Using Artificial Intelligence in the Computer Aided Manufacturing of Friction Stir Welds

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Abstract

The use of Artificial Intelligence (AI) in the Computer Aided Manufacturing (CAM) of Friction Stir Welds (FSW) is being investigated in the collaborative <u>aiCAM</u>^{stir} <u>project</u>. Computional Fluid Dynamics (CFD) were used for optimising the tool design of FSW tools for lap welding^[1] in the first task of the ongoing project (Fig. 1 to 3). Analytical modelling was used to calculate the FSW power. The vision is to develop a software-package that adjusts the parameters automatically based on CFD, analytical modelling, parameter monitoring, image analysis and non-destructive testing.

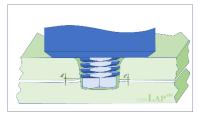


Fig.1: Pentagonal tool for disrupting the oxide layer during lap welding^{[4][5]}

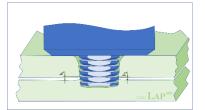


Fig. 2: Counterflow tool with left-handed, right-handed and neutral threads on 3 ridges^[3]

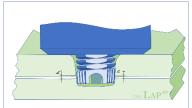


Fig. 3: Cylindrical tool with three rifeled prongs to disrupt the oxide layer^{[2][6]}

Introduction

It is generally difficult to choose and optimise the friction stir welding tool design and welding parameters for lap welding, as shown by many publications. [2] Therefore, it is desired to add a new computer aided manufacturing control system to FSW machines, which recommends (or even automatically optimises) parameters based on computational fluid dynamics (CFD), finite element analysis (FEA), design of experiments (DOE), Wikipedia-like open source cloud data and artificial intelligence (AI) including machine learning.

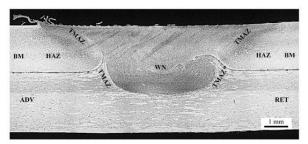


Fig. 4: Benchmark: Conventinal butt welding tool used for lap joints at 1200 rpm at 250 mm/min^[3]

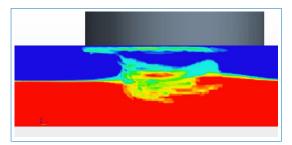


Fig. 5: <u>Computational fluid dynamics</u> analysis of material flow using a conventional butt welding tool^[3]

Computational Fluid Dynamics (CFD)

A preliminary CFD study has been conducted to simulate and understand the effect of the material flow around a profiled tool, with the objective to overcome the problems caused by thinning and hooking in friction stir lap welding.

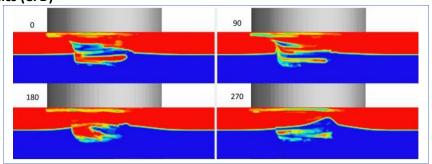


Fig. 6 <u>Simulation of the material flow during friction stir lap welding</u> looking at the tool from different directions at 0°, 90°, 180° and 270°

It was possible to develop a straight-forward model for CFD simulation of FSW. Only two widely available inputs were required: The pseudo static material strength at room temperature and the melting temperature of the workpiece. A good comparison with test data for temperature and mixing of the materials could be achieved as well as an acceptable correlation between the measured and predicted torque by explicit simulation of the thread. It could be shown that the thread position and the rotation affects the mixing of the sheets.

Analytical Equations and Derivation of the FSW Torque and Power

The welding speed during friction stir welding depends on variables defined within the associated welding procedure. The FSW conditions are defined by adopting a combination of the linear and rotation speeds of the tool. The power required to make a weld is the result of the torque needed to turn the tool at the chosen rotation speed. These observations provide a simplified set of equations for the prediction of the power needed to make a Friction Stir Weld. The final equation is easy to use and has a wide range of applicability.

Strength, σ [edit] A simple assumption about the relationship between the workpiece material strength and temperature is made. The ambient value is assumed and a linear variation of strength occurs down to zero strength at the material melting point. $\sigma = \sigma_0 - \frac{\sigma_0}{T_m - T_0} (T - T_0)$ Torque, t [edit]The torque is derived from a requirement to yield the workpiece material at the FSW tool. It is assumed that the stress on the face of the tool is equal to the strength of the material at the temperature r. Integration of this stress across the area of the shoulder (ignoring the presence of the pin) gives the following expression. $t = \frac{2}{3}\pi R^3 \sigma$ Power, P [edit]The FSW power is equal to the torque, t, multiplied by the rotation speed, ω . Use of the equation above gives the following expression. $P = \frac{2\pi R^3 \omega \sigma_0 k (T_m - T_0)}{3k(T_m - T_0) + R^2 \omega \sigma_0 e^{-\left(\frac{vR}{2a}\right)}}$

Fig. 7: Specific equations of the FSW power

Vision

A cloud has been set-up on www.aicamstir.com, onto which FSW operators can upload images and information on parameter settings during feasibility studies, prototyping, production rampup and series production. At a later stage they will get feedback about the weld quality and recommendations on optimising the parameters. In the final stage, such a system would be integrated into the FSW machine, and the machine would optimise the parameters itself within boundaries set by the operator.



Fig 8: FSW at different rotation speeds

The recommentations will be based on a variety of inputs such as rotation speed, welding speed, force and torque in combination with the results of an automated visual inspection via an optical camera or a suitable non-destructive testing method, e.g. by <u>automated shearography</u>, <u>long-range ultrasonic testing</u> (LRUT), <u>phased array ultrasonic testing</u> (PAUT) or <u>filmfee X-ray</u>. The data processing algorithms will make use of computational fluid dynamics (CFD), finite element analysis (FEA), analytical modelling and automatically updated look-up tables using machine learning and artificial intelligence.

References

- Mike Lewis and Simon D. Smith: <u>The Development of FSW Process Modelling for Use by Process Engineers</u>. In: The Minerals, Metals & Materials Society 2021: Friction Stir Welding and Processing XI. 17 Feb 2021.
- Matthew Champagne (University of New Orleans): <u>Investigation of 2195 and 2219 Post Weld Heat Treatments for Additive Friction Stir Lap Welds</u>. Pages 9, 20-21.
- Egoitz Aldanondo, Javier Vivas, Pedro Álvarez (LORTEK) and Iñaki Hurtado (MU-ENG): Effect of Tool Geometry and Welding Parameters on Friction Stir Welded Lap Joint Formation with AA2099-T83 and AA2060-T8E30 Aluminium Alloys. Metals 2020, 10(7), 872.
- Marc J. Brooker, A. J. M. (Ton) van Deudekom, Stephan W. Kallee and Peter D. Sketchley: <u>Applying Friction Stir Welding to the Ariane 5 Main Motor Thrust Frame</u>. In: European Space Agency Publications ESA SP; 468; 507-512: 2000. ISSN: 0379-6566.
- 5. Stephan W. Kallee, E. Dave Nicholas and Wayne M. Thomas: <u>Industrialisation of friction stir welding or aerospace structures</u>. Paper presented at Structures and Technologies Challenges for Future Launchers, Third European Conference, 11-14 December 2001, Strasbourg.
- Wayne M. Thomas, David G. Staines, Ian M. Norris and Ruis de Frias: <u>Friction Stir Welding –Tools and developments</u>. FSW seminar, IST-Porto, Portugal. 3 December 2002.