

Research Article

Feasibility Analysis and Simulation of Integrated Renewable Energy System for Power Generation: A Hypothetical Study of Rural Health Clinic

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This paper presents the feasibility analysis and study of integrated renewable energy (IRE) using solar photovoltaic (PV) and wind turbine (WT) system in a hypothetical study of rural health clinic in Borno State, Nigeria. Electrical power consumption and metrology data (such as solar radiation and wind speed) were used for designing and analyzing the integrated renewable energy system. The health clinic facility energy consumption is 19 kWh/day with a 3.4 kW peak demand load. The metrological data was collected from National Aeronautics and Space Administration (NASA) website and used to analyze the performance of electrical generation system using HOMER program. The simulation and optimization results show that the optimal integrated renewable energy system configuration consists of 5 kW PV array, BWC Excel-R 7.5 kW DC wind turbine, 24 unit Surrette 6CS25P battery cycle charging, and a 19 kW AC/DC converter and that the PV power can generate electricity at 9,138 kWh/year while the wind turbine system can generate electricity at 7,490 kWh/year, giving the total electrical generation of the system as 16,628 kWh/year. This would be suitable for deployment of 100% clean energy for uninterruptable power performance in the health clinic. The economics analysis result found that the integrated renewable system has total NPC of 137,139 US Dollar. The results of this research show that, with a low energy health facility, it is possible to meet the entire annual energy demand of a health clinic solely through a stand-alone integrated renewable PV/wind energy supply.

1. Introduction

The global environmental concerns over the use of fossil fuels for electric power generation have increased the interest in the utilization of renewable energy resources. In particular, rapid advances in wind turbine generator and photovoltaic technologies have brought opportunities for the utilization of wind and solar resources for electric power generation worldwide [1]. Solar and wind energy systems are omnipresent, freely available, and environmental friendly, and they are considered as promising power generating sources due to their availability and topological advantages for local power generations [2, 3]. However, a drawback, common to solar and wind options, is their unpredictable nature and dependence on weather and climatic changes, and the variations of solar and wind energy may not match with the time distribution of load demand. This shortcoming not only affects the system's energy performance, but also results in batteries being discarded too early. Generally, the independent use of both energy resources may result in considerable oversizing, which in turn makes the design costly. It is prudent that neither a stand-alone solar energy system nor a wind energy system can provide a continuous power supply due to seasonal and periodical variations [2, 4] for stand-alone systems. Fortunately, the problems caused by the variable nature of these resources can be partially or wholly overcome by integrating these two energy resources in a proper combination, using the strengths of one source to overcome the weakness of the other. The use of different energy sources allows improving the system efficiency and reliability of the energy supply and reduces the energy storage requirements compared to systems comprising only one single renewable energy source. With the complementary characteristics between solar energy and wind energy for certain locations, the integrated renewable solar/wind power generation systems with storage banks offer a highly reliable source of power [5, 6], which is suitable to electrical loads that need higher reliability such as the health clinic.

Moreover, the economic aspects of these technologies are now sufficiently promising to also justify their use in smallscale stand-alone applications for residential/ranch, communication, and health clinic use; several design scenarios have been proposed for the design of solar/wind power systems for stand-alone applications [7–9].

Integrated renewable (solar/wind) energy systems use two renewable energy sources, allow improving the system efficiency and power reliability, and reduce the energy storage requirements for stand-alone applications. The integrated renewable (solar/wind) systems is becoming popular in remote area power generation applications due to advancements in renewable energy technologies.

This study is on the feasibility analysis of a health facility load data and the renewable resources and evaluates the performance of the designed stand-alone PV/wind generation systems.

2. Hypothetical Study of a Rural Health Clinic in Nigeria

A standard health clinic in rural Nigeria requiring 19 kWh per day to run is considered and was used in the establishment of a hypothetical study for the electrical load data described by [10]. The power consumption rating that was used for the electrical load data and pattern of use are shown in Tables 1 and 2, respectively. Figure 1 shows the daily profile electricity consumption of this health clinic.

2.1. Load Variation. As from 06.00 hrs to 08.59 hrs, load is at the least (462 W). The load increased a little at 09.00 hrs (992 W) and at 10.00 hrs reached a certain level (1255 W) and remains there till 11:59 hr and at 12:00 hr increased again and reached the highest load (3366 W). It comes down at 13.00 hrs (1837 W) and remains there till 14.59 hrs, decreases little at 15.00 hrs (482 W), and remains there till 17.59 hrs where it starts to increase again. As from 10:00 hr to 15:59 hr, most of the energy generated by solar at these times is stored in the battery for use at night with wind energy.

At night between 18.00 hrs and 05.59 hrs, the load is minimal (502 W). Since wind blows much at night than in day, wind energy and the stored energy in the battery can compensate at these hours of time till day time when solar takes up.

2.2. Meteorological Data Generation for Feasibility Study. Climatic conditions determine the availability and magnitude

TABLE 1: Power consumption rating.

| Power consumption | Power (Watts) | Qty | $\begin{array}{c} \text{Load} \\ (\text{watt} \times \text{qt}) \end{array}$ |
|--|------------------|-----|--|
| Vaccine refrigerator/freezer | 60 | 1 | 60 |
| Small refrigerator (nonmedical use) | 300 | 1 | 300 |
| Centrifuge | 575 | 1 | 575 |
| Hematology mixer | 28 | 1 | 28 |
| Microscope | 15 | 1 | 15 |
| Security light | 10 | 4 | 40 |
| Lighting | 10 | 2 | 20 |
| Sterilizer oven (laboratory autoclave) | 1,564 | 1 | 1,564 |
| Incubator | 400 | 1 | 400 |
| Water bath | 1,000 | 1 | 1,000 |
| Communication via VHF radio | | 1 | |
| Stand-by | 2 | | 2 |
| Transmitting | 30 | | 30 |
| Desktop computer | 200 | 2 | 400 |
| Printer | 65 | 1 | 65 |



FIGURE 1: Daily load profile of the health clinic (load variation).

of solar and wind energy at a particular location. For different districts and locations, climatic conditions, including solar radiation, wind speed, and air temperature, are always changing. At the potential location, an analysis of the characteristics of solar radiation and wind conditions were made for better utilization of the solar and wind energy resources.

The data for monthly average solar radiation and wind speed for a given year (2013) were obtained from National Aeronautics and Space Administration (NASA) [11]. The specific geographical location (latitude and longitude) of the health clinic in Guzamala (Borno State) is at a location of $11^{\circ}05'$ N latitude and $13^{\circ}00'$ E longitude. This location has an annual average solar radiation of 5.90 kWh/m²/d, whereas its annual average wind is 3.8 m/s. In the solar resource, March was the sunniest month of the year. In this month (March), the solar energy resource is 6.7 kWh/m²/day, while in August it is only 5.1 kWh/m²/day, whereas, in the wind resource, September is the least windy month of the year while April

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| Time | | | | | | | Daily lo | ad demai | nds | | | | | | Total/hr |
|-------------|------|------|------|----|----|-----|----------|----------|------|------|----|-----|------|-----|----------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | |
| 0.00-0.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 1.00-1.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 2.00-2.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 3.00-3.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 4.00-4.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 5.00-5.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 6.00-6.59 | 60 | | | | | | | | 400 | | 2 | | | | 462 |
| 7.00-7.59 | 60 | | | | | | | | 400 | | 2 | | | | 462 |
| 8.00-8.59 | 60 | | | | | | | | 400 | | 2 | | | | 462 |
| 9.00-9.59 | 60 | | | | 15 | | 20 | | 400 | | 2 | 30 | 400 | 65 | 992 |
| 10.00-10.59 | 60 | 300 | | 28 | 15 | | 20 | | 400 | | 2 | 30 | 400 | | 1255 |
| 11.00-11.59 | 60 | 300 | | 28 | 15 | | 20 | | 400 | | 2 | 30 | 400 | | 1255 |
| 12.00-12.59 | 60 | 300 | 575 | | 15 | | 20 | 1564 | 400 | | 2 | 30 | 400 | | 3366 |
| 13.00-13.59 | 60 | 300 | 575 | | 15 | | 20 | | 400 | | 2 | | 400 | 65 | 1837 |
| 14.00-14.59 | 60 | 300 | | | | | 20 | | 400 | 1000 | 2 | | | 65 | 1847 |
| 15.00-15.59 | 60 | | | | | | 20 | | 400 | | 2 | | | | 482 |
| 16.00-16.59 | 60 | | | | | | | | 400 | | 2 | | | | 462 |
| 17.00–17.59 | 60 | | | | | | | | 400 | | 2 | | | | 462 |
| 18.00-18.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 19.00-19.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 20.00-20.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 21.00-21.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 22.00-22.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| 23.00-23.59 | 60 | | | | | 40 | | | 400 | | 2 | | | | 502 |
| Total | 1440 | 1500 | 1150 | 56 | 75 | 480 | 140 | 1564 | 9600 | 1000 | 48 | 120 | 2000 | 195 | 19368 |

TABLE 2: The electrical load (daily load demands) data for a health facility.

1: Vaccine refrigerator/freezer, 2: Small refrigerator (nonmedical use), 3: Centrifuge, 4: Hematology mixer, 5: Microscope, 6: Security light, 7: Lighting, 8: Sterilizer oven (laboratory autoclave), 9: Incubator, 10: Water bath, 11: Communication via VHF radio stand-by, 12: Communication via VHF radio transmitting, 13: Desktop computer, 14: Printer.

and March are the windiest. Figures 2(a) and 2(b) show the solar and wind resource profile of this location.

2.3. Solar Radiation Variation. In the months of September, October, January, February, and March, the solar radiation increases with differences from month to month as (0.43), (0.32), (0.26), (0.69), and (0.40), respectively, whereas, in the months of April, May, June, July, August, November, and December, the solar radiation decreases with differences from month to month as (0.08), (0.26), (0.39), (0.54), (0.29), (0.05), and (0.49), respectively.

2.4. Wind Speed Variation. In the months of January and February, the wind speed remains the same without differences from the months. In the months of March, April, October, November, and December, the wind speed increases with differences from month to month as (0.4), (0.1), (0.3), (0.6), and (0.5), respectively. In the months of May, June, July, August, and September, the wind speed decreases with differences from month to month as (0.4), (0.7), (0.2), (0.2),

and (0.2), respectively. In the months of July, August, and September the wind speed has constant decrease of (0.2) differences from month to month.

The difference in months falls in the range of 0.1–0.7, and these differences are due to earth's rotation.

2.5. System Configuration. The block diagram for a typical stand-alone PV/wind generating system is shown in Figure 3. The system consists of PV panels, wind turbine generator, storage batteries, and dump load. These technologies generate DC current—PV, wind, and battery - and are connected to the DC bus (V_{DC}). An inverter, or a DC-to-AC converter, is used to convert DC current ($I_{inv.DC}$) to AC current (I_{inv_AC}). The generating system (PV/Wind) supplied to the load and the storage batteries are charged when the renewable energy (wind and solar) generation exceeds the load demand until a specified upper limit for the battery voltage is reached, when it can no longer accept current. At this point the excess available power is diverted to the dump load (a device that sheds excess energy produced by the system), which



FIGURE 2: (a) HOMER output graphic for solar (clearness index and daily radiation) profile. (b) HOMER output graphic for wind speed profile.

in this study is assumed to be an electric water heater, and the remaining power sold to the community. Batteries will discharge, supplying power to the load when demand exceeds generation. They will continue discharging until a specified lower limit for the battery voltage is reached. At that point, the batteries will stop supplying power to the load, and the renewable energy if available will supply the required power to the load.

3. Modeling and Simulation of Integrated Renewable Solar/Wind System Components

The HOMER software was used to design an optimal integrated renewable power system. The description of HOMER can be found in Ani [12]. Reference to relevant literature provided the design guidelines. The capital costs of all the system components used for the study were gotten from PV system suppliers in Nigeria [13]. The price of PV system is \$2000/kW, while a wind turbine (BWC Excel-R) system costs \$27,000 and a Surrette 6CS25P battery costs \$1,145. The project lifetime is estimated at 20 years and the yearly interest rate applied is 6%. A schematic diagram of an integrated renewable energy system is shown in Figure 4.

4. Results

4.1. Cost of System Component Summary

4.1.1. Solar PV Panels. The proposed PV module is rated at 5 kW. The initial cost of the modules is \$10,000, and its operation and maintenance cost is \$57, with the total NPC (for the PV module only) of \$10,057, as can be seen in Figure 5. The lifetime of the modules will last the project.

4.1.2. Wind Turbine. The BWC Excel-R wind turbine has a capacity of 7.5 kW. Its initial cost is \$27,000, and its operation and maintenance cost is \$3,441, with the total NPC (for the wind turbine only) of \$30,441. The turbine is estimated to last the project.

4.1.3. Battery. The Surrette 6CS25P battery is rated at 6 V and has a capacity 1,156 Ah. Twenty-four batteries initially cost \$27,480 and the replacement cost and the operation and maintenance cost add a further \$11,927 and \$55,056, respectively, and a salvage cost of \$-2,494 having the total NPC (for the batteries only) of \$91,968.

4.2. Converter. The converter is rated 19 kW. Its initial cost is \$3,800, and its operation and maintenance cost is \$872, with the total NPC (for the converter only) of \$4,672. The converter is estimated to last the project.

4.3. Integrated Renewable Energy System Component. The integrated renewable energy component system has total capital of \$68,280; the replacement cost and the operation and maintenance cost add a further \$11,927 and \$59,426, respectively, and a salvage cost of \$-2,494, giving the total NPC (for the coupled (complete) system) of \$137,139, as shown in the appendix (Figure 9). This can convince policy makers of the worthiness of the investment in integrated or single renewable energy.

4.4. Electricity Production. The average solar radiation in this location is relatively high. This gives a relatively good possibility and opportunity to engage the photovoltaic (PV) technique and technology as a component of an integrated renewable PV/wind energy system in order to produce clean energy for powering health clinic loads. Although wind speed is relatively moderate with an average of 3.8 m/s throughout the year, it compensates for solar during the months of poor radiation.

It can be noticed that more solar irradiance can be expected from the month of February to June while less solar irradiance is to be expected from December to January. On the other hand, more wind speed can be expected from the month of December to May while less wind speed is to be expected from August to October.

Solar PV compliment wind power during the months (August, September, and October) of poor wind speed, while wind compensates for solar power during the months (December and January) when solar radiation is less as shown in Figure 6.



FIGURE 3: Configuration of the integrated renewable (PV/wind) energy system with the energy storage and dump load.



FIGURE 4: The network architecture for the HOMER simulator (proposed PV/wind power system).



FIGURE 5: Net present cost of components of the integrated renewable PV/wind energy system.



FIGURE 6: Electrical production of integrated renewable PV/wind energy system.



FIGURE 7: Excess electricity versus battery state of charge.

TABLE 3: Simulation results of the electricity production (kWh/yr), battery and inverter losses, and excess energy of the energy system configuration (PV/wind).

| System operation | PV/wind | system |
|-----------------------------------|---------|--------|
| Consumption | kWh/yr | % |
| DC primary load | 7,082 | 100 |
| The total load to be supplied | 7,082 | 100 |
| Production | kWh/yr | % |
| PV array | 9,138 | 55 |
| Wind turbine | 7,490 | 45 |
| Total energy generated | 16,628 | 100 |
| Losses | kWh | /yr |
| Battery | 46 | 0 |
| Inverter | 1,25 | 50 |
| Total losses | 1,71 | 10 |
| Excess energy going to dump load | 7,83 | 36 |
| Total energy supplied to the load | 7,08 | 32 |

The integrated renewable energy system (PV/Wind) produces 9,138 kWh/yr (55%) from solar PV array and 7,490 kWh/yr (45%) from wind turbine making a total of 16,628 kWh/yr (100%) as shown in Table 3 and Figure 10 in the appendix. The load demand is 7,082 kWh/yr, while the



FIGURE 8: Integrated renewable energy (PV/Wind) versus battery state of charge.



FIGURE 9: The network architecture for the HOMER simulator, proposed PV/wind power system and its optimization results.



FIGURE 10: Cost summary of the integrated renewable energy system.

excess electricity from the system is 7,836 kWh/yr also shown in Table 3 and Figure 10 in the appendix.

4.5. Excess Electricity. Excess electricity always occurs when the battery state of charge (SOC) is at 93% upwards and discharges less (at the rate of 1.5 kW to 2.5 kW) and this is between Novembers and Mays. Between Junes and Octobers when the integrated renewable (solar radiation and wind speed) is low, the battery SOC is at 92% downward and



FIGURE 11: Electricity production summary of the integrated renewable energy system.

| en Architecture. | 5 kW PV 1 BWC Excel-R 24 Sumethe 6CS25P | 19 kW Investi 19 kW Rectifi | er N | | | Total NPI Levelized Operating | C \$137,138 COE: \$1.688/ Cost \$6,003/5 |
|--|---|--------------------------------|------------------|----------------------------------|--|-------------------------------------|--|
| ost Summary Ca | ash Flow Electrical PV | XLR 8 | attery Converter | Emissions Hourly Data | | | |
| | Quantity | Value | Units | Quantity | Value | Units | |
| | Rated capacity | 5.00 | kW/ | Minimum output | 0.00 | kW/ | |
| | Mean output | 1.04 | kW. | Maximum output | 5.83 | kW/ | |
| | Mean output | 25.0 | kWh/d | PV penetration | 129 | 24 | |
| | Capacity factor | 20.9 | 2 | Hours of operation | 4,358 | he/ye | |
| | Total production | 9,138 | kWh/yr | Levelized cost | 0.0960 | \$/k/wh | |
| 24 | | | PV Out | put | | | kW - 50 |
| 24- | | | PV Out | put | | | KW 6.0 |
| 24 | | | PV Out | put | | | KW 5.4 4.8 |
| 24- | | | PV Out | pot | | | kW 5.0 5.4 4.8 4.2 |
| 24- 18- | a and a state of the | | PV Out | pot | or initial and initial | ti dist | 10 5.4 5.4 4.2 2.8 |
| 24. 19. Mg 12. | | | PV Out | pot | 170 | | KW 5.0 6.4 4.3 4.2 2.6 -3.0 |
| 24- 18- Ang to an | | 1 978-1 | PV Out | pot | iei | | WW 6.0 6.4 4.8 4.2 2.8 3.0 2.4 2.4 2.4 |
| 24- 19- Atg to 20- | ie uu. | 17 (0.) | PV Out | ри (49.767, <mark>96</mark>) | | • | kW 69 6,4 4,2 3,5 3,0 2,4 1 1,2 2,4 1,2 1,2 |
| 24 19 10 10 10 10 10 10 10 10 10 10 10 10 10 | 1 0 900 | 17 10.1 | PV Out | 01724 <mark>14</mark> | | • | kW 69 5,4 4,8 4,8 3,8 3,8 2,4 4 1,8 1,2 4 1,2 1,2 1,2 1,2 1,2 1,2 1,2 1,2 1,2 1,2 |
| 24 19 10 10 10 10 10 10 0 0000 6 | 19 900 | 1 770) | PV Out | м 60767 <mark>88</mark> | | | WW 5.4 4.8 4.2 3.0 2.4 1.8 1.2 2.4 1.8 0.0 |
| 24- 18- 60 12- 0- | | 1 770-1 | PV Out | en Tei (el | | | kW 6,4 4,8 4,8 4,8 4,8 4,8 4,8 4,8 4,8 4,8 4 |

FIGURE 12: PV output summary.

| iem Avchitecture. | 5 kW PV 1 BWC Excel-R 24 Sumethe 6CS25P | 19 kW Inverte 19 kW Rectifie | el R | | | | Total N Levelizi Operati | PC: \$137,138 wd CDE: \$1.688/kW/ wg Cost: \$6,003/yr |
|-------------------|---|---------------------------------|-----------------|-----------|--------------------|-------|--------------------------------|---|
| Cost Summary Ca | sh Flow Electrical PV | XLR B. | attery Converte | Emissions | Hourly Data | | | |
| | Quantity | Value | Units | | Quantity | Value | Units | |
| | Total rated capacity | 7.50 | kW. | h | finimum output | 0.00 | kW/ | |
| | Mean output | 0.86 | kW/ | h | faximum output | 8.08 | kW | |
| | Capacity factor | 11.4 | * | V | Vind penetration | 106 | * | |
| | Total production | 7,490 | kWh/yr | H | lours of operation | 7,422 | he/ye | |
| | | | | L | evelized cost | 0.354 | \$/k\wh | |
| | | | | | | | | |

FIGURE 13: Wind turbine (BWC Excel-R) output summary.



FIGURE 14: Battery bank state of charge summary.

discharges much (at the rate of 3 kW to 10 kW) and there will be no excess electricity from this point downward (due to poor solar radiation and less wind speed) as shown in Figures 7 and 8.



FIGURE 15: Converter output summary.

| stem Architecture: | 5 kW PV 1 BWC Exc 24 Sumette | el-R 6CS25P | 19 kW Irwe 19 kW Rec | nter tilfær | | | | Total NPC: \$137,138 Levelized COE: \$1.68 Operating Cost: \$6.00 | 8/kW1 3/w |
|--------------------|------------------------------------|----------------|-------------------------|----------------|-----------|-----------|--------------|---|--------------|
| Cost Summary Ca | ssh Floer El | lectrical PV | XLR | Battery | Converter | Emissions | Houly Data | | |
| | | | | Pol | utant | Emissi | ione (kg/yr) | | |
| | | | C | arbon diox | de | | 0 | | |
| | | | C | arbon mon | oxide | | 0 | | |
| | | | U | inburned h | diocarbor | 10 | 0 | | |
| | | | P | articulate n | notter | | 0 | | |
| | | | S | ultur dioxid | e | | 0 | | |
| | | | N | itrogen mi | des | | 0 | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |

FIGURE 16: Emission output summary.

5. Conclusion

This paper describes the feasibility study of load data and the renewable resources and evaluates the performance of the designed stand-alone PV/wind generation systems. Hourly average wind speed and solar radiation data from the site for the generating unit and the anticipated load data are used to predict the general performance of the generating system. These power systems are very well suited to supply the specific load demand of the rural health clinic that presents a peak in the day time (afternoon) when the solar radiation is maximum and minimal load at night time when the wind blows much (since wind blows much at night than in day). Such performance evaluations are useful in estimating the component sizes needed for generation systems to supply power to loads reliably. It is also helpful in performing a detailed economic analysis (cost benefit study) for the generating unit. Of particular interest is the introduction of dump load model. The excess wind and solargenerated power, when available, are used to heat water in an electric water heater, and the remaining power is sold to the community. This heated water can be used for any purposes in the health clinic such as drinking water. Finally, in the integrated renewable PV/wind energy system, there is no fuel consumption, which means no emission of CO₂, CO, UHC, PM, SO_2 , and NO_r from the energy system. This system configuration would be suitable for deployment of 100% clean energy for uninterruptable power performance.

Appendix

See Figures 9, 10, 11, 12, 13, 14, 15, and 16.

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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