

# Chart for the TE<sub>11</sub> Mode Piston Attenuator

Charles M. Allred

A nomogram is given and described that expedites the determination of the dependence of attenuation on frequency, conductivity, and radius in a cylindrical waveguide, TE<sub>11</sub> mode, piston attenuator.

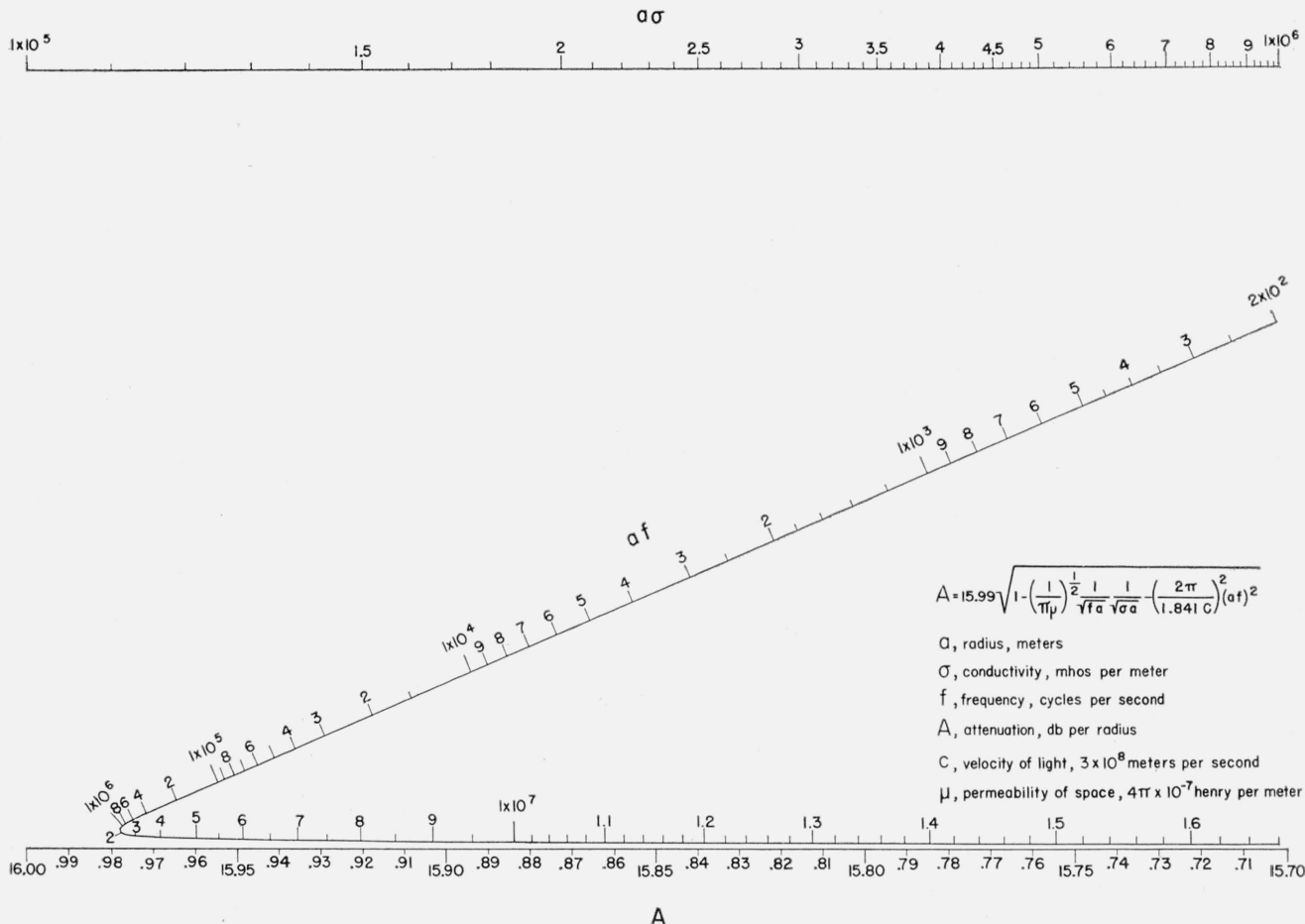


FIGURE 1. TE<sub>11</sub> mode piston attenuator chart.

Piston attenuators (waveguide-below-cutoff) are extensively used as adjustable attenuators because of their desirable characteristics, namely, a linear decibel scale and potentially high accuracy.<sup>1</sup> However, their attenuation constant (decibels per radius of travel) is a slowly changing function of frequency. This variation is due to two factors: (1) the proximity of the operating frequency to the cutoff frequency, and (2) the frequency dependence of skin-depth, which alters the effective diameter of the attenuator.

The accompanying nomograph expedites the determination of the attenuation constant, *A*, for the most commonly used TE<sub>11</sub> mode in a cylindrical guide. A good approximate functional relationship of *A*, the conductivity of the guide (nonmagnetic material), its radius, and the operating frequency is shown on the nomograph, and is the equation the nomograph solves. The effect of skin-depth is negligible for the TM<sub>01</sub> mode, and a nomograph for this mode along with the TE<sub>11</sub> mode for the case of infinite conductivity is already available.<sup>2</sup>

<sup>1</sup> R. E. Grantham and J. J. Freeman, A standard of attenuation for microwave measurements, *Trans. Am. Inst. Elec. Engrs.* **67**, 535 (1948).

<sup>2</sup> R. E. Lafferty, Piston attenuator chart. *Electronics* **21**, No. 2, 132 (1948).

This nomograph may be used in designing an attenuator to secure minimum frequency dependence over a given frequency range and to determine that dependence after its construction. To exemplify the latter, consider the radius  $a=2$  cm, the conductivity  $\sigma=1.5\times 10^7$  mhos per meter, and the frequency  $f=1\times 10^6$  cycles per second; then  $a\sigma=3\times 10^5$  mhos,  $af=2\times 10^4$  meters per second, and the extension to the  $A$  scale of a straight line passing

through the above points on the  $a\sigma$  and  $af$  scales gives a value of 15.94 db per radius for  $A$ . In designing an attenuator, one simply chooses values of  $a$  and  $\sigma$  to place the operating point preferably on the right end of the  $a\sigma$  scale and about the knee of the  $af$  scale.

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