

BASIC RADIO PROPAGATION PREDICTIONS
FOR NOVEMBER 1945
THREE MONTHS IN ADVANCE

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BASIC RADIO PROPAGATION PREDICTIONS FOR NOVEMBER 1945 THREE MONTHS IN ADVANCE

The monthly reports of the IRPL-D series are now distributed to the Army as the TB 11-499 series, by the Adjutant General; to the Navy as the DNC-13-1 series, by the Registered Publications Section, Division of Naval Communications; and to others by the IRPL.

This IRPL-D series is a monthly supplement to the IRPL Radio Propagation Handbook, Part 1, issued by the Army as TM 11-499 and by the Navy as DNC-13-1, and is required in order to make practical application of the basic Handbook.

Comments are invited from users of this report as to the accuracy of predictions when applied to the solution of specific radio propagation problems. Such comments or queries concerning radio propagation should be addressed as follows:

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Navy Department,
Washington 25, D. C.
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National Bureau of Standards,
Washington 25, D. C.

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I. TERMINOLOGY

The following symbols are used, as recommended by the International Radio Propagation Conference held in Washington, D. C., 17 April to 5 May 1944.

$f^{\circ}F2$ =ordinary-wave critical frequency for the $F2$ layer. The term night F layer will no longer be used. The term $F2$ layer is now used for the night F as well as the daytime $F2$ layer.

$f^x F2$ =extraordinary-wave critical frequency for the $F2$ layer.

Es =sporadic, or abnormal E .

fEs =highest frequency of Es reflections.

muf or MUF=maximum usable frequency.

owf or OWF=optimum working frequency.

4000-muf chart=contour chart of muf for 4000-kilometer paths.

2000-muf chart=contour chart of muf for 2000-kilometer paths.

Zero-muf chart=contour chart of vertical-incidence critical frequency, extraordinary wave.

NOTE.—The designation FF_2 has been replaced by F_2 .

II. WORLD-WIDE PREDICTION CHARTS AND THEIR USES

The charts, figures 5 to 11, present world-wide predictions of monthly average maximum usable frequencies for November 1945. Conditions may be markedly different on disturbed days, especially in or near the auroral zones, shown on the map of figure 1. The method of prediction is discussed in the IRPL Radio Propagation Handbook, Part 1, War Dept. TM 11-499, Navy Dept. DNC-13-1, p. 52, 53.

Although ionosphere characteristics are roughly similar for locations of equal latitude, there is also a considerable variation with longitude, especially in the case of the $F2$ layer. This "longitude effect" seems to be related to geomagnetic latitude. Attention was first called to this effect in the report "Radio Propagation Conditions" issued 10 Sept. 1943; it was brought into general operational use in the next issue (14 Oct. 1943).

The longitude effect in the $F2$ layer is taken care of by providing world charts for three zones, in each of which the ionosphere characteristics are independent of longitude, for practical purposes. These zones are indicated on the world map, figure 1.

Two $F2$ charts are provided for each zone, one of which, the "zero-muf chart," shows the vertical-incidence muf, or the critical frequency for the extraordinary wave, and the other, the "4000-muf chart," shows the muf for a transmission distance of 4000 km. Do not confuse the zero-muf charts with the $f^{\circ}F2$ charts appearing in the previous IRPL reports "Radio Propagation Conditions." (Values of $F2$ -zero-muf exceed those of $f^{\circ}F2$ for the same location and local time by an amount approximately equal to half the gyro-frequency for the location. See IRPL Radio Propagation Handbook, Part 1 (War Dept. TM 11-499 and Navy Dept. DNC-13-1), p. 18, 19, 28, and fig. 9).

The longitude variation is operationally negligible in the case of the normal E layer and therefore only one E -layer chart is provided.

The variation of fEs with geomagnetic latitude seems to be well marked and important. Consequently, the fEs charts are constructed on the basis of geomagnetic latitude. Since there are, as yet, insufficient correlated data, the fEs charts are much less precise than the other charts. Instructions for use of these charts appear in section IV, 3.

III. DETERMINATION OF GREAT-CIRCLE DISTANCES, BEARINGS, AND LOCATION OF TRANSMISSION CONTROL POINTS

1. BY USE OF THE WORLD MAP AND GREAT-CIRCLE CHART

Figure 1 is a map of the world. Figure 2 is a chart to the same scale as figure 1, on which the solid-line curves crossing the equator at a single point represent great circles. The numbered dot-dash lines crossing the great circles indicate distances along them in thousands of kilometers. In using figures 1 and 2 proceed as follows:

a. Place a piece of transparent paper over the map, figure 1, and draw the equatorial line (zero degrees). Place dots over the locations of the transmitting and receiving stations. Also mark the meridian whose local times are to be used as the times for calculation. Usually the Greenwich meridian is used.

b. Place this transparency over the chart, figure 2, and, keeping the equatorial line of the transparency always on the equatorial line of figure 2, slide the transparency horizontally until the terminal points marked on it fall either on the same great circle or the same proportional distance between adjacent great-circle curves. Draw in the path.

c. For paths shorter than 4000 km, locate the midpoint of the path, keeping the transparency in position on figure 2 and using as a distance scale the points at which the numbered lines in

figure 2 cross the path as drawn on the transparency.

d. For paths longer than 4000 km, designating the ends as the *A*-end and *B*-end, respectively, locate on the path and mark with a dot the following "control points," scaling the distances as in *c* above:

For *F*2 layer, points *A* and *B*, 2000 km from each end.

For *E* layer, points *A'* and *B'*, 1000 km from each end.

2. BY USE OF THE NOMOGRAM OF FIGURE 4

In figure 3, *Z* and *S* are the locations of the transmitting and receiving stations, where *Z* is the west and *S* the east end of the path. *If a point lies in the Southern Hemisphere, its angle of latitude is always taken as negative. Northern Hemisphere latitudes are taken as positive.*

a. To obtain the great-circle distance ZS (short route):

(1) Draw a slant line from (lat. *Z*—lat. *S*) measured up from the bottom on the left-hand scale to (lat. *Z*+lat. *S*) measured down from the top on the right-hand scale. If (lat. *Z*—lat. *S*) or (lat. *Z*+lat. *S*) is negative, regard it as positive.

(2) Determine the separation in longitude of the stations. Regard as positive. If the angle so obtained is greater than 180°, then subtract from 360°. Measure this angle along the bottom scale, and erect a vertical line to the slant line obtained in (1).

(3) From the intersection of the lines draw a horizontal line to the left-hand scale. This gives *ZS* in degrees.

(4) Convert the distance *ZS* to kilometers, miles or nautical miles, by using the scale at the bottom of figure 4.

Note.—The long great-circle route in degrees is simply $360^\circ - ZS$. The value will always be greater than 180°. Therefore in order to obtain the distance in miles from the conversion scale, the value for the degrees in excess of 180° is added to the value for 180°.

b. To obtain the bearing angle PZS (short route):

(1) Subtract the short-route distance *ZS* in degrees obtained in *a* from 90° to get *h*. The value of *h* may be negative, but will be submitted in (2) below without change of sign.

(2) Draw a slant line from (lat. *Z*—*h*) measured up from the bottom on the left-hand scale to (lat. *Z*+*h*) measured down from the top on the right-hand scale. If (lat. *Z*—*h*) or (lat. *Z*+*h*) is negative, regard it as positive.

(3) From (90°—lat. *S*) measured up from the bottom on the left-hand scale, draw a horizontal line until it intersects the previous slant line.

(4) From the point of intersection draw a vertical line to the bottom scale. This gives the bearing angle *PZS*. The angle may be either east or west of north, and must be determined by inspection of a map.

c. To obtain the bearing angle PSZ:

(1) Repeat steps (1), (2), (3), and (4) in *b*, interchanging *Z* and *S* in all computations. The result obtained is the interior angle *PSZ*, in degrees.

(2) The bearing angle *PSZ* is 360° minus the result obtained in (1) (as bearings are customarily given clockwise from due north).

NOTE.—The long-route bearing angle is simply obtained by adding 180° to the short-route value as determined in *b* or *c* above.

d. To obtain the latitude of Q (mid- or other point of path):

(This calculation is in principle the converse of *b*.)

(1) Obtain *ZQ* in degrees. If *Q* is the midpoint of the path, *ZQ* will be equal to one-half *ZS*. If *Q* is one of the 2000-km "control points," *ZQ* will be approximately 18°, or $ZS - 18^\circ$.

(2) Subtract *ZQ* from 90° to get *h'*. If *h'* is negative, regard it as positive.

(3) Draw a slant line from (lat. *Z*—*h'*) measured up from the bottom on the left-hand scale, to (lat. *Z*+*h'*) measured down from the top on the right-hand scale. If (lat. *Z*—*h'*) or (lat. *Z*+*h'*) is negative, regard it as positive.

(4) From the bearing angle *PZS* (taken always as less than 180°) measured to the right on the bottom scale, draw a vertical line to meet the above slant line.

(5) From this intersection draw a horizontal line to the left-hand scale.

(6) Subtract the reading given from 90° to give the latitude of *Q*. (If the answer is negative then *Q* is in the Southern Hemisphere.)

NOTE.—If *Q* is required where $SQ = 18^\circ$, then perform the above calculation, substituting *S* for *Z*. Make sure that the interior angle is used in the calculations. See *c* above.

e. To obtain the longitude difference t' between Z and Q :

(This calculation is in principle the converse of a.)

(1) Draw a straight line from (lat. $Z - \text{lat. } Q$) measured up from the bottom on the left-hand

scale to (lat. $Z + \text{lat. } Q$) measured down from the top on the right-hand scale. If (lat. $Z - \text{lat. } Q$) or (lat. $Z + \text{lat. } Q$) is negative, regard it as positive.

(2) From the left-hand side, at ZQ , in degrees, draw a horizontal line to the above slant line.

(3) At the intersection drop a vertical line to the bottom scale, which gives t' in degrees.

IV. CALCULATION OF MAXIMUM USABLE FREQUENCIES, OPTIMUM WORKING FREQUENCIES

1. PROCEDURE FOR DETERMINATION OF MUF AND OWF FOR TRANSMISSION DISTANCES UNDER 4000 KM (PROPAGATION BY THE REGULAR LAYERS)

a. Prepare or secure work forms similar to IRPL form AF (see table 1). Note that form AF provides for the inclusion of sporadic E (E_s), which will be discussed under (3) below.

b. Locate the midpoint of the transmission path, using the methods of section III above and by laying the great-circle path transparency back on the world map of figure 1, with the ends of the path in their proper location, determine in which geographical zone, E , I , or W , the midpoint falls.

c. To determine the maximum usable frequency (muf):

(1) Place the great-circle transparency over the F_2 -zero-muf chart for the proper zone of the midpoint of the path, and, keeping the equatorial line of the transparency over the equatorial line of the chart, slide the transparency horizontally until the Greenwich meridian coincides with 00 on the time scale. Note that all points on the great-circle path are in their proper local time relationship to Greenwich because 24 hours on the time scale of a muf chart is drawn to the same scale as 360° of longitude on the world map.

(2) Read the value of F_2 -zero-muf for the midpoint of the path and enter in column d of form AF.

(3) Repeat for 02, 04, etc. on the time scale.

(4) Repeat steps (1), (2), and (3) for the F_2 -4000-muf chart for the proper zone and again for the E -layer 2000-muf chart, figure 11, entering values in columns e and c , respectively.

(5) For each hour place a straightedge between the values of F_2 -zero-muf and F_2 -4000-muf at the left- and right-hand sides, respectively, of the grid

nomogram, figure 13, and read the value of the muf for the actual path length at the intersection point of the straightedge with the appropriate vertical distance line. Enter in column h . Example:

F_2 -zero-muf = 6.8 Mc. F_2 -4000-muf = 23.0 Mc.
For a distance of 2600 km the F_2 -muf is 19.1 Mc.

(6) For each hour place a straightedge between the value of the E -layer 2000-muf on the left-hand scale of the nomogram, figure 14, and the value of the path length on the right-hand scale, and read the E - F_1 -muf for that path length, off the central scale. (Example on nomogram.) Enter in column g .

(7) Compare the values of muf obtained by operations (1) to (6). The higher of the two values (columns g and h of form AF) thus determined is the muf for the path. Enter in column m .

d. To determine the optimum working frequency (owf):

(1) Calculate the F_2 -owf from the F_2 -muf determined under c above by multiplying by 0.85 or using the conversion scale in figure 13. Enter in column l .

(2) Use for the E - F_1 -owf the value of E - F_1 -muf determined under c , (6) above. This represents a change from the previous practice of taking 97 percent of the E - F_1 -muf on the nomogram of figure 14. Enter in column k .

(3) Compare the F_2 -owf and E - F_1 -owf. The higher of the two values (columns k and l of form AF) is that of the path owf. Enter in column n .

2. PROCEDURE FOR DETERMINATION OF MUF AND OWF FOR TRANSMISSION DISTANCES GREATER THAN 4000 KM (PROPAGATION BY THE REGULAR LAYERS)

a. General considerations:

The procedure outlined below is based on the following assumptions:

(1) That there are F_2 -layer control points A and B and E -layer control points A' and B' . (See section III, 1, d above.)

(2) That the highest frequency that will "take off" along the path at the A -end is the

highest frequency that can be propagated at A and A' considered together.

(3) That the highest frequency that will come in along the path at the B -end is the highest frequency that can be propagated at B and B' considered together.

(4) That the highest frequency that can be propagated from the A -end to the B -end is the lower of the two frequencies of (2) and (3) above.

(5) That the frequency obtained in (4) is the same for propagation from the B -end to the A -end.

b. Prepare or secure work forms similar to IRPL form AH (see table 2). Note that form AH provides for the inclusion of the effects of sporadic E (E_s), which will be discussed under 3 below.

c. Locate the control points A and A' at one end of the path and B and B' at the other end of the path as explained under section III, 1, *d* above. For very long paths the "short route" (minor arc of the great-circle path) and the "long route" (major arc) need be considered. Placing the transparency back on the world map, determine as in section IV, 1, *b* above in which geographical zone, E , I , or W , each of the control points A and B falls.

d. To determine the muf:

(1) Place the great-circle transparency over the $F2$ -4000-muf chart for the proper zone of the midpoint of the path for control point A and, keeping the equatorial line of the transparency over the equatorial line of the chart, slide the transparency horizontally until the Greenwich meridian coincides with 00 on the time scale.

(2) Read the value of $F2$ -4000-muf for control point A . Enter in column e of form AII.

(3) Repeat for 02, 04 etc. on the time scale.

(4) Repeat steps (1), (2), and (3) on the E -layer 2000-muf chart, figure 11, using control point A' . Enter values in column d .

(5) Determine the muf for the A -end as the higher of the $F2$ -4000-muf, column e , and the E -layer 2000-muf, column d . Enter in column m .

(6) Read the value of $F2$ -4000-muf for control point B , using the $F2$ -4000-muf chart for the proper zone. Enter values in column i .

(7) Repeat for 02, 04, etc. on the time scale.

(8) Read the values of E -layer 2000-muf on the E -layer 2000-muf chart, figure 11, using control point B' . Enter values in column j .

(9) Determine the muf for the B -end as the higher of the $F2$ -4000-muf column i , and the E -layer 2000-muf, column j . Enter in column n .

(10) Compare the two muf values of columns m and n . The lower of the two is the muf for the transmission path under consideration. Enter in column q .

e. To determine the owf:

(1) Use the scaled data of the previous procedure.

(2) Multiply the $F2$ -4000-muf for the A -end, column e , by 0.85 to obtain the $F2$ -4000-owf for the A -end, column f .

(3) Multiply the $F2$ -4000-muf for the B -end, column i , by 0.85 to obtain the $F2$ -4000-owf for the B -end, column l .

(4) Compare the $F2$ -4000-owf for the A -end, column f , with the E -layer 2000-muf for the A -end, column d . The higher of the two is the owf for the A -end. Enter in column o .

(5) Compare the $F2$ -4000-owf for the B -end, column l , with the E -layer 2000-muf for the B -end, column j . The higher of the two is the owf for the B -end. Enter in column p .

(6) Compare the two owf values of columns o and p . The lower of the two is the owf for the transmission path under consideration. Enter in column r .

3. PROCEDURES FOR INCLUSION OF THE EFFECTS OF E_s

Sporadic- E (E_s) propagation may often allow regular transmission when regular E - or $F2$ -layer propagation would not. E_s data are not yet sufficient to permit accurate calculations of such propagation, but the fE_s charts of figures 12 and 15 are given as a guide to E_s occurrence.

As the fE_s charts are constructed from considerations of geomagnetic latitude, three latitude scales are provided at the right of the charts of figures 12 and 15, one for each of the three zones of figure 1 (E , I , and W).

Until further improvements are made, the following procedures should be used to include the effects of E_s in the calculations of muf and owf.

a. For paths over 4000 km long:

(1) Place the great-circle path transparency prepared in section III, 1, over the median fE_s chart, figure 12, using the latitude scale for the zone containing the control point.

(2) Scale fE_s at control points A' and B' . Enter in columns a and g , respectively, on form AII.

(3) Multiply fE_s by 5 in each case, obtaining

the E_s -2000-muf. Enter in columns b and h , respectively.

(4) In the determination of muf modify the procedure (steps (5) and (9)) of section IV, 2, *d* above to obtain the muf for the A - and B -ends, respectively, as the highest of the *three* items, the $F2$ -4000-muf, the E -layer 2000-muf, and the E_s -2000-muf. No other change is necessary.

(5) In the determination of owf subtract 4 Mc from the E_s -2000-muf to obtain the E_s -2000-owf for the A -end and B -end, respectively, entering the results in columns e and k . Then modify the procedure (steps (4) and (5)) of section IV, 2, *e* to obtain the owf for the A - and B -ends, respectively, as the highest of the *three* items, the $F2$ -4000-owf, the E -layer 2000-muf, and the E_s -2000-owf. No other changes are necessary.

b. For paths under 4000 km long:

(1) Repeat step (1) of *a* above.

(2) Scale fE_s at the midpoint of the path. Enter in column a of form AII.

(3) Multiply fE_s by 5, obtaining the E_s -2000-muf. Enter in column b .

(4) In the determination of muf under IV, 1, *c*, find the *Es*-muf for the path by use of the same nomogram, figure 14, as was used for the *E-F1*-muf. Enter in column *f*. Then modify the procedure in IV, 1, *c*, (7) so that the highest of the three values, the *F2*-muf, the *E-F1*-muf, and the *Es*-muf, columns *h*, *g*, *f*, is the muf for the path.

(5) In the determination of owf under IV, 1, *d*, subtract 4 Mc from the *Es*-2000-muf found under (3) above to obtain the *Es*-2000-owf, entering in column *i*. Now find the *Es*-owf for the path, using the same nomogram, figure 14, as for the *E-F1*-

owf, applying the *Es*-2000-muf to the left-hand scale and reading the answer on the middle scale. Enter in column *j*. Then modify the procedure in section IV, 1, *d* (3) so that the highest of the three values, the *F2*-owf, the *E-F1*-owf, and the *Es*-owf, columns *l*, *k*, *j*, is the owf for the path.

Because of the relative uncertainty with which *Es* is known, it may often be desirable in short-path work to operate on a frequency close to owf for the regular layers only, as calculated by the procedure of IV, 1, *d*, without the inclusion of *Es*.

V. ABSORPTION, DISTANCE RANGE, AND LOWEST USEFUL HIGH FREQUENCY

The procedures outlined in the text of this report will give an adequate solution to most of the high-frequency propagation problems that will normally be encountered in the field. If operating frequencies are chosen near the calculated owf prediction in any given case, best possible results should be had, at least in communications work.

The use of frequencies too far below the owf will result in weak reception because of increasing ionospheric absorption as the frequency decreases. The factor that limits the usefulness of low field intensities is usually atmospheric noise at the receiving location.

The determination of lowest useful high frequencies is more difficult than the determination of muf and the techniques for their prediction are less far advanced.

The subject of absorption, distance range, and lowest useful high frequency is discussed at length in IRPL Radio Propagation Handbook, Part 1, p. 69-97 (War Dept. TM 11-499, Navy Dept. DNC-13-1), and formulas, graphs, and nomograms for calculation are given there.

Simpler and more accurate techniques are being developed and will be released as soon as the work is completed.

VI. SAMPLE MUF AND OWF CALCULATIONS

1. FOR SHORT PATHS

Required: The muf and owf for transmission between Washington, D. C. (39.0° N, 77.5° W) and Miami, Fla. (25.7° N, 80.5° W) for average conditions during the month of November 1945.

Solution:

Let the local time used for this problem be GCT (*Z* time or that of 0° longitude).

The midpoint of the path is at approximately 32.5° N, 79.0° W, and the transmission path length is approximately 1500 km, all in *W* zone.

The values of *E*- and *F2*-layer muf and owf, and also *Es*-owf for all hours, GCT, as determined by using the procedure given in section IV, are given in table 1. The final values are presented graphically in figure 16.

Values of owf obtained by the procedure of section IV, 1, *c* for the regular layers only are underscored in column *l* of table 1, and are plotted in figure 16. Values of *E*-owf in column *k* did not govern at any hour. Hours in which *Es* controls transmission are those for which the dotted-line graph for the owf goes above the solid-line graph.

Actually, in this example, 05 is the only hour when this happens. During the other hours the values of owf of column *n* of form AF coincide with the owf for the regular layers and appear as a solid line.

Figure 16 shows that skip will occur, on the average, during the night hours, if a frequency as high as 9.0 Mc is used. A frequency as high as 8.7 Mc will not skip, on the average, at any time of day, but its use is not advisable because of (a) the day-to-day variability, causing some probability of skip during the night hours, and (b) ionospheric absorption during the daytime, which is more pronounced at low frequencies.

A satisfactory plan to insure continuous transmission at all times, over a path like this, involves the use of two frequencies, one for night and one for day. Figure 16 shows that a night frequency of 5.2 Mc, to be used from 2250 to 1245 GCT, and a day frequency of 11.5 Mc, to be used from 1245 to 2250 GCT, would be satisfactory. The periods of usefulness of these frequencies are shown by the heavy dashed line on figure 16.

2. FOR LONG PATHS

Required: The muf and owf for transmission between Shanghai, China (31.2° N, 122.2° E) and San Francisco, Calif. (37.8° N, 122.4° W) for average conditions during the month of November 1945.

Solution:

Let the local time for this problem be GCT (*Z* time or that of 0° longitude).

The path length is approximately 10,000 km, and the two *F2*-layer control points, *A* and *B*, re-

spectively, are at approximately 43° N, 139° E, and 48° N, 143° W. These are, respectively, in the *E* zone and the *I* zone, as shown on the map, figure 1. The two *E*-layer and *E*_s control points, *A*' and *B*', respectively, are located at approximately 37.5° N, 127° E, and 43° N, 133° W. The bearing of San Francisco from Shanghai is approximately 45° , and of Shanghai from San Francisco, approximately 310° , both determined by means of the nomogram of figure 4.

The values of *muf* and *owf* over this transmission path, as determined by the procedure in section IV, are given in table 2 for all hours, GCT. The final values are shown graphically in figure 17.

Figure 17 shows that skip will occur, on the average, during the night hours if a frequency as high as 10.0 Mc is used, although higher frequencies may be used during a limited portion of the day.

A good practical arrangement to insure continuous transmission at all times is to select three frequencies, in a manner similar to that suggested in the preceding problem. A frequency of 7.4 Mc may be used from 0500 to 2030 GCT, a frequency of 18.0 Mc may be used from 2205 to 0240 GCT, and a transition frequency of 9.8 Mc may be used from 0240 to 0500, and from 2030 to 2205 GCT.

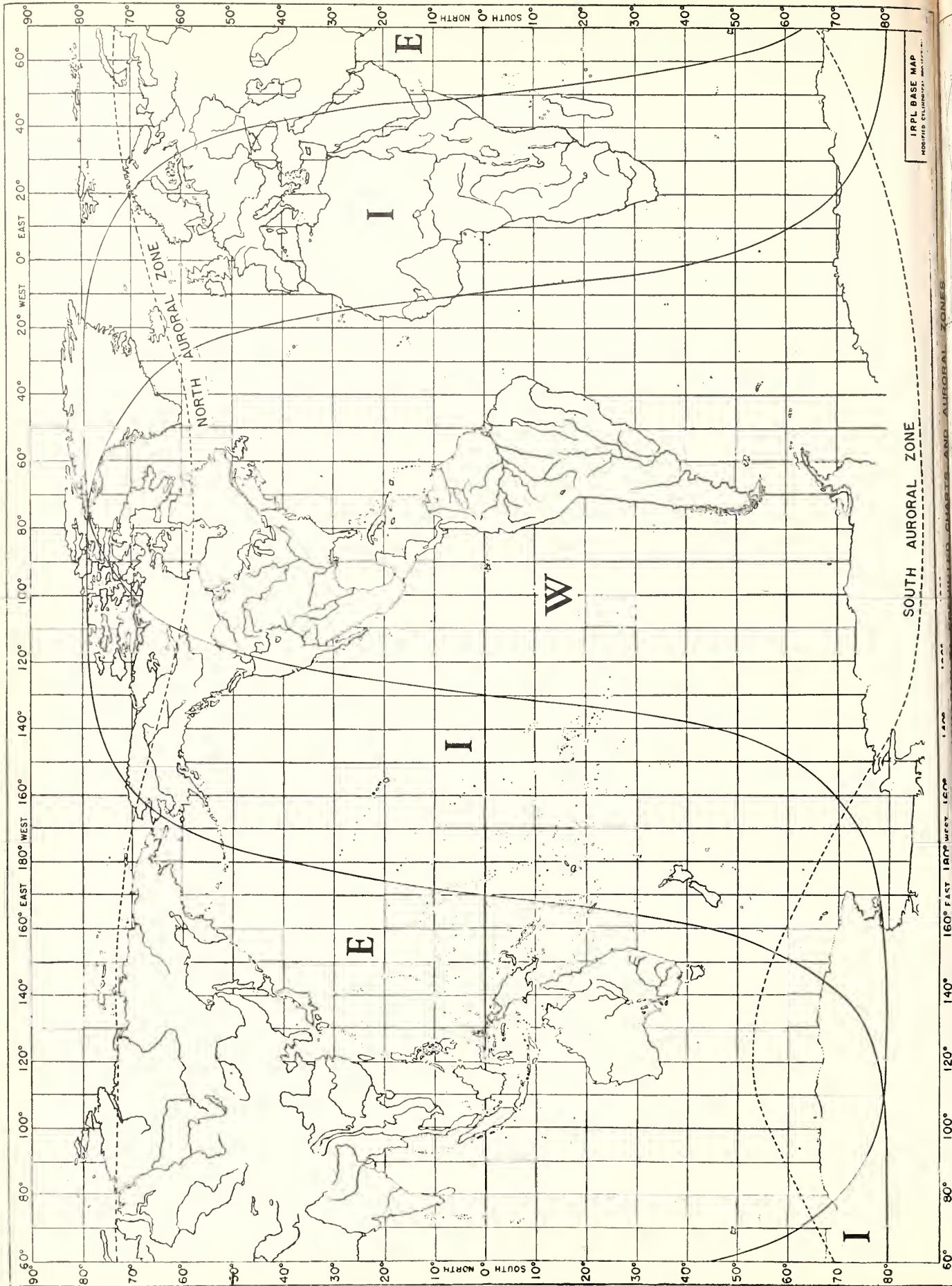
By inspection of the absorption chart and the noise map (figs. 90 and 119 of the IRPL Radio Propagation Handbook, Part 1, War Dept. TM 11-499, Navy Dept. DNC-13-1), it may be seen that considerations of the lowest useful high frequency over this path may be of considerable importance in selecting frequencies for use. Consequently, in cases of transmission failure on the frequencies here recommended, particularly in the case of the transition frequency, changing the frequency to a value slightly under the *muf* for the path may be advisable.

MUF - OWF WORK SHEET FOR PATHS 4000 KM OR LESS

From Washington, D.C. To Miami, Fla. Distance, 1500 km Zone W Predicted for Nov. 1945

Note: All frequencies are in megacycles.

GCT	fEs		E-layer 2000-muf		F2 zero-muf		F2 4000-muf		Es-muf for Path		E-f1-muf for Path		F2-muf for Path		Es for 2000-owf		Es-owf for Path		E-owf for Path		F2-owf for Path		MUF for Path		OWF for Path		
	a	b	c	Scale	d	Scale	e	Scale	f	g	h	i	j	k	l	m	n	o	p	q	r	s	t	u	v	w	x
00		5Xo																									
01				5.7	4.8	4.4	17.6	14.0		10.4																	
02				4.4	4.4	4.2	12.4	12.4		8.4																	
03				4.2	4.2	4.2	12.1	12.1		7.6																	
04	2.1	10.5		4.2	4.2	4.2	11.7	11.7	9.6	7.1	6.5																
05	2.2	11.0		4.2	4.2	4.2	11.1	11.1	10.1	6.9	7.0	5.9															
06	2.1	10.5		4.3	4.3	4.3	11.3	11.3	9.6	7.1	6.5	5.9															
07				4.5	4.5	4.5	12.6	12.6		7.8																	
08				4.6	4.6	4.6	13.6	13.6		8.1																	
09				4.6	4.6	4.6	14.1	14.1		8.3																	
10				4.5	4.5	4.5	13.2	13.2		8.0																	
11				3.9	3.9	3.9	11.8	11.8		6.1																	
12			8.5	5.7	5.7	5.7	17.6	17.6		7.6	10.4																
13			11.5	7.4	7.4	7.4	25.0	25.0		10.6	14.4																
14	2.1	10.5	13.4	8.3	8.3	8.3	27.7	27.7	9.6	12.3	16.0																
15	2.2	11.0	14.6	8.8	8.8	8.8	29.0	29.0	10.1	13.4	16.2																
16	2.3	11.5	15.3	9.2	9.2	9.2	30.7	30.7	10.5	14.0	17.8																
17	2.4	12.0	15.4	9.5	9.5	9.5	31.4	31.4	11.0	14.1	18.3																
18	2.5	12.5	15.4	9.6	9.6	9.6	31.7	31.7	11.3	14.1	18.4																
19	2.4	12.0	15.0	9.6	9.6	9.6	31.7	31.7	11.0	13.7	18.4																
20	2.2	11.0	13.8	9.4	9.4	9.4	31.3	31.3	10.1	12.6	18.1																
21			11.5	9.0	9.0	9.0	30.2	30.2		10.7	17.5																
22			8.9	8.1	8.1	8.1	27.0	27.0	8.3	8.3	15.7																
23			5.2	6.9	6.9	6.9	22.4	22.4	4.7	4.7	13.1																
Done by																											
Checked																											



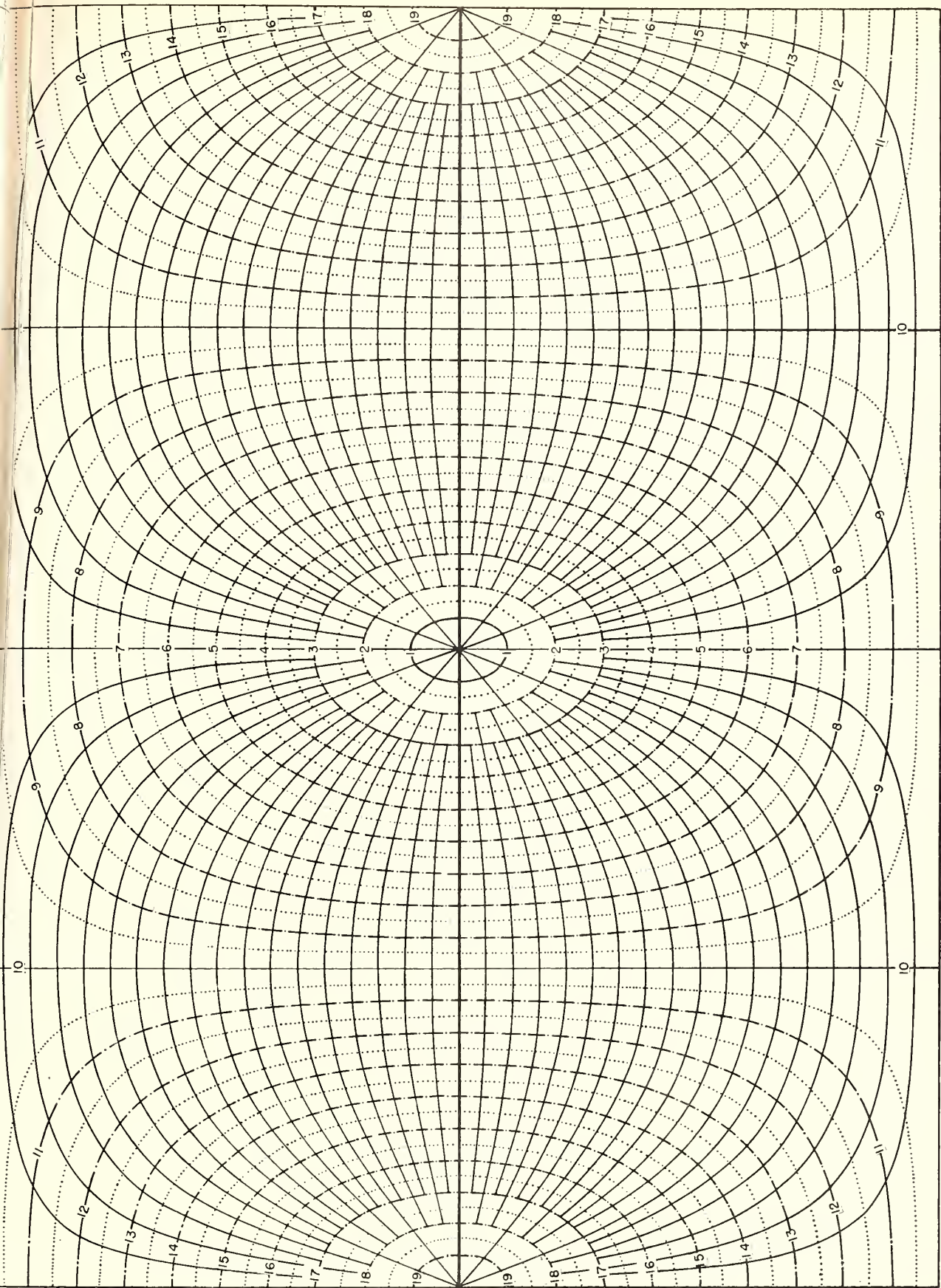


Fig. 2. GREAT CIRCLE CHART CENTERED ON EQUATOR. SOLID LINES REPRESENT GREAT CIRCLES. NUMBERED DOT-DASH LINES INDICATE DISTANCES IN THOUSANDS OF KILOMETERS.

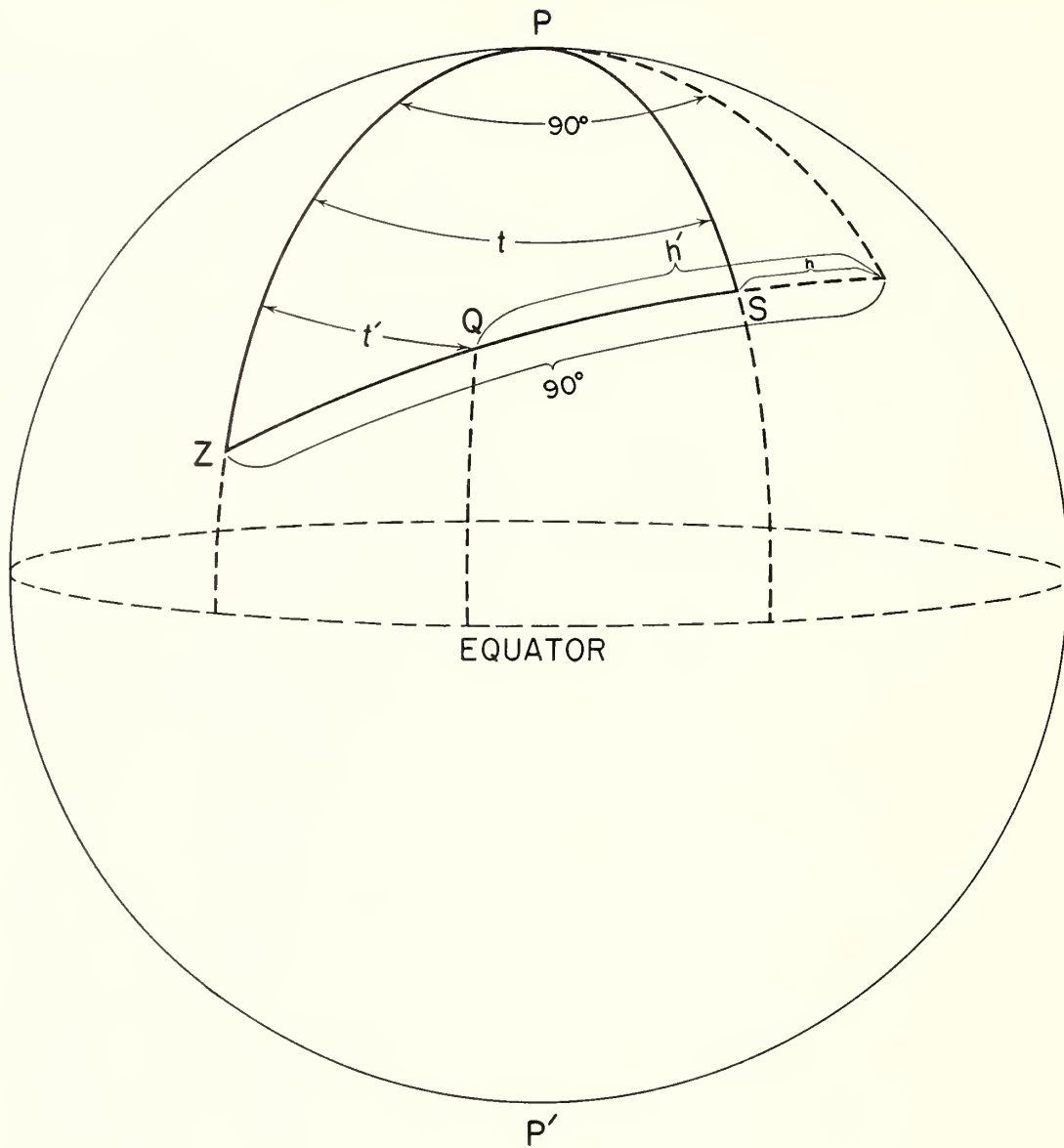


Fig. 3. DIAGRAM OF TRANSMISSION PATH AUXILIARY TO EXPLANATION OF USE OF DISTANCE — BEARING NOMOGRAM, FIG. 4.

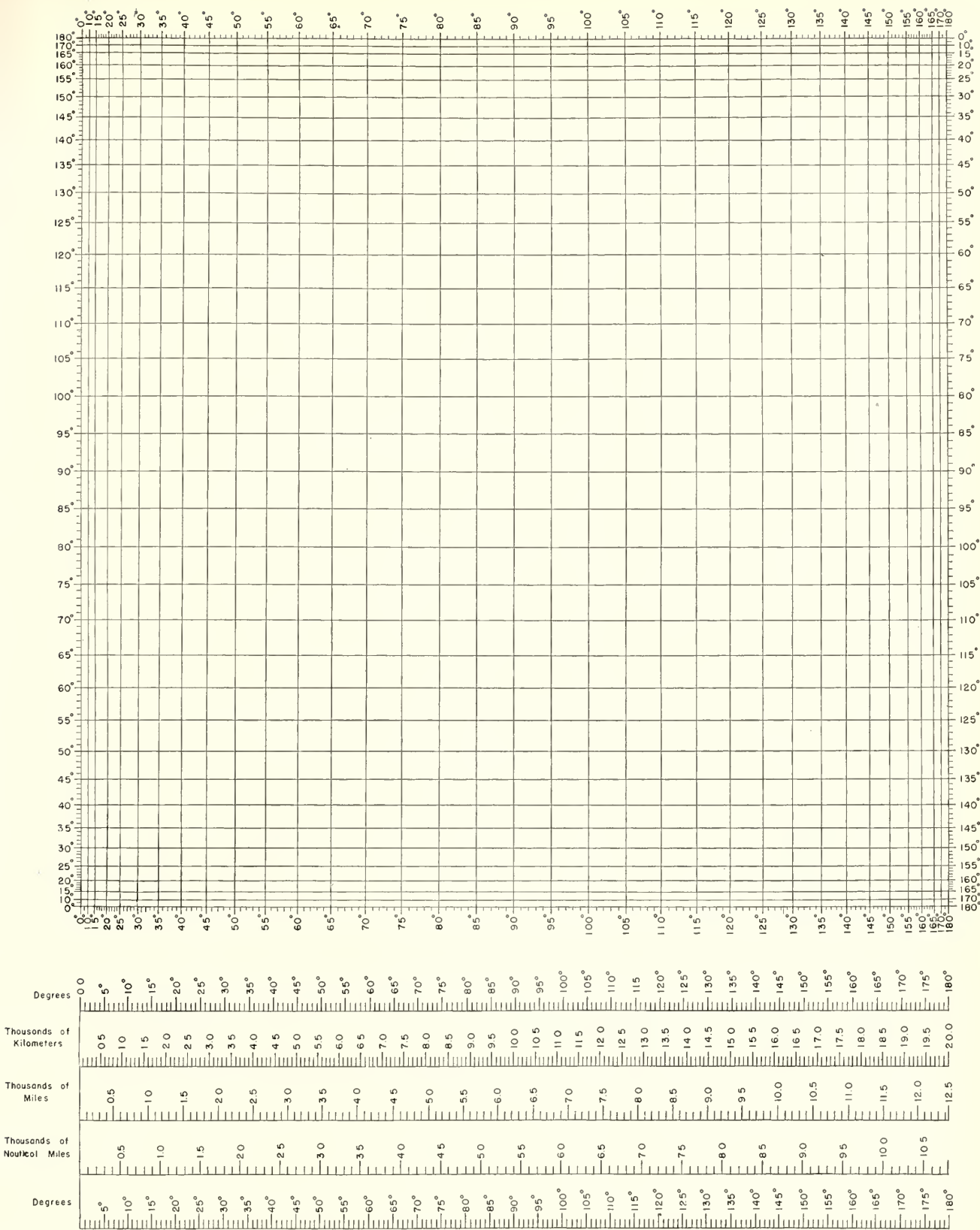


Fig. 4. NOMOGRAM (AFTER D'OCAGNE) FOR OBTAINING GREAT-CIRCLE DISTANCES, BEARINGS, LATITUDE AND LONGITUDE OF TRANSMISSION CONTROL POINTS, SOLAR ZENITH ANGLES.
CONVERSION SCALE FOR VARIOUS DISTANCE UNITS.

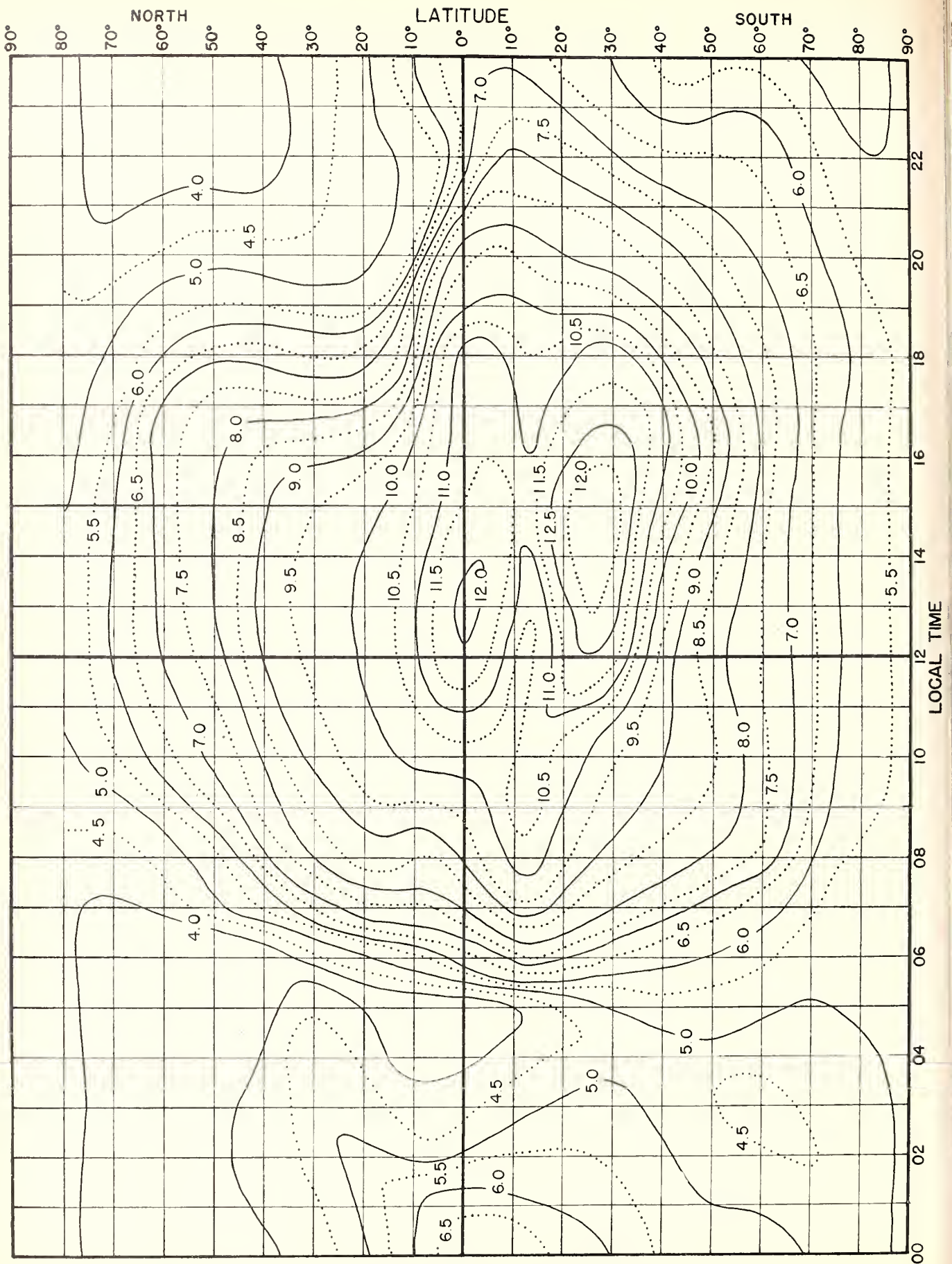


Fig. 5. F_2 ZERO-MUF, IN Mc, W ZONE, PREDICTED FOR NOVEMBER, 1945.

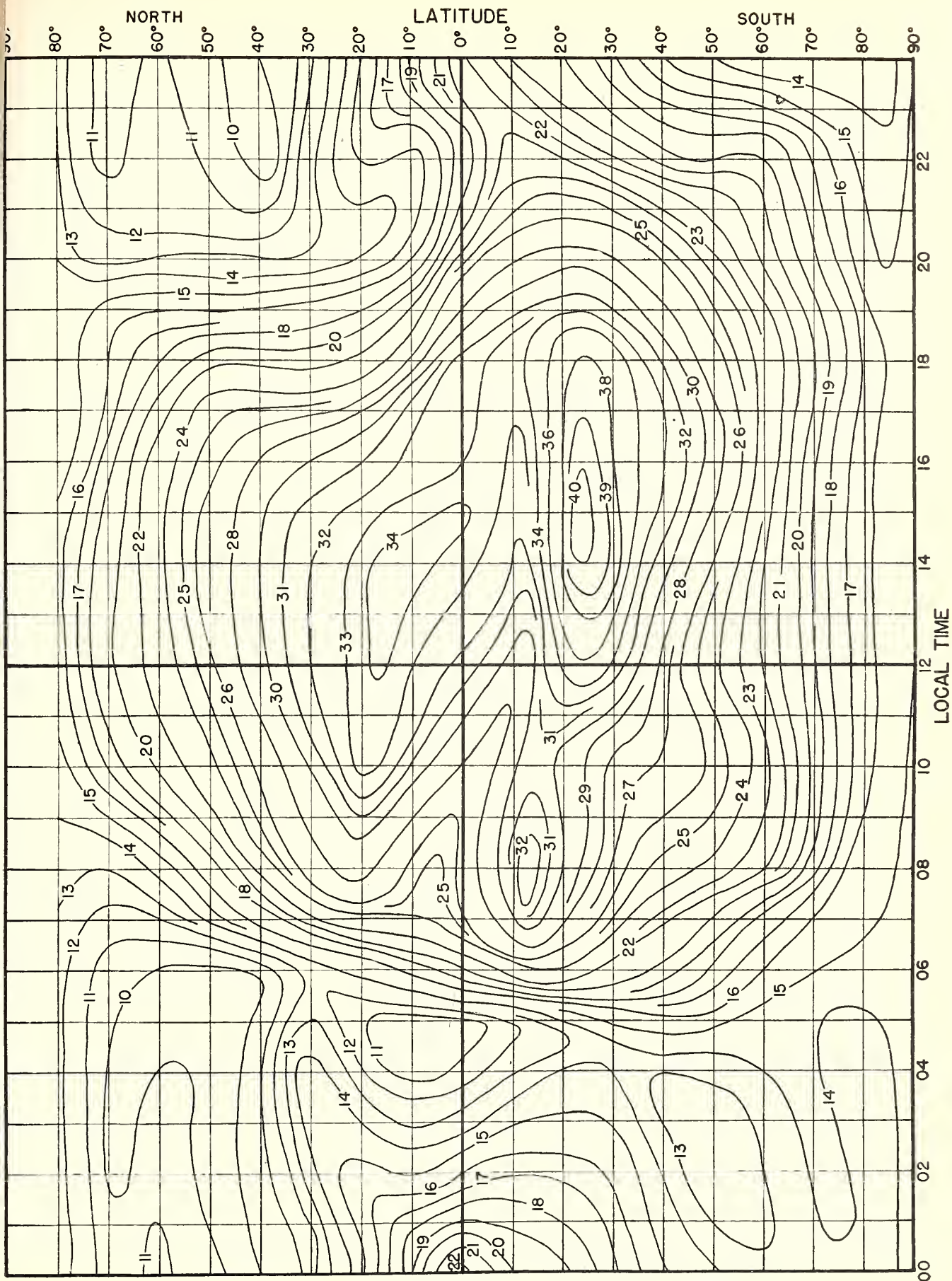


Fig. 6. $F_2 4000-MUF$, IN Mc, W ZONE, PREDICTED FOR NOVEMBER, 1945.

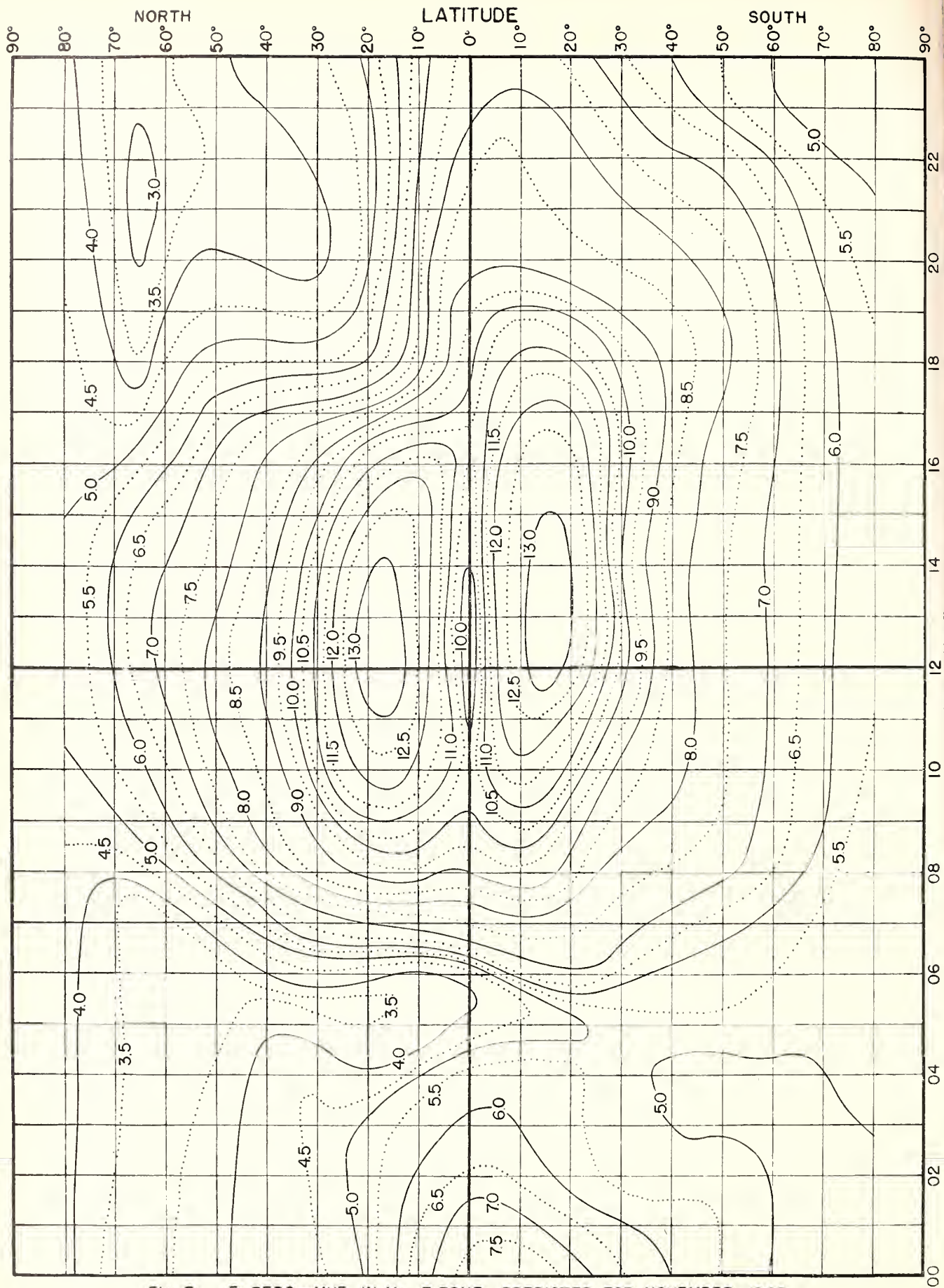


Fig 7. F₂ ZERO—MUF, IN Mc, I ZONE, PREDICTED FOR NOVEMBER, 1945.

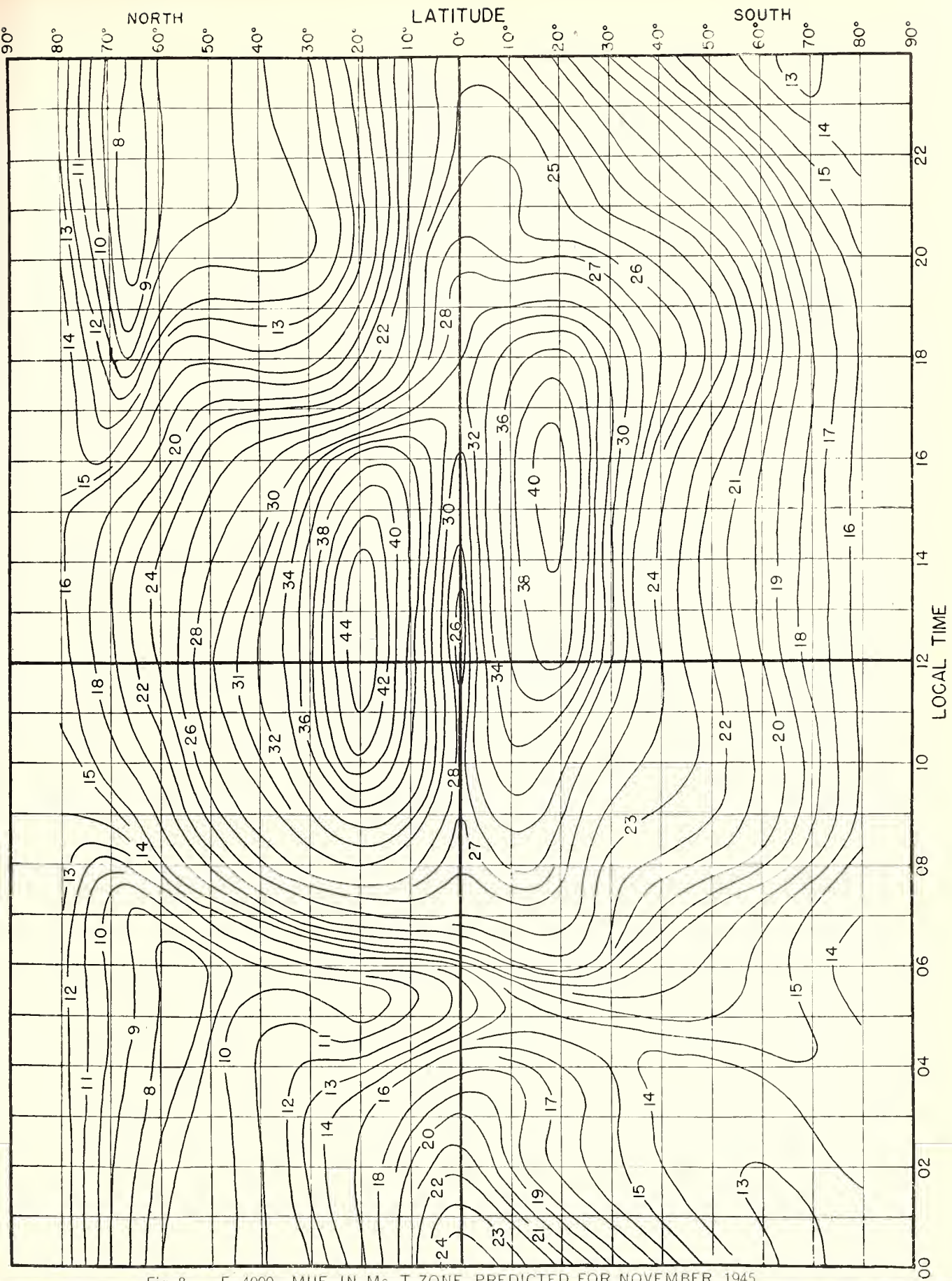


Fig. 8. F₂ 4000—MUF, IN Mc, I ZONE, PREDICTED FOR NOVEMBER, 1945.

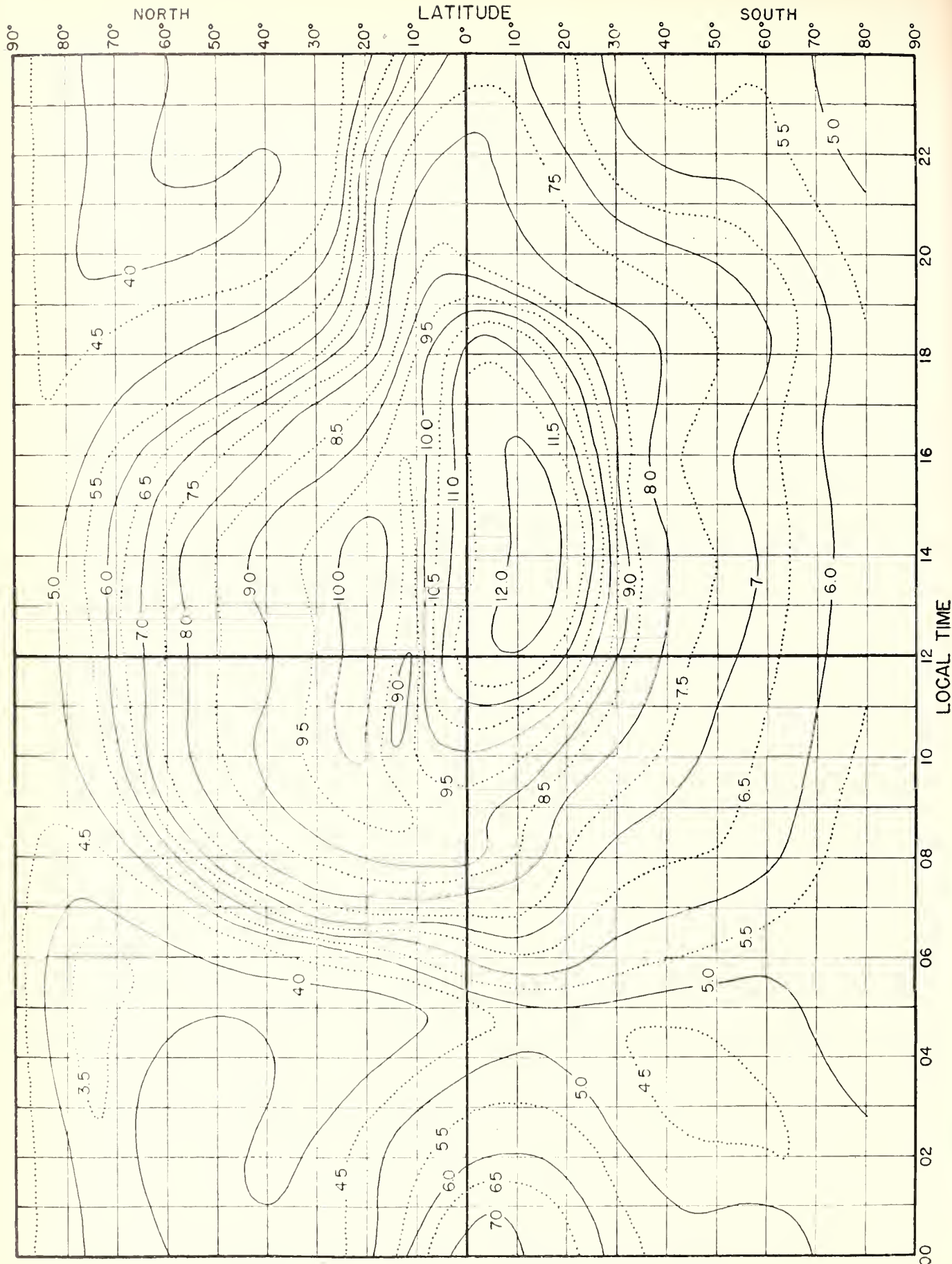


Fig. 9. F_2 ZERO—MUF, IN Mc, E ZONE, PREDICTED FOR NOVEMBER, 1945.

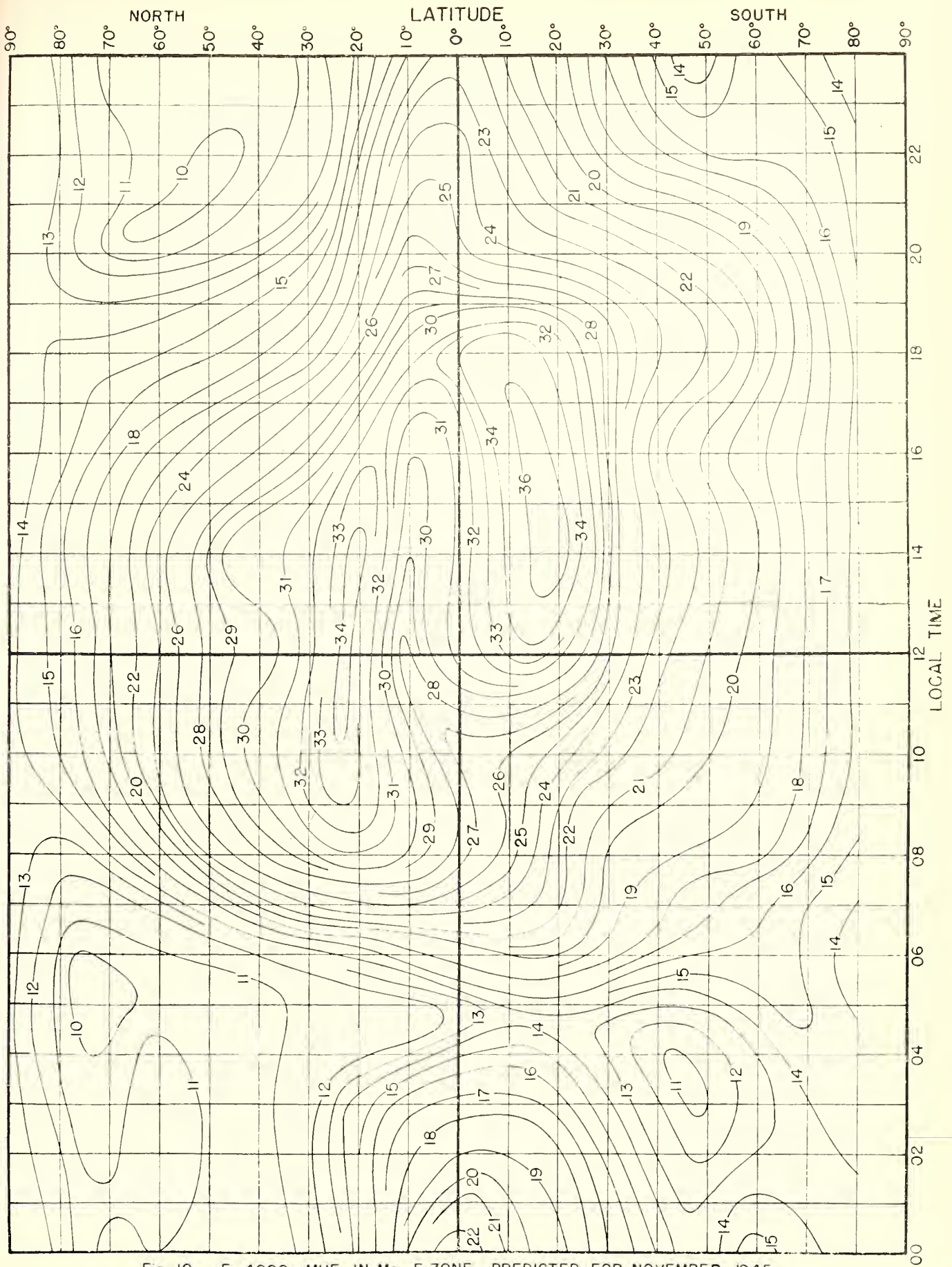


Fig. 10. F_2 4000—MUF, IN Mc, E ZONE, PREDICTED FOR NOVEMBER, 1945.

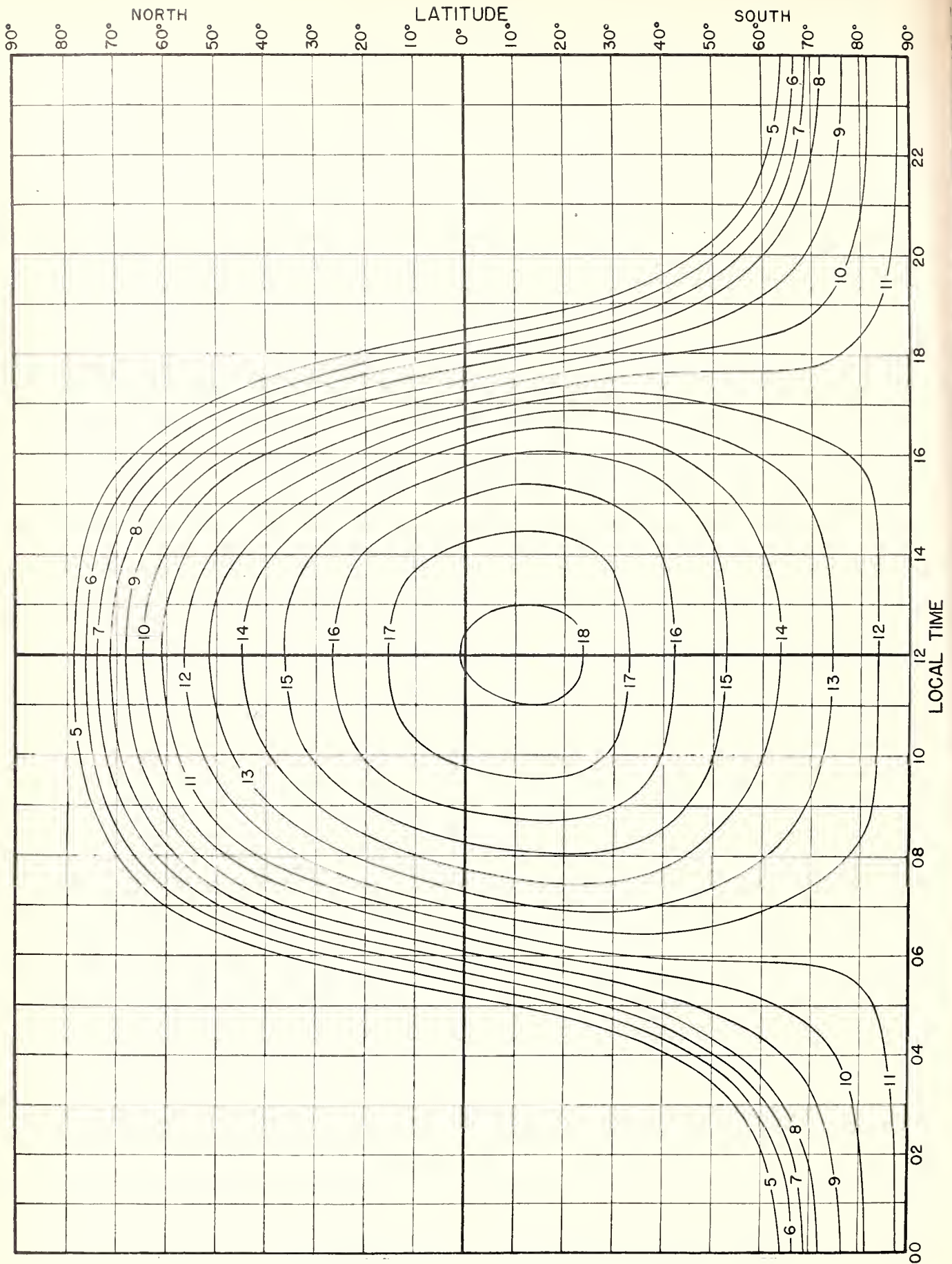


Fig. 11. E-LAYER 2000-MUF, IN Mc, PREDICTED FOR NOVEMBER, 1945.

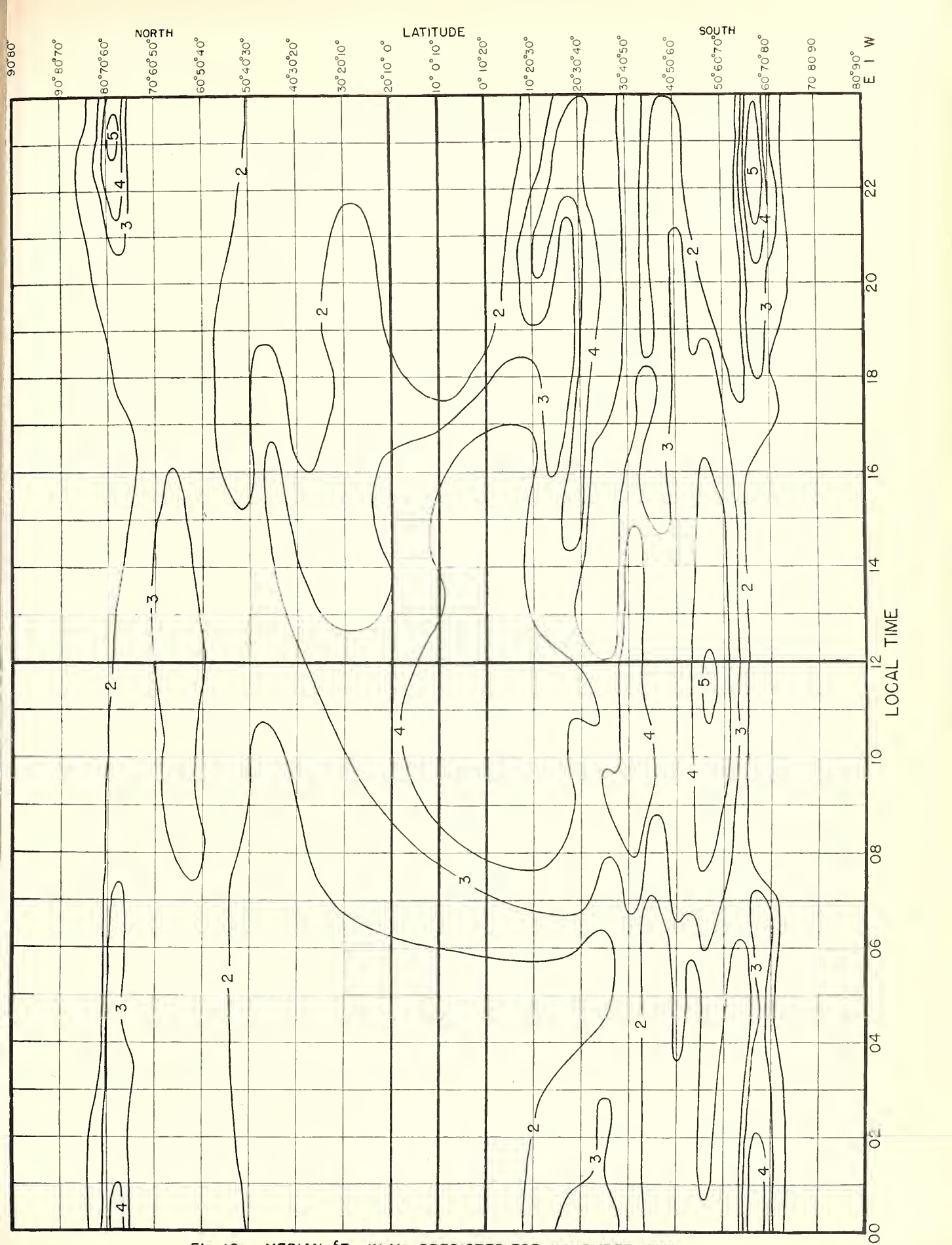


Fig 12. MEDIAN fE_s , IN Mc, PREDICTED FOR NOVEMBER, 1945.

1 km = 0.62137 mile = 0.53961 naut. mi
 1 mile = 1.60935 km = 0.86836 naut. mi
 1 naut. mi = 1.85325 km = 1.1516 mi

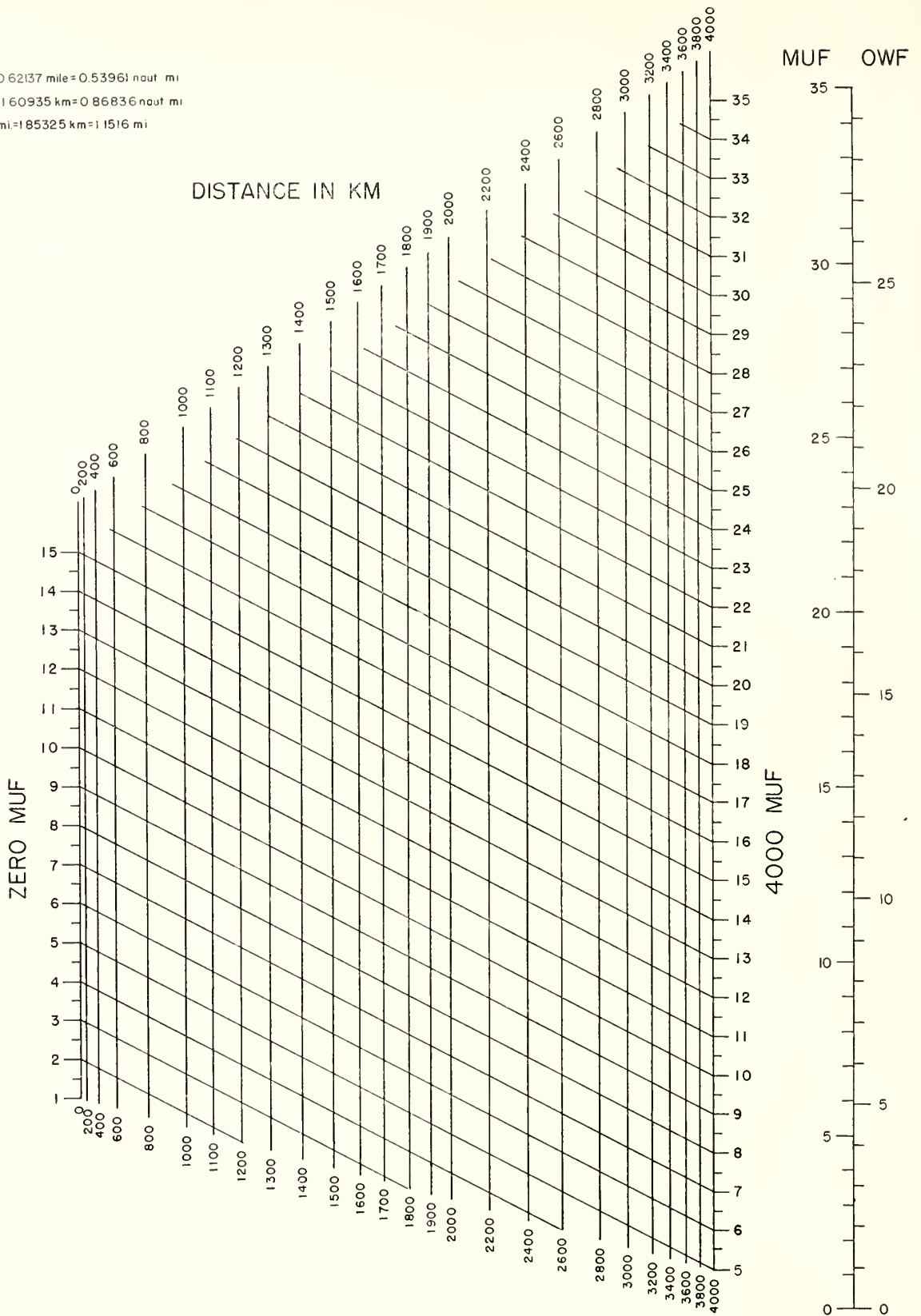


FIG. 13. NOMOGRAM FOR TRANSFORMING F_2 -ZERO-MUF AND F_2 -4000-MUF TO EQUIVALENT MAXIMUM USABLE FREQUENCIES AT INTERMEDIATE TRANSMISSION DISTANCES; CONVERSION SCALE FOR OBTAINING OPTIMUM WORKING FREQUENCIES.

E-Layer 2000-muf

1 km = 0.62137 mile = 0.53961 naut. mi.

1 mile = 1.60935 km = 0.86836 naut. mi.

1 naut. mi. = 1.85325 km = 1.1516 mi.

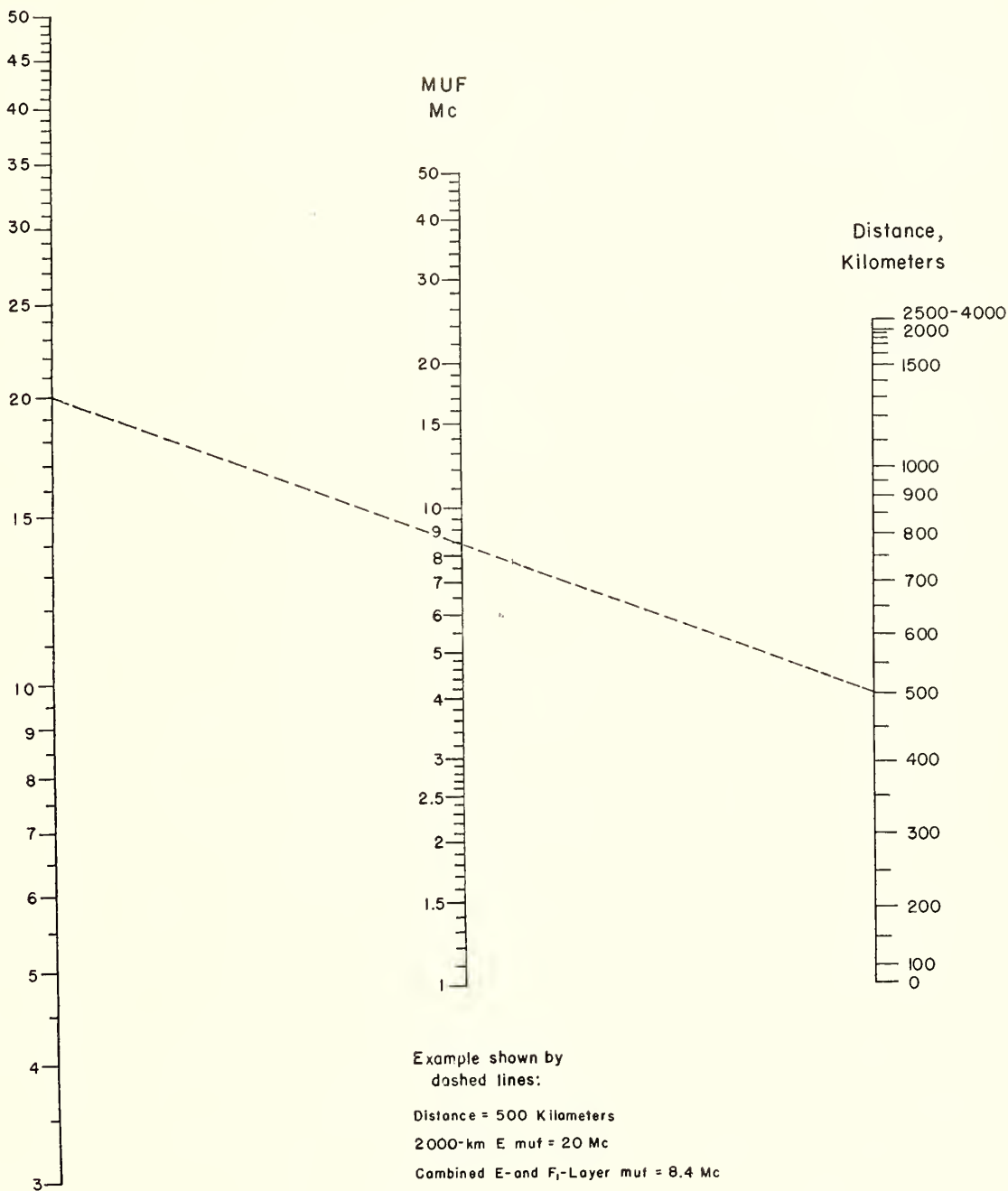


FIG. 14. NOMOGRAM FOR TRANSFORMING E-LAYER 2000-MUF TO EQUIVALENT MAXIMUM USABLE FREQUENCIES AND OPTIMUM WORKING FREQUENCIES DUE TO COMBINED EFFECT OF E LAYER AND F₁ LAYER AT OTHER TRANSMISSION DISTANCES.

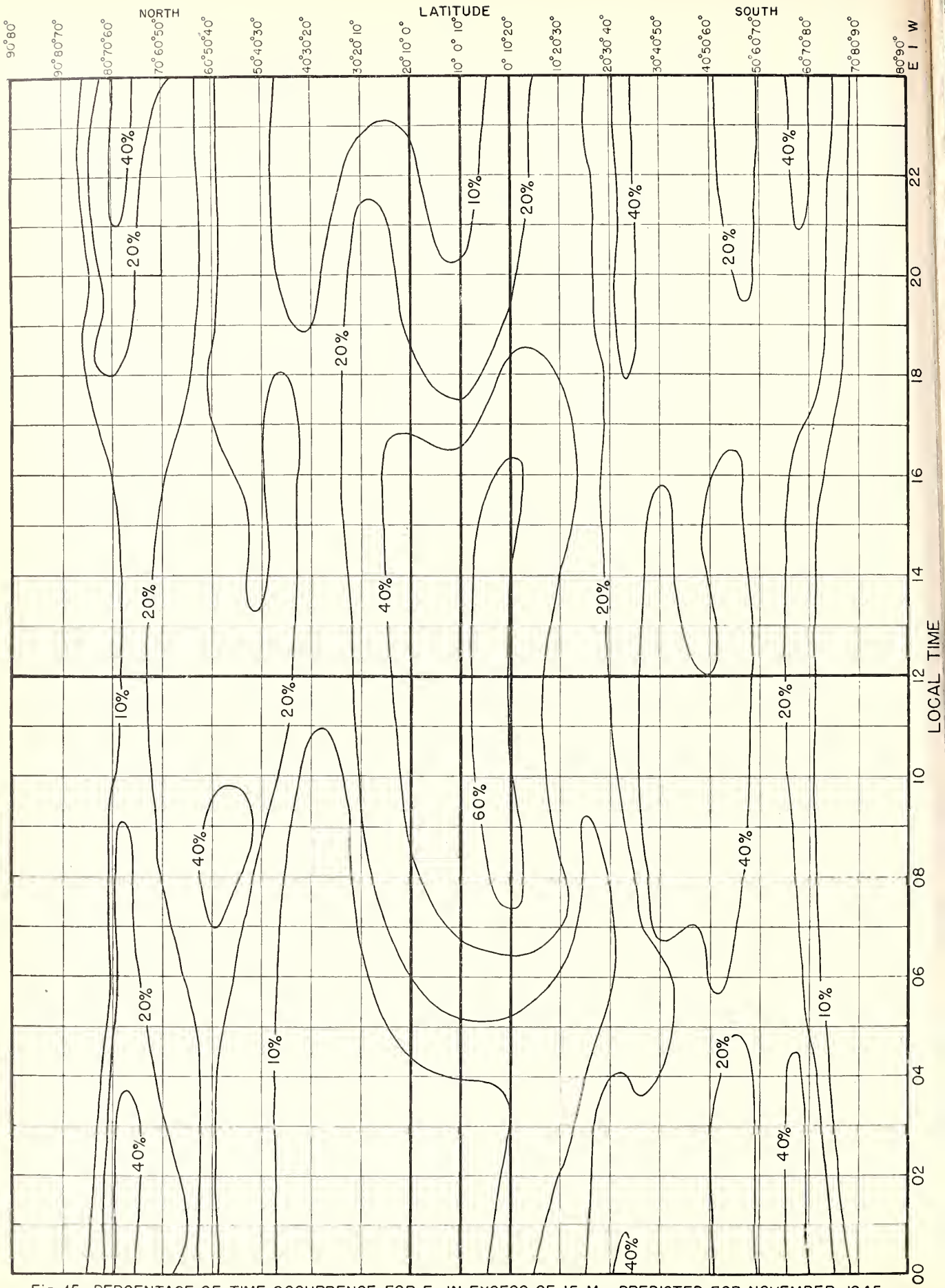
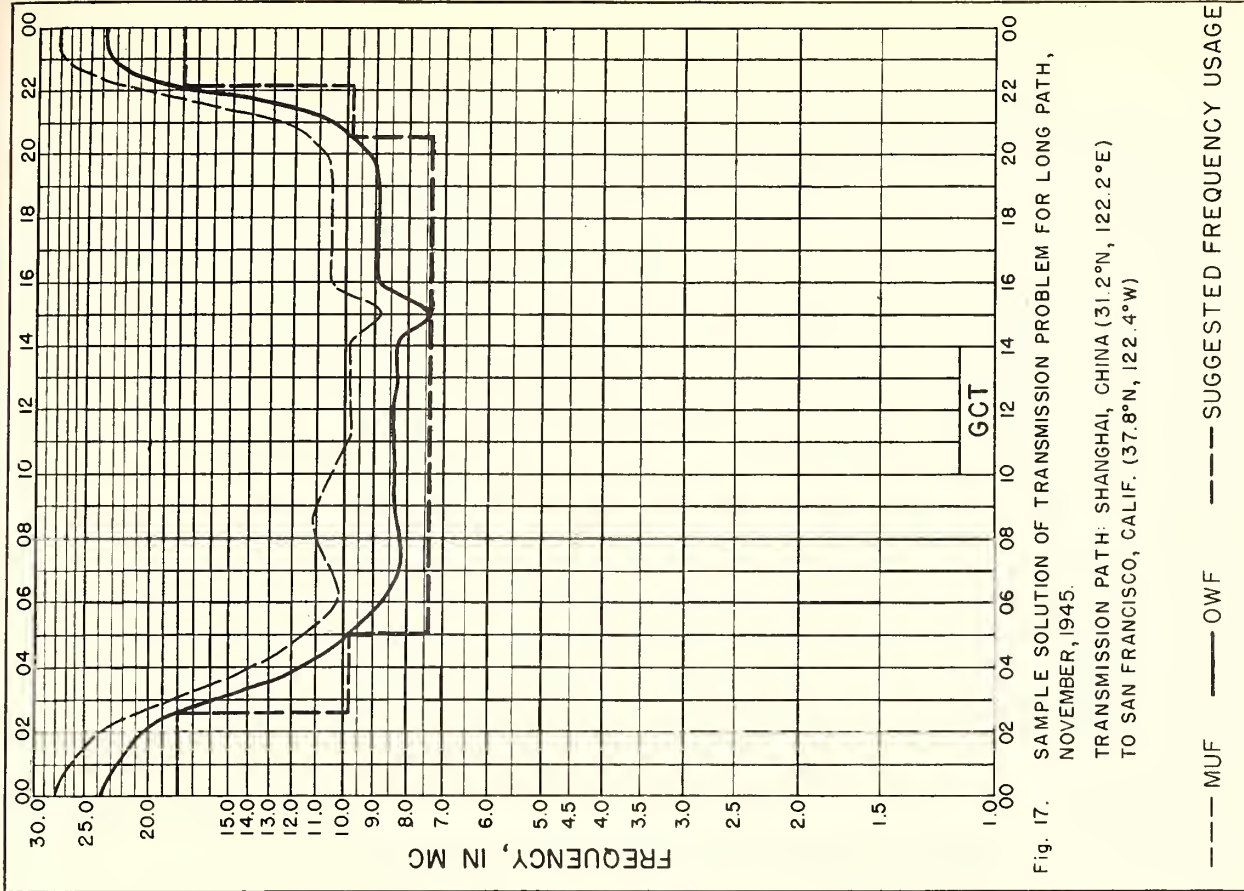
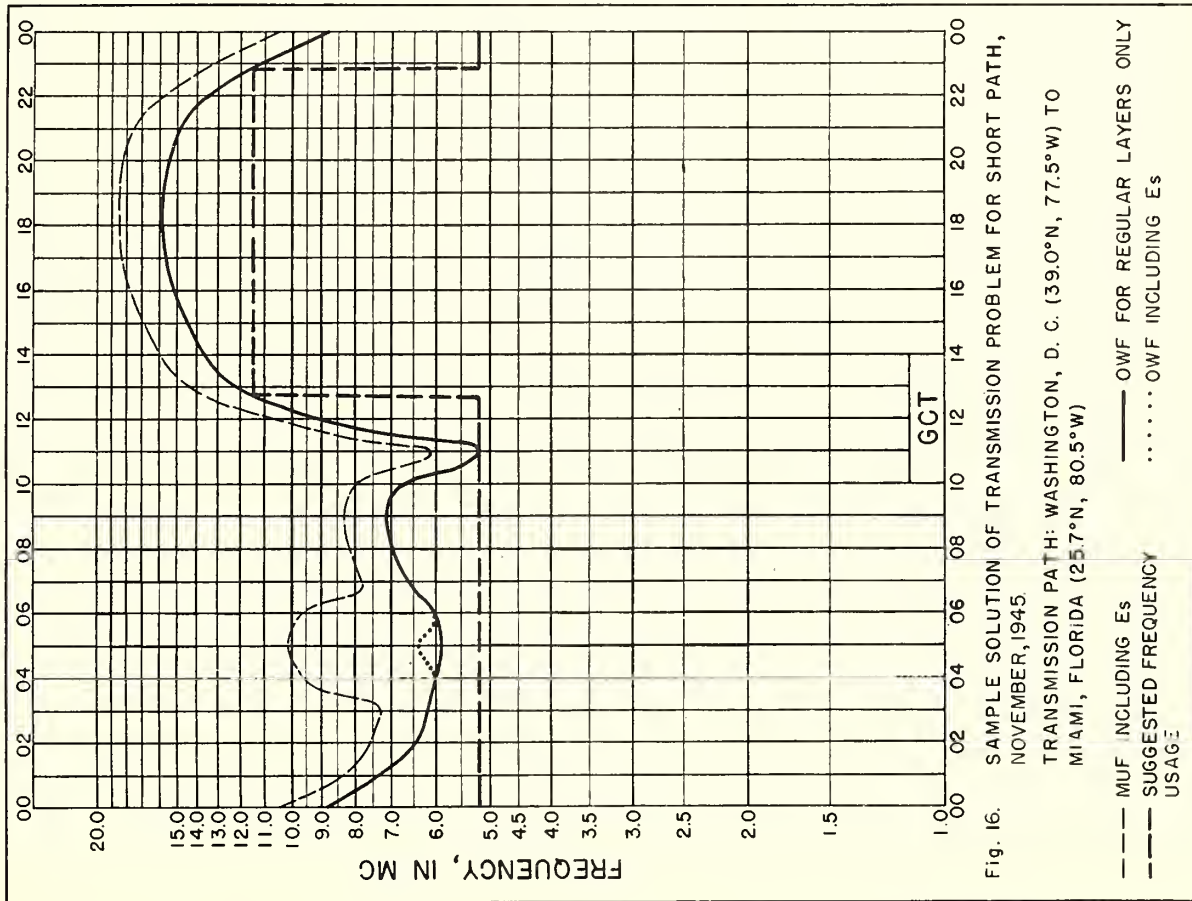


Fig. 15. PERCENTAGE OF TIME OCCURRENCE FOR E_s IN EXCESS OF 15 Mc, PREDICTED FOR NOVEMBER, 1945.





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