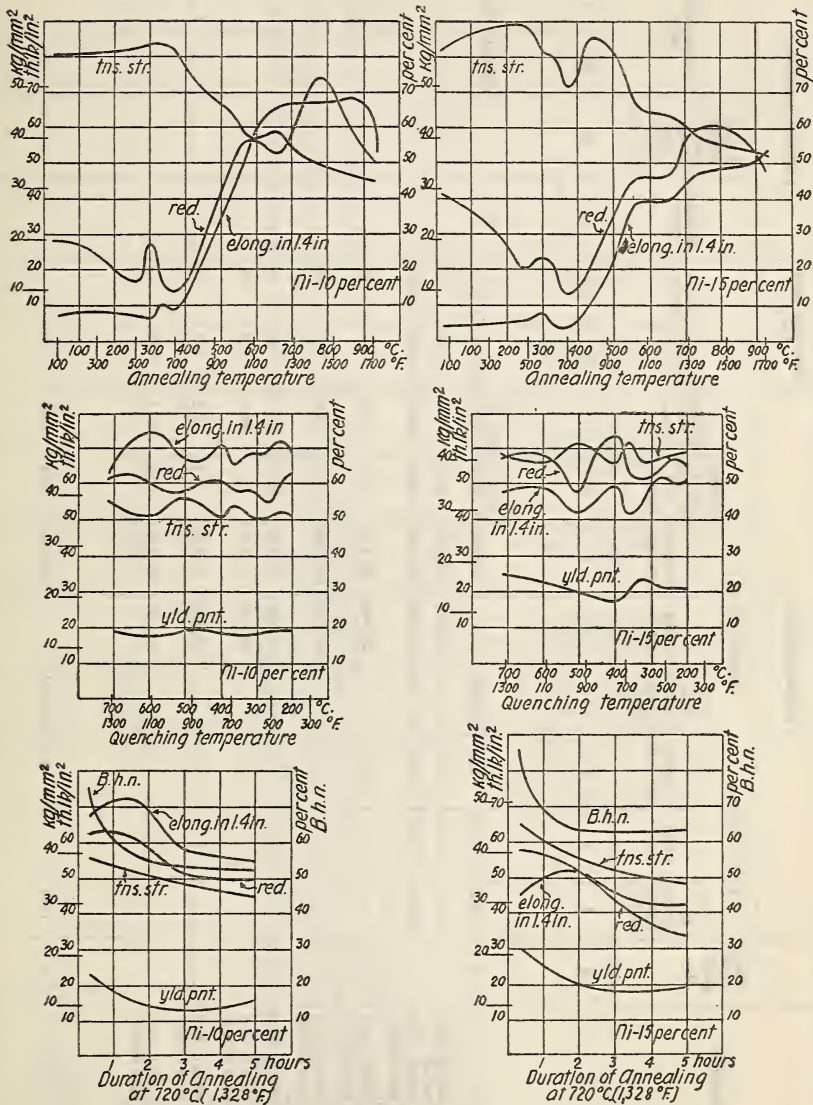


FIG. 16.—Correlation between the heat treatment and the tensile properties of nickel-silvers.

F. C. Thompson, Jour. Inst. Met., 15, p. 230; 1916; 17, p. 119; 1917; 27, p. 227; 1922. For chemical composition see Table 1.

Zinc, nickel, tungsten (platinoid) ⁷ — Cu, 60; Zn, 24; Ni, 14; W, 1-2.	11.0	30.0	15,700	42,600	29.6	32.0	(44)
Zinc, tin (Naval brass) ⁸ — Cu, 61; Zn, 38; Sn, 1.	26.0	43.6	37,000	62,000	25.0	37.0	(169) (169)
Zinc, tin (Tobin bronze) ⁹ — Cu, 58.2; Zn, 39.5; Sn, 2.3.	8.3	42.2	25,000	60,000	35.0	40.0	(169) (169)
Zinc tin (Durama metal) ¹⁰ — Cu, 58.7; Zn, 39.6; Sn, 1.0; Pb, 0.4; Fe, 0.34.	8.4	55.5	54,000	79,000	35.0	40.0	(76)

⁴ Brinell hardness of nickel-silver (with Ni, 9 per cent) = 130 as rolled and 50 as annealed at 930° C. (1,700° F.).
⁵ U. S. Navy Department specification 46S3a, June 1, 1917. German silver: Cu, 66-67; Zn, 18-22; Ni, min. 15; no mechanical requirements. For list of 30 German-silver alloys see Brantt "Metallic Alloys," p. 314, "best" (Horns), "hard Sheffield," Cu, 46; Zn, 20; Ni, 34.
⁶ Modulus of elasticity, 11,000 kg/mm² (15,600,000 lb./in.²). Poisson's ratio 0.37. Winkelman's Handbuch der Physik, 1908, 1, 1, gives for modulus of elasticity of drawn nickel-silver 11,450 kg/mm² (16,270,000 lb./in.²) and for modulus of elasticity in shear (condition not specified) 3,870 kg/mm² (5,500,000 lb./in.²).
⁷ Has high electrical resistance, which does not decrease with heat. Mechanical properties as those of nickel-brass.
⁸ Specification values, naval brass castings, U. S. Navy 46B10C, July 1, 1922, normal proportions: Cu, 62; Zn, 37; Sn, 1. Minimum tensile strength, 17.6 kg/mm² (23,000 lb./in.²) with 15 per cent elongation in 2 in. (50.8 mm).
⁹ Modulus of elasticity, 7,430 kg/mm² (10,600,000 lb./in.²).

Effect of High Temperature on Tensile Properties of Durama Metal of Above Composition.

Temperature.		Proportional limit.		Tensile strength.		Elongation.	Reduction of area.
°C.	°F.	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	Per cent.	Per cent.
24	75	18.0	25,600	40.8	58,000	32	36
95	203	17.2	24,500	34.5	49,000	27	33
148	298	17.0	24,200	31.4	44,700	44	50
170	338	16.4	23,300	28.0	39,800	50	51
214	417	12.5	17,800	18.0	25,600	62	52
320	608	4.5	6,400	6.5	9,230	61	53
420	788	1.6	2,270	2.0	2,840	39	40
542	1,0085	710	30	42

Zinc, tin (Naval brass)— Cu, 59-63; Sn, 0.5-1.5; Fe, max.0.06; Pb, max.0.2; Zn, remainder.	Tubing and sheet, wall or thickness, 0.125-0.25 in. (3.17-6.34 mm).	23.2	38.7	33,000	55,000	25	(198)	
	Tubing and sheet, wall or thickness, over 0.25 in. (6.34 mm).	21.1	35.2	30,000	50,000	27	(198)	
Rods 0-0.5 in. (12.7 mm) diameter. ¹⁰	Rods 0-0.5 in. (12.7 mm) diameter. ¹⁰	19.0	42.2	27,000	60,000	35.0	(199)	
	Rods 0.5-1.0 in. (12.7-25.4 mm) diameter. ¹⁰	18.3	40.8	26,000	58,000	40.0	(199)	
Rods over 1 in. (25.4 mm) diameter. ¹⁰	Rods over 1 in. (25.4 mm) diameter. ¹⁰	17.6	38.0	25,000	54,000	40.0	(199)	
	Sheets (all) ¹¹	15.7	39.4	22,400	56,000	30.0	(199)	
Plates to 0.5 in. (12.7 mm) thick, average. ¹²	Plates to 0.5 in. (12.7 mm) thick, average. ¹²	19.3	38.7	27,500	55,000	32.0	(199)	
	Plates over 0.5 in. (12.7 mm) thick. ¹³	17.6	39.4	25,000	56,000	35.0	(199)	
Tubing wall up to 0.125 in. (3.17 mm) thick.	Tubing wall up to 0.125 in. (3.17 mm) thick.	21.1	42.2	30,000	60,000	28.0	(199)	
Tubing wall over 0.25 in. (6.35 mm) thick.	Tubing wall over 0.25 in. (6.35 mm) thick.	19.7	38.7	28,000	55,000	32.0	(199)	
Zinc, tin, lead (U. S. Navy brass)— Cu, 78; Zn, 16; Sn, 4; Pb, 3.	Cast.....	11.3	20.3	16,100	28,900	19.0	23.2	(169)
	Forged.....	17.3	41.3	24,600	58,700	44.0	42.0	14 87
Zinc, tin, iron— Cu, 59.95; Zn, 0.47; Fe, 0.20.	Cast.....	24.6	45.4	35,000	64,500	38.0	60.0	14 107
	Forged.....	15.1	42.0	21,500	59,800	32.0	33.5	14 98
Cu, 58.90; Zn, 40.10; Sn, 1.00; Fe, trace.	Cast.....	21.4	45.1	30,400	64,100	38.0	44.6	14 107
	Forged.....	18.6	41.1	26,400	58,500	13.0	15.0	14 114
Cu, 58.82; Zn, 38.176; Sn, 2.0; Fe, 0.31.	Cast.....	25.8	33.4	36,800	47,600	1.5	3.2	14 136
	Forged.....	25.8	33.4	36,800	47,600	1.5	3.2	14 136

¹⁰ A. pin having a taper of 1 to 8 shall be driven into one end of a tube until the diameter is increased 15 per cent. The tube shall withstand this test without showing cracks, splits, or other defects.

¹¹ The rods shall stand cold bending without fracture through an angle of 120° around a pin, the radius of which is equal to the diameter or thickness of the rod or bar.

¹² Must stand hammering hot to a fine point and bending cold through 120° with inner radius equal to diameter or thickness of bar.

¹³ Required to bend 120° cold about radius equal to diameter.

¹⁴ 10 mm ball and 1,000 kg (1,204 lb.) load.

Al, 3.08.....	As forged Annealed at 1,000° C. (1,832° F.).	48.0 28.4	54.5 37.5	68,200 31,800	77,500 53,400	31.0 51.0	76.4 83.3	(94) (94)
Al, 6.24.....	As forged. Annealed at 1,000° C. (1,832° F.).	54.6 37.6	60.5 49.1	77,700 53,400	86,000 69,800	28.0 27.0	74.7 55.5	(94) (94)
Silicon— Si,0.01; C,0.01; (laboratory product).	As forged. Melted in vacuo and annealed at 970°C. (1,778° F.).	29.4 11.2	31.8 24.5	41,800 16,000	45,200 34,900	35.0 53.0	78.0 81.5	(95) (95)
Si, 1.71.....	As forged. Annealed at 970° C. (1,778° F.).	48.0 25.2	53.6 38.1	68,100 35,800	76,300 54,200	29.0 50.0	87.2 90.6	(95) (95)
Si, 4.40.....	As forged. Annealed at 970° C. (1,778° F.).	66.1 51.3	74.0 64.4	94,000 72,900	105,000 91,600	6.0 24.0	7.5 25.1	(95) (95)

15. Genelite is a bearing metal. It is a mixture of high-grade synthetic bronze and graphite (40 per cent); made of oxides of tin, lead, and copper, and graphite. All in a finely divided state. Mixture is pressed together and subjected to heat which sinters the metals together; has self-lubricating qualities; possesses high degree of porosity; can absorb 2.5 per cent of oil, and this is made use of in high-speed bearings.

16. White metal (bearing metal), can be easily forged and cold-rolled into sheets; takes high polish; scratches glass, hardness between 6 and 7 (Mohs' scale); not altered by air, does not burn even if area heated to redness; not affected by cold or boiling water or steam; not attacked by nitric acid or ammonia but dissolves in a potash solution. It is attacked by hydrochloric acid and is concentrated sulphuric acid.

17. Modulus of elasticity, 1,450,000-3,500,000 kg./mm² (9,930,000-23,500,000 lb./in.²); modulus of elasticity in shear, 2,650-3,900 kg./mm² (3,700,000-5,540,000 lb./in.²). Poisson's ratio 0.42.

18. Smithsonian Physical Tables, 7th edition, 1920.

19. At 200 kg. (441 lb.) load.

20. Modulus of elasticity, 33,000 kg./mm² (715,000,000 lb./in.²).

21. Compressive strength, 35.1 kg./mm² (50,000 lb./in.²).

22. The effects of carbon and manganese mechanical properties of pure iron.—The results obtained on annealed and normalized specimens of alloys containing from 0 to 1.6 per cent carbon and 0 to 1.6 per cent manganese were as follows: (1) The tensile strength of iron-manganese alloys containing from 0 to 1.6 per cent manganese had been increased by addition of carbon up to 1.0 per cent. The rate of increase of strength was from 0.615 to 0.808 kg./mm² (875 to 1,150 lb./in.²) for each 0.1 per cent of carbon. (2) The yield point of iron-manganese alloys was influenced by the greater was the strengthening effect of carbon. Above 1 per cent of carbon its effect was the decrease of tensile strength. (3) The elongation of iron-manganese alloys was influenced by the increase of carbon content in about the same manner as their tensile strength. The increase of hardness was 1.8-2.6 Brinell units for each 0.1 per cent carbon. Beyond that percentage the effect of carbon content was small. (4) Carbon influenced the proportional limit less than the other properties. Maximum values were reached at lower carbon content than the maximum values for tensile strength and remained about constant over a wide range of carbon content. (5) Manganese increased tensile strength from 0.063 to 0.176 kg./mm² (90 to 250 lb./in.²) for each 0.1 per cent of manganese, the lower limit corresponding to iron with low-carbon content. (6) Proportional limit was influenced by manganese in about the same manner as the tensile strength. (7) Brinell hardness numbers were increased about 0.5 Brinell unit by each 0.01 per cent of manganese, the rate of increase being lower in alloys with low-carbon content than in alloys with high carbon. (8) Manganese had very little effect on ductility. (9) The effect of carbon and manganese were each influenced by the other. The increase of carbon increased the effect of manganese, and vice versa.

23. Properties of Swedish iron (impurities less than 1 per cent) approximately equal those of electrolytic iron. Compressive strength (specimens, 25.4 mm. or 1 inch, diameter, 76.2 mm. or 3 inches, long), 56.3 kg./mm² (80,000 lb./in.²). Modulus of elasticity in tension and compression, 17,600 kg./mm² (25,000,000 lb./in.²). Modulus of elasticity in shear, 7,030 kg./mm² (10,000,000 lb./in.²). Shearing proportional limit, 8.4 kg./mm², or 12,000 lb./in.². Shearing strength, 21.1 kg./mm², or 30,000 lb./in.².

24. 500 kg. (1,102 lb.) load.

25. Erichsen values for good trade quality sheets, 0.4 mm (0.0156 in.) thickness, soft annealed:

Kind of sheet.	Depth of cup.	
	mm	in.
Sheet metal, hoop iron, polished.....	9.5	0.374
Charcoal iron, finned sheet.....	7.5	.295
Second quality, finned sheet.....	6.7	.264

26. Smithsonian Physical Tables, 7th edition, 1920.

TABLE 9.—Standard Terminology for the Ferrous Materials in Principal European Languages.

Names.							
English.	French.	Italian.	Spanish.	German.	Swedish.	Danish.	Dutch.
Species.							
Cast iron.....	Fonte.....	Ghisa.....	Fundición de hierro.....	Roheisen If not remelted, Gusseisen If remelted.	Tackjern Gjutjern.....	Raajern naar deeltlike er omsmetet eller Støbejern.	Gietzyzer (ruwzyzer).
Varieties.							
White cast iron or pig iron.	Fonte blanche.....	Ghisa bianca in pani, Ghisa bianca.	Lingote de hierro blanco y fundición de hierro blanco.	Weisses Roheisen...	Hvitt tackjern.....	Hvidtjern.....	witgietzyzer (witruwzyzer).
Gray cast iron or pig iron.	Fonte grise.....	Ghisa grigia.....	Lingote de hierro gris y fundición de hierro gris.	Graues Roheisen.....	Grått tackjern.....	Graattjern n Graat Raajern.	Grauw gietzyzer.
Mottled cast iron or pig iron.	Fonte truitée.....	Ghisa tritata.....	Lingote de hierro manchado y fundición de hierro truchado.	Halbirtes Roheisen.	Hagelsatt or Halfhvitt or halgrått tackjern.	Spragletjern.....	wit korrelgietzyzer.
Pig iron (white, gray, mottled, etc.).	Gusenes de fonte ou fonte en guesse.	Ghisa.....	Lingote de hierro.....	Gusseisen Roheisen (in Massein oder Güssen), Gusseisen (weiss, grau, halbblott).	Tackjern.....	Pigjern or Raajern..	Ruwzyzer (gemeleerd).
Hot metal, or direct metal.	Fonte de première fusion.	Ghisa da prima fusione liquida.	Metal caliente ó metal directo.	Remelsen Rohelsen, Gusseisen erster Schmelzung.	Tackjern direct glutet från Masugn.	Smettet Raajern.....	Ruwzyzer eerste gieting.
Basic cast iron or pig iron.	Ghisa basica in pani.	Lingote de hierro básico.	Thomasroheisen.....	Thomas Raajern...	Thomas ruwzyzer.
Hematite cast iron or pig iron.	Ghisa ematite in pani.	Lingote de hierro hematites.	Hämatitroheisen.....	Hämatit Raajern...	Häematitruwzyzer.
Malleable pig iron.	Ghisa per affunzione.	Lingote de hierro maleable.	Schmidbares Gusseisen.	Hammerbart-Støbejern.	Smeedbaargietzyzer.
Washed metal.....	Fonte épurée.....	Metallo desforao.....	Fundición de hierro refinada ó lavada.	Entphosphorites Roheisen.	Tvättad.....	Afosforet Raajern...	Ontphospherd gietzyzer.
Refined cast iron.....	Fonte mazée.....	Ghisa afinata.....	Fundición de hierro refinada ó depurada.	Gesseintes Eisen....	Raffineradtjern.....	Raajern til Hardfriskning.	Cezultverd gietzyzer.
Charcoal hearth cast iron.	Fonte mazée.....	Ghisa al carbone di legna.	Fundición refinada en fuego de añoria.	Herdfrischeisen Holzkohlenherdfrisch-Rohelsen.	Tackjern för hårdfriskning.	Raffineret Raajern..	Houiskolen gietzyzer.
Alloy cast iron.....	Fontes spéciales.....	Legas di ghise (ghise special).	Aleaciones de hierro colado.	Sondergusseisen....	Special tackjern.....	Special Raajern.....	Special gietzyzer.

Species.

Malleable castings.....	Fonte malléable.....	Pezzi fusi (getti) di ghisa malleabile.	Piezas de fundición de hierro maleable.	Schmiedbares Gusseisen or schmiedbarer Guss.	Aduceraut jern.....	Hammerbart Stöbeler, Hammerbart Stöbegods.	Smeedbare gieting.
Steel.....	Acier.....	Acciaio.....	Acero.....	Stahl.....	Stål.....	Staal.....	Staal.

Variety A.

Called steel because cast initially into a malleable mass: 1. Soft or low carbon steel, or ingot iron. 2. Half hard and hard, or medium, and high carbon steel, or ingot steel.	Acier doux, acier extra doux, fer fondu. Acier fondu, acier mi-dur, acier dur.	Lingotto di ferro omogeneo acciaio dolce). Lingotto d'acciaio, duré, semi-duré.	Hierro fundido..... Acero fundido.....	Flusseisen ¹ Flussstahl ¹	Gütemetall..... Haardstaal.....	Staal Biddstaal..... Haardstaal.....	Smeelyzer Vloelyzer. Vloelstaal.
---	---	--	---	--	------------------------------------	---	-------------------------------------

Subvarieties.

Bessemer steel.....	Acier Bessemer.....	Acciaio Bessemer.....	Acero Bessemer.....	Bessemer-Flusseisen, Bessemer Flussstahl, Fluss-eisen, Flammen-eisen, Flammen-eisen, Flammen-eisen, Tiegelflussstahl, Gussstahl.	Bessemerstaal..... Martinstaal.....	Bessemer staal..... Martinstaal.....	Bessemer staal. Frischaal, Siemens-Martinstaal.
Open-hearth steel.....	Acier Martin Siemens, acier sur sole.	Acciaio Martin.....	Acero de Solera.....	Flammen-eisen, Flammen-eisen, Tiegelflussstahl, Gussstahl.	Martinstaal.....	Martinstaal.....	Frischaal, Siemens-Martinstaal.
Crucible steel.....	Acier au creuset.	Acciaio al crogiuolo.....	Acero de crisoles.....	Flammen-eisen, Tiegelflussstahl, Gussstahl.	Degetaal or Degel-fuutsaal. Gütsaal.	Digestaal.....	Kroerzenstaal.
Cast steel.....	Moules d'acier.....	Pezzi di acciaio colato.	Acero fundido..... Piezas de acero colado.	Flussware.....	Stål.....	Staal.....	Gietstaal.
Steel castings.....					Stål.....	Staal.....	Vormgietstaal.

Variety B.

Weld steel, or wrought steel, called steel because it is capable of hardening greatly by sudden cooling.	Fer fort ou fer dur.....	Acciaio saldato, Acciaio fucinato.	Acero Soldado.....	Schweisstahl or Schweisseisen. ¹	Wald stål, rarely used, no equivalent.	Svejsstaal.....	Welder Weldstaal.
--	--------------------------	------------------------------------	--------------------	---	--	-----------------	-------------------

¹ According to Weddington cast metal having a tenacity greater than 50 kg/mm² should be called Flussstahl, while with a smaller tenacity it should be called Flusseisen. Weld metal with a tenacity exceeding 42 kg/mm² should be called Schweissestahl and with a less tenacity, Schweisseisen.

TABLE 9.—Standard Terminology for the Ferrous Materials in Principal European Languages—Continued.

English.	Names.											
	French.	Italian.	Spanish.	German.	Swedish.	Danish.	Dutch.					
Blister steel, also called cemented and converted steel.	Acler poule, acier cimenté, acier de cimentation.	Acciaio cementato, Acciaio al crogiuolo, Acciaio a carburazione esterna cementato.	Acero cementado	Zemenstahl	Blåstål, Brännstål, Cementstål.	Blærestaal or Cementstaal.	Cementstaal.					
								Acler raffiné une fois	Acciaio damascato (acciaio saldato).	Schwessstahl	Svebestaal	Welsaal.
								Acler puddlé	Acciaio puddellato	Puddelstahl	Puddelstål	Puddelstaal
Shear steel												
Puddled steel												
Subvarieties.												
Alloy steels	Alliages à base de fer, aciers spéciaux.	Leghe di acciai (acciai speciali).	Aleaciones de Acero.	Sonderstahl	Special stål	Special staal	Specialstaal.					
								Variety C.				
Wrought iron (or weld iron, or, in Great Britain, malleable iron).	Fer soudé	Ferro forcinato, Ferro saldato.	Hierro forjado, Hierro soldado.	Schmiedeeisen and Stabeisen.	Smidestjern Lancashire jern.	Svebsjern	Welyzer.					
								Species.				
Puddled iron.	Fer puddlé	Ferro puddellato	Hierro puddelado	Puddel-eisen	Puddeljern	Svebsjern	Puddelzyer.					
								Varieties.				
Bloomary or knobbed iron.	Fer au bois (obtenu au Bas-Foyer).			Herdfritscheisen	Puddeljern, Lancashire Franche-Comté or Walloon jern.	Svebsjern	Puddelzyer.					
								Puddled iron (or weld iron, or, in Great Britain, malleable iron).				
Puddled iron (or weld iron, or, in Great Britain, malleable iron).												
Bloomary or knobbed iron.												

X. IRON AND STEEL SPECIFICATIONS. (S. A. E.)**1. CLASSIFICATION.**

A numeral index system is used for the specifications given below, which makes it possible to use specification numerals on shop drawings and blue prints that are partially descriptive of the quality of material covered by such numbers. The first figure indicates the class to which the steel belongs. Thus, "1" indicates a carbon steel, "2" a nickel steel, and "3" a nickel-chromium steel. In the case of the alloy steels the second figure generally indicates the approximate percentage of the predominant alloying element. Usually the last two or three figures indicate the average carbon content in "points," or hundredths of 1 per cent. Thus, "2340" indicates a nickel steel of approximately 3 per cent nickel (3.25 to 3.75) and 0.40 per cent carbon (0.35 to 0.45) and 71360 indicates a tungsten steel of about 13 per cent tungsten (12 to 15) and 0.60 per cent carbon (0.50 to 0.70). The basic numerals for the various qualities of steels specified are:

Carbon steels.....	1	Chromium steels.....	5
Nickel steels.....	2	Chromium-vanadium steels.....	6
Nickel-chromium steels.....	3	Tungsten steels.....	7
Molybdenum steels.....	¹ 4	Silico-manganese steels.....	8

2. CHEMICAL COMPOSITIONS.**CARBON STEELS.**

S. A. E. steel No.	Carbon, range.	Manganese, range.	Phosphorus, maximum.	Sulphur, maximum.
1010.....	0.05-0.15	0.30-0.60	0.045	0.05
1015.....	.10-.20	.30-.60	.045	.05
1020.....	.15-.25	.30-.60	.045	.05
1025.....	.20-.30	.50-.80	.045	.05
1030.....	.25-.35	.50-.80	.045	.05
1035.....	.30-.40	.50-.80	.045	.05
1040.....	.35-.45	.50-.80	.045	.05
1045.....	.40-.50	.50-.80	.045	.05
1046.....	.40-.50	.30-.50	.045	.05
1050.....	.45-.55	.50-.80	.045	.05
1095.....	.90-1.05	.25-.50	.040	.05

SCREW STOCKS.

1112.....	0.08-0.16	0.60-0.80	0.09-0.13	0.075-0.15
1120.....	.15-.25	.60-.90	.06	.075-.15

STEEL CASTINGS.

1235.....	As required by physical properties.		0.05	0.05
-----------	-------------------------------------	--	------	------

¹ This numeral has been agreed upon as the index to the molybdenum group, but no specific compositions have as yet been approved.

2. CHEMICAL COMPOSITIONS—Continued.

NICKEL STEELS.

S. A. E. steel No.	Carbon, range.	Manganese, range.	Phosphorus, maximum.	Sulphur, maximum.	Nickel range.
2315.....	0.10-0.20	0.30-0.60	0.04	0.045	3.25-3.75
2320.....	.15-.25	.50-.80	.04	.045	3.25-3.75
2330.....	.25-.35	.50-.80	.04	.045	3.25-3.75
2335.....	.30-.40	.50-.80	.04	.045	3.25-3.75
2340.....	.35-.45	.50-.80	.04	.045	3.25-3.75
2345.....	.40-.50	.50-.80	.04	.045	3.25-3.75
2350.....	.45-.55	.50-.80	.04	.045	3.25-3.75
2512.....	Max. .17	.30-.60	.04	.045	4.50-5.25

NICKEL-CHROMIUM STEEL.

S. A. E. steel No.	Carbon, range.	Manganese, range.	Phosphorus, maximum.	Sulphur, maximum.	Nickel, range.	Chromium, range.
3115.....	0.10-0.20	0.30-0.60	0.04	0.040	1.00-1.50	0.45-0.75
3120.....	.15-.25	.30-.60	.04	.045	1.00-1.50	.45-.75
3125.....	.20-.30	.50-.80	.04	.045	1.00-1.50	.45-.75
3130.....	.25-.35	.50-.80	.04	.045	1.00-1.50	.45-.75
3135.....	.30-.40	.50-.80	.04	.045	1.00-1.50	.45-.75
3140.....	.35-.45	.50-.80	.04	.045	1.00-1.50	.45-.75
3215.....	.10-.20	.30-.60	.04	.040	1.50-2.00	.90-1.25
3220.....	.15-.25	.30-.60	.04	.040	1.50-2.00	.90-1.25
3230.....	.25-.35	.30-.60	.04	.040	1.50-2.00	.90-1.25
3240.....	.35-.45	.30-.60	.04	.040	1.50-2.00	.90-1.25
3245.....	.40-.50	.30-.60	.04	.040	1.50-2.00	.90-1.25
3250.....	.45-.55	.30-.60	.04	.040	1.50-2.00	.90-1.25
3312.....	Max. .17	.30-.60	.04	.040	3.25-3.75	1.25-1.75
3325.....	.20-.30	.30-.60	.04	.040	3.25-3.75	1.25-1.75
3335.....	.30-.40	.30-.60	.04	.040	3.25-3.75	1.25-1.75
3340.....	.35-.45	.30-.60	.04	.040	3.25-3.75	1.25-1.75
3415.....	.10-.20	.45-.75	.04	.040	2.75-3.25	.60-.95
3435.....	.30-.40	.45-.75	.04	.040	2.75-3.25	.60-.95
3450.....	.45-.55	.45-.75	.04	.040	2.75-3.25	.60-.95

CHROMIUM STEEL.

S. A. E. steel No.	Carbon, range.	Manganese, range.	Phosphorus, maximum.	Sulphur, maximum.	Chromium, range.
5120.....	0.15-0.25	0.30-0.60	0.04	0.045	0.60-0.90
5140.....	.35-.45	.50-.80	.04	.045	.80-1.10
5150.....	.45-.55	.50-.80	.04	.045	.80-1.10
52100.....	.95-1.10	.20-.50	.03	.030	1.20-1.50

CHROMIUM-VANADIUM STEELS.

S. A. E. steel No.	Carbon, range.	Manganese, range.	Phosphorus, maximum.	Sulphur, maximum.	Chromium, range.	Vanadium.	
						Minimum.	Desired.
6120.....	0.15-0.25	0.50-0.80	0.04	0.04	0.80-1.10	0.15	0.18
6125.....	.20-.30	.50-.80	.04	.04	.80-1.10	.15	.18
6130.....	.25-.35	.50-.80	.04	.04	.80-1.10	.15	.18
6135.....	.30-.40	.50-.80	.04	.04	.80-1.10	.15	.18
6140.....	.35-.45	.50-.80	.04	.04	.80-1.10	.15	.18
6145.....	.40-.50	.50-.80	.04	.04	.80-1.10	.15	.18
6150.....	.45-.55	.50-.80	.04	.04	.80-1.10	.15	.18
6195.....	.90-1.05	.20-.45	.03	.03	.80-1.10	.15	.18

2. CHEMICAL COMPOSITIONS—Continued.

TUNGSTEN STEELS.

S. A. E. steel No.	Carbon, range.	Manganese, maximum.	Phosphorus, maximum.	Sulphur, maximum.	Chromium, range.	Tungsten, range.
71360.....	0.50-0.70	0.30	0.035	0.035	3.00-4.00	12.00-15.00
71660.....	.50-.70	.30	.035	.035	3.00-4.00	15.00-18.00
7260.....	.50-.70	.30	.035	.035	.50-1.00	1.50-2.00

SILICO-MANGANESE STEELS.

S. A. E. steel No.	Carbon, range.	Manganese, range.	Phosphorus, maximum.	Sulphur, maximum.	Silicon, range.
9250.....	0.45-0.55	0.60-0.90	0.045	0.045	1.80-2.20
9260.....	.55-.65	.60-.90	.045	.045	1.80-2.20

3. HEAT TREATMENT.

The charts below (see figs. 17 to 25) are intended as a guide to the proper heat treatment and to the physical properties that may be expected of a standard 0.505 by 2 in. (12.82 by 50.8 mm) test specimen machined from rolled bars up to 1½-in. (38.10 mm) diameter or square.

Brinell and scleroscope hardnesses are taken at a distance from the center equal to one-half the radius and are not to be compared with surface readings on heat-treated bars. For bars over 1½ in. (38.10 mm) in diameter or square these charts do not apply.

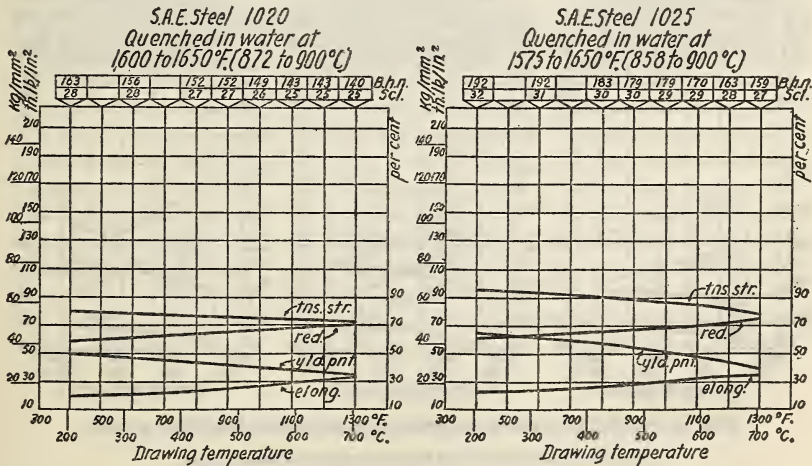


FIG. 17.—Effect of drawing temperature on the tensile properties of steel.

S. A. E. Standard Iron and Steel Specifications, March, 1922.

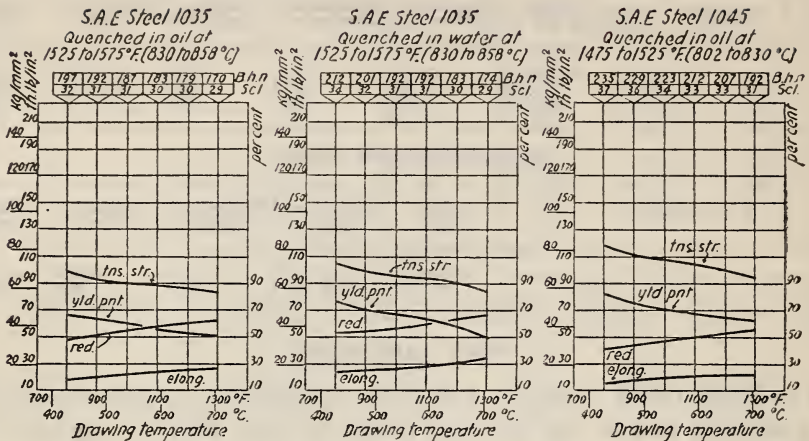


FIG. 18.—Effect of drawing temperature on the tensile properties of steel.

S. A. E. Standard Iron and Steel Specifications, March, 1922.



FIG. 19.—Effect of drawing temperature on the tensile properties of steel.

S. A. E. Standard Iron and Steel Specifications, March, 1922.

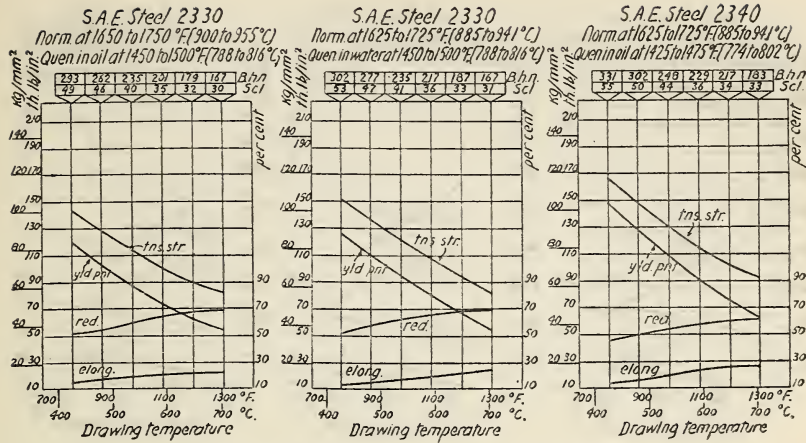


FIG. 20.—Effect of drawing temperature on the tensile properties of steel.

S. A. E. Standard Iron and Steel Specifications, March, 1922.

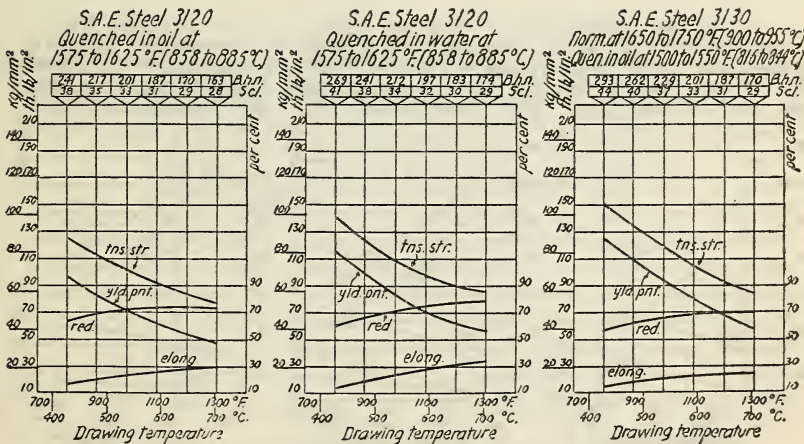


FIG. 21.—Effect of drawing temperature on the tensile properties of steel.

S. A. E. Standard Iron and Steel Specifications, March, 1922.

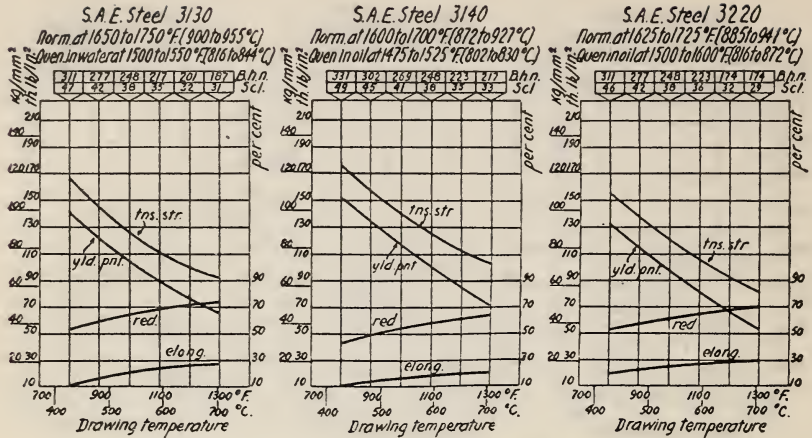


FIG. 22.—Effect of drawing temperature on the tensile properties of steel.

S. A. E. Standard Iron and Steel Specifications, March, 1922.

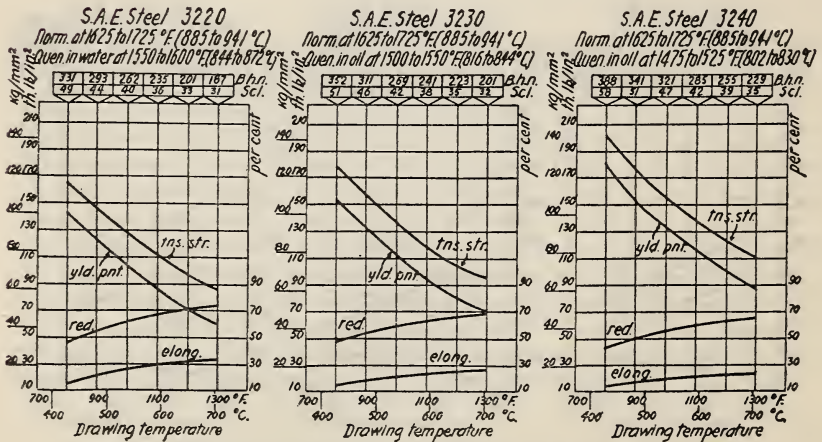


FIG. 23.—Effect of drawing temperature on the tensile properties of steel.

S. A. E. Standard Iron and Steel Specifications, March, 1922.

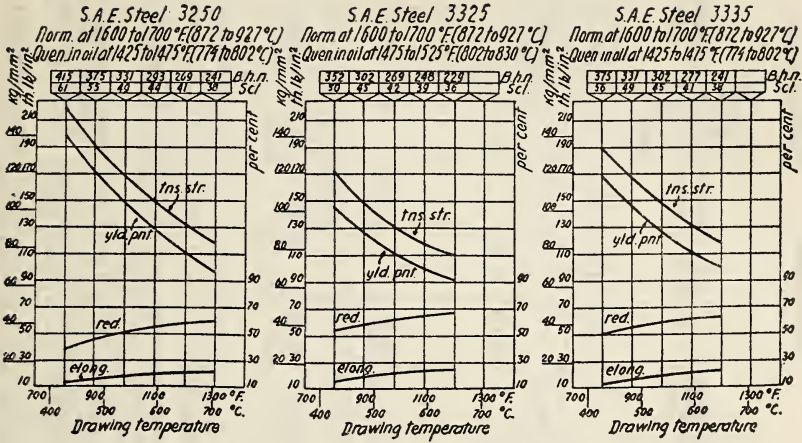


FIG. 24.—Effect of drawing temperature on the tensile properties of steel.

S. A. E. Standard Iron and Steel Specifications, March, 1922.

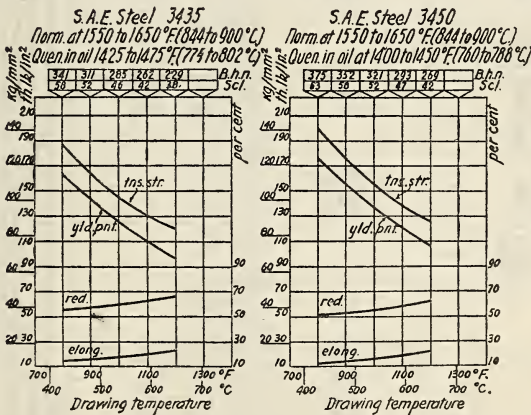


FIG. 25.—Effect of drawing temperature on the tensile properties of steel.

S. A. E. Standard Iron and Steel Specifications, March, 1922.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific grav.	Tensile properties.						Hardness number.			Thermal properties.			Reference.		
			Metric kg/mm ²		English lb./in. ²		Elongation in 50.8 mm or 2 inches.	Reduction of area.	Brinell.	Scleroscope.	Melting point.	Linear coefficient of expansion × 10 ⁶ (per 1°C.).	Casting shrinkage.				
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.								Yield point.		Tensile strength.	
Iron—Continued. Cast iron (gray) ¹ — C, 3.0; Si, 1.3–2.0; Mn, 0.6–0.9; S, max. 0.1; P, max. 0.2. ²	1	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
	2	7.2															
Cast iron (gray), ³ C, 2.5–4.0		7.03–7.13	(?)	8.4–24.6	17.5–26.8	Indeterminate.	Indeterminate.	25,000–38,000	Negligible.	100–150	24–40		°C.		mm/m	in./ft.	(167)
Cast iron (white), ⁴ C, 2.5–4.0		7.58–7.73		28.1–35.1	28.1–35.1	28.1–35.1	28.1–35.1	40,000–50,000		90–200			81,220 (2,228 F.)	10.6 (†)			(100)
Semisteel— C (total), 3.50; Mn, 0.70; P, 0.10; S, 0.16.		7.73		7.0–26.7	7.0–26.7	7.0–26.7	7.0–26.7	9,950–38,000		105–207			81,135 (2,075 F.)				(100)

¹ Modulus of elasticity, in tension or compression, 7,500–10,500 kg/mm² (10,600,000–14,920,000 lb./in.²). Landolt Börnstein Physical Tables (1912) give for Poisson's ratio of gray cast iron 0.25. Modulus of elasticity in shear, 2,900–4,000 kg/mm² (4,125,000–5,600,000 lb./in.²). Compressive strength, specimen 25.4 mm (1 in.) diameter, 76.2 mm (3 in.) long, 56.3–84.4 kg/mm² (90,000–120,000 lb./in.²). A. S. T. M. specification A 48–18, arbitration bar 31.8 mm (1 1/4 in.) diameter, on 304.8 mm (12 in.) span; minimum central load at rupture, 1,430–1,500 kg (2,500–3,300 lb.); minimum central deflection at rupture, 2.5 mm (0.1 in.); tensile strength, 12.7–16.9 kg/mm² (18,000–24,000 lb./in.²).

² A. S. T. M. specification, A 48–18; S, max. 0.10; except S, max. 0.12, for heavy castings.

³ Compressive strength from 24.6 (soft) to 140.6 kg/mm² (hard, close-grained), or 35,000–200,000 lb./in.². For machinery grades of good quality compressive strength from 63.3–105.5 kg/mm² (90,000–150,000 lb./in.²). Transverse tests preferred for testing cast iron. Modulus of rupture for good cast iron, 31.6 kg/mm² (45,000 lb./in.²). Modulus of elasticity in tension, compression, or cross bending, 8,430–10,550 kg/mm² (12,000,000–15,000,000 lb./in.²); for strong cast irons, up to 14,060 kg/mm² (20,000,000 lb./in.²). Shearing strength: Soft (Brinell hardness 92), 14.4 kg/mm² (20,500 lb./in.²); fine-grained (Brinell hardness 150), 23.7 kg/mm² (33,700 lb./in.²); hard, fine-grained (Brinell hardness 217), 28.0 kg/mm² (39,000 lb./in.²). Modulus of elasticity in shear, 4,500–5,770 kg/mm² (6,400,000–8,200,000 lb./in.²); modulus of rupture in torsion, about 24.6 kg/mm² (35,000 lb./in.²).

⁴ If in cooling the carbon is largely precipitated, more or less uniformly in the form of graphite flakes, the iron is soft, presents dull-gray fracture, and is called gray cast iron. When the carbon is retained in combined form (Fe₃C), the cast iron is hard and brittle, it has silvery white fracture, and is called white cast iron. (Johnson's Materials of Construction, p. 697, 1918.)

⁵ Smithsonian Physical Tables, 1920.

TABLE 10.—Properties of Semisteel—Experimental Results.¹

[Test results at Bureau of Standards on 155 mm shell, January, 1919. Microstructure: Matrix resembling pearlitic steel, embedded in which are flakes of graphite. Composition: Combined C, 0.60-0.76; graphitic C, 2.84-2.94; Mn, 0.88; P, 0.42-0.43; S, 0.077-0.088; Si, 1.22-1.23.]

Metal.	Tensile test.				Compressive test.				Brinell hardness.
	Proportional limit.		Tensile strength.		Proportional limit.		Compressive strength.		
	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	
Semisteel:									
Graphitic C, 2.85; combined C, 0.76.....	7.9	11,200	19.8	28,200	24.3	34,500	72.6	103,300	176
Graphitic C, 2.92; combined C, 0.60.....	4.2	6,000	14.9	21,200	18.3	26,000	61.4	87,300	170

¹ Semisteel—Gray iron to which steel has been added while in the molten condition. It may also be produced by other methods. NONG.—Tension specimens 12.7 mm (0.5 in.) diameter, 40.8 mm (1.6 in.) gauge length; elongation and reduction area negligible. Compression specimens 20.3 mm (0.8 in.) diameter, 61.0 mm (2.4 in.) long; failure occurred in shear. Modulus of elasticity in tension, 9,560 kg/mm², or 13,660,000 lb./in.²

¹ Not well defined.
² Cent. 6.1 technical Engineers Pocketbook, p. 559; 1916.
³ Expansion and contraction of solids.
⁴ Expansion and contraction of solids.
⁵ Expansion and contraction of solids.
⁶ Expansion and contraction of solids.
⁷ Expansion and contraction of solids.
⁸ Expansion and contraction of solids.
⁹ Expansion and contraction of solids.
¹⁰ Expansion and contraction of solids.
¹¹ Expansion and contraction of solids.
¹² Expansion and contraction of solids.
¹³ Expansion and contraction of solids.
¹⁴ Expansion and contraction of solids.
¹⁵ Expansion and contraction of solids.
¹⁶ Expansion and contraction of solids.
¹⁷ Expansion and contraction of solids.
¹⁸ Expansion and contraction of solids.
¹⁹ Expansion and contraction of solids.
²⁰ Expansion and contraction of solids.
²¹ Expansion and contraction of solids.
²² Expansion and contraction of solids.
²³ Expansion and contraction of solids.
²⁴ Expansion and contraction of solids.
²⁵ Expansion and contraction of solids.
²⁶ Expansion and contraction of solids.
²⁷ Expansion and contraction of solids.
²⁸ Expansion and contraction of solids.
²⁹ Expansion and contraction of solids.
³⁰ Expansion and contraction of solids.
³¹ Expansion and contraction of solids.
³² Expansion and contraction of solids.
³³ Expansion and contraction of solids.
³⁴ Expansion and contraction of solids.
³⁵ Expansion and contraction of solids.
³⁶ Expansion and contraction of solids.
³⁷ Expansion and contraction of solids.
³⁸ Expansion and contraction of solids.
³⁹ Expansion and contraction of solids.
⁴⁰ Expansion and contraction of solids.
⁴¹ Expansion and contraction of solids.
⁴² Expansion and contraction of solids.
⁴³ Expansion and contraction of solids.
⁴⁴ Expansion and contraction of solids.
⁴⁵ Expansion and contraction of solids.
⁴⁶ Expansion and contraction of solids.
⁴⁷ Expansion and contraction of solids.
⁴⁸ Expansion and contraction of solids.
⁴⁹ Expansion and contraction of solids.
⁵⁰ Expansion and contraction of solids.
⁵¹ Expansion and contraction of solids.
⁵² Expansion and contraction of solids.
⁵³ Expansion and contraction of solids.
⁵⁴ Expansion and contraction of solids.
⁵⁵ Expansion and contraction of solids.
⁵⁶ Expansion and contraction of solids.
⁵⁷ Expansion and contraction of solids.
⁵⁸ Expansion and contraction of solids.
⁵⁹ Expansion and contraction of solids.
⁶⁰ Expansion and contraction of solids.
⁶¹ Expansion and contraction of solids.
⁶² Expansion and contraction of solids.
⁶³ Expansion and contraction of solids.
⁶⁴ Expansion and contraction of solids.
⁶⁵ Expansion and contraction of solids.
⁶⁶ Expansion and contraction of solids.
⁶⁷ Expansion and contraction of solids.
⁶⁸ Expansion and contraction of solids.
⁶⁹ Expansion and contraction of solids.
⁷⁰ Expansion and contraction of solids.
⁷¹ Expansion and contraction of solids.
⁷² Expansion and contraction of solids.
⁷³ Expansion and contraction of solids.
⁷⁴ Expansion and contraction of solids.
⁷⁵ Expansion and contraction of solids.
⁷⁶ Expansion and contraction of solids.
⁷⁷ Expansion and contraction of solids.
⁷⁸ Expansion and contraction of solids.
⁷⁹ Expansion and contraction of solids.
⁸⁰ Expansion and contraction of solids.
⁸¹ Expansion and contraction of solids.
⁸² Expansion and contraction of solids.
⁸³ Expansion and contraction of solids.
⁸⁴ Expansion and contraction of solids.
⁸⁵ Expansion and contraction of solids.
⁸⁶ Expansion and contraction of solids.
⁸⁷ Expansion and contraction of solids.
⁸⁸ Expansion and contraction of solids.
⁸⁹ Expansion and contraction of solids.
⁹⁰ Expansion and contraction of solids.
⁹¹ Expansion and contraction of solids.
⁹² Expansion and contraction of solids.
⁹³ Expansion and contraction of solids.
⁹⁴ Expansion and contraction of solids.
⁹⁵ Expansion and contraction of solids.
⁹⁶ Expansion and contraction of solids.
⁹⁷ Expansion and contraction of solids.
⁹⁸ Expansion and contraction of solids.
⁹⁹ Expansion and contraction of solids.
¹⁰⁰ Expansion and contraction of solids.

For engine bolt (grade B), area less than $1\frac{1}{4}$ in. ² (806 mm ²).	0.6 tensile strength.	34.4-37.3	49,000-53,000	18 25.0	40.0	(20)
For engine bolt (grade B), area over $1\frac{1}{4}$ in. ² (806 mm ²).	0.55 tensile str. ¹⁵	33.0-37.3	47,000-53,000	18 25.0	40.0	(20)
Extra refined bars (grade C), area less than $1\frac{1}{4}$ in. ² (806 mm ²).	0.6 tensile strength.	33.7-38.0	48,000-54,000	18 25.0	37.0	(20)
Extra refined bars (grade C), area over $1\frac{1}{4}$ in. ² (806 mm ²).	0.55 tensile str. ¹⁵	33.7-38.0	48,000-54,000	18 25.0	37.0	(20)

1 Transverse tests: Specimens 14 in. (356 mm) in length and 1 in. (25.4 mm) wide; span 12 in. (305 mm):

Thickness of specimen.		Minimum load applied at center.		Minimum deflection at center.	
mm	in.	lb.	kg	mm	in.
12.7	1/2	900	408	31.7	1.25
15.9	5/8	1,400	635	25.4	1.00
19.1	3/4	2,000	907	19.1	.75

2 Modulus of elasticity in tension and compression 17,600 kg./mm² (25,000,000 lb./in.²).

3 H. A. Schwartz, Proc. Am. Soc. Test. Mat., 2, p. 247; 1919.

4 Am. Soc. Test. Mat. Specification A47-59.

5 4 in. (101.6 mm) through .8° around a diameter of one thickness.

6 Shear elongation will be measured in 8 in. (203.2 mm) diameter or thickness.

7 Elongation will be measured in 8 in. (203.2 mm) diameter or thickness; flats $\frac{1}{4}$ in. (6.35 mm) and less thickness will be measured on a length equal to 25 times the thickness. On all other materials less than $\frac{3}{4}$ in. (19.1 mm) diameter or thickness, all other material to 180° around a diameter of one thickness. Both grades A and B to be bent to same requirements as cold bends after being heated to 92° C. (170° F.) and quenched in water; the temperature of which should be about 27° C. (80° F.)

8 Flats $\frac{3}{4}$ in. (19.1 mm) and less shall be bent cold around a diameter of two thicknesses; all other material to 180° around a diameter of one thickness. Both grades A and B to be bent to same requirements as cold bends after being heated to 92° C. (170° F.) and quenched in water; the temperature of which should be about 27° C. (80° F.)

9 Compressive strength (specimen 25.4 mm or 1 in. diameter, 76.2 mm or 3 in. long) approximately equal to tensile yield point. Modulus of elasticity in tension and compression, 17,600 kg./mm² (25,000,000 lb./in.²); modulus of elasticity in shear, 7,030 kg./mm² (10,000,000 lb./in.²); shearing proportional limit, 21.1 kg./mm² (30,000 lb./in.²); shearing strength, 35.2 kg./mm² (50,000 lb./in.²).

10 Kent's, Mechanical Engineers Pocketbook, p. 559; 1916.

11 Smithsonian Physical Tables, 7th edition; 1920.

12 Pipe less than 2 in. (50.8 mm) in diameter shall withstand being bent cold through 90° around a cylindrical mandrel, the diameter of which is 15 times the diameter of the pipe, without developing cracks and without opening the weld.

13 In 8 in. (203.2 mm).

14 Cold-bend tests: Grade A.—Test specimen shall withstand being bent through 180° flat on itself in both directions without fracture on the outside of the bent portion. Grade B.—Test specimen shall withstand being bent through 180° around a pin, the diameter of which is equal to the diameter of the specimen, without fracture on the outside of the bent portion. Grade C.—Bars having cross-sectional area under 4 in.² (2,580 mm²) shall withstand being bent through 180° around a pin, the diameter of which is equal to the thickness of bar, without fracture on the outside of the bent portion. Hot bend tests: Grades B and C.—The test specimen when heated to a temperature between 1,700 and 1,800° F. (938 and 983° C.) shall withstand being bent through 180° flat on itself without fracture on the outside of the bent portion.

15 0.5 tensile strength for an area over 4 in.² (2,580 mm²).

C, 0.20; Mn, 0.50; S, 0.06; P, 0.045.	Carbonizing steel, quenched at 1,625° F. (885° C.) and drawn at 900° F. (482° C.).	35.9	49.2	51,000	70,000	34.0	70	(49)
		0.5 tensile strength.	38.7-45.7	0.5 tensile strength.	55,000-65,000	22		
Mild carbon steel, Welding—C, 0 to 0.12; Si, max. 0.25; Mn, 0.30; P, max. 0.04; S, max. 0.04; Cu, Ni, Cr, not more than a trace.	Rolled or forged.	0.5 tensile strength.	38.7-45.7	0.5 tensile strength.	55,000-65,000	22		(203)
		0.5 tensile strength.	38.7-45.7	0.5 tensile strength.	55,000-65,000	22		(23)

¹⁶ The test specimen shall bend cold through 90° without fracture on the outside of the bent portion around a pin, the diameter of which is equal to—for class A, 1½ times the thickness, and for class B, 3 times the thickness.
¹⁷ Shearing strength, 28.1 kg/mm² (40,000 lb./in.²).
¹⁸ Shall be bent cold through 180° flat on itself without fracture.
¹⁹ The minimum elongation of test specimen shall be 35 per cent for type 1 specimen and 30 per cent for types 2 and 3. The elongation shall be measured in accordance with the following table:

Types 2 and 3 from flat bars.		Type 3 from round, square, and hexagon bars.	
Nominal thickness.	Length in which measured.	Nominal thickness.	Length in which measured.
½ in. (3.17 mm) or less.	2	Up to ½ in. (6.35 mm), inclusive.	2
Over ½ in. (3.17 mm) to ¾ in. (4.76 mm), inclusive.	4	Over ½ in. (6.35 mm) to ¾ in. (12.7 mm), inclusive.	4
Over ¾ in. (4.76 mm) to 1 in. (6.35 mm), inclusive.	6	Over ¾ in. (12.7 mm) to 1 in. (19.05 mm), inclusive.	6
Over 1 in. (6.35 mm).	8	Over 1 in. (19.05 mm) to 1½ in. (38.1 mm), inclusive.	8
		Over 1½ in. (38.1 mm), type 1 test specimen.	2

²⁰ In 8 in. (203.2 mm).
²¹ According to W. Dalby, Engineering, April 6, 1917, the correlation between the content of carbon and the strength of mild steel after annealing to allow the perlitic form, may be represented by formula: $f = 35,800 + 124,370 C \text{ lb./in.}^2$ or $25,157 + 80.4 C \text{ kg/mm}^2$, where C is carbon content in per cent. W. Webster, Trans. Amer. Inst. Mech. Eng., 214 and 224, 1893-94, gives for the tensile strength of ¾ in. (9.52 mm) plates of basic Bessemer steel the following correlation: $f = 34,750 + 80,000 C + 50,000 S + P \times 60,000$ to 150,000, corresponding to carbon content from 0.09 to 0.17 per cent lb./in.² or 24.4 + 56.3 C + 35.2 S + P X (63.3 to 195.5, corresponding to carbon content from 0.09 to 0.17 per cent) kg/mm². According to H. H. Campbell, Kent's Mechanical Engineer's Pocketbook, p. 477: 1916; the tensile strength of: Acid steel, 40,000 + 68,000 C + 100,000 P + 80,000 CX Mn lb./in.² or 28.1 + 47.8 C + 70.3 P + 56.3 CX Mn kg/mm²; basic steel, 38,800 + 65,000 C + 100,000 P + 9,000 Mn + 40,000 CX Mn lb./in.² or 27.3 + 45.7 C + 70.3 P + 6.3 Mn + 28.1 CX Mn kg/mm². (See also p. 73, Bureau of Standards results.)
²² Suitable for electrical or autogenous welding of steel castings, forgings, etc.

- ²² Modulus of rupture in torsion: Cold rolled C, 0.087-8.5 kg/mm² (69,000 lb./in.²); cold rolled C, 0.097-76.6 kg/mm² (71,000 lb./in.²); cold rolled C, 0.375-58.3 kg/mm² (83,000 lb./in.²); machinery (open hearth) C, 0.084-11.5 kg/mm² (59,000 lb./in.²). According to Upton, Johnson's "Materials of construction," p. 667, 1918) shearing strength is equal to $\frac{1}{4}$ modulus of rupture in torsion.
- ²³ Smithsonian Physical Tables, 7th edition, 1920. The following values refer to steel in general: Coefficient of expansion for cast steel, 13.22×10^{-6} ; coefficient of expansion for annealed steel, 10.95×10^{-6} .
- ²⁷ Kent's Mechanical Engineer's Pocketbook, p. 559, 1916.
- ²⁸ Shall bend cold through 186° flat on itself without cracking on the outside of the bent portion. Heated to not less than 650° C. (1,200° F.) and quenched in water between 7 and 35° C. (80-95° F.) shall bend through 186° flat on itself without cracking on the outside of the bent portion.
- ²⁹ Elongation in 8 in. (203.2 mm) minimum per cent 1,500,000-± tensile strength in lb./in.² or 1,055-± tensile strength in kg/mm². Need not exceed 30 per cent.
- ³⁰ Average value for the modulus of elasticity, 29,750 kg/mm² (29,500,000 lb./in.²).
- ³¹ The modulus of elasticity in shear, 8,190 kg/mm² (11,700,000 lb./in.²). Poisson's ratio from 0.268 to 0.310 (Love, The Mathematical Theory of Elasticity, 1906).
- ³² Shall bend cold around a pin without cracking on the outside of the bent portion, as follows:

Thickness or diameter of bar.	Plain bars.			Deformed bars.		
	Structural grade.	Intermediate grade.	Hard grade.	Structural grade.	Intermediate grade.	Hard grade.
Under $\frac{3}{4}$ in. (19.1 mm)	180°, $d=t$	180°, $d=2t$	180°, $d=3t$	180°, $d=t$	180°, $d=3t$	180°, $d=4t$
$\frac{3}{4}$ in. or over (19.1 mm)	180°, $d=t$	90°, $d=2t$	90°, $d=3t$	180°, $d=2t$	90°, $d=3t$	90°, $d=t$

d = diameter of pin about which the specimen is bent.
 t = thickness or diameter of the specimen.

- ³³ 1,400,000-± tensile strength in lb./in.² or 984-± tensile strength in kg/mm².
- ³⁴ Elongation in 8 in. (203.2 mm). A deduction of 0.25 per cent shall be made for every $\frac{1}{8}$ in. (0.79 mm) above $\frac{3}{4}$ in. (19.1 mm) and 0.5 per cent for every $\frac{1}{16}$ in. (0.79 mm) below $\frac{1}{4}$ in. (11.1 mm).
- ³⁵ 1,450,000-± tensile strength in lb./in.² or 979-± tensile strength in kg/mm².
- ³⁶ 1,450,000-± tensile strength in lb./in.² or 974-± tensile strength in kg/mm².
- ³⁷ 1,450,000-± tensile strength in lb./in.² or 974-± tensile strength in kg/mm².
- ³⁸ 1,200,000-± tensile strength in lb./in.² or 874-± tensile strength in kg/mm².
- ³⁹ 1,000,000-± tensile strength in lb./in.² or 793-± tensile strength in kg/mm².

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and com- position.	Condition.	Spec- ific grav- ity.	Tensile properties.						Hardness num- ber.				Thermal properties.			Refer- ence.	
			Metric kg/mm ²			English lb./in. ²			Elonga- tion in 50.8 mm or 2 inches.	Reduc- tion of area.	Brinell.	Sclero- scope.	Melting point.	Linear coeff- icient of expan- sion $\times 10^6$ (per 1°C.).	Casting shrink- age.		
			Pro- por- tional limit.	Yield point.	Tensile strength.	Pro- por- tional limit.	Yield point.	Tensile strength.							mm/m		in./ft.
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Steel: ⁴⁰ Min. 0.40-0.70; S, max. 0.05; C ⁴¹ , max. 0.05;	Quenched and tempered forg- ings up to 4 in. (101.6 mm) out- side diameter; or thickness; 2 in. (50.8 mm) max. wall.	38.6	63.3	55,000	90,000	Per cent. 20.5	Per cent. 39.0	(27)
	Quenched and tempered forg- ings 4-7 in. (101.6-177.7 mm), outside diameter or thickness; 3½ in. (88.8 mm) max. wall.	35.1	59.7	50,000	85,000	20.5	39.0	(27)
	Quenched and tempered forg- ings 7-10 in. (177.7-254 mm) outside diame- ter or thick- ness; 5 in. (127 mm) max. wall.	35.1	59.7	50,000	85,000	19.5	37.0	(27)
	Quenched and tempered forg- ings 10-20 in. (254-508 mm) outside diame- ter or thick- ness; 8 in. (203.2 mm) max. wall.	33.7	58.0	48,000	82,500	19.0	36.0	(27)

⁴⁰ Shall bend cold through 180° without cracking on the outside of the bent portion. Around a pin 1 in. (25.4 mm) in diameter for material up to 7 in. thick (177.7 mm); around pin 1½ in. (38.1 mm) in diameter for material 7 to 20 in. thick (177.7 to 508 mm).

⁴¹ Carbon content: 0.25-0.60 for material up to 4 in. thick (101.6 mm); 0.35-0.60 for material 4 to 7 in. thick (101.6-177.7 mm); 0.35-0.65 for material 7 to 10 in. thick (177.7-254 mm); 0.35-0.70 for material 10 to 20 in. thick (254-508 mm).

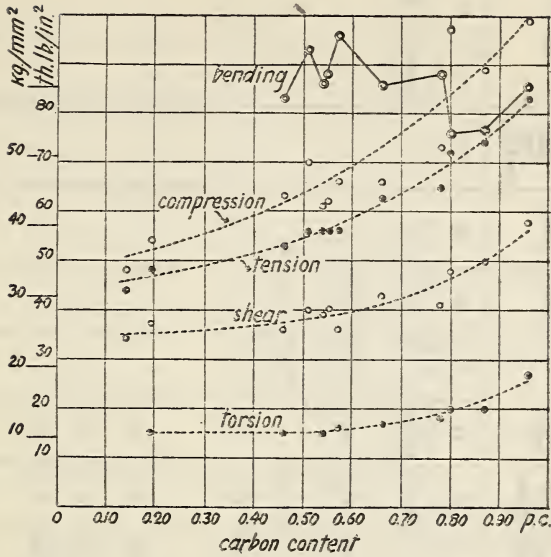


FIG. 26.—Effect of carbon content on the strength of Bessemer steel.

Landolt Börstein Physikalisch-Chemische Tabellen; 1912.

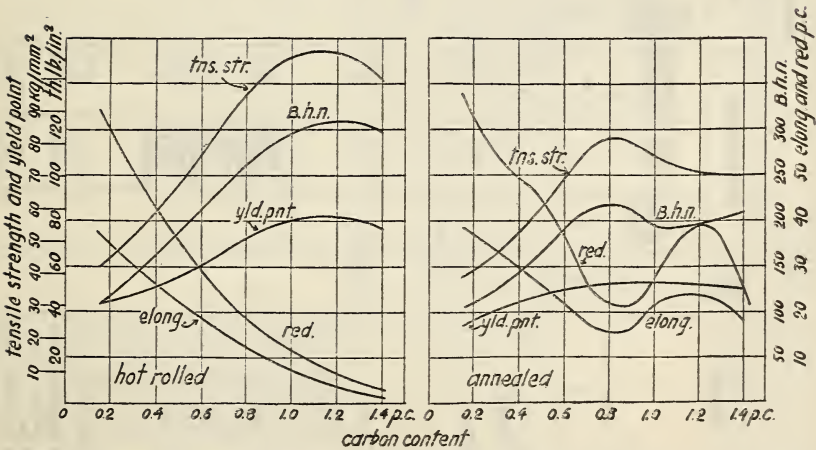


FIG. 27.—Effect of carbon content on the mechanical properties of hot rolled and annealed steel.

Johnson, Materials of Construction; 1918.

Cast, soft.....	0.45	42.2	60,000	22.0	30.0				
	tns. str. min.	tns. str. min.	tns. str. min.	tns. str. min.	tns. str. min.				
P, max. 0.06; S, max. 0.06 (class A). ⁴⁰	0.75	56.2-	80,000-	12.0					(30)
	tns. str.	77.4	110,000						(206)
Cold-rolled or cold-drawn rods and bars 1-1/2 in. (6.35-12.7 mm) diam. or thickness.	min.	52.8	75,000-	16.0					(206)
	tns. str.	70.4	100,000						
Cold-rolled or cold-drawn rods and bars over 1 1/2 in. (12.7-38.1 mm) diam. or thickness.	min.	49.2-	70,000-	18.0					(206)
	tns. str.	63.3	90,000						
P, max. 0.13; S, max. 0.15 (class B).	min.	49.2	70,000	10.0					(206)
	tns. str.								

⁴¹ NOTE.—

Identification (class).	Carbon.		Manganese.		Phosphorus.		Sulphur.	
	Limits.	Desired.	Limits.	Desired.	Not to exceed—	Not to exceed—	Not to exceed—	Not to exceed—
	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.
C 10.....	1.05-0.90	0.95	0.50-0.25	0.35	0.025	0.025	0.025	
C 8.....	.90-.75	.80	.50-.25	.35	.025	.025	.025	
C 6.....	.65-.55	.60	.80-.50	.65	.04	.04	.04	
C 5.....	.55-.45	.50	.80-.50	.65	.04	.04	.04	
C 4.....	.45-.35	.40	.80-.50	.65	.04	.04	.04	
C 3.....	.35-.25	.30	.80-.50	.65	.04	.04	.04	
C 2.....	.25-.15	.20	.80-.50	.65	.04	.04	.04	
C 1.....	.15-.05	.10	Not to exceed .60		.04	.04	.04	

⁴² Shall bend cold about a diameter of 1 in. (25.4 mm) through 120° (class B, D, E, and F) and 90° (class A).
⁴³ Shall bend cold through 180° around a pin, the diameter of which is equal to twice the thickness of the specimen, without cracking on the outside of the bent portion.
⁴⁴ 1,000,000-tensile strength in lb./in.² or 1,123 + tensile strength in kg./mm.², but in no case under 20 per cent.
⁴⁵ Full-size bolts shall bend cold through 45° around a pin, the diameter of which is equal to the diameter of the bolt, without cracking on the outside of the bent portion.
⁴⁶ Shearing strength, 42.2 kg./mm.² (60,000 lb./in.²).
⁴⁷ Shall bend cold around a pin 1 in. (25.4 mm) diameter without cracking on the outside of the bent portion; soft castings through 120° and medium castings through 90°.
⁴⁸ Class A shall be bent cold through 180° to 3 diameters; class B shall be bent cold through 120° to 3 diameters.

C, 0.50-0.70; Mn, max. 0.75; Si, 0.15-0.35; P, max. 0.05; S, max. 0.05.	For tires.....	73.8	105,000	12.0	16.0	(35)
C, 0.60-0.80; Mn, max. 0.75; Si, 0.15-0.35; P, max. 0.05; S, max. 0.05.	do.....	81.0	115,000	10.0	14.0	(35)
C, 0.70-0.85; Mn, max. 0.75; Si, 0.15-0.35; P, max. 0.05; S, max. 0.05.	do.....	88.0	125,000	8.0	12.0	(35)
High carbon ⁵⁰ — C, 0.93; Mn, 0.35; S, 0.16; P, 0.035.	Raw stock..... Quenched at 1,450° F. (788° C.) and drawn at 650° F. (343° C.).	50.8 92.8	72,200 132,000	20.0 11.0	38.0 385	(50) (50)
Extra high carbon ⁵¹ — P, max. 0.04.....	Splice bars.....	70.3	100,000	10.0		(36) (101)

⁵⁰ The test specimens for soft castings shall bend cold through 120° and for medium castings through 90° around a 1 in. (25.4 mm) diameter pin without cracking on the outside. Hard castings shall not be subjected to bend test.

⁵¹ Used in aviation for propeller hubs, wing plates, strut sockets, and hinges.

⁵² Shall bend cold through 180° around a pin 1 in. (25.4 mm) diameter without cracking on the outside of the bent portion.

⁵³ For forgings 8-12 in. (203.2-304.8 mm), elongation 17.0 and reduction 22.0 per cent.

⁵⁴ For forgings 8-12 in. (203.2-304.8 mm), elongation 19.0 and reduction 30.0 per cent; for forgings 12-20 in. (304.8-508 mm), elongation 18.0 and reduction 28.0 per cent.

⁵⁵ Shall bend cold through 90° around a pin, the diameter of which is equal to three times the thickness of the specimen, without cracking on the outside of the bent portion.

⁵⁶ Used in aviation for tail skid shoes, cable wire, and springs.

⁵⁷ Shall bend cold through 60° around a pin, the diameter of which is equal to three times the thickness of the specimen, without cracking on the outside of the bent portion.

⁵⁸ Shearing strength: Swedish, crucible steel, C, 0.12-0.22 kg/mm² (41,500 lb./in.²); C, 0.45-0.45.3 kg/mm² (64,500 lb./in.²); C, 0.71-57.7 kg/mm² (82,500 lb./in.²); C, 0.77-60.0 kg/mm² (85,400 lb./in.²).

TABLE 11.—Tensile Strength of Commercial Steel Music Wire (Hard-Drawn).

[This table represents average values. In sizes finer than shown the values may range from 210.9 to 281.2 kg/mm² (300,000 to 400,000 lb./in.².)]

[Experimental data of American Steel and Wire Co., 1923.]

Diameter.		Tensile strength.		Diameter.		Tensile strength.	
mm	in.	kg/mm ²	lb./in. ²	mm	in.	kg/mm ²	lb./in. ²
0.74	0.029	253.0	360,000	1.14	0.045	224.8	320,000
.84	.033	246.0	350,000	1.25	.049	217.9	310,000
.94	.037	239.0	340,000	1.40	.055	210.8	300,000
1.04	.041	232.0	330,000	1.60	.063	203.9	290,000

TABLE 12.—Properties of High-Tensile Steel Wire.

[British Engineering Standards Association specifications, March, 1919.]

Diameter.		Minimum breaking load.		Number of bends through 180°.	Diameter.		Minimum breaking load.		Number of bends through 180°.
mm	in.	kg	lb.		mm	in.	kg	lb.	
4.06	0.160	1,634	3,603	3	1.42	0.056	250	552	15
3.66	.144	1,324	2,919	3	1.22	.048	184	405	18
3.25	.128	1,111	2,450	3½	1.02	.040	128	282	21
2.95	.116	967	2,131	4	.91	.036	104	229	22
2.64	.104	777	1,713	5	.81	.032	81.2	179	24
2.34	.092	607	1,339	6	.71	.028	62	137	26
2.03	.080	485	1,070	8	.61	.024	46.3	102	28
1.83	.072	393	866	10	.56	.022	38.1	84	30
1.63	.064	327	721	12					

Note.—A torsion test shall be made on a sample cut from each length of wire. It shall stand before breaking the number of turns given by the formula:

Number of turns = 20 turns per length of 100 d , where d is the diameter of the wire.

Bending test shall be made on a sample cut from each length of wire. The sample shall be bent through 90°, first in one direction then in the other (180° reversal over a radius of 5 mm, 0.197 in.).

TABLE 13.—Tensile Requirements of Steel Wire Rope—Continued.

Construction: Number of strands and wires in a strand.	Num-ber of fiber cores.	Diameter.		Approximate weight.		Minimum breaking strength.									
		mm	in.	kg/m	lb./ft.	Cast steel.		Extra strong cast steel.		Plow steel.		High grade plow steel.			
8 by 19.....	1	9.52	3/8	30	.20	3,434	7,570	3,805	8,390	kg	lb.	kg	lb.	kg	lb.
	1	12.70	1/2	52	.35	5,960	13,140	6,532	14,400						
	1	15.88	5/8	83	.56	8,900	19,620	10,070	22,200						
	1	19.06	3/4	119	.80	12,497	27,550	14,370	31,680						
	1	22.24	7/8	161	1.08	16,329	36,000	18,779	41,400						
	1	25.40	1	211	1.42	21,228	46,800	24,249	53,460						

Modulus of elasticity of wire rope: American Steel and Wire Co. gives for new 6-strand rope maximum 12,000,000 lb./in.² (8,430 kg/mm²). According to A. W. Brown, 11,180,000 lb./in.² (7,860 kg/mm²) is a good average for rope after it has been in use long enough for strands to bed into the core. For the old rope he gives 19,000,000 lb./in.² (13,360 kg/mm²). Various authorities give for the modulus of elasticity of wire rope 35 per cent that for steel wire; that is, 10,150,000 lb./in.² (7,130 kg/mm²).

TABLE 14.—Tensile Strength of Steel Wire Rope.¹

[Experimental results of the Bureau of Standards.]

Description and analysis.	Diameter.		Tensile strength.		Tensile strength (net area).	
	mm	in.	kg	lb.	kg/mm ²	lb./in. ²
Plow steel, 6 strands, 19 wires: C, 0.90; S, 0.034; P, 0.024; Mn, 0.48; Si, 0.172.....	50.8	2	137,900	304,000	129.5	184,200
Plow steel, 6 strands, 25 wires: C, 0.77; S, 0.036; P, 0.027; Mn, 0.46; Si, 0.152.....	69.9	2 $\frac{3}{4}$	314,800	694,000	151.2	214,900
Plow steel, 6 strands, 37 wires plus 6 strands, 19 wires: C, 0.58; S, 0.032; P, 0.033; Mn, 0.41; Si, 0.160.....	82.6	3 $\frac{1}{2}$	392,800	866,000	132.2	187,900
Monitor plow steel, 6 strands, 61 wires, plus 6 strands, 19 wires: C, 0.82; S, 0.025; P, 0.019; Mn, 0.23; Si, 0.169.....	82.6	3 $\frac{1}{2}$	425,000	937,000	142.5	202,400

¹ For additional data on strength and other properties of wire rope, see B. S. Tech. Paper No. 121, by Griffith and Bragg, giving results of 275 tensile tests of wire-rope specimens ranging in diameter from $\frac{1}{4}$ in. (6.35 mm) to $3\frac{1}{2}$ in. (82.5 mm) and comprising five of the more common classes used in engineering practice.

Note.—Recommended allowable working load for a wire rope running over a sheave is equal to one-fifth of specified minimum strength.

XI. ALLOY STEELS.¹

1. CARBON STEEL.

Contains maximum C, 1.50 per cent; Mn, 1.00 per cent; Si, 0.35 per cent; P, 0.05 per cent; and S, 0.05 per cent.

2. MANGANESE STEEL.

Contains usually from 10 to 13 per cent of Mn and 1.0 per cent C. Practically nonmagnetic. Has a peculiar hardness, to which it owes its remarkable resistance to abrasion; extremely difficult to machine; has high strength and toughness,² but relatively low elastic limit; has a peculiar property of being toughened and softened by quenching in water, resembling copper in this respect. Principal applications—in castings for crushing and grinding machinery and for railroad crossings.

3. SILICON STEEL.

There are two types of silicon steel, one of which has found application in mechanical engineering. This steel, frequently called silico-manganese steel, has usually the following composition: C, 0.45–0.65; Si, 1.50–2.00; and Mn, 0.50–0.80. It is very brittle in the direction at right angle to rolling.³ Application—used for automobile springs and gears. The other type of silicon steel contains 3–5 per cent silicon; it is low in carbon and manganese; used for electrical transformer sheets on account of high permeability to magnetism; structurally weak and has no constructional value.

¹ (Definition, properties, and uses of alloy steels, as described below, are after G. Norris, Chem. and Met. Eng., 18, p. 739; 1915.)

² In cast or rolled form the steel is glassy brittle, but by reheating to a temperature between 1,000 and 1,100° C. (1,832 to 2,012° F.) and quenching in water the ductility and toughness are wonderfully improved. (Johnson's Materials of Construction, p. 678; 1918.)

³ According to Bullens, silicon manganese steels are quite difficult to heat treat successfully.

4. NICKEL STEEL.

Of all nickel steels by far the most important is low and medium carbon steel with 3-4 per cent Ni (called usually 3½ per cent nickel steel). The presence of manganese in that steel is very essential, and should range from 0.50 to 0.80 per cent. It is a good, all-round engineering steel, with considerably higher elastic limit and tensile strength than corresponding carbon steel and with the same degree of ductility.⁴ Low carbon (0.10-0.20) nickel steel is used extensively for case hardening parts. Nickel steel with carbon 0.20-0.35 is much used for bridge construction. Nickel steel rolls and forges readily and machines easily. Drop forging of nickel steels is falling off in favor of other alloy steels.

5. CHROMIUM STEEL.

Contains about 1 per cent carbon and 1 per cent chromium; has high mineralogical hardness. This steel is not in general use but is confined to a few specialties, as ball and ball races, burglar-proof safes, and bars in jails. Low and medium carbon types are not used to any great extent, other alloy steels being superior. It is liable to crack and check in heat treatment.

6. NICKEL-CHROMIUM STEEL.

Addition of chromium to nickel steel increases greatly the strength and resistance to shock and mineralogical hardness. It is more difficult to forge and heat treat and harder to machine than nickel steel; is liable to seam-iness. Steel containing 0.25-0.40 C, 1.50 Cr, and 3.5 Ni⁵ is used for armor plates and projectiles. Steel with 0.10-0.45 C, 1.0 Cr, and 2.0 Ni is largely used for automobile forgings. This steel has high tensile strength, great hardness, and good shock and fatigue resistance. Steel with 0.10-0.45 C, 0.50 Cr, and 1.50 Ni is used for automobile forgings and is excellent case hardening steel. It is somewhat lower in tensile strength than the other two types.⁶

7. VANADIUM STEEL.

Addition of vanadium (generally under 0.25 per cent) to carbon steel increases considerably (about 30 per cent) the elastic limit and tensile strength without affecting materially the ductility. To an even greater extent it increases the resistance to shock and fatigue. Vanadium steel generally used is a chrome-vanadium steel of the following composition: C, 0.10-0.55; Mn, 0.50-0.80; Cr, 0.80-1.00; V, over 0.15 per cent. 0.10-0.20 C steel is used mainly for case hardening and is the best for this

⁴ Nickel steels have higher resistance to impact than carbon steels. (W. Hatt, *Trans. Am. Soc. Civ. Eng.*, 63, p. 307.)

⁵ Bullens says that the most effective ratio of Ni to Cr is 2½ to 1.

⁶ Comparing with chromium steels of equal strength, nickel chromium steels are tougher, more ductile, and less liable to injury through overheating. (*Johnson's Materials of Construction*, p. 684; 1918.)

purpose; 0.25–0.35 C steel is used for automobile forgings of all kinds; 0.35–0.45 C steel is used for crank shafts, locomotive axles, crank pins, connecting rods, piston rods, automobile transmissions, and rear axle shafts; 0.45–0.55 C steel is extensively used for locomotive and automobile springs and gives remarkable resilience and endurance.

Vanadium steels have a wider heat treatment range than other steels. Cr–V steel forges and machines better than Ni–Cr steel; it is not as liable to injury in forging or heat treatment and is free from seaminess. Vanadium steel is as easily worked as carbon steel. While Ni and Cr interfere seriously with the welding quality of steel, vanadium improves this quality.

8. TUNGSTEN STEEL.

Principally used for tools, magnets, magnetos, and hack saws. Tungsten steels are seldom used in engineering construction.

9. COMPLEX ALLOY STEELS.

The only steel of importance in this class is high-speed steel which contains W, Cr, V, and Co.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.			Thermal properties.			Reference.		
			Metric kg./mm. ²		English lb./in. ²		Reduction of area, per cent.	Scleroscope.	Melting point, °C.	Linear coefficient of expansion × 10 ⁶ (per 1°C.).	Casting shrinkage.						
			Proportional limit.	Tensile strength.	Proportional limit.	Yield point.						Tensile strength.	Elongation in 50.8 mm or 2 inches.				
4	5	6	7	8	9	10	11	12	13	14	15	16	17	18			
Chromium: Molybdenum steel— C, 0.30; Cr, 0.70; Mo, 0.35.	2	8	100.1	113.14	156,625	160,925	18.0	62.2	12	13	14	15	16	17	18		
	Drawn at 843° C. (1,550° F.). ¹																
	Drawn at 871° C. (1,600° F.). ¹		105.4	109.6	149,925	155,850	17.5	60.2								(11)	
	Drawn at 899° C. (1,650° F.). ¹		102.5	109.9	145,775	156,375	17.0	60.2								(11)	
	Drawn at 927° C. (1,700° F.). ¹		99.5	107.9	141,570	153,450	17.0	60.1								(11)	
	Drawn at 955° C. (1,750° F.). ¹		100.3	108.5	142,500	154,350	18.0	60.0								(11)	
	Drawn at 982° C. (1,800° F.). ¹		101.2	108.9	144,000	154,900	17.5	59.0								(11)	
	As rolled, 1 in. (25.4 mm), round.		73.8	98.4	105,000	140,000	15.0	32.0								(11)	
	Molybdenum vanadium medium			152.6	170.8	217,000	243,000	9.0	38.2								(51)
		Drawn at 600° F. (316° C.). ²		145.5	158.2	207,000	225,000	10.8	45.4								(51)
Drawn at 800° F. (427° C.). ²			138.5	147.6	197,000	210,000	14.0	52.5								(51)	
Drawn at 1,000° F. (538° C.). ²			122.3	130.8	174,000	186,000	18.2	59.7								(51)	
Drawn at 1,200° F. (649° C.). ²			73.8	147.5	105,000	209,900	237,200	2.3	4.1	540	71					(176)	
	Quenched in oil at 850° C. (1,562° F.); drawn at 205° C. (401° F.) for one hour.																

¹ Quenching medium, water, 3/4 in. (19.1 mm) round bar.
² 3/8 in. (32.2 mm) rounds, quenched in oil from 1,600° F. (871° C.).

Vanadium steel— C, 0.35; Mn, 0.78; S, 0.027; P, 0.025; Cr, 0.74; Si, 0.17; Co, 0.72; Cr, 0.49; V, 0.145, 8	Raw stock.....	60.0	96.1	85,200	136,700	15.6	45.5	302	42	(52)
Steel— Co, 0.16; Si, 0.61; S, 0.10; P, 0.07; Mn, 1.04; Co, 0.53.	Unannealed bars.....	42.5	59.8	60,500	85,100	29.0	43.0			(80)
	Annealed bars.....	34.6	48.8	49,200	69,400	34.0	47.0			(80)
C, 0.25; Si, 0.64; S, 0.11; P, 0.07; Mn, 1.04; Co, 1.80.	Unannealed bars.....	39.4	64.5	56,000	91,800	19.0	24.0			(80)
	Annealed bars.....	36.2	55.1	51,500	78,400	29.0	39.0			(80)
C, 0.38; Si, 1.21; S, 0.14; P, 0.07; Mn, 0.65; Co, 2.50.	Unannealed bars.....	59.8	81.8	85,100	116,400	15.0	15.0			(80)
	Annealed bars.....	42.6	67.8	60,500	96,400	14.0	24.0			(80)
C, 0.55; Si, 0.69; S, 0.11; P, 0.06; Mn, 0.79; Co, 4.50.	Unannealed bars.....	58.3	89.8	82,900	127,700	15.0	17.0			(80)
	Annealed bars.....	39.4	72.4	56,000	103,000	19.0	22.0			(80)
C, 0.52; Si, 0.75; S, 0.14; P, 0.06; Mn, 0.79; Co, 6.90.	Unannealed bars.....	47.3	86.6	67,200	123,200	13.0	13.0			(80)
	Annealed bars.....	47.3	69.3		96,600	22.0	25.0			(80)

¹ Typical analyses of stainless steels.

Chemical component.	Stainless Iron.	Mild stain- less steel.	Stainless steel.
C.....	0.07	0.15	0.37
Si.....	.08	.09	.19
Mn.....	.12	.16	12.0
Cr.....	11.7	11.8	12.0
Ni.....	.57	.77	.55

With the increase of carbon content the forging becomes more and more difficult. Four to six times as much work may be done on stainless iron as on ordinary stainless steel. Between 900 and 1,150° C. (1,652 to 2,102° F.) the material can be forged with rapid blows. Below 850° C. (1,562° F.) the deformation becomes difficult. Important quality—immune from rusting if the surface is not distorted by rough cut. On harder varieties rash grinding may produce soft spots, which may stain or crack; most resistant to corrosion when in hardened condition. Nitric acid, cold, and boiling, does not appreciably attack stainless steel. It is corroded in sea water when in contact with copper; retains considerable hardness and strength at high temperatures; tensile strength at 700° C. (1,292° F.) 33,600 lb./in.² or 23.7 kg./mm.² Loss of weight by scaling at high temperatures is considerably lower than for any other steel.

² Easy to forge, machine, and work cold.

³ According to heat treatment.

⁴ Easily forged by power hammer; can be hardened; used for cutting tools for soft materials.

⁵ Can be forged by power hammer; is hardened if allowed to cool in the air; suitable for sharp and durable cutting tools, and for hard wearing surfaces.

⁶ Forging qualities, etc., as for medium stainless steel.

⁷ Difficult to forge; possesses great strength at high temperatures; stains more easily than milder varieties.

⁸ Chrome-molybdenum (C, about 0.35; Cr, about 0.86; and Mo, about 0.25) steel compared with other alloy steels which are in the same category from a commercial standpoint and which are treated to the same tensile strength shows: (1) A slightly higher elastic limit; (2) a higher elongation, hence greater ductility; and (3) a much higher reduction of area, hence greater toughness. For constant tensile strength and nearly constant elastic limit molybdenum steel shows increase of elongation and of reduction of area with increase in molybdenum up to 1.0 per cent.

⁹ $\frac{3}{8}$ in. (22.2 mm) rounds quenched in oil from 1,450° F. (788° C.).

¹⁰ Modulus of rupture in torsion 97.0 kg./mm² (138,000 lb./in.²); modulus of rupture in torsion (annealed) 68.8 kg./mm² (98,000 lb./in.²).

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.			Thermal properties.			Reference.			
			Metric kg./mm ²		English lb./in. ²		Reduction in area.	Brinell.	Melting point.	Linear coefficient of expansion ×10 ⁶ (per 1° C.).	Casting shrinkage.							
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.						Yield point.	Tensile strength.					
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	
Cobalt—Contd. Steel—Contd. C, 0.64; Co, 2.68.	As received from forge.			46.0	76.2													(80)
C, 0.62; Co, 5.50.	do.			52.0	76.9													(80)
C, 0.84; Co, 11.18.	do.			51.3	102.3													(80)
C, 0.93; Co, 16.97.	do.			59.9	118.6													(80)
Molybdenum: Steel—																		
C, 0.05; Si, 0.018; Mn, 0.06; Mo, 0.31. ¹¹	Cast, unannealed.		17.3		28.4	24,600	40,300	11				124						(81)
C, 0.06; Si, 0.05; Mn, 0.01; Mo, 0.52. ¹²	do.		17.3		34.7	24,600	49,300	12				95						(81)
	Cast, annealed at 800° C. (1,472° F.).		17.3		36.2	24,600	51,500	25				87						(81)
	Forged, unannealed.		31.5		33.0	44,800	47,000					126						(81)
	Forged, annealed at 800° C. (1,472° F.).		20.5		30.0	29,100	42,600					90						(81)
C, 0.11; Mo, 0.94. ¹³	Cast, unannealed.		36.2		45.7	51,500	65,000	6				160						(81)
	Cast, annealed at 800° C. (1,472° F.).		30.0		44.1	42,600	62,700	8				126						(81)
	Forged, unannealed.		53.5		63.0	76,100	89,600					127						(81)
	Forged, annealed at 800° C. (1,472° F.).		33.0		42.5	47,000	60,400					127						(81)
C, 0.13; Si, 0.08; Mn, 0.02; Mo, 1.78. ¹⁴	Cast, unannealed.		31.5		45.7	44,800	65,000	2				194						(81)
	Cast, annealed at 800° C. (1,472° F.).		26.8		36.2	38,100	51,500	5				131						(81)

	42.5	47.2	60,400	67,200	24	59	179	(81)
Forged, unannealed.	42.5	47.2	60,400	67,200	24	59	179	(81)
Forged, annealed at 800° C. (1,472° F.).	47.2	53.5	67,200	76,100	30	62	121	(81)
Cast, unannealed.	47.3	69.3	67,200	98,500	2	3	248	(81)
Cast, annealed at 800° C. (1,472° F.).	42.5	67.8	60,500	96,400	5	5	196	(81)
Forged, unannealed.	55.1	78.8	78,400	112,000	19	44	188	(81)
Forged, annealed at 800° C. (1,472° F.).	45.6	74.0	64,900	105,200	21	42	192	(81)
Cast, unannealed.	31.5	53.5	44,800	76,100	1	2	188	(81)
Cast, annealed at 800° C. (1,472° F.).	29.9	55.6	42,600	70,200	2	2	212	(81)
Forged, unannealed.	58.2	85.1	82,800	121,000	15	21	212	(81)
Forged, annealed at 800° C. (1,472° F.).	56.7	83.4	80,700	118,700	15	29	223	(81)
Cast, annealed at 800° C. (1,472° F.).	53.6	53.6	76,200	76,200	Nil.	Nil.	300	(81)
Cast, unannealed.	36.2	36.2	51,500	51,500	Nil.	Nil.	306	(81)
Cast, annealed.	59.9	91.4	85,100	130,000	2	2	275	(81)
Forged, unannealed.	52.0	85.1	73,900	121,000	1	1	364	(81)
Forged, annealed at 800° C. (1,472° F.).	18.9	34.7	49,300	49,300	Nil.	1	280	(81)
Cast, unannealed.	18.9	18.9	26,900	26,900	Nil.	Nil.	280	(81)
Cast, annealed at 800° C. (1,472° F.).								

ii Would not forge.

iii Would not forge. Cast unannealed; too hard to machine.

Impact Values of Molybdenum Steels.

Footnote indicating the steel.	Cast unannealed.		Cast annealed at 800° C. (1,472° F.).		Forged unannealed.		Forged annealed at 800° C. (1,472° F.).		Footnote indicating the steel.		Cast unannealed.		Cast annealed at 800° C. (1,472° F.).		Forged unannealed.		Forged annealed at 800° C. (1,472° F.).		
	kgm	ft.-lb.	kgm	ft.-lb.	kgm	ft.-lb.	kgm	ft.-lb.	(a)	(b)	(c)	kgm	ft.-lb.	kgm	ft.-lb.	kgm	ft.-lb.	kgm	ft.-lb.
(11)	1.0	7.2	1.0	7.2	0.5	3.6	2.0	14.5	(11)	(11)	(11)	Nil.	Nil.	4.0	28.9	1.0	7.2	3.5	25.3
(12)	1.5	3.6	1.0	7.2	0.5	3.6	3.0	21.7	(12)	(12)	(12)	Nil.	Nil.	2.0	14.4	1.0	7.2	5	3.6
(13)	2.0	14.5	1.0	7.2	4.0	28.9	14.0	101.3	(13)	(13)	(13)	Nil.	7.2	2.0	14.4	1.0	7.2	5	3.6
(14)	1.0	7.2	1.0	7.2	5.0	36.2	7.5	54.3	(14)	(14)	(14)	1.0	7.2	1.0	7.2	1.0	7.2	5	3.6
(15)	2.0	14.5	1.0	7.2	5.0	36.2	7.5	54.3	(15)	(15)	(15)	1.0	7.2	1.0	7.2	1.0	7.2	5	3.6

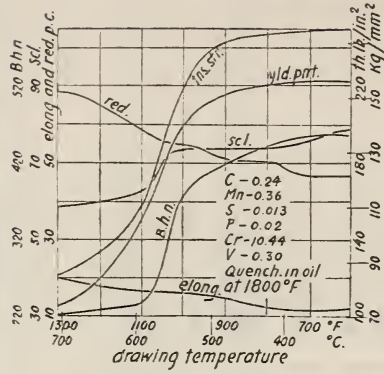


FIG. 28.—Effect of drawing temperature on the tensile properties of stainless steel.

F. Grotts, Chem. ann Met. Eng. 19; 1918.

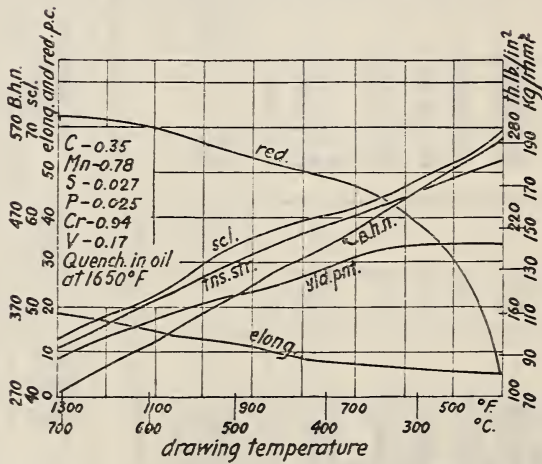


FIG. 29.—Effect of drawing temperature on the tensile properties of chrome-vanadium steel.

F. Grotts, Chem. and Met. Eng. 19; 1918.

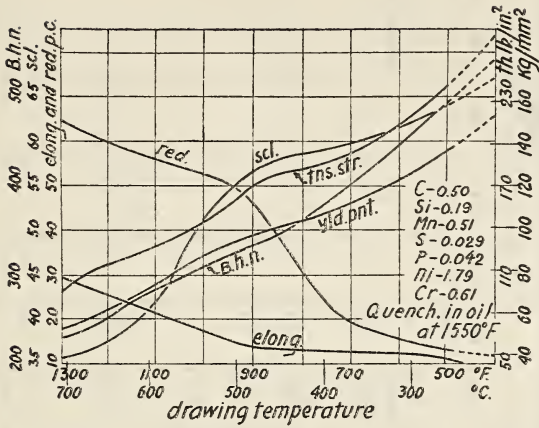


FIG. 30.—Effect of drawing temperature on the tensile properties of chrome-nickel steel.

F. Grotts, Chem. and Met. Eng. 19; 1918.

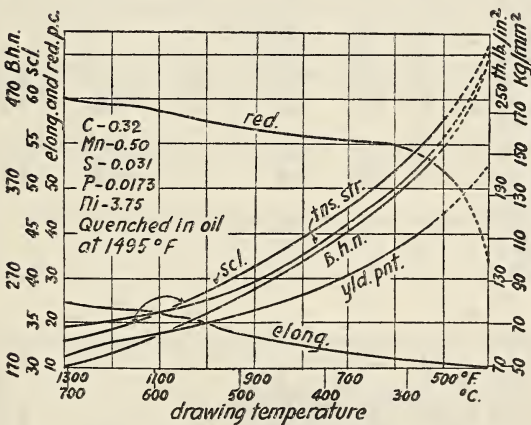


FIG. 31.—Effect of drawing temperature on the tensile properties of nickel steel.

F. Grotts, Chem. and Met. Eng., 19; 1918.

0.60; P.max.; acid, 0.04; basic, 0.03; S,max.0.045; Ni,min.3.25. ³⁰	Plates, shapes, and bars.	35.2	59.8-70.3	50,000	85,000-100,000	(²¹)	25.0			(37)
C, max. 0.45; Mn, max. 0.70; P,max. acid, 0.05; basic, 0.04; S, max. 0.05; Ni, 1.1; plus, annealed, 3.25-2.2 min.	Eyebars flats and rollers, unannealed.	38.7	66.8-77.3	55,000	95,000-110,000	16.0	25.0			(37)
Nickel steel: C,0.32; Mn,0.50; S, 0.035; P, 0.017; Ni,3.74 ³⁴	Raw stock.....	68.3	78.8	97,200	112,200		50.0	217	40	(52)
C, 0.19; Ni, 25.30. ³⁵										(78)
Invar ³⁶ : C,0.1; Mn,0.5; Ni, 36.0; S, negligible quantities.	8.0	21.1-49.3	35.1-70.3	30,000-70,000	50,000-100,000	25-50	40-70	160	19	(172)
Platinite: Ni, 46.0										(102)
Nickel-silicon steel: C,0.49; Si,0.52; Mn,0.65; Ni, 3.25; Al,0.02; Ti,0.03.	Normalized at 770° C. (1,418° F.).	47.2	82.3	67,100	117,200	11.3	18.9	241		(176)
C,0.36; Si,1.15; Mn,0.85; Ni, 3.20; Al,0.01.	Heat treated ³⁸ at 840° C. (1,544° F.).	119.5	201.0	170,000	286,000	0.6	1.1	444		(176)
C,0.49; Si,1.30; Mn,0.78; Ni, 3.05.	Heat treated ³⁸ at 800° C. (1,472° F.).	28.1	96.5	40,800	137,300	13.1	27.1	241		(176)
C,0.49; Si,2.20; Mn,0.94; Ni, 3.05.	Heat treated ³⁸ at 840° C. (1,544° F.).	63.3	193.4	90,000	275,100	8.0	22.9	402		(176)
	Heat treated ³⁸ at 840° C. (1,544° F.).	37.3	90.6	53,000	128,900	21.0	53.3	266		(176)
	Heat treated ³⁸ at 840° C. (1,544° F.).	102.0	208.6	145,000	232,500	7.5	12.9	591		(176)
	Heat treated ³⁸ at 840° C. (1,544° F.).	50.6	109.4	72,000	108,000	14.5	40.9	317		(176)
	Heat treated ³⁸ at 840° C. (1,544° F.).	181.5	219.8	258,100	312,600	8.0	24.9	532		(176)

³⁰ Shall bend cold through 180° flat on itself without cracking on the outside of the bent portion.

³¹ 1,435- tensile strength in kg./mm² or 1,500,000+ tensile strength in lb./in.² per cent. For every $\frac{1}{32}$ in. (0.79 mm) above 1 in. (25.4 mm) in thickness a deduction of 0.25 per cent shall be made from the above values.

³² Shall bend cold through 180° without cracking on the outside of the bent portion around a pin, the diameter of which is equal to the thickness of the specimen, for plates, shapes, and bars under $\frac{1}{4}$ in. (19.1 mm) in thickness; twice the thickness of the specimen for plates, shapes, and bars over $\frac{1}{4}$ in. (19.1 mm); 1 in. (25.4 mm) for pins and rollers.

³³ In 2.16 in. (5,486, mm).

³⁴ Used for bolts, nuts, and parts subjected to shock.

³⁵ Modulus of rupture in torsion, 64,6 kg./mm² (92,000 lb./in.²). Winkelman's Handbuch der Physik, 1908, 1, 1, gives for modulus of elasticity of 25 per cent nickel steel 8,600 kg./mm² (26,450,000 lb./in.²).

³⁶ Invar can be forged, rolled, turned, filed and drawn into wire; takes beautiful polish; withstands corrosive action of water even when immersed for several days; subject to changes in length due to "after effects" following cooling from a high temperature. Invar also gradually elongates with time. Applications.—In clocks and watches, in instruments for geodetic survey, and for measuring lengths standards. Landolt-Börnstein tables (1912) give for modulus of elasticity 15,000 kg./mm² (21,300,000 lb./in.²).

³⁷ Has the same coefficient of expansion as glass.

³⁸ Quenched in oil at the temperature given for normalized specimens and drawn at 175° C. (347° F.) for three hours.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.				Thermal properties.			Reference.	
			Metric kg/mm ²		English lb./in. ²		Elongation in 50.8 mm or 2 inches.	Reduction of area.	Brinell.	Scleroscope.	Melting point.	Linear coefficient of expansion $\times 10^6$ (per 1°C.).	Casting shrinkage.				
			Yield point.	Tensile strength.	Proportional limit.	Yield point.								Tensile strength.			
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Nickel-silicon-cerium steel: C, 0.45; Si, 1.30; Mn, 0.71; Ni, 2.95; Ce, 0.01. C, 0.41; Si, 1.70; Mn, 0.75; Ni, 2.80; Ce, 0.06. C, 0.46; Si, 1.55; Mn, 0.98; Ni, 2.90; Ce, 0.10.	Normalized at 820° C. (1,508° F.), Heat treated ²⁸ Normalized at 840° C. (1,544° F.), Heat treated ²⁸ Normalized ²⁸ (1,544° F.), Heat treated ²⁸		42.2	145.1	218.7	60,000	206,500	311,100	8.5	37.2	555		°C.				(176)
Nickel-silicon-copper steel: C, 0.45; Si, 1.10; Mn, 0.84; Ni, 1.90; Cu, 1.35. C, 0.46; Si, 1.30; Mn, 0.82; Ni, 2.55; Cu, 0.64.	Normalized at 800° C. (1,472° F.), Heat treated ²⁸ Normalized at 800° C. (1,472° F.), Heat treated ²⁸		56.2	90.0	106.0	80,000	128,200	150,800	11.0	27.2	320						(176)
Nickel-silicon-molybdenum steel: C, 0.42; Si, 1.45; Mn, 0.83; Ni, 3.25; Mo, 0.78.	Normalized at 780° C. (1,436° F.), Quenched in oil at 780° C. (1,436° F.); drawn at 175° C. (347° F.) for three hours.		46.4	102.6	102.6	66,000		146,000	23.0	25.9	286						(176)
			58.3	211.0	211.0	83,000	300,100	300,100	5.5	8.4	444						(176)

Nickel-silicon-uranium steel: C, 0.43; Si, 1.30; Mn, 0.90; Ni, 3.00; Al, 0.01; U, 0.34.	93.7	129.0	133,500	183,500	6.0	12.9	289	(176)	
	Normalized at 820° C. (1,508° F.); quenched in oil at 820° C. (1,508° F.); drawn at 175° C. (347° F.) for three hours.	137.2	217.7	150,000	309,800	10.5	35.2	627	(176)
Nickel-silicon-vanadium steel: C, 0.60; Si, 1.30; Mn, 0.79; Ni, 3.15; V, 0.32.	58.3	72.5	83,000	139,000	19.5	48.4	302	(176)	
	Normalized at 800° C. (1,472° F.); quenched in oil at 800° C. (1,472° F.); drawn at 175° C. (347° F.) for three hours.	194.2	241.3	276,500	343,600	5.0	7.8	627	(176)
Nickel-silicon-zirconium steel: C, 0.34; Si, 1.10; Mn, 0.57; Ni, 3.05; Ti, 0.06; Zr, 0.55.	42.2	55.4	60,000	78,900	22.0	44.7	234	(176)	
	Normalized at 860° C. (1,580° F.); quenched in oil at 860° C. (1,580° F.); drawn at 175° C. (347° F.) for three hours.	74.5	163.2	106,000	232,200	6.5	36.5	351	(176)
C, 0.37; Si, 1.15; Mn, 0.56; Ni, 3.05; Al, 0.02; Ti, 0.11; Zr, 0.20.	57.8	78.2	82,200	111,300	21.5	53.3	241	(176)	
	Normalized at 820° C. (1,508° F.); quenched in oil at 820° C. (1,508° F.); drawn at 175° C. (347° F.) for three hours.	91.3	162.2	176.9	130,000	230,900	251,700	532	(176)
Nickel-silicon-zirconium-cobalt steel: C, 0.43; Si, 1.56; Mn, 1.08; Ni, 3.01; Zr, 0.34; Co, 0.37.	123.0	188.6	228.6	175,000	268,300	325,400	534	(176)	
	Quenched in oil at 843° C. (1,550° F.); drawn at 288° C. (550° F.) for one hour.	(176)
Nickel-vanadium steel: ²⁹ C, 0.36; Ni, 3.25; V, 0.45.	(78)
	Oil tempered.....	(78)

²⁸ Quenched in oil at the temperature given for normalized specimens and drawn at 175° C. (347° F.) for three hours.

²⁹ Modulus of rupture in torsion, 71.6 kg./mm.² (162,000 lb./in.²).

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.			Thermal properties.			Reference.		
			Metric kg/mm ²		English lb./in. ²		Elongation in 50.3 mm or 2 inches.	Reduction of area.	Brinell.	Scleroscope.	Melting point.	Linear coefficient of expansion $\times 10^6$ (per 1°C.).	Casting shrinkage.				
			Yield point.	Tensile strength.	Proportional limit.	Yield point.								Tensile strength.		Per ct.	Per ct.
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Resistal: ³⁰ C, 0.33; Mn, 0.76; Si, 4.51; Ni, 25.76; Cr, 15.16. C, 0.33; Mn, 0.80; Si, 4.32; Ni, 25.18; Cr, 15.85. Resistal: ³¹ Grade 2-1	Bar (grade 4)	44.8	107.3	75.4 39.8	86.1	63,660	8	9	10	11	12	13	14	15	16	17	18
As rolled. Quenched in oil from 250° C. (2,408° F.). As rolled. Quenched in oil from 900° C. (1,652° F.). Quenched in air from 900° C. (1,652° F.). Quenched in oil from 900° C. (1,652° F.). Quenched in water from 900° C. (1,652° F.). Quenched in water from 600° C. (1,112° F.). Quenched in water from 850° C. (1,562° F.). Quenched in water from 1,050° C. (1,922° F.).	Sheet 0.038 in. (0.96 mm), (grade 4).	107.3	107.3	75.4 39.8	142.8	152,590	107.3	107.3	25.5 67.5	40.1 67.5	302 187	48	14	15	16	17	(107)
Grade 3-2	As rolled. Quenched in oil from 250° C. (2,408° F.). As rolled. Quenched in oil from 900° C. (1,652° F.). Quenched in air from 900° C. (1,652° F.). Quenched in oil from 900° C. (1,652° F.). Quenched in water from 900° C. (1,652° F.). Quenched in water from 600° C. (1,112° F.). Quenched in water from 850° C. (1,562° F.). Quenched in water from 1,050° C. (1,922° F.).	44.8	107.3	75.4 39.8	142.8	152,590	107.3	107.3	25.5 67.5	40.1 67.5	302 187	48	14	15	16	17	(107)
Grade 2-6	As rolled. Quenched in oil from 250° C. (2,408° F.). As rolled. Quenched in oil from 900° C. (1,652° F.). Quenched in air from 900° C. (1,652° F.). Quenched in oil from 900° C. (1,652° F.). Quenched in water from 900° C. (1,652° F.). Quenched in water from 600° C. (1,112° F.). Quenched in water from 850° C. (1,562° F.). Quenched in water from 1,050° C. (1,922° F.).	44.8	107.3	75.4 39.8	142.8	152,590	107.3	107.3	25.5 67.5	40.1 67.5	302 187	48	14	15	16	17	(107)
Grade 3-8	As rolled. Quenched in oil from 250° C. (2,408° F.). As rolled. Quenched in oil from 900° C. (1,652° F.). Quenched in air from 900° C. (1,652° F.). Quenched in oil from 900° C. (1,652° F.). Quenched in water from 900° C. (1,652° F.). Quenched in water from 600° C. (1,112° F.). Quenched in water from 850° C. (1,562° F.). Quenched in water from 1,050° C. (1,922° F.).	44.8	107.3	75.4 39.8	142.8	152,590	107.3	107.3	25.5 67.5	40.1 67.5	302 187	48	14	15	16	17	(107)

Silicon steel:	Quenched in water from 1,200° C. (2,192° F.), cooled in air after one hour at 1,300° C. (2,372° F.).	40.7	69.9	57,900	99,400	60.0	51.1	38	(53)
C,0.38; Si,0.46; Mn,0.52; Al,0.45.	Normalized at 840° C. (1,544° F.).	30.2	65.0	43,000	89,600	26.3	50.2	163	(176)
C,0.24; Si,1.10; Mn,0.71; Al,0.01.	Heat treated ³⁰ at 900° C. (1,652° F.).	29.5	78.2	42,000	111,200	9.5	30.6	28	(176)
C,0.42; Si,1.50; Mn,0.56; Al,0.01.	Normalized at 850° C. (1,560° F.).	35.3	86.1	79,000	122,500	20.0	51.5	241	(176)
	Heat treated ³⁰	96.2	182.2	137,000	259,400	4.5	15.9	418	(176)

³⁰ Rezistal was found to be fairly resistant to atmospheric corrosion, but the samples tested did not give as good results as 13 per cent chromium steel. Tests at high temperatures gave results somewhat higher than those obtained in high chromium, chromium-tungsten, or silicon-chromium steels.

Temperature.	Tensile strength.		Elongation in 2 in. (50.8 mm).
	° C.	° F.	
700	1,292	23	52,200
800	1,472	42	29,710
960	1,760	19.5	9,750

Compressive elastic limit, 37.4 kg/mm² (81,610 lb./in.²); Compressive strength, 0.7-0.6 kg/mm² (130,300 lb./in.²); Torsional elastic limit, 36.7 kg/mm² (82,150 lb./in.²); Modulus of rupture in torsion, 77-7 kg/mm² (170,500 lb./in.²); Impact value, 24.2 ft.-lb. (32.6 kgm.) Minimum diameter over which it can bend 180° without cracking—four thicknesses.

Highly resistant to attack of all acids. In oxidizing flame rezistal is only slightly stamed after several hours at 1,093° C. (2,000° F.); may remain for days in tap water with practically no rust. Rezistal is tough and strong at all temperatures from -85 to +1,300° C. (-301 to +2,372° F.). When attacked by an oxyacetylene flame it takes 20 times as long to melt a hole as does ordinary steel. Established uses—Rails, racks, trays in enameling furnaces for 871-982° C. (1,600-1,800° F.), valves and parts for internal-combustion engines, cooking utensils, vault plates and hinges that are to resist oxyacetylene flame, saws, and drills, rifle and shotgun barrels, cast cyanide pots, etc. Modulus of elasticity, 19,140 kg/mm² (27,200,000 lb./in.²) in tension and 8,220 kg/mm² (11,700,000 lb./in.²) in shear. For machining rezistal should be annealed at 800-850° C. (1,472-1,562° F.). Rezistal can not be cut successfully with an ordinary hack saw and requires high-speed friction saw or thin carbide wheel. Rezistal can be welded with the oxyacetylene flame.

³² Quenched in oil at the temperature given for normalized specimen and drawn at 175° C. (347° F.) for three hours.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.				Thermal properties.			Reference.	
			Metric kg/mm ²			English lb./in. ²			Elongation in 50.8 mm or 2 inches.	Reduction of 50.8 mm area.	Brinell.	Setero scope.	Melting point.	Linear coefficient of expansion $\times 10^6$ (per 1°C.).	Casting shrinkage.		
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.	Yield point.	Tensile strength.									Per ct.
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Titanium steel: ³³ Ti, 0.5.....																	
Tungsten steel: ³⁴ C, 0.87; Mn, P, 0.35; 0.025; S, 0.015; Si, 0.15; V, 0.77; W, 15.55.	Raw stock.....			59.6	77.3		84,800	110,000	24.0	54.0	207	35					(98)
Uranium steel: C, 0.37; Mn, 0.59; Si, 0.21; P, 0.022; S, 0.025; Ni, 3.51; U, 0.17. ³⁵	Untreated..... Quenched in oil at 1,400° F. (760° C.); drawn at 350° F. (177° C.). Quenched in oil at 1,400° F. (760° C.); drawn at 950° F. (510° C.).			35.1 101.3	66.1 190.5		50,000 144,000	94,000 271,000	22.0 9.3	46.7 29.2	194 541	29 64					(108) (108)
C, 0.32; Mn, 0.66; Si, 0.23; P, 0.024; S, 0.028; U, 0.22. ³⁶	Untreated..... Quenched in wa- ter at 1,550° F. (843° C.); drawn at 350° F. (177° C.). Quenched in wa- ter at 1,550° F. (843° C.); drawn at 850° F. (454° C.).			16.5 96.3	46.4 163.8		23,400 137,000	66,000 233,000	31.0 11.5	60.0 47.0	129 512	22 56					(108) (108)
Vanadium steel: ³⁷ C, 0.22; Mn, 0.72; S, 0.039; P, 0.04; V, 0.12.	Quenched in oil at 1,500° F. (815° C.). Quenched in oil at 1,600° F. (871° C.). Quenched in oil at 1,700° F. (927° C.).			79.5	97.7		113,000	139,000	3.0		286	44					(52)
				118.1	137.3		168,000	195,300	4.5			55					(52)
				121.0	142.0		172,000	202,000	6.75			58					(52)

³⁵ Titanium removes O and N and prevents formation of blowholes in steel. It increases the density of the metal, tensile strength, elastic limit, reduction of area, transverse strength, and ductility, and increases resistance to shock, torsion and impact stresses. Resistance to wear was well shown in a nine-months test of rails. A titanium-treated rail lost 1.39 lb./sq. ft. (66 g./m²) as against .93 lb./sq. ft. (43 g./m²) lost by an ordinary rail. Still more illustrative is the increase in resistance to fatigue, as shown below. The composition of steel was: C, 0.25; Mn, 0.64; Si, 0.45; P, 0.04; S, 0.035.

Without titanium.		With titanium.	
Stress.		Stress.	
Number of revolutions.		Number of revolutions (the same specimen).	
kg/mm ² 27.3	lb./in. ² 38,870	kg/mm ² 27.3	lb./in. ² 38,870
		28.5	40,600
		29.8	42,400
		31.1	44,200
			4,052,000
			10,800,000
			1,919,000
			1,006,000
			(broke)

³⁶ Used for high-speed cutting tools and exhaust valves; retains cutting properties at red heat.

³⁶ Charpy Impact Value.

Untreated.		Quenched in oil at 1,400° F. (760° C.) and drawn at 350° F. (177° C.).		Quenched in oil at 1,400° F. (760° C.) and drawn at 950° F. (510° C.).	
kgm 2.62	ft.-lb. 19.0	kgm 3.23	ft.-lb. 23.4	kgm 4.97	ft.-lb. 36.0

³⁶ Charpy Impact Value.

Untreated.		Quenched in water at 1,550° F. (843° C.) and drawn at 350° F. (177° C.).		Quenched in water at 1,550° F. (843° C.) and drawn at 850° F. (454° C.).	
kgm 1.50	ft.-lb. 10.8	kgm 3.83	ft.-lb. 27.8	kgm 7.12	ft.-lb. 51.7

³⁷ Especially good for sheet steel that has to be punched; very tough

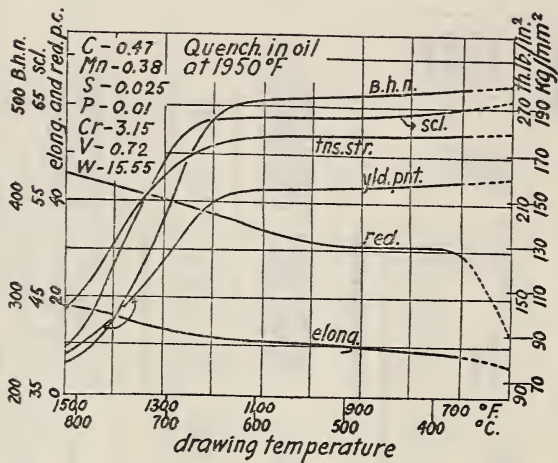


FIG. 32.—Effect of drawing temperature on the tensile properties of tungsten steel.

F. Grotts, Chem. and Met. Eng., 19; 1918.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.				Thermal properties.			Reference.	
			Metric kg./mm ²			English lb./in. ²			Reduction of area.	Brinell.	Scleroscope.	Melting point.	Linear coefficient of expansion ×10 ⁶ (per 1°C.).	Casting shrinkage.			
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.	Yield point.	Tensile strength.						Per ct.	mm/m		in./ft.
Zirconium steel: ⁸⁸ C, 0.42; Mn, 0.09; Sb, 1.50; Ni, 3.00; Zr, 0.34. Lead: ⁸⁹ Pb.	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Pb, commercial	11.35	168.7	198.2	240,000	282,000												(141)
Antimony (hard lead) ⁹¹ Pb; Sb.....	10.71		2.1 1.8 1.25 1.70 2.20		2,900 2,560 1,780 2,420 3,130								0.327	0.29, 24			(97) (97) (109) (109) (109)
			3.89		5,530				14.8		3-4						(185)
			3.82		5,440				15.2		3-4						(185)
			4.16		5,910				19.0		3-4						(185)

⁸⁸ Iron-zirconium removes nitrogen and oxides from steel. Iron-zirconium alloys containing titanium and aluminum are highly resistant to chemical reagents, and are readily malleable. A typical analysis of some of these alloys: Zr, 65; Fe, 32; Al, 1.5; Ti, 0.25. ⁸⁹ Compressive strength of rolled lead, 5 kg./mm² (3,110,000-2,420,000 lb./in.²). Modulus of elasticity in shear, 450 kg./mm² (780,000 lb./in.²). According to Winkelman's Handbook der Physik, I, p. 557, 1908; modulus of elasticity of drawn lead, 1,727 kg./mm² (2,400,000 lb./in.²); modulus of elasticity of annealed lead, 1,823 kg./mm² (2,560,000 lb./in.²). Amagat gives for the Poisson's ratio, 0.427.

⁹¹ Smithsonian Physical Tables, 7th edition, 1920.

⁹² Norr—

Thickness.		Erichsen test depth of cup.	Number of bendings before cracking; when bent over r=0.05 in. (1.97 mm) through an angle of 90° each way.*
mm	in.	mm	
0.88	0.035	9.96	5.6
1.07	.042	9.84	4.3
1.27	.050	9.66	2.9

*Mechanical properties are practically the same in both directions.

Barium (ulco meal) ⁸⁸	9.14	13,000	1	(56)
Pb, 99-99; Ba, Ca, balance, ⁸⁹
Barium (hard-ened lead) ⁹⁰	(57)
Pb, 97-98; Ba, Ca, balance, ⁹¹
Magnesium: Pure ⁹²	1.74	(58)
Hot-rolled.....	14.1	20,000	9	651	26.9
Pure ⁹³	24.6	35,000	(59)
Hot-rolled.....	23.2	33,000	(77)
Pure ⁹⁴	(75)

⁸⁸ Erichsen test.—Depth of cup, 9.76 mm; number of bendings (same conditions as for hard lead) before cracking, 11; number of bendings (same conditions as for hard lead) to complete rupture, 22; the last property practically the same in both directions.

⁸⁹ General appearance of lead; may be cast, drawn, rolled, or extruded; specific gravity and melting point identical with those of lead; has metallic ring of bell metal; none of the brittleness of antimonal lead; pronounced increase in hardness upon aging; aging accelerated by steam heat, excellent structure, free from blowholes, and has low coefficient of friction.

⁹⁰ American Machinist, Nov. 30, 1918.

⁹¹ In 1 in. (35.4 mm).

⁹² Alloy tested in bearings up to 6,000 lb./in.² (4.22 kg/mm²) pressure gave satisfactory results. Hardness of bearing alloys is fully maintained after extended periods of use. Decrease of hardness up to 200° C. (392° F.) was less than that of tin-base alloy.

⁹³ Brinell hardness at 500 kg (1,102 lb.) load; scleroscope, with magnifying hammer.

Bureau of Standards, comparative test.

Genuine Babbitt Metal.

Load.	r. p. m.	Total number of revolutions.	Final temperature.		Rise in temperature.		Friction.		Loss in weight.		
			°C.	°F.	°C.	°F.	kg.	lb.	g.	gr.	
0.070	100	694	89	192	53	95	10.0	22	0.023	0.355	
.141	200	706	102	216	58	104	13.2	29	.021	.324	
.211	300	682	125	257	100	180	17.2	38	.013	.201	
.281	400	603	139	282	94	164	35.8	79	*.054	.833	
Ulco Metal.											
0.070	100	710	56	133	23	41	5.9	13	0.013	0.201	
.141	200	715	69	156	33	59	8.2	18	.021	.324	
.211	300	719	80	176	42	76	12.3	27	.013	.201	
.281	400	711	81	178	43	77	10.4	23	.022	.339	
.351	500	723	77	174	43	77	11.3	25	.014	.216	
.422	600	692	14,960	79	174	45	81	10.9	24	.021	.324
.492	700	648	24,520	62	144	38	68	10.9	24	.020	.309
.562	800	365	12,870	53	127	20	36	10.4	23	.010	.154
.633	900	408	22,300	59	138	22	40	10.9	24	.015	.232
.703	1,000	405	23,200	66	151	36	65	10.0	22	†.014	.216

* Bearing seized and smoking.

† Bearing still in good condition.

⁸⁸ Compressive strength 27.1 kg/mm² (38,500 lb./in.²).

⁸⁹ Modulus of elasticity, 4,260 kg/mm² (6,050,000 lb./in.²).

⁹⁰ Modulus of elasticity, 4,260 kg/mm² (6,050,000 lb./in.²).

⁹¹ Landolt-Börnstein tables (1912) give for modulus of elasticity 4,000 kg/mm² (5,680,000 lb./in.²) and for the modulus of elasticity in shear 1,180-1,700 kg/mm² (1,680,000-2,420,000 lb./in.²).

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific grav.	Tensile properties.						Hardness number.			Thermal properties.			Reference.		
			Metric kg/mm ²		English lb./in. ²		Elongation in 50.8mm or 2 inches.	Reduction of area.	Erinell.	Sclero-scope.	Melting point.	Linear coefficient of expansion ×10 ⁶ /perl °C.	Casting shrinkage.				
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.								Yield point.		Tensile strength.	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Magnesium.....	Cast, sand Forged.....				10.2 23.2			14,500 33,000		Per ct. 5		50 40	°C.		mm	in. ft.	(64) (64)
Magnesium: ⁵¹ Pure.....	Cast.....	1.74			14.1 23.6			20,000 33,600	8								(65) (65)
Dow metal— Mg, 92; Al, 8.....	Cast, sand..... Sand cast, heat treated.....	1.79 1.79			17.9 21.8			25,500 31,000	4 7.5			50 55 50 50					(64) (64)
Dow metal ⁵² Zinc (electron metal), ⁵³	Rolled, bars.....	1.77	4.0	9.9	10.0 23.2	4,830	13,780	14,200 32,800	0 12.0	Per ct. 18.0							(186) (187)
Zinc (electron metal), ⁵³	Semihard.....	1.81		13.0	25.3		18,500	36,000	15.0	16.0		22					(188)
Mg, 95; Zn, 5.....	Hard.....	1.83		14.6	33.7		20,800	48,000	5.0	7.0		27					(188)
Mg, 95.18; Zn, 4.82; Cu, 0.20 (Spec. A) ⁵⁴	Cast, sand.....	1.78		18.9	18.0 25.4		26,900	36,100	7.4 55 19.0			50 41 55 51					(64) (69)
Mg, 95.94; Zn, 4.24; Cu, 0.42 (Spec. B) ⁵⁴	1.79		12.0	28.3		17,000	40,300	55 19.0			55 51					(69)
Mg, 97; Cu, 0.62 (Spec. C) ⁵⁴	1.79		18.9	29.0		26,900	41,200	55 13.0			55 63					(69)
Zinc (electron metal), ⁵⁷	Bars over 1.5 in. diam.(38.1mm). Rods 0.3 in.diam. (7.6mm). Hard, cold worked.				25-28			35,500- 39,800	15-20	8-22							(212)
					27.2			38,700	18-22			55 47					(212)
					35.5			50,500	2-4			55 67					(212)
Manganese: Mn.....		7.42											1,230 (2,246° F.)				(138)
Molybdenum: Mo.....		9.01											2,535 (4,595° F.)				(138)

	Annealed	41.5	59,000	32.0	1,450 (2,642° F.)	(210)
Nickel: Electrolytic— Ni, 99.5						
Pure ⁶⁰ — Ni, 99.0; Fe, Cu, S, Si, Mn, S.	8.6-8.9					(210)
Pure ⁶¹ — Ni, 99.0; Fe, Cu, S, Si, Mn, S.	8.84				1,451 (2,644° F.)	(60)
Pure ⁶² — Ni, 99.0; Fe, Cu, S, Si, Mn, S.	63.3- 77.3	70.3- 84.3	90,000- 120,000	15-20		(60)
Cast (deoxidized).	14.1- 21.1	35.1- 42.2	20,000- 60,000	20-30		(61)
Hot-rolled rods.	14.1- 21.1	49.2- 56.2	20,000- 30,000	40-50		(172)
Sheet, hard-rolled	59.7- 73.8	63.3- 77.4	85,000- 105,000	1-2		(172)
Sheet, annealed.	10.5- 17.6	42.2- 52.7	15,000- 25,000	35-45		(172)
Wire, hard-drawn	59.7- 73.8	63.3- 77.4	85,000- 105,000			(172)
Wire, annealed.	14.1- 21.1	45.7- 52.7	20,000- 30,000			(172)

⁶⁰ At 500 kg (1,102 lb.) load.
⁶¹ Brilliant white color; remains untarnished in a dry air, but in a moist atmosphere becomes covered with a thin white film of oxide; great affinity for oxygen; used largely for deoxidizing castings of copper, brass, nickel, silver, and aluminum; added to nonferrous castings to strengthen them; when cold is fairly malleable, especially after annealing at 400-425° C. (752-797° F.), when it can be rolled with ease.
⁶² Modulus of elasticity, 4,260 kg/mm² (6,050,000 lb./in.²).
⁶³ Erichsen values.—Semihard, 4.52 mm; hard, 2.75 mm.
⁶⁴ The data refers to the German-made alloy; machining properties very satisfactory.

Compression tests on cylinders 0.31 in. (7.88 mm) in diameter and 0.31 in. (7.88 mm) long.

	Spec. A.	Spec. B.	Spec. C.
Load at compression of 0.5 per cent (yield point).....	4.7	9.5	13.2
Permanent reduction in length at load of 15.8 kg/mm ² (22,400 lb./in. ²).....	6,720	13,450	18,820
Permanent reduction in length at load of 31.5 kg/mm ² (44,800 lb./in. ²).....	3.9	2.0	1.0
Crushing load (fracture occurred by shearing).....	10.1	9.1	7.0
	36.3	35.2	37.7
	51,500	50,000	53,600

⁶⁵ In 0.64 in. (16.27 mm.) = $4\sqrt{\text{area}}$
⁶⁶ 1 mm ball, 10 kg. (22 lb.) load, exterior surface.
⁶⁷ 1 mm ball, 10 kg./cm² (0.7-46.6 ft.-lb./in.²); material is very plastic and at the proper temperature may be given any shape under press. Electron metal is attacked readily in moist air, but in dry places it may be used polished. While in touch with other metals, as iron, which have widely different expansion, it is necessary to protect it with paint.
⁶⁸ 10 mm ball, 250 kg. (551 lb.) load.
⁶⁹ Hot shortness at 1,200° C. (2,192° F.); annealing range, 750-900° C. (1,382-1,652° F.).
⁷⁰ Coefficient of expansion X 10⁶ = 12.8 + 0.0075 t.
⁷¹ Modulus of elasticity, 21,400-23,200 kg/mm² (30,000,000-33,000,000 lb./in.²). Nickel is not corroded easily at ordinary temperatures. Exposed to oxidizing or sulphurizing atmospheres at 1,000-1,200° C. (1,832-2,192° F.), the grain boundaries are attacked and intercrystalline fracture takes place on working. Effect of impurities: (1) Carbon.—Up to the limit of solubility from 0.4 to 0.5 per cent improves hot working properties, but cold working properties are impaired. Carbon lowers melting point; (2) Oxygen.—The presence of oxygen destroys malleability; (3) Manganese.—Improves casting properties, increases strength, increases resistance to oxidation; (4) Sulphur.—Above 0.05 per cent impairs ductility; (5) Iron.—The amount present in nickel is usually less than 1.0 per cent and has no appreciable effect upon its properties; (6) Cobalt.—Soluble in all proportions and in small amounts is without appreciable effect on the properties of nickel; and (7) Silicon.—At a silicon content of 3 to 5 per cent the malleability is completely destroyed.
⁷² These values may be raised by cold working to 250-350 Brinell and 40-45 Scleroscope.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.			Thermal properties.			Reference.		
			Metric kg./mm ²		English lb./in. ²		Reduction of area.	Brinell.	Sclero-scope.	Melting point.	Linear coefficient of expansion $\times 10^6$ (per 1°C.).	Casting shrinkage.					
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.						Yield point.	Tensile strength.	15		16	17
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Nickel—Contd. Pure—Contd. Ni, 98.5 ^{as} Ni, 99.95..... Ni, 98.5.....	Cast..... Wrought, annealed. Wrought, commercial. Rolled hard, commercial. Rolled, annealed, commercial. Drawn hard, 0.065 in. (1.65 mm) diameter.	8.30 8.70	12.6 16.7 26.7 29.9 45.7	16.7 23,800 17,900 65,000	17,900 38,000 42,500 65,000	17,900 38,000 42,500 65,000	23,800 38,000 42,500 65,000	38,000 42,500 65,000	Per ct. 5.7 11.0	Per ct. 6.1 6.1	61.76 61.83	12	14 °C.	15 12.1	16 mm/m	17 in./ft.	(109) (109) (109) (109) (109) (109) (62) (173) (173) (9)
Chromium (nichrome) ⁶⁰ — Ni, Cr..... Iron, chromium, manganese (nichrome) 26— Ni, 60; Fe, 26; Cr, 12; Mn, 2. C h r o m i u m (Hill) ⁶⁶ Ni, 60.65; Cr, 21.07; Cu, 6.42; Mo, 4.67; W, 2.12; Al, 1.00; Si, 1.04; Mn, 0.98; Fe, 0.76. Copper, iron σ — Ni, 71; Cu, 27; Fe, 2. Copper (Monel metal)—	Cast..... Wire..... Drawn, hard.....	8.15 8.15	35.1— 38.7 70.3	50,000— 55,000 100,000	50,000— 55,000 100,000	50,000— 55,000 100,000	50,000— 55,000 100,000	50,000— 55,000 100,000	1	179	179	179	179	16.4			(79)

	8.95			es 162	27	(79)
Rolled, hot.....						
Rods to 1 in. (25.4 mm) diam.	44.4	66.6	63,100	40.0		(79)
Rods 1-1½ in. (25.4-44.4 mm) diam.	43.6	65.5	62,000	39.0		(79)
Rods 1½-2½ in. (44.4-63.5 mm) diam.	35.3	61.7	50,100	42.0		(79)
Rods 2½-3½ in. (63.5-88.8 mm) diam.	30.8	60.0	43,800	44.0		(79)
Rods over 3½ in. (88.8 mm) diam.	33.3	59.6	47,300	43.0		(79)
Rectangles.	39.6	60.2	56,400	42.0		(79)
Hexagons.	42.7	61.8	60,700	40.0		(79)
Cast.....	21.1- 28.1	45.7- 56.2	30,000- 40,000	25-35	es 100- 15-25	(172)
Cold-rolled.....	42.2- 65.3	56.2- 77.4	60,000- 80,000	20-30	180-200	(172)
Sheet, hard.....	65.3- 77.4	77.4- 88.3	80,000- 100,000	1-2	180-200	(172)
Sheet, annealed.	17.6- 24.6	45.7- 57.7	110,000- 125,000	35-45	es 100- 120	(172)
Wire, hard.	63.2	70.2	90,000	1-2		(172)
Wire, annealed.	77.4	84.4	110,000	20-30		(172)
	24.6	52.7	35,000	75,000		(172)
Copper (Monel metal) ₁₀	8.83	26.1				(169)
Ni, 67; Cu, 28; Fe, 2.5; Si, 1.5.						
Ni, min. 60; Cu, min. 23; Fe, max. 3.5; Mn, max. 3.5; Al, max. 0.5; C and Si, max. 2.0.						(208)

es Modulus of elasticity, cast, 20,300 kg/mm² (28,900,000 lb./in.²); modulus of elasticity, drawn hard, 23,900 kg/mm² (34,100,000 lb./in.²). Landolt Börnstein tables (1912) give for the modulus of elasticity in shear 7,800 kg/mm² (11,100,000 lb./in.²) and Poisson's ratio 0.30. Winkelman's Handbuch der Physik, 1908, I, 1 gives for modulus of elasticity in shear 8,600 kg/mm² (12,300,000 lb./in.²).

es At 500 kg (1,102 lb.) load.

es Used for heat-treatment boxes, pyrometer protection tubes, skimming ladles, etc. Nichrome boxes retain their strength and shape at high temperatures and do not warp or bulge. Owing to greater durability they may be of half thickness used for casting Nichrome boxes. Boxes casted in water after while hot (saving time). Was successfully tried for nozzles for injector burners and for picking buckets. Can be readily machined. Tensile strength, cast that of cast iron and about the same hardness.

es As intended to replace platinum, highly resistant to the action of nitric and sulphuric acids; casting and drawing very difficult.

es At approximately proportional limit, 17.9-22.5 kg/mm² (25,500-31,600 lb./in.²).

es At 500 kg (1,102 lb.) load.

es Proportional limit—Castings, 10,577.6 kg/mm² (15,000-25,000 lb./in.²), rods, 24,671.6 kg/mm² (35,000-45,000 lb./in.²). Yield point—Castings, 14,171.1 kg/mm² (20,000-30,000 lb./in.²), rods, 42,776.2 kg/mm² (60,000-70,000 lb./in.²). Shearing strength (rod, 1 in. or 50.8 mm), 3,674.2 kg/mm² (55,000-61,000 lb./in.²).

es Compressive proportional limit, 8.4-17.9 kg/mm² (12,000-25,500 lb./in.²).

es Minimum.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.			Thermal properties.			Reference.			
			Metric kg/mm ²			English lb./in. ²			Brinell.	Sclero- scope.	Melting point.	Linear coeff. of expansion $\times 10^6$ (per 1°C.).	Casting shrink- age.					
			Pro- por- tional limit.	Yield point.	Tensile strength.	Pro- por- tional limit.	Yield point.	Tensile strength.					Elonga- tion in 50.8 mm or 2 inches.	Reduction of area.		Per ct.	Per ct.	Per ct.
1	2	8	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	
Silver: Ag.....	Roiled Annealed.....	29.0 16.0	(97) (97)
Silver, copper— Standard— Ag, 92.5; Cu, 7.5	Cast, in iron mold. Cast, sand.....	⁸⁷ 10.35	6.19 7.4	13.4 12.8	17.2 22.2	8,800 10,570	19,000 18,250	24,500 31,600	6.8 41	15.8 54.6	63 60	⁸⁸ 21 ⁸⁸ 18	(123) (123)
Cadmium(stand- ard) ⁸⁸ — Ag, 92.5; Cu, 5.75; Cd, 1.75.	Cast, in iron mold. Cast, sand.....	⁹⁰ 10.35	2.48 3.58	8.9 9.9	13.3 20.7	3,530 5,090	12,700 14,100	18,900 29,500	9.0 40.0	21.4 49.7	74 73	⁸⁸ 23 ⁸⁸ 22	(123) (123)
Tantalum: ⁹¹ Ta.....	Drawn, hard.....	12.8	93.0	132,300	2,250- 2,300	(137)
Tellurium: ⁹² Te.....	Wire, 0.36 mm or 0.0091 in. diam- eter.	⁸⁹ 6.25	1.15	1,635	⁸⁹ 452	⁸⁹ 16.75	(130)
Tin: Sn.....	Roiled..... Annealed..... Cast..... Rolled..... 7.3 1.13 3.51- 4.01	2.5 1.7 2.46 3.500 1,600	3,550 2,420 3,500	⁸⁹ 232	⁸⁹ 22.34	(97) (97) (109) (109)
Aluminum, zinc, cadmium— Sn, 7; Al, 3; Zn, 8; Cd, 3. Antimony, cop- per, zinc (Brittania metal)	Drawn, hard..... Cast, chill.....	10.1	14,300	18.0	41.0	(109) (169)
Sn, 81; Sb, 16; Cu, 2; Zn, 1. Zinc, aluminum— Sn, 86; Zn, 9; Al, 5.	Cast, chill.....	8.6	12,200	41.0	81.0	(169) (169)

Zinc— Sn, 63; Zn, 18; Al, 13; Cu, 3; Sb, 2; Pb, 1 (aluminum solder).	10.2	14,500	1.9	1.5	(169)
do.....	9.1	13,000	1.6	1.3	(169)

⁸⁶ Charpy impact test (standard to by 10 mm specimen): Energy—Mold cast, 2.21 kgm (16.0 ft.-lb.); sand cast, 1.88 kgm (13.6 ft.-lb.).

Compression tests.

Property.	Cast in iron molds.	Cast in sand.
Yield point.....	20.2	12.3
Load at 5 per cent reduction of length.....	28,800	17,450
Load at 10 per cent reduction of length.....	39,000	19.8
Load at 20 per cent reduction of length.....	47,200	28,200
Load at 40 per cent reduction of length.....	58,500	36,600
	76,100	37.5
		53.5
		49.9
		71,000

⁸⁷ Rolled after annealing.

⁸⁸ Magnifying hammer.

⁸⁹ Charpy impact test (standard to by 10 mm specimen): Energy—Mold cast, 2.74 kgm (19.8 ft.-lb.); sand cast, 2.40 kgm (17.4 ft.-lb.).

Compression tests.

Property.	Cast in iron molds.	Cast in sand.
Yield point.....	11.0	10.7
Load at 5 per cent reduction of length.....	15,600	15,250
Load at 10 per cent reduction of length.....	18.3	17.4
Load at 20 per cent reduction of length.....	23.8	24,800
Load at 40 per cent reduction of length.....	33,800	32,300
	35.8	37.8
	51,000	53,900
	60.1	51.7
	83,300	73,600

⁹⁰ Rolled after annealing.

⁹¹ Modulus of elasticity, 19,000 kg/mm² (27,000,000 lb./in.²) (Landolt-Börnstein, Physikalisch-Chemische Tabellen, 1912). Pure tantalum can be hammered into thin sheets or drawn into fine wire. It has hardness of soft steel. At ordinary temperatures (below 300° C. or 572° F.) pure tantalum resists action of all acids except fluoric acid.

⁹² Modulus of elasticity, 4,180 kg/mm² (5,950,000 lb./in.²); modulus of elasticity in shear, 1,570 kg/mm² (2,230,000 lb./in.²).

⁹³ Smithsonian Physical Tables, 7th edition, 1920.

⁹⁴ Compressive strength, cast, 4.22 kg/mm² (6,000 lb./in.²). Landolt-Börnstein Physikalisch-Chemische Tabellen, Berlin, 1912, give for: Modulus of elasticity, 4,000-5,500 kg/mm² (5,680,000-7,820,000 lb./in.²); modulus of elasticity in shear, 1,700 kg/mm² (2,420,000 lb./in.²).

⁹⁵ Smithsonian Physical Tables, 7th edition, 1920.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.				Thermal properties.			Reference.	
			Metric kg./mm ²		English lb./in. ²		Elongation in 50.8 mm or 2 inches.	Reduction of area.	Brinell.	Scleroscope.	Melting point.	Linear coefficient of expansion $\times 10^6$ (per 1°C.).	Casting shrinkage.				
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.							Yield point.	Tensile strength.	mm/m		in./ft.
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Tin—Continued. Antimony, copper (white metal bearing alloys), ⁸⁹ and lead. ⁹⁰ Thallium; ⁸⁸ Ti.		4.5							Per ct.	Per ct.			°C.				
Tungsten; ⁸⁹ W	Ingot sintered 0.20-0.25 in. (5.08-6.35 mm) diam. Rod swaged 0.026 in. (0.56 mm) diam. Drawn wire 0.00114 in. (0.029 mm) diam.	18.0			12.7			18,000	0	0			1,800-1,850 (3,272-3,362°F.)				(97)
					151.0			215,000	4.0	28.0							(10)
					415.0			590,000		65.0			3,540±30 (6,404°F. ± 54)				(10)
														(1)			(131)
																	(132)

⁸⁸ Properties of White Metal Bearing Alloys*—Experimental Results.

Alloy No.	Formula.				Pouring temperatures.		Specific gravity.	Permanent deformation at 21° C. (70° F.).				Brinell hardness at 500 kg (1,102 lb.).		
	Sn	Sb	Cu	Pb	°C.	°F.		At 454 kg=5,000 lb.		At 4,536 kg=10,000 lb.				
	Per cent.	Per cent.	Per cent.	Per cent.			mm	in.	mm	in.				
1.	91.0	4.5	4.5		440	824	0.000	0.0000	0.025	0.0010	0.380	0.0150	At 21° C. (70° F.).	28.6
21.	89.0	7.5	3.5		432	808	0.000	0.0000	0.038	0.0015	0.305	0.0120	At 100° C. (212° F.).	28.3

3.....	83.3	8.3	8.3	491	916	7.46	.025	.0010	.114	.0045	.178	.0070	34.4	13.7
4.....	75.0	12.0	3.0	10.0	360	680	7.52	.013	.0005	.064	.0025	.229	.0050	29.6	12.8
5.....	65.0	15.0	2.0	18.0	380	661	7.75	.025	.0010	.076	.0050	.229	.0090	29.6	11.8
Lead base.															
6.....	20.0	15.0	1.5	63.5	337	638	9.33	.038	.0015	.127	.0050	.457	.0180	24.3	11.1
7.....	10.0	15.0	75.0	329	625	9.73	.025	.0010	.127	.00500230	24.1	11.7
8.....	5.0	15.0	80.0	329	625	10.04	.051	.0020	.229	.0090	1.583	.0620	26.9	10.3
9.....	5.0	10.0	85.0	324	616	10.24	.102	.0040	.305	.0120	2.130	.0840	19.5	8.6
10.....	2.0	15.0	82.0	329	625	10.07	.025	.0010	.254	.0100	3.910	.1540	17.0	8.9
11.....	15.0	85.0	329	625	10.28	.025	.0010	.254	.0100	3.020	.1190	17.0	9.4
12.....	10.0	90.0	334	634	10.67	.064	.0025	.432	.0170	7.240	.2850	14.3	6.4

*Babbitt metal. A. S. T. M. 18, 1, p. 491. Experimental permanent deformation values from compression tests on cylinders 31.8 mm (1¼ in.) diameter by 63.5 mm (2½ in.) long, tested at 21° C. (70° F.). (See readings after reaming loads.)
 † U. S. Navy specification 4632b (Cu, 3-4.5; Sn, 88-89.5; Sb, 7.0-8.0) covers manufacture of antifriction metal castings (composition W).

⁶⁷ Properties of antifriction bearing metals. P. W. Priestley, Met. Ind. (London), 18, p. 323; 1921. 1. Essential characteristics.—The most desirable alloy is one having hard grains embedded in soft material. The function of hard constituent—to resist wear and to provide surface with low coefficient of friction. The softer constituent permits uniform distribution of load and promotes efficient lubrication by leaving the particles of hard constituent in slight relief. Good bearing metal must have proper amount of both constituents. 2. Composition.—Typical composition of antifriction metals employed in construction of aircraft and automobile engines.

Alloy No.	Application.	Sn	Sb	Cu	Pb	Miscellaneous.	Alloy No.	Application.	Sn	Sb	Cu	Pb	Miscellaneous.
1.....	Aircraft, American.....	91.00	4.00	3.50	1.00	0.50	4.....	Aircraft, German.....	80.71	10.05	6.95	2.26	0.03
2.....	Aircraft, British.....	90.72	5.33	3.8015	5.....	Automobile, American.....	84.00	9.00	7.00
3.....	Aircraft, French.....	90.15	3.90	4.8088	6.....	Automobile, British.....	86.00	10.50	3.2525

3. Influence of constituents.—(a) Antimony.—Increases hardness, wearing qualities, and brittleness. (b) Bismuth.—Traces of it may be introduced as a flux. (c) Copper.—Prevents segregation, increases hardness, but in quantities exceeding 5 per cent promotes brittleness. (d) Iron.—Increases hardness and brittleness; is considered undesirable. (e) Lead.—In small quantities (up to 3 per cent) is permissible. Lubricants containing excess of alkali will pit lead rich alloys. (f) Tin.—Improves wearing qualities. Tin-rich alloys are most successful under severe working conditions. (g) Nickel.—In quantities over 0.50 per cent removes liability to cracking without affecting hard wearing qualities. (h) Zinc.—Increases hardness and brittleness, creates a tendency to seize; considered undesirable. 4. Mechanical tests.—There is no direct relationship between the compressive strength, hardness, coefficient of friction, and durability factor. Mechanical tests are of little value. 5. Heat treatment.—Unnecessary in small bearings. It is advisable to heat large bearings to 150° C. (302° F.) and quench in water in order to eliminate the segregation of antimony-rich cuboids.
 For effect of Ti on strength and ductility of steels see Zeitschrift des Vereines der Deutschen Ingenieure, p. 897; 1908.
⁶⁸ Modulus of elasticity of drawn wire, 36,200 kg/mm² (51,400,000 lb./in.²), after Dodge. Ordinary annealing treatment makes W brittle and severe working below recrystallization or equipping temperature produces ductility. Tungsten rods which have been worked and recrystallized are stronger than sintered rods. The equipping temperatures of worked tungsten with a 5-minute exposure vary in 2,200° C. (3,992° F.) for a worked rod with 24 per cent reduction to 1,350° C. (2,402° F.) for a fine wire with 60 per cent reduction. Coefficient of expansion at 27° C. (81° F.)—0.000044; coefficient of expansion at 1,027° C. (1,886° F.)—0.0000519; coefficient of expansion at 2,027° C. (3,686° F.)—0.000076. Tungsten has the lowest known coefficient of expansion except diamond and molybdenum.

TABLE 1.—Tensile and Thermal Properties of Metals—Continued.

Material and composition.	Condition.	Specific gravity.	Tensile properties.						Hardness number.			Thermal properties.			Relevance.		
			Metric kg./mm ²		English lb./in. ²		Elongation in 50.8 mm or 2 inches.	Reduction of area.	Brinell.	Sclero-scope.	Melting point.	Linear coefficient of expansion ×10 ⁶ (per 1° C.).	Casting shrinkage.				
			Proportional limit.	Yield point.	Tensile strength.	Proportional limit.								Yield point.		Tensile strength.	
1	2	8	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Tungsten—Contd.																	
W ²	Wire 5 mm (0.197 in.) diam.				324.0												
	Wire 1.2 mm (0.047 in.) diam.				408.0												
	Rolled sheets	19.3-21.4			352.0 322-427												
Uranium: ⁶		18.7															
U ⁷																	
Vanadium:		5.5															
V ⁸																	
Zinc: ⁹		7.09															
Zn	Cast.			3.4													
	Rolled.			6.3													
	Annealed.			7.5													
Zn ⁷	Rolled; tested parallel to direction of rolling.		0.5	8.0	21.4	710	11,400	30,400	27.2	43			1,850				(116a)
Zn, Pb, 0.021-1.04; Cd, 0.03-0.91; Fe, 0.025 ⁹	Rolled; tested perpendicular to direction of rolling.			9.6	25.9	1,280	13,640	36,800	9.7	17			1,680				(97)
Zn ⁹	Rolling plate (0.019-0.22 in. (0.48-5.66 mm); parallel to direction of rolling.				18.3-10.0								419	26			
	Rolled, plate (0.019-0.22 in. (0.48-5.66 mm); perpendicular to direction of rolling.				22.4-14.2												
Zn, impur. Pb, Fe, Cd. ¹⁰	Cast, coarse, crystalline. ¹¹	7.0			2.8			4,000			12.42	8					(96)

Zirconium: ¹⁶ Zr.....	Cast, fine, crys- talline, ¹¹	8.4	12,000	12,48	10	(96)
	Rolled ^{11, 13}	19.0	27,000			(96)
	Do, ^{11, 14}	25.3	36,000			(96)
	Drawn, hard ¹⁵	7.1	25,000		1,530	(96)
		6.4				(54)

² Tungsten is not affected by air or water at temperatures below red heat.

³ Modulus of elasticity, 42,200 kg/mm² (60,000,000 lb./in.²).

⁴ Mohs' scale.

⁵ Zr is a lustrous white metal; burns brilliantly at 170° C. (338° F.) though unattacked by air at normal temperatures. Metal decomposes in boiling water; struck with hard substance emits copious sparks. Chief use—in high-grade steels. Uranium steel is claimed to be superior to most other alloy steels. Zr hardens steel without imparting brittleness. In high-speed steel Zr tends to promote the formation of carbides upon which the property of "red-hardness" depends. (The Metal Industry, 20, Jan. 6, 1922.)

⁶ Bluish-white metal unaffected at ordinary temperatures in dry air, but tarnishes in damp air; annealing temperature 100° C. (212° F.).

⁷ Effect of temperature on tensile properties of zinc.—Haines in 1911 found that at 86-90° C. (176-194° F.) impure metal became remarkably soft, as well as at 130° C. (302° F.). At 110° C. (230° F.) it was as hard as at 30° C. (86° F.) and more brittle. Pure zinc showed no changes at 100° C. (212° F.), but hardened at 200° C. (392° F.). Moore in 1915 made tensile tests of sheets from 1.0-2.000 in. (.25-.4-0.15 mm.). No analysis given. Metal stronger across the grain, but more ductile with the grain than across it. Modulus of elasticity, 8,360 kg/mm² (11,500,000 lb./in.²). Miss Bingham in 1920. Pure zinc annealed. Tensile strength fell steadily from 10.9 kg/mm² (24,000 lb./in.²) at 16° C. (50° F.); sharp inflection at 130° C. (336° F.), marking rise of tensile strength. The elongation was at first 60 per cent., two maximums at 106° C. (330° F.) and 186° C. (356° F.). For quenched metal the elongation rose steadily from 30 per cent. at 42° per cent. at 100° C. (212° F.). At 186° C. (356° F.) there was a sudden fall from 33 to 19 per cent.

⁸ Effect of temperature on tensile properties of zinc.—Kose in 1912 had found the sclerochrome hardness (magnifying hammer) of cast metal, 12.5; rolled, 36. On annealing the hardness was 32 at 150° C. (302° F.), 140 at 170° C. (336° F.), and fell slowly to 7.5 at 100° C. (212° F.). Beyond 100° C. (212° F.) the effect was very small. Mathewson, Irwin, and Binkley, in 1928: (a) Sclerochrome hardness of rolled metal, 28.4; softened at 75° C. (167° F.); completely softened (hardness 15) when annealed one hour at 100° C. (212° F.). Higher temperature had no further effect. (b) Medium zinc rolled. Sclerochrome hardness 24; began to soften at 100° C. (212° F.), and was completely softened at 125° C. (337° F.) (hardness 14). (c) Annealing of soft and dead stock material gave only a slight drop in hardness.

⁹ Results of the investigation by D. H. Ingeall.—(a) Absolute values for mechanical properties of rolled zinc are not obtainable, as material is variable: (b) rolled zinc is stronger reduction by rolling; (c) ductility of pure-rolled zinc with 77-86 per cent has a tensile strength of 9.5 kg/mm² (21,500 lb./in.²) which rises to 21.1 kg/mm² (50,000 lb./in.²) with 96 per cent reduction by rolling; (d) ductility of pure-rolled zinc with 77-86 per cent reduction is 80 per cent along and 90 per cent across rolling. Beyond 88 per cent reduction the ductility rises sharply until at 96 per cent reduction material is quite ductile in either direction; and (e) annealing at 200° C. (392° F.) makes pure-rolled zinc weak and brittle.

¹⁰ Modulus of elasticity. Parallel to direction of rolling, 9,910 kg/mm² (22,800,000 lb./in.²), perpendicular to direction of rolling, 10,200 kg/mm² (24,500,000 lb./in.²), Landolt-Börnstein tables (1912) give for the modulus of elasticity in shear, 4,000 kg/mm² (5,600,000 lb./in.²).

¹¹ Tensile strength depends to a great extent upon the rate of loading: In tests lasting 6 minutes the tensile strength was 20.5 kg/mm² (49,100 lb./in.²); in tests lasting 81 minutes the tensile strength was 16.4 kg/mm² (23,300 lb./in.²).

Effect of Temperature on Tensile Properties.

Temperature.		Tensile strength.		Elonga- tion.		Temperature.		Tensile strength.		Elonga- tion.	
°C.	°F.	kg/mm ²	lb./in. ²	Per cent.	Per cent.	°C.	°F.	kg/mm ²	lb./in. ²	Per cent.	Per cent.
27	81	14.5	20,600	12.4	150	302	4.1	5,790	101.5	101.5	101.5
80	176	8.8	12,500	29.4	170	338	5.6	7,960	17.1	17.1	17.1
120	248	6.3	8,960	59.4	200	392	4.3	6,120	7.2	7.2	7.2

¹² Zinc either rolled or cast has no well-defined yield point and its elastic limit is very low. Zinc possesses a high degree of plasticity. Modulus of elasticity: Cast, 7,750 kg/mm² (17,025,000 lb./in.²); rolled, 8,450 kg/mm² (20,000,000 lb./in.²). Compression, load on cylinder 2.54 mm or 1 in. by 96.0 mm (2.6 in.) at 20 per cent deformation: Cast, free from Cd, 17.3 kg/mm² (24,500 lb./in.²); cast, with Cd, 0.26-27.4 kg/mm² (39,000 lb./in.²). Proc. A. S. T. M., 18, p. 688. Modulus of rupture averages twice the corresponding tensile strength. Shearing strength, rolled, averages 13.6 kg/mm² (19,400 lb./in.²).

¹³ Marks Mech. Eng. Handbook, p. 577; 1916.

¹⁴ The steel was grain oriented.

¹⁵ Tested along grain or direction of rolling.

¹⁶ B. S. Circular No. 108.

¹⁷ Zirconium steel was proposed for armor plates and as self-hardening tool steel. Aluminum-zirconium has about the same properties as aluminum-titanium. Zr is used as a refractory in form of oxide-zirconia. Fused zirconia has a very low coefficient of expansion—0.000084 per 1° C.—near that of quartz glass. Its mineralogical hardness is between that of corundum and quartz; specific gravity, 5.89; melting point, 2,950° C. (5,342° F.).

TABLE 16.—Correlation Between the Tensile Strength of Steel, and its Hardness.¹

Steel.	Tensile strength in terms of Brinell hardness number.	Tensile strength in terms of scleroscope hardness.	Brinell hardness in terms of scleroscope hardness.	Steel.	Tensile strength in terms of Brinell hardness number.	Tensile strength in terms of scleroscope hardness.	Brinell hardness in terms of scleroscope hardness.	
Carbon steel.....	th. lb./in. ² 0.73 Bhn.—28	th. lb./in. ² 4.4 Scl.—28	5.6 Scl.+14	Steel.	th. lb./in. ² 0.68 Bhn.—22	th. lb./in. ² 3.7 Scl.—1	5.4 Scl.+33	
Nickel steel.....	.71 Bhn.—32	3.5 Scl.—6	5.0 Scl.+48		Low chrome-nickel steel.....	.71 Bhn.—33	3.7 Scl.—1	4.8 Scl.+36
Chrome-vanadium steel.....	.71 Bhn.—29	4.2 Scl.—21	5.5 Scl.+27		High chrome-nickel steel.....			

¹ After R. Abbott, Proc. Am. Soc. Test. Mat., 15 (2); 1915.

TABLE 17.—Impact Properties of Some Metals.¹

[Bureau of Standards results, 1923.]

Material and composition.	Energy absorbed.				Tensile properties.					
	Notch parallel to the plane of rolling.		Notch perpendicular to the plane of rolling.		Yield point.		Tensile strength.		Elongation in zin. (50.8 mm).	Reduction of area.
	kgm	ft.-lb.	kgm	ft.-lb.	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	Per ct.	Per ct.
Duralumin: Cu, 4.0; Si, 0.54; Fe, 0.58; Mn, 0.58; Mg, 0.60; Al, balance	1.47	10.60	1.06	7.64	29.6	42,200	42.9	61,100	15.8	17.6
Brass (hard): Cu, 65.23; Zn, 34.67; Pb, 0.07; Fe, 0.03	2.69	19.45	2.65	19.15	29.2	41,600	36.9	52,500	39.8	51.3
Nickel silver: Cu, 63.92; Ni, 18.09; Zn, 17.58; Mg, 0.24; Fe, 0.15; Pb, 0.02	2.32	16.82	2.31	16.74	41.3	58,800	45.5	64,800	18.5	35.8
Monel metal: Ni, 67.2; Cu, 27.5; Fe, 2.55; Mn, 2.27; C, 0.27; Si, 0.13; S, 0.014	12.89	93.35	10.41	75.30	28.2	40,200	62.1	88,400	47.3	62.0
Carbon steel (boiler plate): C, 0.25; Mn, 0.50; Si, 0.01; P, 0.007; S, 0.035	2.26	16.33	2.10	15.22	25.1	35,800	44.0	62,600	37.5	57.2
3½ per cent nickel steel: C, 0.44; Si, 0.24; Mn, 0.63; S, 0.027; P, 0.009; Ni, 3.50	3.48	25.15	3.52	25.48	56.2	80,000	85.0	121,000	19.8	49.6
Carbon tool steel: C, 1.00; Mn, 0.24; Si, 0.20; S, 0.025; P, 0.013	0.32	2.29	0.29	2.13	29.2	41,600	53.8	76,600	31.0	45.5
Chromium-tungsten tool steel: C, 0.88; Mn, 1.15; Si, 0.26; S, 0.007; P, 0.010; Cr, 0.50; W, 0.40	1.84	13.33	1.82	13.18	(?)

¹ The materials were as received from the mill. The specimens were 10 by 10 mm with 2 mm V-notch and were tested in an Izod machine of 120 ft.-lb. (16.6 kgm) capacity. They were cut in the direction of rolling.

² Bhn.=175.

TABLE 18.—Impact Properties of Carbon Steel.

[F. C. Langenberg, Chem. and Met. Eng., November 16, 1921.]

[Chemical composition and Charpy values $\frac{\text{kgm}}{\text{ft.-lb.}}$ of heat-treated bar stock.]

Chemical Composition.						Heat Treatment.							
C	Mn	S	P	Si	Cr	Original.	V ₁	V ₂	V ₃	V ₄	V ₅	V ₆	V ₇
0.14	0.45	0.035	0.018	0.131	6.28	3.88	5.27	6.52	6.63	6.85	6.69	7.27
.18	.56	.043	.024	.132	45.39	28.01	38.10	47.18	47.95	49.50	48.34	52.61
.32	.51	.027	.009	.128	5.74	4.26	4.94	6.39	6.22	6.17	6.49	6.98
.46	.40	.050	.020	.144	41.51	30.72	35.69	46.24	45.00	44.62	46.87	50.51
.49	.60	.028	.013	.127	3.18	2.11	1.51	2.61	2.66	2.75	3.09	3.64
.57	.65	.028	.012	.167	22.98	15.20	10.94	18.85	19.24	19.86	22.34	26.30
.71	.67	.025	.027	.147	3.17	1.11	1.94	1.93	1.92	2.17	2.30
.83	.55	.028	.018	.152	10.70	7.99	14.04	13.96	13.89	15.67	16.60
1.01	.39	.029	.016	.160	1.76	1.43	2.22	2.01	1.98	2.42	2.66
1.22	.34	.031	.025	.181	12.72	10.32	16.06	14.51	14.35	17.53	19.24
1.39	.20	.029	.015	.191	1.16	1.10	1.74	1.50	1.55	1.66	1.94
1.46	.20	.035	.011	.133	0.35	8.38	7.91	12.57	10.86	11.17	12.02	14.04
						.61	.34	6.5	1.05	1.42	2.17
						4.42	2.48	4.73	7.60	10.32	15.67
						.18	.1947	.46	.60	.88
						1.31	1.39	3.42	3.33	4.34	6.36
						.29	.2045	.44	.58	.61
						2.09	1.47	3.25	3.18	4.19	4.42
						.19	.1834	.29	.36	.36
						1.39	1.31	2.48	2.09	2.63	2.63
						.13	.1227	.18	.20	.22
						.93	.85	1.86	1.31	1.47	1.62
						.11	.1727	.28	.28	.27
						.77	1.24	1.94	2.01	2.01	1.94

Heat treatments.—Original, as received; V₁, annealed just above A₃; V₂, hardened in water from just above A₃; V₃, hardened in oil from just above A₃; V₄, quenched in oil from just above A₃ and drawn at 375° C. (707° F.); V₅, quenched in oil from just above A₃ and drawn at 460° C. (860° F.); V₆, quenched in oil from just above A₃ and drawn at 560° C. (1,040° F.); V₇, quenched in oil from just above A₃ and drawn at 650° C. (1,202° F.).

TABLE 18.—Impact Properties of Carbon Steel—Continued.

Quenching Temperatures.

Carbon content.	°C.		Carbon content.	°C.		Carbon content.	°C.		Carbon content.	°C.	
	°F.	°F.		°F.	°F.		°F.	°F.			
0.14	866	1,591	0.46	819	1,506	0.71	800	1,472	1.22	790	1,454
.18	858	1,576	.49	816	1,501	.83	795	1,463	1.39	790	1,454
.32	836	1,537	.57	809	1,488	1.01	790	1,454	1.46	790	1,454

TABLE 19.—Effect of Low Temperatures on Hardness and Impact Resistance of Metals.¹

[L. Guillet and J. Cournot, *Revue de Metallurgie*, April, 1922.]

[Hardness tests were made with a 10 mm ball and 1,000 kg (2,204 lb.) load. For Ni, Cr steel the load was 3,000 kg (6,612 lb.) and for cobalt 500 kg (1,102 lb.); time, 10 sec. The impact tests were made in a Guillery rotary machine on Mesnager type of specimens.]

Metals and alloys tested.	Brinell hardness.				Impact resistance $\frac{\text{kgm}}{\text{ft.-lb.}}$			
	+20° C.	-20° C.	-80° C.	Liquid air.	+20° C.	-20° C.	-80° C.	Liquid air.
	(68° F.).	(-4° F.).	(-112° F.).		(68° F.).	(-4° F.).	(-112° F.).	
Electrolytic iron, annealed.....	80	77	77	269	21.2	17.5	2.5	1.9
Soft steel, annealed, C, 0.1.....	110	107	114	273	153.3	126.5	18.1	13.7
Medium steel, C, 0.33, annealed.....	176	174	190	286	31.9	32.5	22.5	1.8
Hard steel, C, 0.79, annealed.....	230	230	231	330	230.7	235.1	162.7	13.0
Cemented nickel steel, C, 0.06; Ni, 2.30; annealed.	130	132	135	230	13.1	11.2	10.0	3.7
Nickel-chromium steel, C, 0.11; Ni, 5.74; Cr, 1.74; annealed.	251	269	282	388	94.8	81.0	72.3	26.8
Nickel-chromium steel, C, 0.25; Ni, 4.25; Cr, 1.20; quenched in air.	450	466	444	578	104.2	81.0	72.3	26.8
Ferronickel (Ni, 36.8 p. c.), annealed.....	157	171	239	31.2	31.2	23.1	3.1
Ferronickel (Ni, 47.0 p. c.), annealed.....	184	192	238	225.8	225.8	167.1	22.4
Ferronickel (Ni, 57.4 p. c.), annealed.....	197	212	240	11.8	7.5	3.1	1.9
Ferronickel (Ni, 98.8 p. c.), annealed.....	98	103	120	85.3	54.2	22.4	13.7
Cobalt.....	174	222	11.2	10.0	11.2	10.0
Copper (pure), Cu, 99.9.....	51	52	53	66	81.0	72.3	81.0	72.3
Brass, Cu, 52.0; Zn, 42.5; Ni, 4.0; Pb, 1.3....	118	114	118	148	² 41.2	² 36.2	17.5
Brass, Cu, 60.4; Zn, 39.3; Pb, 0.2.....	76	76	76	98	298.0	262.0	126.5
Aluminum, commercial, Si, 0.25; Fe, 0.06....	24	25	24	53	32.5	29.4	29.4
Duralumin, Cu, 3.6; Mn, 0.5; Si, 0.6; Fe, 0.6; Mg, 0.5.	101	96	101	129	235.1	212.6	212.6
Aluminum-zinc (Zn, 15 p. c.).....	55	47	48	76	26.2	² 35.0	31.8
Aluminum-zinc (Zn, 30 p. c.).....	129	137	121	192	189.5	253.2	230.0
Aluminum-zinc-lead (Zn, 15.0; Pb, 1.5).....	55	51	49	83	² 47.5	² 46.2	² 40.6
					343.5	334.2	293.6
					² 20.6	² 18.7	² 20.6	² 20.1
					149.0	135.3	149.0	145.4
					8.1	7.5	8.8	6.9
					58.6	54.2	63.6	49.9
					16.2	16.2	17.5	16.8
					117.2	117.2	126.5	121.5
					11.2	10.6	11.2	13.1
					81.0	76.7	81.0	94.8
					5.0	5.6	5.0	5.6
					36.1	40.5	36.1	40.5
					11.2	11.2	10.0	9.3
					81.0	81.0	72.3	67.3
					2.5	2.5	1.9	1.8
					18.1	18.1	13.7	13.0
					10.0	10.0	10.0	8.1
					72.3	72.3	72.3	58.6

¹ For tensile strength and ductility at low temperatures of various metals and ferrous alloys see J. Dewar and R. Hadfield, *Proc. Roy. Soc. of London*, 74, p. 325; 1904-5. See also "Hardness of steels at low temperatures," by M. Robin, *Revue de Metallurgie*, p. 162; 1909.

² Specimen not broken.

TABLE 20.—Effect of Temperature on the Impact Resistance of Annealed Steels. (See fig. 60.)

[Proc. Interna. Assoc. for Testing Materials, 5th Congress, Vol. 3, 4.]

Chemical composition of tested steels.

Steel.	C	Si	Mn	S	P	Annealing treatment in air at temperature—	
						°C.	°F.
Extra soft.....	Per cent. 0.218	Per cent. 1.26	Per cent. 0.24	Per cent. 0.041	Per cent. 0.013	850	1,562
Soft.....	.345	.20	.51	.048	.068	800	1,472
Half hard.....	.491	.44	.34	.044	.062	800	1,472
Martin (hard).....	.725	.40	.33	.025	.013	750	1,382
Tool.....	1.224	.05	.04	.040	.023	700	1,292
2 per cent Ni.....	.085	.01	.15	.017	Ni=2.29	890	1,562
7 per cent Ni.....	.165	.13	.20	Ni=7.10	600	1,112
Nickel chrome.....	.105	.11	.34	Ni=4.38	Cr=0.85	750	1,382

TABLE 21.—Fatigue Properties of Manganese and Aluminum Bronze. (See fig. 14.)

[W. Corse and G. Comstock, Proc. A. S. T. M., vol. 16 (2), p. 117; 1916.]

Chemical Composition and Tensile Properties of Tested Samples.

Material.	Chemical composition.	Proportional limit.		Tensile strength.		Elongation in 50.8 mm or 2 in.	Reduction of area.
		kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²		
Manganese bronze (cast).	Zn,41.0; Fe,1.0; Sn,1.0; Mn, 0.5; Al,0.5; Cu, balance.	20.5	29,200	61.4	87,400	Per cent. 25.0	Per cent. 25.2
Aluminum bronze (cast)	Al,10.0; Fe,1.0; Cu, balance....	14.3	20,400	54.0	76,900	30.5	27.6
Aluminum bronze (quenched at 850° C. or 1,562° F.; tempered at 630° C. or 1,116° F.).	Al,10.0; Fe,1.0; Cu, balance.....	30.4	43,300	62.2	88,500	13.0	14.2

XII. FATIGUE PROPERTIES OF STEEL.

SUMMARY.

A. [D. J. McAdam, jr., Chem. and Met. Eng., December 14, 1921.]

[See figures 33 to 35.]

1. The endurance stress for 100,000,000 cycles bears no definite relation to the corresponding proportional limit. The ratio is higher in annealed material than in quenched and tempered material. In ingot iron and annealed mild steels of lower carbon content the endurance stress for 100,000,000 cycles is above the proportional limit. In quenched and tempered steel it is often less than half the proportional limit.

2. The endurance stresses for 100,000,000 cycles have been found to bear a surprisingly uniform relation to the corresponding ultimate tensile stresses. In many kinds of material investigated this ratio varies from about 0.35 to 0.54, the highest value being found in ingot iron.

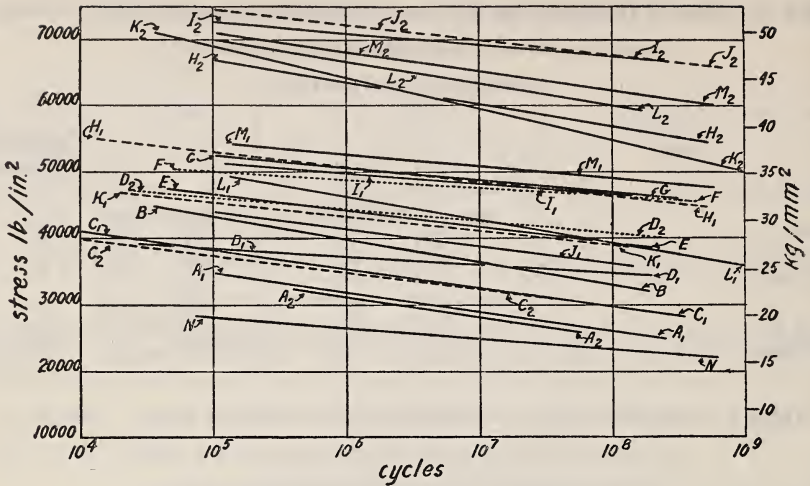


FIG. 33.—Fatigue properties of carbon and alloy steels.

D. J. McAdam, Chem. and Met. Eng., Dec. 14, 1921. For the chemical composition and heat treatment see Table 22. Tests were made in a White-Souther machine on tapered specimens.

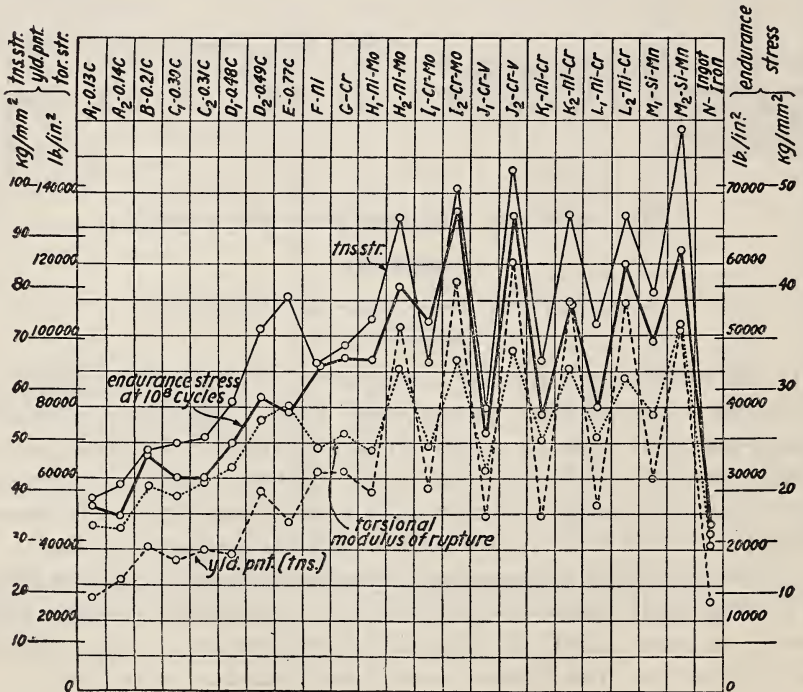


FIG. 34.—Fatigue properties of carbon and alloy steels compared with other properties.

D. J. McAdam, Chem. and Met. Eng., Dec. 14, 1921. For the chemical composition and heat treatment of steels see Table 22.

3. The ratio of endurance stress to Brinell hardness number, and the ratio of endurance stress to maximum torsional stress are nearly as uniform as the ratio of endurance stress to ultimate tensile stress.

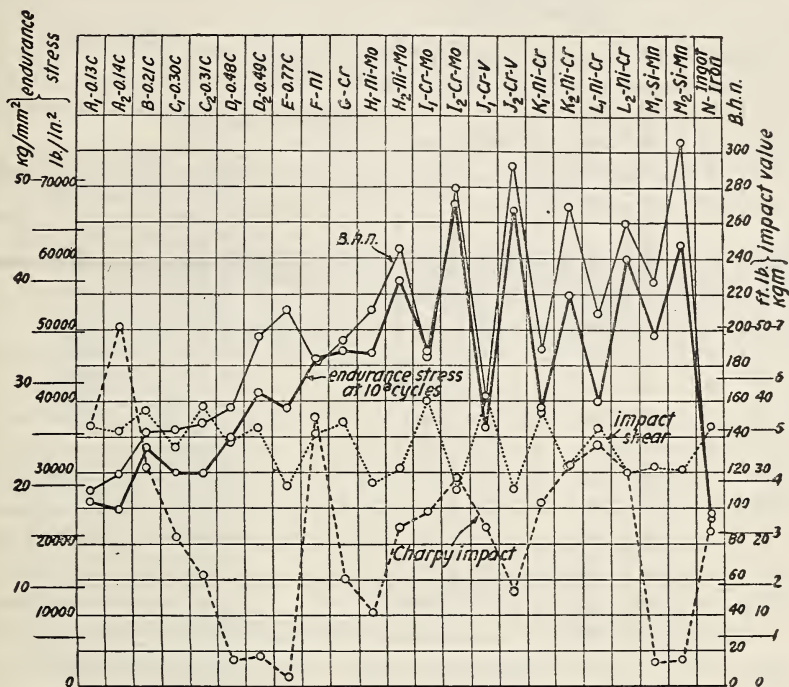


FIG. 35.—Fatigue properties of carbon and alloy steels compared with other properties.

D. J. McAdam, Chem. and Met. Eng., Dec. 14, 1921. For the chemical composition and heat treatment of steels see Table 22.

4. Until further evidence accumulates it may be stated that chemical composition has little effect on endurance properties other than its effect on tensile strength.

5. A comparison of impact test results with the results of endurance tests so far has shown no definite relationship.

TABLE 22.—Fatigue Properties of Carbon and Alloy Steels. (See figs. 33–35.)

[D. J. McAdam, Chemical and Metallurgical Engineering, December 14, 1921.]

Chemical Composition and Heat Treatment of Tested Steels.

Material.	Chemical composition.									Heat treatment.
	C	Mn	P	S	Si	Ni	Cr	V	Mo	
A ₁	0.13	0.56	0.008	0.047	0.17	Annealed at 732° C. (1,350° F.).
A ₂14	.53	.008	.056	.17	As, 0.010	As rolled.
B.....	.21	.82	.060	.080	.08	0.206	0.017	Do.
C ₁29	.52	.010	.051	.17	Annealed at 649° C. (1,200° F.).
C ₂31	.47	.013	.030	.16	Quenched in oil at 830° C. (1,525° F.) and annealed at 649° C. (1,200° F.).
D ₁48	.60	.010	.038	.19	Annealed at 732° C. (1,350° F.).
D ₂49	.63	.011	.036	.18	Quenched in oil at 871° C. (1,600° F.) and annealed at 621° C. (1,150° F.).
E.....	.77	.55	.037	.047	.18	Annealed at 732° C. (1,350° F.).
F.....	.29	.66	.005	.046	.14	3.70	To approximate proportional limit of 60,000 lb./in. ² (42.2 kg/mm ²).
G.....	.21	.59	.017	.017	.79	.13	13.31	To approximate proportional limit of 60,000 lb./in. ² (42.2 kg/mm ²).
H ₁41	.45	.037	.020	.20	1.7213	To approximate proportional limit of 60,000 lb./in. ² (42.2 kg/mm ²).
H ₂42	.47	.038	.020	.25	1.6812	To approximate proportional limit of 110,000 lb./in. ² (77.4 kg/mm ²).
I ₁40	.52	.033	.024	.2695	To approximate proportional limit of 60,000 lb./in. ² (42.2 kg/mm ²).
I ₂42	.53	.032	.023	.25	1.0409	To approximate proportional limit of 110,000 lb./in. ² (77.4 kg/mm ²).
J ₁24	.30	.046	.044	.29	1.73	1.16	0.23	To approximate proportional limit of 60,000 lb./in. ² (42.2 kg/mm ²).
J ₂53	.50	.005	.038	.22	1.46	.23	To approximate proportional limit of 110,000 lb./in. ² (77.4 kg/mm ²).
K ₁43	.63	.012	.038	.22	.47	1.10	To approximate proportional limit of 60,000 lb./in. ² (42.2 kg/mm ²).
K ₂41	.64	.009	.033	.20	1.45	1.10	To approximate proportional limit of 110,000 lb./in. ² (77.4 kg/mm ²).
L ₁33	.47	.007	.052	.18	3.18	.96	To approximate proportional limit 60,000 lb./in. ² (42.2 kg/mm ²).
L ₂33	.46	.006	.051	.19	3.16	.95	To approximate proportional limit of 110,000 lb./in. ² (77.4 kg/mm ²).
M ₁55	.65	.024	.037	1.97	To approximate proportional limit of 60,000 lb./in. ² (42.2 kg/mm ²).
M ₂51	.66	.029	.045	1.96	To approximate proportional limit of 110,000 lb./in. ² (77.4 kg/mm ²).
N.....	.023	.037	.002	.031	.005	As rolled.

B. [H. F. Moore, Ill. U. Eng. Exp. Sta. Bul. No. 124, p. 132; 1921.]

(See figs. 36 and 37.)

The following conclusions were drawn from the results obtained in the investigation:

1. For the metals tested under reversed stress there was observed a well-defined critical stress at which the relation between stress and the number of reversals necessary to cause failure changed markedly. Below this critical stress the metals withstood 100,000,000 reversals of stress and, so far as can be predicted from test results, would have withstood an indefinite number of such reversals. The name *endurance limit* has been given to this critical stress.

2. In the reconnaissance tests made in the field of ferrous metals no simple relation was found between the endurance limit and the "elastic limit," however determined. The ultimate tensile strength seemed to be a better index of the endurance limit under reversed stress than was the elastic limit. The Brinell hardness test seemed to furnish a still better

index of the endurance limit. The reason why the Brinell test and, to a less degree, the ultimate tensile strength seem to be better indices of the endurance limit than the elastic limit is not clear, and this result should be regarded as tentative. Elastic limits determined from compression tests and torsion tests gave no better index than did those from tension tests.

3. The single-blow impact tests (Charpy tests) and the repeated-impact tests did not furnish a reliable index for the endurance limit under reversed stress of the ferrous metals tested.

4. Accelerated or short-time tests of metals under repeated stress, using high stresses and consequent small numbers of repetitions to cause

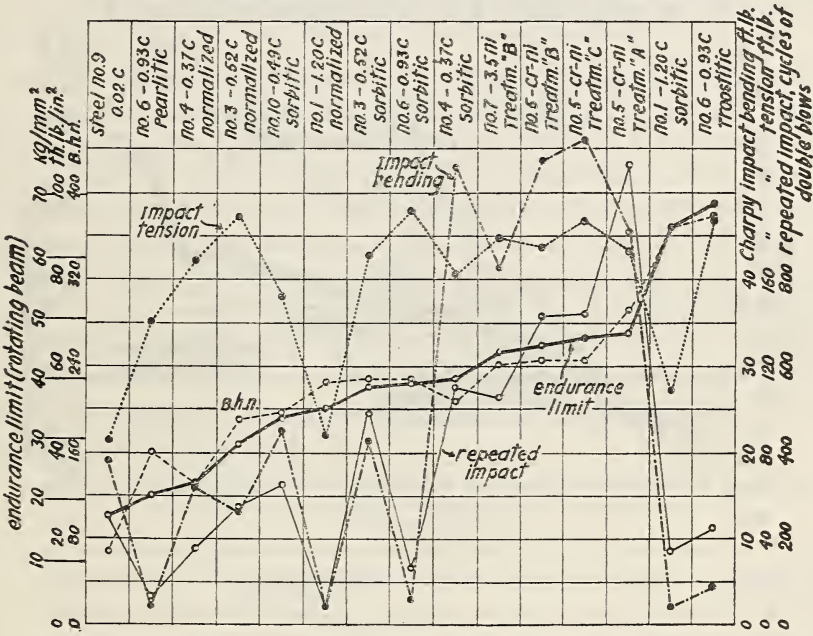


FIG. 36.—Correlation between the endurance limit and other properties of steels.

H. F. Moore, III. U. Eng. Exp. Sta. Bul., No. 124, 1921. Tests were made in a Farmer machine.

failure, are not reliable as indices of the ability of metal to withstand millions of repetitions of low stress.

5. The endurance limit for the ferrous metals tested could be predicted with a good degree of accuracy by the measurement of rise of temperature under reversed stress applied for a few minutes. This relation is explicable in view of the intercrystalline and intracrystalline slippage under repeated stress shown by the microscope. It is believed that this test, which is a development of a test proposed by C. E. Stromeyer, can be developed into a reliable commercial test of ferrous metals under repeated stress. Its applicability to nonferrous metals has not been investigated.

6. Abrupt changes of outline of specimens subjected to repeated stress greatly lowered their resistance. Cracks, nicks, and grooves caused in machine parts by wear, by accidental blows, by accidental heavy overload, or by improper heat treatment may cause such abrupt change of outline. Shoulders with short-radius fillets are a marked source of weakness.

7. Poor surface finish on specimens subjected to reversed stress was found to be a source of weakness. This weakness may be explained by

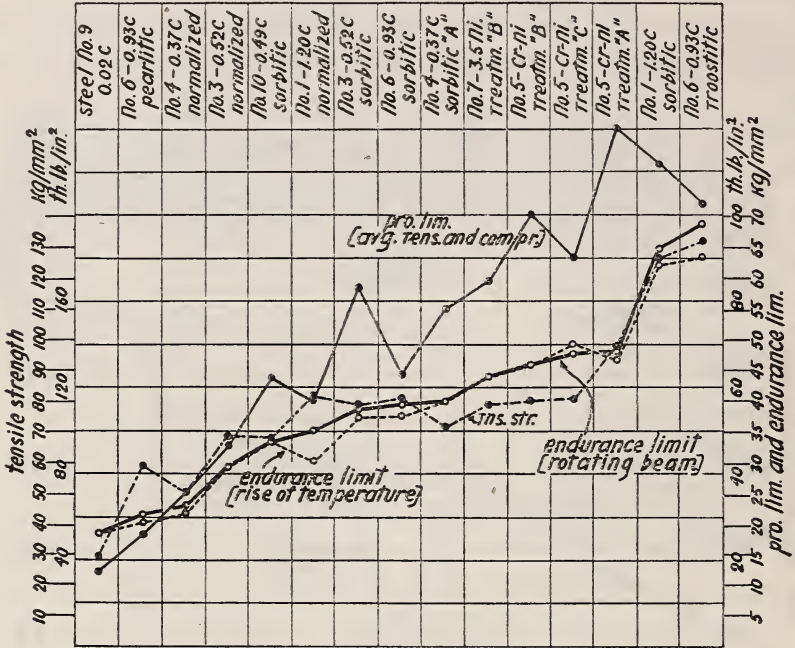


FIG. 37.—Correlation between the endurance limit and the tensile properties of steels.

H. F. Moore, Ill. U. Eng. Exp. Sta. Bul., No. 124, 1921. Tests were made in a Farmer machine.

the formation of cracks due to localized stress at the bottom of scratches or tool marks.

8. Stress above the endurance limits, due to either a heavy overload applied a few times or a light overload applied some thousands of times, was found to reduce somewhat the endurance limit of two ferrous metals tested.

9. In none of the ferrous metals tested did the endurance limit under completely reversed stress fall below 36 per cent of the tensile strength; for only one metal did it fall below 40 per cent, while for several metals it was more than 50 per cent. However, these metals were to a high degree free from inclusions or other internal defects; the specimens had no abrupt changes of outline and had a good surface finish.

10. It is well known that subjecting steel to a stress beyond the yield point raises the static elastic tensile strength to a marked degree. The effect is less marked on the endurance limit, although some increase was observed for 0.18 carbon steel with the surface polished after being stretched well beyond the yield point. Annealing of commercial cold-drawn screw stock was found to lower its endurance limit somewhat less than it did its static elastic strength.

11. The test results herein reported indicate the effectiveness of proper heat treatment in raising the endurance limit of the ferrous metals tested. Here, again, it should be noted that an increase in static elastic strength due to heat treatment is not a reliable index of increase of endurance limit under reversed stress.

12. The phenomenon known as "fatigue" of metals under repeated stress might better be called the "progressive failure" of metals. The most probable explanation seems to be that such failure is a progressive spread of microscopic fractures. A nucleus for damage may be a very small area of high, localized stress due to a groove, a scratch, or a crack; in other cases failure may be due to internal inclusions or irregularities of structure; it may be due to internal stress remaining after heat treatment; it may be due to a grain or group of grains unfavorably placed to resist stress; or failure may begin in the weaker grains of a metal whose structure consists of two or more kinds of grains; or it may, of course, begin in any portion of the metal which by accidental overload or otherwise is stressed to the yield point.

TABLE 23.—Effect of High Temperature on the Tensile Properties of Cast Iron.¹

(See Tables 24 and 25.)

	Chemical composition of materials used.				Chemical composition of materials used.		
	A-1	A-2	A-3		A-1	A-2	A-3
Total carbon.....	3.286	3.144	2.845	S.....	0.110	0.110	0.155
Graphitic carbon.....	2.716	2.334	1.950	P.....	1.541	.868	1.036
Si.....	1.745	1.840	1.447	Mn.....	.155	.510	.450

¹ A. Campion and J. Donaldson, *The Met. Ind.*, London, Aug. 11, 1922.

A-1 is used for stove plate and other light castings.

A-2 is a strong cast iron used for steam turbines and other marine work.

A-3 is a semisteel used for dies for tube drawing.

TABLE 24.—Effect of High Temperature on the Tensile Strength of Cast Iron.¹

[For chemical composition, see Table 23.]

Temperature.		A-1				A-2				A-3			
		As cast.		Annealed.		As cast.		Annealed.		As cast.		Annealed.	
°C.	°F.	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²
15	59	16.0	22,700	17.3	24,600	23.6	33,600	23.6	33,600	26.1	37,200	26.4	37,600
100	212	15.6	22,200	17.3	24,600	23.5	33,400	23.9	34,000	25.8	36,800	26.4	37,600
200	392	15.3	21,700	18.1	25,800	22.7	32,200	23.3	33,100	25.3	36,000	26.6	37,800
250	482					21.9	31,100			24.6	35,000		
300	572	16.0	22,700	17.7	25,200	21.0	29,800	23.5	33,400	25.0	35,600	26.6	37,800
350	662					22.0	31,400						
400	752	16.1	22,800	17.8	25,300	23.3	33,200	23.7	33,800	26.7	38,000	26.6	37,850
500	932	15.8	22,500	17.3	24,600	22.0	31,200	22.7	32,300	25.0	35,600	25.0	35,500
600	1,112	11.5	16,350	12.8	18,100	20.2	28,700						
700	1,292	5.3	7,500	6.3	8,950	10.1	14,350						
800	1,472					4.25	6,050						

¹ The Met. Ind., London, Aug. 11, 1922.TABLE 25.—Effect of Repeated Heating and Cooling on Tensile Strength of Cast Iron.¹

[For chemical composition, see Table 23.]

Condition.	A-1		A-2		A-3	
	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²
Original.....	16.1	22,800	23.6	33,600	26.1	37,200
After 25 heatings at 450° C. (842° F.).....	15.3	21,800	21.2	30,200	23.4	33,200
After 25 heatings at 350° C. (1,022° F.).....			20.5	29,100	22.0	31,300
After 55 heatings at 550° C. (1,022° F.).....	11.8	16,800				

¹ The Met. Ind., London, Aug. 11, 1922.

TABLE 26.—Effect of Temperature on Tensile Properties of Some Metals (see fig. 47).

No.	Alloy.	Composition.						
		Sn	Pb	Cu	Fe	Zn	P	Al
	Name.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.
1	Copper-tin bronze.....	12.46	0.06	87.02	0.30	0.20		
2	do.....	10.22	Trace.	89.50	.38	0	0.035	
3	Brass.....	5.69	3.02	86.19	.20	5.03		
4	Aluminum bronze.....	.03	.16	94.94	.14			4.90
5	do.....	.48	.17	88.86	.75	.15		9.67
6	Cast manganese bronze.....	.51	Trace.	58.10	2.21	39.05	(Mn, 0.055)	
7	U. S. Navy brass "S-C".....	3.98	2.78	80.52	.24	12.80		
8	U. S. Navy bronze "M".....	7.72	1.22	86.92	.23	3.62		
9	U. S. Navy gun bronze "G".....	10.40	.39	87.60	.11	1.31		
10	Cast Monel metal.....	.08	.13	27.11	5.46	(Mn, 2.33)	(Ni, 64.79)	(C, 0.32)
16	Rolled rod brass.....	.00	2.53	62.30	.15	34.84		
18	Rolled Monel metal.....			27.22	2.38	(Mn, 1.56)	(Ni, 68.64)	(C, 0.025)
		Si	Mn	S	P	Graph C.	Comb C	C
11	Soft cast iron.....	2.57	0.60	0.103	0.73	3.31	0.17	
12	Cast iron ("semisteel").....	1.76	1.15	.103	.44	3.00	.47	
13	Cupola malleable iron.....	.92	.51	.152	.183	2.96	Trace.	
14	Cast steel.....	.22	.61	.068	.045			0.302
15	Cold-rolled shafting.....	.031	.80	1.08	.079			.140
17	30 per cent nickel steel, rolled.....	.14	2.80	.017	.011	(Ni, 30.92)		.285

NOTE.—Analyses of materials used in tensile tests. Bregowsky and Spring, Proc. Internat. Assoc. for Testing Materials, 7 (1), 1912.

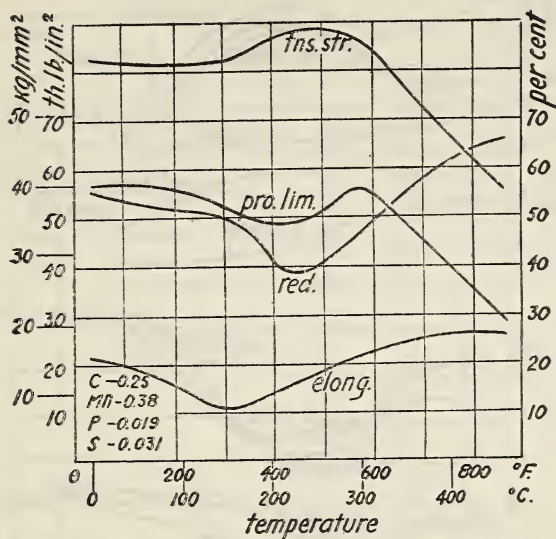


FIG. 38.—Tensile properties of cold-rolled boiler plate at elevated temperatures.

H. J. French, Chem. and Met. Eng., August 2, 1922.

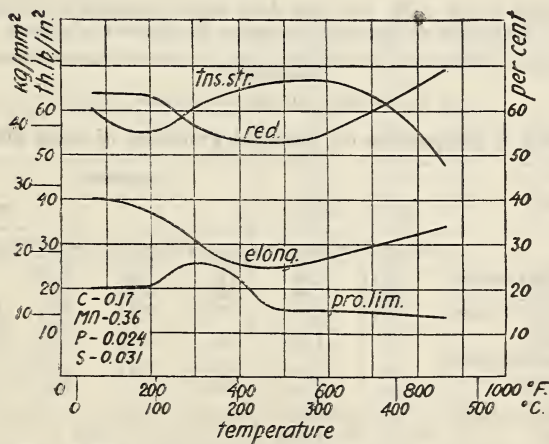


FIG. 39.—Tensile properties of hot-rolled boiler plate at elevated temperatures.

H. J. French, Chem. and Met. Eng., August 2, 1922.

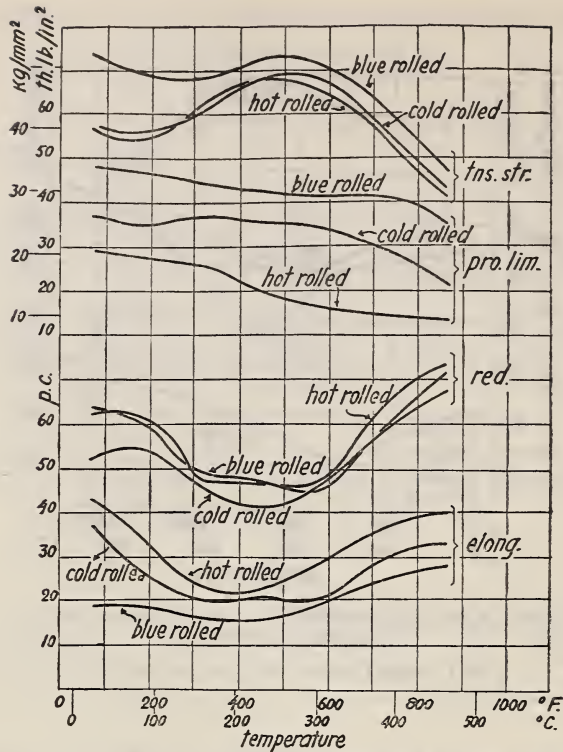


FIG. 40.—Tensile properties of cold, hot, and blue rolled boiler plate at elevated temperatures as determined on specimens cut across the direction of rolling.

Cold and blue rolled plates reduced 1/16 in. (1.6 mm) from 1/2 in. (12.7 mm) at room temperature and 300° C. (572° F.), respectively.

H. J. French, Chem. and Met. Eng., August 2, 1922.

TABLE 27.—Effect of Temperature on Torsional Properties of Some Metals (see fig. 48).

Alloy and name.	Composition.								
	Si	Mn	S	P	C	Ni	V	Cr	
A. Cold-rolled shafting.....	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	
B. Cumberland cold-rolled shafting.....	0.011	0.73	0.117	0.198	0.093	
C. O. H. machinery steel.....	.024	.50	.110	.101	.083	
D. 3 3/4 per cent nickel-vanadium steel.....	.132	.45	.042	.032	.365	3.25	0.45	
E. 25 per cent nickel steel.....186	25.03	
F. 30 per cent nickel steel.....	.14	2.80	.017	.011	.275	30.92	
P. Medium Cumberland cold-rolled steel.....	.12	.51	.050	.013	.375	
N. Vanadium tool steel.....	.16	.32	.034	.014	.722145	0.49	

Alloy and name.	Sn	Pb	Cu	Fe	Ni	Mn	C	Zn	P	Al
	Per ct.	Per ct.	Per ct.	Per ct.	Per ct.	Per ct.	Per ct.	Per ct.	Per ct.	Per ct.
G. 1 1/2" rolled Monel metal.....	0.28	27.08	2.50	68.40	1.52	0.186
M. 3/4" rolled Monel metal.....	27.22	2.38	68.64	1.56	.225
H. Rod brass.....	0.18	2.34	61.08	.42	35.72
I. Tobin bronze.....	.80	0	59.86	.46	38.94	0.0015
J. Elephant (phosphor) bronze.....	3.87	0	95.52	.16	0	.307
K. Delta metal.....	.76	.56	56.56	2.40	39.36	.004
L. Parsons' manganese bronze.....	.54	0	59.58	1.22	38.08	7.34

NOTE.—Analyses of materials used in torsional tests. Bregowsky and Spring, Proc. Internat. Assoc. for Testing Materials, 7 (1); 1912.

TABLE 28.—Effect of Temperature on the Tensile Properties of Some Metals.¹

Metal.	Temperature.		Tensile strength.		Elongation. Per cent.	Reduction of area. Per cent.
	°C.	°F.	kg/mm ²	lb./in. ²		
Cadmium, annealed at 100° C. (212° F.).....	20	68	6.4	9,100	17	49
	130	266	2.45	3,480	34	51
	237	459	.55	780	45	44
Copper, annealed at 600° C. (1,112° F.) ²	20	68	22.8	32,400	32	67
	160	320	18.4	26,200	32	71
	300	572	13.2	18,750	30	50
	410	770	8.5	12,100	19	24
	555	1,031	4.85	6,900	14	19
	650	1,202	3.3	4,700	15	20
	793	1,460	1.9	2,700	14	34
	970	1,778	.8	1,140	6	15
Low carbon steel, annealed at 900° C. (1,652° F.).....	20	68	33.4	47,500	21	68
	225	437	43.0	61,200	4	57
	275	527	44.5	63,300	7	51
	335	635	37.1	52,800	18	61
	407	764	27.0	38,400	21	68
	617	1,142	7.6	10,800	45	95
	807	1,484	2.3	3,270	39	89
	835	1,535	2.2	3,130	39	88
	1,010	1,850	2.9	4,120
	1,100	2,012	2.7	3,840
	1,200	2,192	1.3	1,850
Medium carbon steel, annealed at 700° C. (1,292° F.).....	20	68	45.0	64,000	16	63
	250	482	57.2	81,300	5	43
	330	626	52.6	74,700	9	54
	412	774	44.5	63,300	19	55
	485	905	27.8	39,500	20	62
	617	1,142	15.0	21,300	32	80
	722	1,332	7.0	9,940	35	63
	Lead, annealed at 100° C. (212° F.).....	20	68	1.35	1,920	31
82		180	.8	1,140	24	100
150		302	.5	710	33	100
195		383	.4	570	20	100
265		509	.2	280	20	100
Magnesium, annealed at 350° C. (662° F.).....		20	68	17.0	24,200	0
	83	181	13.4	19,050	10	13
	175	347	6.75	9,600	35	45
	273	523	2.95	4,190	46	76
	355	671	1.6	2,270	50	87
	550	1,022	.3	430	40	100
	Nickel, annealed at 900° C. (1,652° F.).....	20	68	49.3	70,000	26
195		383	44.8	63,600	26	66
300		572	44.8	63,600	31	67
455		851	30.2	42,900	20	31
593		1,100	20.6	29,300	16	25
800		1,472	9.2	13,100	11	18
1,000		1,832	4.0	5,690	11	15
1,100		2,012	2.5	3,550	11	24
Tin, annealed at 50° C. (122° F.).....	20	68	27.5	39,100	40	74
	53	127	17.5	24,900	45	72
	100	212	10.5	14,900	45	82
	153	307	6.5	9,240	41	97
	180	356	4.5	6,400	10	12
	297	405	2.5	3,550	0	0
	Zinc, annealed at 200° C. (392° F.).....	20	68	11.3	16,050	5
112		234	7.25	10,300	8	15
150		302	5.0	7,100	7	10
247		477	2.25	3,200	6	11
330		626	1.25	1,780	8	15
405		761	.03	40	2	2

¹ P. Ludwik, Zeitschrift des Vereines der Deutscher Ingenieure, p. 657, Aug. 14, 1915.² The rate of loading not given.

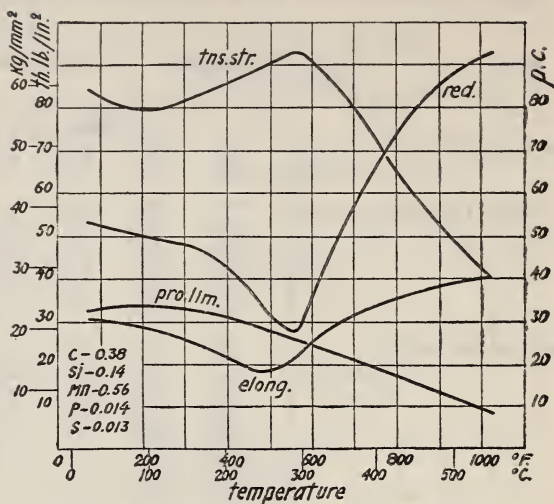


FIG. 41.—Tensile properties at elevated temperatures of 0.38 per cent carbon steel.

H. J. French, B. S. Tech. Paper No. 205; 1921.

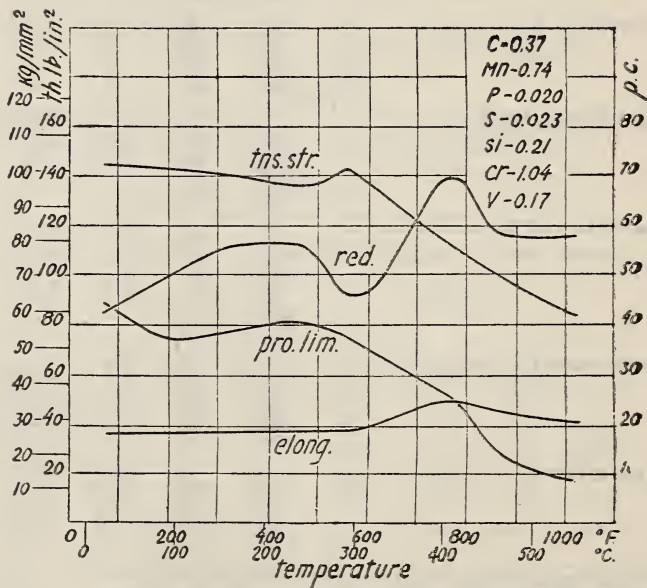


FIG. 42.—Tensile properties at elevated temperatures of chromium-vanadium steel containing 1 per cent chromium, 0.2 per cent vanadium, and 0.37 per cent carbon.

H. J. French, B. S. Tech. Paper No. 205; 1921.

TABLE 29.—Effect of Temperature on the Tensile Strength of High-Speed Steel.¹

Temperature.		Tensile strength.				Temperature.		Tensile strength.			
°C.	°F.	Grade A.		Grade B.		°C.	°F.	Grade A.		Grade B.	
		C, 0.63; Cr, 3.55; V, 0.97; W, 17.04.		C, 0.65; Cr, 3.33; V, 1.78; W, 13.85.				C, 0.63; Cr, 3.55; V, 0.97; W, 17.04.		C, 0.65; Cr, 3.33; V, 1.78; W, 13.85.	
		kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²			kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²
38	100	171.2	243,500	151.1	215,000	538	1,000	168.7	240,000	156.8	223,000
204	400	180.3	256,500	191.9	273,000	593	1,100	154.7	220,000	140.6	200,000
316	600	202.0	287,500	182.9	260,000	649	1,200	130.1	185,000	112.5	160,000
427	800	200.4	285,000								

¹ Met. Ind., London, Apr. 14, 1922.TABLE 30.—Flow of Steels Under Constant Load at High Temperatures.¹

[For Chemical Composition and Heat Treatment of Tested Steels, see Table 31.]

Type of steel.	Temperature range.		Actual duration of test before fracture or withdrawal.	Estimated time at load of 13.4 kg/mm ² or 19,000 lb./in. causing fracture.	Elongation on middle 50.8 mm or 2 inches.	Reduction of area.
	°C.	°F.				
0.30 per cent carbon.....	500-550	932-1,022	1,739 withdrawn	² 3,400		
	550-600	1,022-1,112	956 broken	956	30.0	85
	600-650	1,112-1,202	28 broken	28	29.0	88
	700	1,292		3 min.	32.5	92
	775	1,427		² 6 sec.		
0.45 per cent carbon.....	500-550	932-1,022	1,405 withdrawn	² 2,600		
	550-600	1,022-1,112	195 broken	195	32.0	84
	600-650	1,112-1,202	26 broken	26	32.0	84
	680	1,256		3 min.	33.0	90
	775	1,427		² 6 sec.		
Nickel-chromium.....	500-550	932-1,022	701 broken	701	40.0	85
	550-600	1,022-1,112	88 broken	88	41.0	88
	600-650	1,112-1,202	8 broken	8	38.0	91
	685	1,265		3 min.	40.0	94
	805	1,481		² 6 sec.		
14.7 per cent chromium.....	500-550	932-1,022	1,740 withdrawn	² 10,000		
	550-600	1,022-1,112	1,728 broken	1,728	34.0	84
	600-650	1,112-1,202	79 broken	79	37.0	85
	735	1,355		3 min.	36.0	91
	800	1,472		² 6 sec.		
High-speed.....	500-550	932-1,022	1,717 withdrawn	² 81,000		
	550-600	1,022-1,112	2,002 withdrawn	² 25,000		
	600-650	1,112-1,202	380 withdrawn	² 4,500		
	650-700	1,202-1,292	564 broken	564	19.0	47
	700-750	1,292-1,382	21 broken	21	24.0	60
	815	1,499		3 min.	32.0	82
Nickel-chromium alloy (as cast).....	500-550	932-1,022	521 withdrawn			
	550-600	1,022-1,112	3,604 withdrawn	² 108,120		
	600-650	1,112-1,202	6,041 broken	6,041	17.5	40
	650-700	1,202-1,292	901 broken	901	14.5	23
	700-750	1,292-1,382	273 broken	273	27.0	51
	895	1,643		3 min.	24.5	44
	925	1,697		1 min.	25.0	47
	965	1,769		² 6 sec.		

¹ J. H. S. Dickenson, Eng., Sept. 15, 1922.² Estimated time.

TABLE 31.—Flow of Steels Under Constant Load at High Temperatures. See Table 30.¹

[Chemical Composition and Heat Treatment of Tested Steels.]

Class of steel.	Diameter of bar.	Heat treatment before machining.	Chemical composition.								
			C	Si	Mn	S	P	Ni	Cr	W	V
0.30 per cent carbon.	Inches. $\frac{7}{8}$ (22.2 mm)	Oil hardened, 850° C. (1,562° F.); tempered, 575° C. (1,067° F.).	0.30	0.12	0.54	0.027	0.038	0.51	0.14
0.45 per cent carbon.	1 (25.4 mm)	Water hardened, 850° C. (1,562° F.); tempered, 600° C. (1,112° F.).	.45	.37	.79	.022	.02402
Nickel-chromium..	$\frac{3}{8}$ (19.05 mm)	Oil hardened, 830° C. (1,526° F.); tempered, 600° C. (1,112° F.).	.25	.11	.36	.031	.026	3.63	.55
14.7 per cent chromium.	$\frac{3}{4}$ (22.2 mm)	Oil hardened, 925° C. (1,697° F.); tempered, 650° C. (1,202° F.).	.26	.59	.17	.066	.016	.39	14.68
High-speed.....	$\frac{1}{2}$ (20.6 mm)	Annealed, 800° C. (1,472° F.).	.60	.28	.23	.044	.029	3.49	14.09	0.72
Nickel-chromium alloy (cast).54	.73	.10	.032	.030	69.90	15.50

¹ J. H. S. Dickenson, Eng., Sept. 15, 1922.

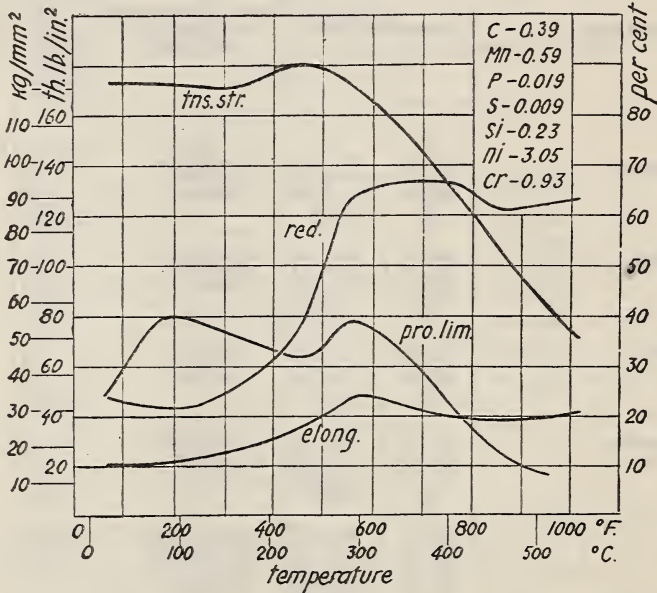


FIG. 43.—Tensile properties at elevated temperatures of nickel-chromium steel containing 3 per cent nickel, 1 per cent chromium, and 0.39 per cent carbon.

H. J. French, B. S. Tech. Paper No. 205; 1921.

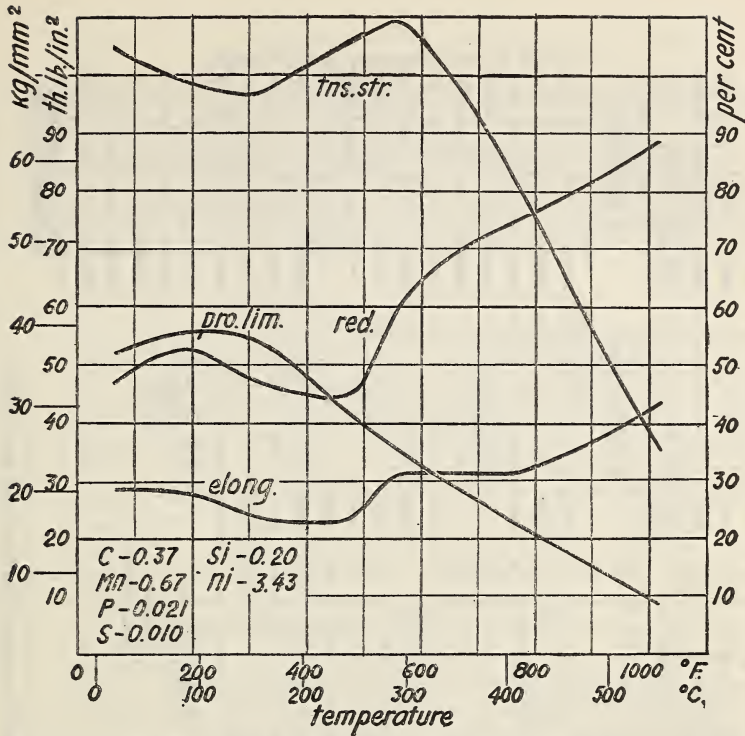


FIG. 44.—Tensile properties at elevated temperatures of 3½ per cent nickel steel containing 0.37 per cent carbon.

H. J. French, B. S. Tech. Paper No. 205; 1921.

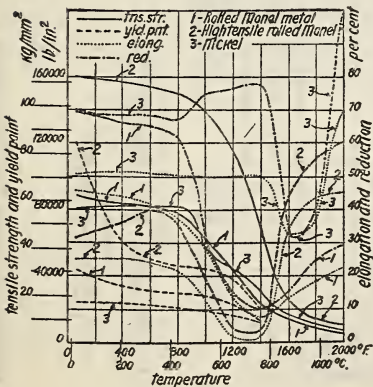


FIG. 45.—Tensile properties of Monel metal and nickel at high temperatures.

Communicated by P. Merica of the International Nickel Co., 1922.

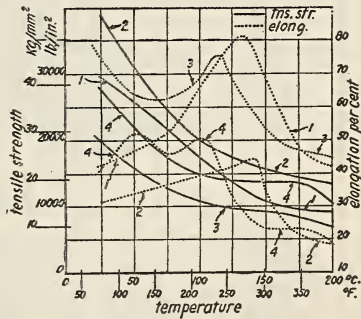


FIG. 46.—Variation of tensile properties of rolled zinc with temperature.

C. Mathewson, C. Trevin, and W. Finkeldey, Trans. Am. Inst. Min. Met. Eng., 64, p. 305; 1920.

1. With grain } common zinc with 0.37 Pb,
 2. Across grain } 0.016 Fe, 0.04 Cd.
 3. With grain } Pure zinc with 0.065 Pb,
 4. Across grain } 0.018 Fe.
- Thickness of specimens was 1.4 mm or 0.055 in. Scleroscope hardness of common zinc, 27 and that of pure zinc, 23.

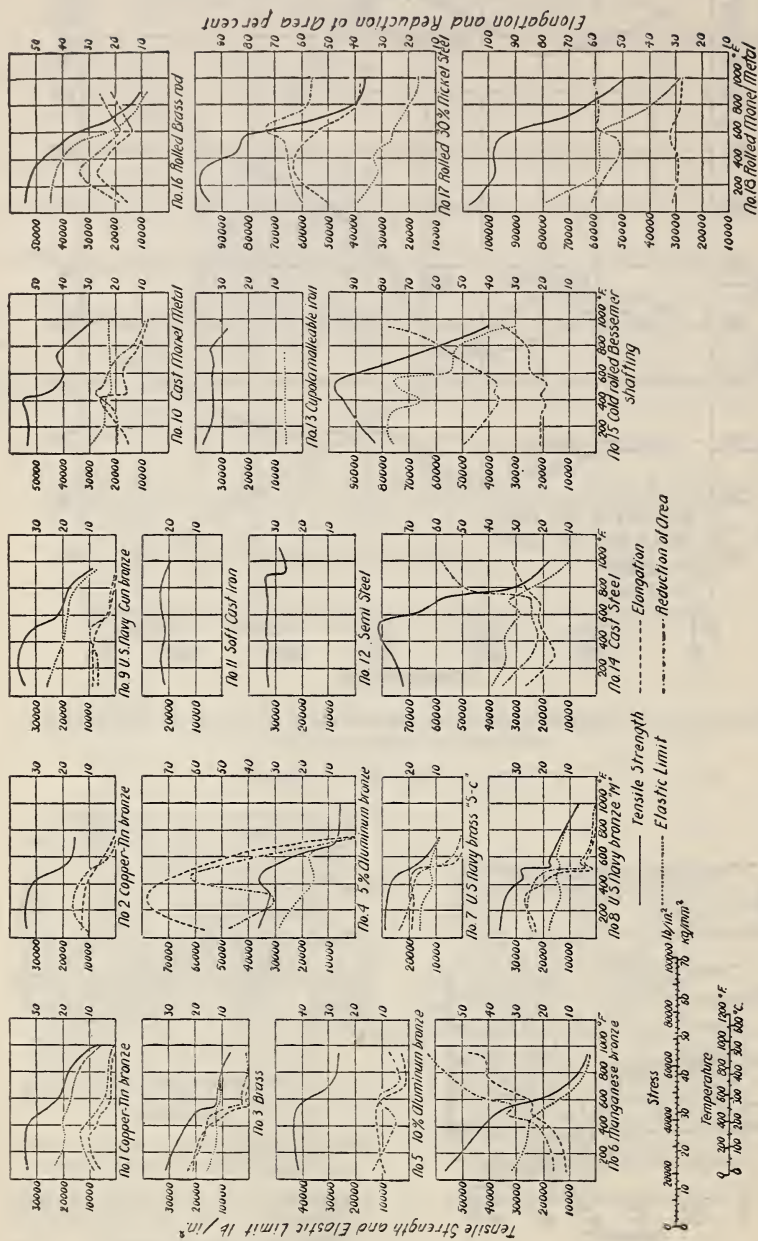


FIG. 47.—Effect of temperature on tensile properties of some metals.

Bregowsky and Spring, Proc. 6th congress of the International Association for Testing Materials, VII, 1, 1912. For chemical composition of tested metals see Table 26.

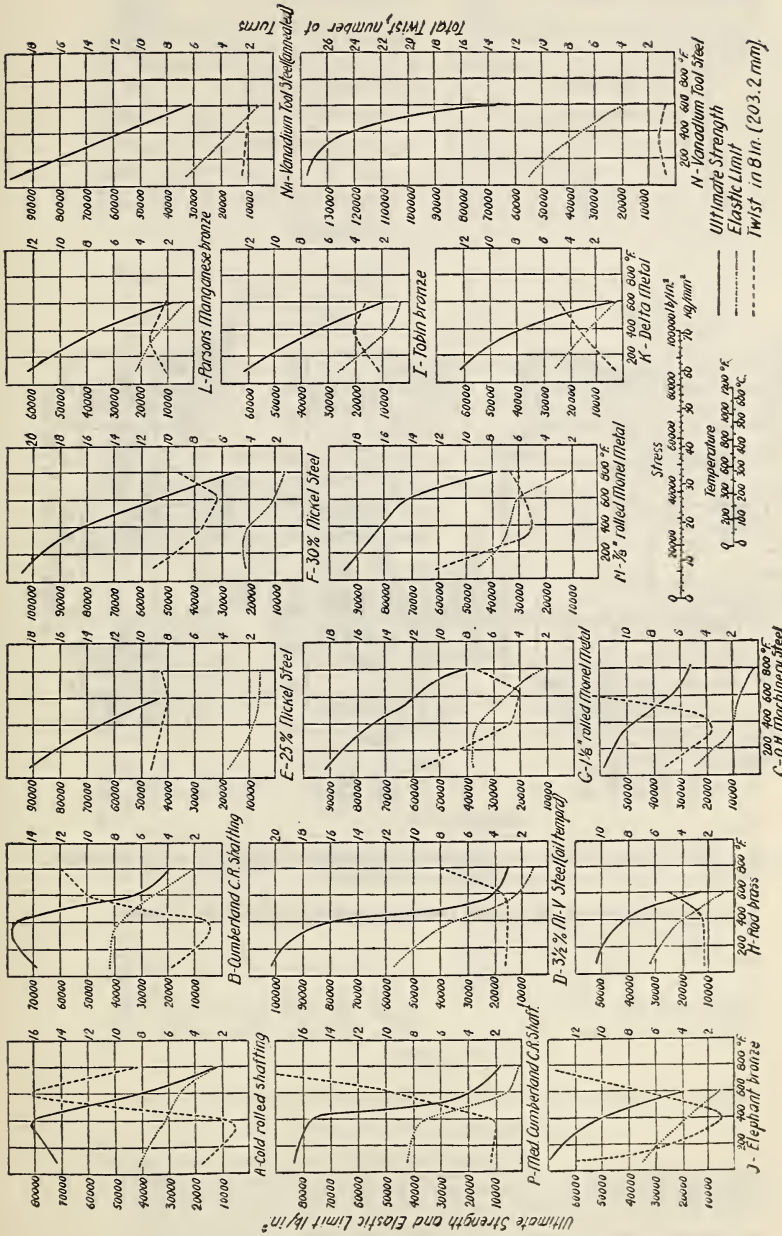


FIG. 48.—Effect of temperature on torsional properties of some metals.

Bregowsky and Spring, Proc. 6th congress of the International Association for Testing Materials, VII, 1, 1912. For chemical composition of tested metals see Table 26.

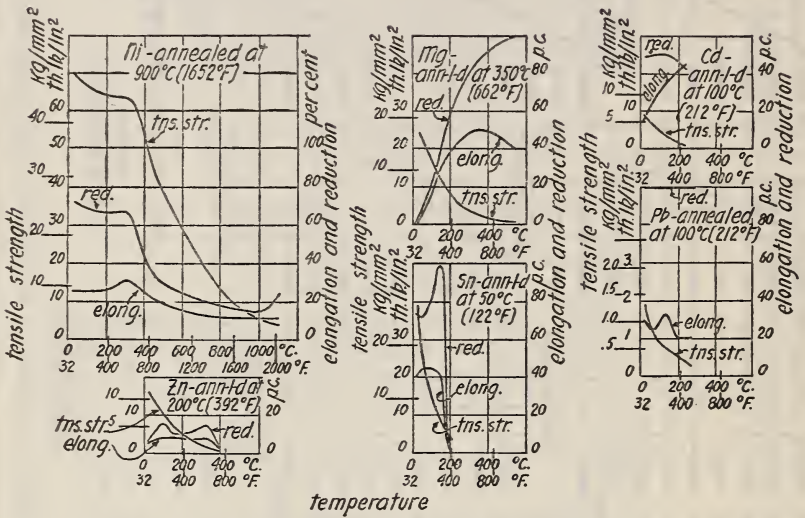


FIG. 49.—Effect of temperature on the tensile properties of nickel, zinc, magnesium, tin, cadmium, and lead.

P. Ludwik, Zeitschrift des Vereines Deutscher Ingenieure, p. 657, Aug. 14, 1915.

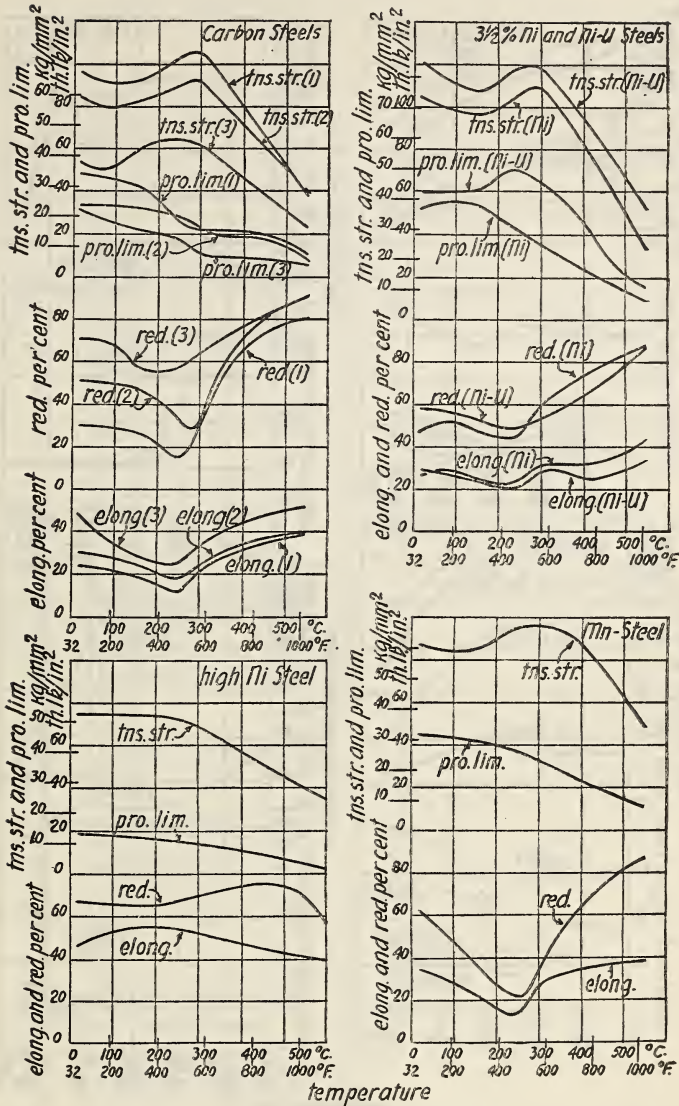


FIG. 50.—Effect of high temperature on the tensile properties of steels.

H. J. French, B. S. Tech. Paper No. 219; 1922.

Chemical composition and heat treatment of tested steels:

Carbon: (1) C, 0.59; Mn, 0.40; Si, 0.05; P, 0.017; S, 0.027; Cr, 0.05. Cooled in air from 850° C. (1,562° F.). (2) C, 0.38; Mn, 0.55; Si, 0.14; P, 0.014; S, 0.013. Cooled in air from 850° C. (1,562° F.). (3) C, 0.18; Mn, 0.43; P, 0.017; S, 0.035. Cooled in air from 900° C. (1,652° F.).

3 1/2 per cent Ni: C, 0.37; Mn, 0.67; Si, 0.20; P, 0.021; S, 0.010; Ni, 3.43. Air cooled from 800° C. (1,472° F.).

Nickel-uranium: C, 0.43; Mn, 0.50; Si, 0.50; P, 0.007; S, 0.010; Ni, 2.79; U, 0.35. Quenched in water from 800° C. (1,472° F.) and cooled in air from 600° C. (1,112° F.).

High Ni: C, 0.20; Mn, 0.80; Si, 0.15; Ni, 28.6. Cooled in air from 800° C. (1,472° F.).

Manganese: C, 0.28; Mn, 1.26; Si, 0.12; P, 0.07; S, 0.047; Ni, 0.12; Cr, 0.05. Cooled in air from 850° C. (1,562° F.).

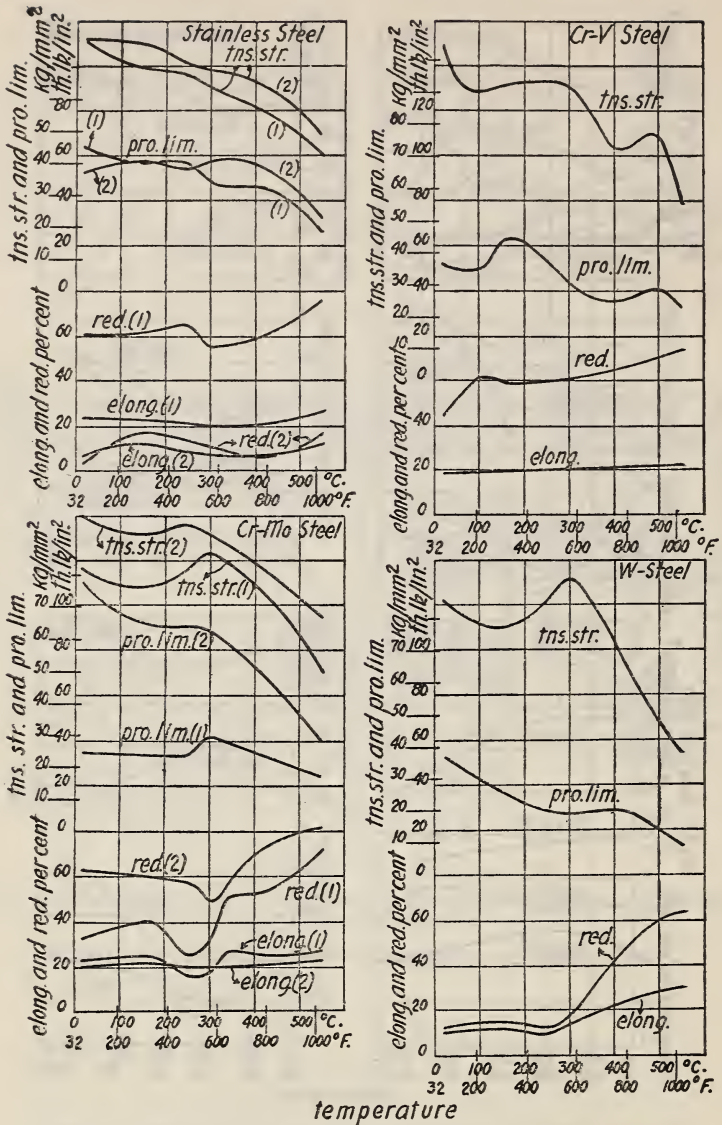


FIG. 51.—Effect of high temperature on the tensile properties of steels.

H. J. French, B. S. Tech. Paper No. 219; 1922.

Chemical composition and heat treatment of tested steels:

Stainless: C, 0.31; Mn, 0.24; Si, 0.054; P, 0.020; S, 0.020; Cr, 12.75. (1) Quenched in oil from 955° C. (1,751° F.) and cooled in air from 675° C. (1,247° F.). (2) Quenched in oil from 1,150° C. (2,102° F.) and cooled in air from 675° C. (1,247° F.).
 Chromium Vanadium (die steel): C, 0.38; Mn, 0.56; Si, 0.16; P, 0.011; S, 0.014; Cr, 1.98; V, 0.18. Cooled in air from 800° C. (1,472° F.).
 Chromium-molybdenum: C, 0.27; Mn, 0.62; Si, 0.26; P, 0.018; S, 0.008; Cr, 0.99; Mo, 0.41; Ni, 0.08. (1) Cooled in air from 815° C. (1,499° F.). (2) Quenched in oil from 845° C. (1,553° F.) and cooled in air from 600° C. (1,112° F.).
 Tungsten: C, 0.95; Si, 0.26; W, 1.17. Cooled in air from 815° C. (1,499° F.).

TABLE 32.—Tensile Strength of Steels at Elevated Temperatures Under Rapidly (1–2 min.) Applied Load.¹

[For Chemical Composition and Heat Treatment of Tested Steels see Table 31.]

Temperature. °C. Room temperature, ... 100 200 300 400 500 600 700 800 900 1,000	0.30 per cent carbon.			0.45 per cent carbon. ²			Nickel-chromium.			14.7 per cent chromium.			High-speed.		
	Tensile strength.		Reduction of area.	Tensile strength.		Reduction of area.	Tensile strength.		Reduction of area.	Tensile strength.		Reduction of area.	Tensile strength.		Reduction of area.
	kg/mm ²	lb./in. ²	Per cent.	kg/mm ²	lb./in. ²	Per cent.	kg/mm ²	lb./in. ²	Per cent.	kg/mm ²	lb./in. ²	Per cent.	kg/mm ²	lb./in. ²	Per cent.
	68.0	96,800	64.8	80.4	114,400	64.8	83.1	118,200	66.8	85.0	121,000	86.1	122,500	15.0	
	63.6	90,500	59.2	74.0	105,200	59.2	80.6	114,700	64.8	78.5	111,800	86.6	123,200	23.0	
	392	93,500	55.8	74.9	106,600	60.4	80.3	114,300	62.6	74.3	105,800	82.5	117,400	21.4	
	572	102,200	51.0	77.5	110,200	53.4	82.5	117,400	55.2	73.6	104,800	83.1	118,200	32.0	
	752	91,300	67.8	73.6	104,800	69.9	74.0	105,300	68.8	70.0	99,500	70.9	100,800	27.6	
	932	43.5	61,800	52.2	74,400	83.4	56.7	80,600	82.7	59.8	85,100	58.9	83,800	32.0	
	1,112	32.8	46,600	38.4	54,700	84.1	36.5	52,000	88.6	43.5	61,800	42.7	60,700	58.1	
	1,292	19.8	28,200	16.4	23,300	92.0	21.1	30,000	88.6	27.4	39,000	36.2	51,500	62.6	
	1,472	11.3	16,100	12.9	18,400	93.4	13.9	19,700	96.2	13.9	19,700	21.4	30,500	65.4	
	1,652	8.0	11,400	6.9	9,850	95.2	8.5	12,100	95.4	10.1	14,300	16.4	23,300	53.3	
	1,832	6.3	8,960	5.4	7,610	98.8	5.7	8,060	99.9	9.6	13,700	11.3	16,100	80.3	

² Oil hardened 870° C. (t, 598° F.), tempered 600° C. (t, 112° F.).

¹ J. H. S. Dickenson. Eng., Sept. 15, 1922.

TABLE 33.—Tensile Properties of Molybdenum Wire at High Temperatures.¹

Condition.	Temperature.		Tensile strength.		Elongation in 50.8 mm (2 in.).	Reduction of area.
	°C	°F.	kg/mm ²	lb./in. ²	Per cent.	Per cent.
Treated to develop extremely large grains.....	-185	-301	68.5	97,500	0.0	0.0
	25	77	29.9	42,500	3.15	.0
	100	212	24.6	35,000	4.30	.0
	200	392	19.7	28,000	8.70	.0
	300	572	21.8	31,000	10.20	100
	400	752	19.3	27,500	6.25	100
	500	932	19.0	27,000	3.10	100
	600	1,112	19.7	28,000	2.35	100
	700	1,292	21.1	30,000	3.15	100
	900	1,652	20.7	29,500	3.10	100
Treated to develop very small grains.....	-185	-301	105.9	150,500	.40	0.0
	-50	-58	105.5	150,000	11.75	55
	25	77	88.0	125,000	20.00	66
	100	212	80.2	114,000	17.30	68
	200	392	73.9	105,000	14.00	78
	300	572	66.8	95,000	9.40	85
	400	752	61.8	88,000	7.00	86
	500	932	56.2	80,000	6.25	89
	600	1,112	55.5	79,000	2.35	90
	700	1,292	53.3	76,500	2.35	93
900	1,652	49.9	71,000	1.80	93	
Swaged and drawn hot at 1,300 to 1,000° C. (2,372 to 1,832° F.) from 0.125 to 0.025 in. (3.33 to 0.65 mm).	-185	-301	147.8	210,000	0.0	0.0
	25	77	104.0	148,000	4.70	68
	100	212	92.2	131,000	1.55	71
	200	392	84.4	120,000	.80	75
	300	572	73.2	104,000	.80	79
	400	752	70.3	100,000	.80	87
	500	932	68.9	98,000	Less than .5	89
	600	1,112	67.5	96,000	Less than .5	88
	700	1,292	56.2	80,000	Less than .5	89
	900	1,652	54.8	² 78,000	Less than .5	88

¹ W. P. Sykes, Trans. Am. Inst. Min. and Metal. Eng., 64, p. 780, 1920.² Rapid loading.

TABLE 34.—Tensile Properties of Nickel Wire at High Temperatures.¹

Condition.	Temperature.		Tensile strength.		Elongation in 50.8 mm (2 in.).	Reduction of area.
	°C.	°F.	kg/mm ²	lb./in. ²		
Drawn cold from 0.040 to 0.025 in. (1.02 to 0.64 mm).....	-185	-301	102.0	145,000	3.15	60
	25	77	87.2	124,000	1.06	70
	100	212	85.8	122,000	.8	65
	200	392	81.6	116,000	.0	60
	300	572	78.0	111,000	.0	75
	400	752	67.5	96,000	.8	73
	500	932	59.7	85,000	.8	69
	600	1,112	58.3	83,000	.8	65
	700	1,292	14.1	20,000	20.3	50
	800	1,472	12.0	17,000	20.5	45
Drawn at 400° C. (752° F.) from 0.040 to 0.025 in. (1.02 to 0.64 mm).	-185	-301	91.0	129,500	3.98	50
	25	77	77.4	110,000	3.12	73
	100	212	73.2	104,000	2.35	73
	200	392	68.9	98,000	2.35	73
	300	572	60.4	86,000	1.55	68
	400	752	54.1	77,000	1.60	63
	500	932	48.5	69,000	1.60	73
	600	1,112	40.8	58,000	1.60	68
	700	1,292	12.7	18,000	13.0	47
	800	1,472	7.7	11,000	18.0	48
Drawn cold from 0.095 to 0.025 in. (2.41 to 0.64 mm).....	-185	-301	109.0	155,000	3.12	54
	25	77	93.5	133,000	1.06	58
	100	212	90.7	129,000	.80	52
	200	392	85.1	121,000	.0	52
	300	572	83.7	119,000	.0	58
	400	752	75.2	107,000	.0	56
	500	932	61.2	87,000	.80	63
	600	1,112	58.4	83,000	.80	55
	700	1,292	15.5	22,000	18.5	82
	800	1,472	9.1	13,000	15.5	65
Drawn cold from 0.095 to 0.025 in. (2.41 to 0.64 mm) and annealed at 800° C. (1,472° F.).	-185	-301	59.0	84,000	20.0	59
	25	77	42.2	60,000	22.0	75
	100	212	39.3	56,000	20.3	73
	200	392	35.1	50,000	15.5	68
	300	572	35.1	50,000	17.5	75
	400	752	30.2	43,000	17.25	75
	500	932	23.9	34,000	19.5	75
	600	1,112	17.6	25,000	15.5	65
	700	1,292	12.0	17,000	15.5	60
	800	1,472	9.1	13,000	15.5	45
900	1,652	6.3	9,000	15.5	39	
1,000	1,832	4.9	7,000	26.5	48	

¹ W. P. Sykes, Trans. Am. Inst. Min. and Metal. Eng., 64, p. 780, 1920.

² Rapid loading.

TABLE 35.—Compression Tests of Some Steels at High Temperature.¹

[See Figs. 52 to 57.]

CHEMICAL ANALYSIS OF TESTED STEELS.²

Steel.	Chemical composition.						
	C	Mn	P	S	Si	Cr	Ni
	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.
A.....	0.07	0.43	0.069	0.052	0.008
B.....	.10	.37	.012	.051	.009
C.....	.32	.53	.013	.037	.015
D.....	.95	.20	.014	.011	.250
E.....	.33	.59	.010	.065	.144	0.51	1.14
F.....	.31	.50	.032	.029	.17	.94	2.89

¹ Results obtained by H. J. French, unpublished data of the Bureau of Standards, 1923.

² The specimens were 0.75 in. (19.05 mm) in diameter and 3.25 in. (82.55 mm) long. The speed of the testing machine was about 0.07 in. (1.78 mm) per minute.

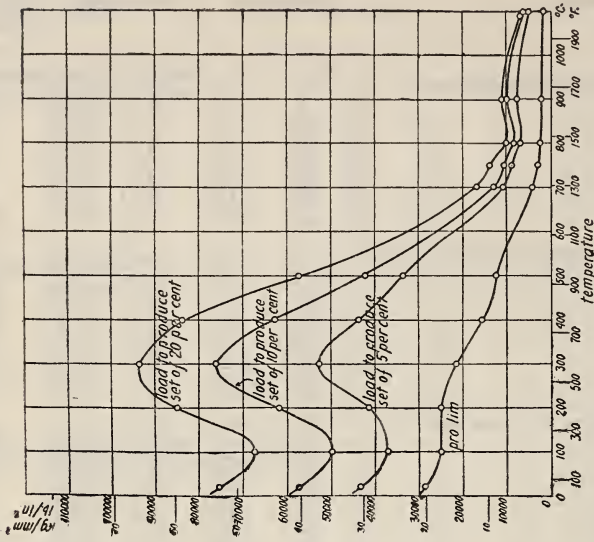


FIG. 53.—Compression tests of 0.10 per cent carbon steel at elevated temperature.

Results obtained by H. J. French, unpublished data of the Bureau of Standards, 1933. For chemical composition see Table 35, material B.

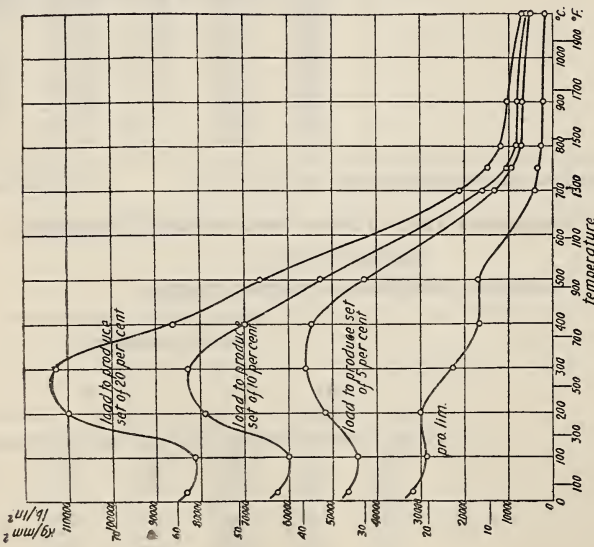


FIG. 52.—Compression tests of wrought iron at elevated temperatures.

Results obtained by H. J. French, unpublished data of the Bureau of Standards, 1933. For chemical composition see Table 35, material A.

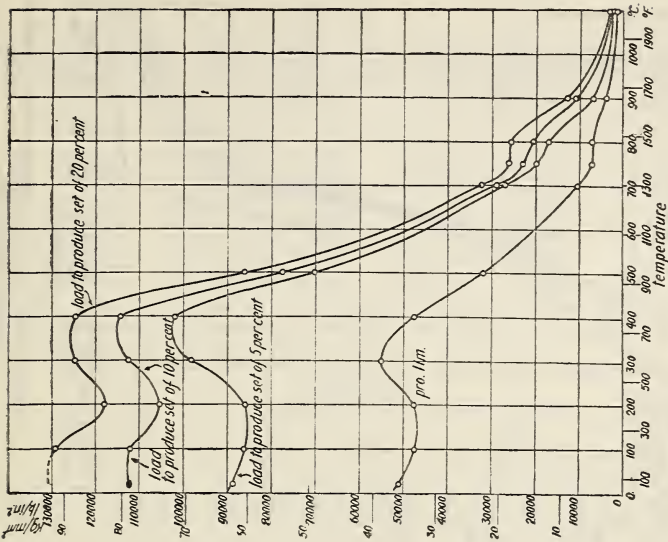


FIG. 55.—Compression tests of 0.95 per cent carbon steel at elevated temperature.

Results obtained by H. J. French, unpublished data of the Bureau of Standards, 1923. For chemical composition see Table 35, material D.

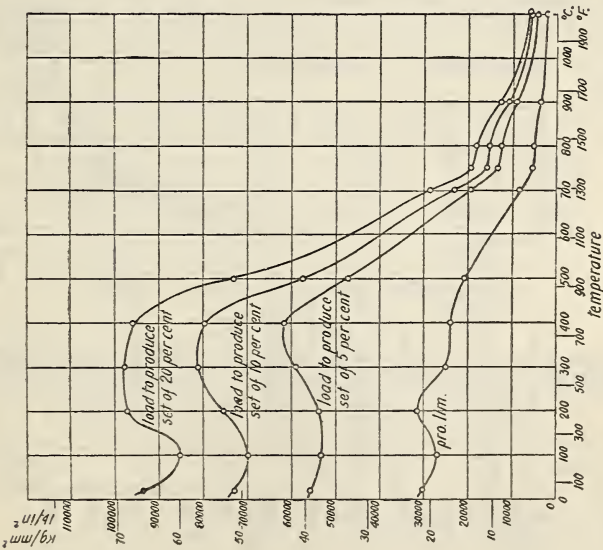


FIG. 54.—Compression tests of 0.32 per cent carbon steel at elevated temperature.

Results obtained by H. J. French, unpublished data of the Bureau of Standards, 1923. For chemical composition see Table 35, material C.

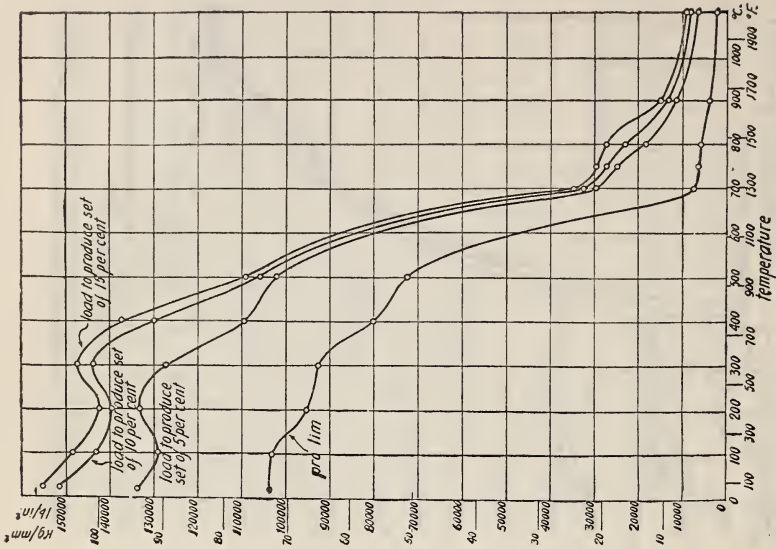


FIG. 57.—Compression tests of chrome-nickel steel at elevated temperature.

Results obtained by H. J. French, unpublished data of the Bureau of Standards, 1923. For chemical composition see Table 35, material F.

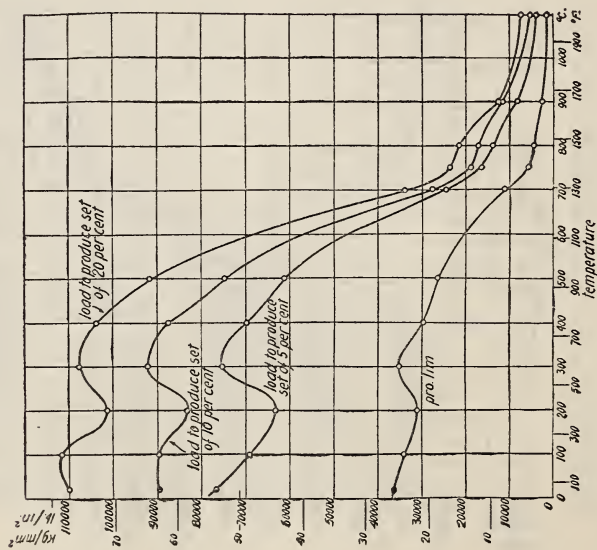


FIG. 56.—Compression tests of chrome-nickel steel at elevated temperature.

Results obtained by H. J. French, unpublished data of the Bureau of Standards, 1923. For chemical composition see Table 35, material E.

TABLE 36.—Compression Tests of White Metal Bearing Alloys at Elevated Temperatures.¹

[For chemical composition of tested alloys, see Table 37.]

Alloy No.	25° C. (77° F.).			50° C. (122° F.).			75° C. (167° F.).			100° C. (212° F.).		
	Yield point, kg/mm ² , lb./in. ² .	Ultimate strength, kg/mm ² , lb./in. ² .	Brinell hardness.	Yield point, kg/mm ² , lb./in. ² .	Ultimate strength, kg/mm ² , lb./in. ² .	Brinell hardness.	Yield point, kg/mm ² , lb./in. ² .	Ultimate strength, kg/mm ² , lb./in. ² .	Brinell hardness.	Yield point, kg/mm ² , lb./in. ² .	Ultimate strength, kg/mm ² , lb./in. ² .	Brinell hardness.
1.....	3.1 4,400	9.04 12,850	17	2.67 3,800	7.32 10,400	14	2.22 3,150	5.94 8,450	11	1.86 2,650	4.89 6,950	8
2.....	4.4 6,250	10.67 15,175		22	3.41 4,850		8.34 11,850	2.81 4,000		6.61 9,400	2.00 2,850	
3.....	4.04 5,750	11.55 16,425	22	3.51 5,000	8.56 12,175	18	2.99 4,250	7.10 10,100	15	2.36 3,350	5.43 7,725	11
4.....	3.3 4,700	9.64 13,700	22	2.57 3,650	7.07 10,050	16	2.04 2,900	5.52 7,850	11	1.51 2,150	4.25 6,050	8
5.....	2.64 3,750	10.56 15,000	20	1.86 2,650	7.93 11,275	17	1.58 2,250	5.55 7,900	11	1.09 1,550	3.36 4,770	8

¹ J. R. Freeman, jr., and R. W. Woodward, U. S. Bureau of Standards Technologic Paper No. 188; 1921.

TABLE 37.—Chemical Composition of White Metal Bearing Alloys.

[See Table 36.]

Alloy No.....	1	2	3	4	5
Copper.....per cent..	4.56	3.51	5.65	2.90	None.
Antimony.....do....	4.52	7.57	6.90	10.50	10.03
Tin.....do.....	Balance.	Balance.	Balance.	Balance.	Balance.
Lead.....do.....	None.	None.	0.09	25.05	84.95
Iron ¹do.....					

¹ Less than 0.05.

TABLE 38.—Tensile Properties of Some Bearing Alloys at Elevated Temperature.¹

Alloy.				Temperature.		Proportional limit.		Tensile strength.		Elongation in 2 in. (50.8 mm).	Reduction of area.
Cu	Sn	Pb	Zn	°C.	°F.	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	Per cent.	Per cent.
85	5	5	5	Room temperature.		14.1	20,000	26.8	38,100	36	32.0
				100	212	12.2	17,400	23.7	33,700	24	24.5
70	5	20	5	Room temperature.		14.1	20,100	22.7	32,300	20	17.0
				100	212	12.4	17,600	20.5	29,200	19	19.5

¹ G. H. Clamer, Am. Inst. Met. Trans., 9, p. 241; 1915.

TABLE 39.—Elasticity at High Temperatures.¹

[See Figs. 58 and 59.]

[Determinations of the modulus of elasticity in shear at temperatures approaching melting point have been made on a wire suspended in a cylinder evacuated to a pressure of only 1.3 mm (to avoid oxidation). The diameter of wire was about 1.5 mm or 0.059 in. and its length about 380 mm or 15 in. The wire was heated by electric current passing through it.]

CHEMICAL COMPOSITION OF TESTED ALLOYS.

Name.	Cu	Al	Zn	Mn	Ni	Sn	Mg
	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.
Brass.....	60.0	40.0
Red brass.....	85.0	15.0
Nickel silver ²
Manganin.....	84.0	12.0	4.0
Phosphor bronze.....	93.0	7.0
Duralumin.....	4.2	94.76	0.5

¹ K. Koch und C. Danneker, Annalen der Physik, 47, p. 197; 1915.

² Was not determined.

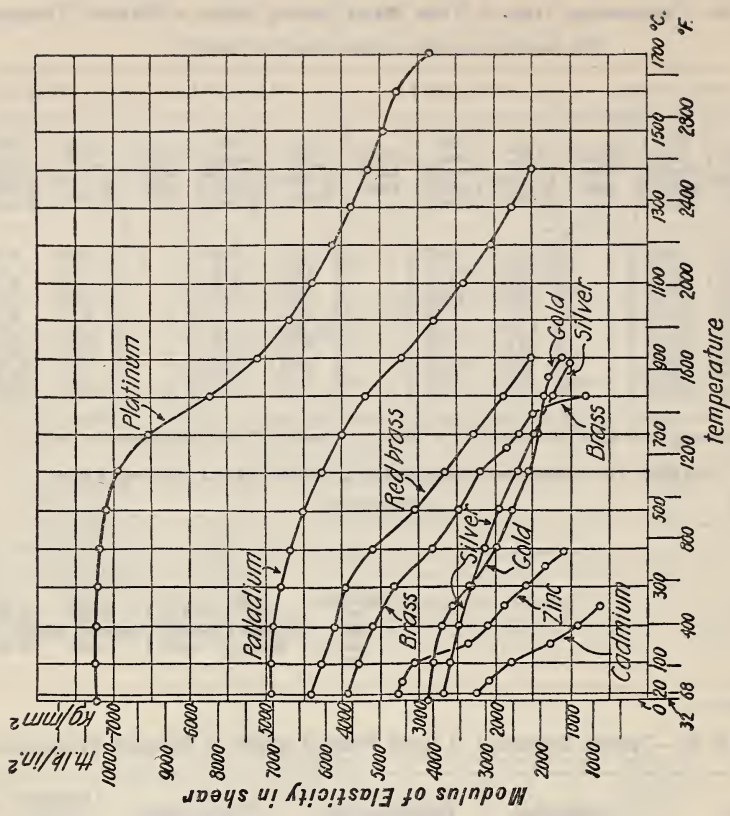


FIG. 59.—Effect of temperature on the modulus of elasticity in shear.

K. Koch and C. Danneker, Annalen der Physik, 47; 1915. For chemical composition of tested metals see Table 39.

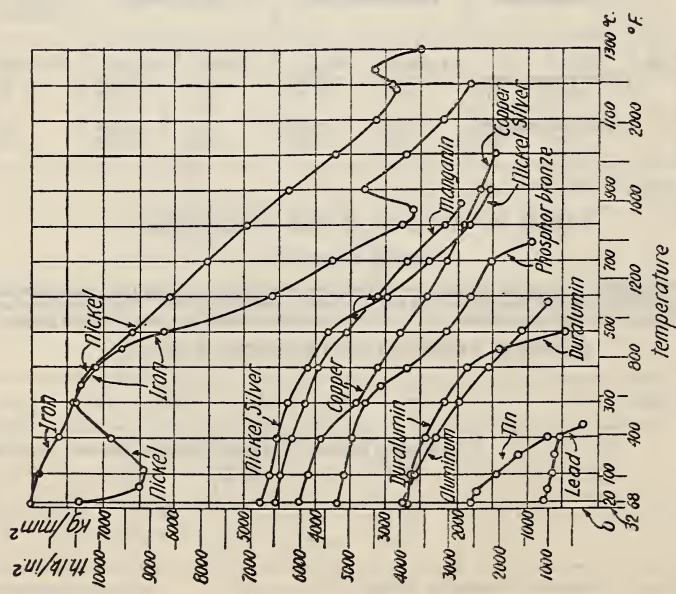


FIG. 58.—Effect of temperature on the modulus of elasticity in shear.

TABLE 40.—Elasticity at Low Temperatures.¹

[Modulus of elasticity was determined at temperatures from that of liquid air to 100° C. (212° F.)-]

Metal.	Melting point, absolute degrees Centigrade.	Ratio of Young's modulus at zero absolute to that of zero Centigrade.	Metal.	Melting point, absolute degrees Centigrade.	Ratio of Young's modulus at zero absolute to that of zero Centigrade.
Rhodium.....	2,270	1.18	Magnesium.....	903	1.57
Platinum.....	2,045	1.27	Aluminum.....	870	1.44
Iron.....	1,870	1.27	Zinc.....	690	2.00
Palladium.....	1,770	1.27	Lead.....	595	1.80
Nickel.....	1,720	1.12	Cadmium.....	585	2.50
Copper.....	1,324	1.37	Bismuth.....	530	1.85
Gold.....	1,315	1.32	Tin.....	500	2.22
Silver.....	1,224	1.37			

¹ A. Mallock, Proc. Roy. Soc. of London, 95, A, p. 429; 1919.

Note.—Modulus itself does not bear any simple relation to the melting point, but there is some relation between the variation of the modulus with temperature and the melting point.

TABLE 41.—Effect of Temperature on Modulus of Elasticity of Annealed Metals.¹

Material.	15° C. (59° F.).		100° C. (212° F.).		200° C. (392° F.).	
	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²	kg/mm ²	lb./in. ²
Copper.....	10,519	14,950,000	9,327	14,000,000	7,862	11,200,000
Gold.....	5,584	7,925,000	5,408	7,680,000	5,482	7,790,000
Lead.....	1,727	2,450,000	1,650	2,320,000		
Platinum.....	15,518	22,100,000	14,178	20,150,000	12,964	18,400,000
Silver.....	7,140	10,150,000	7,274	10,350,000	6,374	9,050,000
Iron.....	20,794	29,550,000	21,877	31,100,000	17,700	25,200,000
Cast steel.....	19,561	27,800,000	19,014	27,000,000	17,926	25,500,000

¹ Winkelman, Handbuch der Physik, 1, i, p. 564; 1908.

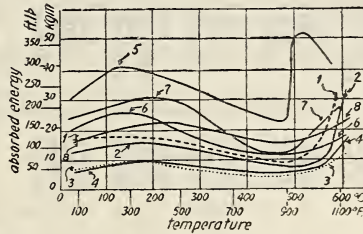


FIG. 60.—Effect of temperature on the impact resistance of annealed steels.

Proc. Internat. Association for Testing Materials, 5th Congress, III-4. The test pieces were of Mesnager type, 10 by 10 by 60 mm with notches 2 mm wide and 2 mm deep with round bottom. For chemical composition of tested steels see Table 20.

TABLE 42.—Effect of Annealing Temperature on Elastic Properties of Cold-Rolled Brass Tube.¹

Property.	Material. ²	Annealing temperature, °C.							
		100 (212° F.).	215 (419° F.).	310 (590° F.).	410 (770° F.).	520 (968° F.).	610 (1,130° F.).	710 (1,310° F.).	800 (1,472° F.).
Modulus of elasticity in tension.	{Hard.....	10,680	10,835	10,970	11,550	11,500	11,270	11,270	12,400
	{Half hard.....	15,170,000 (kg./mm. ²) 11,850 (lb./in. ²)	15,630,000 (kg./mm. ²) 12,010 (lb./in. ²)	15,810,000 (kg./mm. ²) 11,810 (lb./in. ²)	16,810,000 (kg./mm. ²) 12,300 (lb./in. ²)	17,090,000 (kg./mm. ²) 12,300 (lb./in. ²)	16,950,000 (kg./mm. ²) 11,910 (lb./in. ²)	16,020,000 (kg./mm. ²) 12,000 (lb./in. ²)	16,020,000 (kg./mm. ²) 12,250 (lb./in. ²)
Modulus of elasticity in compression.	{Hard.....	10,120	9,910	10,640	10,640	10,600	9,960	9,540
	{Half hard.....	14,400,000 (kg./mm. ²) 10,510 (lb./in. ²)	14,100,000 (kg./mm. ²) 11,490 (lb./in. ²)	14,100,000 (kg./mm. ²) 11,200 (lb./in. ²)	15,130,000 (kg./mm. ²) 11,410 (lb./in. ²)	15,080,000 (kg./mm. ²) 11,300 (lb./in. ²)	14,170,000 (kg./mm. ²) 10,330 (lb./in. ²)	13,570,000 (kg./mm. ²) 10,960 (lb./in. ²)	15,600,000 (kg./mm. ²) 11,100 (lb./in. ²)
Compressive elastic limit.	{Hard.....	23.9	33.3	33.5	13.5	15.5	8.9
	{Half hard.....	34,000 (kg./mm. ²) 18.9 (lb./in. ²)	29,600 (kg./mm. ²) 17.8 (lb./in. ²)	47,400 (kg./mm. ²) 24.5 (lb./in. ²)	33,200 (kg./mm. ²) 24.9 (lb./in. ²)	35,500 (kg./mm. ²) 25,300 (lb./in. ²)	20,200 (kg./mm. ²) 14.2 (lb./in. ²)	12,650 (kg./mm. ²) 8.7 (lb./in. ²)	4.4 (kg./mm. ²) 6,180 (lb./in. ²)
Compressive strength.	{Hard.....	39.2	47.0	18.2	18.2	17.2	11.8	8.3
	{Half hard.....	55,700 (kg./mm. ²) 28.2 (lb./in. ²)	54,300 (kg./mm. ²) 28.7 (lb./in. ²)	66,800 (kg./mm. ²) 36.7 (lb./in. ²)	56,500 (kg./mm. ²) 34.1 (lb./in. ²)	48,400 (kg./mm. ²) 35,900 (lb./in. ²)	24,400 (kg./mm. ²) 15.7 (lb./in. ²)	16,750 (kg./mm. ²) 11.5 (lb./in. ²)	11,900 (kg./mm. ²) 9.7 (lb./in. ²)
Modulus of elasticity in shear.	{Hard.....	3,810	3,880	3,950	4,180	4,240	4,100	4,100	4,420
	{Half hard.....	5,420,000 (kg./mm. ²) 3,870 (lb./in. ²)	5,530,000 (kg./mm. ²) 3,870 (lb./in. ²)	5,620,000 (kg./mm. ²) 3,980 (lb./in. ²)	5,620,000 (kg./mm. ²) 3,970 (lb./in. ²)	5,650,000 (kg./mm. ²) 4,000 (lb./in. ²)	6,030,000 (kg./mm. ²) 4,170 (lb./in. ²)	5,840,000 (kg./mm. ²) 4,210 (lb./in. ²)	6,290,000 (kg./mm. ²) 4,720 (lb./in. ²)
Shearing strength.	{Hard.....	36.7	35.9	34.4	16.6	16.2	14.0	10.5	6.4
	{Half hard.....	52,200 (kg./mm. ²) 22.2 (lb./in. ²)	51,100 (kg./mm. ²) 22.1 (lb./in. ²)	49,000 (kg./mm. ²) 23.6 (lb./in. ²)	43,000 (kg./mm. ²) 20.9 (lb./in. ²)	29,800 (kg./mm. ²) 33,600 (lb./in. ²)	23,100 (kg./mm. ²) 13.1 (lb./in. ²)	19,900 (kg./mm. ²) 11.3 (lb./in. ²)	15,000 (kg./mm. ²) 10.3 (lb./in. ²)

¹ F. C. Lea, V. A. Collins, and E. A. F. Reavey, Jour. Inst. of Metals, 29, p. 217, 1933.

²The chemical composition of tested materials: {hard..... 67.08 Cu 32.45 Zn 0.44 Fe
{half hard... 73.85 Cu 25.90 Zn 0.25 Fe

XIII. MANILA ROPE.

TABLE 43.—Weight and Strength of Manila Rope—Specification Values.

[From U. S. Government standard specifications adopted Apr. 4, 1918, and formulated jointly by cordage manufacturers and Government representatives. Rope to be made of manila or Abaca fiber, with no fiber of grade lower than U. S. Government grade (1) to be three-strand¹ medium laid, with maximum weights and minimum strengths shown in the table below, lubricant content to be not less than 8 nor more than 12 per cent of the weight of the rope as sold.]

Approximate diameter.		Circumference.		Maximum net weight.		Minimum breaking strength.	
mm	in.	mm	in.	kg/m	lb./ft.	kg	lb.
6.3	$\frac{1}{4}$	19.1	$\frac{3}{4}$	0.029	0.0196	317	700
7.9	$\frac{5}{16}$	25.4	1	.042	.0286	544	1,200
9.5	$\frac{3}{8}$	28.6	1 $\frac{1}{16}$.061	.0408	657	1,450
11.1	$\frac{7}{16}$	31.8	1 $\frac{1}{8}$.080	.0539	793	1,750
11.9	$\frac{1}{2}$	34.9	1 $\frac{3}{8}$.095	.0637	952	2,100
12.7	$\frac{9}{16}$	38.1	1 $\frac{1}{2}$.109	.0735	1,110	2,450
14.3	$\frac{5}{8}$	44.5	1 $\frac{3}{4}$.153	.1029	1,430	3,150
15.9	$\frac{3}{4}$	50.8	2	.195	.1307	1,810	4,000
19.1	$\frac{7}{8}$	57.2	2 $\frac{1}{8}$.241	.1617	2,220	4,900
20.6	$\frac{1}{2}$	63.5	2 $\frac{3}{8}$.284	.1911	2,680	5,900
22.2	$\frac{7}{8}$	69.8	2 $\frac{3}{4}$.328	.2205	3,170	7,000
25.4	$\frac{1}{8}$	76.2	3	.394	.2645	3,720	8,200
27.0	1	82.6	3 $\frac{1}{8}$.459	.3087	4,310	9,500
28.6	1 $\frac{1}{16}$	89.9	3 $\frac{1}{4}$.525	.3528	4,990	11,000
31.8	1 $\frac{1}{8}$	95.2	3 $\frac{3}{8}$.612	.4115	5,670	12,500
33.3	1 $\frac{1}{4}$	101.6	4	.700	.4703	6,440	14,200
34.9	1 $\frac{1}{2}$	108.0	4 $\frac{1}{4}$.787	.5290	7,260	16,000
38.1	1 $\frac{3}{8}$	114.3	4 $\frac{3}{8}$.875	.5879	7,940	17,500
39.7	1 $\frac{7}{16}$	120.7	4 $\frac{7}{16}$.984	.6615	8,840	19,500
41.2	1 $\frac{1}{2}$	127.0	5	1.094	.7348	9,750	21,500
44.5	1 $\frac{3}{4}$	139.7	5 $\frac{1}{2}$	1.312	.8818	11,550	25,500
50.8	2	152.4	6	1.576	1.059	13,610	30,000
52.4	2 $\frac{1}{16}$	165.1	6 $\frac{1}{2}$	1.823	1.225	15,420	34,000
57.2	2 $\frac{1}{8}$	177.8	7	2.144	1.441	17,460	38,500
63.5	2 $\frac{3}{8}$	190.5	7 $\frac{1}{2}$	2.450	1.646	19,730	43,500
66.7	2 $\frac{1}{2}$	203.2	8	2.799	1.881	22,220	49,000
73.0	2 $\frac{7}{8}$	215.9	8 $\frac{1}{2}$	3.136	2.107	24,940	55,000
76.2	3	228.6	9	3.543	2.381	27,670	61,000
79.4	3 $\frac{1}{8}$	241.3	9 $\frac{1}{2}$	3.936	2.645	30,390	67,000
82.5	3 $\frac{1}{4}$	254.0	10	4.375	2.940	33,110	73,000

¹ Four-strand medium-laid rope, when ordered, may run up to 7 per cent heavier than three-strand rope of the same size, and must show 95 per cent of the strength required for three-strand rope of the same size.

TABLE 44.—Strength of Manila Rope.

[Experimental formula derived from the tests $L=5,000 d (d+1)$, where L is breaking load in pounds; d—diameter of rope in inches. (U. S. Bureau of Standards Tech. Paper No. 198; 1921.)]

Diameter.		Number of tests.	Observed breaking load.						Government standard specifications, breaking load.	
cm	in.		Maximum.		Minimum.		Average.		kg	lb.
			kg	lb.	kg	lb.	kg	lb.	kg	lb.
1.27	$\frac{1}{2}$	23	1,777	3,920	1,043	2,300	1,474	3,250	1,111	2,450
1.59	$\frac{5}{16}$	17	2,971	6,550	1,928	4,250	2,404	5,300	1,814	4,000
1.91	$\frac{3}{8}$	14	3,183	7,020	2,350	5,180	2,881	6,350	2,223	4,900
2.06	$\frac{7}{16}$	26	3,959	8,730	2,654	5,850	3,220	7,100	2,676	5,900
2.54	1	72	5,761	12,700	3,538	7,800	4,432	9,770	3,720	8,200
2.86	1 $\frac{1}{8}$	9	5,851	12,900	3,946	8,700	5,207	11,480	4,990	11,000
3.17	1 $\frac{1}{4}$	76	7,983	17,600	4,727	10,420	6,192	13,650	5,670	12,500
3.81	1 $\frac{1}{2}$	48	11,249	24,800	6,023	13,280	8,364	18,440	7,938	17,500
4.12	1 $\frac{3}{8}$	14	11,435	25,210	7,444	16,410	9,902	21,830	9,752	21,500
4.44	1 $\frac{7}{16}$	14	14,120	31,130	9,072	20,000	11,078	24,400	11,567	25,500
5.08	2	5	12,338	27,200	10,496	23,140	11,857	26,140	13,608	30,000
6.35	2 $\frac{1}{2}$	8	24,812	54,700	14,651	32,300	19,958	44,000	19,732	43,500
7.62	3	22	33,566	74,000	20,412	45,000	26,898	59,300	27,670	61,000
8.88	3 $\frac{1}{2}$	17	47,628	105,000	26,354	58,100	38,919	85,800
10.16	4	2	52,482	115,700	39,690	87,500	46,086	101,600
11.43	4 $\frac{1}{2}$	1	49,896	110,000	49,896	110,000

XIV. WOOD.

The data on mechanical and physical properties of woods grown in the United States given in the tables below have been taken from Bulletin 556, Forest Service, U. S. Department of Agriculture, and are based upon about 130,000 tests.

The strength of green material should be made the basis of stresses. The bulletin recommends the following method of utilizing its data for green material. (Table 45.)

1. STATIC BENDING.

(a) For carefully selected structural timbers (with all exceptionally light pieces excluded) subjected to bending in dry, interior construction and where only small deflections are allowable safe working stresses are about one-fifth the modulus of rupture values given for green material. (Table 45.) (b) The values for modulus of elasticity are derived from the static bending test but are applicable to both beams and columns. Various factors tend to produce unequal local stresses which in their turn lead to deflections greater than those calculated from the average moduli of elasticity: For this reason it is good practice in the design of structures to use values for moduli of elasticity about one-half those given in Table 45.

2. COMPRESSION PARALLEL TO GRAIN.

A safe working stress for carefully selected structural timbers used as columns and in dry, interior construction (all exceptionally light pieces excluded) is about one-third the crushing strength as given in the table for tests on green materials. (Table 45.)

If the column is longer than about 10 times its least dimension, some formula should be used which will take care of the increased stress caused by eccentric loading or by the bending of the column.

3. COMPRESSION PERPENDICULAR TO GRAIN.

Two-thirds of the fiber stress at elastic limit, as given in the table for tests on green material may be used as a safe stress in dry, interior construction.

4. SHEARING STRENGTH PARALLEL TO GRAIN.

Only about one-eighth of the values given in the table for green material should be used as allowable stress in horizontal shear in beams. For small details in timbers unaffected by shakes or checks the allowable stress may be taken as one-fourth the value listed for green timber.

5. TENSION PERPENDICULAR TO GRAIN.

The allowable stress should be one-fifth the values given in Table 45.

Table 46 should be considered as supplementary to Table 45. The properties of all species are not changed in the same proportion by drying, and all the properties are not equally affected.

The figures in Table 47 are presented as an aid to the interpretation of data given in Tables 45 and 46. They will assist in rendering more nearly comparable data which are not compared directly because of differences of moisture.

Column 2 (Table 47).—Suppose, it is desired to compare the modulus of rupture of air-dry black locust with that of air-dry bitternut hickory. According to Table 47 a 1 per cent change of moisture causes a 4 per cent change of modulus of rupture. Changing the hickory from 9.2 to 10 per cent moisture will decrease the strength by $(10 - 9.2) \times 4$ per cent = 3.2 per cent; 3.2 per cent of 18,850 = 600. Then the moduli of rupture of black locust and bitternut hickory each at 10 per cent moisture are 20,700 and 18,250 lb./in.², respectively.

Column 3.—Strength properties of a given species can be estimated with fair accuracy from the average specific gravity, since each varies according to some power of the specific gravity.

Suppose it is desired to estimate the modulus of rupture and work to maximum load of a stick of timber whose specific gravity is known to be 25 per cent above the average. Since modulus of rupture varies as the first and work to maximum load as the second power of the specific gravity, it is probable that the modulus of rupture and work to maximum load are, respectively, about 125 and 156 per cent ($1.56 = 1.25^2$) of the average values for the species.

TABLE 45.—Results of Tests on 126 Species of Wood Tested

U. S. Department of Agriculture

[Test specimens were 2 by 2 inches (50.8 by 50.8 mm) in section. Bending specimens

Common and botanical name and locality where grown.	Number of rings—		Percentage of summer wood.					Specific gravity oven dry (100° C. or 212° F.) based on—		Weight (green).		Shrinkage from green to oven dry condition.			Static bending.										
	Number of trees.		Percentage of moisture content determined at 100° C. (212° F.).					Volume when green		Volume when oven dry.		In volume (per cent of dimensions when green).		Radial (per cent of dimensions when green).			Tangential (per cent of dimensions when green).			Fiber stress at elastic limit.		Modulus of rupture.		Modulus of elasticity.	
	Per cm	Per in.	1	2	3	4	5	6	7	8	kg/m ³	lb./ft. ³	11	12	13	14	15	16	17	18	19	th. kg/cm ²	th. lb./in. ²	th. kg/cm ²	th. lb./in. ²
HARDWOODS.																									
Alder, red (<i>Alnus oregona</i>), Washington.	6	4.3	11	...	98	0.37	0.43	736	46	12.6	4.4	7.3	267	3,800	457	6,500	82.3	1,170							
Ash, biltmorean (<i>Fraxinus biltmoreana</i>), Tennessee.	5	6.7	17	49	42	.51	.58	720	45	12.6	4.2	6.9	387	5,500	654	9,300	94.2	1,340							
Ash, black (<i>Fraxinus nigra</i>), Michigan, Wisconsin.	15	9.5	24	53	83	.46	.53	848	53	15.2	5.0	7.8	183	2,600	422	6,000	71.7	1,020							
Ash, blue (<i>Fraxinus quadrangulata</i>), Kentucky.	5	4.7	12	49	39	.53	.60	736	46	11.7	3.9	6.5	401	5,700	675	9,600	87.2	1,240							
Ash, green (<i>Fraxinus lanceolata</i>), Missouri, Louisiana.	10	7.1	18	58	48	.52	.61	768	48	12.5	4.6	7.1	372	5,300	668	9,500	98.4	1,400							
Ash, Oregon (<i>Fraxinus oregona</i>), Oregon.	3	4.7	12	63	48	.50	.58	736	46	13.2	4.1	8.1	295	4,200	534	7,600	79.4	1,130							
Ash, pumpkin (<i>Fraxinus profunda</i>), Missouri.	3	8.3	21	46	51	.48	.55	736	46	12.0	3.7	6.3	316	4,500	534	7,600	73.1	1,040							
Ash, white (forest grown) (<i>Fraxinus americana</i>), Arkansas, West Virginia.	10	6.3	16	50	43	.52	.60	736	46	12.6	4.2	6.5	344	4,900	640	9,100	95.0	1,350							
Ash, white (second growth) (<i>Fraxinus americana</i>), New York.	5	3.5	9	63	40	.58	.71	817	51	14.0	5.3	8.7	429	6,100	759	10,800	115.4	1,640							
Aspen (<i>Populus tremuloides</i>), Wisconsin.	5	3.1	8	...	107	.36	.42	752	47	11.1	3.3	6.9	204	2,900	372	5,300	59.0	840							
Aspen, large-tooth (<i>Populus grandidentata</i>), Wisconsin.	5	3.1	8	...	96	.35	.41	688	43	11.6	3.1	7.9	225	3,200	408	5,800	83.0	1,180							
Basswood (<i>Tilia americana</i>), Pennsylvania, Wisconsin.	8	7.5	19	29	103	.33	.40	657	41	15.8	6.6	9.3	190	2,700	351	5,000	72.4	1,030							
Beech (<i>Fagus atropunica</i>), Indiana, Pennsylvania.	10	7.5	19	30	62	.54	.66	880	55	16.2	4.8	10.6	316	4,500	576	8,200	87.2	1,240							
Birch, paper (<i>Betula papyrifera</i>), Wisconsin.	5	2.4	6	36	72	.47	.60	817	51	16.3	6.6	8.2	204	2,900	408	5,800	71.0	1,010							
Birch, sweet (<i>Betula lenta</i>), Pennsylvania.	5	10.6	27	...	61	.59	.70	945	59	15.0	6.3	7.6	316	4,500	605	8,600	104.6	1,490							
Birch, yellow (<i>Betula lutea</i>), Pennsylvania, Wisconsin.	10	7.5	19	26	68	.54	.66	928	58	16.8	7.4	9.0	323	4,600	605	8,600	108.2	1,540							
Buckeye, yellow (<i>Aesculus octandra</i>), Tennessee.	5	5.9	15	...	141	.33	.38	785	49	12.0	3.5	7.8	183	2,600	337	4,800	68.9	980							
Buckthorn, cascara (<i>Rhamnus purshiana</i>), Oregon.	5	6.7	17	...	61	.50	.55	801	50	7.6	3.2	4.6	239	3,400	443	6,300	44.3	630							
Butternut (<i>Juglans cinerea</i>), Tennessee, Wisconsin.	10	3.5	9	...	104	.36	.40	737	46	10.2	3.3	6.1	204	2,900	380	5,400	68.2	970							
Cherry, black (<i>Prunus serotina</i>), Pennsylvania.	5	4.3	11	...	55	.47	.53	737	46	11.5	3.7	7.1	295	4,200	562	8,000	92.1	1,310							
Cherry, wild red (<i>Prunus pennsylvanica</i>), Tennessee.	5	2.4	6	...	46	.36	.42	528	33	12.8	2.8	10.3	204	2,900	351	5,000	73.1	1,040							
Chestnut (<i>Castanea dentata</i>), Maryland, Tennessee.	10	3.9	10	48	122	.40	.46	881	55	11.6	3.4	6.7	218	3,100	394	5,600	65.4	930							
Chinquapin, western (<i>Castanopsis chrysophylla</i>), Oregon.	5	5.9	15	...	134	.42	.48	976	61	13.2	4.6	7.4	295	4,200	492	7,000	71.7	1,020							

in a Green Condition in the Form of Small, Clear Pieces.

Bulletin No. 556, Sept. 15, 1917.]

were 30 inches (762 mm) long; others were shorter, depending on the kind of test.]

Static bending—Continued.				Impact bending.					Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.					
Work in bending—				Fiber stress at elastic limit.	Work in bending to elastic limit.	Height of drop causing complete failure; 11.03 kg (50 lb.) hammer.				Fiber stress at elastic limit.	Maximum crushing strength.	Compression perpendicular to grain; fiber stress at elastic limit.	Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		End.	Side.	kg	lb.	kg	lb.		
To elastic limit.	To maximum load.					cm	in.	kg/cm ²	lb./in. ²				kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²					kg	lb.
kg/cm ²	in. lb./in. ²	kg/cm ²	in. lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	in. lb./in. ²	cm	in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg	lb.	kg	lb.	41	42	43
20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	
0.049	0.70	0.56	8.0	562	8,000	0.18	2.6	55.9	22	185	2,650	208	2,960	21.8	310	54.2	770	27.4	390	250	550	200	440	
.092	1.31	.82	11.6	837	11,900	.34	4.9	76.2	30	250	3,560	280	3,980	61.9	880	86.5	1,230	38.0	540	431	950	386	850	
.030	.42	.87	12.4	506	7,200	.18	2.5	81.3	32	114	1,620	161	2,290	30.2	430	61.2	870	34.4	490	263	580	250	550	
.103	1.47	1.03	14.7	781	11,100	.35	5.0	109.2	43	249	3,540	294	4,180	69.6	990	108.3	1,540	40.8	580	518	1,140	468	1,030	
.080	1.14	.83	11.8	802	11,400	.35	5.0	86.4	34	250	3,560	295	4,200	64.0	910	88.6	1,260	41.5	590	436	960	395	870	
.065	.92	.86	12.2	626	8,900	.21	3.0	99.1	39	193	2,740	247	3,510	45.7	650	83.7	1,190	34.4	490	386	850	359	790	
.076	1.08	.66	9.4	619	8,800	.26	3.7	78.8	31	199	2,830	236	3,360	69.6	990	85.1	1,210	40.1	570	400	880	341	750	
.072	1.03	.94	13.4	823	11,700	.35	5.0	91.5	36	227	3,230	257	3,800	56.2	800	88.6	1,260	43.6	620	454	1,000	409	900	
.091	1.30	1.15	16.3	970	13,800	.41	5.9	119.4	47	258	3,820	324	4,610	55.5	790	112.5	1,600	55.5	790	518	1,140	491	1,080	
.046	.65	.48	6.9	485	6,900	.18	2.5	71.2	28	114	1,620	152	2,160	14.1	200	43.6	620	12.7	180	123	270	145	320	
.035	.50	.43	6.1	534	7,600	.19	2.7	45.7	18	150	2,130	191	2,720	19.0	270	57.0	810	27.4	390	200	440	168	370	
.030	.42	.37	5.2	436	6,200	.14	2.0	43.2	17	120	1,710	155	2,210	14.8	210	42.9	610	19.7	280	127	280	114	250	
.070	.99	.88	12.5	732	10,400	.30	4.2	101.6	40	179	2,550	231	3,280	42.9	610	85.1	1,210	53.4	760	431	950	372	820	
.034	.49	1.05	15.0	548	7,800	.19	2.7	114.3	45	116	1,650	155	2,210	21.1	300	55.5	790	26.7	380	182	400	222	490	
.057	.81	1.10	15.6	668	9,500	.22	3.1	111.8	44	186	2,650	250	3,560	36.6	520	85.8	1,220	38.7	550	463	1,020	404	890	
.056	.80	1.17	16.6	822	11,700	.32	4.5	101.6	40	194	2,760	243	3,460	31.6	450	78.0	1,110	33.7	480	372	820	336	740	
.029	.41	.38	5.4	457	6,500	.15	2.1	45.7	18	115	1,640	144	2,050	14.8	210	46.4	660	22.5	320	164	360	132	290	
.073	1.04	.94	13.4	612	8,700	.25	3.6	147.4	58	132	1,880	230	3,270	47.1	670	80.8	1,150	35.8	510	309	680	331	730	
.037	.52	.58	8.2	513	7,300	.18	2.5	61.0	24	138	1,960	170	2,420	19.0	270	53.4	760	30.2	430	186	410	177	390	
.056	.80	.90	12.8	717	10,200	.29	4.1	83.9	33	207	2,940	249	3,540	30.9	440	79.4	1,130	40.1	570	341	750	300	660	
.033	.47	.44	6.2	464	6,600	.15	2.1	55.8	22	129	1,830	153	2,170	18.3	260	47.8	680	21.1	300	200	440	177	390	
.041	.59	.49	7.0	555	7,900	.20	2.8	61.0	24	143	2,040	174	2,470	26.7	380	56.2	800	30.2	430	241	530	191	420	
.077	1.09	.67	9.5	619	8,800	.24	3.4	78.8	31	135	1,920	212	3,020	34.4	490	71.0	1,010	33.7	480	331	730	272	600	

TABLE 45.—Results of Tests on 126 Species of Wood Tested in

Common and botanical name and locality where grown.	Number of trees.		Number of rings—		Percentage of moisture content determined at 100° C. (212° F.).			Specific gravity oven dry (100° C. or 212° F.) based on—		Weight (green).		Shrinkage from green to oven dry condition.			Static bending.				
	Per cm	Per in.	Per cent	Summer wood.	Volume when green.	Volume when oven dry.	kg/m ³	lb./ft. ³	In volume (per cent of dimensions when green).	Radial (per cent of dimensions when green).	Tangential (per cent of dimensions when green).	Fiber stress at elastic limit.		Modulus of rupture.		Modulus of elasticity.			
												kg/cm ²	lb./in. ²	kg/cm ²	lb./in.	th. kg/cm ²	th. lb./in. ²		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
HARDWOODS—Continued.																			
Cottonwood (<i>Populus deltoides</i>), Missouri.	5	2.4	6	...	111	0.37	0.43	784	49	14.1	3.9	9.2	204	2,900	373	5,300	71.0	1,010	
Cottonwood, black (<i>Populus trichocarpa</i>), Washington.	5	2.4	6	...	132	.32	.37	737	46	12.4	3.6	8.6	204	2,900	338	4,800	75.2	1,070	
Cucumber tree (<i>Magnolia acuminata</i>), Tennessee.	5	5.5	14	...	80	.44	.52	800	50	13.6	5.2	8.8	295	4,200	520	7,400	110.0	1,560	
Dogwood, flowering (<i>Cornus florida</i>), Tennessee.	5	9.5	24	...	62	.64	.80	1,040	65	19.9	7.1	11.3	338	4,800	619	8,800	82.9	1,180	
Dogwood, western (<i>Cornus nuttallii</i>), Oregon.	5	8.3	21	...	52	.58	.70	880	55	17.2	6.4	9.6	295	4,200	577	8,200	76.6	1,090	
Elder, pale (<i>Sambucus glauca</i>), Oregon.	5	2.4	6	...	124	.46	.57	1,040	65	15.6	4.4	9.0	239	3,400	464	6,600	63.2	900	
Elm, cork (<i>Ulmus racemosa</i>), Wisconsin.	10	1.1	23	50	50	.58	.66	865	54	14.1	4.8	8.1	323	4,600	668	9,500	83.6	1,190	
Elm, slippery (<i>Ulmus pubescens</i>), Indiana, Wisconsin.	6	6.3	16	54	85	.48	.56	897	56	13.8	4.9	8.9	281	4,000	562	8,000	86.5	1,230	
Elm, white (<i>Ulmus americana</i>), Wisconsin, Pennsylvania.	6	7.1	18	31	88	.44	.54	832	52	14.4	4.2	9.5	253	3,600	485	6,900	72.4	1,030	
Gum, black (<i>Nyssa sylvatica</i>), Tennessee.	5	10.6	27	...	55	.46	.55	720	45	13.9	4.4	7.7	281	4,000	492	7,000	72.4	1,030	
Gum, blue (<i>Eucalyptus globulus</i>), California.	5	79	.62	.80	1,120	70	22.5	7.6	15.3	534	7,600	717	11,200	141.0	2,010	
Gum, cotton (<i>Nyssa aquatica</i>), Louisiana.	6	3.9	10	26	97	.46	.52	897	56	12.5	4.2	7.6	295	4,200	513	7,300	73.8	1,050	
Gum, red (<i>Liquidambar styraciflua</i>), Missouri.	10	6.3	16	...	81	.44	.53	800	50	15.0	5.2	9.9	260	3,700	478	6,800	80.8	1,150	
Hackberry (<i>Celtis occidentalis</i>), Indiana, Wisconsin.	6	4.7	12	56	65	.48	.56	800	50	13.8	4.8	8.9	204	2,900	457	6,500	66.8	950	
Haw, pear (<i>Crataegus tomentosa</i>), Wisconsin.	2	4.3	11	...	63	.62	...	1,010	63	274	3,900	534	7,600	67.5	960	
Hickory, big shellbark (<i>Hicoria laciniosa</i>), Mississippi, Ohio.	19	7.5	19	65	61	.62	...	1,010	63	19.2	7.6	12.6	394	5,600	738	10,500	94.2	1,340	
Hickory, bitternut (<i>Hicoria maiana</i>), Ohio.	11	4.3	11	70	66	.60	...	1,010	63	387	5,500	724	10,300	98.4	1,400	
Hickory, mockernut (<i>Hicoria alba</i>), West Virginia, Mississippi, Pennsylvania.	20	7.1	18	63	59	.64	...	1,025	64	17.9	7.8	11.0	443	6,300	780	11,100	110.4	1,570	
Hickory, nutmeg (<i>Hicoria myristicaeformis</i>), Mississippi.	5	8.7	22	59	74	.56	...	977	61	344	4,900	640	9,100	90.7	1,290	
Hickory, pecan (<i>Hicoria pecan</i>), Missouri.	5	4.7	12	63	63	.60	.69	977	61	13.6	4.9	8.9	366	5,200	689	9,800	96.3	1,370	
Hickory, pignut (<i>Hicoria glabra</i>), Ohio, Mississippi, Pennsylvania, West Virginia.	60	7.9	20	65	54	.66	...	1,025	64	17.9	7.2	11.5	436	6,200	822	11,700	116.0	1,650	
Hickory, shagbark (<i>Hicoria ovata</i>), Ohio, Mississippi, Pennsylvania, West Virginia.	24	7.5	19	66	60	.64	...	1,025	64	16.7	7.0	10.5	415	5,900	774	11,000	110.0	1,570	
Hickory, water (<i>Hicoria aquatica</i>), Mississippi.	2	5.9	15	67	80	.61	...	1,104	69	422	6,000	752	10,700	119.6	1,560	
Holly, American (<i>Ilex opaca</i>), Tennessee.	5	10.6	27	...	82	.50	.61	913	57	16.2	4.5	9.5	239	3,400	457	6,500	63.3	900	
Hornbeam (<i>Ostrya virginiana</i>), Wisconsin.	5	11.4	29	...	52	.63	.76	962	60	18.6	8.2	9.6	316	4,500	597	8,500	80.8	1,150	

a Green Condition in the Form of Small, Clear Pieces—Continued.

Static bending—Continued.				Impact bending.					Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.				
Work in bending—				Fiber stress at elastic limit.		Work in bending to elastic limit.		Height of drop causing complete failure; 11.03 kg (50-lb.) hammer.		Fiber stress at elastic limit.		Maximum crushing strength.								End.		Side.	
To elastic limit.		To maximum load.		kg/cm ²	lb./in. ²	kgcm/cm ³	in. lb./in. ³	cm	in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg	lb.	kg	lb.
20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43
0.034	0.49	0.51	7.3	506	7,200	0.16	2.3	53.4	21	124	1,770	160	2,280	16.9	240	47.8	680	28.8	410	173	380	154	340
.031	.44	.35	5.0	478	6,800	.15	2.2	50.8	20	124	1,770	152	2,160	14.1	200	42.2	600	19.0	270	127	280	114	250
.046	.66	.70	10.0	654	9,300	.20	2.9	76.2	30	194	2,760	221	3,140	28.8	410	69.6	990	30.9	440	272	600	236	520
.078	1.11	1.48	21.0	499	7,100	.25	3.5	147.4	58	256	3,640	72.4	1,030	106.8	1,520	640	1,410	640	1,410
.065	.92	1.19	17.0	689	9,800	.25	3.6	142.3	56	160	2,280	256	3,640	61.2	870	91.4	1,300	52.0	740	518	1,140	445	980
.051	.72	.62	8.8	562	8,000	.20	2.9	96.6	38	172	2,450	214	3,040	36.5	520	76.6	1,090	39.4	560	345	760	327	720
.084	1.20	1.39	19.8	773	11,000	.29	4.1	127.0	50	202	2,870	266	3,780	52.7	750	89.3	1,270	46.4	660	445	980	449	990
.058	.82	1.08	15.4	647	9,200	.24	3.4	119.4	47	200	2,840	233	3,320	35.8	510	78.1	1,110	45.7	650	340	750	300	660
.058	.83	.77	11.0	570	8,100	.20	2.9	86.4	34	161	2,290	202	2,880	27.4	390	64.7	920	39.4	560	277	610	250	550
.064	.91	.56	8.0	689	9,800	.28	4.0	76.2	30	172	2,440	214	3,040	42.2	600	77.4	1,100	40.1	570	359	790	291	640
.116	1.65	.98	13.9	998	14,200	.33	4.7	101.6	40	342	4,870	369	5,250	71.7	1,020	109.0	1,550	45.0	640	595	1,310	608	1,340
.069	.98	.58	8.3	632	9,000	.23	3.3	76.2	30	194	2,760	237	3,370	41.5	590	83.7	1,190	42.2	600	363	800	322	710
.057	.81	.66	9.4	703	10,000	.27	3.9	83.9	33	166	2,360	200	2,840	32.3	460	75.2	1,070	35.8	510	286	630	236	520
.041	.58	1.20	14.5	556	7,900	.22	3.1	122.0	48	145	2,060	186	2,650	34.4	490	75.2	1,070	44.3	630	345	760	313	690
.063	.89	1.60	22.7	219	3,110	68.9	980	95.6	1,360	554	1,220	545	1,200
.096	1.36	2.10	29.9	998	14,200	.49	7.0	264.1	104	193	2,740	276	3,920	70.3	1,000	83.7	1,190
.086	1.22	1.41	20.0	1,116	15,900	.60	8.5	167.6	66	304	4,330	321	4,570	69.6	990	87.2	1,240
.097	1.38	1.83	26.1	1,062	15,100	.47	6.7	223.5	88	274	3,900	315	4,480	70.3	1,000	90.0	1,280
.075	1.06	1.60	22.8	900	12,800	.43	6.1	137.2	54	255	3,620	280	3,980	66.1	940	72.4	1,030
.083	1.18	1.03	14.6	865	12,300	.35	5.0	134.6	53	214	3,040	280	3,990	67.5	960	104.0	1,480	47.8	680	577	1,270	595	1,310
.094	1.34	2.23	31.7	1,188	16,900	.62	8.8	226.0	89	278	3,950	338	4,810	80.2	1,140	96.3	1,370
.090	1.28	1.67	23.7	1,012	14,400	.45	6.4	187.9	74	241	3,430	322	4,580	70.3	1,000	92.8	1,320
.091	1.29	1.32	18.8	963	13,700	.43	6.1	142.4	56	228	3,240	328	4,660	76.7	1,090	101.2	1,440
.051	.72	.76	10.8	627	8,900	.31	4.4	129.5	51	139	1,970	186	2,640	42.9	610	79.5	1,130	42.9	610	391	860	359	790
.072	1.02	.93	13.3	745	10,600	.25	3.5	185.4	73	184	2,620	251	3,570	51.3	730	96.3	1,370	31.6	450	527	1,160	532	1,170

TABLE 45.—Results of Tests on 126 Species of Wood Tested in

Common and botanical name and locality where grown.	Number of rings—		Percentage of moisture content determined at 100° C. (212° F.) based on—				Specific gravity oven dry (100° C. or 212° F.) based on—		Weight (green).		Shrinkage from green to oven dry condition.			Static bending.				
	Number of trees.	Per cm	Per in.	Percentage of summer wood.		Volume when green.	Volume when oven dry.	kg/m ³	lb./ft. ³	In volume (per cent of dimensions when green).	Radial (per cent of dimensions when green).	Tangential (per cent of dimensions when green).	Fiber stress at elastic limit.		Modulus of rupture.		Modulus of elasticity.	
				5	6								7	8	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
HARDWOODS—Continued.																		
Laurel, California (<i>Umbellularia californica</i>), Oregon.	5	2.4	6	...	70	0.51	0.59	880	55	11.9	2.8	8.1	274	3,900	464	6,600	50.6	720
Laurel, mountain (<i>Kalmia latifolia</i>), Tennessee.	5	9.5	24	...	62	.62	.74	992	62	14.4	5.6	8.8	408	5,800	591	8,400	64.7	920
Locust, black (<i>Robinia pseudacacia</i>), Tennessee.	3	4.3	11	51	40	.66	.71	928	58	9.8	4.4	6.9	619	8,800	970	13,800	130.0	1,850
Locust, honey (<i>Gleditsia triacanthos</i>), Missouri, Indiana.	6	3.5	9	45	63	.60	.67	976	61	10.8	4.2	6.6	394	5,600	717	10,200	90.7	1,290
Madrona (<i>Arbutus menziesii</i>), California, Oregon.	6	3.9	10	...	68	.57	.69	962	60	17.4	5.4	11.9	330	4,700	534	7,600	61.9	880
Magnolia, evergreen (<i>Magnolia foetida</i>), Louisiana.	2	5.9	15	...	117	.46	.53	992	62	12.3	5.4	6.6	259	3,600	478	6,800	78.1	1,110
Maple, Oregon (<i>Acer macrophyllum</i>), Washington.	5	4.7	12	...	72	.44	.51	752	47	11.6	3.7	7.1	309	4,400	520	7,400	77.4	1,100
Maple, red (<i>Acer rubrum</i>), Pennsylvania, Wisconsin.	9	6.3	16	24	70	.48	.54	816	51	12.5	3.8	8.1	288	4,100	548	7,800	99.8	1,420
Maple, silver (<i>Acer saccharinum</i>), Wisconsin.	5	2.8	7	...	66	.44	.51	736	46	12.0	3.0	7.2	218	3,100	408	5,800	66.1	940
Maple, sugar (<i>Acer saccharum</i>), Indiana, Pennsylvania, Wisconsin.	17	8.3	21	49	60	.56	.66	897	56	14.5	4.8	9.2	351	5,000	640	9,100	104.2	1,480
Oak, bur (<i>Quercus macrocarpa</i>), Wisconsin.	5	4.7	12	59	70	.58	.67	977	61	12.7	4.4	8.8	253	3,600	506	7,200	61.9	880
Oak, California black (<i>Quercus californica</i>), California, Oregon.	10	6.3	16	52	106	.51	.58	1,058	66	12.1	3.6	6.6	239	3,400	436	6,200	52.0	740
Oak, canyon live (<i>Quercus chrysolepis</i>), California.	3	5.1	13	...	62	.70	.84	1,138	71	16.2	8.0	14.3	443	6,300	745	10,600	94.2	1,340
Oak, chestnut (<i>Quercus prinus</i>), Tennessee.	5	9.1	23	50	72	.57	.67	992	62	16.7	5.5	9.7	323	4,600	563	8,000	96.3	1,370
Oak, cow (<i>Quercus michauxii</i>), Louisiana.	4	4.7	12	58	76	.60	.76	1,040	65	19.4	5.9	9.2	337	4,800	598	8,500	95.0	1,350
Oak, laurel (<i>Quercus laurifolia</i>), Louisiana.	5	4.3	11	61	84	.56	.70	1,025	64	19.0	3.9	9.5	316	4,500	550	7,900	97.8	1,390
Oak, Pacific post (<i>Quercus garryana</i>), Oregon.	10	6.3	16	49	72	.64	.75	1,105	69	13.4	4.2	9.0	323	4,600	541	7,700	55.5	790
Oak, post (<i>Quercus minor</i>), Arkansas, Louisiana.	10	10.2	26	54	69	.60	.74	1,010	63	16.2	5.4	9.8	351	5,000	570	8,100	76.6	1,090
Oak, red (<i>Quercus rubra</i>), Arkansas, Louisiana, Indiana, Tennessee.	21	4.3	11	62	84	.56	.65	1,025	64	14.2	3.9	8.3	260	3,700	541	7,700	90.7	1,290
Oak, Spanish (highland) (<i>Quercus digitata</i>), Louisiana.	4	7.9	20	46	90	.52	.62	992	62	16.3	4.5	8.7	395	4,200	485	6,900	80.2	1,140
Oak, Spanish (lowland) (<i>Quercus pagodaefolia</i>), Louisiana.	3	2.8	7	63	78	.61	.71	1,072	67	16.4	5.2	10.8	457	6,500	760	10,800	126.0	1,790
Oak, water (<i>Quercus minor</i>), Louisiana.	5	3.9	10	61	81	.56	.68	1,008	63	16.4	4.2	9.3	394	5,600	626	8,900	109.0	1,550
Oak, white (<i>Quercus alba</i>), Arkansas, Louisiana, Indiana.	20	6.7	17	60	68	.60	.71	992	62	15.8	5.3	9.0	330	4,700	584	8,300	87.9	1,250
Oak, willow (<i>Quercus phellos</i>), Louisiana.	2	5.5	14	56	94	.56	.69	1,072	67	18.9	5.0	9.6	309	4,400	520	7,400	90.7	1,290

a Green Condition in the Form of Small, Clear Pieces—Continued.

Static bending—Continued.				Impact bending.					Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.				
Work in bending—				Fiber stress at elastic limit.		Work in bending to elastic limit.		Height of drop causing complete failure; 11.03 kg (50-lb.) hammer.		Fiber stress at elastic limit.		Maximum crushing strength.								End.		Side.	
To elastic limit.		To maximum load.		kg/cm ²		lb./in. ²		kg/cm ³		lb./in. ²		kg/cm ²		lb./in. ²		kg/cm ²		lb./in. ²		kg		lb.	
20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43
0.086	1.23	1.18	16.8	584	8,300	0.29	4.1	144.8	57	138	1,960	212	3,020	56.2	800	89.3	1,270	54.8	780	463	1,020	454	1,000
.143	2.03	.88	12.5	717	10,200	.37	5.2	81.3	32	303	4,310	78.1	1,110	117.4	1,670	636	1,400	590	1,300
.166	2.36	1.08	15.4	1,290	18,300	.56	7.9	111.8	44	442	6,280	478	6,800	100.5	1,430	123.6	1,760	54.2	770	745	1,640	713	1,570
.098	1.40	.89	12.6	830	11,800	.32	4.6	119.4	47	233	3,320	331	4,420	99.8	1,420	116.6	1,660	65.4	930	654	1,440	632	1,390
.100	1.43	.79	11.2	717	10,200	.33	4.7	101.6	40	165	2,340	233	3,320	54.8	780	99.8	1,420	54.2	770	509	1,120	427	940
.047	.67	1.08	15.4	618	8,800	.22	3.2	137.2	54	155	2,200	190	2,700	40.1	570	73.1	1,040	42.9	610	354	780	336	740
.072	1.02	.61	8.7	597	8,500	.20	2.8	58.5	23	167	2,380	228	3,240	38.6	550	78.1	1,110	42.2	600	345	760	281	620
.042	.60	.75	10.6	696	9,900	.26	3.7	76.2	30	176	2,500	235	3,350	36.5	520	75.9	1,080	40.8	580	336	740	272	600
.043	.61	.77	11.0	478	6,800	.18	2.6	73.7	29	137	1,950	175	2,490	32.3	460	73.8	1,050	39.4	560	304	670	268	590
.076	1.08	.84	11.9	851	12,100	.35	5.0	91.5	36	219	3,120	271	3,860	52.7	750	97.0	1,380	54.2	770	454	1,000	413	910
.063	.89	.75	10.7	703	10,000	.33	4.7	111.8	44	162	2,310	231	3,290	59.1	840	94.9	1,350	56.2	800	527	1,160	504	1,110
.072	1.03	.62	8.8	576	8,200	.24	3.4	76.2	30	132	1,880	197	2,800	62.6	890	80.2	1,140	49.2	700	413	910	386	850
.170	1.70	1.01	14.4	788	11,200	.27	3.9	119.4	47	285	4,050	330	4,690	104.0	1,480	119.6	1,700	68.2	970	722	1,590	713	1,570
.063	.90	.66	9.4	844	12,000	.32	4.6	88.9	35	203	2,890	247	3,520	46.4	660	85.1	1,210	48.5	690	440	970	404	890
.070	1.00	.90	12.8	731	10,400	.22	3.2	114.3	45	215	3,060	249	3,540	50.0	710	88.6	1,260	47.1	670	500	1,100	504	1,110
.060	.86	.79	11.2	731	10,400	.24	3.4	99.1	39	192	2,730	223	3,170	50.0	710	83.0	1,180	54.2	770	463	1,020	454	1,000
.106	1.51	.96	13.7	724	10,300	.34	4.8	124.5	49	176	2,510	251	3,570	97.1	1,380	114.5	1,630	66.1	940	649	1,430	631	1,390
.092	1.31	.77	11.0	766	10,900	.29	4.1	111.7	44	200	2,840	245	3,480	74.6	1,060	90.0	1,280	55.5	790	527	1,160	513	1,130
.046	.65	.81	11.5	731	10,400	.27	3.9	104.2	41	164	2,330	225	3,200	51.3	730	78.8	1,120	52.0	740	463	1,020	431	950
.065	.93	.56	8.0	640	9,100	.22	3.1	73.7	29	153	2,180	213	3,030	47.8	680	65.4	930	33.7	480	413	910	391	860
.093	1.32	1.03	14.7	865	12,300	.27	3.8	137.2	54	264	3,760	325	4,620	66.1	940	92.8	1,320	56.2	800	577	1,270	563	1,240
.080	1.14	.78	11.1	816	11,600	.27	3.8	99.1	39	225	3,200	263	3,740	54.2	770	87.2	1,240	57.6	820	477	1,050	459	1,010
.076	1.08	.81	11.5	752	10,700	.30	4.2	106.6	42	210	2,990	250	3,560	58.4	830	87.9	1,250	54.2	770	509	1,120	481	1,060
.062	.88	.62	8.8	647	9,200	.20	2.9	88.9	35	174	2,480	211	3,000	52.7	750	83.0	1,180	53.4	760	463	1,020	445	980

TABLE 45.—Results of Tests on 126 Species of Wood Tested in

Common and botanical name and locality where grown.	Number of rings—		Percentage of moisture content determined at 100° C. (212° F.),				Specific gravity oven dry (100° C. or 212° F.) based on—		Weight (green).		Shrinkage from green to oven dry condition.			Static bending.				
	Number of trees.	Per cm	Per in.	Percentage of summer wood.		Volume when green.	Volume when oven dry.	kg/m ³	lb./ft. ³	In volume (per cent of dimensions when green).	Radial (per cent of dimensions when green).	Tangential (per cent of dimensions when green).	Fiber stress at elastic limit.		Modulus of rupture.	Modulus of elasticity.		
				7	8								kg/cm ²	lb./in.		th. kg/cm ²	th. lb./in. ²	
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
HARDWOODS—Continued.																		
Oak, yellow (<i>Quercus velutina</i>), Arkansas, Wisconsin.	8	5.9	15	71	78	0.56	.67	1,008	63	14.2	4.5	9.7	323	4,600	576	8,200	83.0	1,180
Persimmon (<i>Diopyros virginiana</i>), Missouri.	5	5.5	14	...	58	.64	.78	1,008	63	18.3	7.5	10.8	394	5,600	703	10,000	96.3	1,370
Poplar, yellow (<i>Liriodendron tulipifera</i>), Tennessee.	5	5.5	14	...	64	.37	.42	608	38	11.4	4.1	6.9	225	3,200	394	5,600	85.1	1,210
Rhododendron, great (<i>Rhododendron maximum</i>), Tennessee.	5	11.0	28	...	99	.50	.60	992	62	16.2	6.3	8.7	323	4,600	485	6,900	61.2	870
Sassafras (<i>Sassafras sassafras</i>), Tennessee.	5	7.5	19	48	67	.42	.47	704	44	10.3	4.0	6.2	253	3,600	422	6,000	64.0	910
Serviceberry (<i>Amelanchier canadensis</i>), Tennessee.	5	7.5	19	...	48	.66	.79	977	61	18.7	6.7	10.8	394	5,600	675	9,600	115.3	1,640
Silverbell-tree (<i>Mohrodendrum carolinum</i>), Tennessee.	5	7.9	20	...	70	.42	.48	704	44	12.6	3.8	7.6	246	3,500	457	6,500	81.6	1,160
Sourwood (<i>Oxydendrum arboreum</i>), Tennessee.	5	9.4	24	...	69	.50	.59	848	53	15.2	6.3	8.9	309	4,400	542	7,700	92.8	1,320
Sumac, staghorn (<i>Rhus hirta</i>), Wisconsin.	5	3.5	9	61	45	.45	656	41	211	3,000	408	5,800	57.0	810
Sugarberry (<i>Celtis mississippiensis</i>), Missouri.	5	6.7	17	38	62	.47	.54	768	48	12.7	5.0	7.3	225	3,200	464	6,600	57.0	810
Sycamore (<i>Platanus occidentalis</i>), Indiana, Tennessee.	10	6.3	16	77	83	.46	.54	832	52	14.2	5.1	7.6	232	3,300	457	6,500	74.6	1,060
Umbrella, Fraser (<i>Magnolia fraseri</i>), Tennessee.	5	5.9	15	...	89	.40	.48	753	47	13.0	4.4	7.5	239	3,400	429	6,100	83.7	1,190
Walnut, black (<i>Juglans nigra</i>), Kentucky.	5	4.7	12	...	81	.51	.56	928	58	11.3	5.2	7.1	380	5,400	668	9,500	99.8	1,420
Willow, black (<i>Salix nigra</i>), Wisconsin, Missouri.	10	2.0	5	...	138	.34	.41	800	50	13.8	2.6	7.8	127	1,800	267	3,800	39.4	560
Willow, western black (<i>Salix lasiandra</i>), Oregon.	5	2.0	5	...	105	.39	.47	800	50	13.8	2.9	9.0	218	3,100	394	5,600	71.7	1,020
Witch-hazel (<i>Hamamelis virginiana</i>), Tennessee.	5	5.5	14	...	70	.56	.71	944	59	18.8	351	5,000	584	8,300	78.1	1,110
CONIFERS.																		
Cedar, incense (<i>Libocedrus decurrens</i>), California, Oregon.	8	6.3	16	30	108	.35	.36	720	45	7.6	3.3	5.7	274	3,900	436	6,200	59.1	840
Cedar, Port Orford (<i>Chamaecyparis lawsoniana</i>), Oregon.	5	9.5	24	25	52	.41	.47	624	39	10.7	5.2	8.1	274	3,900	478	6,800	105.4	1,500
Cedar, western red (<i>Thuja plicata</i>), Washington, Montana.	10	7.9	20	36	39	.31	.34	432	27	8.1	2.5	5.1	232	3,300	366	5,200	66.8	950
Cedar, white (<i>Thuja occidentalis</i>), Wisconsin.	5	9.1	23	36	55	.29	.32	448	28	7.0	2.1	4.9	183	2,600	295	4,200	32.3	460
Cypress, bald (<i>Taxodium distichum</i>), Louisiana, Missouri.	10	6.3	16	31	87	.41	.47	768	48	10.7	3.8	6.0	281	4,000	478	6,800	83.7	1,190
Cypress, yellow (<i>Chamaecyparis nootkatensis</i>), Oregon.	5	12.2	31	...	40	.40	.44	560	35	7.9	1.9	5.0	253	3,600	436	6,200	67.5	960
Douglas fir (<i>Pseudotsuga taxifolia</i>), Washington, Oregon.	18	5.1	13	35	36	.45	.52	608	38	12.6	5.0	7.9	351	5,000	548	7,800	111.2	1,580

a Green Condition in the Form of Small, Clear Pieces—Continued.

Static bending—Continued.				Impact bending.					Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.				
Work in bending—		Fiber stress at elastic limit.	Work in bending to elastic limit.	Height of drop causing complete failure; 11.03 kg (50-lb.) hammer.		Fiber stress at elastic limit.		Maximum crushing strength.		Fiber stress at elastic limit.	Maximum crushing strength.	Compression perpendicular to grain; fiber stress at elastic limit.	Shearing strength parallel to the grain.	Tensile strength perpendicular to grain.	End.	Side.							
To elastic limit.	To maximum load.			cm	in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²								kg/cm ²	lb./in. ²	kg	lb.	kg	lb.	
kg/cm ²	in. lb./in. ²	kg/cm ²	in. lb./in. ²	kg/cm ²	lb./in. ²	cm	in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg	lb.	kg	lb.				
20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43
0.084	1.20	0.87	12.3	760	10,800	0.31	4.4	101.6	40	202	2,870	256	3,640	61.2	870	83.0	1,180	58.4	830	454	1,000	481	1,060
.095	1.35	.91	13.0	851	12,100	.32	4.5	104.1	41	213	3,030	293	4,170	78.0	1,110	103.4	1,470	54.2	770	563	1,240	581	1,280
.034	.48	.39	5.6	562	8,000	.18	2.6	43.2	17	141	2,000	179	2,550	21.8	310	55.5	790	32.3	460	191	420	154	340
.097	1.38	.85	12.1	66.1	26	263	3,470	62.6	890	87.2	1,240	454	1,000	391	860
.056	.80	.50	7.1	598	8,500	.25	3.5	94.0	37	170	2,410	192	2,730	32.3	460	66.8	950	36.5	520	277	610	236	520
.076	1.08	1.14	16.2	858	12,200	.29	4.1	160.0	63	225	3,200	287	4,080	54.8	780	88.6	1,260	51.3	730	568	1,250	563	1,240
.044	.62	.62	8.8	640	9,100	.23	3.3	68.6	27	148	2,110	199	2,830	30.2	430	65.4	930	32.3	460	250	550	213	470
.058	.82	.69	9.8	760	10,800	.29	4.1	96.6	38	191	2,720	229	3,250	47.8	680	81.6	1,160	49.9	710	391	860	331	730
.047	.67	.76	10.8	188	2,680	33.7	480	304	670	268	590
.055	.78	.84	12.0	576	8,200	.22	3.2	83.9	33	137	1,950	197	2,800	40.8	580	73.8	1,050	46.4	660	381	840	336	740
.042	.60	.53	7.5	619	8,800	.23	3.3	66.1	26	168	2,390	205	2,920	31.6	450	70.3	1,000	44.3	630	318	700	277	610
.039	.55	.58	8.3	604	8,600	.20	2.9	58.4	23	158	2,250	184	2,610	23.2	330	58.4	830	31.6	450	259	570	227	500
.082	1.16	1.26	14.6	837	11,900	.32	4.5	94.0	37	253	3,600	302	4,300	42.2	600	85.8	1,220	40.1	570	436	960	409	900
.025	.36	.76	10.8	358	5,100	.14	2.0	91.5	36	68.2	970	106.1	1,510	14.8	210	43.6	620	30.2	430	159	350	164	360
.041	.58	.76	10.8	534	7,600	.18	2.5	83.9	33	127.1	1,810	164.4	2,340	23.2	330	61.2	870	25.3	360	223	490	227	500
.091	1.29	1.37	19.5	872	12,400	.44	6.3	101.6	40	239	3,400	43.6	620	78.8	1,120	459	1,010	445	980
.066	.94	.45	6.4	513	7,300	.17	2.4	43.2	17	201.8	2,870	221.5	3,150	32.3	460	58.4	830	19.7	280	259	570	177	390
.041	.59	.55	7.8	654	9,300	.19	2.7	63.5	25	208.8	2,970	230.5	3,280	26.7	380	61.9	880	16.9	240	254	560	218	480
.045	.64	.35	5.0	499	7,100	.17	2.4	43.2	17	175.6	2,500	199.5	2,840	21.8	310	50.6	720	14.8	210	195	430	118	260
.042	.60	.40	5.7	372	5,300	.14	2.0	38.1	15	98.8	1,420	140	1,990	20.4	290	43.6	620	16.9	240	145	320	104	230
.060	.86	.45	6.4	562	8,000	.18	2.6	61.0	24	218	3,100	245	3,490	33.0	470	57.6	820	19.7	280	213	470	173	380
.054	.77	.67	9.5	604	8,600	.22	3.2	68.6	27	168	2,390	203	2,880	28.8	410	57.6	820	18.3	260	236	520	186	410
.060	.86	.47	6.7	661	9,400	.20	2.9	63.5	25	239	3,400	277	3,940	37.2	530	64.0	910	14.1	200	232	510	213	470

TABLE 45.—Results of Tests on 126 Species of Wood Tested in

Common and botanical name and locality where grown.	Number of trees.		Number of rings—		Percentage of moisture content determined at 100° C. (212° F.)				Specific gravity oven dry (100° C. or 212° F.) based on—		Weight (green).		Shrinkage from green to oven dry condition.			Static bending.				
	Per cm	Per in.	Per cent of summer wood.	Per cent of summer wood.	Volume when green.	Volume when oven dry.	kg/m ³	lb./ft. ³	In volume (per cent of dimensions when green).	Radial (per cent of dimensions when green).	Tangential (per cent of dimensions when green).	kg/cm ²	lb./in. ²	Fiber stress at elastic limit.		Modulus of rupture.		Modulus of elasticity.		
														kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	th. kg/cm ²	th. lb./in. ²	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19		
CONIFERS—Continued.																				
Douglas fir (<i>Pseudotsuga taxifolia</i>), Montana, Wyoming.	10	8.7	22	27	38	0.40	0.44	544	34	10.6	3.6	6.2	253	3,600	450	6,400	83.0	1,180		
Fir, Alpine (<i>Abies lasiocarpa</i>), Colorado.	5	5.9	15	14	47	.31	.32	448	28	9.0	2.5	7.1	169	2,400	309	4,400	60.4	860		
Fir, amabilis (<i>Abies amabilis</i>), Oregon, Washington.	20	3.1	8	26	102	.37	.42	752	47	14.1	4.5	10.0	274	3,900	443	6,300	91.4	1,300		
Fir, balsam (<i>Abies balsamea</i>), Wisconsin.	5	4.7	12	26	117	.34	.41	720	45	10.8	2.8	6.6	211	3,000	344	4,900	67.5	960		
Fir, grand (<i>Abies grandis</i>), Montana, Oregon.	10	7.1	18	30	94	.37	.42	705	44	10.6	3.2	7.2	253	3,600	429	6,100	91.4	1,300		
Fir, noble (<i>Abies nobilis</i>), Oregon.	5	9.1	23	17	41	.35	.41	496	31	13.6	4.9	9.1	239	3,400	401	5,700	90.0	1,280		
Fir, white (<i>Abies concolor</i>), California.	5	3.9	10	30	156	.35	.44	897	56	10.2	3.4	7.0	274	3,900	422	6,000	79.4	1,130		
Hemlock, black (<i>Tsuga mertensiana</i>), Montana.	5	9.1	23	45	70	.42	.48	720	45	10.8	4.4	7.1	246	3,500	422	6,000	66.1	940		
Hemlock, eastern (<i>Tsuga canadensis</i>), Tennessee, Wisconsin.	10	7.9	20	34	105	.38	.44	768	48	10.4	3.0	6.4	295	4,200	471	6,700	78.7	1,120		
Hemlock, western (<i>Tsuga heterophylla</i>), Washington.	5	3.9	10	27	71	.38	.43	656	41	11.6	4.5	7.9	239	3,400	429	6,100	83.7	1,190		
Larch, western (<i>Larix occidentalis</i>), Montana, Washington.	13	12.6	32	37	58	.48	.59	768	48	13.2	4.2	8.1	323	4,600	527	7,500	94.9	1,350		
Pine, Cuban (<i>Pinus heterophylla</i>), Florida.	5	6.7	17	44	47	.58	.68	849	53	12.7	5.9	7.5	393	5,600	618	8,800	114.6	1,630		
Pine, jack (<i>Pinus divaricata</i>), Wisconsin.	5	2.8	7	30	105	.39	.46	801	50	10.4	3.4	6.5	211	3,000	380	5,400	64.7	920		
Pine, Jeffrey (<i>Pinus jeffreyi</i>), California.	5	7.1	18	23	101	.37	.42	753	47	9.9	4.4	6.7	225	3,200	352	5,000	68.9	980		
Pine, loblolly (<i>Pinus taeda</i>), Florida, North Carolina, South Carolina.	15	3.1	8	42	70	.50	.59	865	54	12.6	5.5	7.5	309	4,400	527	7,500	97.0	1,380		
Pine, lodgepole (<i>Pinus contorta</i>), Colorado, Montana, Wyoming.	28	9.5	24	22	65	.38	.44	625	39	11.5	4.5	6.7	211	3,000	387	5,500	76.0	1,080		
Pine, longleaf (<i>Pinus palustris</i>), Florida, Louisiana, Mississippi.	34	7.1	18	39	47	.55	.64	801	50	12.3	5.3	7.5	380	5,400	612	8,700	114.5	1,630		
Pine, Norway (<i>Pinus resinosa</i>), Wisconsin.	5	8.7	22	41	54	.44	.51	673	42	11.5	4.6	7.2	260	3,700	450	6,400	97.0	1,380		
Pine, pitch (<i>Pinus rigida</i>), Tennessee.	5	4.7	12	30	85	.47	.54	865	54	11.7	4.8	7.4	260	3,700	471	6,700	78.8	1,120		
Pine, pond (<i>Pinus serotina</i>), Florida.	5	5.1	13	35	56	.50	.58	785	49	11.2	5.1	7.1	316	4,500	520	7,400	90.0	1,280		
Pine, shortleaf (<i>Pinus echinata</i>), Arkansas, Louisiana.	12	4.7	12	40	64	.50	.58	800	50	12.6	5.1	8.2	316	4,500	562	8,000	101.9	1,450		
Pine, sugar (<i>Pinus lambertiana</i>), California.	5	4.7	12	34	123	.36	.39	800	50	8.4	2.9	5.6	232	3,300	372	5,300	68.2	970		
Pine, table-mountain (<i>Pinus pungens</i>), Tennessee.	5	5.9	15	29	75	.49	.55	865	54	10.9	3.4	6.8	316	4,500	527	7,500	89.3	1,270		
Pine, western white (<i>Pinus monticola</i>), Montana.	5	11.0	28	33	58	.39	.45	625	39	11.5	4.1	7.4	246	3,500	401	5,700	93.5	1,330		

a Green Condition in the Form of Small, Clear Pieces—Continued.

Static bending—Continued.				Impact bending.					Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.								
Work in bending—				Fiber stress at elastic limit.	Work in bending to elastic limit.	Height of drop causing complete failure; 11.03 kg (50-lb.) hammer.				Fiber stress at elastic limit.	Maximum crushing strength.		Fiber stress at elastic limit.	Maximum crushing strength.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg	lb.	kg	lb.	
To elastic limit.	To maximum load.					cm	in.	kg/cm ²	lb./in. ²		kg/cm ²	lb./in. ²															kg/cm ²
20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43				
0.046	0.65	0.48	6.8	640	9,100	0.21	3.0	50.8	20	177	2,520	211	3,000	31.6	450	61.9	880	24.6	350	204	450	182	400				
.027	.39	.31	4.4	373	5,300	.11	1.6	22.9	9	117	1,660	145	2,060	21.8	310	42.9	610	127	280	100	220				
.042	.60	.42	6.0	548	7,800	.15	2.2	53.4	21	167	2,380	205	2,930	22.5	320	47.1	670	16.9	240	163	360	141	310				
.037	.52	.33	4.7	485	6,900	.16	2.3	40.7	16	156	2,220	169	2,400	14.8	210	42.9	610	12.7	180	132	290	132	290				
.041	.58	.39	5.6	569	8,100	.18	2.6	55.9	22	188	2,680	212	3,010	23.9	340	53.4	760	16.2	230	191	420	163	360				
.037	.53	.44	6.2	555	7,900	.18	2.6	50.8	20	167	2,370	190	2,700	21.8	310	49.2	700	12.7	180	136	300	114	250				
.054	.77	.37	5.2	507	7,200	.15	2.2	45.7	18	184	2,610	197	2,800	30.9	440	51.3	730	18.3	260	173	380	150	330				
.055	.78	.66	9.4	619	8,800	.25	3.6	91.5	36	182	2,590	203	2,890	28.1	400	61.9	880	25.3	360	263	580	209	460				
.062	.88	.48	6.8	555	7,900	.20	2.8	50.8	20	191	2,710	230	3,270	35.1	500	61.9	880	18.3	260	232	510	186	410				
.041	.58	.42	6.0	548	7,800	.17	2.4	50.8	20	161	2,290	203	2,890	24.6	350	57.0	810	18.3	260	245	540	195	430				
.071	1.01	.50	7.1	661	9,400	.26	3.7	61.0	24	228	3,250	267	3,800	39.4	560	64.7	920	16.2	230	213	470	204	450				
.077	1.10	.56	7.9	795	11,300	.27	3.9	94.1	37	278	3,950	314	4,470	41.5	590	72.4	1,030	20.4	290	259	570	286	630				
.039	.55	.41	5.9	548	7,800	.23	3.3	76.2	30	158	2,250	182	2,580	26.7	380	53.4	760	21.8	310	173	380	168	370				
.042	.60	.33	4.7	506	7,200	.18	2.6	53.4	21	143	2,030	167	2,370	24.6	350	48.5	690	18.3	260	145	320	154	340				
.057	.81	.56	8.0	668	9,500	.22	3.1	81.3	32	202	2,870	252	3,580	38.7	550	63.2	900	19.7	280	182	400	204	450				
.034	.49	.39	5.6	506	7,200	.16	2.3	50.8	20	148	2,100	184	2,610	21.8	310	48.5	690	15.5	220	145	320	150	330				
.070	1.00	.56	8.0	759	10,800	.25	3.5	86.4	34	270	3,840	309	4,390	42.2	600	75.2	1,070	20.4	290	250	550	268	590				
.041	.59	.41	5.8	527	7,500	.15	2.2	71.2	28	174	2,470	217	3,080	25.3	360	54.8	780	13.4	190	163	360	154	340				
.053	.75	.60	8.5	640	9,100	.24	3.4	73.7	29	148	2,100	214	3,040	35.9	510	66.8	950	24.6	350	209	460	218	480				
.065	.93	.53	7.5	661	9,400	.22	3.2	83.9	33	210	2,990	257	3,660	38.0	540	66.1	940	19.7	280	209	460	232	510				
.056	.79	.61	8.7	788	11,200	.28	4.0	99.1	39	255	3,650	268	3,810	33.7	480	62.6	890	23.2	330	223	490	254	560				
.046	.66	.35	5.0	471	6,700	.16	2.3	43.2	17	164	2,340	183	2,600	24.6	350	49.9	710	19.0	270	150	330	145	320				
.066	.94	.57	8.1	718	10,200	.27	3.8	73.7	29	210	2,980	249	3,540	39.4	560	67.5	960	22.5	320	218	480	223	490				
.038	.54	.36	5.1	534	7,600	.16	2.3	58.4	23	195	2,770	216	3,070	21.1	300	49.9	710	17.6	250	150	330	150	330				

TABLE 45.—Results of Tests on 126 Species of Wood Tested in

Common and botanical name and locality where grown.	Number of rings—			Percentage of summer wood.	Percentage of moisture content determined at 100° C. (212° F.), based on—	Specific gravity oven dry (100° C. or 212° F.) based on—	Weight (green).	Shrinkage from green to oven dry condition.			Static bending.									
	Number of trees.		Per in.					Volume when green.	Volume when oven dry.	kg/m ³	lb./ft. ³	In volume (per cent of dimensions when green).	Radial (per cent of dimensions when green).	Tangential (per cent of dimensions when green).	Fiber stress at elastic limit.		Modulus of rupture.		Modulus of elasticity.	
	Per cm	Per in.													kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	th. kg/cm ²	th. lb./in. ²
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19		
CONIFERS—Continued.																				
Pine, western yellow (<i>Pinus ponderosa</i>), Colorado, Montana, Arizona, Washington, California.	25	7.9	20	22	95	0.38	0.42	737	46	10.0	3.9	6.4	218	3,100	365	5,200	71.0	1,010		
Pine, white (<i>Pinus strobus</i>), Wisconsin.	5	6.3	16	31	74	.36	.39	625	39	7.8	2.2	5.9	239	3,400	372	5,300	75.2	1,070		
Spruce, Engelmann (<i>Picea engelmanni</i>), Colorado.	10	5.5	14	14	100	.31	.35	609	38	10.4	3.4	6.6	176	2,500	295	4,200	58.3	830		
Spruce, red (<i>Picea rubens</i>), New Hampshire, Tennessee.	9	6.7	17	27	43	.38	.41	545	34	11.8	3.8	7.8	239	3,400	401	5,700	83.0	1,180		
Spruce, Sitka (<i>Picea sitchensis</i>), Washington.	5	3.5	9	24	53	.34	.37	529	33	11.2	4.5	7.4	211	3,000	387	5,500	83.0	1,180		
Spruce, white (<i>Picea canadensis</i>), New Hampshire, Wisconsin.	7	5.5	14	27	46	.36	.43	529	33	14.8	3.7	7.3	232	3,300	380	5,400	68.9	980		
Tamarack (<i>Larix laricina</i>), Wisconsin.	5	7.9	20	38	52	.49	.56	753	47	13.6	3.7	7.4	295	4,200	506	7,200	87.2	1,240		
Yew, western (<i>Taxus brevifolia</i>), Washington.	5	10.6	27	...	44	.60	.67	865	54	9.7	4.0	5.4	457	6,500	710	10,100	69.6	990		

a Green Condition in the Form of Small, Clear Pieces—Continued.

Static bending—Continued.				Impact bending.						Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.			
Work in bending—				Fiber stress at elastic limit.		Work in bending to elastic limit.		Height of drop causing complete failure; 11.03 kg (50-lb.) hammer.		Fiber stress at elastic limit.		Maximum crushing strength.								End.		Side.	
To elastic limit.		To maximum load.																					
kg/cm ²	in. lb./in. ²	kg/cm ²	in. lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	in. lb./in. ²	cm	in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg	lb.	kg	lb.
20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43
0.038	0.54	0.36	5.1	471	6,700	0.16	2.3	48.3	19	146	2,080	173	2,460	23.9	340	47.8	680	19.7	280	141	310	145	320
.044	.62	.41	5.9	457	6,500	.15	2.1	45.7	18	167	2,370	191	2,720	21.8	310	45.0	640	18.3	260	136	300	136	300
.030	.43	.34	4.9	408	5,800	.13	1.9	35.6	14	122	1,740	139	1,980	20.4	290	41.5	590	113	250	109	240	
.039	.56	.43	6.1	506	7,200	.16	2.3	45.7	18	166	2,360	193	2,740	24.6	350	54.2	770	15.5	220	191	420	159	350
.031	.44	.45	6.4	553	7,900	.18	2.5	73.7	29	160	2,280	183	2,600	23.2	330	54.8	780	16.2	230	195	430	168	370
.046	.66	.40	5.7	478	6,800	.14	2.0	50.8	20	160	2,280	167	2,380	19.0	270	47.1	670	14.1	200	136	300	127	280
.059	.84	.51	7.2	548	7,800	.19	2.7	71.2	28	211	3,010	245	3,480	33.7	480	60.4	860	18.3	260	182	400	173	380
.173	2.46	1.42	20.2	921	13,100	.44	6.2	96.6	38	239	3,400	323	4,600	73.2	1,040	114.0	1,620	31.6	450	608	1,340	522	1,150

TABLE 46.—Results of Tests on 126 Species of Wood Tested

U. S. Department of Agriculture

[Test specimens were 2 by 2 in. (50.8 by 50.8 mm) in section. Bending specimens

Common and botanical name and locality where grown.	Number of rings.		Percentage of summer wood.				Weight (air dry).		Static bending.									
	Per cm	Per in.	Percentage of moisture content determined at 100° C. (212° F.).	Specific gravity oven dry (100° C. or 212° F.) based on volume when air dry.	kg/m ³	lb./ft. ³	Fiber stress at elastic limit.	Modulus of rupture.	Modulus of elasticity.	Work in bending.								
										kg/cm ²	lb./in. ²	th. kg/cm ²	th. lb./in. ²	To elastic limit.		To maximum load.		
	kg/cm ³	in. lb./in. ³	kgcm/cm ³	in. lb./in. ³														
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	
HARDWOODS.																		
Alder, red (<i>Alnus oregona</i>), Washington.	4.3	11	...	8.6	0.42	464	29	570	8,100	759	10,800	101.1	1,440	0.17	2.37	0.60	8.5	
Ash, hiltmore (<i>Fraxinus hiltmoreana</i>), Tennessee.	6.7	17	49	5.3	.57	608	38	851	12,100	1,096	15,600	123.6	1,760	.32	4.60	.82	11.7	
Ash, black (<i>Fraxinus nigra</i>), Michigan, Wisconsin.	9.5	24	52	10.4	.50	544	34	584	8,300	978	13,900	118.0	1,680	.13	1.84	1.09	15.5	
Ash, blue (<i>Fraxinus quadrangulata</i>), Kentucky.	4.7	12	49	9.6	.58	640	40	612	8,700	1,040	14,800	100.5	1,430	.21	3.00	1.00	14.3	
Ash, green (<i>Fraxinus lanceolata</i>), Missouri, Louisiana.	7.1	18	58	10.4	.57	624	39	665	9,460	1,046	14,900	118.8	1,690	.21	3.00	.96	13.6	
Ash, Oregon (<i>Fraxinus oregona</i>), Oregon.	4.7	12	63	8.4	.57	624	39	562	8,000	1,019	14,500	100.5	1,430	.18	2.58	1.06	15.1	
Ash, pumpkin (<i>Fraxinus profunda</i>), Missouri.	8.3	21	46	9.6	.53	576	36	492	7,000	830	11,800	92.1	1,310	.15	2.11	.55	7.8	
Ash, white (forest grown) (<i>Fraxinus americana</i>), Arkansas, West Virginia.	6.3	16	50	8.7	.58	641	40	717	10,200	1,180	16,800	127.2	1,810	.23	3.29	1.06	15.1	
Ash, white (second growth) (<i>Fraxinus americana</i>), New York.	3.5	9	63	9.5	.64	705	44	1054	15,000	1,306	18,600	139.2	1,980	.34	4.80	1.19	17.0	
Aspen, large-tooth (<i>Populus grandidentata</i>), Wisconsin.	3.1	8	...	5.2	.42	448	28	534	7,600	760	10,800	90.7	1,290	.17	2.43	.51	7.3	
Aspen, large-tooth (<i>Populus grandidentata</i>), Wisconsin.	3.1	8	...	8.0	.40	432	27	499	7,100	767	10,900	115.2	1,640	.13	1.83	.47	6.7	
Basswood (<i>Tilia americana</i>), Pennsylvania, Wisconsin.	7.5	19	29	8.4	.38	416	26	513	7,300	717	10,200	111.1	1,580	.14	1.99	.57	8.1	
Beech (<i>Fagus atropunicea</i>), Indiana, Pennsylvania.	7.5	19	30	11.2	.63	705	44	632	9,000	1,054	15,000	118.0	1,680	.20	2.91	.96	13.7	
Birch, paper (<i>Betula papyrifera</i>), Wisconsin.	2.4	6	36	4.2	.58	608	38	802	11,400	1,124	16,000	127.1	1,810	.30	4.32	.93	13.2	
Birch, sweet (<i>Betula lenta</i>), Pennsylvania.	10.6	27	...	9.0	.66	721	45	935	13,300	1,376	19,600	150.4	2,140	.32	4.56	1.19	17.0	
Birch, yellow (<i>Betula lutea</i>), Pennsylvania, Wisconsin.	7.5	19	26	9.6	.63	705	44	865	12,300	1,329	18,900	154.6	2,200	.28	3.93	1.42	20.2	
Buckeye, yellow (<i>Aesculus octandra</i>), Tennessee.	5.9	15	...	6.2	.38	400	25	492	7,000	654	9,300	90.0	1,280	.16	2.20	.44	6.2	
Buckthorn, cascara (<i>Rhamnus purshiana</i>), Oregon.	6.7	17	...	4.0	.53	545	34	597	8,500	738	10,500	87.2	1,240	.23	3.28	.40	5.7	
Butternut (<i>Juglans cinerea</i>), Tennessee, Wisconsin.	3.5	9	...	7.6	.39	416	26	513	7,300	654	9,300	88.6	1,260	.16	2.32	.58	8.2	
Cherry, black (<i>Prunus serotina</i>), Pennsylvania.	4.3	11	...	9.2	.51	560	35	774	11,000	971	13,800	108.2	1,540	.32	4.48	.77	11.0	
Cherry, wild red (<i>Prunus pennsylvanica</i>), Tennessee.	2.4	6	...	6.6	.41	432	27	548	7,800	752	10,700	98.5	1,400	.18	2.54	.65	9.3	
Chestnut (<i>Castanea dentata</i>), Maryland, Tennessee.	3.9	10	48	8.6	.44	480	30	520	7,400	682	9,700	93.5	1,330	.17	2.41	.45	6.4	
Chinquapin, western (<i>Castanopsis chrysophylla</i>), Oregon.	5.9	15	...	4.8	.48	496	31	837	11,900	992	14,100	99.2	1,410	.43	6.14	.67	9.5	
Cottonwood (<i>Populus deltoides</i>), Missouri.	2.4	6	...	4.7	.43	448	28	604	8,600	801	11,400	115.4	1,640	.18	2.61	.52	7.4	
Cottonwood, black (<i>Populus trichocarpa</i>), Washington.	2.4	6	...	8.5	.36	384	24	436	6,200	675	9,600	92.1	1,310	.11	1.62	.51	7.2	
Cucumber tree (<i>Magnolia acuminata</i>), Tennessee.	5.5	14	...	6.8	.50	529	33	752	10,700	1,083	15,400	136.4	1,940	.23	3.22	.94	13.4	
Dogwood, flowering (<i>Cornus florida</i>), Tennessee.	9.5	24	...	7.5	.77	833	52	830	11,800	1,288	18,300	119.5	1,700	.33	4.63	1.33	18.9	

in an Air-Dry Condition in the Form of Small, Clear Pieces.

Bulletin No. 556, Sept, 15, 1917.

were 30 in. (762 mm) long; others were shorter, depending on kind of test.]

Impact bending.				Height of drop causing complete failure; 11.03 kg (50-lb.) hammer.		Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.			
Fiber stress at elastic limit.		Work in bending to elastic limit.				Fiber stress at elastic limit.		Maximum crushing strength.								End.		Side.	
kg/cm ²	lb./in. ²	kgcm/cm ³	in. lb./in. ³	cm	in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg	lb.	kg	lb.		
19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38
914	13,000	0.41	5.9	50.8	20	376	5,350	496	7,050	45.7	650	58.1	1,210	30.2	430	531	1,170	295	650
1,391	19,800	.73	10.4	116.9	46	502	7,140	729	10,370	142.0	2,020	138.5	1,970	56.9	810	936	2,060	604	1,330
858	12,200	.37	5.3	91.5	36	356	5,070	484	6,890	75.9	1,080	121.5	1,730	51.3	730	568	1,250	404	890
1,447	20,600	.74	10.5	106.6	42	430	6,120	544	7,740	134.3	1,910	151.0	2,150	30.9	440	858	1,890	618	1,360
1,223	17,400	.58	8.2	78.8	31	375	5,330	533	7,580	123.6	1,760	146.1	2,080	49.9	710	804	1,770	572	1,260
1,054	15,000	.44	6.2	78.8	31	331	4,710	499	7,100	140.6	2,000	146.9	2,090	54.8	780	758	1,670	590	1,300
1,069	15,200	.56	7.9	55.9	22	284	4,040	443	6,300	140.6	2,000	132.8	1,890	58.4	830	700	1,540	468	1,030
1,195	17,000	.62	8.8	91.5	36	394	5,600	576	8,190	108.3	1,540	148.2	2,110	61.9	880	886	1,950	599	1,320
1,673	23,800	.90	12.8	116.9	46	598	8,500	662	9,420	147.0	2,090	177.1	2,520	79.4	1,130	1,017	2,240	763	1,680
738	10,500	.28	4.0	61.0	24	316	4,490	450	6,400	38.7	550	62.5	890	26.7	380	386	850	191	420
1,061	15,100	.49	7.0	68.6	27	356	5,060	498	7,080	45.7	650	91.4	1,300	26.7	380	322	710	209	460
788	11,200	.32	4.6	40.7	16	311	4,430	420	5,980	40.8	580	97.2	1,240	26.0	370	268	590	204	450
1,385	19,700	.65	9.2	88.9	35	342	4,870	520	7,400	94.2	1,340	138.4	1,970	62.6	890	636	1,400	540	1,190
970	13,800	.46	6.6	61.0	24	477	6,780	666	9,470	64.0	910	114.5	1,630	677	1,490	581	1,280
1,876	26,700	.93	13.2	122.0	48	511	7,270	751	10,680	123.0	1,750	188.3	2,680	42.9	610	949	2,090	677	1,490
1,490	21,200	.70	9.9	147.3	58	543	7,720	686	9,760	99.2	1,410	132.0	1,880	62.6	890	722	1,590	599	1,320
893	12,700	.45	6.4	35.6	14	297	4,220	413	5,870	45.0	640	80.2	1,140	46.4	660	250	550	181	400
788	11,200	.38	5.4	40.7	16	387	5,510	646	9,190	140.5	2,000	140.0	1,990	813	1,790	581	1,280
907	12,900	.40	5.7	61.0	24	316	4,490	470	6,680	53.4	760	95.6	1,360	30.9	440	295	650	241	530
1,040	14,800	.41	5.9	71.2	28	515	7,330	588	8,370	71.7	1,020	135.6	1,930	39.4	560	768	1,690	468	1,030
851	12,100	.37	5.2	91.5	36	384	5,460	456	6,490	49.2	700	87.2	1,240	23.9	340	422	930	263	580
808	11,500	.38	5.4	45.7	18	311	4,420	465	6,620	65.4	930	81.6	1,160	33.0	470	354	780	263	580
879	12,500	.42	6.0	73.7	29	406	5,780	560	7,970	60.4	860	101.9	1,450	418	920	377	830
527	7,500	.17	2.4	48.3	19	356	5,060	550	7,830	51.3	730	78.8	1,120	49.2	700	336	740	218	480
766	10,900	.31	4.4	55.9	22	310	4,410	382	5,440	32.3	460	81.6	1,160	23.9	340	304	670	177	390
1,251	17,800	.53	7.6	94.0	37	423	6,020	600	8,540	60.5	860	107.5	1,530	57.3	815	527	1,160	359	790
1,356	19,300	.71	10.1	101.6	40	424	6,030	498	7,090	173.5	2,470	192.8	2,740	121.5	1,730	1,353	2,980	1,149	2,530

TABLE 46.—Results of Tests on 126 Species of Wood Tested in

Common and botanical name and locality where grown.	Number of rings.		Percentage of summer wood. Percentage of moisture content deter- mined at 100° C. (212° F.).				Weight (air dry).				Static bending.							
											Fiber stress at elastic limit.		Modulus of rupture.		Modulus of elasticity.		Work in bending.	
	Per cm	Per in.	Per cent	Per cent	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	th. kg/cm ²	th. lb./in. ²	kgcm/cm ³	in. lb./in. ³	kgcm/cm ³	in. lb./in. ³		
	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	
HARDWOODS—Continued.																		
Dogwood, western (<i>Cornus nuttallii</i>), Oregon.	8.3	21	...	5.3	0.68	721	45	710	10,100	858	12,200	123.8	1,760	0.23	3.26	0.60	8.5	
Elder, pale (<i>Sambucus glauca</i>), Oregon.	2.4	6	...	4.6	.55	577	36	534	7,600	795	11,300	78.7	1,120	.18	2.51	.75	10.7	
Elm, cork (<i>Ulmus racemosa</i>), Wisconsin.	11.0	28	50	8.5	.65	705	44	661	9,400	1,160	16,500	113.3	1,610	.23	3.32	1.32	18.7	
Elm, slippery (<i>Ulmus pubescens</i>), Indiana, Wisconsin.	6.3	16	54	8.3	.54	592	37	651	9,400	1,048	14,900	110.5	1,570	.23	3.28	1.22	17.3	
Elm, white (<i>Ulmus americana</i>), Wisconsin, Pennsylvania.	7.1	18	34	8.8	.51	560	35	647	9,200	1,027	14,600	104.9	1,490	.24	3.46	.96	13.7	
Gum, black (<i>Nyssa sylvatica</i>), Tennessee.	10.6	27	...	7.2	.52	560	35	647	9,200	767	10,900	89.3	1,270	.27	3.84	.39	5.6	
Gum, blue (<i>Eucalyptus globulus</i>), California.	5.7	.82	865	54	1012	1,440	1,448	20,600	182.6	2,600	.34	4.82	.82	11.6	
Gum, cotton (<i>Nyssa aquatica</i>), Louisiana.	3.9	10	26	6.1	.52	545	34	689	9,800	795	11,300	96.3	1,370	.29	4.19	.45	6.4	
Gum, red (<i>Liquidambar styraciflua</i>), Missouri.	6.3	16	...	11.3	.49	545	34	591	8,400	865	12,300	105.4	1,500	.24	3.39	.83	11.8	
Hackberry (<i>Celtis occidentalis</i>), Indiana, Wisconsin.	4.7	12	56	9.2	.54	592	37	485	6,900	865	12,300	87.9	1,250	.15	2.18	.87	12.4	
Haw, pear (<i>Crataegus tomentosa</i>), Wisconsin.	4.3	11	...	8.6	.70	768	48	632	9,000	1,209	1,720	96.2	1,370	.23	3.30	1.67	23.8	
Hickory, big shellbark (<i>Hicoria laciniosa</i>), Mississippi, Ohio.	7.1	18	77	8.7	.71	768	48	689	9,800	1,440	20,500	143.4	2,040	.18	2.59	1.57	22.4	
Hickory, bitternut (<i>Hicoria minima</i>), Ohio.	5.1	13	77	9.2	.68	737	45	724	10,300	1,320	18,800	132.0	1,880	.22	3.19	1.26	17.9	
Hickory, mockernut (<i>Hicoria alba</i>), Mississippi, Pennsylvania.	7.1	18	73	8.9	.75	801	50	949	13,500	1,518	21,600	167.2	2,380	.29	4.19	1.55	22.0	
Hickory, nutmeg (<i>Hicoria myristicaeformis</i>), Mississippi.	8.9	.62	673	42	647	9,200	1,355	19,300	127.9	1,820	.17	2.40	1.81	25.7	
Hickory, pecan (<i>Hicoria pecan</i>), Missouri.	4.7	12	63	6.2	.70	737	46	844	12,000	1,139	16,200	136.4	1,940	.30	4.33	.94	13.4	
Hickory, pignut (<i>Hicoria glabra</i>), Ohio, Mississippi, Pennsylvania, West Virginia.	6.3	16	74	9.6	.78	849	53	893	12,700	1,581	22,500	169.4	2,410	.27	3.87	2.12	30.2	
Hickory, shagbark (<i>Hicoria ovata</i>), Ohio, Mississippi, Pennsylvania, West Virginia.	8.7	22	70	9.4	.74	801	50	837	11,900	1,538	22,600	160.9	2,290	.25	3.55	1.85	26.3	
Hickory, water (<i>Hicoria aquatica</i>), Mississippi.	5.9	15	70	8.8	.62	673	42	830	11,800	1,409	20,200	151.8	2,160	.25	3.55	1.36	19.4	
Holly, American (<i>Ilex opaca</i>), Tennessee.	10.6	27	...	6.4	.60	641	40	562	3,000	893	12,700	86.5	1,230	.21	2.95	.75	10.6	
Hornbeam (<i>Ostrya virginiana</i>), Wisconsin.	11.4	29	...	5.6	.75	785	49	977	13,900	1,306	18,600	148.3	2,110	.38	5.34	1.01	14.4	
Laurel, California (<i>Umbellularia californica</i>), Oregon.	2.4	6	...	4.9	.58	608	38	471	6,700	632	9,000	78.0	1,110	.17	2.40	.37	5.2	
Laurel, mountain (<i>Kalmia latifolia</i>), Tennessee.	9.5	24	...	5.0	.72	753	47	766	10,900	928	13,200	99.2	1,410	.34	4.77	.64	9.1	
Locust, black (<i>Robinia pseudacacia</i>), Tennessee.	4.3	11	51	10.0	.70	768	48	971	13,800	1,454	20,700	146.9	2,090	.37	5.29	1.34	19.1	
Locust, honey (<i>Gleditsia triacanthos</i>), Missouri.	3.9	10	37	6.0	.63	673	42	752	10,700	1,174	16,700	118.7	1,690	.26	3.76	.89	12.6	
Madrona (<i>Arbutus menziessii</i>), California, Oregon.	3.9	10	...	4.5	.70	721	45	668	9,500	893	12,700	105.4	1,500	.24	3.45	.54	7.6	
Magnolia, evergreen (<i>Magnolia foetida</i>), Louisiana.	5.9	15	...	8.8	.51	560	35	548	7,800	879	12,500	104.1	1,480	.17	2.39	.86	12.3	
Maple, Oregon (<i>Acer macrophyllum</i>), Washington.	4.7	12	...	8.3	.50	545	34	534	7,600	844	12,000	111.1	1,580	.14	1.93	.54	7.6	
Maple, red (<i>Acer rubrum</i>), Pennsylvania, Wisconsin.	5.5	14	24	10.1	.54	592	37	647	9,200	998	14,200	122.2	1,740	.20	2.80	.90	12.8	

an Air-Dry Condition in the Form of Small, Clear Pieces—Continued.

Impact bending.				Height of drop causing complete failure; 11.03 kg (50-lb.) hammer.		Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to the grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.			
Fiber stress at elastic limit.		Work in bending to elastic limit.				Fiber stress at elastic limit.		Maximum crushing strength.								End.		Side.	
kg/cm ²	lb./in. ²	kgcm/cm ³	in. lb./in. ³	cm	in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg	lb.	kg	lb.		
19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38
766	10,900	0.27	3.8	66.1	26	418	5,950	795	11,310	173.5	2,470	144.9	2,060	98.5	1,400	1,139	2,510	745	1,640
851	12,100	.48	6.9	76.2	30	291	4,140	492	6,990	68.9	980	418	920	409	900
1,301	18,500	.66	9.4	134.6	53	387	5,510	592	8,420	130.6	1,860	150.5	2,140	52.0	740	786	1,730	668	1,470
1,251	17,800	.66	9.4	114.3	45	377	5,370	548	7,800	87.2	1,240	127.2	1,810	34.4	490	554	1,220	409	900
1,166	16,600	.70	9.9	111.8	44	370	5,270	482	6,850	59.7	850	122.3	1,740	42.8	610	563	1,240	395	870
1,209	17,200	.64	9.1	48.3	19	285	4,060	493	7,000	105.4	1,500	102.6	1,460	33.0	470	626	1,380	386	850
1,770	25,200	.89	12.6	106.6	42	802	11,400	977	13,900	158.1	2,250	144.0	2,050	836	1,840	749	1,650
1,034	14,700	.55	7.8	50.8	20	383	5,450	556	7,910	107.5	1,530	129.3	1,840	66.1	940	668	1,470	449	990
1,355	19,300	.73	10.4	81.3	32	348	4,960	423	6,020	55.5	790	123.0	1,750	61.2	870	458	1,010	327	720
1,110	15,800	.61	8.7	106.6	42	295	4,200	453	6,450	93.5	1,330	125.9	1,790	40.1	570	549	1,210	422	930
950	13,500	.39	5.5	50.8	20	334	4,750	592	8,420	132.1	1,880	134.9	1,920	1,030	2,270	766	1,680
1,764	25,100	1.02	14.5	213.3	84	682	9,710	186.9	2,660	170.8	2,430
1,862	26,500	.98	14.0	167.6	66	744	10,600	168.0	2,390	144.0	2,050
1,540	21,900	.75	10.6	188.0	74	746	10,610	178.5	2,540	133.5	1,900
.....	559	7,960	163.0	2,320	147.5	2,100
1,434	20,400	.73	10.4	104.2	41	434	6,170	766	10,890	235.4	3,350	178.5	2,540	92.1	1,310	1,075	2,370	971	2,140
1,841	26,200	.94	13.4	177.8	70	748	10,640	201.0	2,860	172.2	2,450
1,580	22,500	.75	10.7	165.1	65	752	10,700	173.5	2,470	164.5	2,340
.....	132.1	52	435	6,190	713	10,140	155.4	2,210	130.5	1,860
1,040	14,800	.60	8.5	68.6	27	313	4,450	550	7,820	107.1	1,520	144.9	2,060	52.0	740	804	1,770	522	1,150
1,166	16,600	.53	7.6	101.6	40	584	8,310	826	11,750	161.7	2,300	148.4	2,110	1,430	3,150	1,085	2,390
879	12,500	.44	6.2	55.9	22	367	5,220	572	8,140	135.6	1,930	164.4	2,340	66.8	950	899	1,980	663	1,460
1,223	17,400	.65	9.3	116.9	46	370	5,270	501	7,120	170.1	2,420	1,212	2,670	990	2,180
1,519	21,600	.71	10.1	150.0	59	547	7,790	765	10,880	177.2	2,520	190.5	2,710	43.6	620	713	1,570	786	1,730
1,195	17,000	.65	9.3	114.3	45	458	6,520	669	9,520	196.9	2,800	181.4	2,580	57.6	820	922	2,030	726	1,600
752	10,700	.31	4.4	40.7	16	407	5,790	765	10,800	185.5	2,640	154.0	2,190	1,190	2,620	876	1,930
1,054	15,000	.53	7.5	63.5	25	277	3,940	464	6,600	87.9	1,250	119.5	1,700	54.8	780	672	1,480	508	1,120
.....	76.2	30	448	6,370	505	7,180	78.8	1,120	141.3	2,010	36.6	520	740	1,630	431	950
1,195	17,000	.58	8.2	78.8	31	332	5,430	515	7,330	90.0	1,280	138.5	1,970	46.4	660	695	1,530	449	990

TABLE 46.—Results of Tests on 126 Species of Wood Tested in

Common and botanical name and locality where grown.	Number of rings.		Percentage of summer wood.			Weight (air dry).		Static bending.									
								Fiber stress at elastic limit.		Modulus of rupture.		Modulus of elasticity.		Work in bending.			
	Per cm	Per in.	4	5	6	7	8	Fiber stress at elastic limit.		Modulus of rupture.		Modulus of elasticity.		To elastic limit.		To maximum load.	
								kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	th. kg/cm ²	th. lb./in. ²	kgcm/cm ³	in. lb./in. ³	kgcm/cm ³	in. lb./in. ³
2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	
HARDWOODS—Continued.																	
Maple, silver (<i>Acer saccharinum</i>), Wisconsin.	2.8	7	...	8.2	0.48	513	32	542	7,700	710	10,100	85.1	1,210	0.19	2.67	0.53	7.6
Maple, sugar (<i>Acer saccharum</i>), Indiana, Pennsylvania, Wisconsin.	8.3	21	49	10.5	.62	689	43	731	10,400	1,110	15,800	127.9	1,820	.25	3.52	.96	13.6
Oak, bur (<i>Quercus macrocarpa</i>), Wisconsin.	4.7	12	59	10.2	.65	721	45	492	7,000	766	10,900	74.5	1,060	.20	2.79	.68	9.6
Oak, California black (<i>Quercus californica</i>), California, Oregon.	6.3	16	52	5.2	.60	641	40	590	8,400	738	10,500	81.6	1,160	.26	3.72	.40	5.7
Oak, canyon live (<i>Quercus chrysolepis</i>), California.	5.1	13	...	5.0	.82	865	54	837	11,900	1,033	14,700	127.2	1,810	.61	8.67	.55	7.8
Oak, chestnut (<i>Quercus prinus</i>), Tennessee.	9.1	23	50	9.5	.68	737	46	745	10,600	1,054	15,000	115.2	1,640	.27	3.85	.81	11.5
Oak, cow (<i>Quercus michauxii</i>), Louisiana.	4.7	12	58	11.3	.68	753	47	527	7,500	1,019	14,500	127.1	1,810	.12	1.75	.84	11.9
Oak, laurel (<i>Quercus laurifolia</i>), Louisiana.	4.3	11	61	9.5	.64	705	44	612	8,700	984	14,000	124.4	1,770	.17	2.47	.84	12.0
Oak, Pacific post (<i>Quercus garryana</i>), Oregon.	6.3	16	49	6.6	.76	817	51	548	7,800	823	11,700	89.3	1,270	.19	2.73	.60	8.5
Oak, post (<i>Quercus minor</i>), Arkansas, Louisiana.	10.2	26	54	11.2	.68	753	47	548	7,800	956	13,600	108.2	1,540	.16	2.34	.94	13.3
Oak, red (<i>Quercus rubra</i>), Louisiana, Arkansas, Indiana, Tennessee.	4.3	11	62	10.9	.63	705	44	604	8,600	999	14,200	131.4	1,870	.16	2.32	.94	13.3
Oak, Spanish (highland) (<i>Quercus digitata</i>), Louisiana.	7.9	20	46	10.1	.60	656	41	450	6,400	830	11,800	109.6	1,560	.11	1.55	.68	9.7
Oak, Spanish (lowland) (<i>Quercus pagodaefolia</i>), Louisiana.	2.8	7	63	10.0	.69	753	47	844	12,000	1,363	19,400	166.0	2,360	.24	3.45	1.32	18.8
Oak, water (<i>Quercus nigra</i>), Louisiana.	3.9	10	61	10.8	.64	705	44	647	9,200	1,124	16,000	144.6	2,060	.17	2.36	1.59	22.6
Oak, white (<i>Quercus alba</i>), Arkansas, Louisiana, Indiana.	6.7	17	60	11.5	.69	758	48	584	8,300	1,069	15,200	125.0	1,780	.16	2.31	1.04	14.8
Oak, willow (<i>Quercus phellos</i>), Louisiana.	5.5	14	56	9.8	.72	785	49	752	10,700	1,153	16,400	143.4	2,040	.22	3.18	1.12	16.0
Oak, yellow (<i>Quercus velutina</i>), Arkansas, Wisconsin.	5.5	14	62	11.6	.61	673	42	562	8,000	992	14,100	116.0	1,650	.15	2.18	.96	13.7
Persimmon (<i>Diospyros virginiana</i>), Missouri.	5.5	14	...	5.5	.81	849	53	1082	15,400	1,666	23,700	173.0	2,460	.40	5.70	1.19	16.9
Poplar, yellow (<i>Liriodendron tulipifera</i>), Tennessee.	5.5	14	...	6.1	.41	433	27	591	8,400	830	11,800	113.1	1,610	.18	2.52	.53	7.5
Rhododendron, great (<i>Rhododendron maximum</i>), Tennessee.	11.0	28	...	4.6	.63	656	41	591	8,400	1,012	14,400	89.3	1,270	.22	3.09	.88	12.5
Sassafras (<i>Sassafras sassafras</i>), Tennessee.	7.5	19	48	6.8	.46	497	31	542	7,700	745	10,600	85.8	1,220	.19	2.71	.67	9.5
Servicberry (<i>Amelanchier canadensis</i>), Tennessee.	7.5	19	...	8.4	.77	833	52	942	13,400	1,406	20,000	137.7	1,960	.34	4.88	1.39	19.8
Silverbell-tree (<i>Mohrodendrum carolinum</i>), Tennessee.	7.9	20	...	6.1	.47	497	31	513	7,300	689	9,800	98.4	1,400	.16	2.22	.44	6.2
Sourwood (<i>Oxydendrum arborescens</i>), Tennessee.	9.5	24	...	6.8	.57	608	38	766	10,900	970	13,800	115.2	1,640	.27	3.87	.80	11.4
Sumac, staghorn (<i>Rhus hirta</i>), Wisconsin.	3.5	9	61	8.0	.48	513	32	732	10,400	851	12,100	95.0	1,350	.32	4.50	.55	7.8
Sugarberry (<i>Celtis mississippiensis</i>), Missouri.	6.7	17	38	5.0	.54	560	35	668	9,500	914	13,000	99.2	1,410	.30	4.23	.75	10.7
Sycamore (<i>Platanus occidentalis</i>), Indiana, Tennessee.	6.3	16	77	9.2	.50	545	34	534	7,600	795	11,300	106.1	1,510	.15	2.20	.65	9.2
Umbrella, Fraser (<i>magnolia fraseri</i>), Tennessee.	5.9	15	...	6.4	.47	497	31	654	9,300	893	12,700	106.9	1,520	.23	3.27	.77	10.9
Walnut, black (<i>Juglans nigra</i>), Kentucky.	4.7	12	...	4.8	.57	592	37	1020	14,500	1,259	17,900	128.0	1,820	.45	6.43	.65	9.2

an Air-Dry Condition in the Form of Small, Clear Pieces—Continued.

Impact bending.				Height of drop causing complete failure; 11.03 kg (50-lb.) hammer.		Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.			
Fiber stress at elastic limit.		Work in bending to elastic limit.				Fiber stress at elastic limit.		Maximum crushing strength.								End.		Side.	
kg/cm ²	lb./in. ²	kgcm/cm ³	in. lb./in. ³	cm	in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg	lb.	kg	lb.		
19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38
1,054	15,000	0.66	9.4	61.0	24	394	5,600	464	6,600	83.0	1,180	120.2	1,710	34.4	490	626	1,380	341	750
1,343	19,100	.65	9.3	83.9	33	426	6,060	602	8,570	113.9	1,620	172.2	2,450	54.2	770	908	2,000	649	1,430
1,075	15,300	.60	8.6	68.6	27	260	3,700	467	6,640	117.3	1,670	135.0	1,920	45.7	650	663	1,460	645	1,420
647	9,200	.29	4.2	30.5	12	312	4,440	592	8,420	130.8	1,860	120.2	1,710	58.4	830	617	1,360	581	1,280
1,005	14,300	.47	6.7	81.3	32	570	3,100	939	13,360	203.0	2,890	192.5	2,740	105.5	1,500	1,525	3,360	1,430	3,150
1,490	21,200	.63	9.0	106.7	42	371	5,280	551	7,940	83.0	1,180	112.5	1,600	106.1	1,510	608	1,340	545	1,200
1,350	19,200	.57	8.1	104.2	41	311	4,420	533	7,580	99.9	1,420	154.0	2,190	49.2	700	595	1,310	572	1,260
1,069	15,200	.41	5.9	99.1	39	371	5,280	578	8,230	104.6	1,490	142.6	2,030	55.5	790	581	1,280	572	1,260
893	12,700	.40	5.7	58.4	23	353	5,020	602	8,570	180.0	2,560	155.2	2,210	56.9	810	949	2,090	808	1,780
1,251	17,800	.60	8.6	116.9	46	278	3,960	484	6,890	133.5	1,900	133.5	1,900	54.8	780	618	1,360	632	1,390
1,300	18,500	.64	9.1	99.1	39	324	4,610	518	7,370	85.1	1,210	123.6	1,760	54.8	780	681	1,500	595	1,310
1,160	16,500	.58	8.3	66.1	26	213	3,030	478	6,800	82.9	1,180	107.5	1,530	36.5	520	477	1,050	499	1,100
1,771	25,200	.93	13.2	124.4	49	493	7,010	683	9,720	121.5	1,730	152.5	2,170	60.4	860	645	1,640	699	1,540
1,364	19,400	.60	8.6	111.8	44	276	3,930	506	7,200	92.9	1,320	141.3	2,010	66.1	940	658	1,450	554	1,220
1,210	17,200	.53	7.6	96.6	38	305	4,350	535	7,610	94.2	1,340	147.0	2,090	56.2	800	699	1,540	622	1,370
1,230	17,500	.65	9.3	111.8	44	345	4,910	578	8,230	115.2	1,640	126.5	1,800	100.5	1,430	695	1,530	736	1,620
1,012	14,400	.45	6.4	104.2	41	336	4,780	468	6,660	81.6	1,160	138.5	1,970	57.6	820	636	1,400	549	1,210
1,574	22,400	.82	11.7	88.9	35	647	9,210	987	14,050	275.0	3,910	187.5	2,670	106.9	1,520	1,694	3,730	1,444	3,180
1,300	18,600	.63	8.9	55.9	22	314	4,470	526	7,480	52.0	740	82.3	1,170	40.1	570	268	590	204	450
647	9,200	.23	3.3	40.7	16	387	5,510	658	9,360	135.0	1,920	62.6	890
823	11,700	.43	6.1	78.8	31	244	3,470	426	6,060	103.4	1,470	97.0	1,380	43.6	620	304	670	313	690
1,722	24,500	.86	12.3	147.4	58	608	8,640	775	11,020	161.6	2,300	120.9	1,720	1,130	2,490	921	2,030
1,124	16,000	.56	8.0	58.4	23	304	4,330	484	6,890	60.4	860	92.1	1,310	33.7	480	482	1,060	295	650
1,455	20,700	.81	11.5	96.6	38	394	5,600	576	8,190	96.3	1,370	118.0	1,680	31.6	450	763	1,680	482	1,050
.....	398	5,660	545	7,750	96.4	1,370	426	960	327	720
992	14,100	.52	7.4	94.0	37	419	5,960	594	8,450	141.3	2,010	101.9	1,450	49.2	700	745	1,640	504	1,110
760	10,800	.28	4.0	71.2	28	301	4,260	441	6,280	71.0	1,010	102.5	1,460	52.7	750	441	970	368	810
1,152	16,400	.52	7.4	71.2	28	367	5,220	527	7,500	59.1	840	94.2	1,340	55.5	790	445	980	313	690
1,363	19,400	.79	11.3	83.9	33	554	7,880	750	10,660	137.8	1,960	104.0	1,480	54.8	780	504	1,110	490	1,080

TABLE 46.—Results of Tests on 126 Species of Wood Tested in

Common and botanical name and locality where grown.	Number of rings.		Percentage of moisture content determined at 100° C. (212° F.).				Weight (air dry).		Static bending.									
	Per cm	Per in.	3	4	5	6	7	8	Fiber stress at elastic limit.	Modulus of rupture.	Modulus of elasticity.	Work in bending.						
												To elastic limit.		To maximum load.				
	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	
HARDWOODS—Continued.																		
Willow, black (<i>Salix nigra</i>), Wisconsin, Missouri.	2.0	5	...	6.4	0.38	417	26	394	5,600	534	7,600	58.4	830	0.17	2.45	0.48	6.8	
Willow, western black (<i>Salix lasiandra</i>), Oregon.	2.0	5	...	4.0	.47	497	31	562	8,000	781	11,100	108.2	1,540	.17	2.39	.59	8.4	
Witch-hazel (<i>Hamamelis virginiana</i>), Tennessee.	5.5	14	...	5.1	.65	689	43	844	12,000	1,428	20,300	116.6	1,660	.34	4.85	1.53	21.8	
CONIFERS.																		
Cedar incense (<i>Libocedrus decurrens</i>), California, Oregon.	6.7	17	30	5.1	.36	386	24	520	7,400	661	9,400	91.4	1,300	.16	2.31	.34	4.9	
Cedar, Port Orford (<i>Chamaecyparis lawsoniana</i>), Oregon.	9.5	24	25	9.0	.45	497	31	626	8,900	1,020	14,500	143.4	2,040	.16	2.25	
Cedar, western red (<i>Thuja plicata</i>), Washington, Montana.	7.9	20	36	7.4	.34	352	22	429	6,100	619	8,800	87.9	1,250	.12	1.68	.45	6.4	
Cedar, white (<i>Thuja occidentalis</i>), Wisconsin.	9.1	23	36	11.2	.31	352	22	358	5,100	471	6,700	56.9	810	.13	1.84	.33	4.7	
Cypress, bald (<i>Taxodium distichum</i>), Louisiana, Missouri.	6.3	16	31	9.0	.44	481	30	612	8,700	794	11,300	108.3	1,540	.21	3.03	.51	7.3	
Cypress, yellow (<i>Chamaecyparis nootkatensis</i>), Oregon.	12.2	31	...	5.5	.43	448	28	632	9,000	900	12,800	100.5	1,430	.24	3.37	.60	8.5	
Douglas fir (<i>Pseudotsuga taxifolia</i>), Montana, Wyoming.	8.7	22	27	9.4	.44	481	30	485	6,900	724	10,300	102.5	1,460	.13	1.83	.46	6.5	
Douglas fir (<i>Pseudotsuga taxifolia</i>), Washington, Oregon.	5.1	13	35	6.2	.51	545	34	745	10,600	984	14,000	155.2	2,210	.21	2.94	.59	8.4	
Fir, Alpine (<i>Abies lasiocarpa</i>), Colorado.	5.9	15	14	15.9	.32	368	23	337	4,800	422	6,000	62.6	890	.12	1.73	.24	3.4	
Fir, anabilis (<i>Abies amabilis</i>), Washington.	4.7	12	36	9.3	.39	433	27	492	7,000	745	10,600	112.4	1,600	.12	1.73	.72	10.3	
Fir, balsam (<i>Abies balsamea</i>), Wisconsin.	4.7	12	26	4.8	.38	400	25	513	7,300	696	9,900	101.3	1,440	.15	2.11	.38	5.4	
Fir, grand (<i>Abies grandis</i>), Montana, Oregon.	7.1	18	30	6.8	.41	433	27	499	7,100	773	11,000	125.8	1,790	.12	1.66	.58	8.3	
Fir, noble (<i>Abies nobilis</i>), Oregon.	9.1	23	17	8.4	.39	417	26	542	7,700	844	12,000	123.0	1,750	.13	1.92	.66	9.4	
Fir, white (<i>Abies concolor</i>), California.	3.9	10	30	9.6	.38	417	26	492	7,000	689	9,800	104.7	1,490	.13	1.86	.39	5.5	
Hemlock, black (<i>Tsuga mertensiana</i>), Montana.	9.1	23	45	8.0	.46	497	31	520	7,400	802	11,400	83.0	1,180	.19	2.74	.64	9.1	
Hemlock, eastern (<i>Tsuga canadensis</i>), Tennessee, Wisconsin.	7.9	20	34	8.6	.42	448	28	506	7,200	682	9,700	91.4	1,300	.16	2.32	.41	5.8	
Hemlock, western (<i>Tsuga heterophylla</i>), Washington.	3.9	10	27	5.4	.42	448	28	562	8,000	759	10,800	106.8	1,520	.17	2.48	.43	6.1	
Larch, western (<i>Larix occidentalis</i>), Montana, Washington.	14.2	36	37	8.3	.54	577	36	710	10,100	949	13,500	128.5	1,830	.22	3.06	.58	8.2	
Pine, Cuban (<i>Pinus heterophylla</i>), Florida.	6.7	17	44	8.8	.66	721	45	872	12,400	1,285	18,300	156.0	2,220	.27	3.88	.92	13.1	
Pine, jack (<i>Pinus divaricata</i>), Wisconsin.	2.8	7	30	6.1	.44	465	29	457	6,500	682	9,700	98.5	1,400	.13	1.81	.36	5.1	
Pine, Jeffrey (<i>Pinus jeffreyi</i>), California.	7.1	18	23	8.7	.41	448	28	619	8,800	766	10,900	92.1	1,310	.24	3.42	.50	7.1	
Pine, loblolly (<i>Pinus taeda</i>), Florida.	3.5	9	42	6.5	.57	608	38	823	11,700	1,096	15,600	149.6	2,130	.26	3.70	.63	9.0	
Pine, lodgepole (<i>Pinus contorta</i>), Montana, Wyoming, Colorado.	9.5	24	22	7.1	.43	448	28	632	9,000	809	11,500	102.6	1,460	.23	3.24	.53	7.6	
Pine, longleaf (<i>Pinus palustris</i>), Florida, Louisiana, Mississippi.	7.1	18	38	9.2	.66	673	42	830	11,800	1,175	16,700	154.6	2,200	.25	3.58	.79	11.3	
Pine, Norway (<i>Pinus resinosa</i>), Wisconsin.	8.7	22	41	12.5	.48	545	34	647	9,200	865	12,300	125.8	1,790	.19	2.68	.70	9.9	

an Air-Dry Condition in the Form of Small, Clear Pieces—Continued.

Impact bending.				Height of drop causing complete failure; 11.03 kg (50-lb.) hammer.		Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.			
Fiber stress at elastic limit.		Work in bending to elastic limit.				Fiber stress at elastic limit.		Maximum crushing strength.								End.	Side.		
kg/cm ²	lb./in. ²	kg/cm ³	in. lb./in. ³	cm	in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg	lb.	kg	lb.	kg	lb.
19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38
647	9,200	0.34	4.8	41.7	16	202	2,880	353	5,030	49.9	710	94.2	1,340	33.0	470	309	680	227	500
977	13,900	.50	7.1	76.2	30	351	5,000	500	7,120	64.7	920	99.1	1,410	46.4	660	558	1,230	332	730
.....						453	6,440	592	8,430	152.5	2,170				1,163	2,560	881	1,940
780	11,100	.37	5.2	43.2	17	450	6,400	506	7,200	59.0	840	63.3	900	19.0	270	472	1,040	236	520
1,236	17,600	.51	7.2	99.1	39	541	7,700	545	7,750	71.7	1,020	105.4	1,500	44.3	630	431	950	318	700
675	9,600	.24	3.4	40.7	16	379	5,390	444	6,320	49.2	700	64.7	920	12.7	180	341	750	173	380
506	7,200	.20	2.8	30.5	12	200	2,840	291	4,140	27.4	390	63.3	900	16.9	240	213	470	154	340
788	11,200	.33	4.7	66.1	26	419	5,970	540	7,690	64.0	910	76.0	1,080	19.7	1,280	363	800	250	550
1,026	14,600	.56	7.9	73.7	29	547	7,780	568	8,060	67.5	960	78.8	1,120	30.2	430	368	810	266	580
935	13,300	.39	5.6	71.2	28	374	5,320	498	7,090	66.7	950	76.0	1,080	22.5	320	341	750	300	660
1,005	14,300	.38	5.4	83.9	33	651	9,260	751	10,680	85.8	1,220	89.3	1,270	23.2	330	418	920	368	810
471	6,700	.15	2.1	35.5	14	230	3,270	239	3,400	35.1	500	71.0	1,010	191	420	154	340
837	11,900	.37	5.3	61.0	24	356	5,070	460	6,540	40.8	580	83.0	1,180	20.4	290	327	720	213	470
597	8,500	.20	2.9	58.4	23	467	6,640	37.3	530	55.5	790	12.7	180	336	740	227	500
984	14,000	.41	5.8	81.3	32	420	5,970	496	7,060	59.7	850	70.3	1,000	13.4	190	372	820	254	560
879	12,500	.32	4.6	68.6	27	432	6,140	509	7,240	59.7	850	76.6	1,090	9.1	130	391	860	213	470
591	8,400	.23	3.2	35.5	14	294	4,180	432	6,150	50.4	720	74.5	1,060	18.3	260	354	780	209	460
1,096	15,600	.56	7.9	91.5	36	206	4,360	528	7,510	99.8	1,420	88.6	1,260	23.9	340	586	1,290	313	690
879	12,500	.42	6.0	61.0	24	368	5,240	496	7,060	74.5	1,060	81.6	1,160	13.4	190	391	860	222	490
914	13,000	.42	6.0	66.1	26	547	7,780	556	7,910	58.3	830	82.3	1,170	11.9	170	463	1,020	282	620
1,195	17,000	.60	8.6	86.4	34	592	8,420	677	9,640	90.0	1,280	107.5	1,530	23.9	340	627	1,380	395	870
1,265	18,000	.51	7.2	106.6	42	644	9,160	836	11,890	113.9	1,620	135.0	1,920	45.7	650	545	1,200	527	1,160
921	13,100	.39	5.6	94.0	37	546	7,770	80.9	1,150	93.5	1,330	30.9	440	395	870	336	740
999	14,200	.44	6.2	73.7	29	365	5,200	490	6,980	70.3	1,000	101.9	1,450	28.8	410	336	740	250	550
1,040	14,800	.41	5.9	66.1	26	561	7,980	794	11,300	112.4	1,600	120.9	1,720	26.0	370	468	1,030	381	840
759	10,800	.33	4.7	50.8	20	441	6,270	513	7,300	78.7	1,120	68.9	980	26.7	380	291	640	227	500
1,052	16,400	.46	6.6	81.3	32	650	9,250	765	10,880	117.4	1,670	115.3	1,640	29.5	420	518	1,140	463	1,020
1,062	15,100	.44	6.3	63.5	25	398	5,660	498	7,080	58.3	830	88.6	1,260	33.0	470	318	700	272	600

TABLE 46.—Results of Tests on 126 Species of Wood Tested in

Common and botanical name and locality where grown.	Num-ber of rings.		Percentage of moisture content deter-mined at 100° C. (212° F.). Specific gravity oven dry (100° C. or 212° F.) based on volume when air dry.					Weight (air dry).		Static bending.							
										Fiber stress at elastic limit.		Modulus of rupture.		Modulus of elasticity.		Work in bending.	
	Per cm	Per in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	th. kg/cm ²	th. lb./in. ²	kgcm/cm ³	in. lb./in. ³	kgcm/cm ³	in. lb./in. ³	To elastic limit.	To mari-mum load.			
	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
CONFERS—Continued.																	
Pine, pitch (<i>Pinus rigida</i>), Tennessee.	4.7	12	30	7.6	0.52	560	35	548	7,800	872	12,400	105.4	1,500	0.18	2.56	0.61	8.7
Pine, pond (<i>Pinus serotina</i>), Florida.	5.1	13	35	6.2	.56	592	37	794	11,300	1,027	14,600	144.0	2,050	.24	3.43	.65	9.2
Pine, shortleaf (<i>Pinus echinata</i>), Arkansas, Louisiana.	3.9	10	40	11.0	.54	608	38	647	9,200	977	13,900	138.4	1,970	.17	2.46	.71	10.1
Pine, sugar (<i>Pinus lambertiana</i>), California.	4.7	12	34	11.4	.37	417	26	450	6,400	604	8,600	85.1	1,210	.13	1.79	.35	5.0
Pine, table mountain (<i>Pinus pungens</i>), Tennessee.	5.9	15	29	8.0	.53	577	36	661	9,400	942	13,400	116.0	1,650	.22	3.06	.63	8.9
Pine, western white (<i>Pinus monticola</i>), Montana.	11.0	28	33	7.9	.43	464	29	555	7,900	808	11,500	118.8	1,690	.15	2.17	.70	10.0
Pine, western yellow (<i>Pinus ponderosa</i>), Colorado, Montana, Arizona, Washington, California.	7.9	20	22	10.8	.41	448	28	485	6,900	689	9,800	94.2	1,340	.15	2.13	.45	6.4
Pine, white (<i>Pinus strobus</i>), Wisconsin.	6.3	16	31	9.9	.39	433	27	492	7,000	675	9,600	99.8	1,420	.14	2.04	.45	6.4
Spruce, Engelmann (<i>Picea engelmanni</i>), Colorado.	5.5	14	14	14.8	.32	384	24	316	4,500	478	6,800	72.4	1,030	.077	1.09	.38	5.4
Spruce, red (<i>Picea rubens</i>), New Hampshire, Tennessee.	6.7	17	32	10.8	.41	448	28	520	7,400	760	10,800	109.0	1,550	.14	1.97	.61	8.7
Spruce, Sitka (<i>Picea sitchensis</i>), Washington.	3.5	9	24	8.9	.38	417	26	506	7,200	788	11,200	113.3	1,610	.13	1.78	.73	10.4
Spruce, white (<i>Picea canadensis</i>), New Hampshire, Wisconsin.	5.5	14	27	9.6	.40	448	28	415	5,900	647	9,200	97.8	1,390	.10	1.40	.58	8.2
Tamarack (<i>Larix laricina</i>), Wisconsin.	7.9	20	38	11.0	.53	592	37	590	8,400	844	12,000	118.0	1,680	.17	2.35	.50	7.1
Yew, western (<i>Taxus brevifolia</i>), Washington.	10.6	27	...	9.2	.63	689	43	710	10,100	1,180	16,800	102.8	1,460	.28	3.94	1.29	18.4

an Air-Dry Condition in the Form of Small, Clear Pieces—Continued.

Impact bending.				Height of drop causing complete failure; 11.03 kg (50-lb.) hammer.		Compression parallel to grain.				Compression perpendicular to grain; fiber stress at elastic limit.		Shearing strength parallel to the grain.		Tensile strength perpendicular to grain.		Hardness, load required to embed a 1.13 cm (0.444 in.) ball to one-half its diameter.			
Fiber stress at elastic limit.		Work in bending to elastic limit.				Fiber stress at elastic limit.		Maximum crushing strength.								End.		Side.	
kg/cm ²	lb./in. ²	kgcm/cm ³	in. lb./in. ³	cm	in.	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg/cm ²	lb./in. ²	kg	lb.	kg	lb.		
19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38
1,210	17,200	0.75	10.7	71.2	28	316	4,490	534	7,600	82.3	1,170	117.4	1,670	40.8	580	372	820	313	690
1,104	15,700	.44	6.3	66.1	26	578	8,220	752	10,690	111.0	1,580	121.0	1,720	28.8	410	463	1,020	404	890
1,166	16,600	.46	6.5	91.5	36	498	7,080	608	8,660	92.1	1,310	97.8	1,390	28.8	410	427	940	399	880
710	10,100	.30	4.3	43.2	17	333	4,740	365	5,190	45.0	640	75.9	1,080	24.6	350	295	650	209	460
1,116	15,900	.53	7.6	73.7	29	320	4,560	597	8,500	107.6	1,530	90.7	1,290	377	830	331	730
1,046	14,900	.41	5.8	73.7	29	408	5,810	551	7,840	56.9	810	41.4	590	213	470	191	420
703	10,000	.29	4.1	40.7	16	316	4,490	421	5,990	53.4	760	81.6	1,160	28.8	410	259	570	209	460
654	9,300	.23	3.3	45.7	18	356	5,070	447	6,360	53.4	760	75.2	1,070	23.9	340	277	610	213	470
584	8,300	.22	3.2	38.1	15	209	2,980	268	3,810	36.5	520	64.0	910	177	390	132	290
851	12,100	.34	4.9	71.2	28	385	5,470	448	6,380	43.6	620	81.6	1,160	26.7	380	304	670	232	510
977	13,900	.37	5.2	63.5	25	406	5,770	71.0	1,010	85.1	1,210	354	780	241	530
682	9,700	.25	3.5	50.8	20	325	4,620	423	6,020	41.5	590	68.2	970	24.6	350	345	760	254	560
914	13,000	.40	5.7	58.4	23	362	5,150	534	7,590	76.0	1,080	96.3	1,370	28.8	410	327	720	291	640
837	11,900	.37	5.3	76.2	30	332	4,720	648	9,220	188.3	2,680	174.2	2,480	28.8	410	1,058	2,330	818	1,800

TABLE 47.—Approximate Figures for Change of Properties of Woods With Change of Moisture Content; Variation of Property With Specific Gravity.

[For use with Tables 45 and 46.]

Property.	Average increase (or decrease) in value effected by lowering (or raising) the moisture content 1 per cent when at about 12 per cent.	Approximate power of specific gravity according to which property varies.
	Per cent.	
Shrinkage.....		1
Static bending:		
Fiber stress at elastic limit.....	6	1
Modulus of rupture.....	4	1
Modulus of elasticity.....	2	1
Work to elastic limit.....	8	2
Work to maximum load.....	-1	2
Impact bending:		
Fiber stress at elastic limit.....	4	1
Work to elastic limit.....	5	2
Height of drop.....	-3	2
Compression parallel to grain:		
Fiber stress at elastic limit.....	5	1
Crushing strength.....	4	1
Compression perpendicular to grain:		
Fiber stress at elastic limit.....	6	2
Hardness, end.....	3	2
Hardness, side.....	1	2
Shearing strength parallel to grain.....	4	1
Tension perpendicular to grain.....	1	2

¹ Minus indicates decrease effected by lowering moisture contents.

LIST OF REFERENCES.

1. Aluminum Co. of Amer., tests; 1921.
2. E. Weintraub, Amer. Electrochemical Soc., transactions, **16**, pp. 165-184; 1909.
3. Amer. Electrochemical Soc., Jour., **36**, p. 323; 1919.
4. A. Hirsch, Amer. Electrochemical Soc., Jour., **37**, p. 359; 1920.
5. E. Haynes, Amer. Inst. of Metals, transactions, **9**, p. 333; 1915.
6. W. M. Corse, Amer. Inst. of Metals, transactions, **9**, p. 194; 1915.
7. G. H. Clamer, Amer. Inst. of Metals, transactions, **9**, p. 241; 1915.
8. W. B. Price, Amer. Inst. of Metals, transactions, **10**, p. 133; 1916.
9. Amer. Inst. of Metals, transactions, **9**, p. 211; 1915.
10. Z. Jeffries, Amer. Inst. of Mining Eng., Bulletin No. 138, June, 1918.
11. G. Sargent, Amer. Soc. for Testing Materials, proceedings, pp. 5-28; 1920.
12. P. D. Merica, R. G. Waltenberg, and A. S. McCabe, Amer. Soc. for Testing Materials, proceedings, p. 922; 1921.
13. Amer. Soc. for Testing Materials, specifications B 26-21; 1921.
14. Amer. Soc. for Testing Materials, specifications B 31-21 (appendix); 1921.
15. Amer. Soc. for Testing Materials, specifications B 9-16; 1916.
16. Amer. Soc. for Testing Materials, specifications B 7-14; 1914.
17. Amer. Soc. for Testing Materials, specifications A 47-19; 1919.
18. Amer. Soc. for Testing Materials, specifications A 73-18; 1918.
19. Amer. Soc. for Testing Materials, specifications A 72-21; 1921.
20. Amer. Soc. for Testing Materials, specifications A 84-21; 1921.
21. Amer. Soc. for Testing Materials, specifications A 42-18; 1918.

22. Amer. Soc. for Testing Materials, specifications A 3-14; 1914.
23. Amer. Soc. for Testing Materials, specifications A 9-21; 1921.
24. Amer. Soc. for Testing Materials, specifications A 12-21; 1921.
25. Amer. Soc. for Testing Materials, specifications A 31-21; 1921.
26. Amer. Soc. for Testing Materials, specifications A 15-14; 1914.
27. Amer. Soc. for Testing Materials, specifications A 19-21; 1921.
28. Amer. Soc. for Testing Materials, specifications A 4-14; 1914.
29. Amer. Soc. for Testing Materials, specifications A 50-21; 1921.
30. Amer. Soc. for Testing Materials, specifications A 27-21; 1921.
31. Amer. Soc. for Testing Materials, specifications A 22-21; 1921.
32. Amer. Soc. for Testing Materials, specifications A 20-21; 1921.
33. Amer. Soc. for Testing Materials, specifications A 5-14; 1914.
34. Amer. Soc. for Testing Materials, specifications A 49-21; 1921.
35. Amer. Soc. for Testing Materials, specifications A 26-16; 1916.
36. Amer. Soc. for Testing Materials, specifications A 6-14; 1914.
37. Amer. Soc. for Testing Materials, specifications A 8-21; 1921.
38. K. R. Koch, *Annalen der Physik*, **359**, p. 1; 1917.
39. R. Anderson, *Brass World*, November, 1921.
40. R. Anderson, *Brass World*, December, 1921.
41. R. Anderson, *Brass World*, p. 133; May, 1921.
42. Hatfield, "Cast Iron;" 1918.
43. P. D. Merica, *Chem. and Metallurgical Eng.*, September 15, 1918.
44. C. H. Jones, *Chem. and Metallurgical Eng.*, **22**, January 7, 1920.
45. W. M. Corse, *Chem. and Metallurgical Eng.*, **20**, p. 162; 1919.
46. O. L. Kowalke, *Chem. and Metallurgical Eng.*, **22**, p. 37; 1920.
47. W. B. Price, *Chem. and Metallurgical Eng.*, July 27, 1921.
48. J. S. Negru, *Chem. and Metallurgical Eng.*, **21**, pp. 353-359; 1919.
49. F. Grotts, *Chem. and Metallurgical Eng.*, **19**, p. 125; 1918.
50. F. Grotts, *Chem. and Metallurgical Eng.*, **19**, pp. 191-193; 1918.
51. A. H. Hunter, *Chem. and Metallurgical Eng.*, July 6, 1921.
52. F. Grotts, *Chem. and Metallurgical Eng.*, **19**, pp. 121, 191, 241; 1918.
53. *Chem. and Metallurgical Eng.*, **25**, p. 797; 1921.
54. *Chem. and Metallurgical Eng.*, **19**, p. 684; 1918.
55. L. J. Gurevitch and Hromatko, *Chem. and Metallurgical Eng.*, July 13, 1921.
56. F. C. Frary and S. N. Temple, *Chem. and Metallurgical Eng.*, **19**, p. 523; 1918.
57. *Chem. and Metallurgical Eng.*, **25**, p. 799; 1921.
58. J. Rooney, *Chem. and Metallurgical Eng.*, **22**, p. 60; 1920.
59. W. Grosvenor, *Chem. and Metallurgical Eng.*, **14**, p. 262; 1916.
60. J. F. Thompson, *Chem. and Metallurgical Eng.*, **21**, p. 550; 1919.
61. P. D. Merica, *Chem. and Metallurgical Eng.*, **24**, pp. 73, 197; 1921.
62. *Chem. and Metallurgical Eng.*, **15**, p. 159; 1916.
63. Frye, *Civ. Eng. Pocketbook*; 1918.
64. Dow Chemical Co., tests; 1921.
65. *Engineer*, **127**, p. 402; 1919.
66. *Engineer*, p. 504, November 11, 1921.
67. *Engineering*, **113**, p. 807; 1922.
68. R. Rolfe, *Engineering*, October 21, 1921.
69. S. Beckinsale, *Engineering*, November 4, 1921.
70. D. H. Ingall, *Engineering*, **112**, p. 489; 1921.
71. Kempe, *Engineering Yearbook*, p. 240; 1921.
72. *Foundry*, **43**, p. 160; 1915.
73. A. B. Wilson, *Foundry*, **48**, p. 915; 1920.
74. E. Molinari, "General and Industrial Chemistry"; 1920.
75. Winkelman, *Handbuch der Physik*, **1**, p. 557; 1908.

76. "Hütte," **1**, p. 495; 1920.
77. "Hütte," **1**, p. 496; 1920.
78. Bregowsky and Spring, Internat. Assoc. for Testing Materials, proceedings, VII-1: 1912.
79. International Nickel Co., tests; 1919.
80. J. O. Arnold and A. A. Read, Inst. of Mech. Eng., proceedings, p. 247; 1915.
81. R. A. Hadfield, Inst. of Mech. Eng., proceedings, p. 701; 1915.
82. J. O. Arnold and A. A. Read, Inst. of Mech. Eng., proceedings, p. 629; 1915.
83. A. A. Read and R. H. Greaves, Inst. of Metals Jour., **15**, p. 264; 1916.
84. Inst. of Metals Jour., **14**, p. 55; 1915.
85. F. C. Thompson, Inst. of Metals, Jour., **15**, p. 230; 1916.
86. F. C. Thompson, Inst. of Metals, Jour., **17**, p. 119; 1917.
87. F. C. Thompson, Inst. of Metals, Jour., **27**, p. 227; 1922.
88. H. R. Williams, Inst. of Metals, Jour., **23**, p. 580; 1920.
89. J. Arnott, Inst. of Metals, Jour., **23**, p. 545; 1920.
90. L. P. Webbert, Iron Age, **94**, p. 539; 1914.
91. H. Kalmus and C. Harper, Jour. of Industrial and Eng. Chem., p. 9; 1915.
92. Jour. of Industrial and Eng. Chem., **9**, p. 1144; 1917.
93. T. D. Yensen, Ill. Univ. Eng. Expt. Sta., Bulletin No. 72; 1914.
94. T. D. Yensen and W. A. Gatward, Ill. Univ. Eng. Expt. Sta., Bulletin No. 95; 1917.
95. T. D. Yensen, Ill. Univ. Eng. Expt. Sta., Bulletin No. 83; 1915.
96. H. F. Moore, Ill. Univ. Eng. Expt. Sta., Bulletin No. 52; 1911.
97. Landolt-Börnstein Physikalisch-Chemische Tabellen; 1912.
98. Machinery's Encyclopedia; 1917.
99. Major Engineering Co., tests.
100. J. B. Johnson, "Materials of Construction," pp. 688-718; 1918.
101. J. B. Johnson, "Materials of Construction," p. 616; 1918.
102. J. B. Johnson, "Materials of Construction," p. 678; 1918.
103. H. F. Moore, "Materials of Engineering," p. 182; 1917.
104. McCook Field, Reports, April 2, 1918.
105. McCook Field, Reports, December 2, 1920.
106. McCook Field, Reports, No. 641; 1921.
107. McCook Field, Reports, June 8, 1921.
108. McCook Field, Reports, November 23, 1920.
109. Marks, Mechanical Engineer's Handbook; 1916.
110. W. Rosenhain, Metal Industry, London, **17**, p. 410; 1920.
111. Metal Industry, London, **11**, p. 169; 1917.
112. Metal Industry, London, **4**, p. 368; 1912.
113. B. Welbourn, Metal Industry, London, **12**, p. 70; 1918.
114. Metal Industry, London, **11**, p. 168; 1917.
115. P. D. Merica, Metal Industry, London, **18**, p. 445; 1921.
116. Metal Industry, London, **11**, September 7, 1917.
- (116a) Metal Industry, London, January 6, 1922.
117. O. Smalley, Metal Industry, London, July 28, 1922.
118. O. Smalley, Metal Industry, London, August 11, 1922.
119. O. Smalley, Metal Industry, London, August 4, 1922.
120. F. A. Livermore, Metal Industry, London, December 2, 1921.
121. Metal Industry, London, July 9, 1920.
122. Metal Industry, London, August 12, 1921.
123. E. A. Smith and H. Turner, Metal Industry, London, October 10, 1919.
124. J. L. Houghton, Metal Industry, London, **18**, p. 4; 1921.
125. W. T. Brannt, "Metallic Alloys," p. 159; 1908.
126. W. T. Brannt, "Metallic Alloys," pp. 98, 161; 1908.
127. Metall und Erz, **15**, p. 461; 1918.

128. A. Martens, Mitteilungen aus dem Mechanischer Technische Laboratory der Technische Hochschule im München, Heft **20**, 1887.
129. O. Meyer, Oesterreichische Zeitschrift für Berg und Hüttenwesen, October 7 and 14, 1905.
130. P. W. Bridgman, Phys. Rev., **9**, p. 138; 1917.
131. T. Langmuir, Phys. Rev., **6**, p. 138; 1915.
132. A. Worthing, Phys. Rev., **10**, p. 638; 1917.
133. W. Rosenhain, Report on aluminum alloy rivets to the British Aeronautical Research Com., May, 1919.
134. W. Rosenhain, Hanson, and others, Eleventh Report to the British Alloys Research Com., 1921.
135. M. L. Guillet, Revue de Metallurgie, December, 1919.
136. A. Portevin, Revue de Metallurgie, **18**, p. 761; 1921.
137. A. Siemens, Royal Inst., proceedings, **19**, pp. 590-597; 1909.
138. Smithsonian Physical Tables, 7th edition, 1920.
139. Soc. of Automotive Engineers, handbook, 1913.
140. Soc. of Automotive Engineers, iron and steel specifications, March 19, 1922.
141. Soc. of Automotive Engineers, Journ., **4**, p. 520; 1919.
142. Soc. of Automotive Engineers, nonferrous metal specifications No. 30, March, 1922.
143. Soc. of Automotive Engineers, nonferrous metal specifications No. 32, March, 1922.
144. Soc. of Automotive Engineers, nonferrous metal specifications No. 33, March, 1922.
145. Soc. of Automotive Engineers, nonferrous metal specifications No. 31, March, 1922.
146. Soc. of Automotive Engineers, nonferrous metal specifications No. 71, March, 1922.
147. Soc. of Automotive Engineers, nonferrous metal specifications Nos. 68 and 69, March, 1922.
148. Soc. of Automotive Engineers, nonferrous metal specifications No. 63, March, 1922.
149. Soc. of Automotive Engineers, nonferrous metal specifications No. 67, March, 1922.
150. Soc. of Automotive Engineers, nonferrous metal specifications No. 66, March, 1923.
151. Soc. of Automotive Engineers, nonferrous metal specifications No. 64, March, 1922.
152. Soc. of Automotive Engineers, nonferrous metal specifications No. 40, March, 1922.
153. Soc. of Automotive Engineers, nonferrous metal specifications No. 81, March, 1922.
154. Soc. of Automotive Engineers, nonferrous metal specifications No. 65, March, 1922.
155. Soc. of Automotive Engineers, nonferrous metal specifications No. 62, March, 1922.
156. Soc. of Automotive Engineers, nonferrous metal specifications No. 80, March, 1922.
157. Soc. of Automotive Engineers, nonferrous metal specifications No. 74, March, 1922.
158. Soc. of Automotive Engineers, nonferrous metal specifications No. 70, March, 1922.
159. Soc. of Automotive Engineers, nonferrous metal specifications No. 41, March, 1922.
160. Soc. of Automotive Engineers, nonferrous metal specifications No. 43, March, 1922.
161. Soc. of Automotive Engineers, nonferrous metal specifications No. 42, March, 1922.
162. Soc. of Automotive Engineers, nonferrous metal specifications No. 76, March, 1922.
163. Soc. of Automotive Engineers, nonferrous metal specifications No. 73, March, 1922.
164. Soc. of Automotive Engineers, transactions, **11**, part 2, p. 272; 1916.
165. G. Bengough and O. Hudson, Soc. of Chem. Industries, Jour., January 31, 1908.
166. O. Bauer und W. Schneider, Stahl und Eisen, **1**, p. 647; 1921.
167. M. Foerster, Taschenbuch für den Maschinenbau, p. 396; 1914.
168. B. S. Circular No. 76; 1919.
169. B. S. Circular No. 101 (various sources); 1921.
170. B. S. Circular No. 73; 1918.
171. B. S. Circular No. 74; 1918.
172. B. S. Circular No. 58; 1924.
173. B. S. Circular No. 100; 1921.
174. B. S. Sci. Paper No. 453; 1922.
175. B. S. Tech. Paper No. 109; 1919.
176. B. S. Tech. Paper No. 207; 1922.
177. B. S. tests, report No. 0106b19; 1919.
178. B. S. tests, report No. 0829a19; 1919.

179. B. S. tests, report No. 0915a20; 1920.
180. B. S. tests, report No. 0805f18; 1918.
181. B. S. tests, report No. 0205a21; 1921.
182. B. S. tests, report No. 0508c18; 1918.
183. B. S. tests, report No. 0825b18; 1918.
184. B. S. tests, average results from the tests of Bureau of Standards.
185. B. S. tests, report No. 0217b22; 1922.
186. B. S. tests, report No. 1027a20; 1920.
187. B. S. tests, report No. 0504a21, 1921.
188. B. S. tests, report No. 1109a20; 1920.
189. U. S. Navy specifications No. 46B17, December 2, 1918.
190. U. S. Navy specifications No. 46N1a, March 1, 1917.
191. U. S. Navy specifications No. 46B14c, September 1, 1920.
192. U. S. Navy specifications No. 22W5, December 1, 1915.
193. U. S. Navy specifications No. 46M6b, February 1, 1919.
194. U. S. Navy specifications No. 46B5d, December 1, 1919.
195. U. S. Navy specifications No. 46M8b, February 1, 1918.
196. U. S. Navy specifications No. 46M4a, March 1, 1916.
197. U. S. Navy specifications No. 49B3a, May 1, 1917.
198. U. S. Navy specifications No. 46B13c, June 1, 1917.
199. U. S. Navy specifications No. 46B6e, February 1, 1919.
200. U. S. Navy specifications No. 49I1a, March 1, 1917.
201. U. S. Navy specifications No. 47I1b, May 1, 1922.
202. U. S. Navy specifications No. 46S2c, April 2, 1923.
203. U. S. Navy specifications No. 46S10a, March 1, 1917.
204. U. S. Navy specifications No. 46S6a, April 1, 1920.
205. U. S. Navy specifications No. 49S1f, November 1, 1922.
206. U. S. Navy specifications No. 47S3b, July 2, 1917.
207. U. S. Navy specifications No. 46M7c, January 3, 1922.
208. U. S. Navy specifications No. 46M1b, February 2, 1920.
209. G. Oosterheld, *Zeitschrift für Anorganische Chemie*, 97, p. 1; 1916.
210. W. von Selve, *Zeitschrift für Metallkunde*, pp. 40, 51; 1921.
211. *Zeitschrift des Vereines der Deutschen Ingenieure*, November 5, 1921.
212. *Zeitschrift des Vereines der Deutschen Ingenieure*, August 27, 1921.

INDEX

In view of the volume of this circular and a considerable number of graphical charts scattered through it, the cross references have been made fairly complete.

However, the general arrangement of materials made it unnecessary to indicate where a particular property of a given material is mentioned.

This index will locate an individual property only when it is found in a table or chart separate from the main table of properties of the material.

The reader should consult first the material in question and then the key words for individual properties, which may be given separately somewhere else.

	Page.		Page.
Abbreviations	6	Aluminum, Ag	27
Admiralty gun metal	52, 53	Cu	19, 20, 30
Aich's metal	60	Cu, Fe, Zn, Ni	21
Alloy "A"	20	Cu, Mg	21
Alloy "B"	20	Cu, Mn	21, 22
Alloy "C"	20	Cu, Ni, Mg	23, 24
Alloy "D"	22	Cu, Ni, Mg, Mn	24
Alloy "E"	28	Cu, Ni, Mn	24
Alloy "H"	22	Cu, Sn	24
Alloy "L-5"	27	Cu, Zn, Fe	24
Alloy "Y"	23	Mg	25
Alloy No. 5	41	Ni	25
Alloy No. 10	22	Ni, Cu	26
Alloy No. 11	21	Si	26, 27
Alloy No. 12	19	Ti	41
Alloy No. 17-S	22	Zn	27, 31
Alloy 3/20	28	Zn, Cu	27, 28
Alloy steels, definitions and uses	101-103	Zn, Cu, Mn	28
Alpax	26	W	27
Aluminum brass	58	Alzene	27
Aluminum bronze	38, 39, 40, 41, 139	Argental	27
effect of temperature	154	Antimony, pure	29
fatigue properties	37		
Aluminum, pure	16, 17	Babbitt	132
effect of temperature on tensile properties	18	Bearing alloys	46, 47, 48, 49, 132, 133
effect of low temperature on hard- ness and impact resistance	138	compressive properties at ele- vated temperatures	165
elasticity at high and low tem- peratures	166, 167	tensile properties at elevated temperatures	165
Aluminum, rivets	21	Bearing, ceco metal	42
sheet	18	Bearing metal, bronze	45
solder	131	Bearings, car journal	46, 48, 49
titanium bronze	41	Bell metal	44
		Benedict nickel	43

	Page.		Page.
Beryllium. <i>See</i> Glucinum.		Cast iron.....	84
Bismuth, alloys.....	29	effect of repeated heating and cooling.....	146
pure.....	29	effect of temperature.....	146, 154
elasticity at low temperature...	167	gray.....	84
Boiler plate, effect of temperature on tensile properties.....	147, 148	malleable.....	86
impact resistance.....	137	effect of temperature.....	154
Boron.....	29	white.....	84
Brass.....	55, 56, 57, 60, 137	Ceco, bearing metal.....	42
Brass, aluminum.....	58	Cerium.....	32
effect of temperature on modulus of elasticity in shear.....	166	Chemical symbols.....	7
effect of temperature.....	154, 155	Chromium.....	32
effect of low temperature on hardness and impact resistance.....	138	Cobalt, pure.....	32
impact properties.....	137	effect of low temperature on hardness.....	138
naval.....	70, 71	Cr, Mo, Fe, Mn, C.....	32
Navy.....	71	Composition "G".....	51
Navy, effect of temperature on tensile properties.....	154	Constantan.....	42
nickel, white.....	64	Conversion factors.....	6
tube, effect of annealing temperature..	168	Cooperite.....	129
Brazin, metal.....	57	Copper, cables.....	33
Britannia metal.....	130	nomenclature of alloys.....	37
Bronze, aluminum.....	38, 39, 40, 41, 139	pure.....	32-36
effect of temperature.....	154	effect of low temperature on hardness and impact resistance.....	138
fatigue properties.....	37	effect of temperature.....	31, 149
aluminum-titanium.....	41	elasticity at high and low temperatures.....	166, 167
effect of temperature.....	154, 155	Al, Fe.....	38, 39, 40
English, gear.....	50	Al, Sn.....	40
Lynx.....	42	Al, Ti.....	41
manganese.....	59, 61, 62, 63, 139	Ce.....	41
fatigue properties.....	37	Fe, Al.....	42
effect of temperature.....	154	Mn, Ni.....	42
Navy.....	53	Ni.....	42, 43
effect of temperature.....	154	Ni, Al.....	43
nickel.....	49	Pb.....	42
phosphor.....	46, 49, 50, 51, 54	Pb, Sn.....	42
elasticity at high temperature..	166	Pb, Sn, Ni.....	42
semiplastic.....	44	Sn.....	44, 47, 49, 50
Silliman.....	40	Sn, Ni, Zn.....	49
trolley wire.....	54	Sn, P.....	49, 50
victor.....	58	Sn, Pb.....	44, 45
white.....	64	Sn, Pb, P.....	45, 46
Cadmium.....	29	Sn, Pb, Zn.....	46, 47, 48
effect of temperature.....	149, 156	Sn, Pb, Zn, P.....	46
elasticity at high and low temperatures.....	166, 167	Sn, Si.....	51
Carbon, effect on properties of iron.....	73	Sn, Zn.....	51, 52, 53
effect on strength of steel.....	89, 93	Sn, Zn, P.....	52, 54
Car-journal bearings.....	46-49	Sn, Zn, Pb.....	53
		Zn.....	55, 56, 57

	Page.		Page.
Copper, Zn, Al.....	58	Gold, pure	72
Zn, Al, Fe, V.....	58	elasticity at high and low tem-	
Zn, Al, Mn, Fe.....	58, 59	peratures.....	166, 167
Zn, Al, Mn, V.....	59	Government bronze.....	51, 53
Zn, Fe.....	59, 60, 61	Gun bronze.....	44, 53
Zn, Fe, Mn.....	61	Gun metal.....	53
Zn, Fe, Sn.....	59	admiralty.....	52
Zn, Fe, Sn, Al, Mn.....	59, 61	leaded.....	44
Zn, Mn.....	62, 63	Hardness, relation to tensile strength of	
Zn, Mn, Fe.....	63	steel.....	136
Zn, Ni.....	64, 65, 68	Illium.....	126
Zn, Ni, W.....	69	Impact properties of metals..	137, 138, 139, 167
Zn, Pb.....	61	Impact properties of steels, effect of tem-	
Zn, Pb, Sn.....	62	perature.....	167
Zn, Sn.....	69, 70, 71	Invar.....	113
Zn, Sn, Fe.....	71	Iridium.....	72
Zn, Sn, Fe, Al, Mn.....	62	Iron, Al.....	72, 73
Zn, Sn, Pb.....	71	Si.....	73
Definitions.....	9-15	and steel specifications, S. A. E....	77-83
Delta metal.....	61	malleable.....	86
Dow metal.....	124	effect of temperature.....	154
Drawing temperature, effect on tensile		pure.....	72
properties of steel.....	79-83, 110, 111, 120	effect of temperature on hard-	
Duralumin.....	22, 137	ness and impact resistance... ..	138
effect of cold working.....	31	elasticity at high and low tem-	
effect of heat treatment.....	23, 30	perature.....	166, 167
effect of low temperature on hard-		wrought.....	86, 87, 88
ness and impact resistance.....	138	effect of temperature on com-	
effect of temperature on tensile		pressive properties.....	162
properties.....	30	Journal bearings.....	46-49
elasticity at high temperature... ..	166	Lead, Ba.....	123
impact properties.....	137	Sb.....	121, 122
Duralumin rivets.....	23	pure.....	121
Durana metal.....	69	effect of temperature.....	149, 156
Elasticity of metals at high and low		effect on properties of copper alloys .	53
temperatures.....	166, 167	elasticity at high and low tem-	
Electron metal.....	124	peratures.....	166, 167
English gear bronze.....	50	Leaded gun metal.....	44
Fatigue properties of aluminum and		Lipowitz's alloy.....	29
manganese bronzes.....	37	Low temperature, effect on hardness and	
Fatigue properties of steel.....	139-145	impact properties of metals.....	138
Ferronickel, effect of low temperature on		effect on modulus of elasticity.....	167
hardness and impact resistance.....	138	Lynite.....	20
Ferrous materials, terminology.....	74-76	Lynx bronze.....	42
Flow of steels at high temperature.....	151	Magnalium.....	25
Gear, phosphor bronze.....	49, 50	Magnesium, Al.....	124
Genelite.....	72	Zn.....	124
German silver.....	68	effect of temperature.....	149, 156
Glucinum.....	72	elasticity at low temperature.....	167
Gold, Cu.....	72	pure.....	123, 124
Cu, Ag.....	72		

	Page.		Page.
Major metal	21	Partinium	27
Malleable iron	86	Phosphor bronze	46, 49, 50, 51, 54
Malleable cast iron, effect of tempera- ture	154	elasticity at high temperature . .	166
Manganese	124	Platinite	113
bronze	59, 61, 62, 63, 139	Platinoid	69
effect of temperature	154	Platinum	129
fatigue properties	37	elasticity at high and low tempera- tures	166, 167
effect on properties of iron	73	Red brass	46, 62
Manganin	42	Red metal	57
effect of temperature on modulus of elasticity in shear	166	References, list	194
Manila rope	169	Rezistal	116
Modulus of elasticity, effect of tempera- ture	166, 167	Rhodium, elasticity at low tempera- ture	167
Moisture content, effect on properties of wood	194	Rivets, alloy 3/20	28
Molybdenum	124	aluminum	21
wire, effect of temperature	160	duralumin	23
Monel metal	126, 127, 128, 137	Roman metal	42
effect of temperature	153, 154, 155	Rope, manila	169
impact properties	137	wire	99, 100, 101
Muntz metal	56	Rose's metal	29
Music wire	98	Semisteel	84, 85
Naval brass	70, 71	effect of temperature	154
Navy brass	71	Silliman bronze	40
Navy gun bronze	53	Silumin	27
Navy valve bronze	53	Silver, Cu	130
Newton's alloy	29	Cu, Cd	130
Nichrome	126	pure	129, 130
Nickel, Cr, Cu, Mo, W	126	elasticity at high and low tem- peratures	166, 167
Cu, Fe, Mn	126, 127, 128	Solder, aluminum	131
Fe, Cr, Mn	126	Specimens, standard	10
Mn, Fe, Si	128	Stainless iron	106
Ta	129	steel	108, 158
W, Zr	129	effect of temperatures	158
Nickel brass, white	64	effect of drawing temperature . .	110
Nickel bronze	49	Steel, Cr	105, 106
pure	125, 126	Cr, effect of heat treatment	105
elasticity at high and low tem- peratures	166, 167	Cr, effect of temperature	156
effect of temperature	149, 153, 156, 161	Cr, Mo	104
Nickel silver	64, 65, 68, 137	Cr, Mo, effect of temperature	158
effect of heat treatment	66, 67	Cr, Mo, V	104
elasticity at high temperature . .	166	Cr, Ni	106
impact properties	137	Cr, Ni, effect of drawing tempera- ture	111
Nongram	52	Cr, Ni, effect of temperature on compressive properties	164
Palladium	129	Cr, Ni, Mo	106
elasticity at high and low tempera- tures	166, 167	Cr, V	107

	Page.		Page.
Steel, Cr, V, effect of drawing temperature	101	Steel and iron specifications, S. A. E.	77-83
Cr, V, effect of temperature	150, 158	carbon	88-97, 137
Cr, W, impact properties	137	effect of drawing temperature ..	79, 80
Co	107, 108	effect of temperature on tensile properties	147, 148, 149, 150, 154, 157, 159
Mn, effect of temperature	157	effect of temperature on compressive properties	162, 163
Mo	108, 109, 112	effect of temperature on torsional properties	155
Ni	112, 113, 137	effect of temperature on impact resistance	167
Ni, effect of drawing temperature	80, 81, 111	effect of low temperature on hardness and impact resistance	138
Ni, effect of temperature on tensile properties	153, 154, 157	Ni, impact properties	137
Ni, effect of temperature on torsional properties	155	Ni, Cr, effect of temperature on tensile properties	152, 159
Ni, effect of temperature on impact resistance	167	Ni, Cr, effect of temperature on impact resistance	167
Ni, effect of low temperature on hardness and impact resistance ..	138	Ni, Cr, effect of low temperature on hardness and impact resistance ..	138
Ni, impact properties	137	Ni, Cr, effect of drawing temperature	81, 82, 83
Ni, Cr, effect of temperature on tensile properties	152, 159	Ni, Cr, Si	116
Ni, Cr, effect of temperature on impact resistance	167	Ni, Mo	112
Ni, Cr, effect of low temperature on hardness and impact resistance ..	138	Ni, Si	113
Ni, Cr, effect of drawing temperature	81, 82, 83	Ni, Si, Ce	114
Ni, Cr, Si	116	Ni, Si, Cu	114
Ni, Mo	112	Ni, Si, Mo	114
Ni, Si	113	Ni, Si, U	115
Ni, Si, Ce	114	Ni, Si, V	115
Ni, Si, Cu	114	Ni, Si, Zr	115
Ni, Si, Mo	114	Ni, Si, Zr, Co	115
Ni, Si, U	115	Ni, V	115
Ni, Si, V	115	Ni, V, effect of temperature on torsional properties	155
Ni, Si, Zr	115	Ni, U, effect of temperature	157
Ni, Si, Zr, Co	115	Si	117
Ni, V	115	Ti	118
Ni, V, effect of temperature on torsional properties	155	V	118
Ni, U, effect of temperature	157	V, effect of temperature on torsional properties	155
Si	117	U	118
Ti	118	W	118
V	118	W, effect of temperature	158
V, effect of temperature on torsional properties	155	W, effect of drawing temperature ..	120
U	118		
W	118	Stellite	32
W, effect of temperature	158	Sterro metal	59
W, effect of drawing temperature ..	120	Stone's English gear bronze	50
		Tantalum	130
		Tellurium	130
		Tensilite	59
		Temperature, effect on tensile properties of metals, see the metal in question	
		effect on compressive properties of steels	162, 163, 164
		effect on compressive properties of white metal bearing alloys	165
		effect on hardness and impact resistance of some metals	138, 167
		effect on torsional properties of cold rolled steel, Ni-steel, Ni-V steel, V-steel, brass, elephant bronze, Mn-bronze, Tobin bronze, Delta metal, Monel metal	155
		effect on moduli of elasticity of metals	166, 167
		Terminology of ferrous materials	74-76
		Tin, Al, Zn, Cd	130
		Sb, Cu	132
		Sb, Cu, Zn	130

	Page.		Page.
Tin, Zn, Al, Cu, Sb, Pb.....	131	White bronze.....	64
Zn, Al, Pb, Cu, Sb.....	131	White metal bearing alloys.....	132
Zn, Al, Sb.....	131	effect of temperature on compres-	
pure.....	130	sive properties.....	165
effect of temperature.....	149, 156	White nickel brass.....	64
elasticity at high and low tem-		Wire copper.....	35, 36
peratures.....	166, 167	rope.....	99, 100, 101
Titanium.....	132	steel.....	98
Tobin bronze.....	69, 70	Wood, change of properties with change	
Torpedo bronze.....	70	of moisture content.....	194
Torsional properties, effect of tempera-		properties in an air dry condition.....	184-193
ture on carbon steel, Ni-V steel, Ni		properties in a green condition... ..	172-183
steel, V steel, brass, elephant bronze,		Wood's metal.....	29
Mn bronze, Tobin bronze, Delta metal,		Wrought iron.....	86, 87, 88
Monel metal.....	155	effect of temperature on compres-	
Trolley wire.....	54	sive properties.....	162
Tungsten.....	132, 134	Yellow brass.....	56, 61, 62
Ulco metal.....	123	Zinc.....	134, 135
Uranium.....	134	effect of temperature.....	149, 153, 156
Valve bronze.....	53	elasticity at high and low tem-	
Vanadium.....	134	peratures.....	166, 167
Victor bronze.....	58	Zirconium.....	135

