



DUDLEY KNOX LIBRARY  
NAVAL POSTGRADUATE SCHOOL  
MONTEREY CA 93943-5101





# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



## THEESIS

AN EXAMINATION OF THE PERFORMANCE  
OF A NATURAL TRUNCATION POINT AND  
ACCEPTANCE RULE FOR A CURTAILED WALD  
SEQUENTIAL SAMPLING PLAN WITH  
BERNOULLI PARAMETERS

by

Cameron J. Lewis  
September 1992

Thesis Advisor

Prof. Glenn F. Lindsay

Approved for public release; distribution is unlimited.



Unclassified

SECURITY CLASSIFICATION OF THIS PAGE

## REPORT DOCUMENTATION PAGE

1a. REPORT SECURITY CLASSIFICATION Unclassified		1b. RESTRICTIVE MARKINGS Unclassified	
2a. SECURITY CLASSIFICATION AUTHORITY		3. DISTRIBUTION/AVAILABILITY OF REPORT Approved for public release; distribution is unlimited.	
2b. DECLASSIFICATION/DOWNGRADING SCHEDULE			
4. PERFORMING ORGANIZATION REPORT NUMBER(S)		5. MONITORING ORGANIZATION REPORT NUMBER(S)	
6a. NAME OF PERFORMING ORGANIZATION Naval Postgraduate School		6b. OFFICE SYMBOL (If Applicable) OR	
6c. ADDRESS (city, state, and ZIP code)  Monterey, CA 93943-5000		7a. NAME OF MONITORING ORGANIZATION Naval Postgraduate School	
8a. NAME OF FUNDING/SPONSORING ORGANIZATION		8b. OFFICE SYMBOL (If Applicable)	
8c. ADDRESS (city, state, and ZIP code)		9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER	
		10. SOURCE OF FUNDING NUMBERS	
		PROGRAM ELEMENT NO.	PROJECT NO.
		TASK NO.	WORK UNIT ACCESSION NO.
11. TITLE (Include Security Classification) AN EXAMINATION OF THE PERFORMANCE OF A NATURAL TRUNCATION POINT AND ACCEPTANCE RULE FOR A CURTAILED WALD SEQUENTIAL SAMPLING PLAN WITH BERNoulli PARAMETERS (U)			
12. PERSONAL AUTHOR(S) Lewis, Cameron J,			
13a. TYPE OF REPORT Master's Thesis	13b. TIME COVERED FROM            TO		14. DATE OF REPORT (year, month, day) 1992 September
15. PAGE COUNT 128			
16. SUPPLEMENTARY NOTATION The views expressed in this thesis are those of the author and do not reflect the official policy or position of the Department of Defense or the U.S. Government.			
17. COSATI CODES		18. SUBJECT TERMS (continue on reverse if necessary and identify by block number)	
FIELD	GROUP	SUBGROUP	
19. ABSTRACT (Continue on reverse if necessary and identify by block number) This paper examines the performance of a proposed truncation and acceptance rule for the Wald Sequential Probability Ratio test for Bernoulli parameters and the rules influence on errors of the first and second kind as well as the average number of items sampled for inspection. The proposed truncation and acceptance rule suggest that there exists a natural truncation point for every Sequential Probability Ratio test such that the desired error probabilities are not exceeded or that one of the true errors is smaller than desired and the other will be exceeded by an insignificant amount. A computer program is used to simulate the sampling process and provide estimates of the true values of a plan's Operating Characteristic curve, its average sample number , as well as the probability of implementing the truncation and acceptance rule. Results suggest that truncation and rejection of a lot at the natural truncation point will maintain a plan's desired Operating Characteristic curve. The cases examined also suggest that any modifications to the natural truncation point truncation and acceptance rule may cause an unacceptable deviation from the desired Operating Characteristic curve. Finally, a linear equation was developed which provides an estimate of the upper limit on the probability of implementing a truncation and acceptance rule and that in most cases, this upper limit is less than 0.15.			
20. DISTRIBUTION/AVAILABILITY OF ABSTRACT <input checked="" type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS RPT. <input type="checkbox"/> DTIC USERS		21. ABSTRACT SECURITY CLASSIFICATION Unclassified	
22a. NAME OF RESPONSIBLE INDIVIDUAL G. F. Lindsay		22b. TELEPHONE (Include Area Code) (408) 646-2688	22c. OFFICE SYMBOL Code OR/RL

Approved for public release; distribution is unlimited.

AN EXAMINATION OF THE PERFORMANCE OF A NATURAL  
TRUNCATION POINT AND ACCEPTANCE RULE FOR A  
CURTAILED WALD SEQUENTIAL SAMPLING PLAN WITH  
BERNOULLI PARAMETERS

by

Cameron J. Lewis

Lieutenant, United States Coast Guard  
B.S., United States Coast Guard Academy, 1985

Submitted in partial fulfillment of the requirements  
for the degree of

MASTER OF SCIENCE IN OPERATIONS RESEARCH

from the

NAVAL POSTGRADUATE SCHOOL  
September 1992

## ABSTRACT

This paper examines the performance of a proposed truncation and acceptance rule for the Wald Sequential Probability Ratio test for Bernoulli parameters, and the rule's influence on errors of the first and second kind as well as the average number of items sampled for inspection. The proposed truncation and acceptance rule suggests that there exists a natural truncation point for every sequential probability ratio test such that the desired error probabilities are not exceeded or that one of the true errors is smaller than desired and the other will be exceeded by an insignificant amount. A computer program is used to simulate the sampling process and provide estimates of the true values of a plan's Operating Characteristic curve, its average sample number, as well as the probability of implementing the truncation and acceptance rule. Results suggest that truncation and rejection of a lot at the natural truncation point will maintain a plan's desired Operating Characteristic curve. The cases examined also suggest that any modification to the natural truncation point truncation and acceptance rule may cause an unacceptable deviation from the desired Operating Characteristic curve. Finally , a linear equation was developed which provides an estimate of the upper limit on the probability of implementing a truncation and acceptance rule, and that in most cases, this upper limit is less than 0.15.

## TABLE OF CONTENTS

I..	INTRODUCTION -----	1
II.	WALDS SEQUENTIAL PROBABILITY RATIO TEST -----	3
	A. BERNOUlli PARAMETERS AND ERRORS OF THE FIRST AND SECOND KIND -----	3
	B. SEQUENTIAL PROBABILITY RATIO -----	5
	C. SEQUENTIAL SAMPLING CHART -----	6
	D. THE OC CURVE FOR A SPR SAMPLING PLAN -----	9
	E. THE AVERAGE SAMPLE NUMBER CURVE -----	10
III.	NATURAL TRUNCATION POINT AND ACCEPTANCE RULE -	12
	A. THE NATURAL TRUNCATION POINT -----	12
	B. ACCEPTANCE RULES -----	16
IV.	EXPERIMENTAL PROCEDURES -----	19
	A. PARAMETER SPECIFICATION -----	19
	B. DEFINITION OF CONFORMING AND NONCONFORMING -	20
	C. COMPUTER SIMULATION -----	22
V.	RESULTS AND CONCLUSIONS -----	25
	A. NATURAL TRUNCATION POINT -----	25
	B. THE $(h_1 - m)$ ACCEPTANCE RULE -----	27
	C. THE EXTENDED $(h_1 - m)$ ACCEPTANCE RULE -----	29
	D. PROBABILITY OF IMPLEMENTING THE $(h_1-1)$ ACCEPTANCE RULE -----	30
	E. AREAS FOR FURTHER STUDY -----	31
	LIST OF REFERENCES -----	122
	INITIAL DISTRIBUTION LIST -----	123

## I. INTRODUCTION

Quality control has been a part of every industry for as long as there has been industry. Statistical quality control, on the other hand, is a relatively new thing with its greatest developments occurring in just the past 80 or so years [Ref. 1]. During those 80 years, the military played a major role in forcing industry to adopt statistical quality controls as a way of assuring that the quality of products they were buying met their specific requirements. A number of procedures were developed for sample inspection, most of which required inspectors to randomly draw a fixed number of sample items from a lot and inspect each one. If from these drawn items the number of defective or nonconforming items exceeded a specified critical value the lot was rejected , otherwise it was accepted.

During the late 1940's , Abraham Wald indicated that there could be a fairly large economy in the average number of items inspected , or the Average Sample Number (ASN) , sometimes as much as 50%, through the use of sequential statistics [Ref. 1]. However there is one shortfall of this sequential method and that is that the number of items sampled typically has a large variance and the maximum number of items that may need to be inspected before a decision can be made is unbounded. Wald suggested a way of truncating the process but warned that this could change the probabilities of the errors of the first and second kind [Ref. 6]. In recent years there have been a number of papers written about this problem , suggesting decision rules and methods for truncation. One of these papers , by Jurgen Petersen , suggests that there is a natural truncation point (NTP) for every

Sequential Probability Ratio (SPR) test at which a decision can be such that the desired errors will not be exceeded or that one of the true errors will be smaller than required and the other will be exceeded by an insignificant amount [Ref. 5].

This paper shall examine and evaluate the effects of using the NTP and decision rule on the Operating Characteristic (OC) and ASN of given SPR plans. It will also attempt to find the probability that in any given lot of items the truncation and acceptance rule may need to be implemented , that is , that decision to accept or reject will not have been made prior to the truncation point.

In order to evaluate the proposed truncation and acceptance rules, a computer program was written to simulate a SPR sampling process using these rules. This program provides estimates of the probability of acceptance , the ASN , and the probability that the rule will be implemented for a number of specified sampling plans. These computed values will then be compared to Wald's theoretical values for the same SPR plans when no truncation rule is used.

This study will proceed in the following way: Chapter II will describe the Wald Sequential Probability Ratio Test for a Bernoulli parameter. It will include a description of planned errors of the first and second kind, the testing procedure and sequential-sampling chart , the development of OC curves, and the calculation of the theoretical ASN . The third chapter will be a description of the NTP and decision rule that will be used and a brief explanation of how the NTP was obtained. Chapter IV will describe the simulation and the SPR plans that were evaluated and in the final chapter, the results of the simulation will be discussed and conclusions drawn.

## II. WALD'S SEQUENTIAL PROBABILITY RATIO TEST

The sequential method of quality control is a hypothesis test in which items are drawn from a lot sequentially and where one of three decisions can be made at any point during the test: (1) to accept the null hypothesis , (2) to reject the null hypothesis , (3) to continue the test by sampling more items. If either the first or second decision is made, the testing is terminated. If the third decision is made, the process is continued, selecting one item at a time until either the first or second decision is made. This testing method as well as definitions of the null hypothesis , Bernoulli parameters , and possible errors will be described in the following sections.

### A. BERNOULLI PARAMETERS AND ERRORS OF THE FIRST AND SECOND KIND

Like most quality control plans, Wald's SPR test requires that a number of parameters be specified. The first of these parameters is the Acceptable Quality Level or AQL. The AQL is the proportion of nonconforming items that may be found in a lot and still have the lot called acceptable. This acceptable proportion is designated as the Bernoulli parameter P1. P1 is usually specified by the consumer as well as a value for  $\alpha$  such that:

$$\Pr (\text{Rejecting a lot} \mid P_a = P1) = \alpha , \quad (1a)$$

or

$$\Pr(\text{Accepting a lot} \mid Pa = P_1) = 1 - \alpha , \quad (1b)$$

where  $Pa$  is the actual proportion of nonconforming items in the lot. These equations describe the Type I error associated with acceptance sampling. Stated in terms of a hypothesis test, the null hypothesis is that the actual proportion nonconforming is  $P_1$ , and  $\alpha$  is the significance level for the test.

The value of  $\alpha$  is often known as the "producers risk" for it is the chance that the producer takes of having a lot consisting of satisfactory items rejected by the test. The consumer also has a risk associated with acceptance sampling. This consumer's risk is designated as  $\beta$  such that the

$$\Pr(\text{Accepting a lot} \mid Pa = P_2) = \beta , \quad (2)$$

where  $P_2$  is greater than  $P_1$  and is a value of the lot fraction nonconforming that the consumer is willing to take a  $\beta(100)\%$  chance of accepting. The consumer's risk equation describes a value of a Type II error associated with acceptance sampling.

The hypothesis test associated with acceptance sampling is

$$H_0: Pa = P_1$$

$$H_a: Pa > P_1$$

with  $\alpha$ ,  $\beta$ ,  $P_1$ , and  $P_2$  specified as discussed above. The values of  $P_2$  and  $\beta$  define a point on the test's Operating Characteristic (OC) curve. Note that the hypothesis test is only a one-sided test for it would make little sense to test for  $Pa$  being less than the AQL. The typical values for  $\alpha$  and  $\beta$  are 0.05 and 0.10 respectively, and when

used in Equations (1b) and (2) , define two points on the test's OC curve.

## B. SEQUENTIAL PROBABILITY RATIO

In the Wald Sequential plan, items are drawn randomly from a lot one item at a time and inspected. After the  $n$ th item is inspected with  $c$  nonconforming items having been found, the sequential probability ratio is computed, compared against two test values A and B, and a decision is made as follows:

$$SPR = \frac{\Pr(\text{reaching } n, c / P_a = P_2)}{\Pr(\text{reaching } n, c / P_a = P_1)} = \left[ \frac{P_2(1-P_1)}{P_1(1-P_2)} \right]^c * \left[ \frac{1-P_2}{1-P_1} \right]^n, \quad (3)$$

and if  $SPR \geq A$  then stop sampling and reject  $H_0$ ,  
if  $SPR \leq B$  then stop sampling and accept  $H_0$ , and  
if  $B \leq SPR \leq A$  then continue sampling .

The constants A and B are derived so that the test will meet the requirements of Equations (1) and (2) . An upper limit for the constant A is found to be the ratio of the probability of rejecting the null hypothesis  $H_0$  when the alternative hypothesis  $H_a$  is true divided by the probability of rejecting  $H_0$  when  $H_0$  is true, yielding

$$A \leq \frac{1 - \beta}{\alpha}. \quad (4)$$

A lower limit for B is found to be the ratio of the probability that  $H_0$  is accepted given that  $H_a$  is true divided by the probability that  $H_0$  is accepted given that  $H_0$  is

true or written as an inequality:

$$B \geq \frac{\beta}{1 - \alpha} . \quad (5)$$

Wald showed that when the inequalities in Equations (4) and (5) are replaced by equalities, we have conservative values for A and B. [Ref. 6]

### C. SEQUENTIAL SAMPLING CHART

Wald then greatly simplified the SPR test by removing the requirement of computing the SPR every time a sample is taken. He removed this requirement by developing a chart on which an inspector needed only to plot a point, where the abscissa is the total number of items inspected up to that time and the ordinate is the total number of those items which were found to be nonconforming [Ref. 1]. If the plotted point stays between the two parallel lines on the sampling chart, no decision is made about the lot and the inspection is continued. If a point is plotted and it falls on or above the upper parallel line the inspection is terminated and the lot rejected, but if a point is plotted and it falls on or below the lower of the two parallel lines, the inspection is terminated and the lot is accepted. Figure 1 shows what a typical

sequential sampling chart may look like and how the points are plotted until a decision can be made. In Figure I , the decision would be made is to reject the lot.

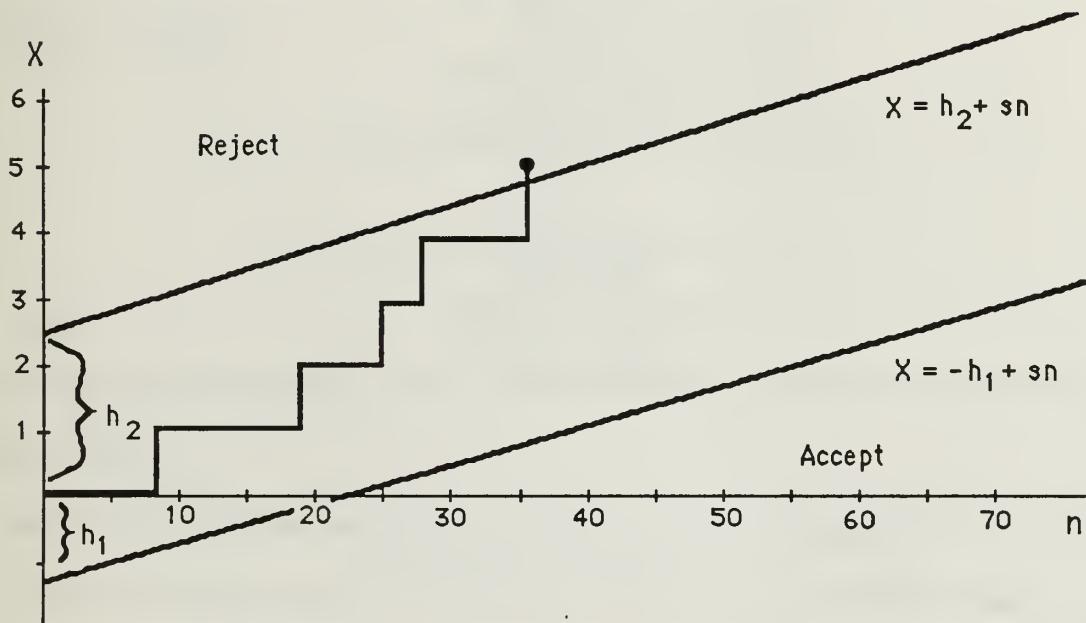


Figure 1 -AN EXAMPLE OF A SEQUENTIAL SAMPLING CHART

The values of  $h_1$  ,  $h_2$  , and  $s$  are arbitrary labels for constants which can be derived by setting the values for A and B equal to the right hand side of Equation (3) and then solving for c. When the value for A is set equal to the right hand side of Equation (3) and c is solved for, the result takes the form of  $c= -h_1+sn$  . When B is set equal to the right hand side of Equation (3) and c is solved for, the result takes the form of  $c=h_2+sn$  where [Ref. 1]

$$h_1 = \frac{\ln \left[ \frac{1-\alpha}{\beta} \right]}{\ln \left[ \frac{P_2(1-P_1)}{P_1(1-P_2)} \right]} , \quad (6)$$

$$h_2 = \frac{\ln \left[ \frac{1-\beta}{\alpha} \right]}{\ln \left[ \frac{P_2(1-P_1)}{P_1(1-P_2)} \right]} , \quad \text{and} \quad (7)$$

$$s = \frac{\ln \left[ \frac{(1-P_1)}{(1-P_2)} \right]}{\ln \left[ \frac{P_2(1-P_1)}{P_1(1-P_2)} \right]} . \quad (8)$$

There are a number of items to note about the sequential sampling chart. The first item to note is that there is a minimum number of samples that need to be taken before a decision can be made. The second item worthy of being pointed out is that not all values of  $n$  represent an opportunity for accepting or rejecting  $H_0$ . Acceptance can occur only at those values of  $n$  where  $-h_1+s(n-1) < X \leq -h_1+s_n$ , where both  $X$  and  $n$  are non-negative integers. The values of  $n$  that meet this condition will be called acceptance points. The final item worth noting is that since the acceptance and rejection lines are parallel to each other, the maximum number of items that need to be sampled before a decision can be made is unbounded. It is this difficulty with sequential sampling that led to the truncation and acceptance rule that will be discussed in the next chapter.

## D. THE OC CURVE FOR A SPR SAMPLING PLAN

The Operating Characteristic (OC) curve for SPR sampling plan is a curve that shows the probability of accepting a lot of items given the actual proportion of nonconforming items in that lot ( $P_a$ ). This OC curve should reflect the desired parameters such that

$$\Pr(\text{accepting } H_0 \mid P_a = P_1) = 1 - \alpha ,$$

and

$$\Pr(\text{accepting } H_0 \mid P_a = P_2) = \beta$$

are two points on the plan's curve. It also has been shown that a third point on the curve is [Ref. 1]

$$\Pr(\text{accepting } H_0 / P_a = s) = \frac{h_2}{h_1 + h_2} .$$

Other points on the OC curve can be obtained from the parametric equations

$$P_a = \frac{1 - \left[ \frac{1 - P_2}{1 - P_1} \right]^\theta}{\left[ \frac{P_2}{P_1} \right]^\theta - \left[ \frac{1 - P_2}{1 - P_1} \right]^\theta} , \quad (9)$$

$$\text{and } \Pr(\text{accept } H_0 / P_a) = \frac{\left[ \frac{1 - \beta}{\alpha} \right]^\theta - 1}{\left[ \frac{1 - \beta}{\alpha} \right]^\theta - \left[ \frac{\beta}{1 - \alpha} \right]^\theta} , \quad (10)$$

where  $\theta$  is an arbitrary value which ranges from negative infinity to infinity such

that for  $\epsilon = 1$ , we have  $P_a = P_1$ , for  $\epsilon = -1$  we have  $P_a = P_2$  and for  $\epsilon = 0$ ,  $P_a = s$ . An example of an Operating Characteristic curve is shown in Figure 2.

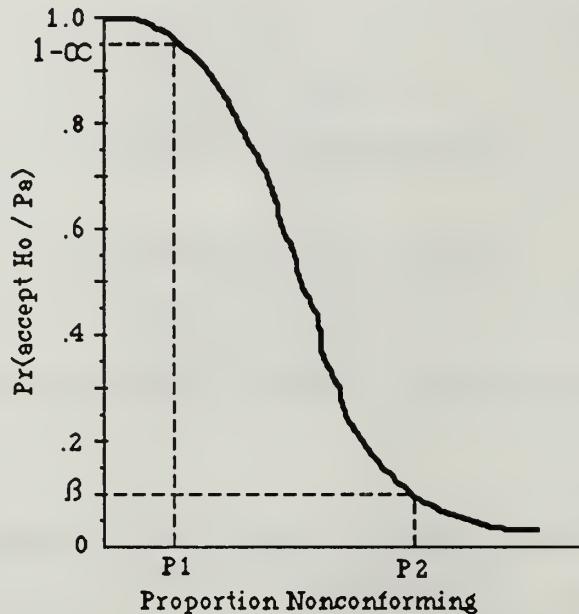


Figure 2 - AN OPERATING CHARACTERISTIC CURVE

#### E. THE AVERAGE SAMPLE NUMBER (ASN) CURVE

As discussed earlier in this paper, the number of items that will be required to be sampled before a decision can be made is a random variable, but Wald showed that it is possible to compute its expected value as a function of the plan's parameters and  $P_a$ . The equation for computing the ASN is as follows [Ref 1]:

$$ASN(P_a) = \frac{\Pr(\text{accept} | P_a) h_1 - (1 - \Pr(\text{accept} | P_a)) h_2}{s - P_a} . \quad (11)$$

Equation (11) can be simplified at specific values of  $P_a$  such that  $ASN(P_a = 0) = h_1/s$  ,

$ASN(P_a=1) = h_2/(1-s)$  , and  $ASN(P_a=s) = h_1 h_2 / s(1-s)$ .

There are several items that should be noted about the ASN for any given SPR plan. The first of these is that the maximum ASN for any given plan will occur around the point where  $P_a = s$  and it is possible that this ASN will be larger than the sample numbers for some other types of sampling plans [Ref. 1]. Second is that the larger the difference between  $P_1$  and  $P_2$  , the smaller the ASN. A final observation is that the greater the values of  $\alpha$  and  $\beta$  , the smaller the ASN. Figure 3 shows what a typical ASN curve might look like.

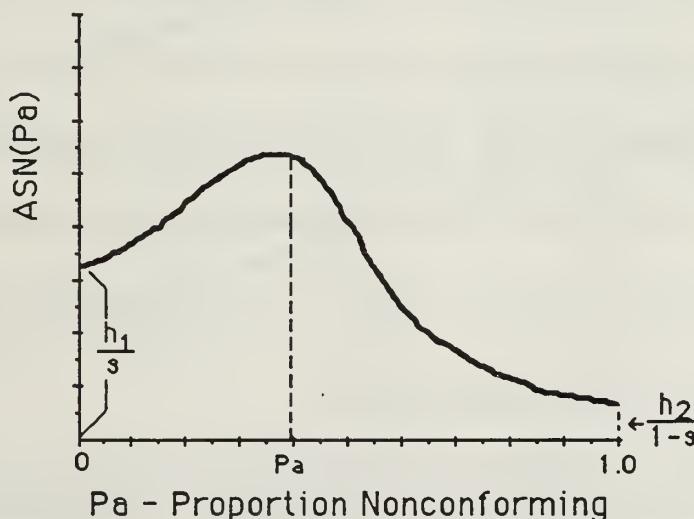


Figure 3 - AN ASN CURVE

### III. THE NATURAL TRUNCATION POINT AND ACCEPTANCE RULE

It has been shown that the probability that a sequential test will eventually terminate is 1.0, but we have also seen that the maximum value for  $n$  at which this termination will occur is unbounded [Ref. 6 , p. 157-158]. It is because this maximum value is unbounded that we may find it necessary to set a definite upper limit ,  $n_0$  , for the number of items to be inspected. It is at this truncation point that the test will be terminated and a decision on whether to accept or reject  $H_0$  will be made. Wald warns that if we truncated the sequential process at the  $n_0$ th trial, we will be changing the probabilities of errors of the first and second kind by some unknown amount, but as  $n_0$  becomes larger, the effect of this change will be smaller [Ref. 6].

In his paper, Petersen suggested that for every SPR plan there exists a natural truncation point (NTP) at which the test may be stopped and neither of the two error probabilities will be exceeded, or that the error of the second kind will be insignificantly greater than  $\beta$  [Ref. 5 , p 22]. In the following sections we will give a brief description of the NTP and the decision rules that will be used when it is reached.

#### A. THE NATURAL TRUNCATION POINT

We have seen that not every point on the sequential sampling chart represents an opportunity to accept the null hypothesis. The only points at which the null hypothesis can be accepted are the values of  $n$  at which the equation  $(-h_1 + s_n)$  is

equal to or has just become greater than a value of  $X$ , which is the number of nonconforming items that have been found in the sample of size  $n$ . These special values of sample number  $n$  are called acceptance points and are designated as  $A_0, A_1, A_2, \dots$ , where at each sample number  $A_i$  there is an unconditional probability that the test will be terminated given that the null hypothesis is true [Ref. 5].

A similar observation can be made about the opportunity to reject the null hypothesis. There are a number of points at which the number of nonconforming items needed to reject the null hypothesis increases by one. Analogous to above, these special values of sample number  $n$  are called rejection points. While these rejection points are interesting to note, we will see that they do not play a role in identifying the natural truncation points. Figure 4 shows the location of some acceptance and rejection points on a typical SPR chart.

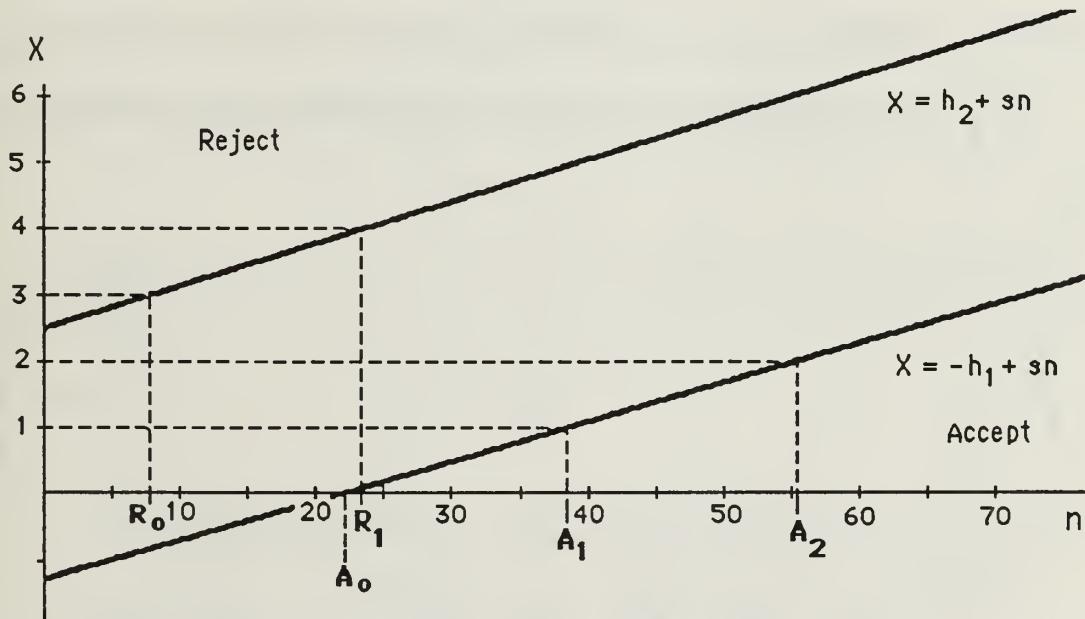


Figure 4 - SEQUENTIAL PROBABILITY RATION CHART  
WITH ACCEPTANCE AND REJECTION POINTS HIGHLIGHTED

If there is no truncation, the sum of the acceptance probabilities for all the values of  $A_i$  up to and including  $n$  is the probability that  $H_0$  will be accepted when

at most  $n$  samples are drawn. Given that  $n < A_{i+1}$ , the following statements can be made about the acceptance probability when at most  $n$  samples have been drawn [Ref. 5 , p 16]:

- (i) Since  $-h_1 < 0$  , the  $\Pr(\text{accept } H_0 \mid n = 0) = 0$ .
- (ii) As  $n$  increases in size, the  $\Pr(\text{accept } H_0 \mid n)$  never decreases , and only increases at acceptance points.
- (iii) For all sample numbers between  $A_i$  and  $A_{i+1}$  , the  $\Pr(\text{accept } H_0 \mid n)$  is a constant and is equal to the  $\Pr(\text{accept } H_0 \mid n = A_i)$ .

Figure 4 shows how the acceptance probability accumulates for an arbitrary sampling plan when the null hypothesis is true , that is  $P_a = P_1$  [Ref. 5].

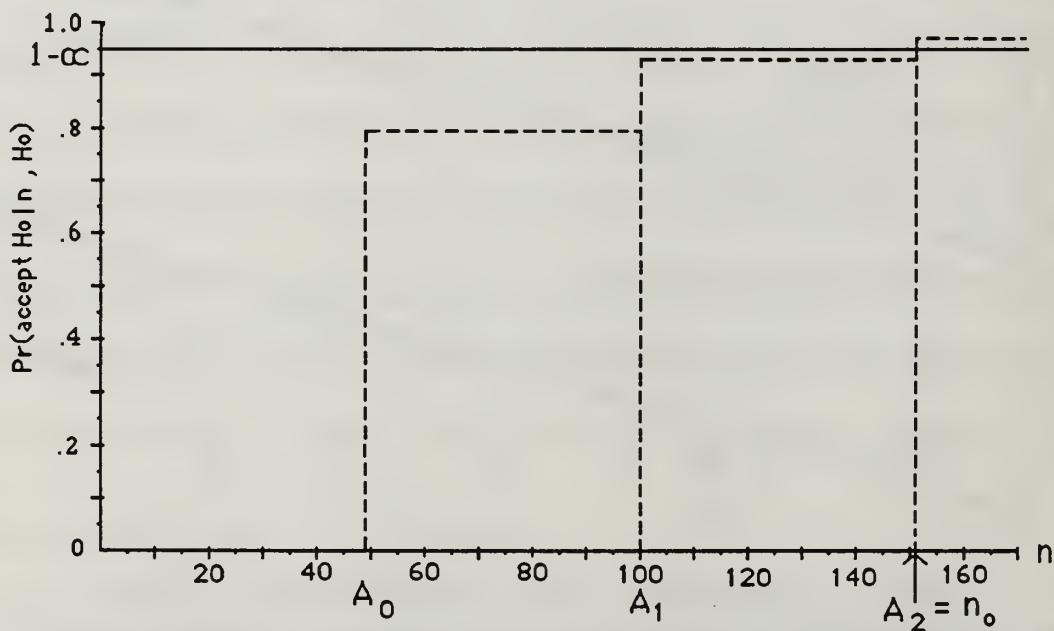


Figure 4 - ACCUMULATED ACCEPTANCE PROBABILITY

In the above example, the acceptance point  $A_2$  is the first point where the probability of acceptance exceeds the  $(1- \alpha)$  requirement. It is this point that is designated as

this plan's natural truncation point ,  $n_0$ .

At  $n_0$  ,  $\alpha$  can be considered as an upper bound for the probability of a Type I error. It is also possible to compute an upper bound for the probability of an error of the second kind as  $n$  approaches  $n_0$ . It has been shown that as  $n$  increases , the upper limit for the probability of a Type II error decreases , approaching  $\beta$  from above [Ref. 6, p 62-64].

It is also possible to show that the sum of the acceptance probabilities, when the alternate hypothesis is true , approaches  $\beta$  as  $n$  increases . In addition, it has been suggested that the true probability of a Type II error will be at most, insignificantly greater than the planned error when  $n$  is equal to the natural truncation point [Ref. 5]. Figure 5 shows how the acceptance probability may accumulate for an arbitrary sampling plan when the alternate hypothesis is true , that is  $P_a = P_2$  .

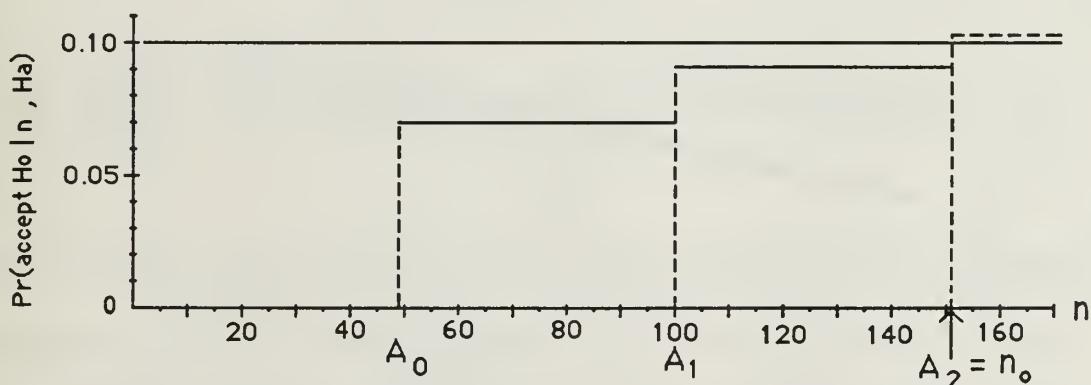


Figure 5 - ACCUMULATED ACCEPTANCE PROBABILITY  
WHEN THE ALTERNATE HYPOTHESIS IS TRUE

If the true probability of a Type II error does not significantly exceed  $\beta$  for any sample number  $n$ , it is then not necessary to specify a special truncation point to control it.

## B. ACCEPTANCE RULES

Once the natural truncation point is reached , a decision must be made as whether to accept or reject the null hypothesis. We will examine three related rules starting with the simplest and working toward slightly more complicated ones. The simplest and most conservative rule is that if no decision has been made after the last item has been sampled the null hypothesis should be rejected. By rejecting  $H_0$ , we insure that the true probability of errors of the first and second kind are as close to the desired values as possible [Ref. 6].

The second decision rule is known as the  $(h_1-m)$  rule. This rule divides the region between the upper rejection and lower acceptance lines into two parts. The line which makes this division is the line  $-(h_1-m)+sn$  where  $m$  is a positive integer such that  $0 \leq m \leq ( h_2 - (-h_1))$ . Figure 6 shows how the region is divided when  $m=2$ .

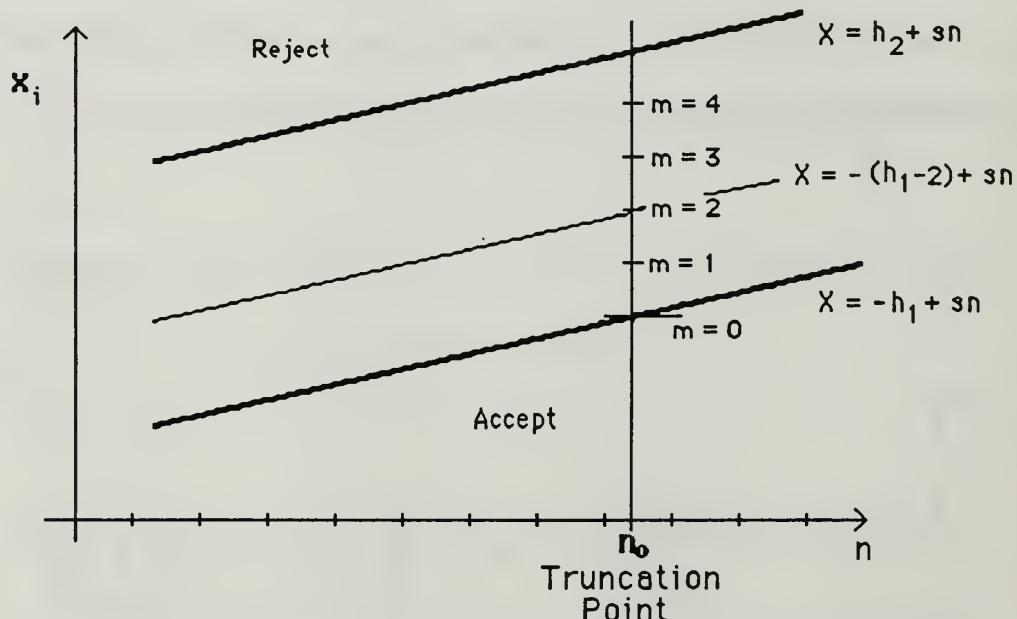


Figure 6 - AN EXAMPLE OF DIVIDING THE SAMPLING CHART  
USING THE  $(h_1 - m)$  ACCEPTANCE RULE.

Under this rule, if the natural truncation point is reached before a decision has been made, the null hypothesis is rejected only if the plot of the number of

nonconforming items found falls on or above the  $-(h_1-m)+sn$  dividing line. If the number of nonconforming items is less than  $-(h_1-m)+sn$ , then  $H_0$  is accepted.

The final rule that will be examined is an extension of the  $(h_1-m)$  acceptance rule and attempts to reduce the ASN of a plan by finding earlier truncation points..

Under this rule, one of the two desired errors is fixed and the other is allowed to vary in an attempt to lower the value of the truncation point. Petersen describes a sample number  $n_i^*$  which is strictly less than the NTP but at which we are assured that the probability of a Type I error will not exceed  $\alpha$ . He also describes  $n_i^{**}$  which is the smallest sample number for which  $\beta$  is not exceeded. These sample numbers can be found using the following equations:

$$n_i^* = \text{int} \left[ \frac{\log[1-\alpha - \Pr(\text{accept } \oplus A_i | H_0)] + A_i \log(1-P_1) - \log[\Pr(X(A_i) = i+m)]}{\log(1-P_1)} \right] \quad (11)$$

$$n_i^{**} = \text{int} \left[ A_i + \frac{\log[\beta - \Pr(\text{accept } \oplus A_i | H_0)] - \log[\Pr(X(A_i) = i+m)]}{\log(1-P_1)} + 1 \right] \quad (12)$$

where  $\Pr(X(A_i) = i+m)$  is the probability that the number of nonconforming items at acceptance point  $A_i$  will be less then or equal to  $i+m$ , given that the null hypothesis is true in Equation (11) and that the alternate hypothesis is true in Equation (12). [Ref. 5]

While the derivation of Equations (11) and (12) is fairly complicated and will not be discussed here, there are several items that should be noted about using the

extended (h<sub>1</sub>-m) acceptance rule. The first item to note is that it is possible that  $n_i^*$  and  $n_i^{**}$  may not exist for every given sampling plan. Second is that if the new truncation points do exist, once  $n_i^*$  or  $n_i^{**}$  is reached, decisions are made in the same way as the non-extended (h<sub>1</sub>-m) rule, and finally while this plan fixes one error at a desired value , the amount by which the alternate error will vary from its desired value is unknown and possibly can be quite large.

Theoretically the above truncation rules should reduce the ASN of an given plan by truncating a sampling process at a specific point while maintaining the desired operating characteristic. The following section will describe the experimental procedures and computer simulation used to test the validity of the claims made above.

#### IV. EXPERIMENTAL PROCEDURES

In any sequential sampling procedure, there are a number of steps that must be taken before the actual sampling and testing of items begin. First, the plan's parameters must be specified. Second, the definition of conforming and nonconforming must be clarified, and finally a procedure for random sampling and testing must be determined. It is only after these three steps have been accomplished that the actual testing may begin and decisions as whether to accept or reject lots may be made. The following section will discuss these three steps in detail as well as describe the computer simulation that was used to simulate the sampling process.

##### A. PARAMETER SPECIFICATION

Before the beginning of any sampling process, the parameters  $\alpha$ ,  $\beta$ ,  $P_1$ , and  $P_2$  must be specified. These values are used in Equations (6), (7), and (8) to compute the values of  $h_1$ ,  $h_2$ , and  $s$  which in turn are used to determine the acceptance and rejection zones on the sequential sampling chart. For the work presented in this paper,  $\alpha$  and  $\beta$  were set at 0.05 and 0.10 respectively and remained constant throughout the test. These values were selected because they are typical values used in quality control. For the parameters  $P_1$  and  $P_2$ , twenty six pairs of  $P_1$  and  $P_2$  values were arbitrarily selected. The values for  $P_1$  and  $P_2$  were selected to provide a good range for testing the truncation points and stopping rules. For ease of testing, the parameters were divided into four "Plan Sets" according to the four values of  $P_1$  that were used. Table I provides a list of the parameter pairs used as well as their

natural truncation point and extended rule truncation points  $n_i^*$ , and  $n_i^{**}$ . The truncation points for the extended rule were computed using the  $(h_1-1)$  extended rule for reasons that will be discussed later.

Table I - PARAMETER VALUES USED IN THE SIMULATION  
AND THEIR TRUNCATION POINTS.

	P1	P2	NTP	$n_i^*$	$n_i^{**}$		P1	P2	NTP	$n_i^*$	$n_i^{**}$
Plan Set 1	0.005	0.01	4605	4346	4352	Plan Set 3	0.015	0.03	1523	#	#
		0.02	702	530	579			0.04	636	#	527
		0.03	375	163	218			0.05	371	#	280
		0.04	182	71	116			0.06	233	178	186
		0.05	151	76	96			0.07	179	138	140
		0.06	129	83	83		0.020	0.03	4192	#	#
		0.07	74	71	71			0.04	1148	#	#
Plan Set 2	0.010	0.03	714	#	#	Plan Set 4		0.05	560	#	471
		0.04	350	#	281			0.06	356	273	277
		0.05	215	138	164			0.07	243	209	211
		0.06	151	82	106			0.08	174	134	140
		0.07	133	84	91			0.09	134	102	106
		0.08	90	36	57			0.10	107	79	88
		* Does not exist under $(h_1-1)$ rule									

## B. DEFINITION OF CONFORMING AND NONCONFORMING

In quality control an item may be considered nonconforming if a specific measurement does not fall within required parameters. These parameters usually fall into one of two types of tests , one-way or two-way tests. A test that is one-way requires the item being inspected to meet some minimum or maximum limit. As long as this maximum or minimum is met, the item is considered good or

acceptable. For example, if a chain company may require a quarter-inch chain to have a minimum breaking strength of two thousand pounds, that is what they will test for. They may not care that the actual breaking strength is twenty-six hundred pounds , all they care is that the chains meet the minimum requirements.

A two-way test has two parameters that must be met, a minimum and a maximum. The most common two-way test measures to see if a specific characteristic of an item falls between these two parameters. If the measurement falls between the minimum and maximum , the item is considered acceptable, otherwise it is rejected as unacceptable . An example of a two-way test may be a potato chip company measuring to see if a twelve ounce bag of chips is actually being filled with 12 oz. of chips. If a bag has too few ounces of chips in it the law may not allow them to call it a 12 oz. bag. If a bag has much more then 12 oz. in it , the company may be losing money. Not wanting to break the law or lose money, the company specifies a minimum and maximum weight for the number of ounces of chips that a bag should have. The company then tests bags of chips one at a time. If enough bags of chips meet the specified requirements, the machine that fill the bags is working properly. On the other hand if enough bags of chips do not meet the requirements, the company may decide that the filling machine requires adjustments or repairs.

While the above two tests are not the only type of examinations used in quality control, they are probably the most common. For the purpose of this paper, the two-way test will be used in the examination of the proposed truncation rules. In a computer simulation, a lot of 5000 numbers will be created from a normal

distribution. Each number represents some attribute of the item being tested. From this lot of numbers, one item at a time will be drawn , without replacement , and compared to a set of parameters such that the probability of the items falling outside these parameters is a fixed and known. If the item falls within the specific parameters it is classified as acceptable or conforming, otherwise it is classified as a nonconforming item. Inspection continues one item at a time until a decision can be made. Details of the simulation will be discussed in the following section.

### C. COMPUTER SIMULATION

A computer program was written to simulate the Wald SPR sampling process and compute the ASN and its standard deviation , the Operating Characteristic, and number of times the stopping rule was utilized for each SPR plan. The computer simulation was written in VS FORTRAN 77 and utilized the AMDAHL 5990-500 Dual-Processor mainframe computer system at the Naval Postgraduate School (NPS) Computer Center during the period of April to September 1992. The simulation also utilized the NPS Random Number Package with double precision written by P.A. Lewis and L. Uribe.

The input variables for the simulation consisted of five parameters denoted by  $P_1$  ,  $P_2$  ,  $Pa$  ,  $NTP$  , and  $Za$ . With the exception of  $Za$ , all the parameters are the same as the ones discussed earlier in this paper. The parameter  $Za$  is the measurement parameter used in the two-way test discussed above such that the probability that an items measurement falls outside  $-Za$  and  $Za$  is  $Pa$ .

As discussed before, twenty-six pairs of parameters  $P_1$  and  $P_2$  were used in the

simulation and were divided into four "Plan Sets" according to the four different values of P1 that were used. Each pair of parameters P1 and P2 within a Plan Set is called a plan since each different pair of P1 and P2 will have a different OC curve. For each plan , six to eighteen OC points, designated by Pa, were used to develop each Plan's OC and ASN curves. Table II gives an example of two plans and the values for Pa that were used in the simulation.

Table II - EXAMPLE OF THE PARAMETERS FROM PLAN SET 1  
PLANS C AND D

Plan C			Plan D		
P1	P2	Pa	P1	P2	Pa
0.005	0.03	0.005	0.005	0.04	0.005
		0.007			0.007
		0.010			0.010
		0.013			0.013
		0.016			0.016
		0.019			0.019
		0.022			0.022
		0.025			0.025
		0.028			0.028
		0.030			0.031
					0.034
					0.037
					0.040

A lot of 5000 random numbers was created from a normal distribution with a mean of zero and variance of one for each value of Pa. Each number represented an arbitrary measurement of some attribute of the items being tested. From one lot at a time, items were randomly selected one item at a time without replacement and tested against the parameter Za. This selection process continued until a decision as

whether to accept or reject the lot could be made. The process was then repeated 5000 times so that the final estimate of each OC point was the result of 5000 lots of 5000 items going through the SPR process.

One of the sets of rules that should be kept in mind when conducting any random sampling process is that the method by which items are selected should ensure that each member of a lot has an equal chance of being selected. It should also avoid using any method of selection that associates the selection of the item with the classification of the item being selected. Since the items in the lots came from a normal distribution a sampling order was created for each lot from a uniform[0,5000] distribution. By selecting items according to a sampling order from a different distribution, we were assured that the sampling process was as close to random as possible.

## V. RESULTS AND CONCLUSIONS

When a Wald SPR sampling process is truncated its operating characteristics will vary with the location of the truncation point and the type of acceptance rule used. As the location of the truncation point becomes larger, the true values of the OC curve will approach the values of the OC curve of the nontruncated sampling plan. For this paper, the values obtained from the simulation for the OC and ASN curves will be known as the true values for a plan. These values will be compared to the values of the nontruncated SPR sampling process obtained from Equations (10) and (11). The values for the OC curve and ASN obtained from Equations (10) and (11) will be known as a plan's theoretical values.

### A. NATURAL TRUNCATION POINT

As discussed earlier in this paper, the first truncation and acceptance rule examined was an automatic rejection of a lot if the sampling process reaches the NTP. The normal approximation for the two-sided test for the Difference of Two Proportions (DTP), at a 0.05 level of significance, was used to compare the theoretical and true values of the operating characteristic at each value of  $P_a$  such that:

$$H_0: P(\text{accept} \mid P_a)_{\text{true}} = P(\text{accept} \mid P_a)_{\text{theo.}}$$

$$H_a: P(\text{accept} \mid P_a)_{\text{true}} \neq P(\text{accept} \mid P_a)_{\text{theo.}}$$

According to test statistics, there appears to be no difference between the theoretical

and true values for any of the plans tested. In other words, for plans with parameter values in the range of those studied here, the NTP stopping rule provides a point at which the SPR sampling process can be truncated while maintaining the errors of the first and second kind at their desired values. The results of the above testing can be found in Tables III and IV of Appendix B under the heading  $m=0$ .

The true ASN and theoretical ASN at each value of  $Pa$  were also compared but this time a one-sided Paired Difference T test (PDT), at a 0.05 level of significance, was used. The associated hypothesis test was

$$H_0: ASN_{true} = ASN_{theo.}$$

$$H_a: ASN_{true} < ASN_{theo.}$$

which when rewritten as a PDT is

$$H_0: (ASN_{true} - ASN_{theo.}) = 0$$

$$H_a: (ASN_{true} - ASN_{theo.}) < 0.$$

The paired difference statistic has a student's t distribution with  $n-1$  degrees of freedom. In the above testing,  $n=5000$  and therefore the t statistic is essentially normal. Results of the tests using the normal distribution can be found in Tables VI, IX, XII, and XV of Appendix B and showed that in almost all of the plans, the true ASN did not show any statistical savings over the theoretical values.

There are two items worthy of noting when discussing the two comparison tests used above. The first item is that the use of a two-sided test is not entirely appropriate for the DTP test because at different areas of the OC curve the alternate

hypothesis ,  $P(\text{accept} \mid Pa)_{\text{true}} \neq P(\text{accept} \mid Pa)_{\text{theo.}}$ , may be desirable. For example, it may be desirable for the  $P(\text{accept} \mid Pa \text{ is near } P1)_{\text{true}} > P(\text{accept} \mid Pa \text{ is near } P1)_{\text{theo.}}$ . or  $P(\text{accept} \mid Pa \text{ is near } P2)_{\text{true}} < P(\text{accept} \mid Pa \text{ is near } P2)_{\text{theo.}}$  because then the probability of either type of error would be less than required and therefore better. The second item worthy of noting is that while the differences between the true and theoretical values of a number may be statistically significant, the numerical differences may often be fairly small. When the sample size being used in the test is large, in this case 5000 , a small difference between numbers may often lead to rejection of the null hypothesis. It is therefore important to look at the actual numerical differences as well as the Z values obtained from the test statistics. These items will also hold true in the following sections.

## B. THE $(h_1 - m)$ ACCEPTANCE RULE

The second truncation and acceptance rule examined was the  $(h_1 - m)$  acceptance rule. As discussed before, if no decision has been made prior to reaching the NTP the lot is accepted if the number of nonconforming items found up to that point is less than  $-(h_1 - m) + sn$  , where n is the NTP. If the number of nonconforming items found up to that point is equal to or greater than  $-(h_1 - m)+sn$  the lot is rejected. For this set of rules, the simulation was run using the same lots and sampling order used to test the first rule but was with  $m=1$  ,  $m=2$  ,  $m=3$  , and then  $m=4$ . Using the same lots and sampling order allowed direct comparison between runs with different values of m.

The results from this set of tests can also be found in Tables XVII through XX of Appendix B and show that as  $m$  increases in value, the probability of a Type I error decreases at a decreasing rate. That is for every increase in  $m$ , the decrease in the probability of a Type I error becomes smaller and smaller and approaches zero as  $m$  approaches ( $h_2 - (-h_1)$ ). On the other hand, as  $m$  increases in value, the probability of a Type II error increases. Like the decreases in the probability of a Type I error, the increases in the probability of a Type II error becomes smaller as  $m$  increases but do not approach zero as quickly as alpha. In other words, every increase in the probability of a Type II error is not necessarily accompanied by an equal decrease in the probability of a Type I error.

For all values of  $m > 0$  the  $\Pr(\text{accept } H_0 \mid P_a = P_2)$  was greater than  $\beta$ . The differences between the true values of the probability of a Type II error and their desired values are statistically significant in all the plans tested but as discussed above, the actual numerical differences are not always that great. It is therefore necessary to make a decision as to how much you may be willing to let the probability of a Type II error vary from its desired value of  $\beta$  in order to obtain some improvement in the probability of a Type I error. Since all the true values along a given the OC curve varied similarly when  $m$  is changed, the 95% confidence interval (CI) for the probability of a Type II error and a number of other OC points was computed for the different values of  $m$ . The computed CI for the probability of a Type II error at  $m=1$  was  $\{0.106, 0.118\}$  with a maximum value of 0.128. The CI for the probability of a Type II error at  $m=2$  was  $\{0.12, 0.137\}$  with a maximum value of 0.148. Since the true values for  $\beta$  and the other OC points using  $m=1$  are generally

very close to the theoretical values, the  $(h_1 - 1)$  truncation and acceptance rule is recognized as a reasonable truncation and acceptance rule for a Wald SPR sampling process. Unlike the  $m=1$  rule , the deviations of the theoretical OC values from the true OC values for the rules using  $m \geq 2$  are considered too great and therefore the  $(h_1 - m)$  truncation and acceptance rule for  $m \geq 2$  is rejected as reasonable truncation and acceptance rule. Results of testing can be found in Tables V through XVI of Appendix B.

### C. THE EXTENDED $(h_1 - m)$ ACCEPTANCE RULE

As discussed earlier , the extended  $(h_1 - m)$  acceptance rule attempts to reduce the ASN of a plan by finding truncation points which are strictly less then the NTP. To do this, only one of the true errors will be guaranteed to equal the desired value.

The point  $n_i^*$  holds alpha constant, for it is smallest sample number at which the probability of a Type I error is equal to alpha. The point  $n_i^{**}$  holds beta constant for it is the smallest sample number at which the probability of a Type II error is equal to beta. Since only the  $(h_1 - 1)$  acceptance rule is being recognized as an acceptable truncation and acceptance rule , the values for  $n_i^*$  and  $n_i^{**}$  were computed only for the extended  $(h_1 - 1)$  acceptance rule.

The performance of the extended  $(h_1 - 1)$  acceptance rule in most test cases was poor. While it did a good job holding one error close to the required value , the

other operating characteristics quickly deviated from their theoretical values so that by the time the alternate error was reached, its true value was usually more than twice its desired value. In addition, for most cases the extended acceptance rule provided only a small savings in ASN , and for a small number of points, the ASN for the nonextended acceptance rule was actually smaller. Results of the testing can be found in Tables XVII through XX of Appendix B.

Overall, the performance of the extended  $(h_1 - 1)$  acceptance rule was poor and the rule is not recommended as a truncation and acceptance rule with one possible exception. If the difference between  $P_1$  and  $P_2$  is large and it is known that  $P_a$  is very close to  $P_1$ , then using the extended acceptance rule may provide some savings in ASN. In all other cases, the nonextended  $m=0$  or  $m=1$  rule is recommended.

#### D. PROBABILITY OF IMPLEMENTING $(h_1 - 1)$ ACCEPTANCE RULE

The probability that a truncation and acceptance rule will need to be implemented depends greatly on the true value of the actual proportion of noncomforming items in the lot,  $P_a$  , which is itself a unknown. Even though the actual probability of implementing a truncation and acceptance rule is unknown, it is possible to get a rough upper limit for it by using some known parameters such as  $P_1$  ,  $P_2$  , and  $s$ .

We have seen that as the difference between  $P_1$  and  $P_2$  increases, the ASN of a plan decreases and that the maximum value for the ASN of a plan occurs when  $P_a$  is approximately equal to  $s$ . It is when  $P_a$  is approximately equal to  $s$  that we have the greatest probability of reaching a truncation point and therefore a need to implement a truncation and acceptance rule. Using this knowlege and the computed

probabilities of implementing a truncation rule found from the simulation , a number of models were fitted to the values P1 , P2 , and s using the SAS stepwise logistic regression [Ref. 7] resulting in the following fitted model

$$\hat{P}_{\text{reaching NTP}} = \frac{\text{Exp}[-2.3415+0.294113\ln(P2-P1)-0.158121\ln(s)]}{1+\text{Exp}[-2.3415+0.294113\ln(P2-P1)-0.158121\ln(s)]} .(13)$$

The Chi-square test for goodness-of-fit for the Equation (13) resulted in p-value , 0.0001 and testing of the equation against the actual results from the simulation proved it to be quite accurate over the simulated range. Results of this testing can be seen in Table XXI of Appendix E. Further testing showed that it provided reasonable predictions for parameter sets outside of the simulation range. A 95% confidence limit for the maximum probability was also computed and found to be approximately [0.101 , 0.138].

One point to remember is that this equation only provides a rough upper limit for the probability of implementing a truncation rule and that if Pa is closer to P1 or P2, the actual probability will most likely be quite a bit smaller. graphs of the actual probabilities for each plan can be found in Appendix E, Figures 46 through 51.

## E. AREAS FOR FURTHER STUDY

This paper studied the curtailed Wald SPR sampling plan using only one set of values for alpha and beta. A further area of studied might be on how changing the values of alpha and beta impacts on these test results. It is hoped that the work provided in this paper will be beneficial to those interested in sequential sampling and quality control.

## APPENDIX A

### Computer Program Wald2

#### PROGRAM WALD2

```
C
C THE FOLLOWING PROGRAM SIMULATES THE USE OF A WALD
C SEQUENTIAL SAMPLING PLAN AND EVALUATES THE MEAN AND
C VARIANCE OF THE AVERAGE NUMBER OF ITEMS SAMPLED FOR A GIVEN
C PROBABILITY OF A NONCONFORMING ITEM.
C ie. Pr(item is nonconforming) = Pa
C
C THE PROGRAM CREATES LOTS OF 5000 ITEMS FROM WHICH ONE ITEM AT
C A TIME WILL BE RANDOMLY SAMPLED WITHOUT REPLACEMENT AND
C COMPARED TO A SPECIFIED ITEM REQUIREMENT. THE NUMBER OF
C NONCONFORMING ITEMS WILL BE COUNTED UNTIL A DECISION TO
C ACCEPT OR REJECT THE LOT CAN BE MADE. THE PROCESS WILL BE
C REPEATED FOR DIFFERENT STOPPING RULES AS DISCUSSED IN THE
C THESIS PAPER.
C
INCLUDE 'SEQDAT DEF'
INCLUDE 'LOTSEED DEF'
INCLUDE 'COUNTER DEF'
INCLUDE 'STATS DEF'
C
INTEGER I
SEED1(1) = #####
SEED2(1) = #####
C
C STARTING SEED VALUES CAN BE CHANGED AT ANY TIME AND WILL
C CHANGE AUTOMATICALLY EVERY TIME A NEW LOT IS CREATED
C
C//////////////////////////////STARTPLANSET1/////////////////////////////
C
DO 10 I = 1, 5
C
C THE FOLLOWING SUBROUTINE INITIALIZES VARIABLE THAT WILL BE
C USED IN THE SIMULATION
C
CALL INITOC1
C
C THE FOLLOWING SUBROUTINE CREATES THE SPECIFICS OF EACH PLAN
C
CALL SPECS
```

```
C  
C THE FOLLOWING SECTION STARTS THE SIMULATION FOR PLAN SET 1  
C  
DO 20 N = 1 , 82  
DO 30 R = 1 , 1000  
C  
C THE FOLLOWING FORMS THE LOTS AND SAMPLING SCHEDULE  
C  
CALL FORMLOT  
C  
C THE FOLLOWING SUBPROGRAM INSPECTS EACH LOT  
C  
CALL OCINSP  
C  
30 CONTINUE  
20 CONTINUE  
C  
C THE FOLLOWING SUBPROGRAMS COMPUTE THE DESIRED STATISTICS  
C AND DISPLAYS THEM  
C  
CALL STATCOMP  
CALL DISPLAY1  
10 CONTINUE  
C  
C//////////ENDPART1//////////  
C  
C//////////STARTPLAN SET2//////////  
C  
DO 40 I = 1 , 5  
C  
C THE FOLLOWING SUBROUTINE INITIALIZES VARIABLE THAT WILL BE  
C USED IN THE SIMULATION  
C  
CALL INITOC2  
C  
C THE FOLLOWING SUBROUTINE CREATES THE SPECIFICS OF EACH PLAN  
C  
CALL SPECS  
C  
C THE FOLLOWING SECTION STARTS THE SIMULATION FOR PLAN SET 1  
C  
DO 50 N = 1 , 82  
DO 60 R = 1 , 1000  
C  
C THE FOLLOWING FORMS THE LOTS AND SAMPLING SCHEDULE  
C
```

```

CALL FORMLOT
C
C THE FOLLOWING SUBPROGRAM INSPECTS EACH LOT
C
    CALL OCINSP
C
30    CONTINUE
20    CONTINUE
C
C THE FOLLOWING SUBPROGRAMS COMPUTE THE DESIRED STATISTICS
C AND DISPLAYS THEM
C
    CALL STATCOMP
    CALL DISPLAY2
10 CONTINUE
C
C//////////////ENDPART2///////////////
C

*** SAME AS ABOVE FOR PLAN SETS 3 AND 4 *****

C-----
C      SUBROUTINE INITOC1
C
INCLUDE 'SEQDAT2 DEF'
INCLUDE 'STATS2 DEF'
INCLUDE 'LOUTS DEF'
C
INTEGER I , J
C
DO 10 I = 1 , 82
    P1 = 0.0
    P2 = 0.0
    Pa = 0.0
    Za(I) = 0.0
    NTP(I) = 0
    DO 20 J = 1 , 1000
        NINSP(I , J) = 0
        RULE(I , J) = .FALSE.
        REJECT2(I , J) = .FALSE.
20    CONTINUE
10    CONTINUE
OPEN( 13 , FILE = '/OCPLAN1 DATA')
WRITE(* , *) "
WRITE(* , *)     P1      P2      Pa      NTP   "
DO 30 I = 1 , 82

```

```

      READ( 13 , * ) P1(I) , P2(I) , Pa(I) , NTP(I)
      WRITE( 15 , * ) P1(I) , P2(I) , Pa(I) , NTP(I)
15      FORMAT(1X , F5.3 , 2X , F4.2 , 2X , F5.3 , 2X , I4)
30      CONTINUE
      CLOSE(13)
      RETURN
      END
C-----SUBROUTINE INITOC2
C
      INCLUDE 'SEQDAT2 DEF'
      INCLUDE 'STATS2 DEF'
      INCLUDE ' LOTT'S DEF'
C
      INTEGER I , J
C
      DO 10 I = 1 , 82
          P1 = 0.0
          P2 = 0.0
          Pa = 0.0
          Za(I) = 0.0
          NTP(I) = 0
          DO 20 J = 1 , 1000
              NINSP(I , J) = 0
              RULE(I , J) = .FALSE.
              REJECT2(I , J) = .FALSE.
20      CONTINUE
10      CONTINUE
      OPEN( 13 , FILE = '/OCPLAN2 DATA')
      WRITE(* , * ) " "
      WRITE(* , * ) " P1    P2    Pa    NTP  "
      DO 30 I = 1 , 82
          READ( 13 , * ) P1(I) , P2(I) , Pa(I) , NTP(I)
          WRITE( 15 , * ) P1(I) , P2(I) , Pa(I) , NTP(I)
15      FORMAT(1X , F5.3 , 2X , F4.2 , 2X , F5.3 , 2X , I4)
30      CONTINUE
      CLOSE(13)
      RETURN
      END
C-----*****
***** SAME FOR PLAN SETS 3 AND 4 *****
C-----SUBROUTINE SPECS
C
      INCLUDE 'SEQDAT2 DEF'
      INCLUDE 'PLAN2 DEF'

```

```

C
C THE SUBROUTINE COMPUTE h1 , h2 , and s FOR EACH PLAN
C
    INTEGER I
    REAL DENOM
C
    DO I = 1 , 82
        DENOM = LOG( ( P2(I)*(1.0-P1(I)) ) / ( P1(I)*( 1.0-P2(I)) ) )
        H1(I) = 2.25129 / DENOM
        H2(I) = 2.89037 / DENOM
        S(I) = LOG9 (1.0 - P1(I)) / ( 1.0 - P2(I)) / DENOM
10   CONTINUE
    RETURN
    END
C-----  

    SUBROUTINE FORMLOT
C
C THIS SUBPROGRAM USES THE NAVAL POSTGRADUATE SCHOOLS
C RANDOM NUMBER GENERATOR TO CREATE A LOT OF 5000 ITEMS FROM
C A NORMAL DIST. AND THE RANDOM ORDER IN WHICH THE WILL BE
C SAMPLED
C
    INCLUDE 'LOUTS DEF'
    INCLUDE 'LOTSEED DEF'
    INCLUDE 'COUNTER DEF'
C
    INTEGER I
C
    CALL SNOR( SEED1(1) , LOT , 5000 , 2 , 0 )
    CALL SLINT( SEED2(1) , RANHLD , 5000 , 2 )
C
    DO 10 I = 1 , 5000
        SAMPNUM(I) = NINT(RANHLD(I) * 0.00000232)
10   CONTINUE
    RETURN
    END
C-----  

    SUBROUTINE OCINSP
C
C THIS SUBROUTINE INSPECTS THE ITEMS IN THE LOTS AND COLLECTS THE
C DATA THAT WILL BE USED TO DETERMINE THE OC CURVE AND ASN.
C
    INCLUDE 'SEQDAT2 DEF'
    INCLUDE 'STATS2 DEF'
    INCLUDE 'COUNTER DEF'
    INCLUDE 'LOUTS DEF'

```

```

INCLUDE 'PLAN2 DEF'
C
  INTEGER SUMX , C , M
  REAL UPX , LOWX , ITEM
  LOGICAL STPINSP

C
  ITEM = 0.0
  SUMX = 0
  C = 0
  M = 1
C  NOTE THAT THIS IS THE M IN THE H1-M RULE , M=0 MEANS REJECT AT
C  NTP
  STPINSP = .FALSE.

C
99  IF( .NOT.STPINSP ) THEN
    C = C+ 1
    ITEM = ABS( LOT ( SAMPNUM (C) ) )
    IF (ITEM .GT. Za (N) ) THEN
      SUMX = SUMX + 1
    ENDIF
    UPX = H2(N) + C * S(N)
    LOWX = C * S(N) - H1(N)

C
    IF( C .GE. NTP(N) ) THEN
      RULE( N , R ) = .TRUE.
      STPINSP = .TRUE.
      NINSP( N , R ) = C
      IF ( SUMX .GT. LOWX + M ) THEM
        REJECT2(N , R ) = .TRUE.
      ENDIF
      ELSEIF( SUMX . GE. UPX) THEN
        REJECT2(N , R ) = .TRUE.
        STPINSP = .TRUE.
        NINSP( N , R ) = C
      ELSEIF( SUMX . LE. LOWX) THEN
        STPINSP = .TRUE.
        NINSP( N , R ) = C
      ENDIF
      GOTO 99
    ENDIF
    RETURN
  END

```

---

```

C----- SUBROUTINE STATCOMP
C
C THIS SUBROUTINE COMPUTES THE DESIRED STATISTICS SUCH AS ASN

```

```

C
INCLUDE 'SEQDAT2 DEF'
INCLUDE 'STATS2 DEF'
INCLUDE 'PLAN2 DEF'
C
INTEGER I , J , SUMINSP(82)
REAL EXSQ(82)
C
DO 10 I = 1 , 82
    SUNINSP (I) = 0
    EXSQ(I) = 0.0
    NREJ2(I) = 0
    NSTP2(I) = 0
    CI2(I) = 0.0
    DO 20 J = 1 , 1000
        SUMINSP(I) = SUMINSP(I) + NINSP( I , J )
        IF(RULE( I, J )) THEN
            NSTP2(I) = NSTP2(I) + 1
        ENDIF
10   CONTINUE
        AVEN2(I) = SUMINSP(I) / 1000.0
        DO 25 J = 1 , 1000
            EXSQ(I) = EXSQ(I) + (( NINSP(I , J) - AVEN2(I) ) **2)
25   CONTINUE
        SAVEN2(I) = SQRT( EXSQ(I) / 1000.0 )
        CI2 = ( SAVEN2(I) / 100.0 ) * 1.95996
        UPCI2(I) = AVEN2(I) + CI2(I)
        LOWCI2(I) = AVEN2(I) - CI2(I)
10   CONTINUE
C
RETURN
END
C-----SUBROUTINE DISPLAY1
C
C THIS SUBROUTINE DISPLAYS THE STATISTICS AND WRITES THEM INTO
C A FILE
C
INCLUDE 'STATS2 DEF'
INCLUDE 'SEQDAT2 DEF'
C
INTEGER I
C
IF( I .EQ. 1 ) THEN
    OPEN(31 , FILE= '/OCOUT1A DATA')
IF( I .EQ. 2 ) THEN

```

```

      OPEN(32 ,FILE= '/OCOUT1B DATA')
IF( I .EQ. 3) THEN
      OPEN(33 ,FILE= '/OCOUT1C DATA')
IF( I .EQ. 4) THEN
      OPEN(34 ,FILE= '/OCOUT1D DATA')
ELSE
      OPEN(35 ,FILE = '/OCOUT1E DATA')
ENDIF
C
DO 10 I=1 ,82
      WRITE(*,*)
      WRITE(*,*)
      WRITE(*,*)
      WRITE(*,11) P1(I) ,P2(I) ,Pa(I) ,NTP(I)
      FORMAT( 4X ,F5.3 ,4X ,F5.3 ,5X ,F5.3 ,7X ,I4 )
      WRITE(*,13) AVEN2(I)
      FORMAT( 1X ,'MEAN NUMBER INSPECTED. ',2X ,F10.3)
      WRITE(*,15) SAVEN2(I)
      FORMAT( 1X ,'STD DEV OF NUM INSP ',2X ,F10.3)
      WRITE(*,17) LOWCI2(I) ,UPCI2(I)
      FORMAT(1X ,'95% CI ON MEAN (',1X ,F10.3 ,1X ,',' 1X ,F10.3 ,1X ,')')
      WRITE(*,19) NREJ2(I)
      FORMAT(1X ,'NUMBER OF LOTS REJECTED ',2X ,F8.1)
      WRITE(*,20) NSTP2(I)
      FORMAT(1X ,'# OF TIMES STOPPING RULE WAS USED' ,2X ,F8.1)
C
      IF ( I .EQ. 1 ) THEN
          WRITE(31 ,21 ) P1(I) ,P2(I) ,Pa(I) AVEN2(I) ,SAVEN2(I), NREJ2(I) ,
&NSTP2(I)
          FORMAT(1X ,3(F5.3 ,1X) ,3(F10.3 ,1X) ,F8.1)
          IF ( I .EQ. 1 ) THEN
              WRITE(31 ,22 ) P1(I) ,P2(I) ,Pa(I) AVEN2(I) ,SAVEN2(I), NREJ2(I) ,
&NSTP2(I)
              FORMAT(1X ,3(F5.3 ,1X) ,3(F10.3 ,1X) ,F8.1)
              IF ( I .EQ. 1 ) THEN
                  WRITE(31 ,23 ) P1(I) ,P2(I) ,Pa(I) AVEN2(I) ,SAVEN2(I), NREJ2(I) ,
&NSTP2(I)
                  FORMAT(1X ,3(F5.3 ,1X) ,3(F10.3 ,1X) ,F8.1)
                  IF ( I .EQ. 1 ) THEN
                      WRITE(31 ,24 ) P1(I) ,P2(I) ,Pa(I) AVEN2(I) ,SAVEN2(I), NREJ2(I) ,
&NSTP2(I)
                      FORMAT(1X ,3(F5.3 ,1X) ,3(F10.3 ,1X) ,F8.1)
                      ELSE
                          WRITE(31 ,25 ) P1(I) ,P2(I) ,Pa(I) AVEN2(I) ,SAVEN2(I), NREJ2(I) ,
&NSTP2(I)
                          FORMAT(1X ,3(F5.3 ,1X) ,3(F10.3 ,1X) ,F8.1)

```

```
        ENDIF
C
10    CONTINUE
      CLOSE(31)
      CLOSE(32)
      CLOSE(33)
      CLOSE(34)
      CLOSE(35)
      RETURN
      END
C-----  
**** SAME TYPE OF SUBROUTINE FOR DISPLAYING PLAN SETS 2 , 3, AND 4  
      JUST NEED TO CHANGE THE OUTPUT FILES *****  
C-----
```

## APPENDIX B

**Table III - OC CURVE DATA FOR PLAN SET I**  
**(h<sub>1</sub>-m) ACCEPTANCE RULE FOR m={0, 1, 2}**

P <sub>1</sub>	P <sub>2</sub>	P <sub>m</sub>	m = 0			m = 1			m = 2		
			Accorded		% Loss	Accorded		% Loss	Accorded		% Loss
			P <sup>*</sup>	P <sup>**</sup>	Z	P <sup>*</sup> , P <sup>**</sup>	Z	P <sup>*</sup> , P <sup>**</sup>	Z	P <sup>*</sup> , P <sup>**</sup>	Z
0.005	0.01	0.005	0.050	0.007	-8.28	0.000	-5.00	0.015	-4.41	0.000	-4.41
		0.005	0.020	0.762	-5.00	0.754	-5.78	0.762	-5.17	0.754	-5.17
		0.007	0.024	0.829	-5.00	0.820	-2.55	0.829	-2.01	0.820	-2.01
		0.008	0.025	0.902	1.75	0.904	1.00	0.902	2.27	0.904	2.27
		0.008	0.203	0.200	0.00	0.200	0.47	0.200	0.85	0.200	0.85
		0.010	0.100	0.110	1.02	0.110	1.02	0.110	2.02	0.110	2.02
0.005	0.02	0.005	0.050	0.005	-2.44	0.000	0.005	0.000	0.000	0.000	0.000
		0.005	0.765	0.761	-2.39	0.762	-2.23	0.765	0.410	0.762	0.410
		0.010	0.837	0.837	0.00	0.835	3.41	0.838	0.10	0.835	0.10
		0.012	0.467	0.462	-0.32	0.465	0.497	0.462	0.534	0.465	0.534
		0.014	0.850	0.847	1.14	0.850	0.373	0.850	0.403	0.850	0.403
		0.018	0.224	0.251	2.01	0.258	2.00	0.250	0.70	0.250	0.70
		0.014	0.146	0.193	1.33	0.175	2.32	0.183	0.70	0.183	0.70
		0.020	0.100	0.112	1.33	0.122	2.21	0.183	2.25	0.183	2.25
0.005	0.03	0.005	0.050	0.051	0.15	0.058	2.00	0.050	1.87	0.050	1.87
		0.007	0.002	0.015	2.46	0.024	2.00	0.060	2.00	0.060	2.00
		0.010	0.767	0.746	-1.65	0.658	1.44	0.801	2.81	0.801	2.81
		0.013	0.809	0.805	-0.28	0.850	2.88	0.885	0.93	0.885	0.93
		0.016	0.487	0.489	1.39	0.815	2.04	0.837	0.43	0.837	0.43
		0.019	0.241	0.280	2.57	0.405	4.10	0.327	5.59	0.327	5.59
		0.022	0.245	0.273	2.02	0.208	2.00	0.305	4.25	0.305	4.25
		0.025	0.179	0.189	0.82	0.212	2.71	0.226	2.79	0.226	2.79
		0.028	0.128	0.122	0.38	0.141	1.20	0.151	2.10	0.151	2.10
		0.030	0.100	0.110	1.93	0.120	2.02	0.132	2.16	0.132	2.16
0.005	0.04	0.005	0.050	0.052	0.29	0.077	4.65	0.000	5.16	0.000	5.16
		0.007	0.005	0.000	-0.53	0.031	2.00	0.037	5.76	0.037	5.76
		0.010	0.012	0.798	-1.12	0.061	4.19	0.075	5.49	0.075	5.49
		0.013	0.700	0.698	-0.08	0.701	5.42	0.800	7.82	0.800	7.82
		0.016	0.594	0.524	-0.02	0.681	4.20	0.587	4.81	0.587	4.81
		0.019	0.492	0.509	1.03	0.910	7.80	0.645	9.77	0.645	9.77
		0.022	0.399	0.389	-1.05	0.471	4.59	0.514	7.89	0.514	7.89
		0.025	0.310	0.314	-0.34	0.286	4.43	0.414	6.23	0.414	6.23
		0.028	0.254	0.257	0.22	0.232	5.49	0.370	7.02	0.370	7.02
		0.031	0.189	0.200	0.08	0.250	2.07	0.205	5.26	0.205	5.26
		0.034	0.150	0.162	-0.01	0.195	2.00	0.217	5.00	0.217	5.00
		0.037	0.125	0.123	-0.19	0.149	2.21	0.160	5.92	0.160	5.92
		0.040	0.100	0.103	0.21	0.129	2.79	0.143	5.10	0.143	5.10
0.005	0.05	0.005	0.050	0.073	3.70	0.001	6.37	0.003	5.89	0.003	5.89
		0.008	0.001	0.006	1.57	0.033	4.00	0.026	5.94	0.026	5.94
		0.011	0.012	0.028	1.32	0.073	6.30	0.081	5.26	0.081	5.26

Table III - OC CURVE DATA FOR PLAN SET I  
 (h<sub>1</sub>-m) ACCEPTANCE RULE FOR m={ 0, 1, 2 }  
 (CONTINUED)

0.014	0.725	0.899	-1.82	BCC.	0.774	4.59	0.782	4.18			
0.017	0.640	0.899	-0.13	BCC.	0.709	4.59	0.723	5.62			
0.020	0.552	0.899	0.19	BCC.	0.644	2.97	0.653	5.62			
0.023	0.473	0.605	2.92		0.574	5.85	0.682	5.62			
0.026	0.395	0.434	5.89		0.491	5.85	0.519	7.42			
0.029	0.310	0.289	1.93	BCC.	0.413	5.85	0.428	5.89			
0.032	0.235	0.272	-0.70	BCC.	0.309	5.85	0.340	5.84			
0.035	0.241	0.389	1.87	BCC.	0.309	4.41	0.315	5.89			
0.038	0.203	0.249	5.89		0.299	5.85	0.299	5.89			
0.041	0.171	0.289	1.84	BCC.	0.214	5.85	0.230	4.99			
0.044	0.142	0.389	0.27	BCC.	0.127	2.19	0.179	3.19			
0.047	0.119	0.389	1.89	BCC.	0.167	5.85	0.182	5.89			
0.050	0.100	0.097	-1.41	BCC.	0.101	0.11	BCC.	0.103	0.31		
0.005	0.00	0.005	0.899	7.42		0.399	5.85	0.398	5.42		
		0.009	0.870	0.812	5.85	0.931	5.70	0.931	5.70		
		0.016	0.700	0.812	5.85	0.857	5.85	0.858	5.89		
		0.017	0.895	0.716	1.48	BCC.	0.789	4.41	0.790	5.83	
		0.021	0.895	0.889	5.89		0.716	7.72	0.717	7.80	
		0.025	0.895	0.542	8.72		0.594	5.85	0.599	6.16	
		0.028	0.423	0.389	5.89		0.802	5.85	0.800	5.89	
		0.033	0.252	0.389	5.85		0.399	5.85	0.442	5.89	
		0.027	0.895	0.931	1.93	BCC.	0.399	5.85	0.373	5.87	
		0.041	0.245	0.389	0.27	BCC.	0.399	2.87	0.368	5.89	
		0.045	0.202	0.812	0.70	BCC.	0.399	2.74	0.241	5.89	
		0.049	0.187	0.389	-0.62	BCC.	0.167	1.25	BCC.	0.183	1.33
		0.053	0.187	0.389	-1.22	BCC.	0.125	-0.18	BCC.	0.183	5.89
		0.057	0.119	0.389	0.27	BCC.	0.127	2.90	BCC.	0.139	5.89
		0.060	0.100	0.124	2.41		0.127	5.85	0.129	2.79	
0.005	0.07	0.005	0.899	1.87	BCC.	0.894	0.02	0.894	0.02		
		0.010	0.899	0.871	0.47	BCC.	0.894	7.66	0.899	7.78	
		0.015	0.767	0.789	1.52	BCC.	0.873	0.72	0.875	0.91	
		0.020	0.895	0.889	-0.47	BCC.	0.769	5.87	0.781	5.44	
		0.025	0.891	0.577	1.82	BCC.	0.797	0.89	0.799	0.72	
		0.030	0.464	0.389	1.82	BCC.	0.817	0.72	0.829	10.29	
		0.005	0.397	0.389	0.19	BCC.	0.594	7.44	0.608	7.79	
		0.040	0.221	0.297	-1.84	BCC.	0.594	5.85	0.408	5.72	
		0.045	0.239	0.239	-2.10		0.299	5.85	0.325	5.89	
		0.050	0.219	0.211	-0.62	BCC.	0.299	4.91	0.299	5.89	
		0.055	0.181	0.189	0.85	BCC.	0.242	4.80	0.249	5.19	
		0.060	0.148	0.153	0.44	BCC.	0.217	5.85	0.222	5.89	
		0.065	0.121	0.110	-1.89	BCC.	0.165	2.12	0.157	5.89	
		0.070	0.100	0.116	3.82	BCC.	0.141	5.85	0.145	5.84	

Table IV - OC CURVE DATA FOR PLAN SET II  
 (h1-m) ACCEPTANCE RULE FOR m={ 0, 1, 2 }

P1	P2	P3	P4	m = 0			m = 1			m = 2		
				Accept	% Loss	Z	P <sub>NP</sub>	Accept	% Loss	Z	P <sub>NP</sub>	Accept
0.01	0.02	0.010	0.050									
				P'	P'	P'	P'	P'	P'	P'	P'	P'
0.010	0.019	0.010	0.050	0.593	1.05	0.007	0.70	0.971	2.21			
0.010	0.019	0.019	0.050	0.996	1.18	0.017	2.28	0.983	2.21			
0.010	0.019	0.012	0.050	0.839	2.28	0.000	2.28	0.971	2.21			
0.010	0.019	0.700	0.700	0.714	0.38	0.007	0.722	1.02	0.785	2.28		
0.010	0.019	0.881	0.881	0.882	-1.18	0.000	0.888	2.28	0.882	1.00	0.000	
0.020	0.029	0.448	0.454	0.454	0.38	0.005	0.478	1.71	0.497	2.18		
0.022	0.022	0.243	0.211	0.211	-2.74	0.021	0.211	-1.49	0.262	0.73	0.000	
0.024	0.020	0.250	0.274	0.274	1.72	0.005	0.284	2.42	0.391	0.81		
0.020	0.020	0.189	0.182	0.182	-2.67	0.005	0.174	-1.18	0.187	0.000	0.000	
0.020	0.020	0.189	0.182	0.182	1.17	0.005	0.199	1.02	0.183	2.12		
0.020	0.020	0.100	0.119	0.119	1.02	0.005	0.199	0.91	0.124	4.00		
0.01	0.04	0.010	0.050	0.000	1.21	0.000	0.000	2.21	0.979	0.00		
0.010	0.019	0.001	0.001	0.001	-0.29	0.005	0.007	1.02	0.999	0.00		
0.010	0.700	0.700	0.700	-1.02	0.000	0.000	0.70	0.922	0.00			
0.010	0.003	0.843	0.843	-2.68	0.000	0.000	0.01	0.731	2.28			
0.022	0.849	0.829	0.829	-1.27	0.000	0.000	1.04	0.922	0.00			
0.025	0.428	0.397	0.397	-2.50	0.026	0.026	-0.84	0.474	2.41			
0.025	0.325	0.321	0.321	0.30	0.005	0.000	2.07	0.402	0.00			
0.021	0.260	0.257	0.257	0.57	0.005	0.002	2.28	0.901	0.00			
0.024	0.188	0.179	0.179	-0.49	0.005	0.199	1.12	0.227	2.28			
0.027	0.127	0.129	0.129	-0.29	0.005	0.147	0.61	0.184	2.28			
0.040	0.100	0.290	0.290	-1.08	0.005	0.007	-0.32	0.184	0.42			
0.01	0.05	0.010	0.050	0.020	-1.01	0.005	0.000	0.29	0.983	2.28		
0.013	0.050	0.321	0.321	-2.50	0.005	0.007	2.04	0.937	2.28			
0.010	0.020	0.047	0.047	1.03	0.005	0.000	6.24	0.998	7.59			
0.010	0.743	0.741	0.741	-0.14	0.005	0.791	0.59	0.826	0.00			
0.023	0.054	0.056	0.056	0.60	0.005	0.722	0.42	0.768	7.59			
0.025	0.050	0.072	0.072	0.57	0.005	0.190	4.82	0.826	0.00			
0.028	0.487	0.060	0.060	-0.57	0.005	0.810	2.72	0.862	0.01			
0.021	0.487	0.375	0.375	-0.29	0.005	0.924	2.28	0.826	0.97			
0.034	0.303	0.300	0.300	-0.21	0.005	0.337	2.30	0.874	4.74			
0.037	0.054	0.253	0.253	-0.07	0.005	0.269	0.59	0.826	0.01			
0.040	0.203	0.182	0.182	-0.39	0.005	0.917	1.02	0.247	4.00			
0.030	0.177	0.182	0.182	-1.26	0.005	0.190	0.89	0.210	2.64			
0.044	0.184	0.144	0.144	-0.39	0.005	0.157	0.29	0.183	0.00			
0.047	0.125	0.121	0.121	0.57	0.005	0.190	2.72	0.168	0.00			
0.050	0.100	0.162	0.162	2.41	0.005	0.190	3.44	0.146	0.00			
0.01	0.05	0.010	0.000	0.000	0.74	0.005	0.074	2.27	0.979	0.00		
0.010	0.010	0.009	0.017	0.017	0.005	0.000	0.69	0.983	7.59			
0.010	0.055	0.047	0.047	-0.71	0.005	0.002	2.62	0.810	2.20			

Table IV - OC CURVE DATA FOR PLAN SET I  
 (h<sub>1</sub>-m) ACCEPTANCE RULE FOR m={ 0, 1, 2 }  
 (CONTINUED)

	0.015	0.786	0.782	-1.81	REG.	0.819	2.82		0.844	4.72
	0.022	0.711	0.685	-1.11	REG.	0.782	2.44		0.795	3.18
	0.025	0.642	0.612	-1.24	REG.	0.875	2.12		0.721	3.80
	0.025	0.665	0.644	-1.24	REG.	0.829	2.02		0.892	5.89
	0.021	0.488	0.424	-2.20		0.812	2.82	REG.	0.395	4.87
	0.025	0.492	0.387	-2.20		0.429	1.72	REG.	0.490	4.87
	0.040	0.209	0.203	-0.97	REG.	0.353	2.02		0.395	4.70
	0.040	0.284	0.248	-1.16	REG.	0.353	1.84	REG.	0.248	4.70
	0.040	0.224	0.192	-0.89	REG.	0.250	1.84	REG.	0.237	4.87
	0.040	0.195	0.188	-0.25	REG.	0.213	2.22		0.247	4.70
	0.051	0.187	0.170	0.82	REG.	0.188	2.02		0.210	2.00
	0.054	0.182	0.120	-1.41	REG.	0.180	2.72	REG.	0.170	2.84
	0.067	0.110	0.105	-1.40	REG.	0.114	-0.49	REG.	0.125	1.82
	0.060	0.162	0.075	-2.20		0.079	-2.33		0.023	-0.76
0.01 0.07	0.010	0.280	0.255	0.74	REG.	0.528	2.22		0.022	2.00
	0.015	0.486	0.303	1.74	REG.	0.824	2.62		0.828	4.87
	0.020	0.786	0.612	2.54		0.867	2.02		0.975	7.89
	0.025	0.700	0.387	-0.21	REG.	0.782	2.02		0.768	4.87
	0.040	0.287	0.577	-0.84	REG.	0.842	2.02		0.871	5.89
	0.028	0.498	0.470	-0.44	REG.	0.539	2.12		0.570	4.89
	0.040	0.292	0.203	0.90	REG.	0.447	2.02		0.471	4.88
	0.040	0.209	0.202	-0.21	REG.	0.520	2.02		0.248	4.84
	0.050	0.250	0.544	-0.44	REG.	0.270	1.84	REG.	0.288	2.71
	0.055	0.182	0.198	-1.27	REG.	0.212	2.02	REG.	0.228	2.00
	0.060	0.162	0.198	-1.40	REG.	0.148	0.81	REG.	0.187	2.89
	0.065	0.100	0.118	-0.77	REG.	0.120	0.28	REG.	0.148	1.87
	0.070	0.100	0.104	0.96	REG.	0.111	1.12	REG.	0.119	1.92
0.01 0.08	0.010	0.800	0.823	0.90	REG.	0.873	2.66		0.873	2.97
	0.010	0.898	0.891	-1.10	REG.	0.821	2.66		0.929	4.82
	0.025	0.808	0.788	-1.40	REG.	0.855	2.97		0.873	4.86
	0.025	0.727	0.700	-0.14	REG.	0.811	2.66		0.900	7.84
	0.025	0.613	0.623	1.81	REG.	0.714	2.66		0.735	4.83
	0.035	0.642	0.644	0.96	REG.	0.613	4.48		0.848	4.83
	0.040	0.654	0.420	-1.40	REG.	0.824	4.48		0.848	4.88
	0.040	0.287	0.293	0.96	REG.	0.480	2.02		0.514	4.87
	0.055	0.219	0.292	-1.40	REG.	0.380	2.66		0.420	7.13
	0.055	0.241	0.270	2.74		0.335	2.66		0.373	4.95
	0.055	0.224	0.228	0.96	REG.	0.373	2.66		0.394	4.74
	0.060	0.182	0.198	-1.41	REG.	0.295	1.80	REG.	0.231	2.89
	0.070	0.181	0.122	-2.97		0.152	0.99	REG.	0.187	2.84
	0.075	0.195	0.119	-2.20	REG.	0.148	2.12		0.163	2.91
	0.080	0.100	0.100	0.82	REG.	0.135	2.64		0.148	4.81

Table V - DATA OUTPUT PLAN SET I

## (h1-1) ACCEPTANCE RULE

				Plan D1						Ave	
P1	P2	P3	NCO	ABN(PA)	INADPEN	Std Dev	Mean CI (+/-)	# PA	% Loss	# Times	Plan run
0.005	0.01	0.005	4505	1207	1212.8	823.9	40.8	0.950	0.922	18.5	0.820
		0.006		1803	1812.2	1185.7	80.9	0.928	0.778	82.5	0.852
		0.007		2085	1742.9	1208.8	82.9	0.924	0.905	85.5	0.859
		0.008		1764	1899.7	1197.0	82.5	0.975	0.491	88.5	0.857
		0.009		1485	1856.2	1128.4	49.4	0.203	0.240	40	0.840
		0.010		1225	1821.2	1022.2	44.8	0.190	0.147	23	0.823
0.005	0.02	0.006	792	204	277.8	194.0	7.2	0.999	0.921	84	0.864
		0.008		801	382.4	182.0	8.0	0.785	0.902	88.5	0.887
		0.010		325	329.1	199.0	0.7	0.937	0.982	127	0.827
		0.012		202	818.1	202.8	0.9	0.467	0.502	121	0.121
		0.014		270	288.0	198.6	0.7	0.320	0.257	85	0.885
		0.016		241	288.8	182.1	8.8	0.224	0.272	78.5	0.877
		0.018		213	282.5	179.5	7.0	0.148	0.188	45	0.845
		0.020		186	224.5	184.0	7.2	0.190	0.123	30.5	0.831
0.005	0.03	0.005	375	122	124.2	84.9	2.8	0.950	0.962	20	0.820
		0.007		124	144.4	82.9	2.9	0.992	0.915	48.5	0.859
		0.010		149	155.8	98.3	4.2	0.707	0.785	84.5	0.885
		0.013		160	183.2	101.8	4.5	0.909	0.983	190.5	0.101
		0.016		128	154.6	102.8	4.5	0.467	0.514	84.5	0.885
		0.019		126	146.8	100.8	4.4	0.341	0.379	87.5	0.868
		0.022		113	126.0	87.4	4.3	0.245	0.289	50	0.869
		0.025		100	123.4	91.7	4.0	0.176	0.194	24	0.834
		0.028		88	107.0	83.0	3.7	0.128	0.120	10	0.818
		0.030		82	102.1	79.0	3.5	0.100	0.110	12.5	0.814
0.005	0.04	0.005	182	80	79.8	24.9	1.8	0.950	0.973	83.5	0.864
		0.007		84	86.9	41.9	1.8	0.995	0.925	115	0.115
		0.010		89	95.1	48.4	2.1	0.912	0.889	170	0.170
		0.013		99	94.0	50.9	2.2	0.709	0.780	184.5	0.185
		0.016		83	96.8	51.0	2.3	0.594	0.698	100	0.189
		0.019		82	82.9	54.4	2.4	0.492	0.561	101	0.191
		0.022		79	80.4	54.2	2.4	0.399	0.461	100	0.169
		0.025		74	88.1	52.3	2.2	0.319	0.289	144.5	0.145
		0.028		69	79.7	52.1	2.3	0.264	0.316	110.5	0.117
		0.031		83	78.9	52.8	2.3	0.199	0.252	104	0.104
		0.034		59	71.3	51.7	2.2	0.159	0.193	80	0.090
		0.037		53	66.7	49.3	2.2	0.126	0.166	70.5	0.071
		0.040		49	81.1	48.4	2.0	0.100	0.134	40	0.048
0.005	0.05	0.005	151	88	90.2	28.3	1.2	0.950	0.982	43	0.842
		0.008		82	97.5	34.0	1.5	0.991	0.934	100	0.120
		0.011		83	71.1	37.3	1.6	0.912	0.873	180	0.120

Table V - DATA OUTPUT PLAN SET I  
 (h1-1) ACCEPTANCE RULE  
 (CONTINUED)

		0.014	63	70.0	38.5	1.7	0.725	0.794	124.5	0.125	
		0.017	63	72.1	41.4	1.9	0.840	0.805	142.5	0.143	
		0.020	70	71.0	42.5	1.9	0.853	0.837	145.5	0.148	
		0.023	62	70.7	42.0	1.9	0.473	0.653	120	0.130	
		0.026	57	69.0	42.1	1.9	0.399	0.492	121	0.121	
		0.029	55	68.2	41.7	1.9	0.330	0.422	120	0.120	
		0.032	49	62.0	41.5	1.9	0.288	0.345	87	0.087	
		0.035	48	60.4	41.2	1.9	0.241	0.200	80.5	0.081	
		0.038	42	55.7	39.7	1.7	0.203	0.200	55.5	0.065	
		0.041	41	52.2	37.1	1.9	0.171	0.181	40.5	0.041	
		0.044	38	49.0	35.8	1.9	0.142	0.183	28	0.028	
		0.047	38	45.5	34.0	1.9	0.119	0.124	24.5	0.025	
		0.050	34	42.3	31.8	1.4	0.100	0.091	12.5	0.012	
0.005	0.06	0.005	120	46	48.0	21.7	0.0	0.950	0.976	34.5	0.035
		0.008	48	63.5	27.0	1.2	0.878	0.938	65.5	0.048	
		0.012	49	58.0	30.0	1.4	0.788	0.858	38	0.038	
		0.017	80	58.0	32.0	1.4	0.895	0.775	104	0.104	
		0.021	88	58.2	34.2	1.6	0.900	0.875	111.5	0.112	
		0.025	49	58.0	34.5	1.6	0.499	0.607	101	0.101	
		0.029	43	53.1	34.5	1.6	0.423	0.515	88.5	0.097	
		0.032	40	51.0	34.1	1.6	0.352	0.432	52	0.082	
		0.037	38	49.2	32.0	1.4	0.292	0.371	33	0.062	
		0.041	25	47.7	33.4	1.6	0.245	0.288	50	0.060	
		0.045	23	43.2	30.2	1.3	0.203	0.224	24	0.034	
		0.048	21	41.3	29.1	1.3	0.187	0.188	28	0.028	
		0.053	29	37.5	27.3	1.2	0.137	0.153	17.5	0.018	
		0.057	27	35.0	26.7	1.2	0.118	0.115	12.5	0.014	
		0.060	25	34.4	25.8	1.1	0.100	0.098	10.5	0.011	
0.005	0.07	0.005	74	37	40.2	14.9	0.7	0.850	0.870	160	0.158
		0.010	38	43.0	17.5	0.8	0.946	0.879	82.5	0.123	
		0.015	40	44.5	19.0	0.9	0.767	0.870	285.5	0.285	
		0.020	41	44.4	20.1	0.9	0.669	0.705	276.5	0.277	
		0.025	42	44.7	20.5	0.9	0.581	0.696	200.5	0.200	
		0.030	38	42.7	20.0	0.9	0.484	0.570	222.5	0.233	
		0.035	34	40.8	21.2	0.9	0.397	0.495	205.5	0.204	
		0.040	31	39.7	21.3	0.9	0.321	0.423	176.5	0.177	
		0.045	29	39.0	20.9	0.9	0.269	0.342	140	0.140	
		0.050	27	35.5	20.7	0.9	0.210	0.304	127.5	0.128	
		0.055	25	33.0	20.4	0.9	0.181	0.244	100	0.100	
		0.060	23	31.7	19.9	0.9	0.148	0.205	80.5	0.090	
		0.065	21	29.6	19.1	0.9	0.121	0.167	65.5	0.087	
		0.070	20	28.2	18.0	0.9	0.100	0.131	50.5	0.083	

Table VI - ASN TESTING , PLAN SET I  
 (h1-1) ACCEPTANCE RULE

P1	P2	Ps	ASN(Ps)	Mean #	Inspected	Difference	Computed		Ho: $\mu_1 = \mu_2$		Ho: $\mu_1 < \mu_2$	
							1	Statistic	t(0.05)	Ho: $\mu_1 < \mu_2$	t(0.01)	Ho: $\mu_1 < \mu_2$
0.005	0.01	0.005	1287	1312.5	25.35	1.21	-1.646	Accept	-2.328	Acc.		
		0.006	1603	1613.2	10.47	0.41	-1.646	Accept	-2.328	Acc.		
		0.007	2085	1743.9	-341.08	-12.64	-1.646	R	-2.328	R		
		0.008	1764	1698.7	-64.03	-2.39	-1.646	R	-2.328	R		
		0.009	1485	1555.2	70.04	2.78	-1.646	Accept	-2.328	Acc.		
		0.010	1225	1321.2	96.46	4.22	-1.646	Accept	-2.328	Acc.		
		0.005	264	277.5	13.85	3.76	-1.646	Accept	-2.328	Acc.		
		0.008	301	302.4	1.50	0.37	-1.646	Accept	-2.328	Acc.		
		0.010	325	329.1	3.73	0.84	-1.646	Accept	-2.328	Acc.		
		0.012	302	318.1	16.30	3.58	-1.646	Accept	-2.328	Acc.		
0.005	0.02	0.006	270	298.0	28.12	6.34	-1.646	Accept	-2.328	Acc.		
		0.014	241	288.8	47.50	11.00	-1.646	Accept	-2.328	Acc.		
		0.016	213	252.5	39.95	9.95	-1.646	Accept	-2.328	Acc.		
		0.018	213	252.5	39.95	9.95	-1.646	Accept	-2.328	Acc.		
		0.020	186	224.5	38.85	10.59	-1.646	Accept	-2.328	Acc.		
		0.005	122	124.3	1.87	1.29	-1.646	Accept	-2.328	Acc.		
		0.007	134	144.4	10.50	5.68	-1.646	Accept	-2.328	Acc.		
		0.010	146	155.8	10.21	4.74	-1.646	Accept	-2.328	Acc.		
		0.013	150	163.2	13.19	5.80	-1.646	Accept	-2.328	Acc.		
		0.016	138	154.6	16.61	7.23	-1.646	Accept	-2.328	Acc.		
0.005	0.03	0.005	126	146.8	21.20	9.42	-1.646	Accept	-2.328	Acc.		
		0.019	113	136.0	23.39	10.74	-1.646	Accept	-2.328	Acc.		
		0.022	100	123.4	23.48	11.45	-1.646	Accept	-2.328	Acc.		
		0.025	88	107.6	19.41	10.36	-1.646	Accept	-2.328	Acc.		
		0.030	82	102.1	19.82	11.12	-1.646	Accept	-2.328	Acc.		
		0.005	80	79.8	0.26	0.33	-1.646	Accept	-2.328	Acc.		
		0.007	84	86.8	2.49	2.86	-1.646	Accept	-2.328	Acc.		
		0.010	88	95.1	7.11	6.57	-1.646	Accept	-2.328	Acc.		
		0.013	89	94.9	5.61	4.96	-1.646	Accept	-2.328	Acc.		
		0.016	83	96.6	13.92	11.99	-1.646	Accept	-2.328	Acc.		
0.005	0.04	0.005	83	93.6	10.99	9.03	-1.646	Accept	-2.328	Acc.		
		0.019	79	90.4	11.71	9.85	-1.646	Accept	-2.328	Acc.		
		0.022	74	88.1	14.50	12.16	-1.646	Accept	-2.328	Acc.		
		0.025	68	79.7	11.61	8.78	-1.646	Accept	-2.328	Acc.		
		0.028	63	76.9	13.74	11.64	-1.646	Accept	-2.328	Acc.		
		0.031	58	71.3	13.37	11.57	-1.646	Accept	-2.328	Acc.		
		0.034	53	66.7	13.20	11.97	-1.646	Accept	-2.328	Acc.		
		0.037	49	61.1	11.92	11.49	-1.646	Accept	-2.328	Acc.		
		0.040	49	61.1	11.92	11.49	-1.646	Accept	-2.328	Acc.		
		0.005	58	60.3	2.02	3.43	-1.646	Accept	-2.328	Acc.		
0.005	0.05	0.008	62	67.5	5.49	7.06	-1.646	Accept	-2.328	Acc.		
		0.011	63	71.1	7.84	9.40	-1.646	Accept	-2.328	Acc.		

Table VI - ASN TESTING , PLAN SET I  
 (h1-1) ACCEPTANCE RULE  
 (CONTINUED)

0.014	63	70.9	8.04	9.34	-1.646	Accept	-2.328	Acc.	
0.017	63	72.1	8.82	9.52	-1.646	Accept	-2.328	Acc.	
0.020	70	71.8	2.06	2.16	-1.646	Accept	-2.328	Acc.	
0.023	62	70.7	8.65	9.21	-1.646	Accept	-2.328	Acc.	
0.026	57	69.0	11.89	12.62	-1.646	Accept	-2.328	Acc.	
0.029	55	66.3	11.19	12.01	-1.646	Accept	-2.328	Acc.	
0.032	49	63.8	14.50	15.63	-1.646	Accept	-2.328	Acc.	
0.035	46	60.4	13.92	15.11	-1.646	Accept	-2.328	Acc.	
0.038	43	56.7	13.24	14.92	-1.646	Accept	-2.328	Acc.	
0.041	41	52.2	11.49	13.87	-1.646	Accept	-2.328	Acc.	
0.044	38	49.0	10.70	13.45	-1.646	Accept	-2.328	Acc.	
0.047	36	45.5	9.47	12.48	-1.646	Accept	-2.328	Acc.	
0.050	34	42.3	8.40	11.81	-1.646	Accept	-2.328	Acc.	
0.005	0.06	46	48.8	3.17	6.55	-1.646	Accept	-2.328	Acc.
	0.009	48	53.5	5.20	8.62	-1.646	Accept	-2.328	Acc.
	0.013	49	56.8	7.99	11.59	-1.646	Accept	-2.328	Acc.
	0.017	50	58.0	7.61	10.53	-1.646	Accept	-2.328	Acc.
	0.021	56	58.2	2.13	2.78	-1.646	Accept	-2.328	Acc.
	0.025	49	56.6	7.20	9.34	-1.646	Accept	-2.328	Acc.
	0.029	43	55.1	12.22	15.82	-1.646	Accept	-2.328	Acc.
	0.033	40	51.9	11.46	15.02	-1.646	Accept	-2.328	Acc.
	0.037	38	49.3	11.80	15.92	-1.646	Accept	-2.328	Acc.
	0.041	35	47.7	12.79	17.12	-1.646	Accept	-2.328	Acc.
	0.045	33	43.3	10.69	15.82	-1.646	Accept	-2.328	Acc.
	0.049	31	41.3	10.83	16.62	-1.646	Accept	-2.328	Acc.
	0.053	29	37.5	8.91	14.61	-1.646	Accept	-2.328	Acc.
	0.057	27	35.9	9.37	15.72	-1.646	Accept	-2.328	Acc.
	0.060	25	34.4	9.09	15.76	-1.646	Accept	-2.328	Acc.
0.005	0.07	37	40.2	2.82	8.48	-1.646	Accept	-2.328	Acc.
	0.010	39	43.0	3.91	9.99	-1.646	Accept	-2.328	Acc.
	0.015	40	44.5	4.90	11.87	-1.646	Accept	-2.328	Acc.
	0.020	41	44.4	2.99	6.05	-1.646	Accept	-2.328	Acc.
	0.025	42	44.7	2.36	5.15	-1.646	Accept	-2.328	Acc.
	0.030	38	42.7	5.07	10.86	-1.646	Accept	-2.328	Acc.
	0.035	34	40.8	7.18	15.09	-1.646	Accept	-2.328	Acc.
	0.040	31	38.7	7.69	16.17	-1.646	Accept	-2.328	Acc.
	0.045	28	36.8	8.43	18.04	-1.646	Accept	-2.328	Acc.
	0.050	27	35.5	8.96	19.39	-1.646	Accept	-2.328	Acc.
	0.055	25	33.8	9.23	20.24	-1.646	Accept	-2.328	Acc.
	0.060	23	31.7	8.78	19.75	-1.646	Accept	-2.328	Acc.
	0.065	21	29.6	8.14	19.04	-1.646	Accept	-2.328	Acc.
	0.070	20	28.3	8.35	19.85	-1.646	Accept	-2.328	Acc.

Table VII - OC CURVE TESTING , PLAN SET I  
 (h1-1) ACCEPTANCE RULE

P1	P2	Pn	PLAN 01		Z	Z(0.05)	H0: P1 = P2		Z(0.2)	H0: P1 < P2	
			Accord	% Loss			DE(P)	Statistic		+ M -	H0: P1 > P2
			P2	P1							
0.005	0.01	0.005	0.960	0.922	0.005	-6.12	1.960	R	2.054	R	
		0.006	0.960	0.770	0.009	-6.67	1.960	R	2.054	R	
		0.007	0.960	0.695	0.011	-1.78	1.960	Accord	2.054	Accord	
		0.008	0.960	0.491	0.011	2.20	1.960	R	2.054	R	
		0.009	0.960	0.240	0.007	2.20	1.960	R	2.054	R	
		0.010	0.960	0.147	0.007	2.20	1.960	R	2.054	R	
0.005	0.02	0.005	0.960	0.921	0.005	1.70	1.960	Accord	2.054	Accord	
		0.006	0.960	0.795	0.009	0.82	1.960	Accord	2.054	Accord	
		0.010	0.960	0.637	0.011	2.30	1.960	R	2.054	R	
		0.012	0.960	0.467	0.011	2.14	1.960	R	2.054	R	
		0.010	0.960	0.357	0.011	2.20	1.960	R	2.054	R	
		0.010	0.960	0.272	0.011	0.02	1.960	R	2.054	R	
		0.010	0.960	0.148	0.007	4.63	1.960	R	2.054	R	
		0.020	0.960	0.140	0.007	2.20	1.960	R	2.054	R	
0.005	0.02	0.005	0.960	0.962	0.005	2.92	1.960	R	2.054	R	
		0.007	0.960	0.915	0.007	2.20	1.960	R	2.054	R	
		0.010	0.960	0.767	0.009	1.00	1.960	Accord	2.054	Accord	
		0.013	0.960	0.662	0.011	5.01	1.960	R	2.054	R	
		0.018	0.960	0.467	0.011	4.22	1.960	R	2.054	R	
		0.019	0.960	0.341	0.011	2.48	1.960	R	2.054	R	
		0.022	0.960	0.245	0.010	2.23	1.960	R	2.054	R	
		0.025	0.960	0.176	0.009	2.05	1.960	R	2.054	Accord	
		0.028	0.960	0.128	0.008	0.20	1.960	Accord	2.054	Accord	
		0.030	0.960	0.100	0.007	1.46	1.960	Accord	2.054	Accord	
0.005	0.04	0.005	0.960	0.972	0.004	6.35	1.960	R	2.054	R	
		0.007	0.960	0.935	0.008	4.00	1.960	R	2.054	R	
		0.010	0.960	0.868	0.008	7.00	1.960	R	2.054	R	
		0.012	0.960	0.786	0.010	7.60	1.960	R	2.054	R	
		0.014	0.960	0.694	0.011	8.20	1.960	R	2.054	R	
		0.019	0.960	0.492	0.011	8.12	1.960	R	2.054	R	
		0.022	0.960	0.399	0.011	8.59	1.960	R	2.054	R	
		0.025	0.960	0.310	0.011	8.62	1.960	R	2.054	R	
		0.028	0.960	0.264	0.010	9.01	1.960	R	2.054	R	
		0.031	0.960	0.189	0.008	8.62	1.960	R	2.054	R	
		0.034	0.960	0.160	0.008	8.03	1.960	R	2.054	R	
		0.037	0.960	0.125	0.008	8.26	1.960	R	2.054	R	
		0.040	0.960	0.100	0.007	4.72	1.960	R	2.054	R	
0.005	0.05	0.005	0.960	0.982	0.004	7.00	1.960	R	2.054	R	
		0.008	0.960	0.901	0.006	8.03	1.960	R	2.054	R	
		0.011	0.960	0.812	0.008	7.48	1.960	R	2.054	R	

Table VII - OC CURVE TESTING , PLAN SET I  
 (h1-1) ACCEPTANCE RULE

	0.014	0.725	0.795	0.910	7.27	1.000	R	2.054	R
	0.017	0.840	0.705	0.910	8.24	1.000	R	2.054	R
	0.020	0.853	0.627	0.911	7.39	1.000	R	2.054	R
	0.025	0.499	0.552	0.911	7.10	1.000	R	2.054	R
	0.028	0.398	0.493	0.911	6.45	1.000	R	2.054	R
	0.030	0.330	0.423	0.911	6.87	1.000	R	2.054	R
	0.032	0.288	0.345	0.910	6.42	1.000	R	2.054	R
	0.035	0.241	0.298	0.910	6.49	1.000	R	2.054	R
	0.038	0.203	0.260	0.909	6.01	1.000	R	2.054	R
	0.041	0.171	0.191	0.909	7.32	1.000	R	2.054	R
	0.044	0.142	0.153	0.908	7.61	1.000	R	2.054	R
	0.047	0.119	0.153	0.908	7.84	1.000	Accord1	2.054	R
	0.050	0.100	0.991	0.908	-1.37	1.000	Accord1	2.054	R
0.005	0.06	0.005	0.560	0.976	0.04	1.000	R	2.054	R
	0.009	0.078	0.938	0.992	7.00	1.000	R	2.054	R
	0.012	0.788	0.898	0.992	6.44	1.000	R	2.054	R
	0.017	0.492	0.775	0.910	8.08	1.000	R	2.054	R
	0.021	0.600	0.579	0.911	8.08	1.000	R	2.054	R
	0.025	0.492	0.627	0.911	8.08	1.000	R	2.054	R
	0.028	0.422	0.615	0.911	8.21	1.000	R	2.054	R
	0.030	0.252	0.432	0.911	8.08	1.000	R	2.054	R
	0.037	0.293	0.371	0.911	7.20	1.000	R	2.054	R
	0.041	0.148	0.295	0.910	4.12	1.000	R	2.054	R
	0.045	0.202	0.224	0.909	8.08	1.000	R	2.054	R
	0.048	0.187	0.153	0.909	8.08	1.000	R	2.054	R
	0.053	0.137	0.153	0.909	8.08	1.000	R	2.054	R
	0.037	0.116	0.115	0.907	-0.11	1.000	Accord1	2.054	R
	0.055	0.100	0.998	0.907	-0.37	1.000	Accord1	2.054	R
0.005	0.07	0.005	0.580	0.978	0.06	1.000	R	2.054	R
	0.010	0.866	0.839	0.907	10.00	1.000	R	2.054	R
	0.015	0.787	0.870	0.907	11.92	1.000	R	2.054	R
	0.020	0.589	0.785	0.910	11.84	1.000	R	2.054	R
	0.025	0.589	0.898	0.911	12.42	1.000	R	2.054	R
	0.030	0.582	0.879	0.911	10.27	1.000	R	2.054	R
	0.035	0.387	0.895	0.911	8.71	1.000	R	2.054	R
	0.040	0.121	0.423	0.911	8.47	1.000	R	2.054	R
	0.045	0.289	0.242	0.910	7.29	1.000	R	2.054	R
	0.050	0.116	0.898	0.910	8.08	1.000	R	2.054	R
	0.055	0.121	0.244	0.909	8.08	1.000	R	2.054	R
	0.060	0.148	0.808	0.909	8.08	1.000	R	2.054	R
	0.065	0.121	0.187	0.909	8.04	1.000	R	2.054	R
	0.070	0.100	0.181	0.907	8.24	1.000	R	2.054	R

Table VIII - DATA OUTPUT PLAN SET II

## (h1-1) ACCEPTANCE RULE

P1	P2	Pn	NOD	ABN(Pn)	Plan 02		Mean CI (+/-)	Accept # Pn	% Loss Accepted	# Times Accepted	Ave Plan 02
					Mean F Unrected	Std Dev # Unrected					
0.01	0.02	0.010	714	817	218.5	121.4	5.0	0.950	0.084	14.8	0.916
		0.012		882	247.8	159.1	7.0	0.988	0.010	27	0.927
		0.014		871	271.0	176.2	7.7	0.912	0.030	20	0.938
		0.016		895	292.7	180.3	5.0	0.794	0.717	77.5	0.978
		0.018		882	297.1	188.2	5.7	0.881	0.822	22.8	0.984
		0.020		898	297.0	200.0	5.0	0.498	0.485	20	0.980
		0.022		887	291.0	180.5	0.0	0.352	0.335	20	0.984
		0.024		895	292.0	185.2	0.1	0.250	0.285	55.8	0.956
		0.026		822	280.2	179.9	2.0	0.188	0.181	25	0.948
		0.028		199	225.2	181.0	7.1	0.199	0.181	25.5	0.924
		0.030		181	207.0	169.0	4.0	0.100	0.120	25.5	0.921
0.01	0.04	0.010	280	121	120.7	99.6	2.0	0.950	0.988	21	0.921
		0.012		124	156.0	99.6	4.0	0.894	0.901	57	0.957
		0.014		145	166.0	99.6	4.1	0.790	0.860	95	0.986
		0.016		123	192.3	99.6	4.2	0.883	0.888	118	0.918
		0.018		105	181.0	161.0	4.0	0.849	0.579	129.5	0.130
		0.020		105	181.0	161.2	4.0	0.436	0.454	121.5	0.130
		0.022		105	151.0	99.6	4.0	0.325	0.359	95	0.995
		0.024		123	140.6	99.6	4.0	0.260	0.261	78.5	0.979
		0.026		112	127.3	99.6	4.0	0.185	0.208	58.5	0.952
		0.028		102	118.2	99.6	4.0	0.137	0.147	90	0.940
		0.030		82	107.0	79.2	1.5	0.100	0.101	24	0.924
0.01	0.05	0.010	215	81	95.2	48.2	2.0	0.950	0.954	49.5	0.950
		0.012		88	90.0	49.1	2.2	0.900	0.928	64.5	0.965
		0.014		92	97.2	84.8	2.4	0.828	0.883	101.5	0.102
		0.016		94	102.7	67.9	2.5	0.743	0.799	124.5	0.125
		0.018		97	104.1	60.0	2.7	0.554	0.719	129.5	0.129
		0.020		98	105.0	61.5	2.7	0.583	0.614	137	0.137
		0.022		99	102.8	62.2	2.7	0.467	0.614	125.5	0.126
		0.024		91	98.5	62.0	2.7	0.287	0.424	122.5	0.122
		0.026		90	85.9	60.7	2.7	0.203	0.258	92	0.102
		0.028		90	90.7	60.9	2.8	0.254	0.291	63.5	0.984
		0.030		75	85.0	60.1	2.5	0.203	0.223	63.5	0.984
		0.042		71	81.0	66.0	2.5	0.177	0.187	68.5	0.959
		0.044		87	81.1	64.0	2.4	0.154	0.186	66.5	0.947
		0.047		82	78.7	64.0	2.4	0.125	0.142	20	0.938
		0.050		88	70.4	60.5	2.2	0.100	0.110	20.5	0.929
0.01	0.03	0.010	151	80	81.2	30.0	1.0	0.950	0.989	50	0.958
		0.013		82	88.0	35.5	1.0	0.999	0.948	97	0.997
		0.016		80	70.0	30.1	1.7	0.655	0.803	111	0.111

Table VIII - DATA OUTPUT PLAN SET II  
 (h1-1) ACCEPTANCE RULE  
 (CONTINUED)

		0.019	7.0	78.0	42.4	1.0	0.708	0.840	14.0	0.182	
		0.022	7.0	78.0	42.4	1.0	0.711	0.751	16.2	0.182	
		0.025	7.0	78.0	42.4	1.0	0.842	0.885	16.2	0.187	
		0.025	8.0	78.7	42.4	1.0	0.885	0.841	120.5	0.188	
		0.021	7.0	74.0	44.7	2.0	0.488	0.841	157.5	0.188	
		0.020	8.0	73.1	45.2	2.0	0.402	0.429	160.5	0.181	
		0.040	8.0	79.2	30.3	1.0	0.309	0.233	110.5	0.111	
		0.043	8.0	88.1	30.3	1.0	0.294	0.291	182.5	0.104	
		0.048	8.0	88.1	30.3	1.0	0.224	0.247	87.5	0.089	
		0.048	8.0	80.3	41.7	1.0	0.199	0.233	7.5	0.073	
		0.051	8.0	80.3	40.0	1.0	0.187	0.201	8.5	0.069	
		0.054	8.0	86.7	30.3	1.7	0.142	0.184	87.5	0.062	
		0.057	4.1	81.7	30.3	1.0	0.119	0.121	40.5	0.041	
		0.060	4.1	80.2	27.2	1.0	0.100	0.091	21	0.031	
0.01	0.07	0.010	12.3	47	22.5	1.0	0.980	0.989	49.5	0.221	
		0.015	8.0	80.3	20.3	1.0	0.885	0.923	8.5	0.040	
		0.020	8.0	80.3	24.4	1.0	0.788	0.842	110	0.110	
		0.020	8.0	81.2	45.2	1.0	0.790	0.762	110.5	0.110	
		0.020	8.0	80.3	37.2	1.0	0.597	0.841	120.5	0.121	
		0.020	8.0	80.3	30.3	1.7	0.488	0.841	124.5	0.125	
		0.040	8.0	87.0	27.1	1.0	0.399	0.595	102.5	0.104	
		0.043	4.7	84.2	38.9	1.0	0.393	0.389	9.5	0.091	
		0.050	4.2	81.8	28.9	1.0	0.280	0.293	70.5	0.071	
		0.055	4.0	47.9	24.2	1.0	0.192	0.220	8.5	0.062	
		0.060	4.0	44.7	22.1	1.0	0.182	0.187	4.5	0.040	
		0.065	2.3	41.8	32.2	1.4	0.126	0.124	2.0	0.030	
		0.070	2.1	28.2	24.3	1.5	0.100	0.109	2.0	0.020	
0.01	0.08	0.010	8.0	20	40.3	17.0	0.9	0.980	0.976	8.5	0.040
		0.015	4.2	42.2	21.4	0.9	0.892	0.923	110	0.110	
		0.020	4.2	47.0	23.9	1.0	0.898	0.884	170.5	0.177	
		0.025	4.4	48.4	24.6	1.1	0.727	0.795	172.5	0.173	
		0.030	4.6	47.0	25.5	1.1	0.612	0.716	180.5	0.189	
		0.035	4.9	47.1	25.9	1.1	0.643	0.617	170.5	0.177	
		0.040	4.4	98.0	26.2	1.2	0.484	0.524	172	0.172	
		0.045	3.9	44.4	20.7	1.2	0.397	0.489	18.2	0.182	
		0.050	3.7	43.6	27.1	1.2	0.319	0.393	15.7	0.157	
		0.055	3.5	42.1	25.8	1.1	0.241	0.329	12.5	0.125	
		0.060	3.2	38.3	25.2	1.1	0.224	0.274	8.5	0.093	
		0.065	3.0	35.6	25.6	1.1	0.185	0.216	8.5	0.062	
		0.070	3.0	35.6	24.7	1.1	0.151	0.183	70.5	0.071	
		0.075	2.8	32.1	23.5	1.0	0.123	0.120	8.5	0.054	
		0.080	2.6	20.0	22.0	1.0	0.102	0.124	8.5	0.048	

Table IX - ASN TESTING , PLAN SET II

## (h1-1) ACCEPTANCE RULE

P1	P2	P <sub>0</sub>	Mean #	Plan 02		Computed		Ho: $\mu_1 = \mu_2$		Ho: $\mu_1 < \mu_2$	
				ASN(P <sub>0</sub> )	Inspected	Difference	Statistic	t(0.05)	Ha: $\mu_1 < \mu_2$	t(0.01)	Ha: $\mu_1 < \mu_2$
0.01	0.03	0.010	217	216.5		-0.26	-0.09	-1.646	Accept	-2.328	Acc.
		0.012	245	247.5		2.02	0.57	-1.646	Accept	-2.328	Acc.
		0.014	271	271.6		0.77	0.19	-1.646	Accept	-2.328	Acc.
		0.016	295	292.7		-2.27	-0.53	-1.646	Accept	-2.328	Acc.
		0.018	363	297.1		-65.43	-14.76	-1.646	R	-2.328	R
		0.020	298	297.8		-0.54	-0.12	-1.646	Accept	-2.328	Acc.
		0.022	257	291.6		34.75	7.81	-1.646	Accept	-2.328	Acc.
		0.024	250	262.0		12.37	2.99	-1.646	Accept	-2.328	Acc.
		0.026	222	250.2		28.26	7.02	-1.646	Accept	-2.328	Acc.
		0.028	199	225.2		25.75	7.11	-1.646	Accept	-2.328	Acc.
		0.030	181	207.9		26.85	7.60	-1.646	Accept	-2.328	Acc.
0.01	0.04	0.010	121	120.7		0.15	0.10	-1.646	Accept	-2.328	Acc.
		0.013	134	138.0		3.56	1.95	-1.646	Accept	-2.328	Acc.
		0.016	145	155.0		9.81	4.73	-1.646	Accept	-2.328	Acc.
		0.019	182	163.3		1.02	0.46	-1.646	Accept	-2.328	Acc.
		0.022	185	164.9		0.05	0.02	-1.646	Accept	-2.328	Acc.
		0.025	150	161.0		11.02	4.87	-1.646	Accept	-2.328	Acc.
		0.028	138	151.6		13.95	6.33	-1.646	Accept	-2.328	Acc.
		0.031	123	140.6		17.99	8.31	-1.646	Accept	-2.328	Acc.
		0.034	112	127.3		15.22	7.50	-1.646	Accept	-2.328	Acc.
		0.037	102	118.2		16.70	8.66	-1.646	Accept	-2.328	Acc.
		0.040	92	107.6		15.41	8.70	-1.646	Accept	-2.328	Acc.
0.01	0.05	0.010	81	85.2		4.13	4.00	-1.646	Accept	-2.328	Acc.
		0.013	88	90.8		2.59	2.36	-1.646	Accept	-2.328	Acc.
		0.016	92	97.2		4.76	3.89	-1.646	Accept	-2.328	Acc.
		0.019	94	102.7		8.31	6.42	-1.646	Accept	-2.328	Acc.
		0.022	97	104.1		7.46	5.50	-1.646	Accept	-2.328	Acc.
		0.025	98	105.0		7.03	5.11	-1.646	Accept	-2.328	Acc.
		0.028	99	102.8		3.88	2.65	-1.646	Accept	-2.328	Acc.
		0.031	91	99.5		8.35	6.02	-1.646	Accept	-2.328	Acc.
		0.034	90	98.9		6.93	5.11	-1.646	Accept	-2.328	Acc.
		0.037	80	90.7		10.39	7.89	-1.646	Accept	-2.328	Acc.
		0.040	75	85.6		10.63	8.19	-1.646	Accept	-2.328	Acc.
		0.042	71	81.6		10.69	8.40	-1.646	Accept	-2.328	Acc.
		0.044	67	81.1		13.77	11.23	-1.646	Accept	-2.328	Acc.
		0.047	62	75.7		13.26	10.86	-1.646	Accept	-2.328	Acc.
		0.050	58	70.4		12.35	10.93	-1.646	Accept	-2.328	Acc.
0.01	0.06	0.010	60	61.2		0.96	1.40	-1.646	Accept	-2.328	Acc.
		0.013	63	68.0		5.40	6.80	-1.646	Accept	-2.328	Acc.
		0.016	68	70.6		2.77	3.25	-1.646	Accept	-2.328	Acc.

Table IX - ASN TESTING , PLAN SET II  
 (h1-1) ACCEPTANCE RULE  
 (CONTINUED)

0.019	70	74.8	4.83	5.32	-1.646	Accept	-2.328	Acc.		
0.022	72	75.8	3.80	4.00	-1.646	Accept	-2.328	Acc.		
0.025	76	75.4	-0.62	-0.64	-1.646	Accept	-2.328	Acc.		
0.028	80	75.7	-4.75	-4.84	-1.646	R	-2.328	R		
0.031	76	74.6	-1.39	-1.39	-1.646	Accept	-2.328	Acc.		
0.035	65	73.1	7.80	7.72	-1.646	Accept	-2.328	Acc.		
0.040	60	70.2	10.29	10.47	-1.646	Accept	-2.328	Acc.		
0.043	56	66.1	9.66	9.85	-1.646	Accept	-2.328	Acc.		
0.046	53	63.7	10.42	10.79	-1.646	Accept	-2.328	- Acc.		
0.049	51	60.4	9.53	10.21	-1.646	Accept	-2.328	Acc.		
0.051	49	58.4	9.81	10.73	-1.646	Accept	-2.328	Acc.		
0.054	46	55.7	9.94	11.18	-1.646	Accept	-2.328	Acc.		
0.057	43	51.7	8.49	9.93	-1.646	Accept	-2.328	Acc.		
0.060	41	48.0	7.05	8.47	-1.646	Accept	-2.328	Acc.		
0.01	0.07	0.010	47	49.1	1.82	3.08	-1.646	Accept	-2.328	Acc.
		0.015	52	55.9	4.14	6.11	-1.646	Accept	-2.328	Acc.
		0.020	55	60.3	5.29	6.88	-1.646	Accept	-2.328	Acc.
		0.025	58	61.3	3.16	3.94	-1.646	Accept	-2.328	Acc.
		0.030	57	62.2	5.40	6.44	-1.646	Accept	-2.328	Acc.
		0.035	55	60.4	5.39	6.33	-1.646	Accept	-2.328	Acc.
		0.040	49	57.8	8.55	10.32	-1.646	Accept	-2.328	Acc.
		0.045	47	54.2	6.87	8.32	-1.646	Accept	-2.328	Acc.
		0.050	43	51.5	8.87	10.89	-1.646	Accept	-2.328	Acc.
		0.055	39	47.6	8.18	10.70	-1.646	Accept	-2.328	Acc.
		0.060	36	44.7	8.72	11.78	-1.646	Accept	-2.328	Acc.
		0.065	33	41.9	8.41	11.84	-1.646	Accept	-2.328	Acc.
		0.070	31	38.3	7.40	9.85	-1.646	Accept	-2.328	Acc.
0.01	0.08	0.010	39	40.3	1.27	3.18	-1.646	Accept	-2.328	Acc.
		0.015	42	43.2	1.38	2.89	-1.646	Accept	-2.328	Acc.
		0.020	42	47.6	5.44	10.18	-1.646	Accept	-2.328	Acc.
		0.025	44	46.4	2.43	4.42	-1.646	Accept	-2.328	Acc.
		0.030	46	47.9	1.90	3.34	-1.646	Accept	-2.328	Acc.
		0.035	49	47.1	-1.72	-2.98	-1.646	R	-2.328	Acc.
		0.040	44	45.6	1.72	2.93	-1.646	Accept	-2.328	Acc.
		0.045	39	44.4	5.89	9.53	-1.646	Accept	-2.328	Acc.
		0.050	37	43.6	6.76	11.15	-1.646	Accept	-2.328	Acc.
		0.055	35	42.1	7.07	12.24	-1.646	Accept	-2.328	Acc.
		0.060	32	38.3	6.85	11.78	-1.646	Accept	-2.328	Acc.
		0.065	30	36.6	6.99	12.25	-1.646	Accept	-2.328	Acc.
		0.070	28	35.5	7.72	13.97	-1.646	Accept	-2.328	Acc.
		0.075	26	32.1	6.02	11.45	-1.646	Accept	-2.328	Acc.
		0.080	25	29.8	5.24	10.84	-1.646	Accept	-2.328	Acc.

Table X - OC CURVE TESTING , PLAN SET II  
 (h1-1) ACCEPTANCE RULE

P1	P2	P0	PLAN 02		Z	Z(0.05)	Mo: P1 = P2	Z(0.02)	Mo: P1 = P2	
			AccordI	% LCRD						
			@ P0	AccordI@P0						
			P2	P1						
0.01	0.02	0.010	0.850	0.984	0.005	3.09	1.980	R	2.054	R
		0.012	0.895	0.918	0.007	2.18	1.980	R	2.054	R
		0.014	0.912	0.830	0.009	2.08	1.980	R	2.054	R
		0.016	0.706	0.737	0.010	2.12	1.980	R	2.054	R
		0.018	0.581	0.592	0.011	0.95	1.980	AccordI	2.054	AccordI
		0.020	0.449	0.485	0.011	2.21	1.980	R	2.054	R
		0.022	0.252	0.235	0.011	-1.00	1.980	AccordI	2.054	AccordI
		0.024	0.250	0.265	0.010	1.85	1.980	AccordI	2.054	AccordI
		0.026	0.188	0.191	0.009	0.32	1.980	AccordI	2.054	AccordI
		0.028	0.139	0.151	0.009	1.40	1.980	AccordI	2.054	AccordI
		0.030	0.100	0.120	0.007	2.95	1.980	R	2.054	AccordI
0.01	0.04	0.010	0.850	0.988	0.004	4.05	1.980	R	2.054	R
		0.013	0.884	0.901	0.007	2.38	1.980	R	2.054	R
		0.016	0.790	0.800	0.009	1.98	1.980	AccordI	2.054	AccordI
		0.019	0.683	0.694	0.010	0.07	1.980	AccordI	2.054	AccordI
		0.022	0.599	0.579	0.011	2.62	1.980	R	2.054	R
		0.025	0.426	0.454	0.011	1.85	1.980	AccordI	2.054	AccordI
		0.028	0.325	0.359	0.011	2.18	1.980	R	2.054	R
		0.031	0.250	0.261	0.010	1.10	1.980	AccordI	2.054	AccordI
		0.034	0.199	0.203	0.009	2.04	1.980	R	2.054	AccordI
		0.037	0.137	0.147	0.009	1.10	1.980	AccordI	2.054	AccordI
		0.040	0.100	0.101	0.007	0.07	1.980	AccordI	2.054	AccordI
0.01	0.05	0.010	0.850	0.984	0.005	0.84	1.980	AccordI	2.054	AccordI
		0.013	0.900	0.920	0.008	4.40	1.980	R	2.054	R
		0.016	0.828	0.863	0.008	4.32	1.980	R	2.054	R
		0.019	0.742	0.789	0.009	4.00	1.980	R	2.054	R
		0.022	0.654	0.719	0.010	0.18	1.980	R	2.054	R
		0.025	0.563	0.614	0.011	4.61	1.980	R	2.054	R
		0.028	0.467	0.514	0.011	4.17	1.980	R	2.054	R
		0.031	0.387	0.424	0.011	2.31	1.980	R	2.054	R
		0.034	0.302	0.358	0.011	5.10	1.980	R	2.054	R
		0.037	0.254	0.281	0.010	2.84	1.980	R	2.054	R
		0.040	0.203	0.223	0.009	2.10	1.980	R	2.054	R
		0.042	0.177	0.187	0.009	1.11	1.980	AccordI	2.054	AccordI
		0.044	0.154	0.168	0.008	1.38	1.980	AccordI	2.054	AccordI
		0.047	0.126	0.142	0.008	2.23	1.980	R	2.054	R
		0.050	0.100	0.119	0.007	2.72	1.980	R	2.054	R
0.01	0.06	0.010	0.850	0.989	0.004	4.31	1.980	R	2.054	R
		0.013	0.899	0.949	0.006	0.21	1.980	R	2.054	R
		0.016	0.856	0.893	0.007	5.18	1.980	R	2.054	R

Table X - OC CURVE TESTING , PLAN SET II

## (h1-1) ACCEPTANCE RULE

		0.019	0.786	0.840	0.009	8.16	1.000	R	2.054	R
		0.022	0.711	0.751	0.010	4.02	1.000	R	2.054	R
		0.025	0.643	0.685	0.011	4.02	1.000	R	2.054	R
		0.028	0.585	0.601	0.011	2.19	1.000	R	2.054	R
		0.031	0.498	0.547	0.011	8.43	1.000	R	2.054	R
		0.035	0.402	0.429	0.011	2.44	1.000	R	2.054	R
		0.040	0.309	0.358	0.011	4.88	1.000	R	2.054	R
		0.043	0.264	0.291	0.010	2.87	1.000	R	2.054	R
		0.046	0.224	0.247	0.009	8.42	1.000	R	2.054	R
		0.049	0.185	0.233	0.009	8.20	1.000	R	2.054	R
		0.051	0.167	0.201	0.009	2.85	1.000	R	2.054	R
		0.054	0.142	0.184	0.008	2.62	1.000	R	2.054	R
		0.057	0.119	0.121	0.007	8.14	1.000	Accord1	2.054	Accord1
		0.060	0.100	0.091	0.007	-1.37	1.000	Accord1	2.054	Accord1
0.01	0.07	0.010	0.950	0.969	0.004	4.31	1.000	R	2.054	R
		0.015	0.885	0.923	0.007	8.83	1.000	R	2.054	R
		0.020	0.780	0.842	0.008	8.48	1.000	R	2.054	R
		0.025	0.700	0.782	0.010	8.19	1.000	R	2.054	R
		0.030	0.587	0.641	0.011	4.98	1.000	R	2.054	R
		0.035	0.488	0.541	0.011	4.94	1.000	R	2.054	R
		0.040	0.383	0.455	0.011	8.80	1.000	R	2.054	R
		0.045	0.309	0.399	0.011	8.85	1.000	R	2.054	R
		0.050	0.250	0.292	0.010	2.31	1.000	R	2.054	R
		0.055	0.199	0.226	0.009	2.91	1.000	R	2.054	R
		0.060	0.162	0.167	0.008	8.51	1.000	Accord1	2.054	Accord1
		0.065	0.128	0.124	0.008	1.92	1.000	Accord1	2.054	Accord1
		0.070	0.100	0.109	0.007	1.82	1.000	Accord1	2.054	Accord1
0.01	0.08	0.010	0.950	0.976	0.004	8.02	1.000	R	2.054	R
		0.015	0.892	0.923	0.006	4.76	1.000	R	2.054	R
		0.020	0.808	0.864	0.008	8.75	1.000	R	2.054	R
		0.025	0.727	0.795	0.010	7.08	1.000	R	2.054	R
		0.030	0.613	0.716	0.011	8.74	1.000	R	2.054	R
		0.035	0.543	0.617	0.011	8.95	1.000	R	2.054	R
		0.040	0.454	0.524	0.011	7.12	1.000	R	2.054	R
		0.045	0.387	0.468	0.011	7.81	1.000	R	2.054	R
		0.050	0.319	0.392	0.011	8.82	1.000	R	2.054	R
		0.055	0.241	0.329	0.010	8.99	1.000	R	2.054	R
		0.060	0.224	0.274	0.010	8.17	1.000	R	2.054	R
		0.065	0.195	0.216	0.009	8.52	1.000	R	2.054	R
		0.070	0.151	0.162	0.009	1.44	1.000	Accord1	2.054	Accord1
		0.075	0.123	0.120	0.007	8.01	1.000	Accord1	2.054	Accord1
		0.080	0.100	0.124	0.007	2.40	1.000	R	2.054	R

Table XI - DATA OUTPUT PLAN SET III

## (h1-1) ACCEPTANCE RULE

P1	P2	Pn	NCO	ABN(Pn)	Plan 03		Mean CI (+ -)	Accept @ Pn	% Loss Accepted	Avg # Times Run	P(max run)
					Mean # Inspected	Bid Dev @ 1000.					
0.015	0.03	0.015	1532	423	424.8	201.4	13.2	0.950	0.947	18.5	0.917
0.016		467		467	468.0	224.3	14.2	0.926	0.912	29.0	0.926
0.018		542		542	544.9	280.5	16.7	0.925	0.906	49.0	0.949
0.020		605		607.3	400.6	17.0	0.929	0.898	54.9	0.954	
0.022		612		603.7	423.3	18.6	0.920	0.898	76.5	0.977	
0.024		680		674.2	408.6	17.0	0.976	0.997	83.0	0.983	
0.026		820		842.1	285.0	18.0	0.945	0.941	49.5	0.947	
0.028		452		429.3	250.1	16.2	0.167	0.184	25.5	0.920	
0.030		403		459.5	238.7	14.0	0.100	0.120	24.0	0.924	
0.015	0.04	0.015	626	188	194.0	124.9	8.5	0.950	0.950	18.5	0.919
0.017		210		213.8	128.3	8.1	0.912	0.917	21.0	0.931	
0.019		230		226.7	183.6	9.7	0.854	0.885	44.0	0.944	
0.022		254		269.2	170.3	7.5	0.739	0.750	78.0	0.976	
0.025		298		277.6	178.9	7.8	0.594	0.608	96.5	0.997	
0.028		250		260.1	178.6	7.0	0.442	0.467	74.5	0.975	
0.031		228		253.7	174.1	7.0	0.312	0.303	66.0	0.988	
0.034		207		223.2	187.5	6.9	0.219	0.229	45.0	0.945	
0.037		188		204.7	149.9	6.5	0.147	0.153	24.0	0.924	
0.040		184		188.0	127.5	6.0	0.100	0.114	19.5	0.920	
0.015	0.05	0.015	371	114	117.2	70.3	3.1	0.950	0.952	18.5	0.919
0.017		123		128.7	80.9	3.8	0.922	0.927	28.0	0.928	
0.019		132		125.8	98.5	2.9	0.884	0.891	49.5	0.947	
0.022		142		147.4	95.2	4.2	0.800	0.832	65.5	0.986	
0.025		149		152.4	87.3	4.3	0.711	0.747	95.0	0.985	
0.028		163		168.2	102.5	4.5	0.612	0.627	85.0	0.995	
0.031		146		157.8	102.4	4.8	0.488	0.520	82.5	0.984	
0.034		125		148.8	102.3	4.5	0.405	0.399	70.0	0.976	
0.037		132		144.2	98.1	4.3	0.314	0.326	67.5	0.988	
0.040		125		126.7	88.7	4.2	0.254	0.259	69.0	0.950	
0.042		110		120.7	91.7	4.0	0.196	0.213	42.5	0.944	
0.044		110		124.8	90.2	4.0	0.171	0.184	31.5	0.932	
0.047		101		116.9	85.9	3.8	0.121	0.144	25.5	0.928	
0.050		82		106.4	77.9	3.4	0.100	0.106	18.0	0.910	
0.015	0.06	0.015	233	79	82.0	49.7	2.0	0.950	0.981	31.5	0.932
0.017		84		87.0	61.7	2.3	0.929	0.942	49.5	0.947	
0.019		89		90.5	84.4	2.4	0.900	0.919	57.0	0.957	
0.022		84		101.5	80.4	2.0	0.839	0.864	82.5	0.984	
0.025		101		103.8	81.9	2.7	0.777	0.794	87.5	0.998	
0.028		103		105.5	82.6	2.0	0.705	0.724	103.5	0.984	
0.031		111		107.8	85.9	2.0	0.612	0.626	113.5	0.914	

Table XI - DATA OUTPUT PLAN SET III

## (h1-1) ACCEPTANCE RULE

	<b>0.034</b>		100	100.4	87.4	2.0	0.624	0.621	122.0	0.122	
	<b>0.037</b>		94	105.0	89.2	2.0	0.448	0.482	118.0	0.111	
	<b>0.040</b>		94	104.2	89.2	2.0	0.375	0.390	118.0	0.110	
	<b>0.043</b>		96	101.6	88.7	2.0	0.314	0.315	108.0	0.106	
	<b>0.046</b>		92	95.8	94.4	2.0	0.259	0.294	91.0	0.091	
	<b>0.049</b>		77	88.7	83.3	2.0	0.211	0.236	88.0	0.089	
	<b>0.051</b>		74	83.8	80.1	2.0	0.185	0.190	81.0	0.051	
	<b>0.054</b>		69	78.6	87.7	2.5	0.151	0.174	49.5	0.041	
	<b>0.057</b>		95	75.1	88.3	2.4	0.122	0.144	22.0	0.032	
	<b>0.060</b>		91	87.0	83.9	2.4	0.100	0.095	27.0	0.027	
<b>0.015</b>	<b>0.07</b>	<b>0.018</b>	178	90	92.4	22.0	1.5	0.950	0.965	21.0	0.022
	<b>0.017</b>		92	98.8	37.1	1.0	0.926	0.947	25.0	0.025	
	<b>0.019</b>		95	99.9	37.1	1.0	0.905	0.924	48.0	0.048	
	<b>0.022</b>		79	72.9	42.3	1.0	0.882	0.892	88.0	0.088	
	<b>0.025</b>		73	78.4	44.1	1.0	0.809	0.836	82.0	0.083	
	<b>0.028</b>		74	78.2	47.0	2.1	0.743	0.765	102.0	0.103	
	<b>0.031</b>		75	82.8	49.0	2.1	0.670	0.721	118.0	0.117	
	<b>0.034</b>		78	82.2	50.5	2.2	0.609	0.651	115.0	0.115	
	<b>0.037</b>		79	81.0	50.2	2.2	0.537	0.587	118.0	0.110	
	<b>0.040</b>		76	78.0	50.9	2.2	0.473	0.510	103.0	0.103	
	<b>0.043</b>		70	60.1	50.0	2.2	0.411	0.452	109.0	0.100	
	<b>0.046</b>		69	76.0	50.1	2.2	0.352	0.360	82.5	0.084	
	<b>0.049</b>		93	72.7	48.0	2.1	0.209	0.231	81.0	0.081	
	<b>0.051</b>		92	78.8	48.6	2.1	0.272	0.287	73.0	0.073	
	<b>0.054</b>		89	89.3	47.6	2.1	0.226	0.247	82.0	0.053	
	<b>0.057</b>		88	82.5	45.5	2.0	0.199	0.223	47.0	0.047	
	<b>0.060</b>		82	81.3	44.0	2.0	0.171	0.171	39.0	0.039	
	<b>0.063</b>		80	80.0	43.0	1.0	0.145	0.149	31.0	0.031	
	<b>0.066</b>		49	87.2	42.6	1.0	0.120	0.123	21.0	0.022	
	<b>0.068</b>		49	82.0	39.6	1.7	0.111	0.117	18.0	0.018	
	<b>0.070</b>		44	82.5	39.5	1.7	0.100	0.111	21.0	0.021	

Table XII - ASN TESTING , PLAN SET III

## (h1-1) ACCEPTANCE RULE

Plan 03				Computed				Ho: $\mu_1 = \mu_2$		Ho: $\mu_1 < \mu_2$	
P1	P2	P <sub>a</sub>	ASN(P <sub>a</sub> )	Inspected	Difference	Statistic	t(0.05)	Ha: $\mu_1 < \mu_2$	t(0.01)	Ha: $\mu_1 < \mu_2$	
0.015	0.03	0.015	423	434.8	11.62	1.72	-1.646	Accept	-2.328	Accept	
		0.015	467	458.0	-9.04	-1.25	-1.646	Accept	-2.328	Accept	
		0.018	542	544.9	3.04	0.36	-1.646	Accept	-2.328	Accept	
		0.020	565	587.3	22.31	2.49	-1.646	Accept	-2.328	Accept	
		0.022	612	603.7	-8.28	-0.87	-1.646	Accept	-2.328	Accept	
		0.024	580	574.3	-5.39	-0.59	-1.646	Accept	-2.328	Accept	
		0.026	530	542.1	11.69	1.35	-1.646	Accept	-2.328	Accept	
		0.028	453	489.3	36.75	4.70	-1.646	Accept	-2.328	Accept	
		0.030	403	459.6	56.96	7.52	-1.646	Accept	-2.328	Accept	
0.015	0.04	0.015	188	194.0	5.49	1.97	-1.646	Accept	-2.328	Accept	
		0.017	210	213.6	4.12	1.33	-1.646	Accept	-2.328	Accept	
		0.019	230	226.7	-3.58	-1.04	-1.646	Accept	-2.328	Accept	
		0.022	254	259.2	5.56	1.46	-1.646	Accept	-2.328	Accept	
		0.025	298	277.6	-20.27	-5.07	-1.646	R	-2.328	R	
		0.028	250	260.1	9.76	2.44	-1.646	Accept	-2.328	Accept	
		0.031	228	253.7	26.04	6.59	-1.646	Accept	-2.328	Accept	
		0.034	207	223.2	15.76	4.48	-1.646	Accept	-2.328	Accept	
		0.037	186	204.7	19.06	5.73	-1.646	Accept	-2.328	Accept	
		0.040	164	186.0	22.29	7.25	-1.646	Accept	-2.328	Accept	
0.015	0.05	0.015	114	117.2	3.24	2.06	-1.646	Accept	-2.328	Accept	
		0.017	123	128.7	5.52	3.05	-1.646	Accept	-2.328	Accept	
		0.019	132	135.8	4.10	2.12	-1.646	Accept	-2.328	Accept	
		0.022	142	147.4	5.01	2.35	-1.646	Accept	-2.328	Accept	
		0.025	149	152.4	3.89	1.70	-1.646	Accept	-2.328	Accept	
		0.028	153	156.2	3.22	1.39	-1.646	Accept	-2.328	Accept	
		0.031	145	157.6	12.93	5.59	-1.646	Accept	-2.328	Accept	
		0.034	135	148.8	13.47	5.89	-1.646	Accept	-2.328	Accept	
		0.037	132	144.2	12.25	5.58	-1.646	Accept	-2.328	Accept	
		0.040	125	136.7	11.73	5.48	-1.646	Accept	-2.328	Accept	
		0.042	119	130.7	11.74	5.73	-1.646	Accept	-2.328	Accept	
		0.044	110	124.8	14.86	7.37	-1.646	Accept	-2.328	Accept	
		0.047	101	116.8	16.11	8.40	-1.646	Accept	-2.328	Accept	
		0.050	92	106.4	13.92	8.00	-1.646	Accept	-2.328	Accept	
0.015	0.06	0.015	79	83.0	3.54	3.38	-1.646	Accept	-2.328	Accept	
		0.017	84	87.8	3.76	3.25	-1.646	Accept	-2.328	Accept	
		0.019	89	90.5	1.09	0.89	-1.646	Accept	-2.328	Accept	
		0.022	94	101.5	7.05	5.86	-1.646	Accept	-2.328	Accept	
		0.025	101	103.2	1.80	1.30	-1.646	Accept	-2.328	Accept	
		0.028	103	105.5	2.30	1.62	-1.646	Accept	-2.328	Accept	
		0.031	111	107.3	-3.33	-2.26	-1.646	R	-2.328	R	

Table XII - ASN TESTING , PLAN SET III

### (h1-1) ACCEPTANCE RULE

(CONTINUED)

Table XIII - OC CURVE TESTING , PLAN SET III  
 (h1-1) ACCEPTANCE RULE

			PLAN 03								
P1	P2	P0	Accordi	% Loss	RE(P)	Z	Z(0.05)	No: P1 = P2	Z(0.02)	No: P1 = P2	
			@P0	Accordi@P0		Mistatistic	+ M -	No: P1 ≠ P2	+ M -	No: P1 ≠ P2	
0.015	0.03	0.015	0.950	0.947	0.005	-0.81	1.980	Accordi	2.054	Accordi	
		0.015	0.928	0.912	0.008	-2.20	1.980	R	2.054	R	
		0.015	2.084	0.608	0.009	-2.48	1.980	R	2.054	R	
		0.025	2.084	0.608	0.011	-0.15	1.980	Accordi	2.054	Accordi	
		0.022	0.950	0.908	0.011	-1.95	1.980	Accordi	2.054	Accordi	
		0.024	0.375	0.397	0.010	1.99	1.980	R	2.054	Accordi	
		0.025	0.245	0.241	0.010	-0.45	1.980	Accordi	2.054	Accordi	
		0.025	0.167	0.184	0.008	1.82	1.980	Accordi	2.054	Accordi	
		0.030	0.100	0.153	0.008	2.88	1.980	R	2.054	R	
0.015	0.04	0.015	2.084	0.952	0.008	-0.19	1.980	Accordi	2.054	Accordi	
		0.017	0.912	0.917	0.008	0.85	1.980	Accordi	2.054	Accordi	
		0.019	0.950	0.698	0.006	1.82	1.980	Accordi	2.054	Accordi	
		0.022	0.730	0.750	0.010	1.82	1.980	Accordi	2.054	Accordi	
		0.025	0.894	0.608	0.010	1.82	1.980	Accordi	2.054	Accordi	
		0.025	0.442	0.397	0.010	2.31	1.980	R	2.054	R	
		0.031	0.310	0.303	0.010	-1.82	1.980	Accordi	2.054	Accordi	
		0.024	0.310	0.229	0.006	1.89	1.980	Accordi	2.054	Accordi	
		0.027	0.167	0.184	0.008	0.72	1.980	Accordi	2.054	Accordi	
		0.040	0.100	0.114	0.006	1.99	1.980	Accordi	2.054	Accordi	
0.015	0.05	0.015	0.950	0.952	0.008	0.21	1.980	Accordi	2.054	Accordi	
		0.017	0.922	0.917	0.006	2.05	1.980	Accordi	2.054	Accordi	
		0.015	2.084	0.601	0.008	2.88	1.980	Accordi	2.054	Accordi	
		0.022	0.908	0.952	0.006	2.05	1.980	R	2.054	R	
		0.025	0.711	0.747	0.010	2.65	1.980	R	2.054	R	
		0.025	0.912	0.627	0.011	1.82	1.980	Accordi	2.054	Accordi	
		0.031	0.499	0.500	0.011	1.95	1.980	Accordi	2.054	Accordi	
		0.024	0.499	0.608	0.010	-0.55	1.980	Accordi	2.054	Accordi	
		0.037	0.314	0.698	0.010	1.15	1.980	Accordi	2.054	Accordi	
		0.040	0.254	0.250	0.010	-0.45	1.980	Accordi	2.054	Accordi	
		0.042	0.196	0.213	0.006	1.52	1.980	Accordi	2.054	Accordi	
		0.044	0.131	0.144	0.009	1.52	1.980	Accordi	2.054	Accordi	
		0.047	0.131	0.144	0.006	1.52	1.980	Accordi	2.054	Accordi	
		0.050	0.100	0.144	0.007	0.81	1.980	Accordi	2.054	Accordi	
0.015	0.06	0.015	0.950	0.901	0.006	2.27	1.980	R	2.054	R	
		0.017	0.920	0.942	0.006	2.09	1.980	R	2.054	R	
		0.019	0.950	0.610	0.006	2.90	1.980	R	2.054	R	
		0.022	0.950	0.698	0.006	2.10	1.980	R	2.054	R	
		0.025	0.777	0.794	0.006	1.82	1.980	Accordi	2.054	Accordi	
		0.026	0.950	0.724	0.012	2.88	1.980	R	2.054	R	
		0.031	0.812	0.828	0.011	1.27	1.980	Accordi	2.054	Accordi	

**Table XIII - OC CURVE TESTING , PLAN SET III**  
**(h1-1) ACCEPTANCE RULE**  
**(CONTINUED)**

	0.034	0.524	0.521	0.011	-0.27	1.000	Accordi	2.054	Accordi
	0.057	0.448	0.492	0.011	1.39	1.000	Accordi	2.054	Accordi
	0.040	0.375	0.390	0.011	1.30	1.000	Accordi	2.054	Accordi
	0.049	0.314	0.245	0.011	2.00	1.000	R	2.054	R
	0.040	0.259	0.299	0.010	2.45	1.000	R	2.054	R
	0.049	0.211	0.236	0.009	2.01	1.000	R	2.054	R
	0.051	0.123	0.290	0.009	0.57	1.000	Accordi	2.054	Accordi
	0.054	0.181	0.174	0.008	2.76	1.000	R	2.054	R
	0.057	0.122	0.144	0.008	2.01	1.000	R	2.054	R
	0.060	0.100	0.095	0.008	-0.76	1.000	Accordi	2.054	Accordi
0.015	0.07	0.018	0.050	0.005	0.21	1.000	R	2.054	R
	0.017	0.020	0.047	0.005	2.78	1.000	R	2.054	R
	0.019	0.005	0.024	0.006	2.08	1.000	R	2.054	R
	0.022	0.003	0.002	0.007	2.02	1.000	R	2.054	R
	0.025	0.006	0.036	0.009	2.23	1.000	R	2.054	R
	0.028	0.743	0.765	0.910	2.27	1.000	R	2.054	R
	0.031	0.678	0.721	0.910	4.17	1.000	R	2.054	R
	0.034	0.609	0.651	0.911	2.04	1.000	R	2.054	R
	0.037	0.537	0.587	0.911	4.48	1.000	R	2.054	R
	0.040	0.473	0.510	0.911	2.95	1.000	R	2.054	R
	0.043	0.411	0.452	0.911	2.09	1.000	R	2.054	R
	0.046	0.352	0.380	0.911	0.66	1.000	Accordi	2.054	Accordi
	0.049	0.309	0.331	0.910	2.14	1.000	R	2.054	R
	0.051	0.273	0.297	0.910	1.38	1.000	Accordi	2.054	Accordi
	0.054	0.230	0.247	0.910	1.96	1.000	Accordi	2.054	Accordi
	0.057	0.199	0.223	0.909	2.53	1.000	R	2.054	R
	0.060	0.171	0.171	0.908	-0.01	1.000	Accordi	2.054	Accordi
	0.063	0.145	0.149	0.908	0.41	1.000	Accordi	2.054	Accordi
	0.066	0.138	0.123	0.908	-2.06	1.000	R	2.054	R
	0.068	0.111	0.117	0.907	0.76	1.000	Accordi	2.054	Accordi
	0.070	0.100	0.111	0.907	1.53	1.000	Accordi	2.054	Accordi

Table XIV - DATA OUTPUT PLAN SET IV  
 (h1-1) ACCEPTANCE RULE

P1	P2	Pa	NCO	ASN(Pa)	Plan 04		Mean Cl (+ -)	Accept @ Pa	% Loss Accepted	Avg # Times Stop Rule	Pilot Rate
					Mean # Inspected	Bd Dev # Inap.					
0.02	0.03	0.020	4182	1020	1036.6	816.1	25.8	0.950	0.934	14.5	0.915
	0.021		1182	1099.8	947.0	27.1	0.907	0.898	18.0	0.919	
	0.022		1210	1209.8	925.5	40.8	0.849	0.830	20.5	0.921	
	0.023		1484	1277.2	1029.1	45.1	0.782	0.720	32.0	0.939	
	0.024		1602	1423.2	1038.9	45.4	0.654	0.630	42.5	0.942	
	0.026		1461	1419.3	1043.5	45.7	0.405	0.403	37.5	0.938	
	0.027		1420	1272.4	1015.3	44.5	0.293	0.204	31.5	0.932	
	0.028		1219	1303.8	988.1	42.3	0.207	0.224	29.0	0.929	
	0.029		1208	1193.8	899.1	29.4	0.139	0.182	17.0	0.918	
	0.030		1073	1151.6	949.3	37.2	0.100	0.138	18.0	0.915	
0.02	0.04	0.020	1148	816	213.0	209.8	8.2	0.950	0.947	8.5	0.999
	0.023		287	285.4	263.4	11.5	0.870	0.874	21.5	0.932	
	0.027		483	423.3	291.5	12.0	0.883	0.702	54.5	0.955	
	0.031		432	495.5	320.1	14.0	0.436	0.454	71.0	0.971	
	0.034		401	432.5	297.9	13.1	0.278	0.324	49.5	0.950	
	0.037		251	378.5	271.2	11.0	0.167	0.171	31.5	0.932	
	0.040		800	325.0	240.2	10.5	0.100	0.108	15.0	0.915	
	0.045		165	189.3	111.3	4.0	0.950	0.948	19.0	0.919	
	0.050		802	206.0	137.1	6.0	0.853	0.851	45.5	0.946	
	0.030		234	224.7	149.0	6.5	0.683	0.674	75.0	0.975	
0.02	0.05	0.020	680	238	225.6	157.1	6.0	0.467	0.481	99.5	0.991
	0.040		204	210.3	147.1	6.4	0.293	0.324	58.0	0.958	
	0.045		172	182.1	137.1	6.0	0.177	0.178	38.5	0.940	
	0.050		146	188.0	121.0	8.2	0.100	0.112	18.0	0.918	
	0.06	0.020	358	108	198.8	67.9	2.0	0.950	0.962	19.5	0.920
	0.025		124	128.4	84.1	3.7	0.870	0.893	47.0	0.947	
	0.030		128	139.6	92.1	4.1	0.762	0.765	98.5	0.999	
	0.035		148	149.7	97.9	4.3	0.612	0.615	89.0	0.980	
	0.040		141	147.7	97.3	4.3	0.454	0.461	89.5	0.979	
	0.045		130	142.1	98.1	4.3	0.310	0.318	79.0	0.979	
0.02	0.06	0.020	114	124.0	88.9	3.8	0.224	0.218	39.0	0.939	
	0.055		101	100.4	78.6	3.4	0.151	0.142	22.0	0.922	
	0.060		89	101.7	78.9	3.4	0.100	0.102	18.5	0.917	
	0.07	0.020	243	78	77.1	46.8	2.1	0.950	0.957	21.0	0.921
	0.026		89	92.8	59.0	2.6	0.870	0.889	83.5	0.954	
	0.032		88	100.9	64.8	2.0	0.762	0.624	85.5	0.989	
	0.038		105	104.8	98.2	2.0	0.610	0.656	109.0	0.100	
	0.044		97	104.0	97.2	2.0	0.467	0.504	95.5	0.949	
	0.050		89	100.7	97.6	2.0	0.341	0.385	99.0	0.980	
	0.055		87	98.3	91.9	2.7	0.250	0.282	48.5	0.942	

Table XIV - DATA OUTPUT PLAN SET IV  
 (h1-1) ACCEPTANCE RULE  
 (CONTINUED)

			0.060	75	85.7	80.7	2.7	0.185	0.205	41.5	0.042
			0.065	80	77.2	81.3	2.5	0.137	0.140	28.5	0.020
			0.070	81	80.0	81.3	2.2	0.100	0.030	14.5	0.015
0.02	0.02	174	0.020	89	81.3	85.7	1.8	0.050	0.059	22.5	0.022
			0.025	85	80.2	80.4	1.9	0.002	0.029	80.5	0.051
			0.030	71	72.0	44.9	2.0	0.031	0.052	86.0	0.006
			0.035	73	78.7	47.9	2.1	0.728	0.705	112.0	0.112
			0.040	80	78.8	48.9	2.1	0.042	0.085	110.5	0.117
			0.045	75	78.8	48.9	2.1	0.030	0.081	100.0	0.100
			0.050	71	70.8	50.8	2.2	0.438	0.476	122.0	0.122
			0.055	67	70.0	48.8	2.1	0.347	0.390	100.5	0.101
			0.060	63	70.5	48.5	2.0	0.272	0.283	71.0	0.071
			0.065	68	80.4	49.2	2.0	0.215	0.217	80.0	0.060
			0.070	84	80.8	42.1	1.9	0.184	0.182	27.5	0.030
			0.075	49	80.4	42.2	1.9	0.121	0.125	22.0	0.032
			0.080	46	82.7	38.8	1.7	0.100	0.102	23.5	0.024
0.02	0.02	137	0.020	47	49.9	26.4	1.2	0.050	0.063	27.5	0.022
			0.025	53	54.9	31.9	1.4	0.097	0.011	80.0	0.050
			0.030	56	50.6	24.5	1.5	0.016	0.056	86.0	0.006
			0.035	60	52.6	27.3	1.6	0.725	0.767	114.5	0.115
			0.040	62	52.8	28.5	1.7	0.618	0.681	127.5	0.120
			0.050	68	54.8	29.4	1.7	0.605	0.650	121.5	0.132
			0.055	65	51.7	29.0	1.7	0.411	0.459	104.0	0.104
			0.060	62	50.7	28.2	1.7	0.325	0.354	91.0	0.091
			0.065	48	55.7	27.5	1.6	0.254	0.277	73.5	0.074
			0.070	44	52.2	25.5	1.6	0.199	0.198	84.0	0.064
			0.080	41	47.4	22.7	1.6	0.164	0.171	44.0	0.044
			0.085	38	44.7	22.4	1.4	0.123	0.124	29.0	0.020
			0.090	25	42.1	29.7	1.3	0.100	0.102	20.5	0.021
0.02	0.1	107	0.020	39	41.6	21.9	1.0	0.050	0.065	22.5	0.040
			0.025	43	40.0	24.9	1.1	0.002	0.040	98.0	0.022
			0.030	46	47.9	27.2	1.2	0.025	0.071	87.0	0.027
			0.035	48	50.7	29.1	1.3	0.752	0.707	121.5	0.122
			0.040	50	51.9	30.9	1.3	0.660	0.710	123.5	0.134
			0.050	54	52.8	31.3	1.4	0.567	0.605	151.0	0.151
			0.055	49	51.1	31.1	1.4	0.480	0.502	138.5	0.132
			0.060	44	50.7	31.1	1.4	0.393	0.437	125.5	0.120
			0.065	42	47.4	30.7	1.3	0.219	0.254	104.5	0.105
			0.070	39	44.7	34.5	1.5	0.259	0.268	74.5	0.075
			0.080	26	42.0	29.0	1.3	0.211	0.222	76.0	0.076
			0.085	24	40.7	27.8	1.2	0.174	0.189	52.5	0.053
			0.090	22	39.0	27.7	1.2	0.145	0.155	52.0	0.053
			0.095	20	38.5	25.5	1.1	0.121	0.122	52.0	0.023
			0.100	28	32.0	24.8	1.1	0.100	0.117	20.5	0.027

Table XV - ASN TESTING , PLAN SET IV  
 (h1-1) ACCEPTANCE RULE

P1	P2	P <sub>a</sub>	Plan 04		Computed		Ho: μ <sub>1</sub> = μ <sub>2</sub>	Ho: μ <sub>1</sub> < μ <sub>2</sub>	t(0.05)	t(0.01)	Ho: μ <sub>1</sub> = μ <sub>2</sub>
			Mean #	ASN(P <sub>a</sub> )	Inspected	Difference	Statistic	t	Ho: μ <sub>1</sub> < μ <sub>2</sub>		
0.02	0.03	0.020	1028	1036.6	8.95	0.49	-1.646	R	-2.328	Accept	Accept
		0.021	1163	1099.8	-63.01	-3.33	-1.646	R	-2.328	R	
		0.022	1316	1208.8	-106.74	-5.16	-1.646	R	-2.328	R	
		0.023	1484	1377.2	-106.82	-4.64	-1.646	R	-2.328	R	
		0.024	1502	1423.2	-78.84	-3.40	-1.646	R	-2.328	-R	
		0.026	1461	1419.3	-41.75	-1.79	-1.646	R	-2.328	Accept	
		0.027	1428	1372.4	-55.68	-2.45	-1.646	R	-2.328	R	
		0.028	1319	1303.8	-15.01	-0.89	-1.646	Accept	-2.328	Accept	
		0.029	1208	1193.8	-14.06	-0.70	-1.646	Accept	-2.328	Accept	
		0.030	1073	1151.5	78.58	4.14	-1.646	Accept	-2.328	Accept	
0.02	0.04	0.020	315	313.0	-1.78	-0.38	-1.646	Accept	-2.328	Accept	
		0.023	387	385.4	-1.76	-0.30	-1.646	Accept	-2.328	Accept	
		0.027	463	423.3	-39.35	-6.04	-1.646	R	-2.328	R	
		0.031	432	465.5	33.13	4.63	-1.646	Accept	-2.328	Accept	
		0.034	401	432.5	31.75	4.77	-1.646	Accept	-2.328	Accept	
		0.037	351	378.5	27.23	4.49	-1.646	Accept	-2.328	Accept	
		0.040	300	325.0	24.87	4.63	-1.646	Accept	-2.328	Accept	
0.02	0.05	0.020	165	169.3	4.57	1.84	-1.646	Accept	-2.328	Accept	
		0.025	202	206.8	4.48	1.46	-1.646	Accept	-2.328	Accept	
		0.030	234	224.7	-9.18	-2.75	-1.646	R	-2.328	R	
		0.035	238	235.6	-2.08	-0.59	-1.646	Accept	-2.328	Accept	
		0.040	204	216.3	14.50	4.41	-1.646	Accept	-2.328	Accept	
		0.045	172	192.1	20.14	6.57	-1.646	Accept	-2.328	Accept	
		0.050	146	168.6	22.15	8.18	-1.646	Accept	-2.328	Accept	
0.02	0.06	0.020	106	109.5	3.35	2.20	-1.646	Accept	-2.328	Accept	
		0.025	124	129.4	5.48	2.81	-1.646	Accept	-2.328	Accept	
		0.030	138	139.6	1.17	0.56	-1.646	Accept	-2.328	Accept	
		0.035	146	149.7	3.88	1.69	-1.646	Accept	-2.328	Accept	
		0.040	141	147.7	6.26	2.88	-1.646	Accept	-2.328	Accept	
		0.045	130	142.1	11.98	5.41	-1.646	Accept	-2.328	Accept	
		0.050	114	124.0	9.93	5.11	-1.646	Accept	-2.328	Accept	
		0.055	101	109.4	8.51	4.85	-1.646	Accept	-2.328	Accept	
		0.060	89	101.7	12.35	7.18	-1.646	Accept	-2.328	Accept	
0.02	0.07	0.020	76	77.1	0.62	0.60	-1.646	Accept	-2.328	Accept	
		0.026	89	92.8	4.06	3.08	-1.646	Accept	-2.328	Accept	
		0.032	98	100.9	3.26	2.25	-1.646	Accept	-2.328	Accept	
		0.038	105	104.8	-0.06	-0.04	-1.646	Accept	-2.328	Accept	
		0.044	97	104.8	7.35	5.03	-1.646	Accept	-2.328	Accept	
		0.050	89	100.7	12.05	7.97	-1.646	Accept	-2.328	Accept	
		0.055	83	88.3	5.13	3.71	-1.646	Accept	-2.328	Accept	

Table XV- ASN TESTING , PLAN SET IV

## (h1-1) ACCEPTANCE RULE

(CONTINUED)

		0.060	7.5	85.7	10.33	7.61	-1.646	Accept	-2.328	Accept
		0.065	6.8	77.2	9.37	7.28	-1.646	Accept	-2.328	Accept
		0.070	6.1	69.0	7.54	6.58	-1.646	Accept	-2.328	Accept
0.02	0.08	0.020	5.9	61.3	2.45	3.07	-1.646	Accept	-2.328	Accept
		0.025	6.5	68.2	2.79	3.08	-1.646	Accept	-2.328	Accept
		0.030	7.1	73.8	3.06	3.05	-1.646	Accept	-2.328	Accept
		0.035	7.3	78.7	5.73	5.35	-1.646	Accept	-2.328	Accept
		0.040	8.0	79.8	-0.16	-0.15	-1.646	Accept	-2.328	Accept
		0.045	7.5	78.8	3.78	3.51	-1.646	Accept	-2.328	Accept
		0.050	7.1	79.6	9.12	8.03	-1.646	Accept	-2.328	Accept
		0.055	6.7	75.0	7.50	6.88	-1.646	Accept	-2.328	Accept
		0.060	6.3	70.5	7.54	7.25	-1.646	Accept	-2.328	Accept
		0.065	5.8	66.4	8.44	8.17	-1.646	Accept	-2.328	Accept
		0.070	5.4	60.8	6.80	7.22	-1.646	Accept	-2.328	Accept
		0.075	4.9	59.4	10.17	10.78	-1.646	Accept	-2.328	Accept
		0.080	4.6	52.7	7.18	8.32	-1.646	Accept	-2.328	Accept
0.02	0.09	0.020	4.7	48.9	1.57	2.66	-1.646	Accept	-2.328	Accept
		0.026	5.3	54.9	2.30	3.24	-1.646	Accept	-2.328	Accept
		0.032	5.6	59.6	3.92	5.08	-1.646	Accept	-2.328	Accept
		0.038	6.0	63.6	4.03	4.83	-1.646	Accept	-2.328	Accept
		0.044	6.2	63.8	1.50	1.70	-1.646	Accept	-2.328	Accept
		0.050	5.8	64.8	6.83	7.75	-1.646	Accept	-2.328	Accept
		0.056	5.5	61.7	6.77	7.77	-1.646	Accept	-2.328	Accept
		0.062	5.2	58.7	6.76	7.93	-1.646	Accept	-2.328	Accept
		0.068	4.8	55.7	7.52	8.97	-1.646	Accept	-2.328	Accept
		0.074	4.4	52.2	7.95	10.03	-1.646	Accept	-2.328	Accept
		0.080	4.1	47.4	6.72	8.92	-1.646	Accept	-2.328	Accept
		0.085	3.8	44.7	6.57	9.07	-1.646	Accept	-2.328	Accept
		0.090	3.5	42.1	6.60	9.94	-1.646	Accept	-2.328	Accept
0.02	0.1	0.020	3.9	41.6	2.18	4.44	-1.646	Accept	-2.328	Accept
		0.026	4.3	46.0	2.96	5.32	-1.646	Accept	-2.328	Accept
		0.032	4.6	47.8	1.85	3.21	-1.646	Accept	-2.328	Accept
		0.038	4.8	50.7	3.00	4.60	-1.646	Accept	-2.328	Accept
		0.044	5.0	51.9	1.88	2.80	-1.646	Accept	-2.328	Accept
		0.050	5.4	52.8	-1.47	-2.10	-1.646	R	-2.328	Accept
		0.056	4.8	51.1	3.11	4.47	-1.646	Accept	-2.328	Accept
		0.062	4.4	50.7	6.52	9.40	-1.646	Accept	-2.328	Accept
		0.068	4.2	47.4	5.34	7.78	-1.646	Accept	-2.328	Accept
		0.074	3.9	44.7	5.48	7.12	-1.646	Accept	-2.328	Accept
		0.080	3.6	42.9	6.57	10.14	-1.646	Accept	-2.328	Accept
		0.085	3.4	40.7	8.28	10.11	-1.646	Accept	-2.328	Accept
		0.090	3.2	39.0	6.65	10.74	-1.646	Accept	-2.328	Accept
		0.095	3.0	36.5	6.06	10.60	-1.646	Accept	-2.328	Accept
		0.100	2.9	33.8	5.12	9.32	-1.646	Accept	-2.328	Accept

Table XVI - OC CURVE TESTING , PLAN SET IV  
 (h1-1) ACCEPTANCE RULE

			PLAN 04										
P1	P2	P0	Accord1	% Loss	SE(P)	Z	Z(0.05)	H0: P1 = P2	Z(0.02)	H0: P1 < P2	H0: P1 > P2		
			P2	P1		Statistic	+ or -	H0: P1 < P2		H0: P1 > P2			
0.02	0.02	0.020	0.950	0.934	0.005	-2.06	1.960	R	2.054	R			
		0.021	0.907	0.998	0.007	-1.44	1.960	Accord1	2.054	Accord1			
		0.022	0.848	0.920	0.008	-1.95	1.960	Accord1	2.054	Accord1			
		0.023	0.782	0.728	0.010	-2.44	1.960	R	2.054	R			
		0.024	0.654	0.828	0.011	-1.64	1.960	Accord1	2.054	Accord1			
		0.025	0.405	0.403	0.011	-0.10	1.960	Accord1	2.054	Accord1			
		0.027	0.293	0.204	0.010	1.00	1.960	Accord1	2.054	Accord1			
		0.028	0.207	0.224	0.009	1.77	1.960	Accord1	2.054	Accord1			
		0.029	0.139	0.182	0.008	2.12	1.960	R	2.054	Accord1			
		0.030	0.100	0.120	0.007	2.25	1.960	R	2.054	R			
0.02	0.04	0.020	0.950	0.947	0.005	-0.81	1.960	Accord1	2.054	Accord1			
		0.023	0.878	0.874	0.007	-0.05	1.960	Accord1	2.054	Accord1			
		0.027	0.683	0.702	0.010	1.75	1.960	Accord1	2.054	Accord1			
		0.031	0.436	0.454	0.011	1.05	1.960	Accord1	2.054	Accord1			
		0.034	0.278	0.224	0.010	4.42	1.960	R	2.054	R			
		0.037	0.167	0.171	0.008	0.40	1.960	Accord1	2.054	Accord1			
		0.040	0.100	0.108	0.007	1.10	1.960	Accord1	2.054	Accord1			
0.02	0.05	0.020	0.950	0.948	0.005	-0.51	1.960	Accord1	2.054	Accord1			
		0.025	0.853	0.851	0.008	-0.21	1.960	Accord1	2.054	Accord1			
		0.030	0.683	0.674	0.010	-0.90	1.960	Accord1	2.054	Accord1			
		0.035	0.487	0.481	0.011	1.26	1.960	Accord1	2.054	Accord1			
		0.040	0.293	0.324	0.010	2.02	1.960	R	2.054	R			
		0.045	0.177	0.178	0.009	0.01	1.960	Accord1	2.054	Accord1			
		0.050	0.100	0.112	0.007	1.67	1.960	Accord1	2.054	Accord1			
0.02	0.06	0.020	0.950	0.952	0.005	2.60	1.960	R	2.054	R			
		0.025	0.878	0.893	0.007	2.07	1.960	R	2.054	R			
		0.030	0.762	0.765	0.009	0.27	1.960	Accord1	2.054	Accord1			
		0.035	0.612	0.615	0.011	0.21	1.960	Accord1	2.054	Accord1			
		0.040	0.454	0.491	0.011	0.65	1.960	Accord1	2.054	Accord1			
		0.045	0.318	0.319	0.010	-0.03	1.960	Accord1	2.054	Accord1			
		0.050	0.224	0.218	0.009	-0.80	1.960	Accord1	2.054	Accord1			
		0.055	0.151	0.142	0.008	-1.17	1.960	Accord1	2.054	Accord1			
		0.060	0.100	0.102	0.007	0.30	1.960	Accord1	2.054	Accord1			
0.02	0.07	0.020	0.950	0.957	0.005	1.38	1.960	Accord1	2.054	Accord1			
		0.025	0.878	0.880	0.007	1.42	1.960	Accord1	2.054	Accord1			
		0.032	0.782	0.924	0.010	-12.42	1.960	R	2.054	R			
		0.038	0.618	0.950	0.011	2.61	1.960	R	2.054	R			
		0.044	0.487	0.504	0.011	2.20	1.960	R	2.054	R			
		0.050	0.341	0.385	0.011	2.18	1.960	R	2.054	R			
		0.055	0.250	0.282	0.010	2.21	1.960	R	2.054	R			

Table XVI - OC CURVE TESTING , PLAN SET IV  
 (h1-1) ACCEPTANCE RULE  
 (CONTINUED)

		0.060	0.100	0.052	0.009	2.70	1.000	R	2.054	R
		0.055	0.137	0.140	0.009	0.14	1.000	Accept	2.054	Accept
		0.070	0.100	0.080	0.009	-1.53	1.000	Accept	2.054	Accept
	0.02	0.08	0.020	0.052	0.009	1.03	1.000	Accept	2.054	Accept
		0.025	0.002	0.029	0.009	4.21	1.000	R	2.054	R
		0.020	0.031	0.052	0.009	2.52	1.000	R	2.054	R
		0.035	0.728	0.765	0.010	2.79	1.000	R	2.054	R
		0.040	0.842	0.885	0.011	4.02	1.000	R	2.054	R
		0.055	0.886	0.881	0.011	2.79	1.000	R	2.054	R
		0.050	0.426	0.476	0.011	2.06	1.000	R	2.054	R
		0.055	0.347	0.385	0.011	2.06	1.000	R	2.054	R
		0.060	0.272	0.252	0.010	2.06	1.000	Accept	2.054	Accept
		0.060	0.272	0.217	0.009	0.14	1.000	Accept	2.054	Accept
		0.070	0.184	0.182	0.009	-0.29	1.000	Accept	2.054	Accept
		0.075	0.131	0.125	0.007	-0.09	1.000	Accept	2.054	Accept
		0.080	0.100	0.102	0.007	2.06	1.000	Accept	2.054	Accept
0.02	0.08	0.020	0.050	0.063	0.005	2.05	1.000	R	2.054	R
		0.020	0.007	0.011	0.009	2.07	1.000	R	2.054	R
		0.032	0.016	0.052	0.009	2.06	1.000	R	2.054	R
		0.068	0.725	0.767	0.010	2.06	1.000	R	2.054	R
		0.044	0.816	0.861	0.011	2.06	1.000	R	2.054	R
		0.050	0.605	0.559	0.011	4.05	1.000	R	2.054	R
		0.056	0.411	0.459	0.011	4.22	1.000	R	2.054	R
		0.062	0.325	0.354	0.011	2.72	1.000	R	2.054	R
		0.068	0.264	0.277	0.010	2.20	1.000	R	2.054	R
		0.074	0.199	0.186	0.009	-0.29	1.000	Accept	2.054	Accept
		0.080	0.154	0.171	0.008	1.05	1.000	Accept	2.054	Accept
		0.085	0.123	0.124	0.007	0.03	1.000	Accept	2.054	Accept
		0.090	0.100	0.102	0.007	0.30	1.000	Accept	2.054	Accept
0.02	0.1	0.020	0.050	0.065	0.005	2.33	1.000	R	2.054	R
		0.026	0.002	0.040	0.006	0.18	1.000	R	2.054	R
		0.032	0.035	0.071	0.008	4.46	1.000	R	2.054	R
		0.038	0.753	0.787	0.009	2.59	1.000	R	2.054	R
		0.044	0.860	0.710	0.010	4.78	1.000	R	2.054	R
		0.050	0.807	0.805	0.011	2.44	1.000	R	2.054	R
		0.056	0.480	0.502	0.011	1.07	1.000	R	2.054	Accept
		0.062	0.392	0.437	0.011	3.99	1.000	R	2.054	R
		0.068	0.319	0.354	0.011	3.24	1.000	R	2.054	R
		0.074	0.259	0.268	0.010	0.86	1.000	Accept	2.054	Accept
		0.080	0.211	0.222	0.009	1.17	1.000	Accept	2.054	Accept
		0.085	0.174	0.189	0.009	1.75	1.000	Accept	2.054	Accept
		0.090	0.145	0.155	0.009	1.16	1.000	Accept	2.054	Accept
		0.095	0.121	0.132	0.007	1.45	1.000	Accept	2.054	Accept
		0.100	0.100	0.117	0.007	2.27	1.000	R	2.054	R

**Table XVII - OC TESTING , PLAN SET I**  
**EXTENDED (h1-1) ACCEPTANCE RULE**

P1	P2	Pe	Accept @ Pe	NTP	Tuncation			Tuncation		
					M=1	Pr(acc) Hold @ Actual	Pr(acc) NTP	M=1	Pr(acc) Hold @ Actual	
0.005	0.01	0.005	0.850	4805	4346	0.912	0.909	4352	0.928	
		0.006	0.828	4805	4346	0.786	0.754	4352	0.826	
		0.007	0.824	4805	4346	0.573	0.569	4352	0.607	
		0.008	0.375	4805	4346	0.406	0.404	4352	0.439	
		0.009	0.203	4805	4846	0.208	0.209	4352	0.247	
		0.010	0.100	4805	4346	0.121	0.119	4352	0.134	
		0.005	0.006	702	830	0.900	0.826	579	0.085	
0.005	0.02	0.008	0.795	702	830	0.785	0.792	579	0.760	
		0.010	0.637	702	830	0.648	0.688	579	0.686	
		0.012	0.467	702	830	0.470	0.497	579	0.429	
		0.014	0.330	702	830	0.363	0.373	579	0.339	
		0.016	0.224	702	830	0.267	0.286	579	0.252	
		0.018	0.148	702	830	0.173	0.175	579	0.185	
		0.020	0.100	702	830	0.128	0.122	579	0.115	
0.005	0.03	0.005	0.850	375	163	0.852	0.856	218	0.924	
		0.007	0.892	375	163	0.892	0.824	218	0.869	
		0.010	0.767	375	163	0.757	0.766	218	0.715	
		0.013	0.609	375	163	0.646	0.850	218	0.650	
		0.016	0.467	375	163	0.623	0.615	218	0.424	
		0.019	0.341	375	163	0.442	0.405	218	0.329	
		0.022	0.245	375	163	0.343	0.268	218	0.240	
		0.025	0.179	375	163	0.257	0.213	218	0.169	
		0.028	0.129	375	163	0.189	0.141	218	0.114	
		0.030	0.100	375	163	0.175	0.120	218	0.109	
0.005	0.04	0.005	0.850	182	71	0.860	0.977	116	0.889	
		0.007	0.805	182	71	0.811	0.931	116	0.845	
		0.010	0.812	182	71	0.847	0.861	116	0.756	
		0.013	0.708	182	71	0.773	0.781	116	0.624	
		0.016	0.594	182	71	0.887	0.861	116	0.530	
		0.019	0.492	182	71	0.842	0.810	116	0.425	
		0.022	0.399	182	71	0.548	0.471	116	0.337	
		0.025	0.319	182	71	0.460	0.386	116	0.276	
		0.028	0.254	182	71	0.419	0.333	116	0.252	
		0.031	0.199	182	71	0.289	0.250	116	0.182	
		0.034	0.159	182	71	0.205	0.195	116	0.152	
0.005	0.05	0.037	0.125	182	71	0.262	0.149	116	0.145	
		0.040	0.100	182	71	0.221	0.129	116	0.111	
		0.005	0.850	151	76	0.865	0.881	86	0.843	
		0.008	0.891	151	76	0.881	0.833	86	0.843	
		0.011	0.081	151	76	0.015	0.073	86	0.059	

Table XVII - OC TESTING , PLAN SET I  
EXTENDED (h<sub>1</sub>-1) ACCEPTANCE RULE  
(CONTINUED)

		<b>0.014</b>	<b>0.725</b>	<b>151</b>	<b>76</b>	<b>0.697</b>	<b>0.774</b>	<b>86</b>	<b>0.767</b>
		<b>0.017</b>	<b>0.640</b>	<b>151</b>	<b>76</b>	<b>0.659</b>	<b>0.708</b>	<b>86</b>	<b>0.671</b>
		<b>0.020</b>	<b>0.553</b>	<b>151</b>	<b>76</b>	<b>0.676</b>	<b>0.644</b>	<b>86</b>	<b>0.693</b>
		<b>0.023</b>	<b>0.473</b>	<b>151</b>	<b>76</b>	<b>0.634</b>	<b>0.574</b>	<b>86</b>	<b>0.625</b>
		<b>0.026</b>	<b>0.399</b>	<b>151</b>	<b>76</b>	<b>0.470</b>	<b>0.401</b>	<b>86</b>	<b>0.445</b>
		<b>0.029</b>	<b>0.320</b>	<b>151</b>	<b>76</b>	<b>0.400</b>	<b>0.413</b>	<b>86</b>	<b>0.348</b>
		<b>0.032</b>	<b>0.258</b>	<b>151</b>	<b>76</b>	<b>0.326</b>	<b>0.320</b>	<b>86</b>	<b>0.203</b>
		<b>0.035</b>	<b>0.241</b>	<b>151</b>	<b>76</b>	<b>0.309</b>	<b>0.303</b>	<b>86</b>	<b>0.257</b>
		<b>0.038</b>	<b>0.203</b>	<b>151</b>	<b>76</b>	<b>0.298</b>	<b>0.285</b>	<b>86</b>	<b>0.233</b>
		<b>0.041</b>	<b>0.171</b>	<b>151</b>	<b>76</b>	<b>0.230</b>	<b>0.214</b>	<b>86</b>	<b>0.190</b>
		<b>0.044</b>	<b>0.142</b>	<b>151</b>	<b>76</b>	<b>0.192</b>	<b>0.167</b>	<b>86</b>	<b>0.163</b>
		<b>0.047</b>	<b>0.118</b>	<b>151</b>	<b>76</b>	<b>0.174</b>	<b>0.157</b>	<b>86</b>	<b>0.150</b>
		<b>0.050</b>	<b>0.100</b>	<b>151</b>	<b>76</b>	<b>0.114</b>	<b>0.101</b>	<b>86</b>	<b>0.116</b>
<b>0.005</b>	<b>0.06</b>	<b>0.005</b>	<b>0.850</b>	<b>129</b>	<b>83</b>	<b>0.962</b>	<b>0.994</b>	<b>83</b>	<b>0.849</b>
		<b>0.009</b>	<b>0.876</b>	<b>129</b>	<b>83</b>	<b>0.874</b>	<b>0.831</b>	<b>83</b>	<b>0.885</b>
		<b>0.013</b>	<b>0.796</b>	<b>129</b>	<b>83</b>	<b>0.756</b>	<b>0.857</b>	<b>83</b>	<b>0.778</b>
		<b>0.017</b>	<b>0.695</b>	<b>129</b>	<b>83</b>	<b>0.867</b>	<b>0.755</b>	<b>83</b>	<b>0.702</b>
		<b>0.021</b>	<b>0.600</b>	<b>129</b>	<b>83</b>	<b>0.908</b>	<b>0.716</b>	<b>83</b>	<b>0.575</b>
		<b>0.025</b>	<b>0.499</b>	<b>129</b>	<b>83</b>	<b>0.604</b>	<b>0.584</b>	<b>83</b>	<b>0.471</b>
		<b>0.029</b>	<b>0.423</b>	<b>129</b>	<b>83</b>	<b>0.424</b>	<b>0.502</b>	<b>83</b>	<b>0.441</b>
		<b>0.033</b>	<b>0.352</b>	<b>129</b>	<b>83</b>	<b>0.376</b>	<b>0.439</b>	<b>83</b>	<b>0.374</b>
		<b>0.037</b>	<b>0.293</b>	<b>129</b>	<b>83</b>	<b>0.304</b>	<b>0.368</b>	<b>83</b>	<b>0.278</b>
		<b>0.041</b>	<b>0.245</b>	<b>129</b>	<b>83</b>	<b>0.244</b>	<b>0.285</b>	<b>83</b>	<b>0.229</b>
		<b>0.045</b>	<b>0.203</b>	<b>129</b>	<b>83</b>	<b>0.203</b>	<b>0.239</b>	<b>83</b>	<b>0.180</b>
		<b>0.049</b>	<b>0.167</b>	<b>129</b>	<b>83</b>	<b>0.154</b>	<b>0.182</b>	<b>83</b>	<b>0.148</b>
		<b>0.053</b>	<b>0.137</b>	<b>129</b>	<b>83</b>	<b>0.121</b>	<b>0.135</b>	<b>83</b>	<b>0.130</b>
		<b>0.057</b>	<b>0.116</b>	<b>129</b>	<b>83</b>	<b>0.120</b>	<b>0.137</b>	<b>83</b>	<b>0.129</b>
		<b>0.060</b>	<b>0.100</b>	<b>129</b>	<b>83</b>	<b>0.120</b>	<b>0.127</b>	<b>83</b>	<b>0.100</b>
<b>0.005</b>	<b>0.07</b>	<b>0.005</b>	<b>0.850</b>	<b>74</b>	<b>71</b>	<b>0.962</b>	<b>0.984</b>	<b>71</b>	<b>0.859</b>
		<b>0.010</b>	<b>0.866</b>	<b>74</b>	<b>71</b>	<b>0.878</b>	<b>0.939</b>	<b>71</b>	<b>0.883</b>
		<b>0.015</b>	<b>0.767</b>	<b>74</b>	<b>71</b>	<b>0.796</b>	<b>0.873</b>	<b>71</b>	<b>0.792</b>
		<b>0.020</b>	<b>0.689</b>	<b>74</b>	<b>71</b>	<b>0.884</b>	<b>0.760</b>	<b>71</b>	<b>0.670</b>
		<b>0.025</b>	<b>0.581</b>	<b>74</b>	<b>71</b>	<b>0.885</b>	<b>0.707</b>	<b>71</b>	<b>0.569</b>
		<b>0.030</b>	<b>0.464</b>	<b>74</b>	<b>71</b>	<b>0.603</b>	<b>0.617</b>	<b>71</b>	<b>0.492</b>
		<b>0.035</b>	<b>0.387</b>	<b>74</b>	<b>71</b>	<b>0.399</b>	<b>0.804</b>	<b>71</b>	<b>0.415</b>
		<b>0.040</b>	<b>0.321</b>	<b>74</b>	<b>71</b>	<b>0.302</b>	<b>0.404</b>	<b>71</b>	<b>0.323</b>
		<b>0.045</b>	<b>0.269</b>	<b>74</b>	<b>71</b>	<b>0.251</b>	<b>0.330</b>	<b>71</b>	<b>0.290</b>
		<b>0.050</b>	<b>0.219</b>	<b>74</b>	<b>71</b>	<b>0.217</b>	<b>0.285</b>	<b>71</b>	<b>0.230</b>
		<b>0.055</b>	<b>0.181</b>	<b>74</b>	<b>71</b>	<b>0.191</b>	<b>0.243</b>	<b>71</b>	<b>0.181</b>
		<b>0.060</b>	<b>0.148</b>	<b>74</b>	<b>71</b>	<b>0.159</b>	<b>0.217</b>	<b>71</b>	<b>0.126</b>
		<b>0.065</b>	<b>0.121</b>	<b>74</b>	<b>71</b>	<b>0.114</b>	<b>0.165</b>	<b>71</b>	<b>0.118</b>
		<b>0.070</b>	<b>0.100</b>	<b>74</b>	<b>71</b>	<b>0.110</b>	<b>0.141</b>	<b>71</b>	<b>0.114</b>

Table XVIII - OC TESTING , PLAN SET II  
EXTENDED (h<sub>1</sub>-1) ACCEPTANCE RULE

P <sub>1</sub>	P <sub>2</sub>	P <sub>a</sub>	Accept <sub>i</sub> @ P <sub>a</sub>	Tuncation			Tuncation		
				NTP	m=1 Hold $\alpha$	Pr(acc) Actual	NTP	m=1 Hold $\beta$	Pr(acc) Actual
0.01	0.03	0.010	0.950	714	803	0.837	0.867	870	0.835
		0.012	0.895	714	803	0.870	0.917	870	0.868
		0.014	0.812	714	803	0.789	0.852	870	0.772
		0.016	0.708	714	803	0.692	0.732	870	0.673
		0.018	0.561	714	803	0.565	0.588	870	0.578
		0.020	0.448	714	803	0.443	0.475	870	0.446
		0.022	0.352	714	803	0.332	0.331	870	0.376
		0.024	0.250	714	803	0.251	0.294	870	0.256
		0.026	0.188	714	803	0.187	0.174	870	0.187
		0.028	0.139	714	803	0.156	0.158	870	0.151
		0.030	1.000	714	803	0.112	0.124	870	0.097
	0.04	0.010	0.850	350	265	0.845	0.889	281	0.848
		0.013	0.884	350	265	0.894	0.997	281	0.878
		0.016	0.780	350	265	0.778	0.800	281	0.742
		0.019	0.683	350	265	0.878	0.892	281	0.988
		0.022	0.549	350	265	0.568	0.568	281	0.527
		0.025	0.436	350	265	0.444	0.435	281	0.422
		0.028	0.325	350	265	0.328	0.356	281	0.256
		0.031	0.250	350	265	0.261	0.283	281	0.248
		0.034	0.185	350	265	0.212	0.189	281	0.187
		0.037	0.137	350	265	0.189	0.147	281	0.150
		0.040	0.100	350	265	0.102	0.097	281	0.185
0.01	0.05	0.010	0.650	215	138	0.956	0.854	184	0.833
		0.013	0.900	215	138	0.895	0.827	184	0.849
		0.016	0.828	215	138	0.823	0.986	184	0.776
		0.019	0.743	215	138	0.757	0.791	184	0.702
		0.022	0.654	215	138	0.880	0.733	184	0.820
		0.025	0.563	215	138	0.823	0.930	184	0.571
		0.028	0.467	215	138	0.490	0.610	184	0.485
		0.031	0.387	215	138	0.421	0.424	184	0.427
		0.034	0.303	215	138	0.330	0.337	184	0.300
		0.037	0.254	215	138	0.311	0.289	184	0.234
		0.040	0.203	215	138	0.212	0.217	184	0.185
		0.042	0.177	215	138	0.189	0.184	184	0.182
		0.044	0.154	215	138	0.181	0.157	184	0.158
		0.047	0.125	215	138	0.158	0.148	184	0.108
		0.050	0.100	215	138	0.126	0.135	184	0.088
0.01	0.06	0.010	0.850	151	82	0.843	0.874	106	0.810
		0.013	0.899	151	82	0.814	0.852	106	0.868
		0.016	0.855	151	82	0.866	0.893	106	0.823

Table XVIII - OC TESTING , PLAN SET II  
 EXTENDED (h<sub>1</sub>-1) ACCEPTANCE RULE  
 (CONTINUED)

		<b>0.019</b>	<b>0.766</b>	<b>151</b>	<b>82</b>	<b>0.794</b>	<b>0.619</b>	<b>106</b>	<b>0.759</b>
		<b>0.022</b>	<b>0.711</b>	<b>151</b>	<b>82</b>	<b>0.755</b>	<b>0.759</b>	<b>106</b>	<b>0.676</b>
		<b>0.025</b>	<b>0.643</b>	<b>151</b>	<b>82</b>	<b>0.676</b>	<b>0.675</b>	<b>106</b>	<b>0.605</b>
		<b>0.026</b>	<b>0.665</b>	<b>151</b>	<b>82</b>	<b>0.612</b>	<b>0.609</b>	<b>106</b>	<b>0.816</b>
		<b>0.031</b>	<b>0.466</b>	<b>151</b>	<b>92</b>	<b>0.516</b>	<b>0.615</b>	<b>106</b>	<b>0.478</b>
		<b>0.035</b>	<b>0.402</b>	<b>151</b>	<b>92</b>	<b>0.477</b>	<b>0.426</b>	<b>106</b>	<b>0.375</b>
		<b>0.040</b>	<b>0.306</b>	<b>151</b>	<b>92</b>	<b>0.361</b>	<b>0.353</b>	<b>106</b>	<b>0.278</b>
		<b>0.043</b>	<b>0.284</b>	<b>151</b>	<b>92</b>	<b>0.326</b>	<b>0.290</b>	<b>106</b>	<b>0.254</b>
		<b>0.046</b>	<b>0.224</b>	<b>151</b>	<b>92</b>	<b>0.326</b>	<b>0.250</b>	<b>106</b>	<b>0.222</b>
		<b>0.049</b>	<b>0.185</b>	<b>151</b>	<b>92</b>	<b>0.278</b>	<b>0.213</b>	<b>106</b>	<b>0.182</b>
		<b>0.051</b>	<b>0.167</b>	<b>151</b>	<b>92</b>	<b>0.202</b>	<b>0.186</b>	<b>106</b>	<b>0.151</b>
		<b>0.054</b>	<b>0.142</b>	<b>151</b>	<b>92</b>	<b>0.232</b>	<b>0.150</b>	<b>106</b>	<b>0.101</b>
		<b>0.057</b>	<b>0.119</b>	<b>151</b>	<b>92</b>	<b>0.174</b>	<b>0.114</b>	<b>106</b>	<b>0.120</b>
		<b>0.060</b>	<b>0.100</b>	<b>151</b>	<b>92</b>	<b>0.156</b>	<b>0.079</b>	<b>106</b>	<b>0.111</b>
<b>0.01</b>	<b>0.07</b>	<b>0.010</b>	<b>0.950</b>	<b>133</b>	<b>94</b>	<b>0.947</b>	<b>0.866</b>	<b>91</b>	<b>0.934</b>
		<b>0.015</b>	<b>0.885</b>	<b>133</b>	<b>94</b>	<b>0.871</b>	<b>0.924</b>	<b>91</b>	<b>0.877</b>
		<b>0.020</b>	<b>0.786</b>	<b>133</b>	<b>94</b>	<b>0.770</b>	<b>0.857</b>	<b>91</b>	<b>0.784</b>
		<b>0.025</b>	<b>0.700</b>	<b>133</b>	<b>94</b>	<b>0.684</b>	<b>0.752</b>	<b>91</b>	<b>0.680</b>
		<b>0.030</b>	<b>0.587</b>	<b>133</b>	<b>94</b>	<b>0.585</b>	<b>0.643</b>	<b>91</b>	<b>0.533</b>
		<b>0.035</b>	<b>0.486</b>	<b>133</b>	<b>94</b>	<b>0.501</b>	<b>0.536</b>	<b>91</b>	<b>0.466</b>
		<b>0.040</b>	<b>0.393</b>	<b>133</b>	<b>94</b>	<b>0.425</b>	<b>0.447</b>	<b>91</b>	<b>0.380</b>
		<b>0.045</b>	<b>0.309</b>	<b>133</b>	<b>94</b>	<b>0.348</b>	<b>0.340</b>	<b>91</b>	<b>0.268</b>
		<b>0.050</b>	<b>0.250</b>	<b>133</b>	<b>94</b>	<b>0.270</b>	<b>0.270</b>	<b>91</b>	<b>0.251</b>
		<b>0.055</b>	<b>0.189</b>	<b>133</b>	<b>94</b>	<b>0.241</b>	<b>0.210</b>	<b>91</b>	<b>0.183</b>
		<b>0.060</b>	<b>0.162</b>	<b>133</b>	<b>94</b>	<b>0.187</b>	<b>0.166</b>	<b>91</b>	<b>0.170</b>
		<b>0.065</b>	<b>0.126</b>	<b>133</b>	<b>94</b>	<b>0.912</b>	<b>0.130</b>	<b>91</b>	<b>0.133</b>
		<b>0.070</b>	<b>0.100</b>	<b>133</b>	<b>94</b>	<b>0.120</b>	<b>0.111</b>	<b>91</b>	<b>0.102</b>
<b>0.01</b>	<b>0.08</b>	<b>0.010</b>	<b>0.950</b>	<b>80</b>	<b>36</b>	<b>0.946</b>	<b>0.973</b>	<b>57</b>	<b>0.905</b>
		<b>0.015</b>	<b>0.892</b>	<b>80</b>	<b>36</b>	<b>0.897</b>	<b>0.921</b>	<b>57</b>	<b>0.853</b>
		<b>0.020</b>	<b>0.808</b>	<b>80</b>	<b>36</b>	<b>0.831</b>	<b>0.855</b>	<b>57</b>	<b>0.730</b>
		<b>0.025</b>	<b>0.727</b>	<b>80</b>	<b>36</b>	<b>0.796</b>	<b>0.811</b>	<b>57</b>	<b>0.846</b>
		<b>0.030</b>	<b>0.613</b>	<b>80</b>	<b>36</b>	<b>0.708</b>	<b>0.714</b>	<b>57</b>	<b>0.557</b>
		<b>0.035</b>	<b>0.543</b>	<b>80</b>	<b>36</b>	<b>0.683</b>	<b>0.613</b>	<b>57</b>	<b>0.480</b>
		<b>0.040</b>	<b>0.454</b>	<b>80</b>	<b>36</b>	<b>0.604</b>	<b>0.624</b>	<b>57</b>	<b>0.394</b>
		<b>0.045</b>	<b>0.387</b>	<b>80</b>	<b>36</b>	<b>0.555</b>	<b>0.490</b>	<b>57</b>	<b>0.332</b>
		<b>0.050</b>	<b>0.319</b>	<b>80</b>	<b>36</b>	<b>0.478</b>	<b>0.380</b>	<b>57</b>	<b>0.288</b>
		<b>0.055</b>	<b>0.241</b>	<b>80</b>	<b>36</b>	<b>0.407</b>	<b>0.336</b>	<b>57</b>	<b>0.230</b>
		<b>0.060</b>	<b>0.224</b>	<b>80</b>	<b>36</b>	<b>0.351</b>	<b>0.274</b>	<b>57</b>	<b>0.212</b>
		<b>0.065</b>	<b>0.185</b>	<b>80</b>	<b>36</b>	<b>0.328</b>	<b>0.205</b>	<b>57</b>	<b>0.151</b>
		<b>0.070</b>	<b>0.151</b>	<b>80</b>	<b>36</b>	<b>0.263</b>	<b>0.152</b>	<b>57</b>	<b>0.120</b>
		<b>0.075</b>	<b>0.123</b>	<b>80</b>	<b>36</b>	<b>0.243</b>	<b>0.146</b>	<b>57</b>	<b>0.115</b>
		<b>0.080</b>	<b>0.100</b>	<b>80</b>	<b>36</b>	<b>0.231</b>	<b>0.135</b>	<b>57</b>	<b>0.091</b>

**Table XIX - ASN TESTING , PLAN SET I**  
**EXTENDED (h1-1) ACCEPTANCE RULE**

P1	P2	Pa	ASN(Pa)	Hold as Mean #		NTP Mean #	Hold B Mean #		# Saved over NTP	Hold B # Saved over NTP	
				Insp	Insp		Insp	Insp		# Saved	# Saved
0.005	0.01	0.005	1287	1309.2	1322.6	1303.4			12.3	19.2	
		0.006	1603	1609.2	1622.0	1616.0			13.7	104.0	
		0.007	2085	1678.7	1686.5	1758.4			18.0	-82.8	
		0.008	1764	1681.8	1684.2	1728.6			12.3	-34.5	
		0.009	1485	1486.5	1486.8	1801.5			10.3	-4.6	
		0.010	1225	1317.2	1323.4	1306.5			8.2	16.8	
		0.011	264	269.0	277.5	273.0			8.5	4.5	
		0.012	301	266.7	262.4	261.3			13.7	21.1	
		0.013	325	267.0	269.1	262.6			21.6	16.3	
		0.014	302	300.8	310.1	303.1			17.2	15.0	
0.005	0.02	0.006	270	277.2	280.0	293.5			20.8	4.8	
		0.015	241	264.7	268.8	272.5			24.1	18.3	
		0.016	213	240.1	252.5	244.0			12.4	8.5	
		0.020	166	210.8	224.5	220.1			13.7	4.4	
		0.021	122	110.4	124.3	118.9			13.9	4.4	
		0.007	134	115.9	144.4	127.6			26.6	16.6	
		0.010	146	121.6	165.6	130.3			33.6	16.6	
		0.013	180	122.2	183.2	137.2			41.0	26.0	
		0.016	138	116.1	154.8	135.5			38.5	18.1	
		0.019	126	113.4	146.6	128.1			33.4	18.7	
0.005	0.03	0.022	113	109.0	136.0	118.4			27.0	16.6	
		0.025	100	88.7	123.4	106.2			24.7	16.2	
		0.028	88	82.0	107.6	87.1			15.6	10.6	
		0.030	82	60.9	102.1	87.6			11.2	4.5	
		0.005	80	64.7	78.8	75.4			15.1	4.4	
		0.007	84	84.5	88.8	78.4			22.3	8.4	
		0.010	88	84.0	85.1	80.5			31.1	14.6	
		0.013	89	83.1	84.9	81.6			31.6	13.1	
		0.016	85	81.7	88.6	82.1			34.9	14.5	
		0.019	83	81.4	83.6	78.6			32.2	14.6	
0.005	0.04	0.022	79	66.8	80.4	78.2			31.6	14.2	
		0.025	74	67.4	88.1	72.6			30.7	15.6	
		0.028	68	84.5	79.7	71.7			25.2	8.0	
		0.031	63	84.6	78.9	88.6			22.3	10.1	
		0.034	68	80.8	71.3	83.4			20.5	7.8	
		0.037	53	48.5	86.7	89.9			18.2	6.8	
		0.040	49	46.6	81.1	87.6			14.5	3.5	
		0.005	66	63.6	60.3	57.2			6.5	3.1	
		0.008	62	68.0	67.5	61.4			12.5	6.1	
		0.011	63	66.5	71.1	62.5			14.6	6.6	

Table XIX - ASN TESTING , PLAN SET I  
 EXTENDED (h1-1) ACCEPTANCE RULE  
 (CONTINUED)

		<b>0.014</b>	<b>65</b>	<b>66.3</b>	<b>70.9</b>	<b>64.0</b>			<b>14.6</b>	<b>6.6</b>
		<b>0.017</b>	<b>67</b>	<b>65.4</b>	<b>72.1</b>	<b>62.0</b>			<b>16.7</b>	<b>10.1</b>
		<b>0.020</b>	<b>70</b>	<b>66.0</b>	<b>71.6</b>	<b>61.6</b>			<b>15.6</b>	<b>10.2</b>
		<b>0.023</b>	<b>62</b>	<b>63.3</b>	<b>70.7</b>	<b>62.0</b>			<b>17.4</b>	<b>8.7</b>
		<b>0.026</b>	<b>67</b>	<b>63.5</b>	<b>69.0</b>	<b>68.0</b>			<b>15.5</b>	<b>10.0</b>
		<b>0.029</b>	<b>55</b>	<b>62.0</b>	<b>66.3</b>	<b>66.6</b>			<b>14.3</b>	<b>8.7</b>
		<b>0.032</b>	<b>49</b>	<b>48.8</b>	<b>63.6</b>	<b>65.4</b>			<b>14.0</b>	<b>8.4</b>
		<b>0.035</b>	<b>46</b>	<b>48.1</b>	<b>60.4</b>	<b>62.6</b>			<b>11.3</b>	<b>7.8</b>
		<b>0.038</b>	<b>43</b>	<b>47.4</b>	<b>56.7</b>	<b>51.0</b>			<b>8.3</b>	<b>6.7</b>
		<b>0.041</b>	<b>41</b>	<b>45.1</b>	<b>62.2</b>	<b>46.0</b>			<b>7.1</b>	<b>4.2</b>
		<b>0.044</b>	<b>38</b>	<b>43.8</b>	<b>49.0</b>	<b>47.1</b>			<b>6.2</b>	<b>1.8</b>
		<b>0.047</b>	<b>36</b>	<b>41.7</b>	<b>45.5</b>	<b>43.2</b>			<b>8.8</b>	<b>2.3</b>
		<b>0.050</b>	<b>34</b>	<b>38.2</b>	<b>42.3</b>	<b>40.8</b>			<b>8.1</b>	<b>1.0</b>
<b>0.005</b>	<b>0.06</b>	<b>0.005</b>	<b>46</b>	<b>48.0</b>	<b>48.6</b>	<b>47.4</b>			<b>1.8</b>	<b>1.4</b>
		<b>0.009</b>	<b>48</b>	<b>48.8</b>	<b>63.5</b>	<b>66.6</b>			<b>4.6</b>	<b>3.9</b>
		<b>0.013</b>	<b>49</b>	<b>62.0</b>	<b>56.8</b>	<b>51.8</b>			<b>4.8</b>	<b>4.8</b>
		<b>0.017</b>	<b>50</b>	<b>62.0</b>	<b>68.0</b>	<b>51.7</b>			<b>6.0</b>	<b>8.3</b>
		<b>0.021</b>	<b>56</b>	<b>51.6</b>	<b>58.2</b>	<b>50.6</b>			<b>8.6</b>	<b>7.8</b>
		<b>0.025</b>	<b>49</b>	<b>49.1</b>	<b>66.6</b>	<b>51.3</b>			<b>7.5</b>	<b>0.3</b>
		<b>0.029</b>	<b>43</b>	<b>49.6</b>	<b>65.1</b>	<b>48.9</b>			<b>6.5</b>	<b>6.2</b>
		<b>0.033</b>	<b>40</b>	<b>48.4</b>	<b>51.0</b>	<b>48.8</b>			<b>4.6</b>	<b>2.1</b>
		<b>0.037</b>	<b>38</b>	<b>45.8</b>	<b>50.6</b>	<b>45.2</b>			<b>8.0</b>	<b>0.6</b>
		<b>0.041</b>	<b>35</b>	<b>42.8</b>	<b>46.5</b>	<b>43.8</b>			<b>3.7</b>	<b>2.6</b>
		<b>0.045</b>	<b>33</b>	<b>41.1</b>	<b>44.3</b>	<b>40.6</b>			<b>8.2</b>	<b>3.7</b>
		<b>0.049</b>	<b>31</b>	<b>38.4</b>	<b>42.3</b>	<b>38.3</b>			<b>2.8</b>	<b>3.0</b>
		<b>0.053</b>	<b>29</b>	<b>38.5</b>	<b>38.4</b>	<b>38.5</b>			<b>1.6</b>	<b>1.6</b>
		<b>0.057</b>	<b>27</b>	<b>34.1</b>	<b>35.7</b>	<b>34.9</b>			<b>1.6</b>	<b>0.8</b>
		<b>0.060</b>	<b>25</b>	<b>33.9</b>	<b>35.0</b>	<b>32.6</b>			<b>1.1</b>	<b>2.5</b>
<b>0.005</b>	<b>0.07</b>	<b>0.005</b>	<b>37</b>	<b>38.8</b>	<b>40.2</b>	<b>38.6</b>			<b>0.5</b>	<b>0.6</b>
		<b>0.010</b>	<b>39</b>	<b>42.1</b>	<b>42.6</b>	<b>43.0</b>			<b>0.7</b>	<b>-0.2</b>
		<b>0.015</b>	<b>40</b>	<b>43.5</b>	<b>44.2</b>	<b>43.5</b>			<b>0.8</b>	<b>0.8</b>
		<b>0.020</b>	<b>41</b>	<b>43.5</b>	<b>44.3</b>	<b>43.0</b>			<b>0.8</b>	<b>1.3</b>
		<b>0.025</b>	<b>42</b>	<b>43.3</b>	<b>44.2</b>	<b>43.3</b>			<b>0.8</b>	<b>0.0</b>
		<b>0.030</b>	<b>38</b>	<b>43.2</b>	<b>44.0</b>	<b>41.7</b>			<b>0.8</b>	<b>2.3</b>
		<b>0.035</b>	<b>34</b>	<b>40.1</b>	<b>40.8</b>	<b>40.3</b>			<b>0.6</b>	<b>0.5</b>
		<b>0.040</b>	<b>31</b>	<b>38.3</b>	<b>38.6</b>	<b>39.0</b>			<b>0.5</b>	<b>-0.2</b>
		<b>0.045</b>	<b>28</b>	<b>37.2</b>	<b>37.7</b>	<b>37.3</b>			<b>0.5</b>	<b>0.4</b>
		<b>0.050</b>	<b>27</b>	<b>34.8</b>	<b>35.2</b>	<b>35.1</b>			<b>0.4</b>	<b>0.2</b>
		<b>0.055</b>	<b>25</b>	<b>32.1</b>	<b>32.4</b>	<b>33.9</b>			<b>0.3</b>	<b>-1.4</b>
		<b>0.060</b>	<b>23</b>	<b>33.0</b>	<b>33.3</b>	<b>31.8</b>			<b>0.3</b>	<b>1.4</b>
		<b>0.065</b>	<b>21</b>	<b>29.0</b>	<b>28.2</b>	<b>28.8</b>			<b>0.2</b>	<b>-0.6</b>
		<b>0.070</b>	<b>20</b>	<b>27.4</b>	<b>27.6</b>	<b>27.3</b>			<b>0.1</b>	<b>0.2</b>

Table XX - ASN TESTING , PLAN SET II  
EXTENDED (h1-1) ACCEPTANCE RULE

P1	P2	P <sub>s</sub>	ASN(P <sub>s</sub> )	Hold A		NTP		Hold B		Hold C		Hold D	
				Mean S		Mean S		Mean S		Mean S		S Saved	
				Insp	Insp	Insp	Insp	Insp	Insp	Insp	Insp	over NTP	over NTP
0.01	0.03	0.010	217	218.0	218.0	225.4				-1.2	-8.0		
		0.012	245	246.7	246.6	249.8				-3.1	-8.2		
		0.014	271	269.1	264.3	266.6				-4.9	-2.3		
		0.016	295	271.7	264.7	277.3				23.0	17.4		
		0.018	363	291.0	267.0	292.8				16.0	14.1		
		0.020	288	284.0	280.3	284.5				16.3	15.8		
		0.022	267	269.6	298.2	271.0				28.7	27.2		
		0.024	250	266.5	264.6	264.6				8.1	10.0		
		0.026	222	243.6	248.2	236.3				2.6	8.9		
		0.028	198	236.3	216.4	216.0				-19.0	-0.4		
		0.030	181	208.7	205.0	192.3				-1.7	12.7		
0.01	0.04	0.010	121	118.8	121.5	122.6				4.7	-1.1		
		0.013	134	132.7	134.7	135.5				2.1	-0.8		
		0.016	145	142.9	154.6	146.7				11.6	7.9		
		0.019	162	146.5	161.7	153.7				16.2	8.0		
		0.022	185	148.5	168.3	152.6				17.8	13.8		
		0.025	150	150.3	180.5	148.1				10.2	12.4		
		0.028	138	138.4	155.1	143.7				16.6	11.4		
		0.031	123	136.2	141.5	133.7				5.3	7.8		
		0.034	112	121.8	132.3	123.6				10.4	8.8		
		0.037	102	107.8	116.9	114.8				8.1	2.1		
		0.040	82	101.6	107.1	104.3				5.4	2.9		
0.01	0.05	0.010	81	78.8	87.0	82.0				8.2	5.0		
		0.013	86	82.5	90.2	86.7				7.7	3.5		
		0.016	82	87.3	88.2	93.0				10.0	5.2		
		0.019	94	88.8	102.1	84.8				13.3	7.3		
		0.022	67	80.9	104.3	98.5				13.4	5.8		
		0.025	88	81.2	106.1	86.7				14.9	0.5		
		0.028	98	88.1	186.2	85.1				18.1	11.0		
		0.031	81	86.6	89.4	82.5				12.8	8.9		
		0.034	90	84.7	95.5	80.8				10.7	4.7		
		0.037	83	82.8	83.1	85.6				10.3	7.6		
		0.040	75	75.8	88.6	83.7				12.7	4.9		
		0.042	71	75.2	82.1	80.3				8.0	1.8		
		0.044	87	70.5	79.9	76.7				9.4	3.2		
		0.047	82	87.4	77.2	89.7				8.6	7.5		
		0.050	58	99.3	88.8	88.9				-0.5	-0.2		
0.01	0.06	0.010	60	64.8	81.5	80.2				8.6	1.3		
		0.013	83	87.7	88.0	81.9				10.3	8.1		
		0.016	86	88.6	70.0	84.7				10.4	8.3		

Table XX - ASN TESTING , PLAN SET II  
 EXTENDED (h1-1) ACCEPTANCE RULE  
 (CONTINUED)

		<b>0.019</b>	<b>70</b>	<b>60.3</b>	<b>76.2</b>	<b>67.2</b>			<b>14.9</b>	<b>8.0</b>
		<b>0.022</b>	<b>72</b>	<b>60.9</b>	<b>78.6</b>	<b>68.0</b>			<b>14.8</b>	<b>7.7</b>
		<b>0.025</b>	<b>76</b>	<b>60.2</b>	<b>74.4</b>	<b>67.6</b>			<b>14.2</b>	<b>6.9</b>
		<b>0.028</b>	<b>80</b>	<b>60.0</b>	<b>76.6</b>	<b>68.2</b>			<b>17.0</b>	<b>10.7</b>
		<b>0.031</b>	<b>76</b>	<b>56.9</b>	<b>77.0</b>	<b>68.6</b>			<b>17.1</b>	<b>10.2</b>
		<b>0.035</b>	<b>65</b>	<b>60.4</b>	<b>73.6</b>	<b>64.6</b>			<b>16.3</b>	<b>8.2</b>
		<b>0.040</b>	<b>60</b>	<b>64.2</b>	<b>68.1</b>	<b>61.2</b>			<b>14.8</b>	<b>7.8</b>
		<b>0.043</b>	<b>66</b>	<b>63.7</b>	<b>66.0</b>	<b>57.7</b>			<b>12.3</b>	<b>6.3</b>
		<b>0.046</b>	<b>53</b>	<b>52.6</b>	<b>63.7</b>	<b>57.2</b>			<b>8.6</b>	<b>6.6</b>
		<b>0.049</b>	<b>51</b>	<b>50.5</b>	<b>59.6</b>	<b>56.8</b>			<b>8.2</b>	<b>5.1</b>
		<b>0.051</b>	<b>49</b>	<b>48.3</b>	<b>57.6</b>	<b>54.2</b>			<b>6.5</b>	<b>3.6</b>
		<b>0.054</b>	<b>46</b>	<b>48.0</b>	<b>54.5</b>	<b>51.8</b>			<b>8.4</b>	<b>2.7</b>
		<b>0.057</b>	<b>43</b>	<b>46.5</b>	<b>52.0</b>	<b>47.6</b>			<b>5.5</b>	<b>4.5</b>
		<b>0.060</b>	<b>41</b>	<b>42.4</b>	<b>47.2</b>	<b>46.4</b>			<b>4.8</b>	<b>0.7</b>
<b>0.01</b>	<b>0.07</b>	<b>0.010</b>	<b>47</b>	<b>46.2</b>	<b>48.6</b>	<b>40.3</b>			<b>2.6</b>	<b>0.5</b>
		<b>0.015</b>	<b>62</b>	<b>50.8</b>	<b>54.6</b>	<b>50.3</b>			<b>4.0</b>	<b>4.6</b>
		<b>0.020</b>	<b>65</b>	<b>62.0</b>	<b>68.6</b>	<b>54.2</b>			<b>5.6</b>	<b>4.6</b>
		<b>0.025</b>	<b>58</b>	<b>64.3</b>	<b>61.6</b>	<b>65.6</b>			<b>7.2</b>	<b>6.8</b>
		<b>0.030</b>	<b>67</b>	<b>62.5</b>	<b>61.6</b>	<b>55.3</b>			<b>8.1</b>	<b>6.3</b>
		<b>0.035</b>	<b>65</b>	<b>62.1</b>	<b>60.5</b>	<b>59.3</b>			<b>7.4</b>	<b>6.2</b>
		<b>0.040</b>	<b>48</b>	<b>50.8</b>	<b>47.8</b>	<b>42.8</b>			<b>6.8</b>	<b>5.0</b>
		<b>0.045</b>	<b>47</b>	<b>46.0</b>	<b>54.4</b>	<b>40.3</b>			<b>5.4</b>	<b>5.1</b>
		<b>0.050</b>	<b>43</b>	<b>46.4</b>	<b>50.2</b>	<b>40.7</b>			<b>6.6</b>	<b>1.5</b>
		<b>0.055</b>	<b>39</b>	<b>45.0</b>	<b>48.8</b>	<b>44.5</b>			<b>1.0</b>	<b>2.4</b>
		<b>0.060</b>	<b>36</b>	<b>41.8</b>	<b>45.6</b>	<b>43.1</b>			<b>3.0</b>	<b>2.5</b>
		<b>0.065</b>	<b>33</b>	<b>38.4</b>	<b>42.6</b>	<b>39.5</b>			<b>4.4</b>	<b>3.3</b>
		<b>0.070</b>	<b>31</b>	<b>36.4</b>	<b>38.5</b>	<b>36.1</b>			<b>2.2</b>	<b>2.4</b>
<b>0.01</b>	<b>0.08</b>	<b>0.010</b>	<b>39</b>	<b>62.0</b>	<b>38.7</b>	<b>37.2</b>			<b>7.7</b>	<b>2.5</b>
		<b>0.015</b>	<b>42</b>	<b>32.2</b>	<b>43.2</b>	<b>38.6</b>			<b>11.1</b>	<b>4.7</b>
		<b>0.020</b>	<b>43</b>	<b>31.0</b>	<b>46.9</b>	<b>39.5</b>			<b>15.1</b>	<b>7.4</b>
		<b>0.025</b>	<b>44</b>	<b>32.1</b>	<b>46.6</b>	<b>40.2</b>			<b>14.7</b>	<b>8.6</b>
		<b>0.030</b>	<b>46</b>	<b>31.6</b>	<b>47.7</b>	<b>40.1</b>			<b>16.2</b>	<b>7.8</b>
		<b>0.035</b>	<b>48</b>	<b>30.8</b>	<b>46.7</b>	<b>40.1</b>			<b>16.0</b>	<b>6.6</b>
		<b>0.040</b>	<b>44</b>	<b>30.0</b>	<b>46.3</b>	<b>39.7</b>			<b>16.3</b>	<b>6.6</b>
		<b>0.045</b>	<b>39</b>	<b>26.8</b>	<b>44.3</b>	<b>36.7</b>			<b>14.7</b>	<b>7.7</b>
		<b>0.050</b>	<b>37</b>	<b>26.9</b>	<b>43.6</b>	<b>36.6</b>			<b>14.0</b>	<b>7.2</b>
		<b>0.055</b>	<b>35</b>	<b>27.6</b>	<b>41.3</b>	<b>34.5</b>			<b>13.6</b>	<b>6.6</b>
		<b>0.060</b>	<b>32</b>	<b>27.4</b>	<b>38.1</b>	<b>32.7</b>			<b>10.7</b>	<b>6.4</b>
		<b>0.065</b>	<b>30</b>	<b>26.7</b>	<b>37.1</b>	<b>32.3</b>			<b>10.4</b>	<b>4.7</b>
		<b>0.070</b>	<b>28</b>	<b>24.6</b>	<b>35.6</b>	<b>29.6</b>			<b>10.6</b>	<b>0.6</b>
		<b>0.075</b>	<b>26</b>	<b>24.5</b>	<b>32.6</b>	<b>29.3</b>			<b>8.1</b>	<b>8.3</b>
		<b>0.080</b>	<b>25</b>	<b>23.6</b>	<b>29.6</b>	<b>27.4</b>			<b>8.6</b>	<b>2.6</b>

APPENDIX C

PLAN 1 , OC CURVE A

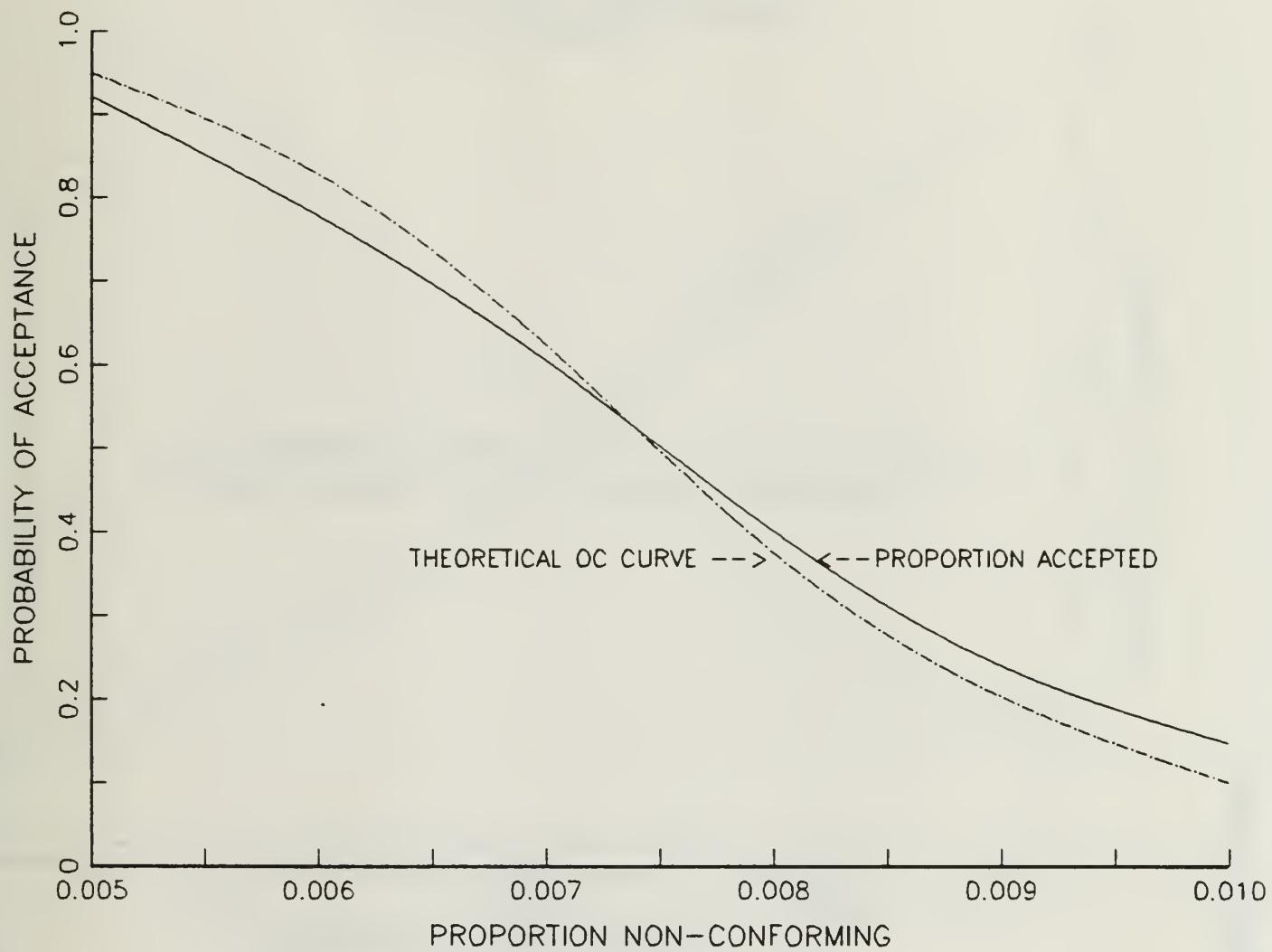


Figure 8 - OC CURVE , PLAN SET I , CURVE A

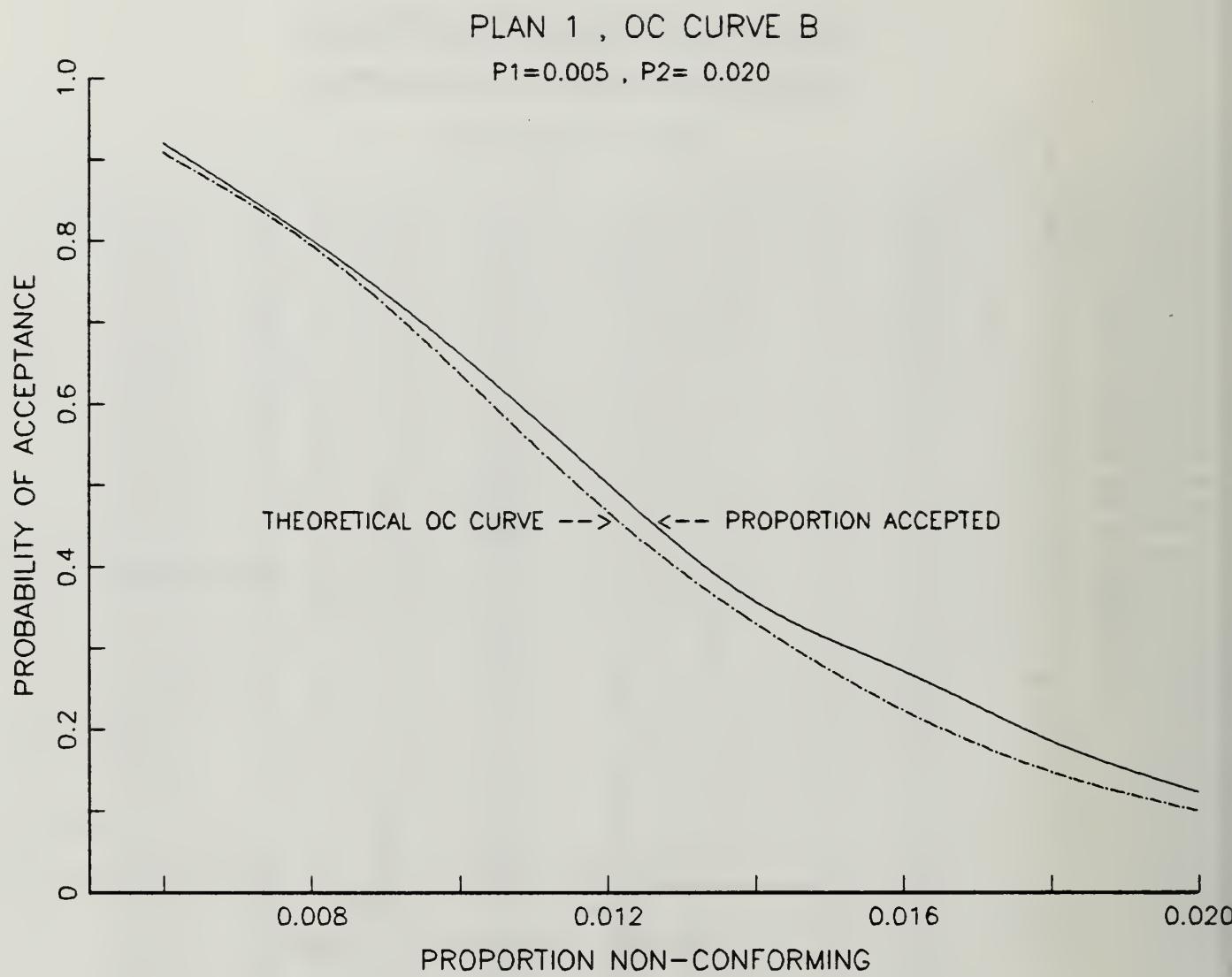


Figure 9 - OC CURVE , PLAN SET I , CURVE B

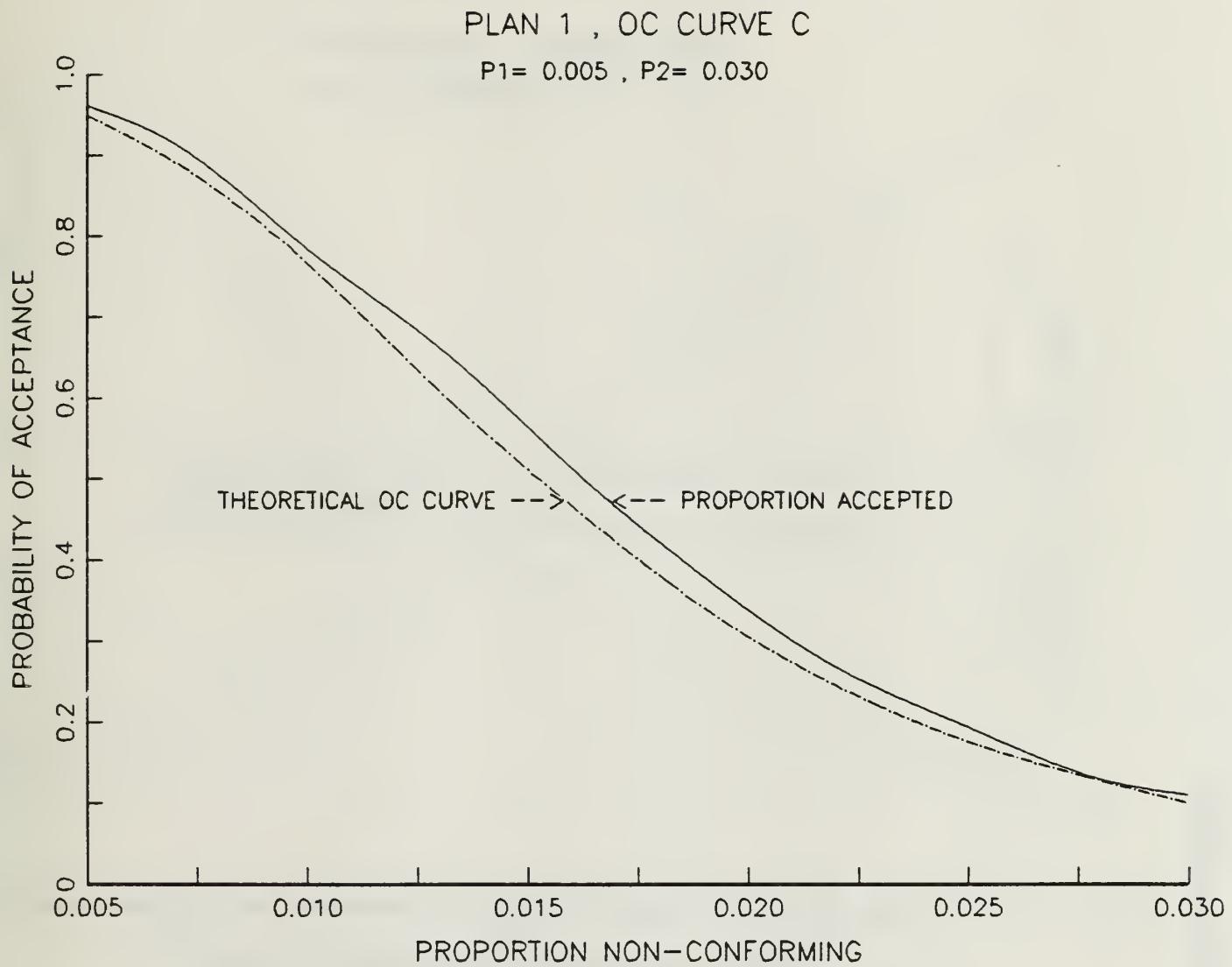


Figure10 - OC CURVE , PLAN SET I , CURVE C

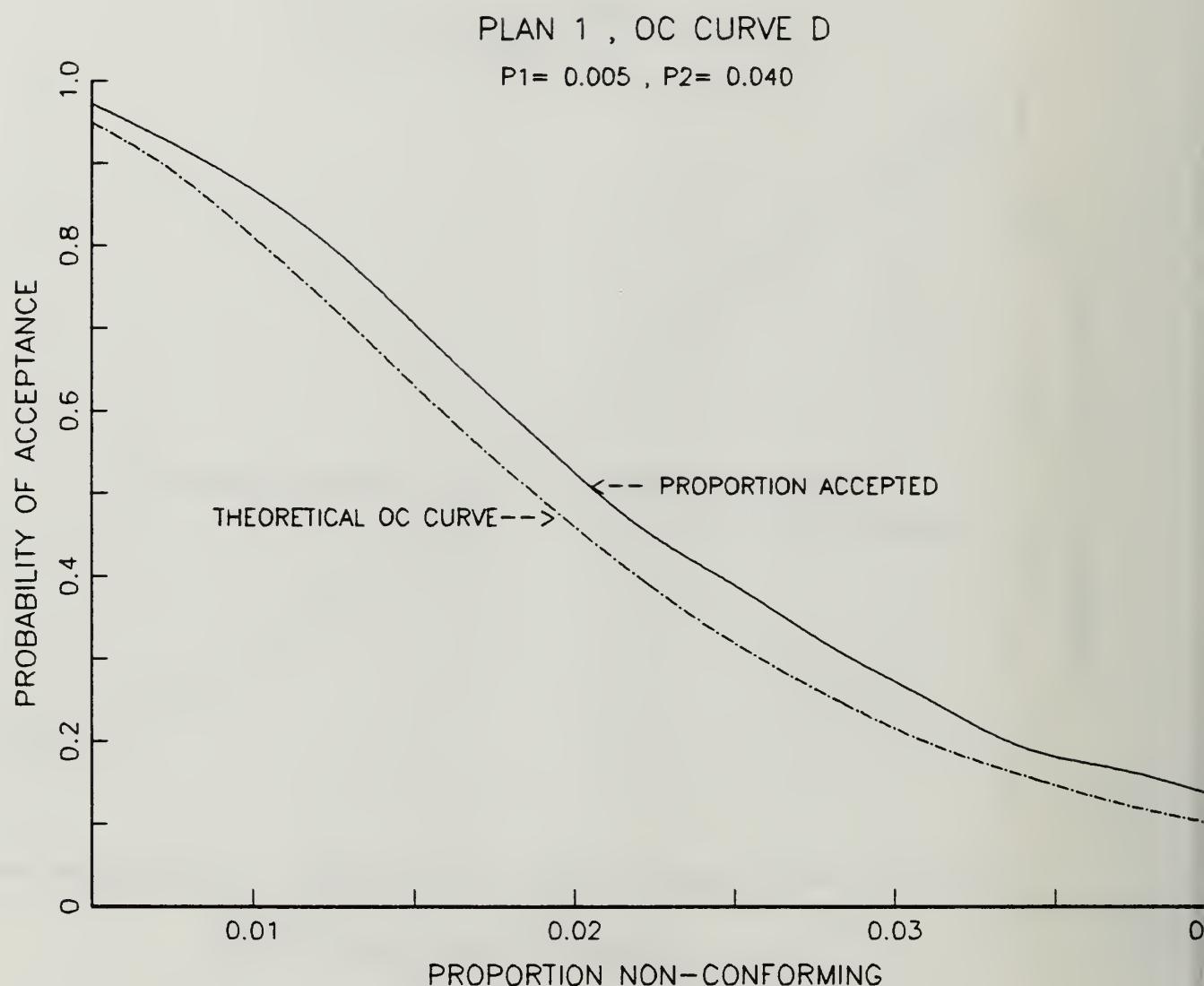


Figure 11 - OC CURVE , PLAN SET I , CURVE D

PLAN 1 , OC CURVE E

P1= 0.005 , P2= 0.050

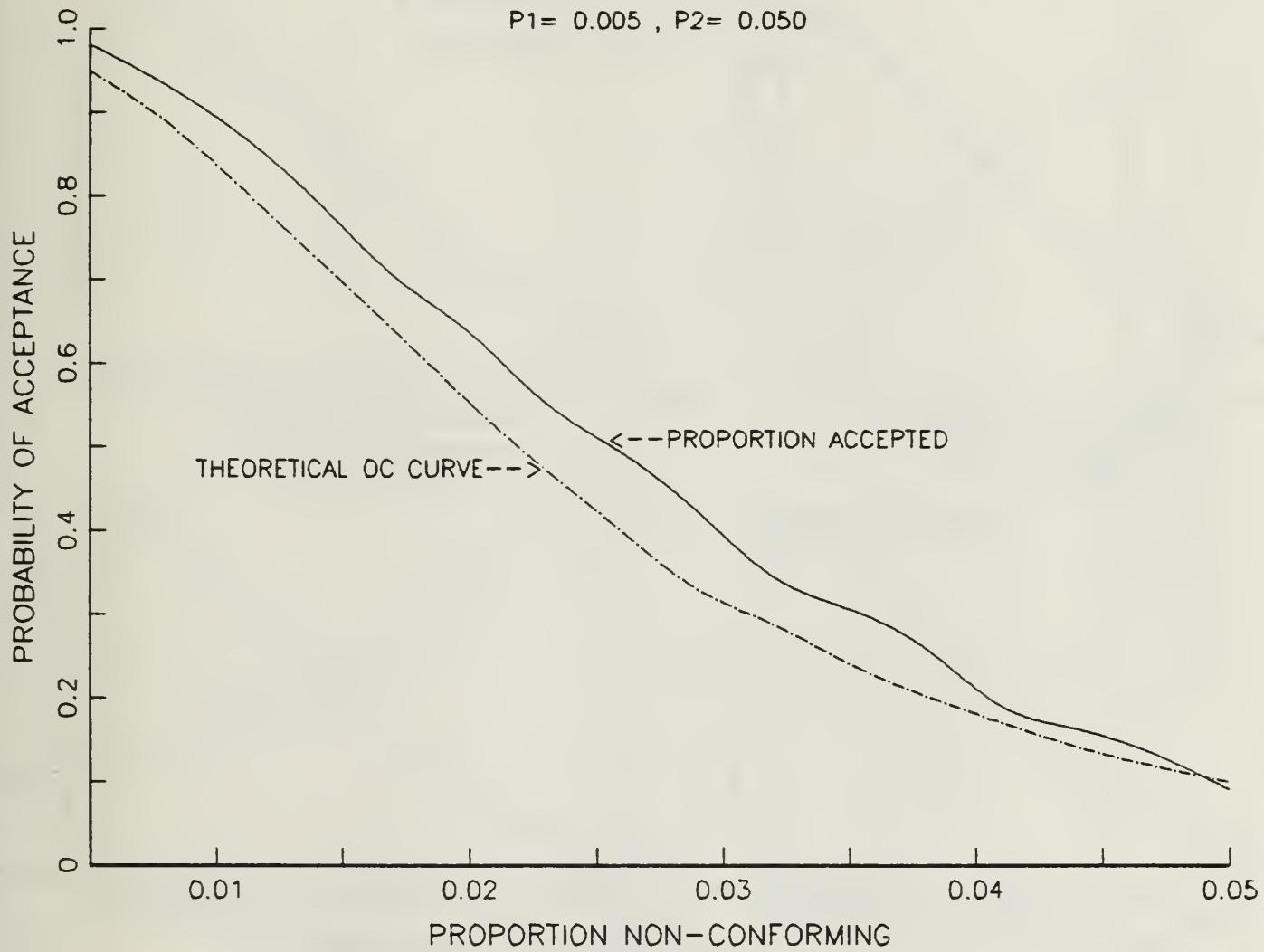


Figure 12 - OC CURVE , PLAN SET I , CURVE E

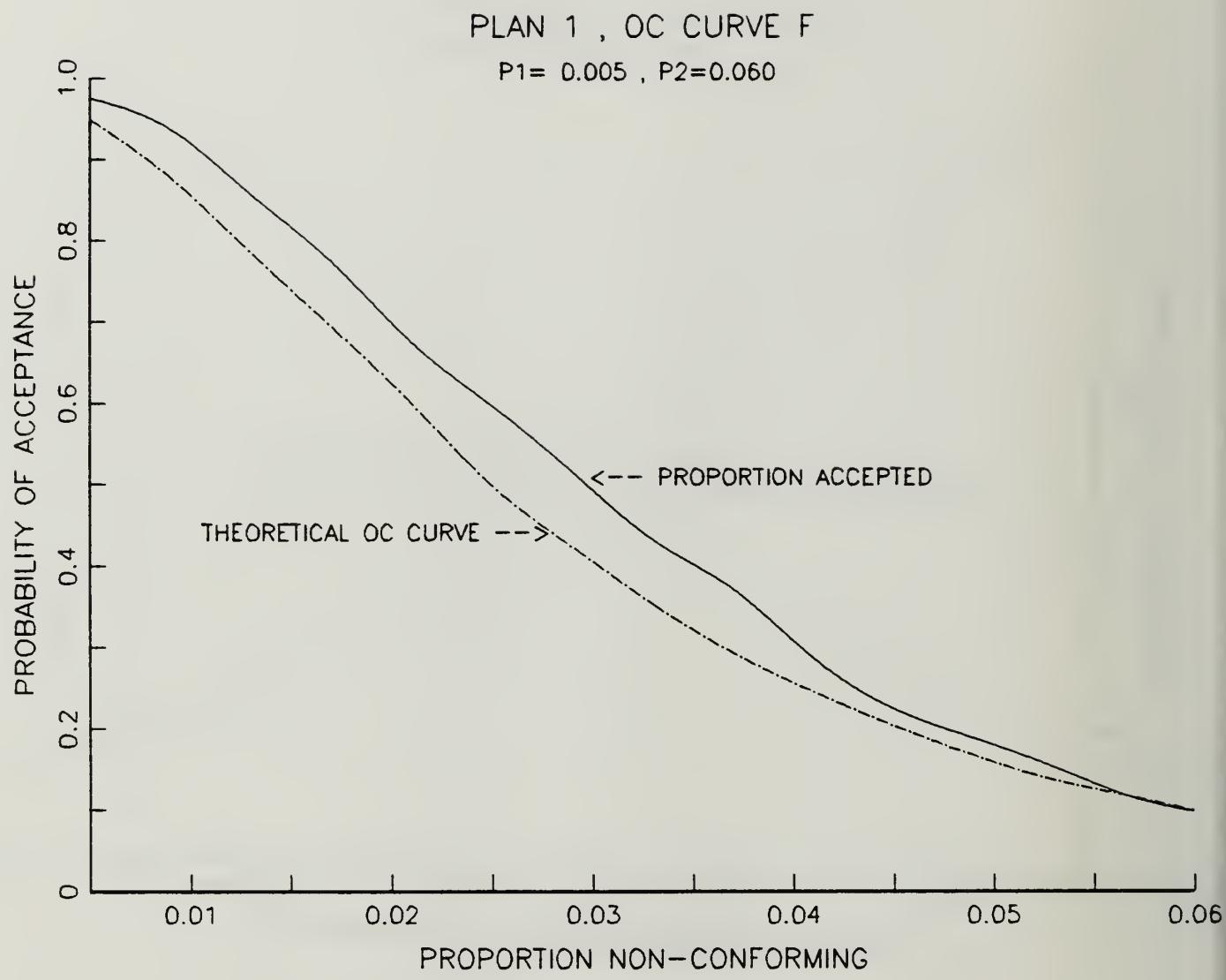


Figure 13 - OC CURVE , PLAN SET I , CURVE F

## PLAN 2 , OC CURVES

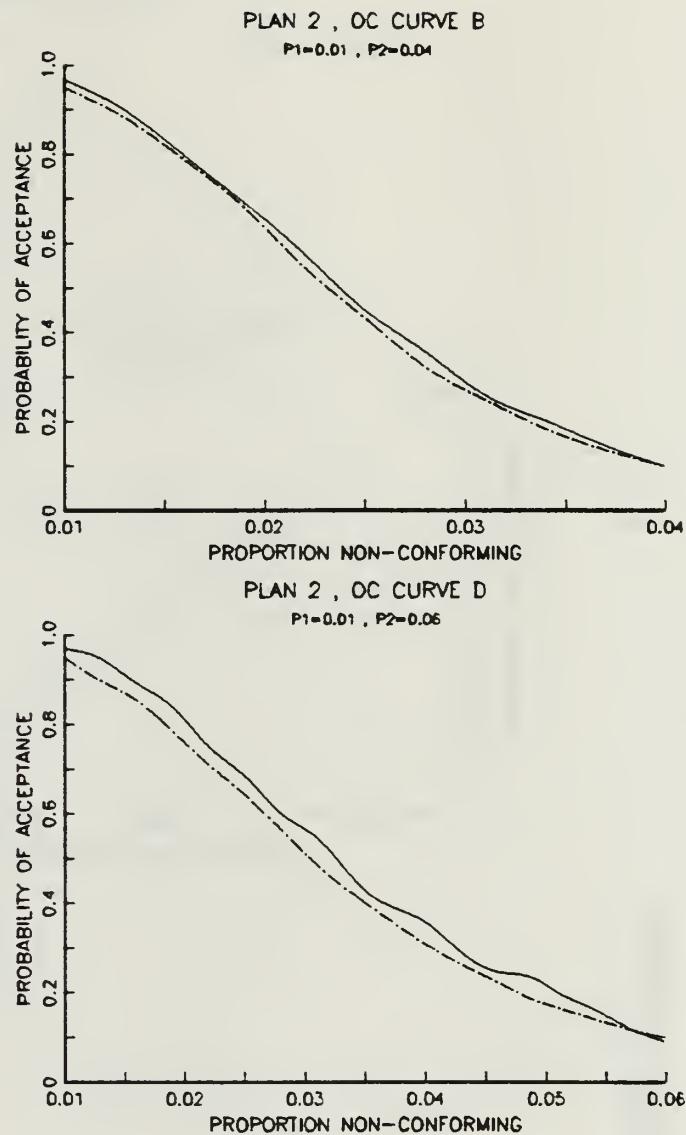
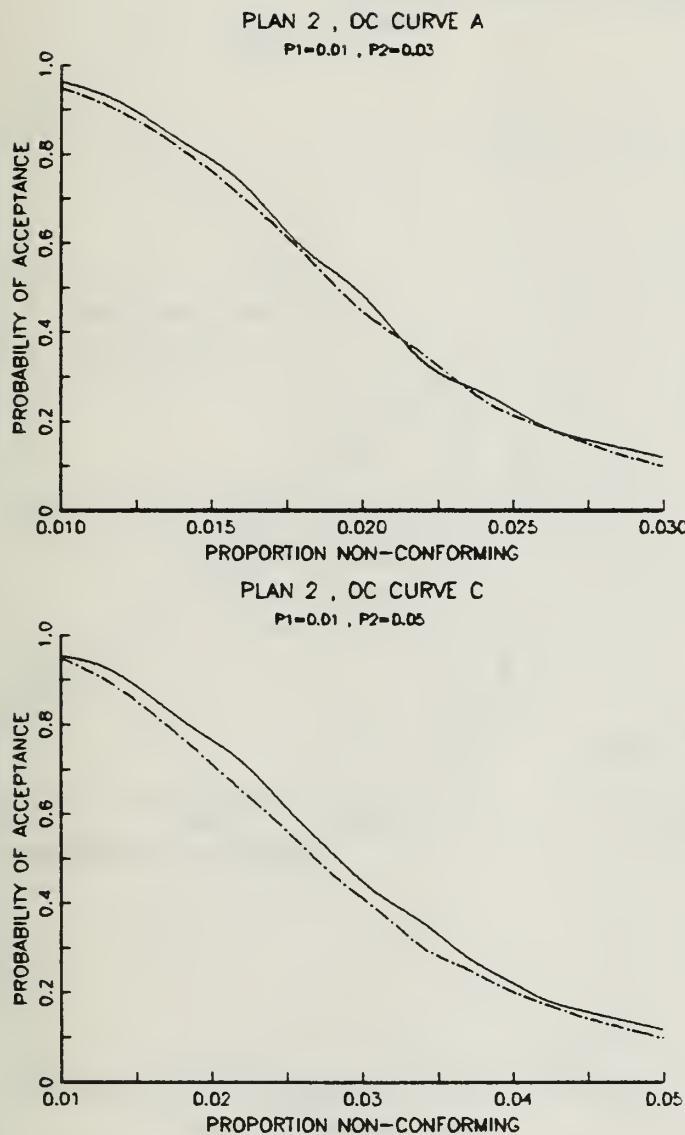


Figure 14 - OC CURVES , PLAN SET II , CURVES A THRU D  
 (SOLID LINE - TRUE , DASHED - THEORETICAL)

## PLAN 2 , OC CURVES

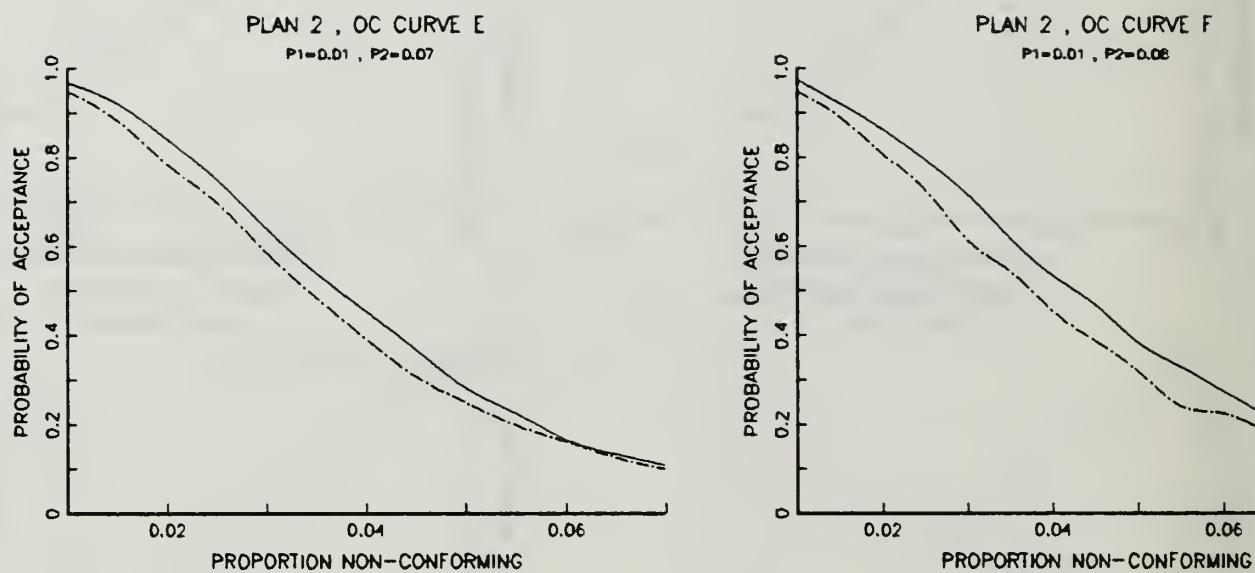


Figure 15 - OC CURVES , PLAN SET II , CURVES E AND D  
(SOLID LINE - TRUE , DASHED - THEORETICAL)

### PLAN 3 , OC CURVES

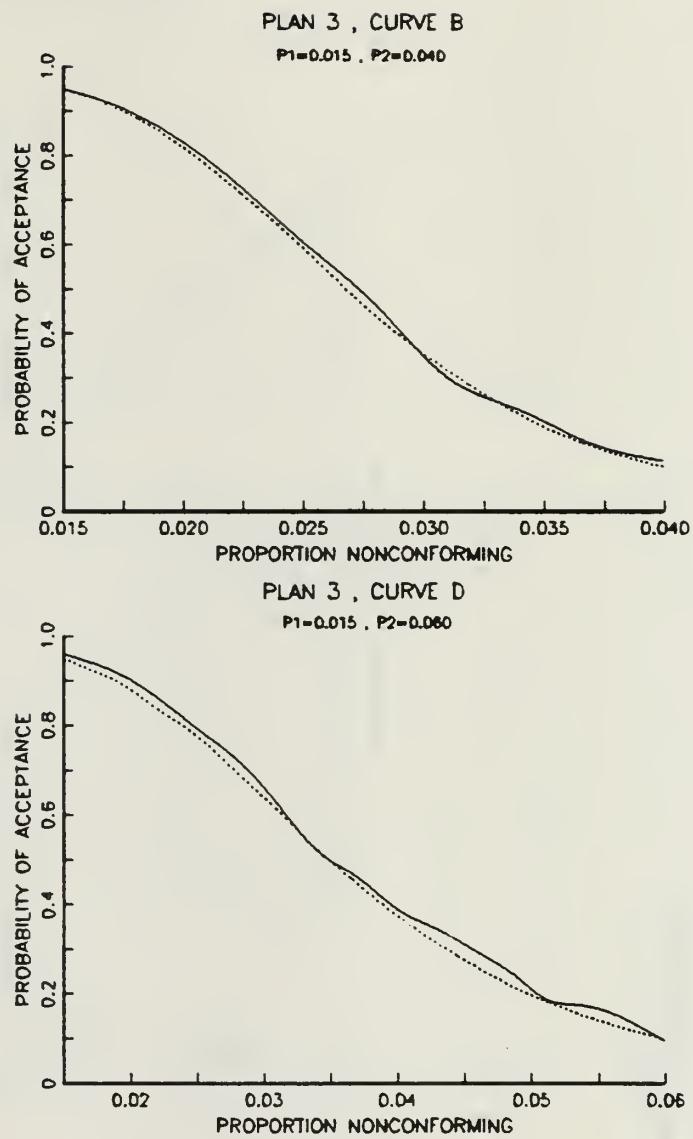
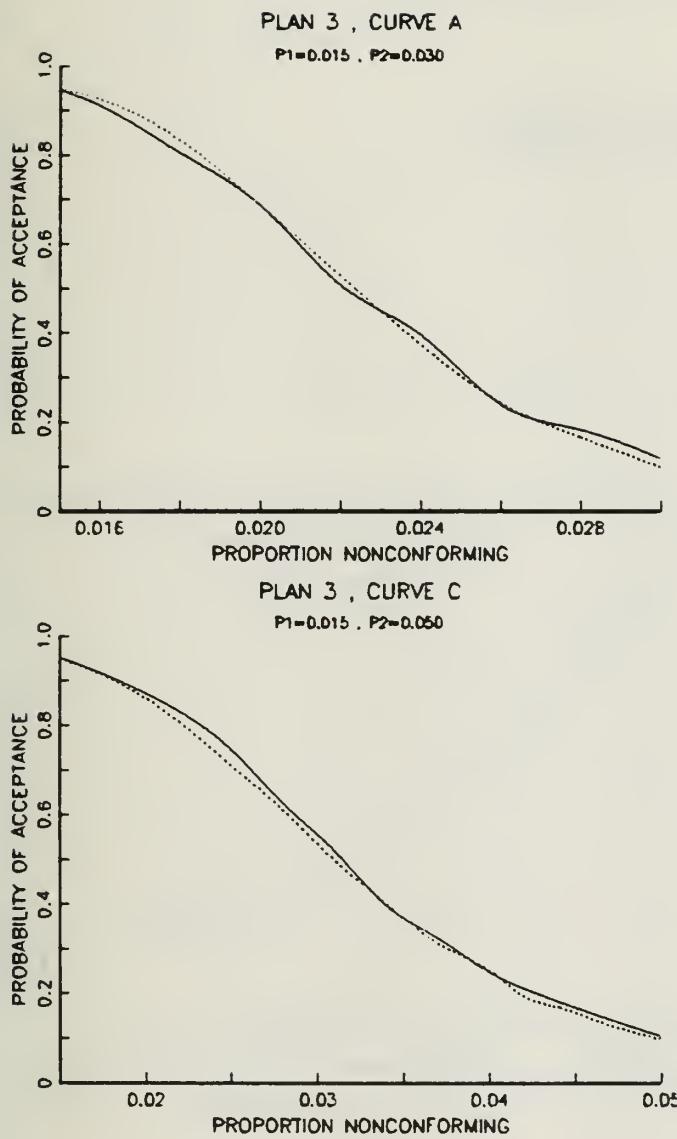


Figure 16 - OC CURVES , PLAN SET III , CURVES A THRU D  
 (SOLID LINE - TRUE , DASHED - THEORETICAL)

PLAN 3 , OC CURVES

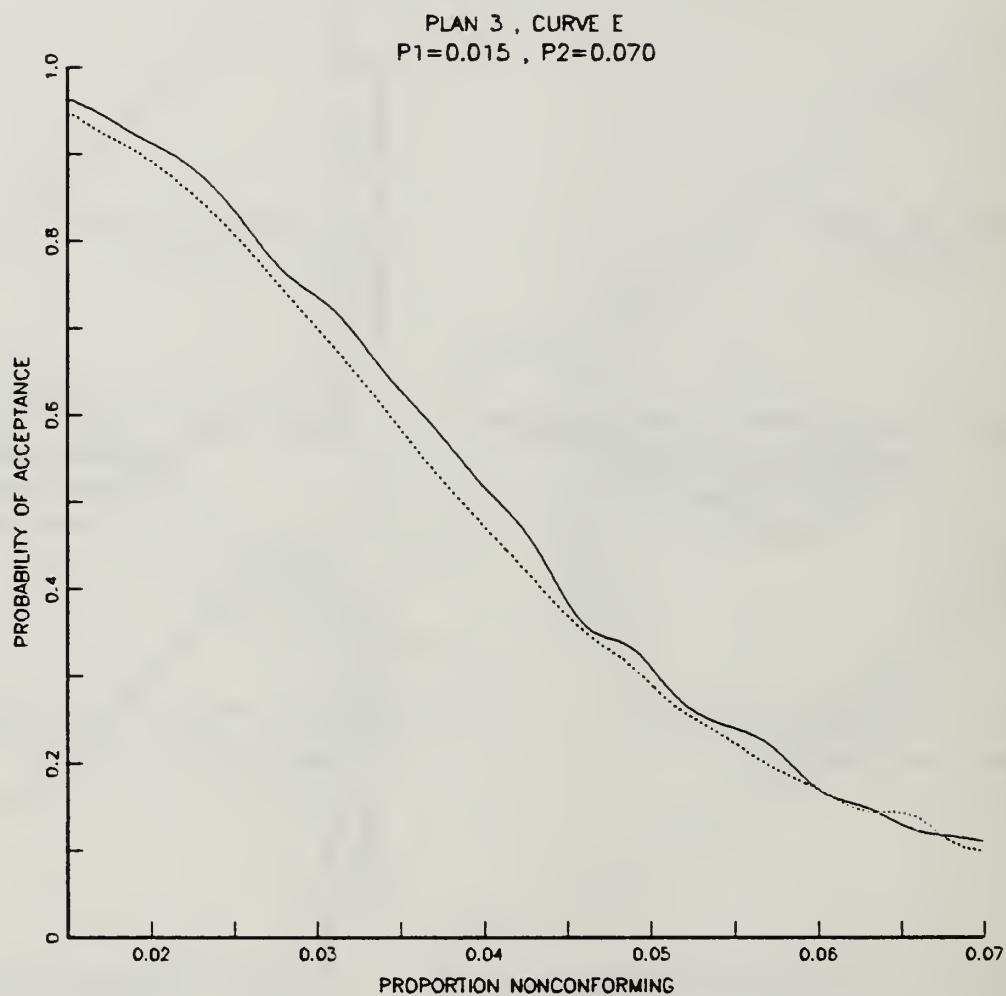


Figure 17 - OC CURVE , PLAN SET III , CURVES E  
(SOLID LINE - TRUE , DASHED - THEORETICAL)

## PLAN 4 , OC CURVES

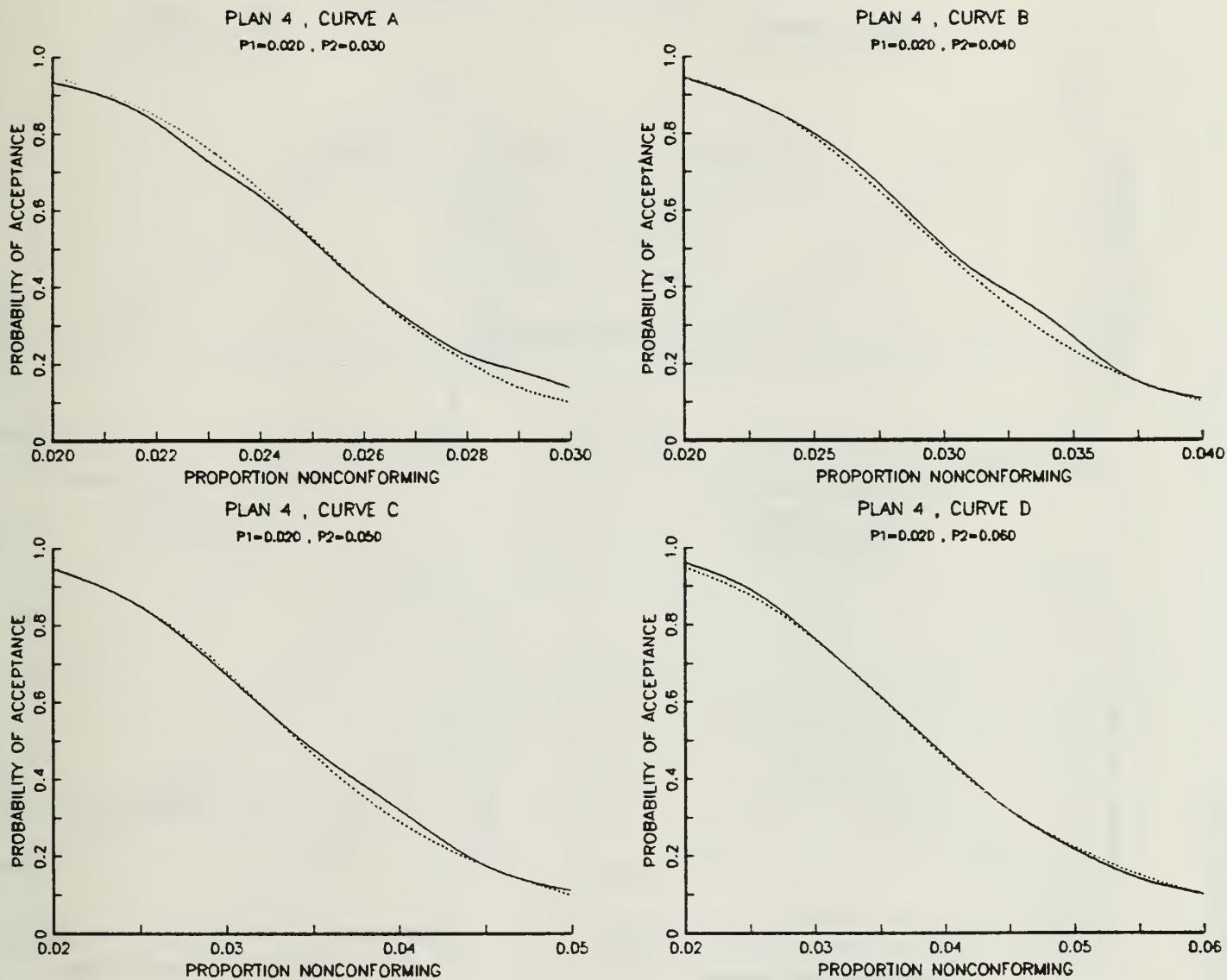


Figure 18 - OC CURVES , PLAN SET IV , CURVES A THRU D  
 (SOLID LINE - TRUE , DASHED - THEORETICAL)

## PLAN 4 , OC CURVES

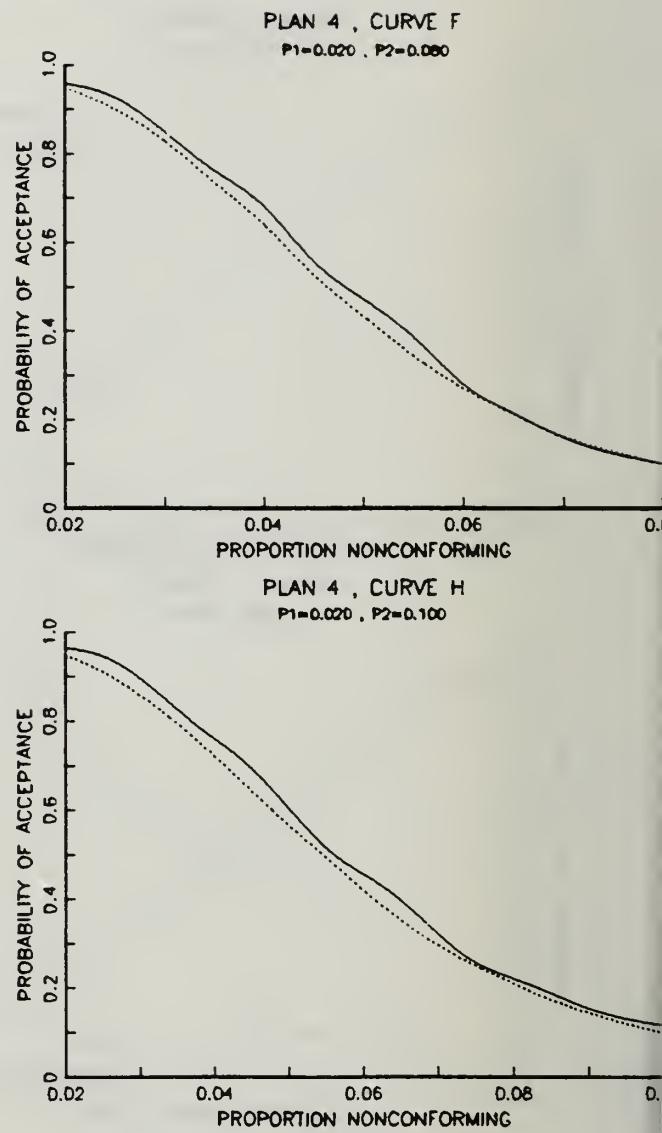
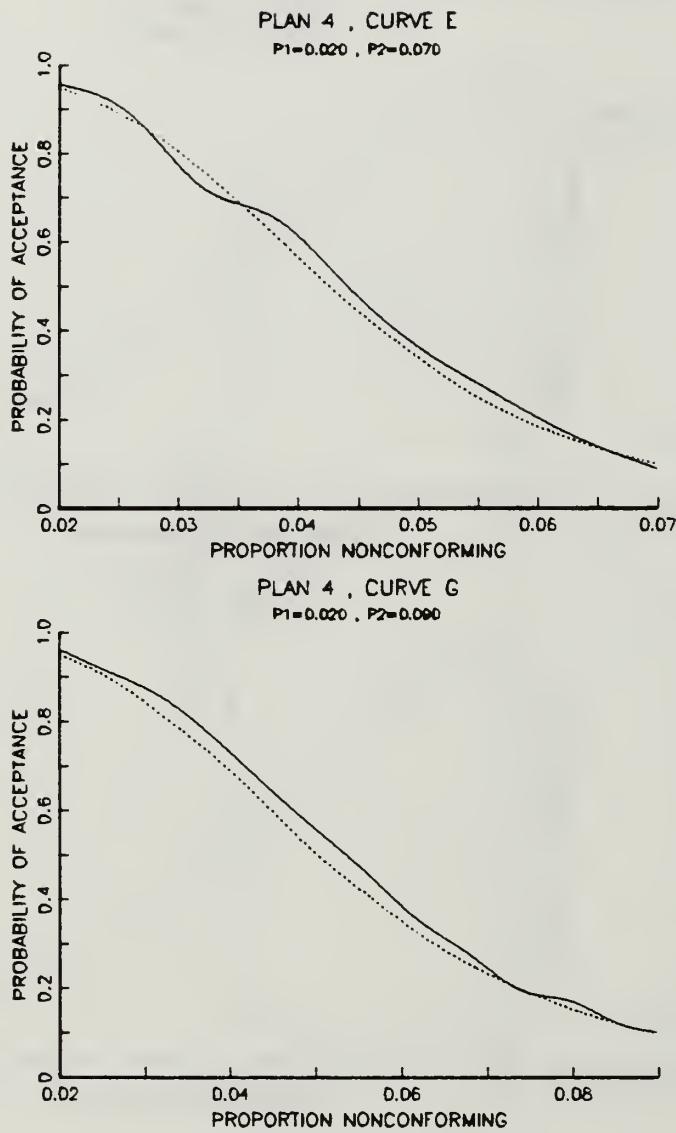


Figure 19 - OC CURVES , PLAN SET IV , CURVES E THRU H  
(SOLID LINE - TRUE , DASHED - THEORETICAL)

APPENDIX D

AVERAGE SAMPLE NUMBERS

PLAN 1 , CURVE A

P1 = 0.005 , P2 = 0.01

SINGLE SAMPLING PLAN

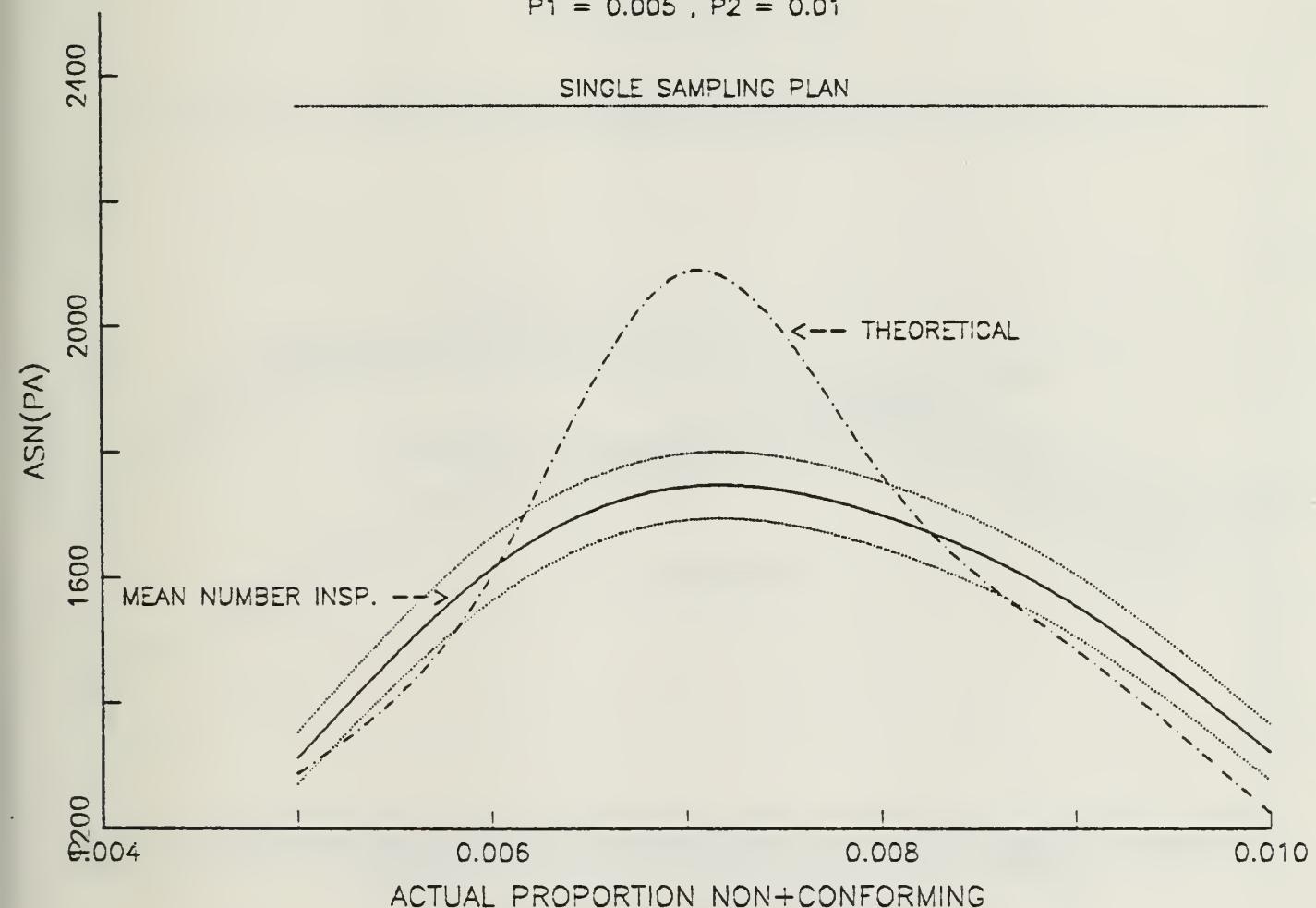


Figure 20 - ASN CURVE , PLAN SET I , CURVE A

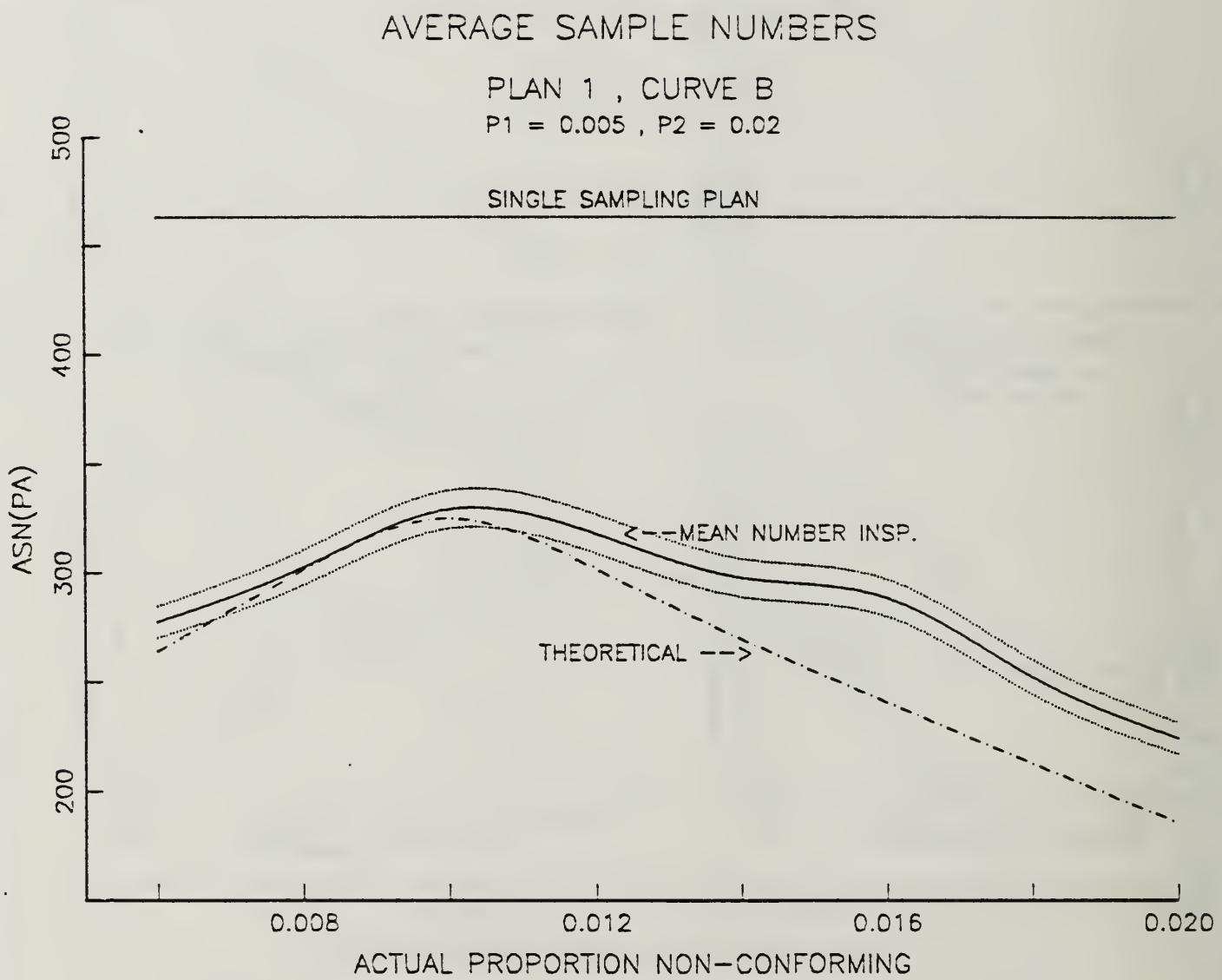


Figure 21 - ASN CURVE , PLAN SET I , CURVE B

### AVERAGE SAMPLE NUMBERS

PLAN 1 , CURVE C

P1 = 0.005 , P2 = 0.03

SINGLE SAMPLING PLAN

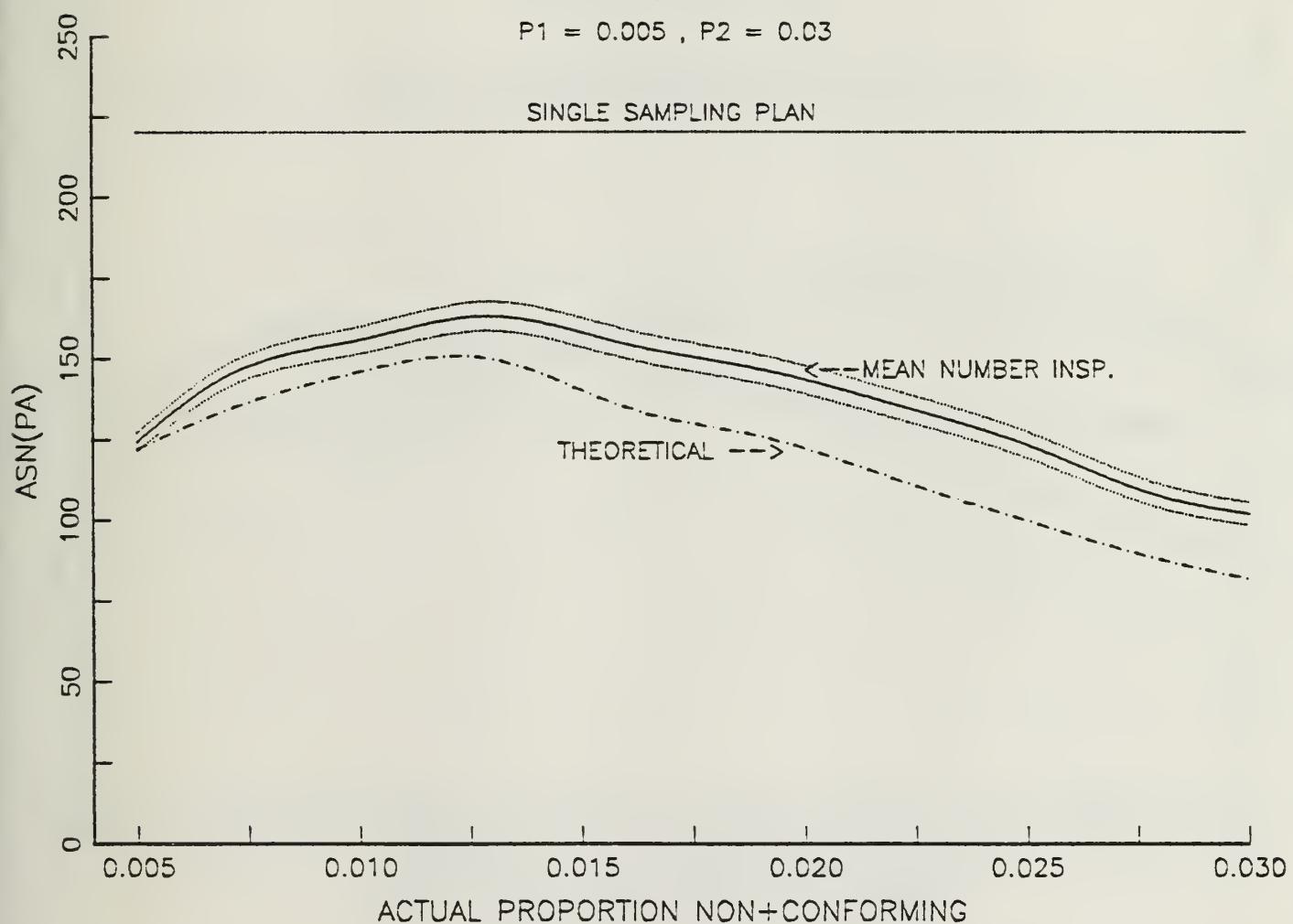


Figure 22 - ASN CURVE , PLAN SET I , CURVE C

## AVERAGE SAMPLE NUMBERS

PLAN 1 , CURVE D  
 $P_1 = 0.005$  ,  $P_2 = 0.04$ 

SINGLE SAMPLING PLAN

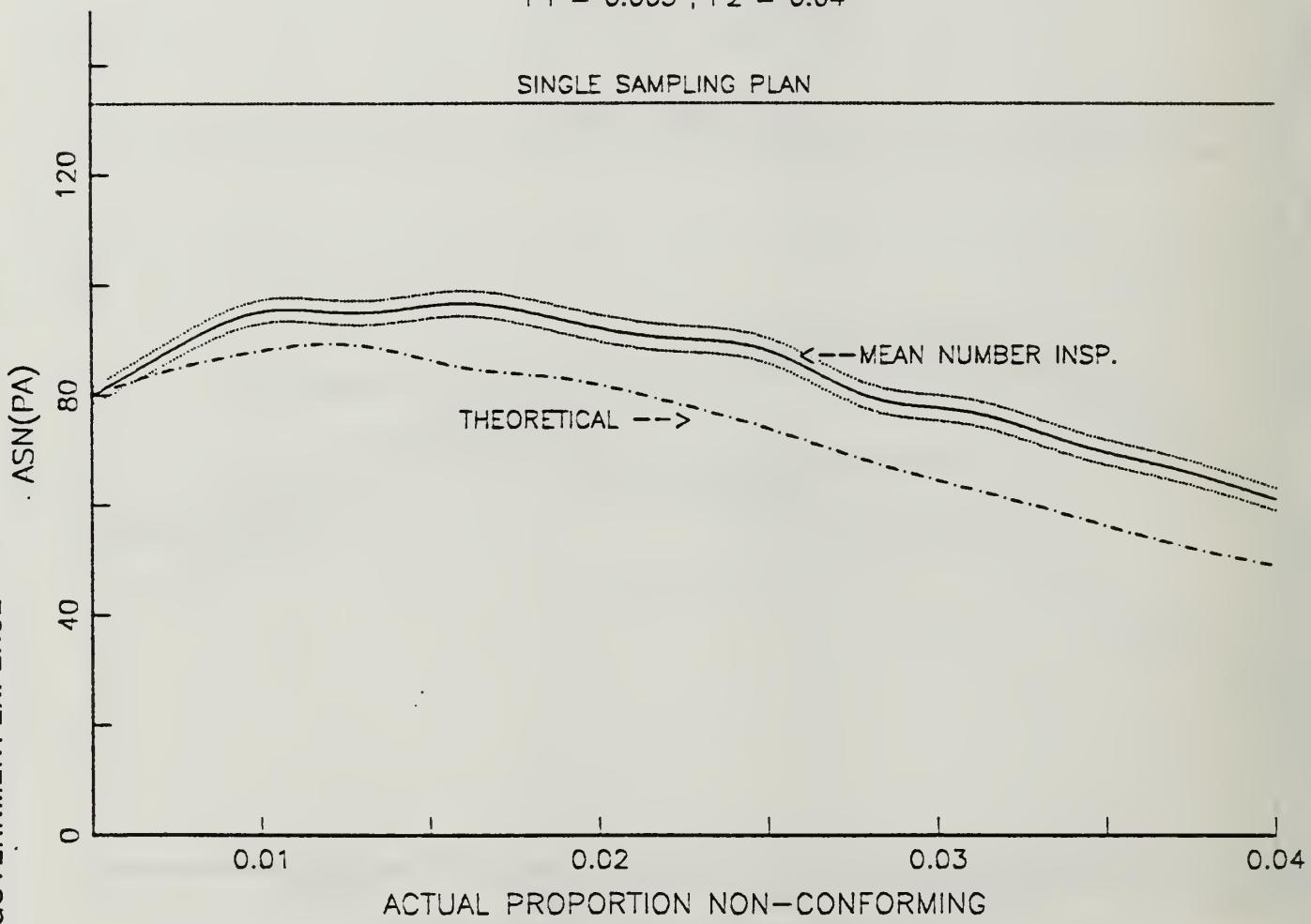


Figure 23 - ASN CURVE , PLAN SET I , CURVE D

### AVERAGE SAMPLE NUMBERS

PLAN 1 , CURVE E

P1 = 0.005 , P2 = 0.05

SINGLE SAMPLING PLAN

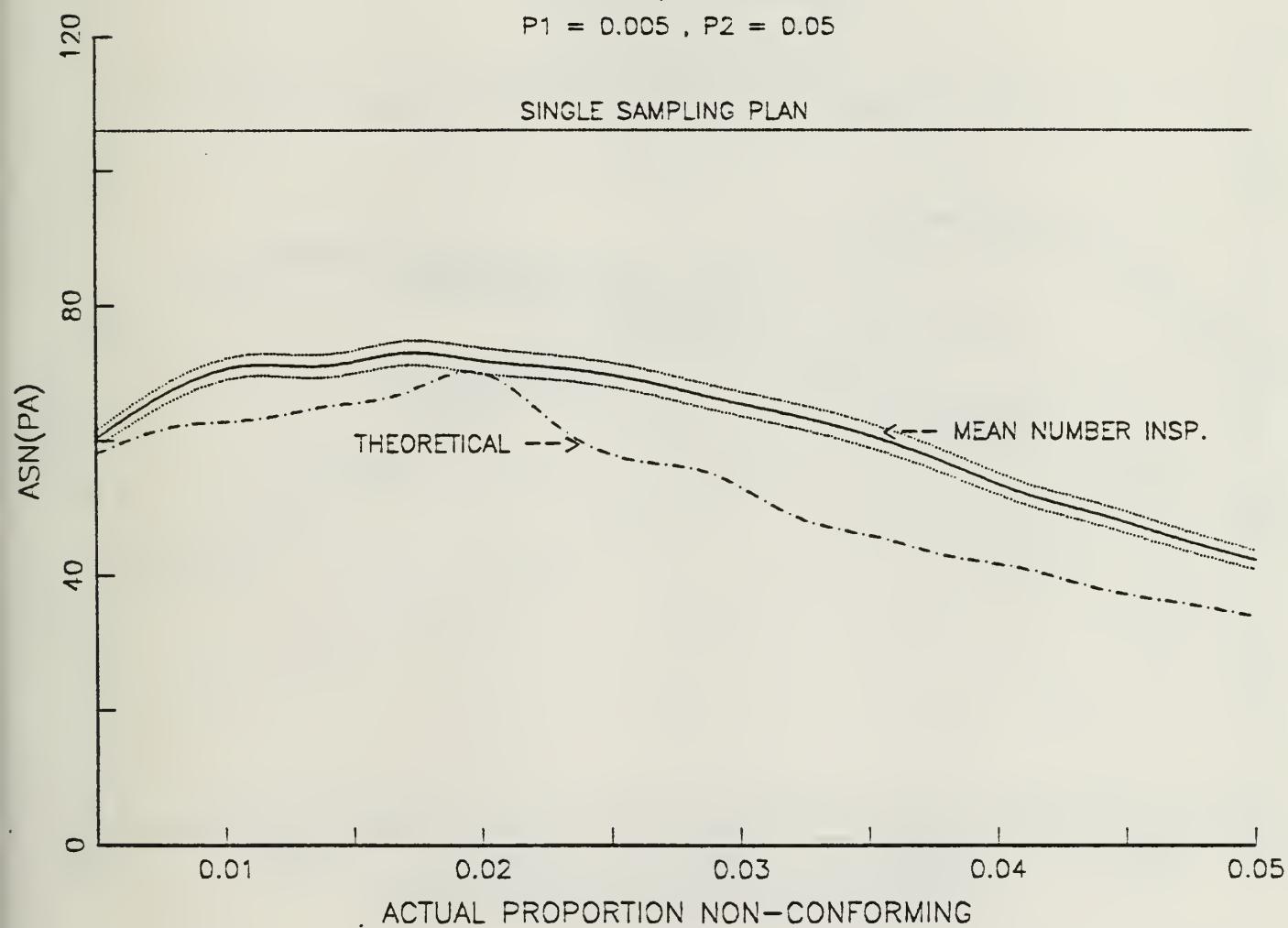


Figure 24 - ASN CURVE , PLAN SET I , CURVE E

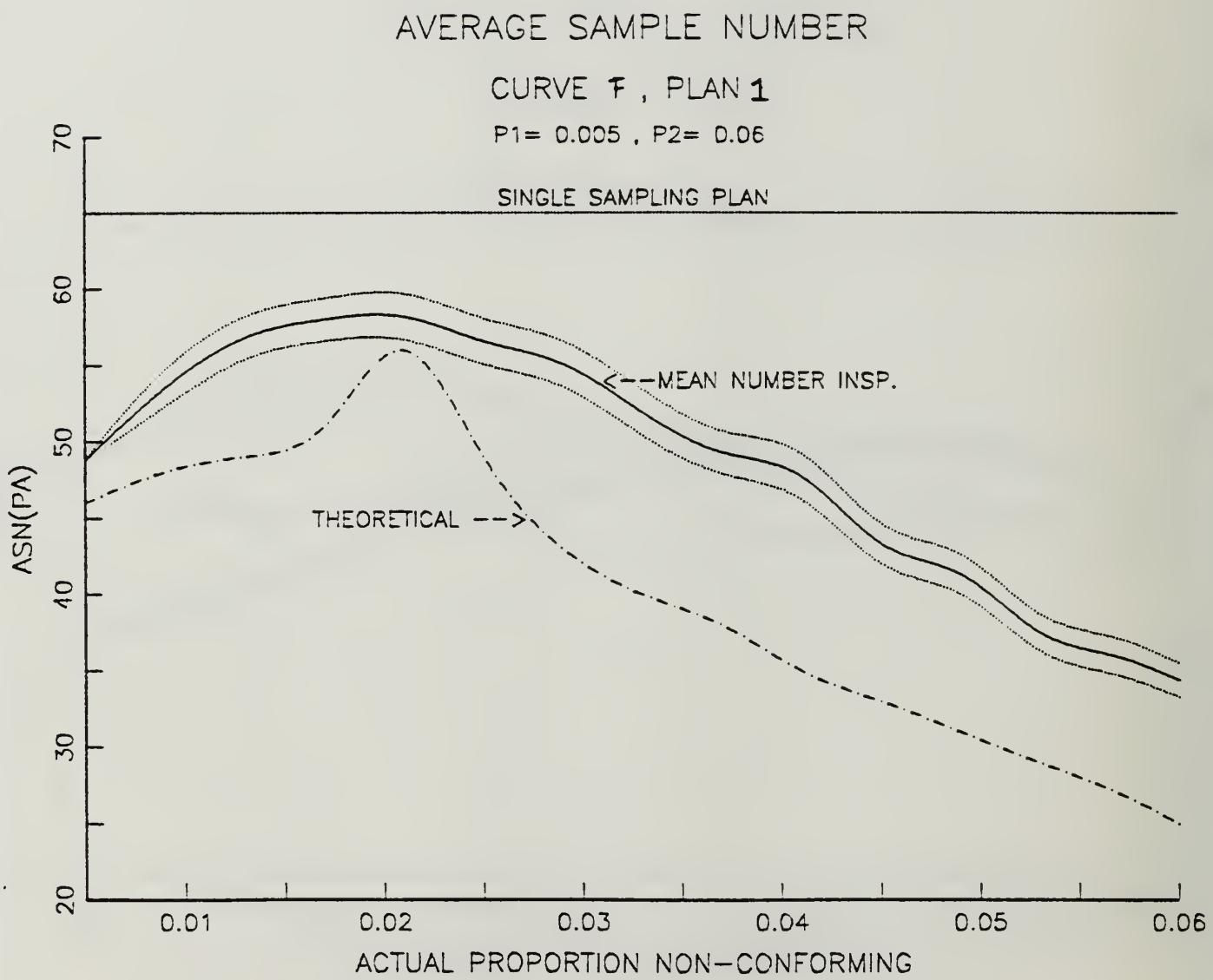


Figure 25 - ASN CURVE , PLAN SET I , CURVE F

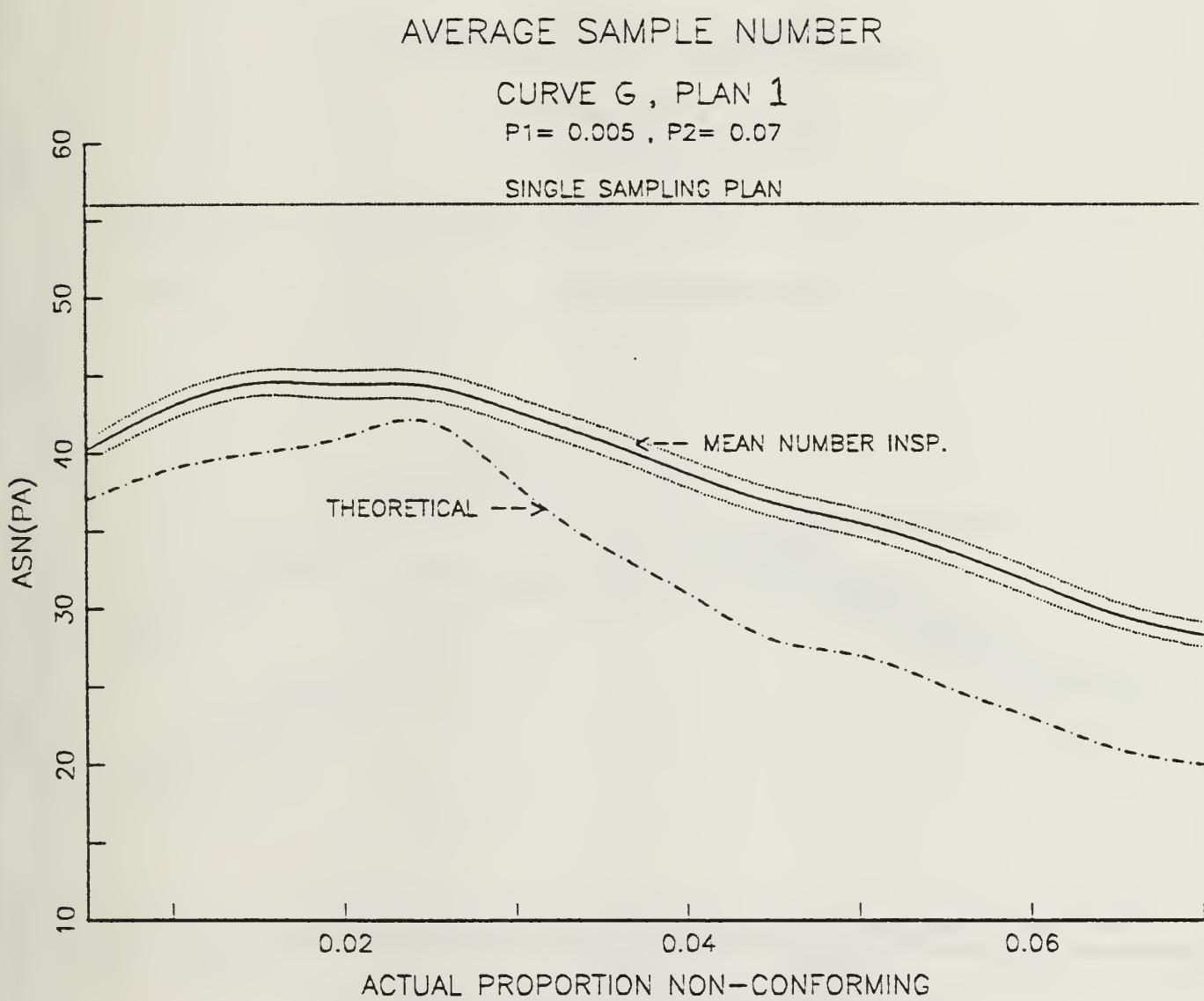


Figure 26 - ASN CURVE , PLAN SET I , CURVE G

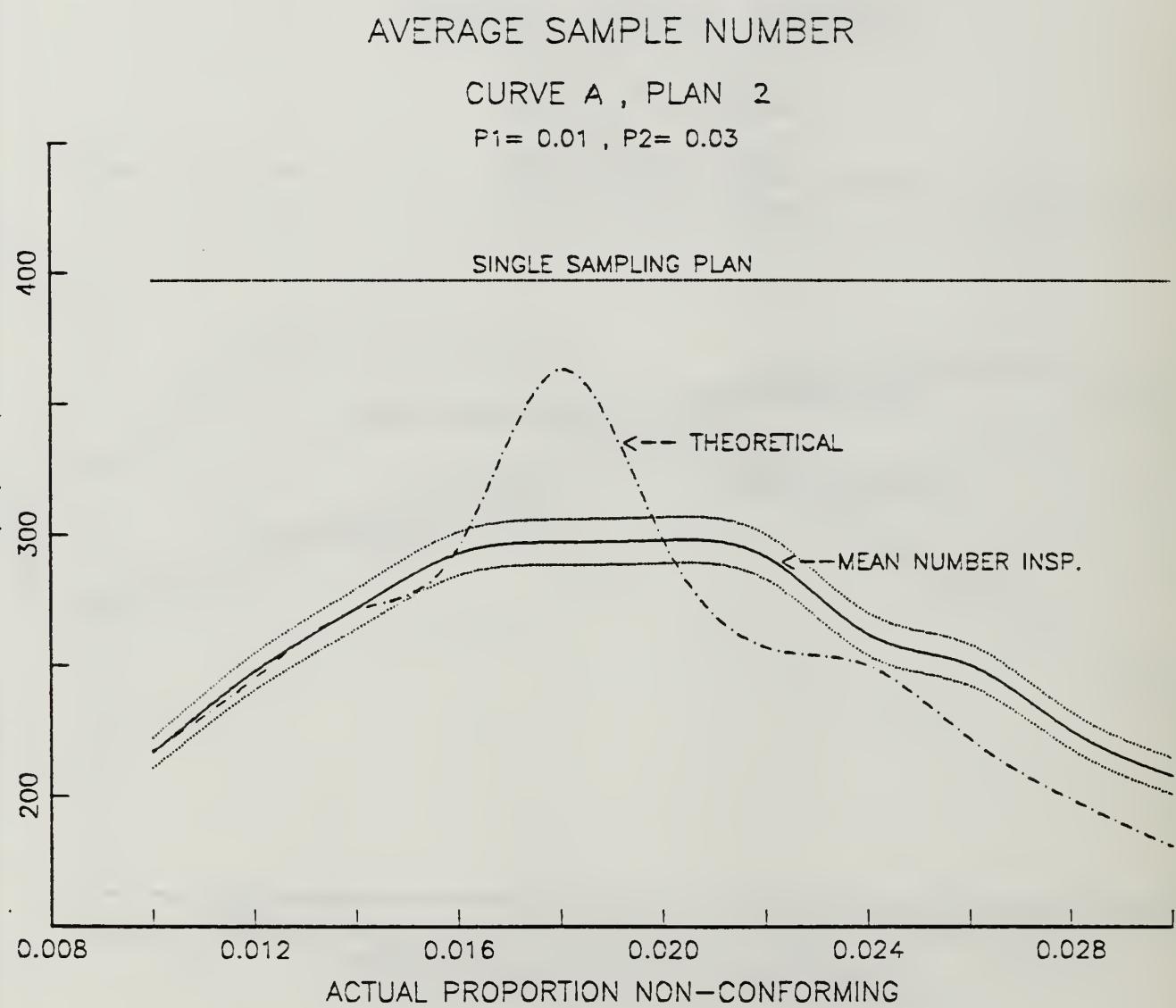


Figure 27 - ASN CURVE , PLAN SET II , CURVE A

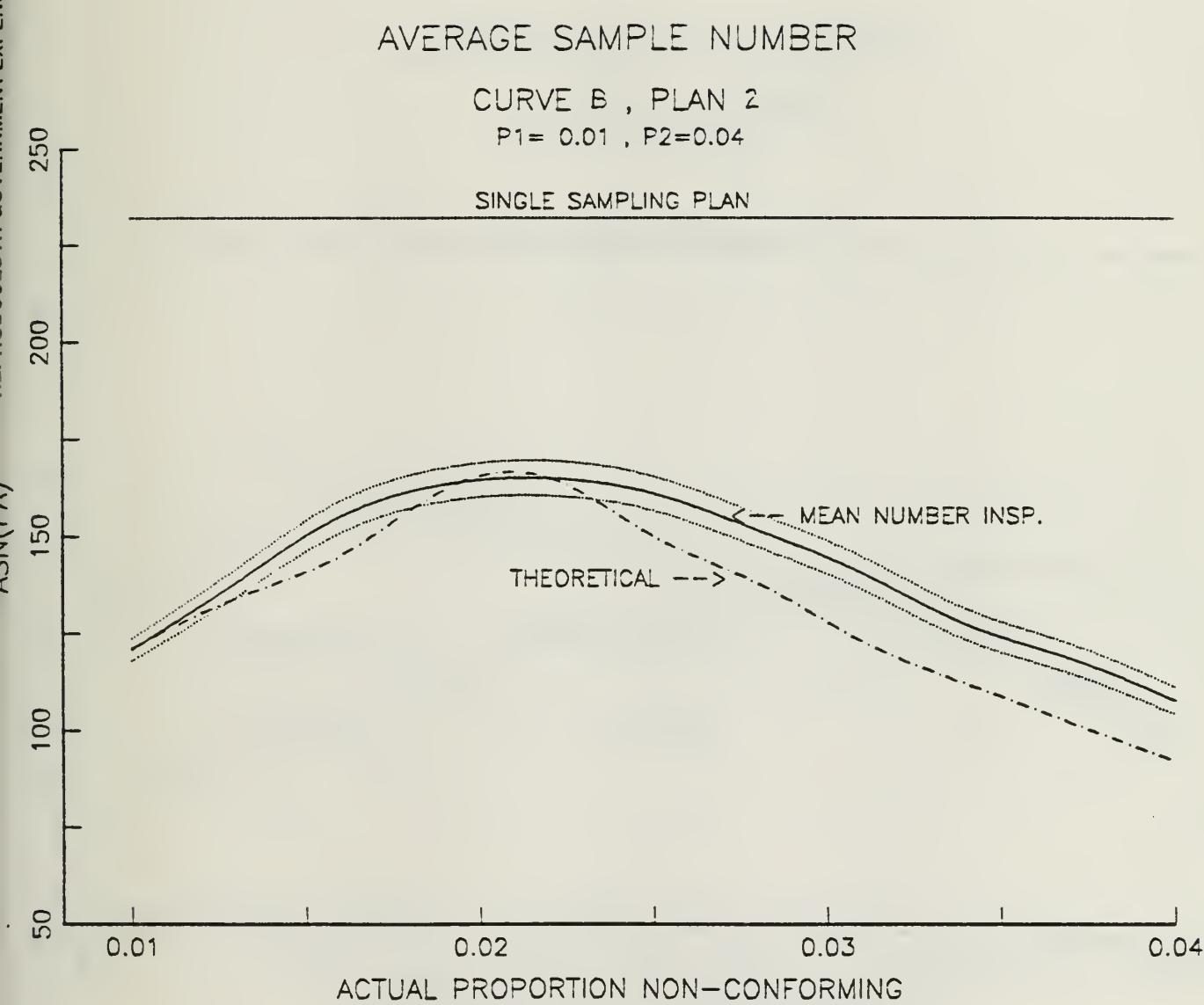


Figure 28 - ASN CURVE , PLAN SET II , CURVE B

REPRODUCED AT GOVERNMENT EXPENSE

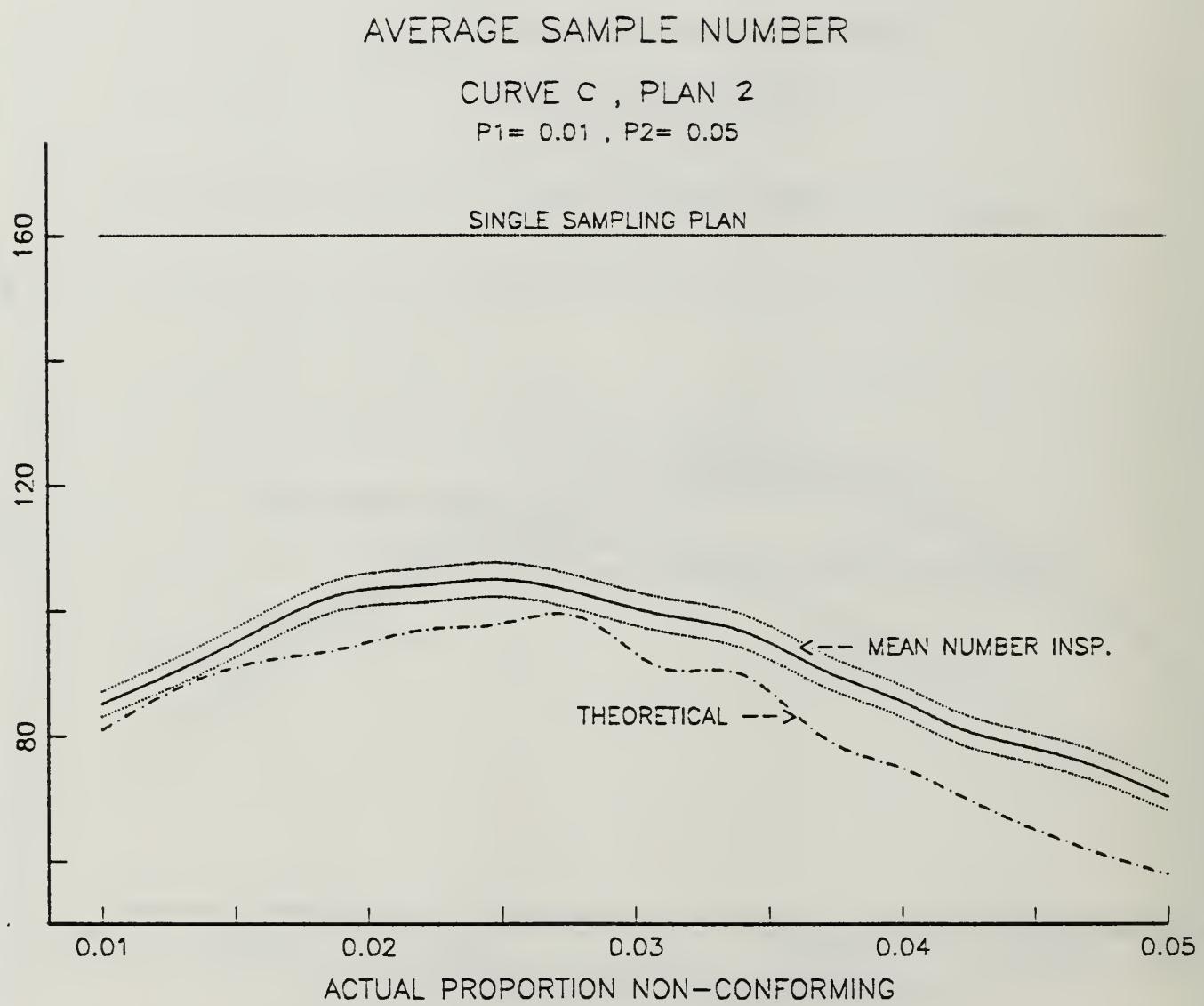


Figure 29 - ASN CURVE , PLAN SET II , CURVE C

## AVERAGE SAMPLE NUMBER

CURVE D , PLAN 2

 $P_1 = 0.01$  ,  $P_2 = 0.06$ 

SINGLE SAMPLING PLAN

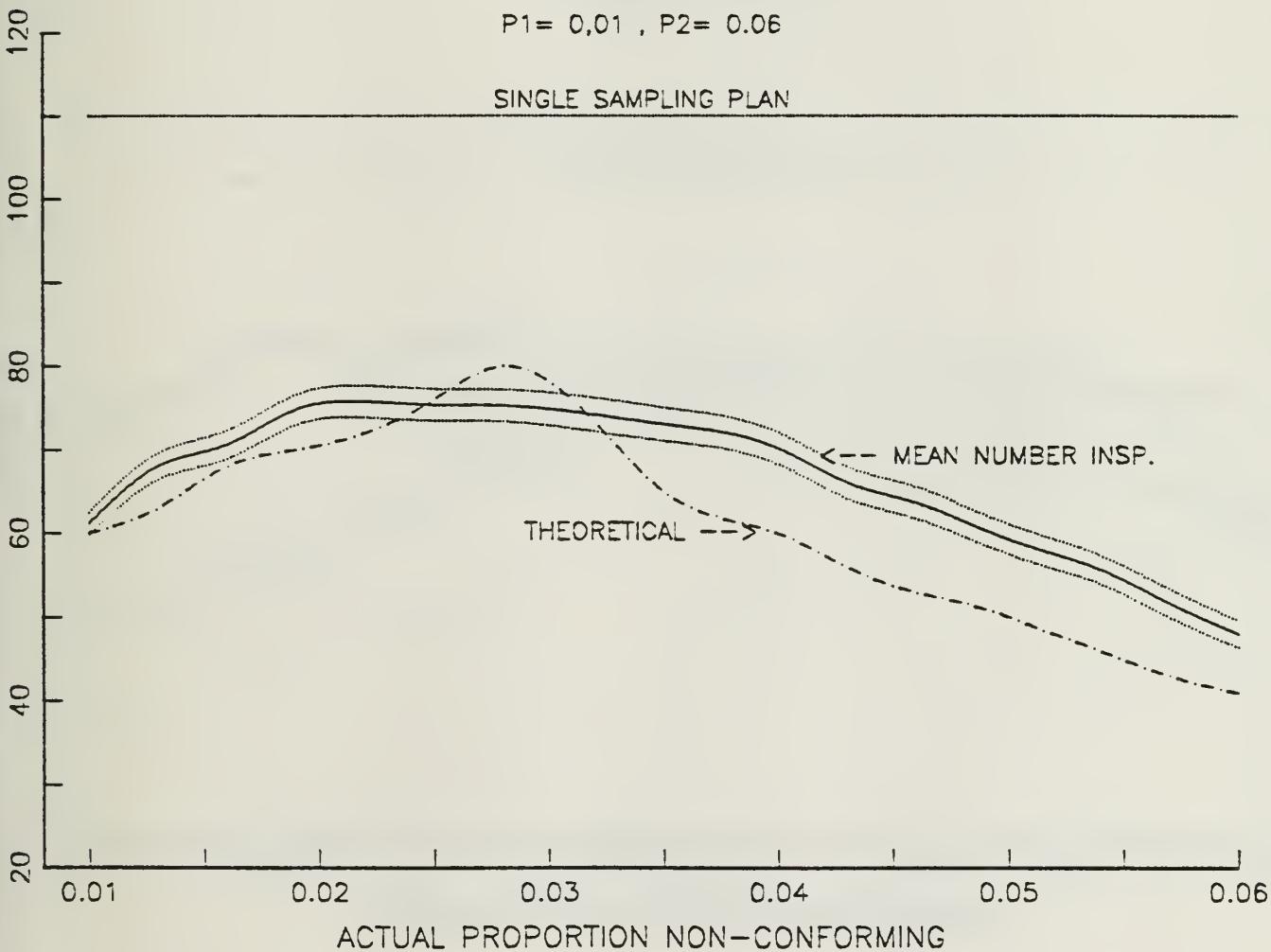


Figure 30 - ASN CURVE , PLAN SET II , CURVE D

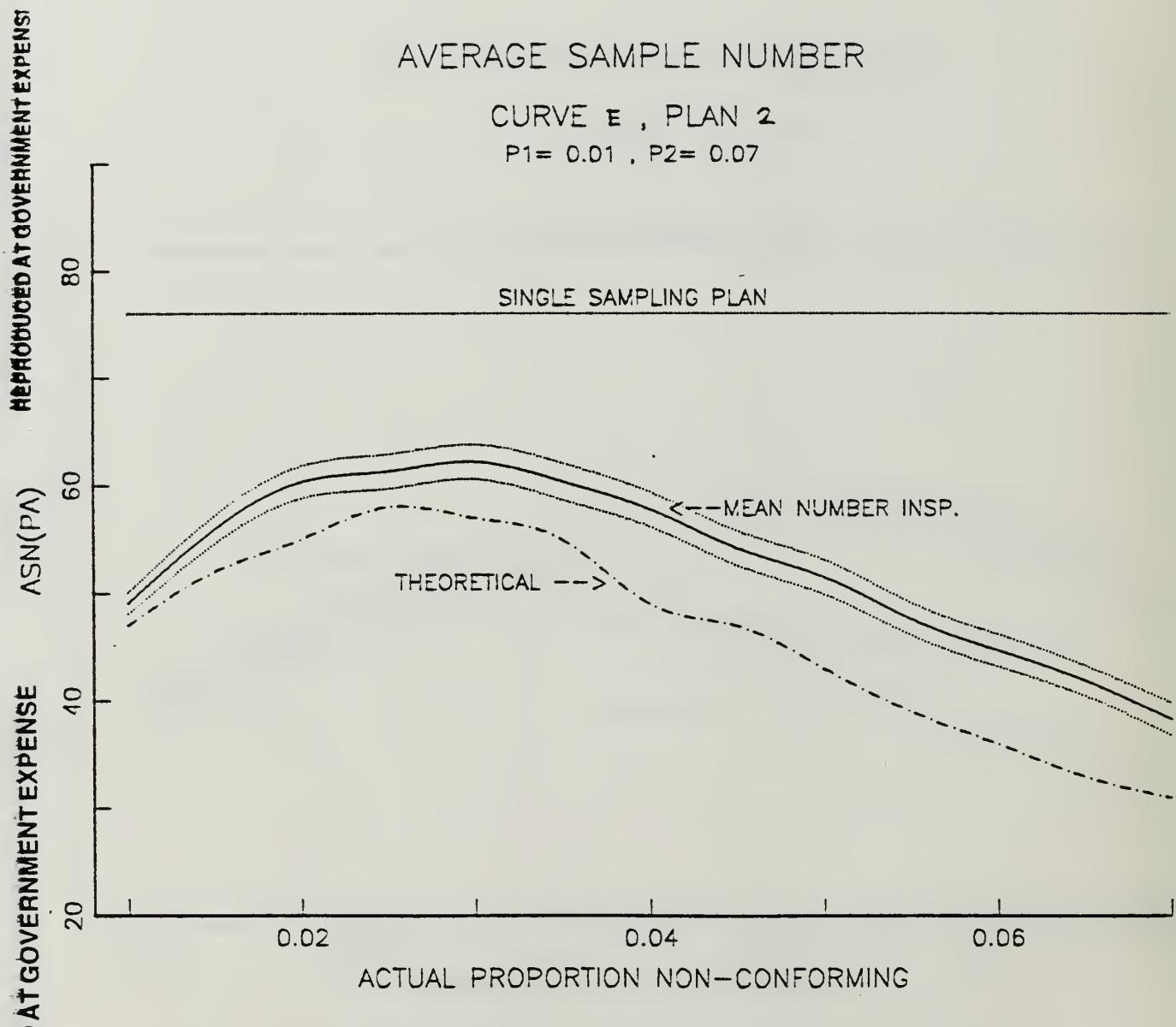


Figure 31 - ASN CURVE , PLAN SET II , CURVE E

## AVERAGE SAMPLE NUMBER

CURVE F , PLAN 2

P1= 0.01 , P2= 0.08

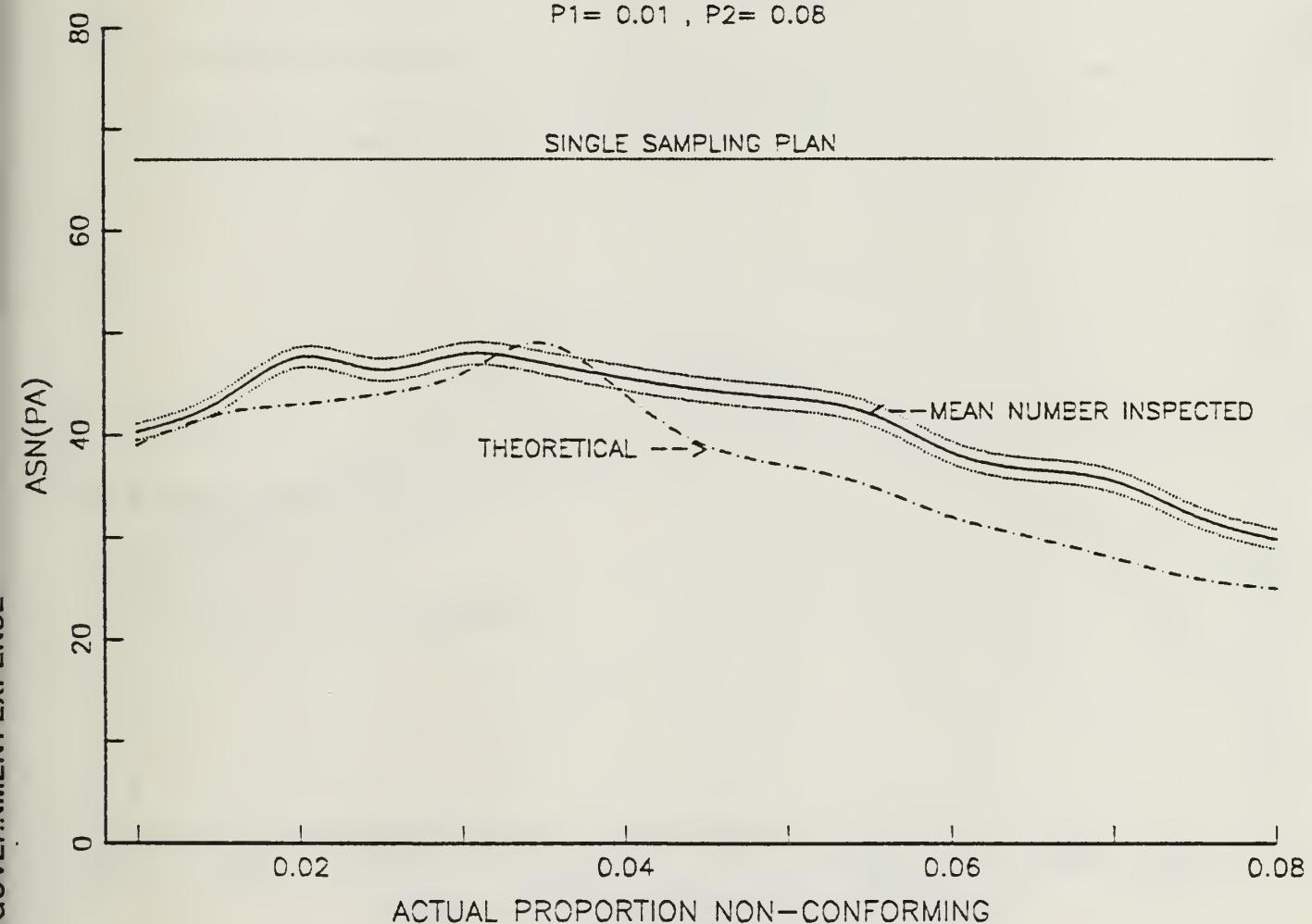


Figure 32 - ASN CURVE , PLAN SET II , CURVE F

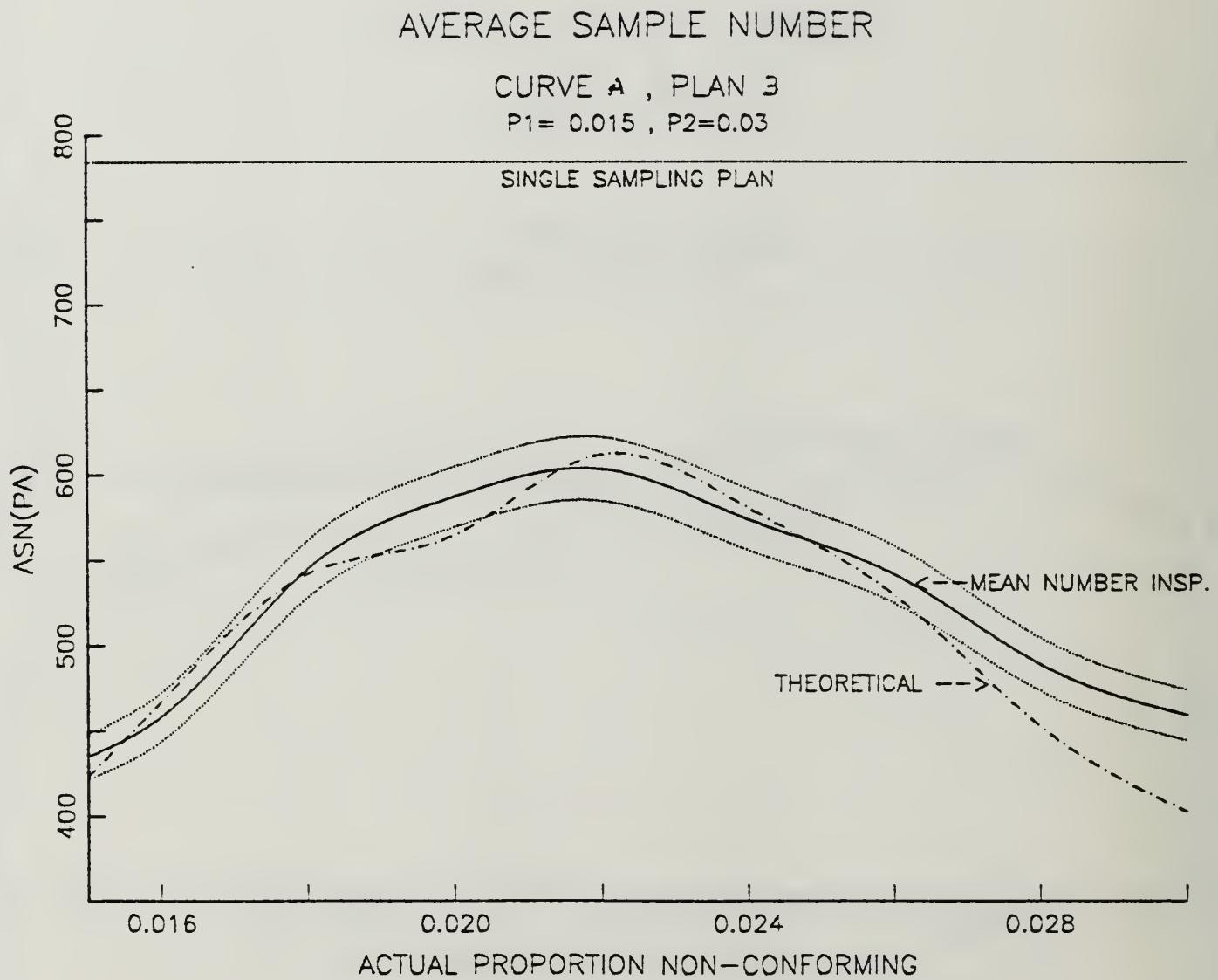


Figure 33 - ASN CURVE , PLAN SET III , CURVE A

### AVERAGE SAMPLE NUMBER

CURVE B , PLAN 3

P1= 0.015 , P2= 0.040

SINGLE SAMPLING PLAN

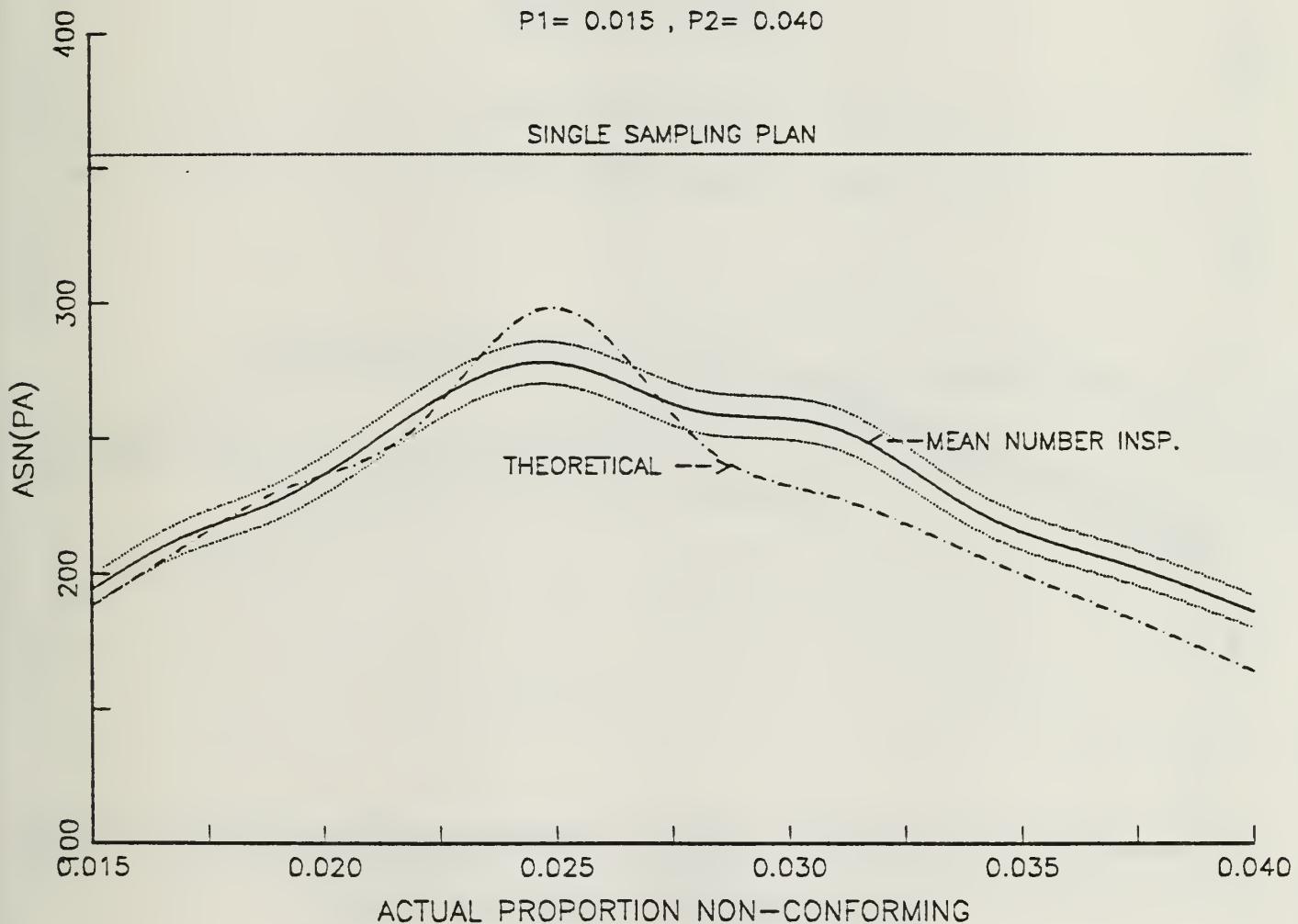


Figure 34 - ASN CURVE , PLAN SET III , CURVE B

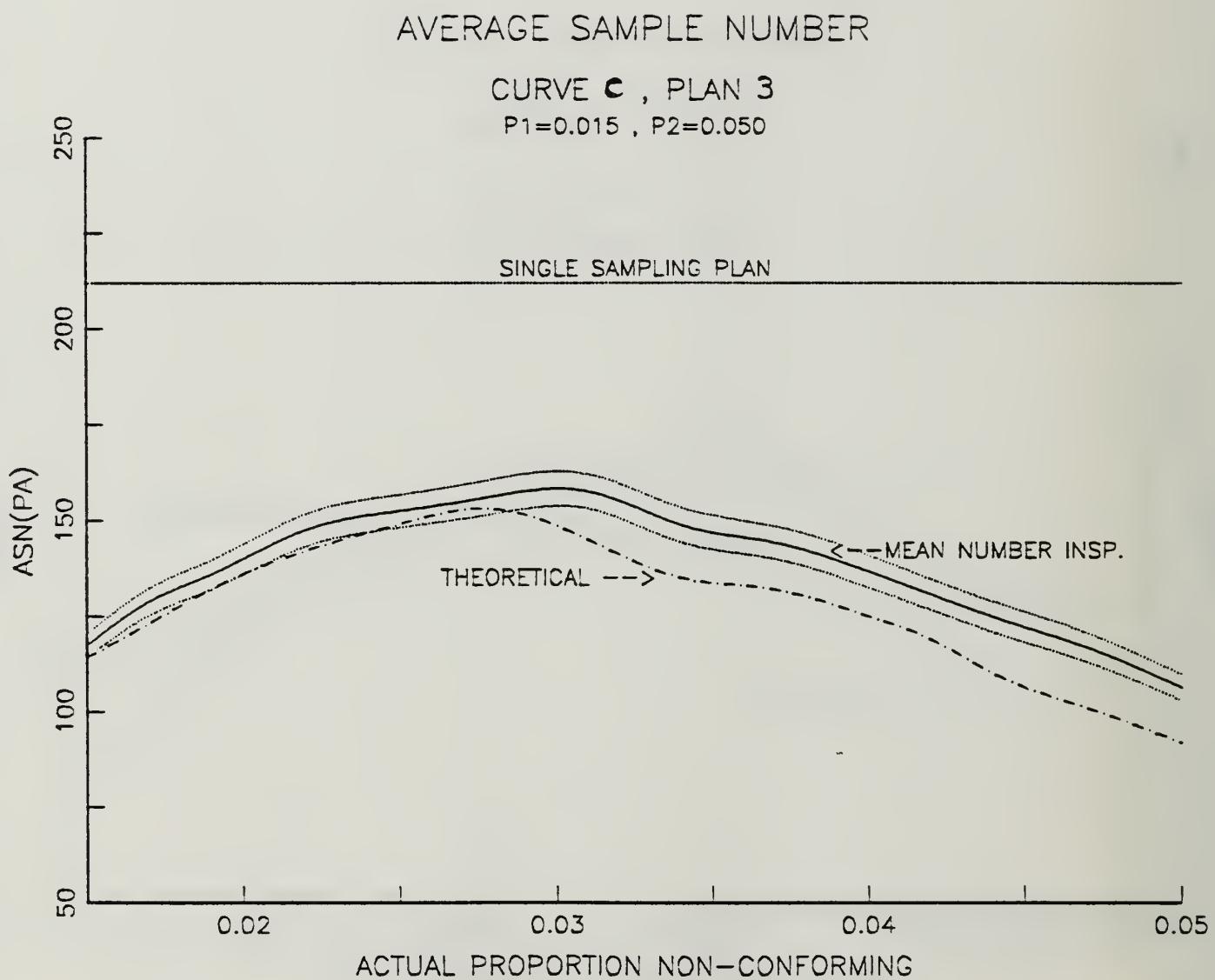


Figure 35 - ASN CURVE , PLAN SET III , CURVE C

AVERAGE SAMPLE NUMBER

CURVE D , PLAN 3

P1= 0.015 , P2=0.06

SINGLE SAMPLING PLAN

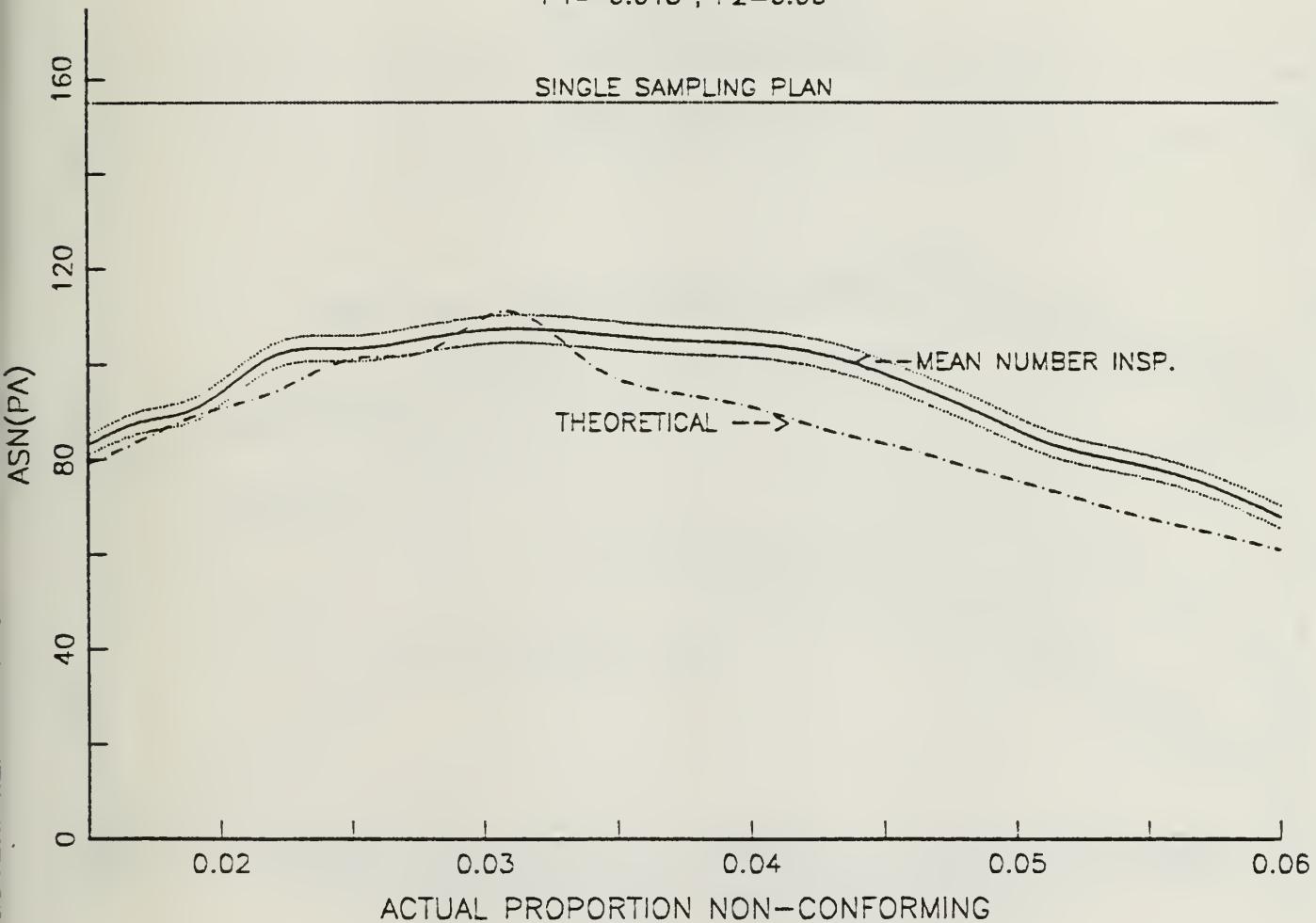


Figure 36 - ASN CURVE , PLAN SET III , CURVE D

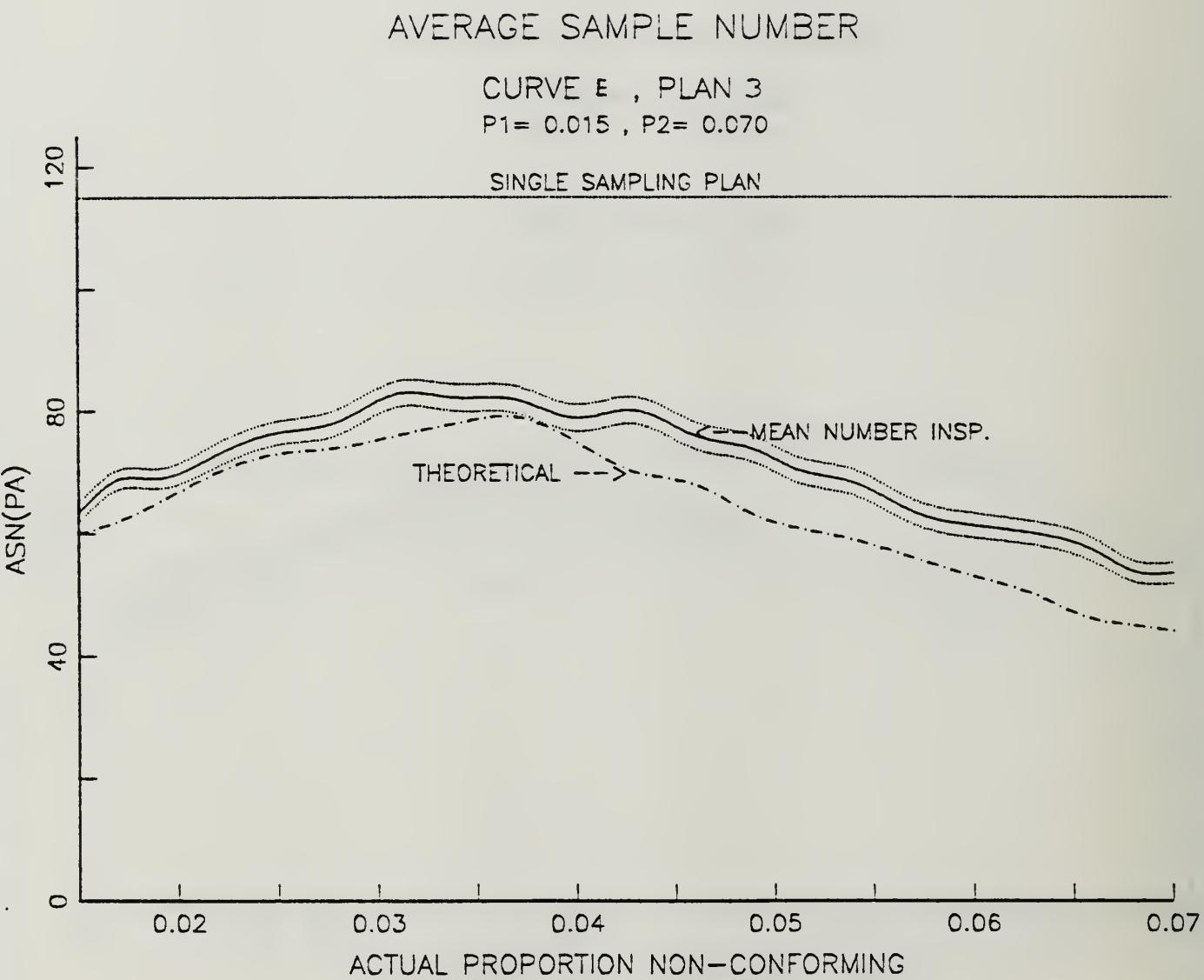


Figure 37 - ASN CURVE , PLAN SET III , CURVE E

# AVERAGE SAMPLE NUMBER

CURVE A , PLAN 4

P1= 0.020 , P2= 0.030

SINGLE SAMPLING PLAN

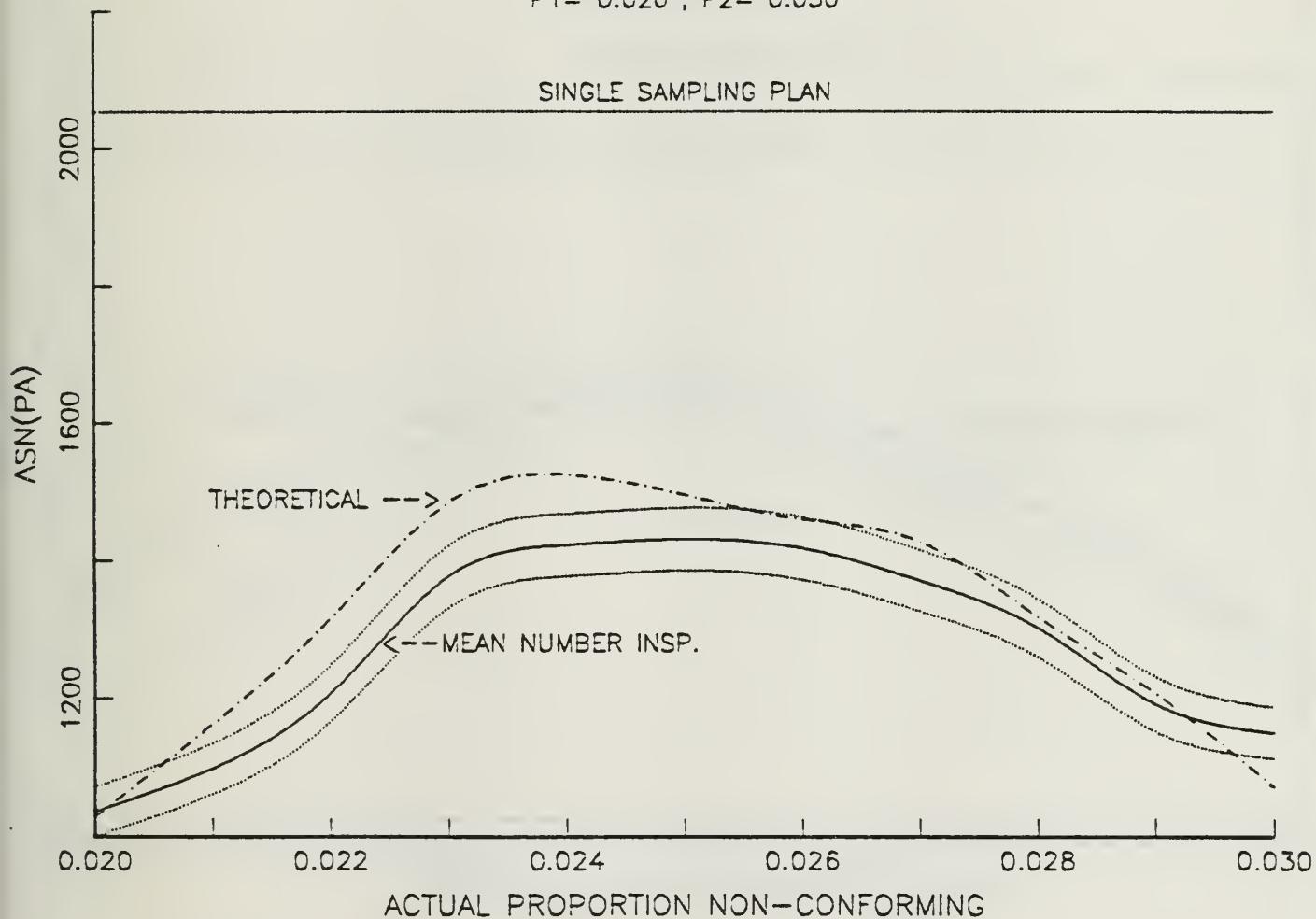


Figure 38 - ASN CURVE , PLAN SET IV , CURVE A

REPRODUCED AT GOVERNMENT EXPENSE

AVERAGE SAMPLE NUMBER

CURVE B , PLAN 4

P1= 0.020 , P2= 0.040

SINGLE SAMPLING PLAN

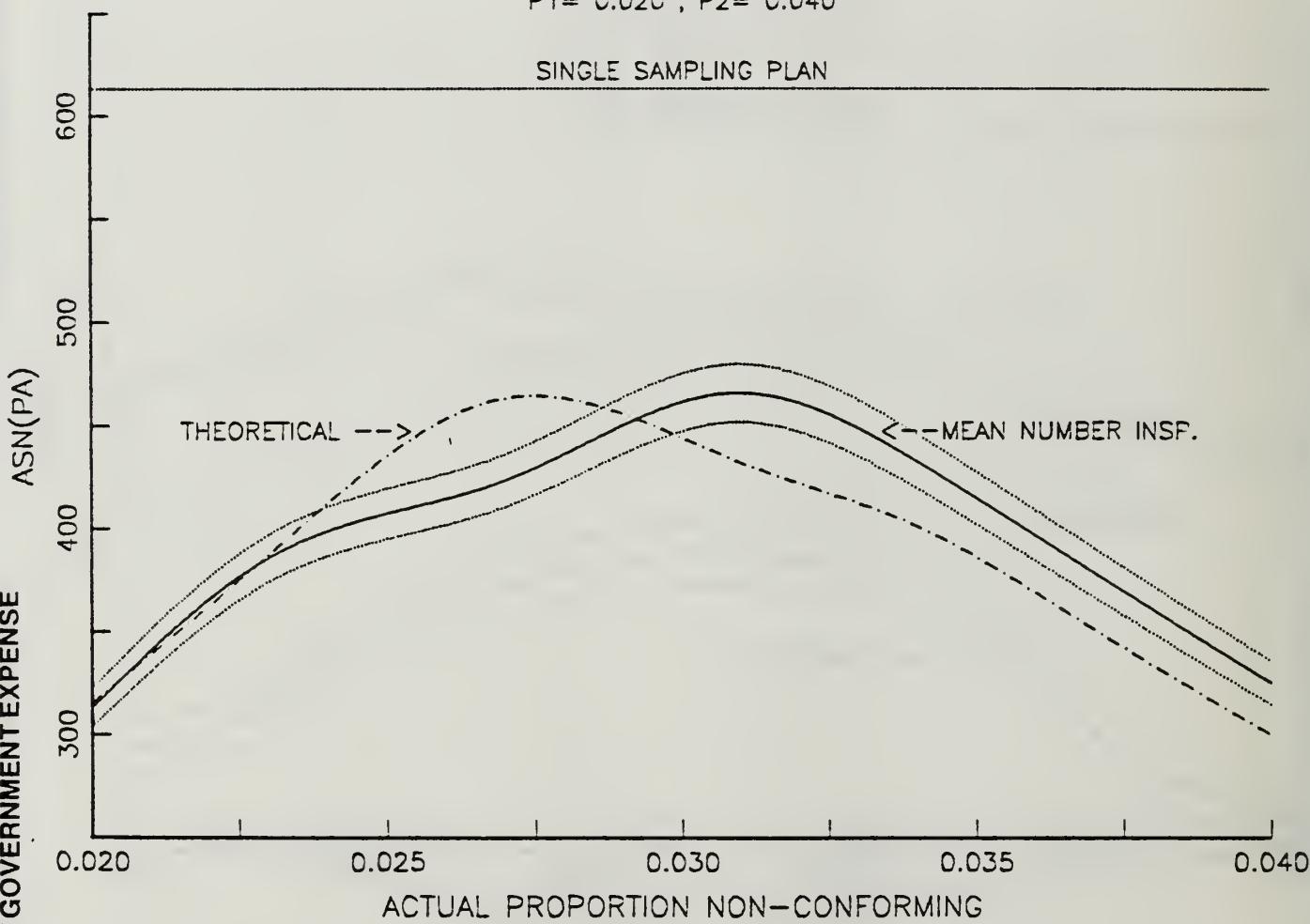


Figure 39 - ASN CURVE , PLAN SET IV , CURVE B

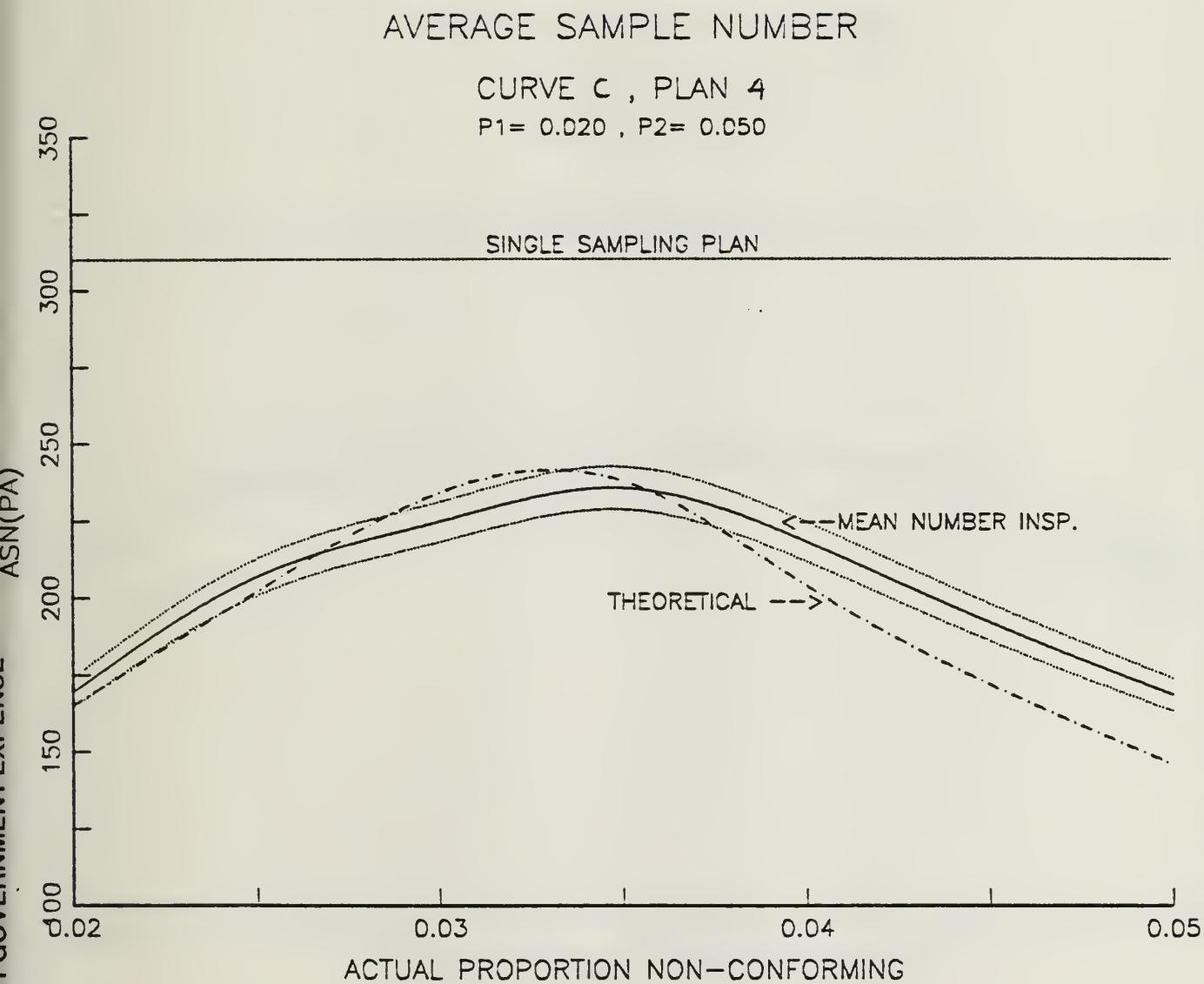


Figure 40 - ASN CURVE , PLAN SET IV , CURVE C

REPRODUCED AT GOVERNMENT EXPENSE

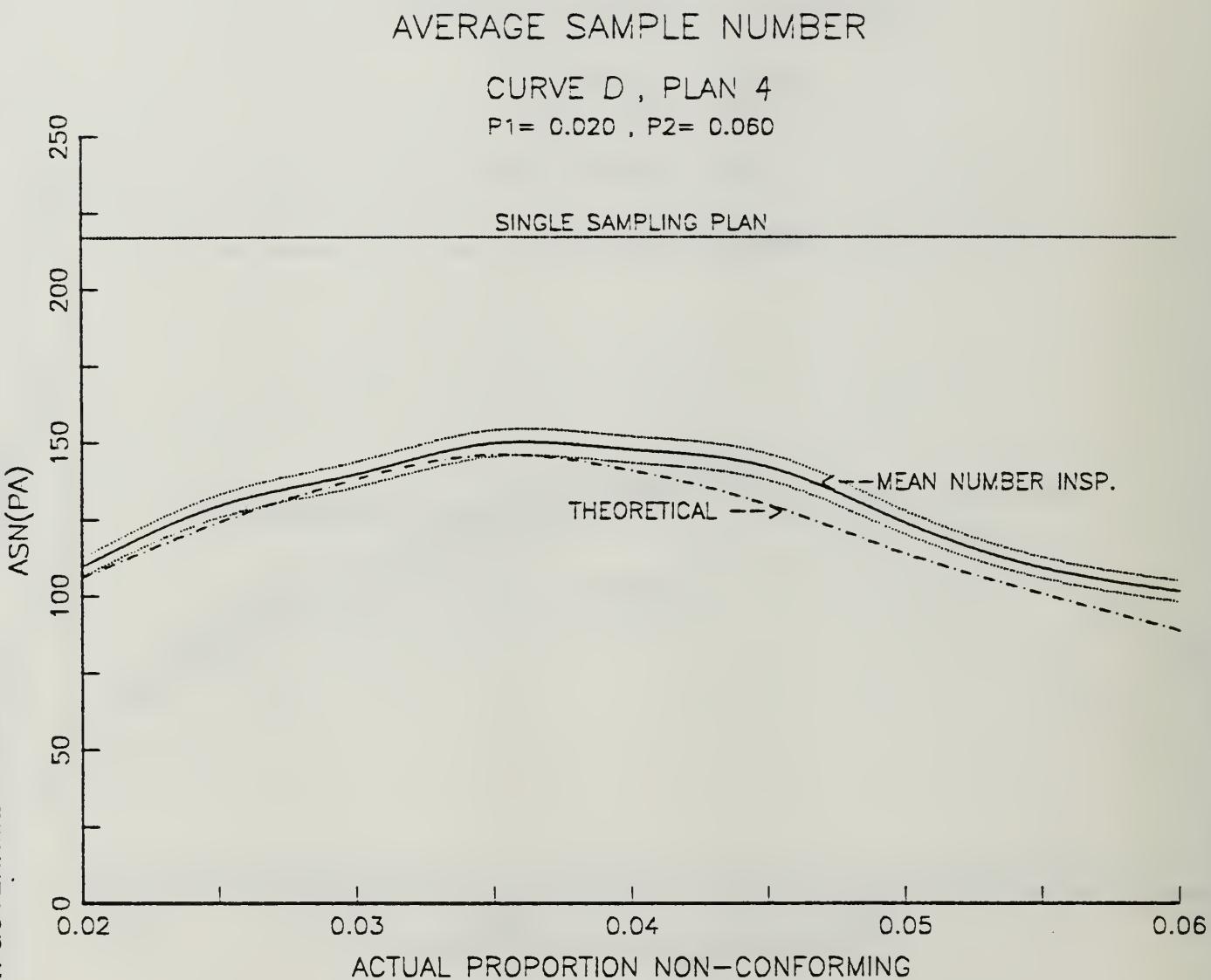


Figure 41 - ASN CURVE , PLAN SET IV , CURVE D

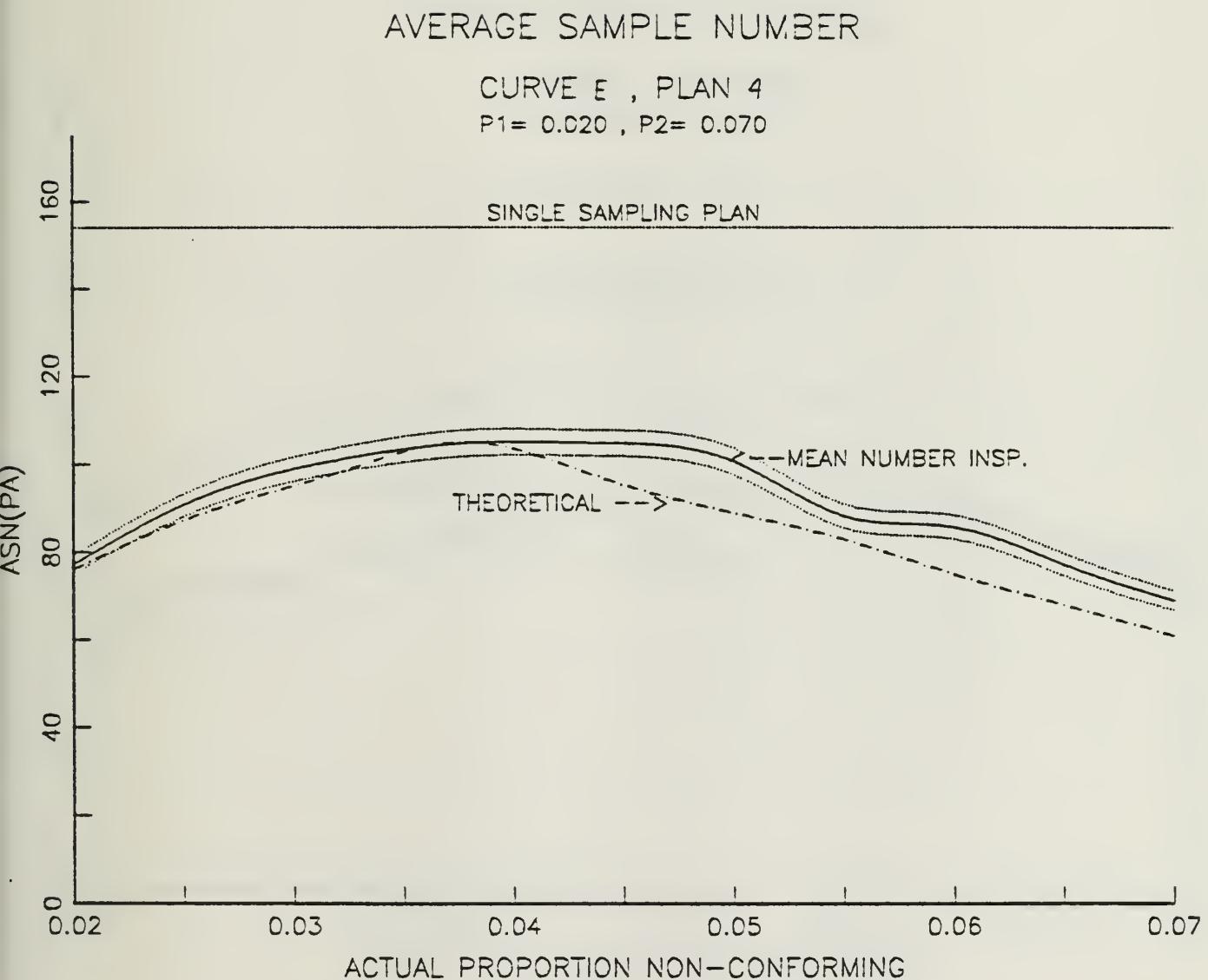


Figure 42 - ASN CURVE , PLAN SET IV , CURVE E

### AVERAGE SAMPLE NUMBER

CURVE F , PLAN 4

P<sub>1</sub>= 0.020 , P<sub>2</sub>= 0.080

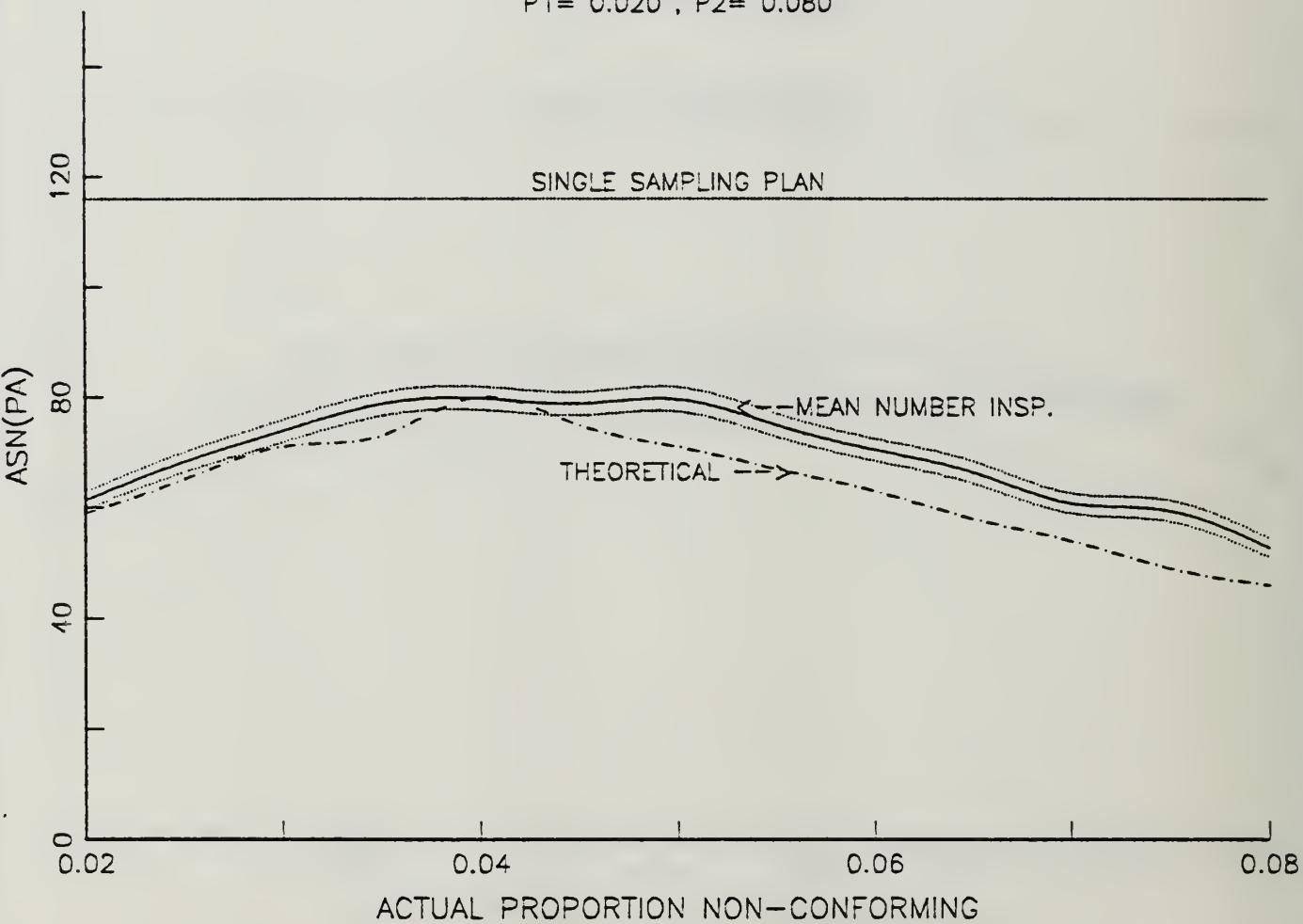


Figure 43 - ASN CURVE , PLAN SET IV , CURVE F

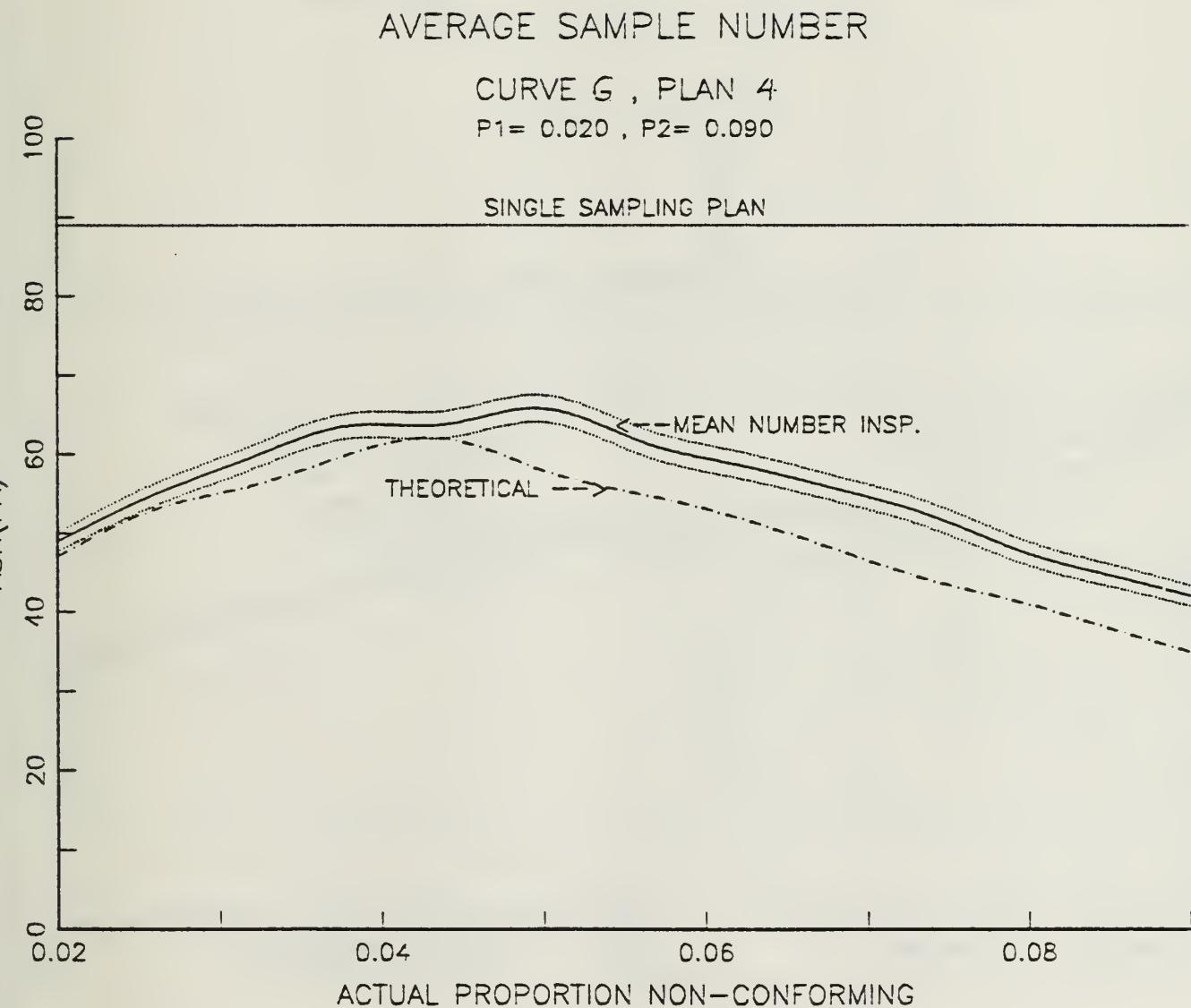


Figure 44 - ASN CURVE , PLAN SET IV , CURVE G

REPRODUCED AT GOVERNMENT EXPENSE

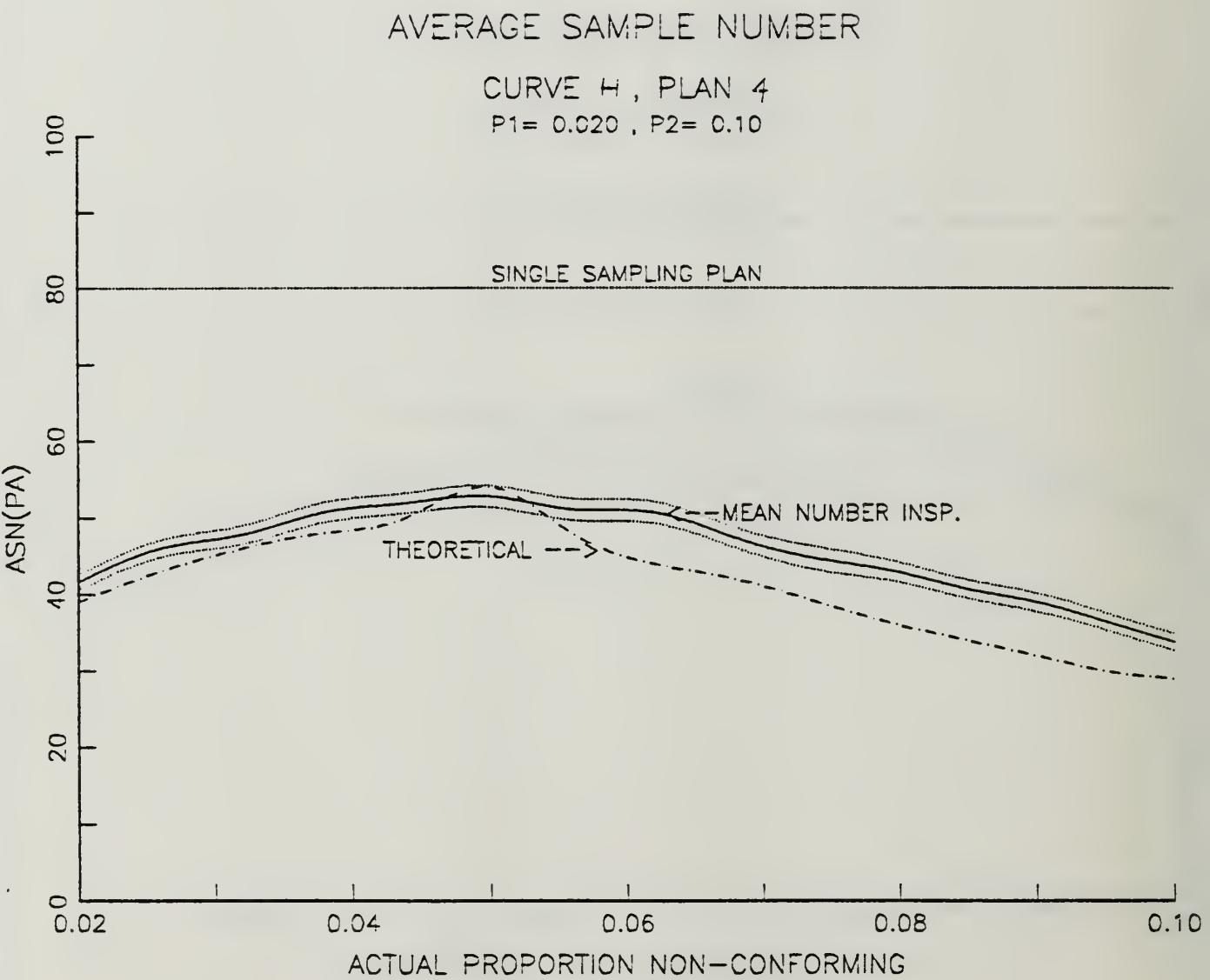


Figure 45 - ASN CURVE , PLAN SET IV , CURVE H

## APPENDIX E

### PROBABILITY OF USING STOPPING RULE

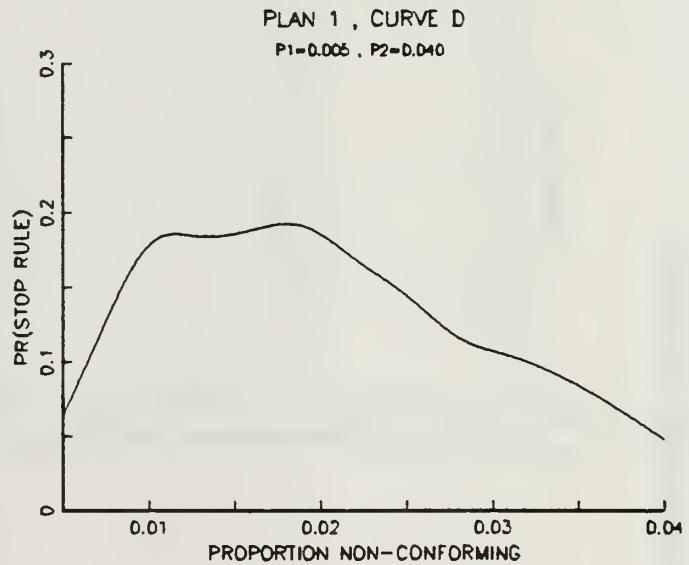
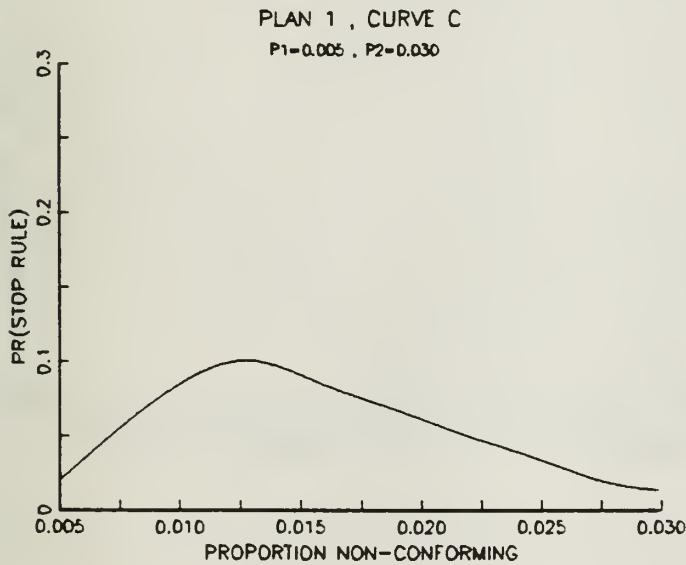
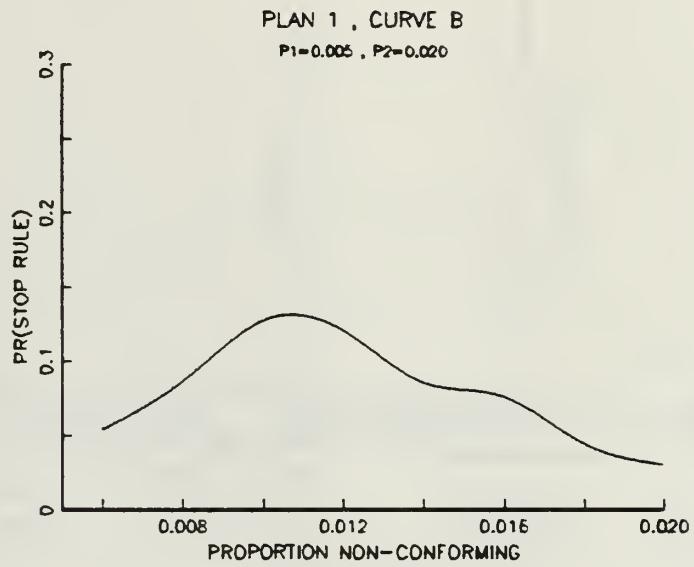
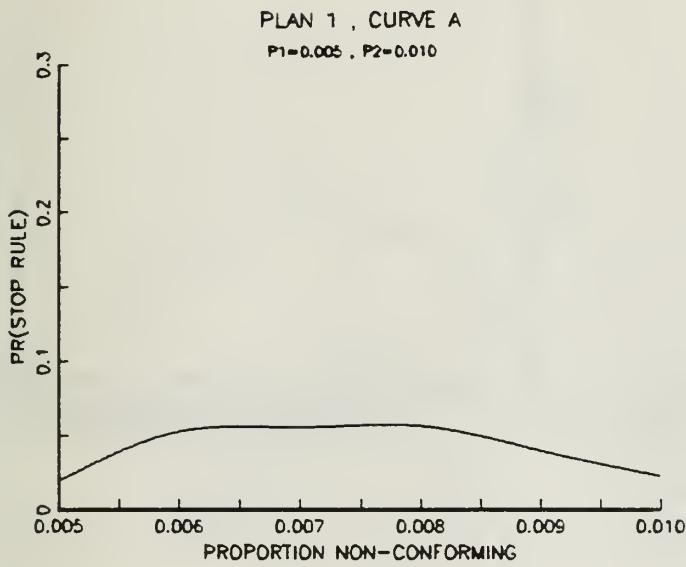


Figure 46 - PROBABILITY OF IMPLEMENTING THE TRUNCATION  
 AND ACCEPTANCE RULE . PLAN I , CURVES A THRU D.

# PROBABILITY OF USING STOPPING RULE

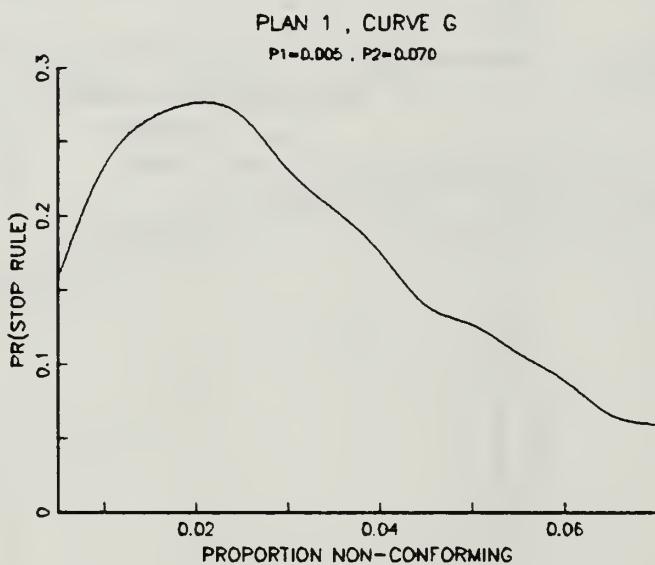
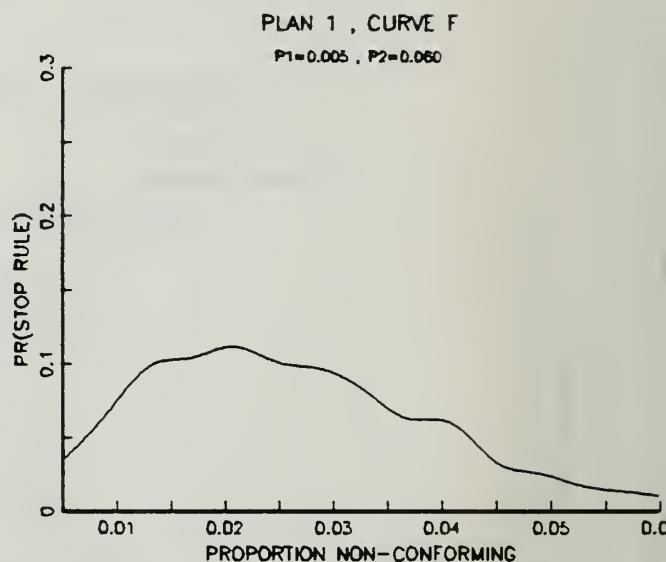
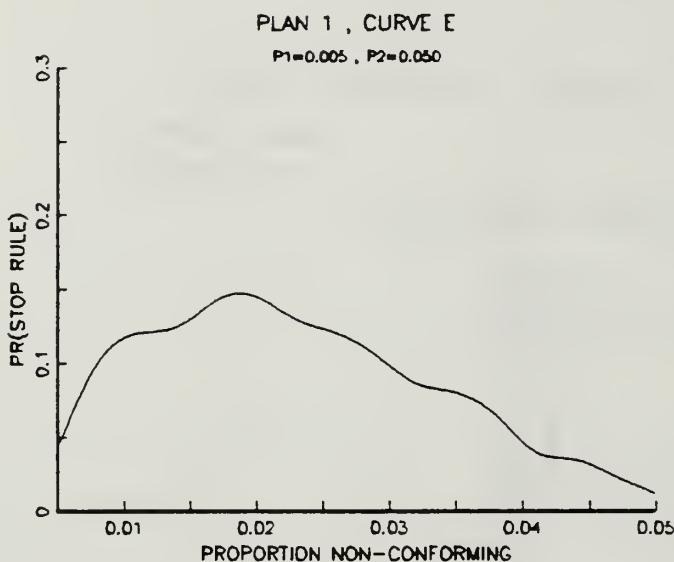


Figure 47 - PROBABILITY OF IMPLEMENTING THE TRUNCATION AND ACCEPTANCE RULE . PLAN I , CURVES E THRU G.

## PPOBABILITY OF USING STOPPING RULE

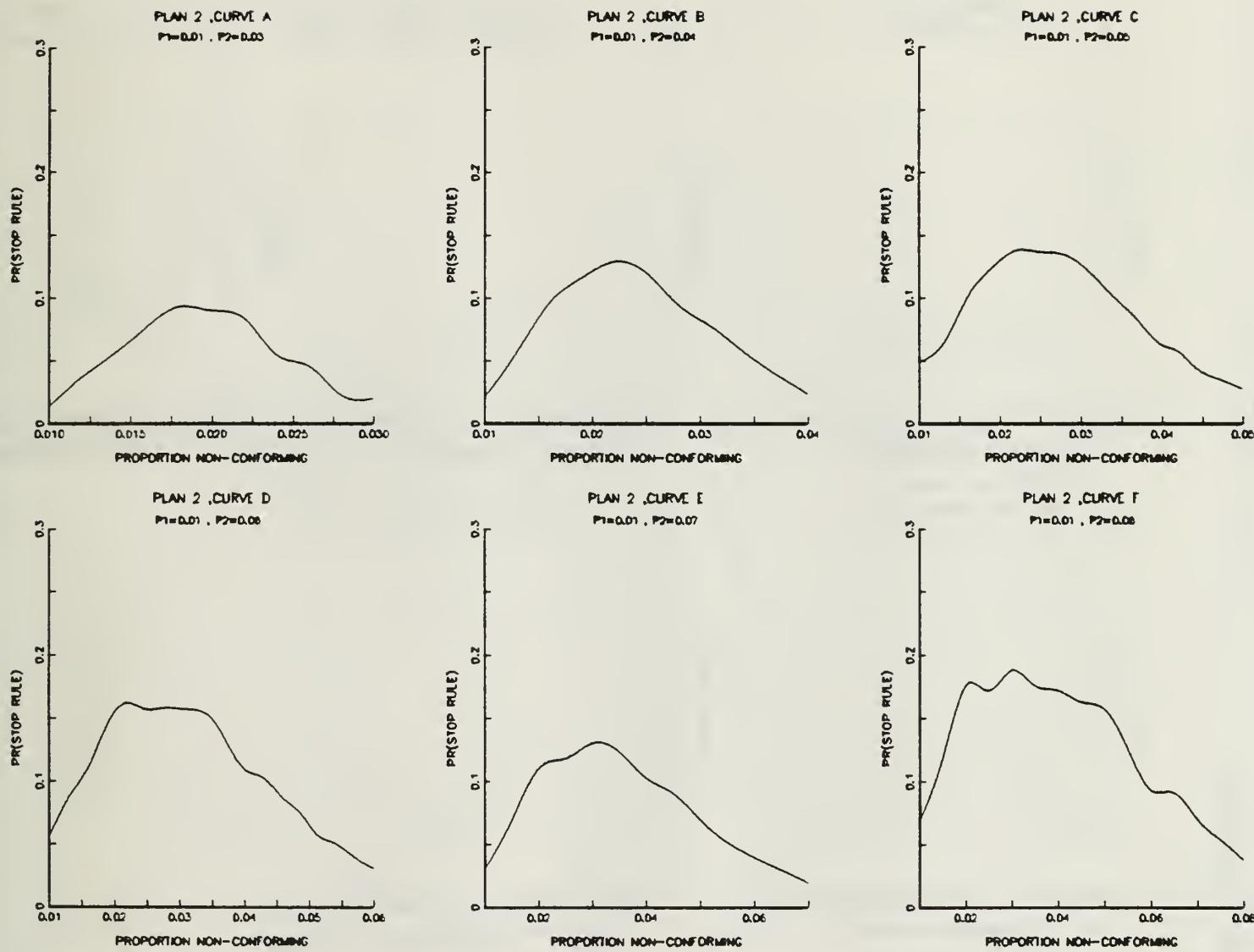


Figure 48 - PROBABILITY OF IMPLIMENTING THE TRUNCATION  
AND ACCEPTANCE RULE . PLAN II , CURVES A THRU F.

# PROBABILITY OF USING STOPPING RULE

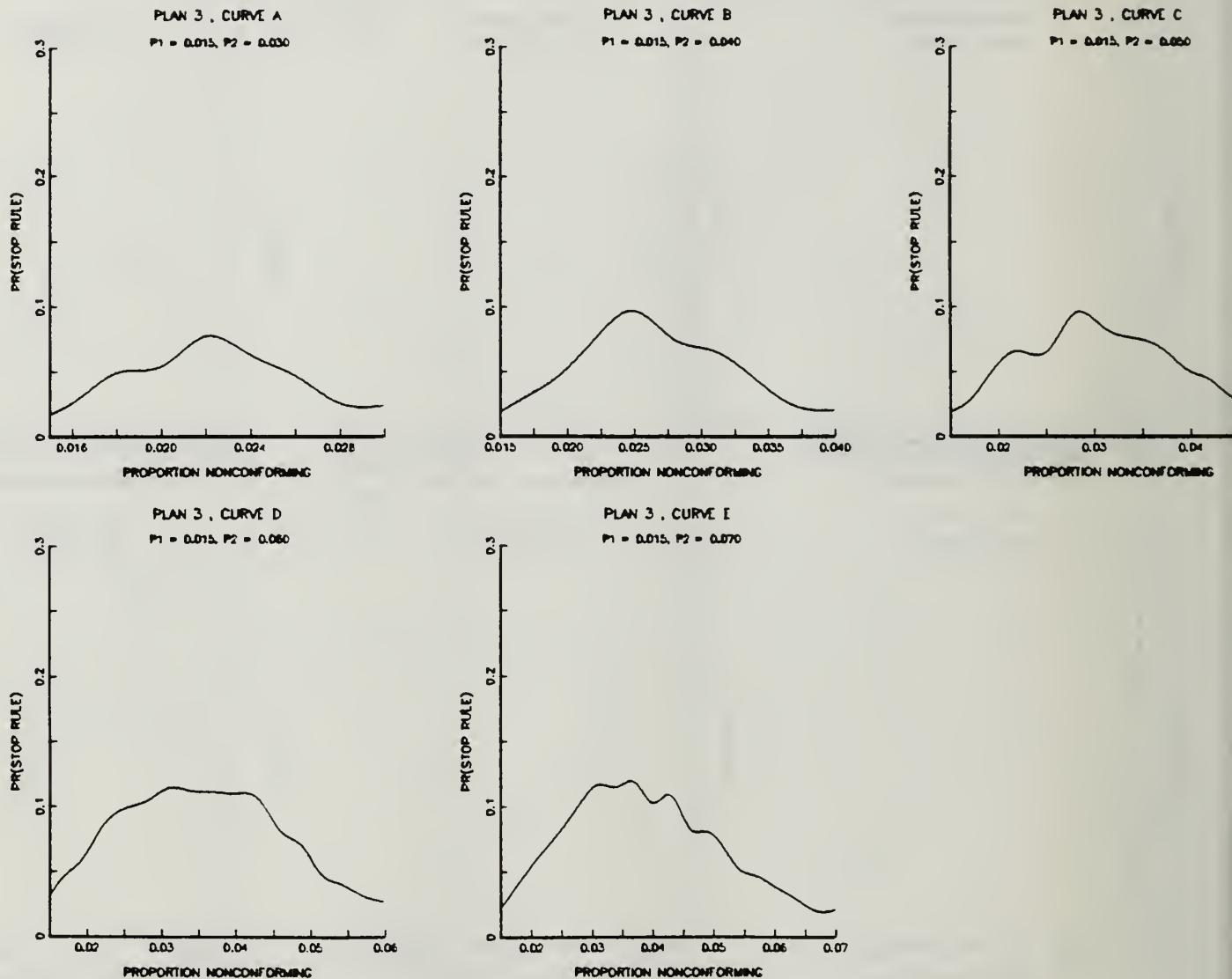


Figure 49 - PROBABILITY OF IMPLEMENTING THE TRUNCATION AND ACCEPTANCE RULE . PLAN III , CURVES A THRU E.

## PROBABILITY OF USING STOPPING RULE

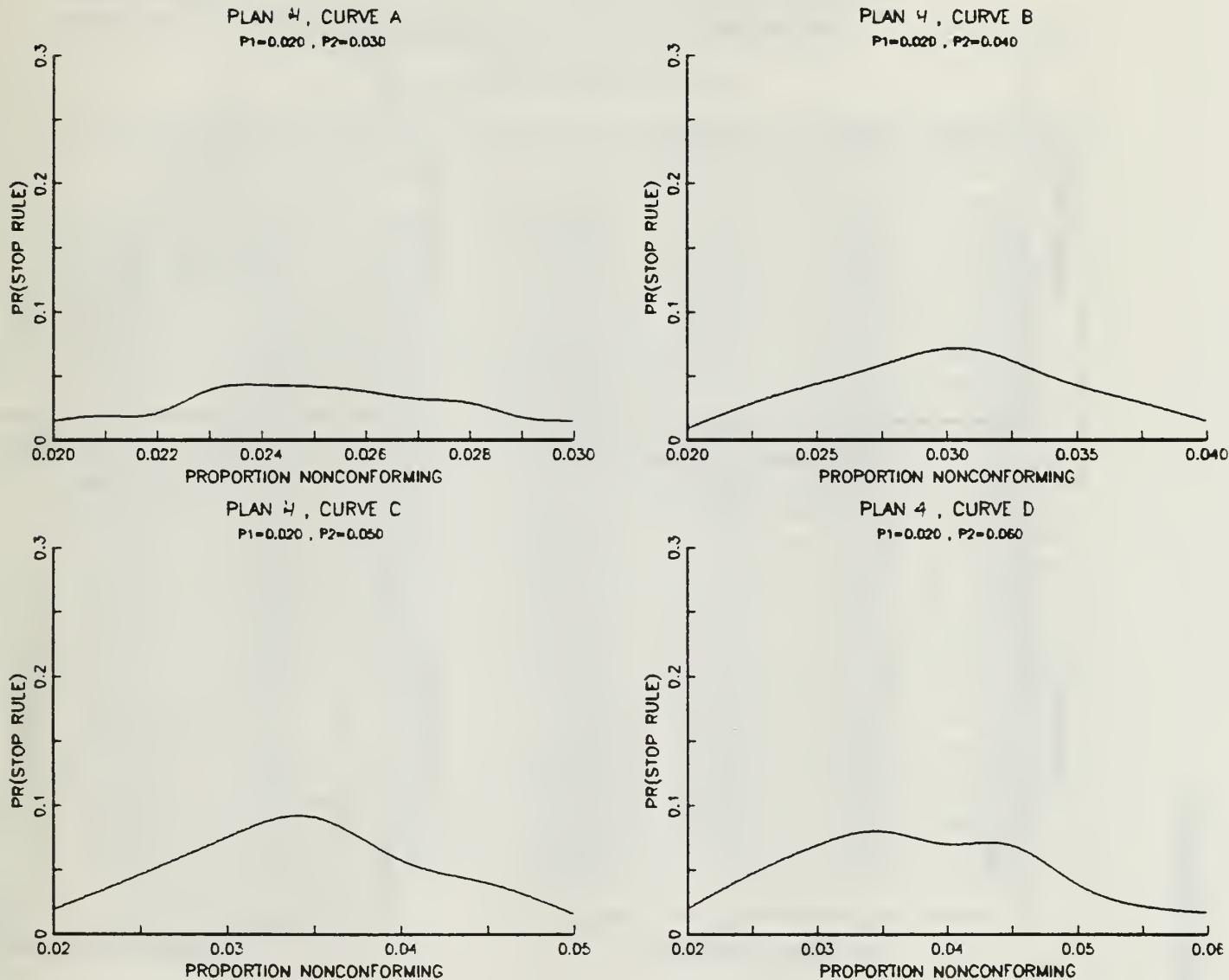


Figure 50 - PROBABILITY OF IMPLEMENTING THE TRUNCATION  
AND ACCEPTANCE RULE . PLAN IV , CURVES A THRU D.

# PROBABILITY OF USING STOPPING RULE

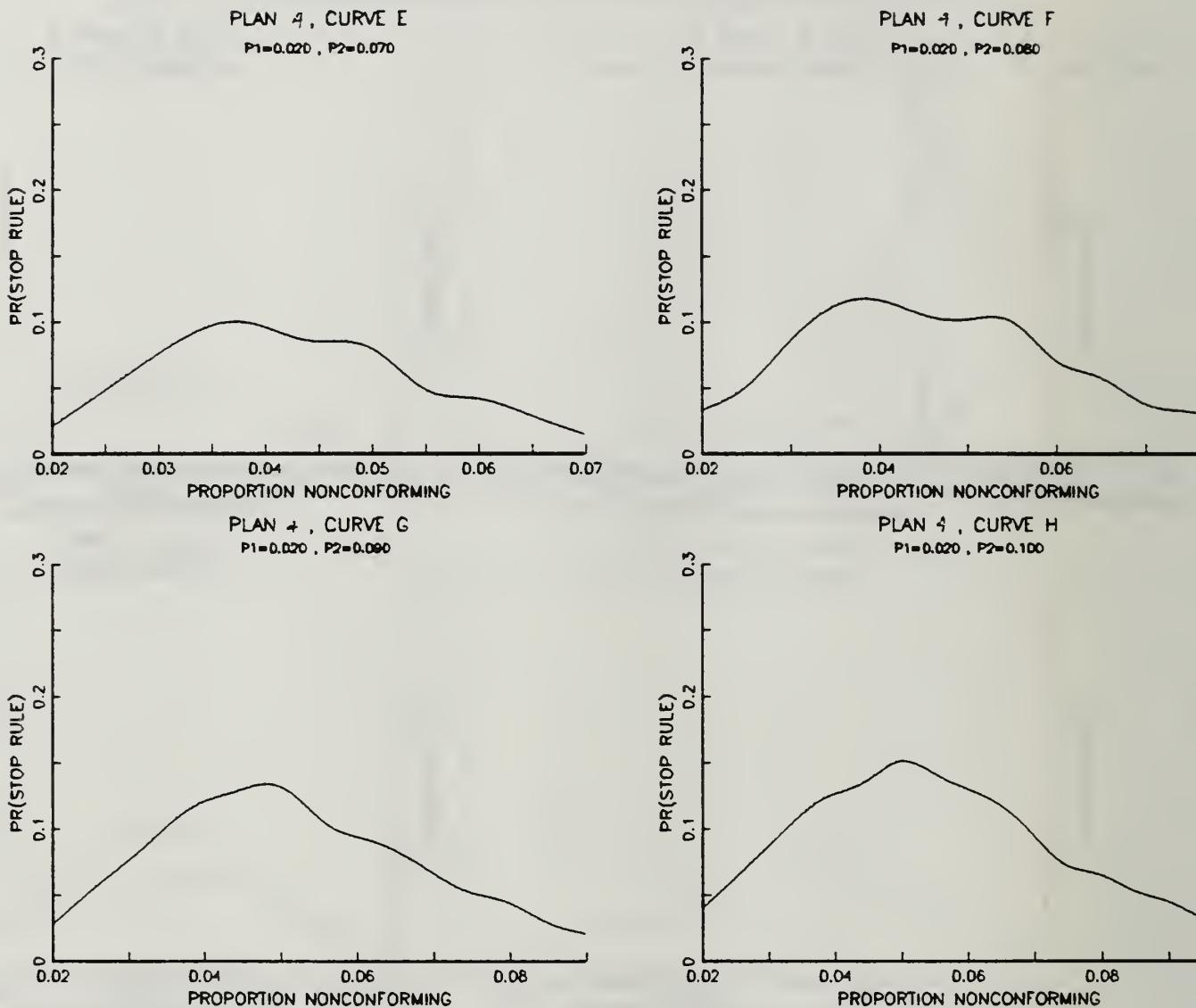


Figure 51 - PROBABILITY OF IMPLEMENTING THE TRUNCATION  
AND ACCEPTANCE RULE . PLAN IV , CURVES E THRU H.

Table XXI - TESTING OF REGRESSION EQUATION  
 FOR THE PROBABILITY OF IMPLIMENTING  
 (h1-1) ACCEPTANCE RULE

P1	P2	Diff	s	Predicted	TRUE	difference
				Pr(NTP)	Pr(NTP)	
0.005	0.010	0.005	0.00722	0.088	0.057	0.03
0.005	0.020	0.015	0.01084	0.114	0.086	0.03
0.005	0.030	0.025	0.01400	0.128	0.101	0.03
0.005	0.040	0.035	0.01693	0.137	0.191	-0.05
0.005	0.050	0.045	0.01970	0.144	0.146	0.00
0.005	0.060	0.055	0.02237	0.149	0.112	0.04
0.005	0.070	0.065	0.02496	0.154	0.207	-0.05
0.010	0.030	0.020	0.01824	0.115	0.094	0.02
0.010	0.040	0.030	0.02172	0.126	0.130	0.00
0.010	0.050	0.040	0.02499	0.134	0.139	-0.01
0.010	0.060	0.050	0.02811	0.140	0.162	-0.02
0.010	0.070	0.060	0.03113	0.146	0.131	0.01
0.010	0.080	0.070	0.03406	0.150	0.189	-0.04
0.015	0.030	0.015	0.02166	0.103	0.077	0.03
0.015	0.040	0.025	0.02554	0.116	0.097	0.02
0.015	0.050	0.035	0.02917	0.126	0.095	0.03
0.015	0.060	0.045	0.03263	0.133	0.122	0.01
0.015	0.070	0.055	0.03596	0.139	0.119	0.02
0.020	0.030	0.010	0.02467	0.089	0.043	0.05
0.020	0.040	0.020	0.02889	0.107	0.071	0.04
0.020	0.050	0.030	0.03282	0.118	0.079	0.04
0.020	0.060	0.040	0.03655	0.126	0.091	0.03
0.020	0.070	0.050	0.04012	0.133	0.100	0.03
0.020	0.080	0.060	0.04359	0.138	0.177	-0.04
0.020	0.090	0.070	0.04696	0.143	0.132	0.01
0.020	0.100	0.080	0.05025	0.147	0.151	0.00

## LIST OF REFERENCES

1. Duncan , A. J. , Quality Control and Industrial Statistics , 5th edition , Richard D. Irwin Inc. , 1986.
2. Koopmans , L. H. , Introduction to Contemporary Statistical Methods , 2nd Edition , Wadsworth Inc. , 1981.
3. Law , A. M. , and Kelton , D. W. , Simulation Modeling and Analysis , 2nd Edition , McGraw-Hill Inc. , 1991.
4. Murgiyanto , B. , An Examination of the Performance of Two Acceptance Decision Rules for Curtailed Wald Sequential Sampling Plans , Thesis M.S. , Operations Research , Naval Postgraduate School , March 1980.
5. Petersen , J. , Truncation and Acceptance Rules for Sequential Tests of a Bernoulli Parameter , Thesis M.S. , Operations Research , Naval Postgraduate School , September 1980.
6. Wald , A., Sequential Analysis , John Wiley and Sons , New York , 1974.
7. SAS/STAT User's Guide, v. 2 , The Sas Institute, Inc., Cary, N.C., 1989.

## INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Technical Information Center Cameron Station Alexandria, Virginia 22304-6145	2
2. Library Code 52 Naval Postgraduate School Monterey, California 93943-5100	2
3. Prof. G. F. Lindsay Dept. of Operations Research, Code 30 Naval Postgraduate School Monterey, California 93943-5100	1
4. Prof. So Youg Sohn Dept. of Operations Research, Code OR/SH Naval Postgraduate School Monterey, California 93943-5100	1
5. Lt Cameron J. Lewis 121 Main St. Wickford, Rhode Island 02852	1







DUDLEY KNOX LIBRARY  
NAVAL POSTGRADUATE SCHOOL  
MONTEREY CA 93943-5101



GAYLORD S



DUDLEY KNOX LIBRARY



3 2768 00019206 6