

# The Raised Cosine Pulse

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# Physical Realization

- The Nyquist channel  $P_{opt}(f)$ : ideal
- the modified  $P(f)$  decreases toward zero gradually rather than abruptly (a rectangle function)
- two parts
- Flat portion  $0 \leq |f| \leq f_1$
- Roll-off portion  $f_1 \leq |f| \leq 2B_0 - f_1$

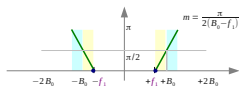
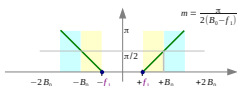
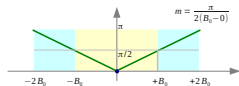
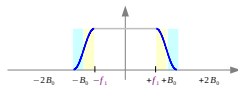
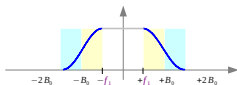
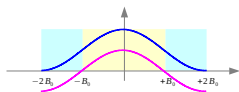
# Flat and Roll-off Portions

- one full cycle of the cosine function
- defined in the frequency domain
- raised up by an amount equal to its amplitude

- $P(f) = \frac{\sqrt{E}}{2B_0}$   $(0 \leq |f| \leq f_1)$

- $P(f) = \frac{\sqrt{E}}{4B_0} \left\{ 1 + \cos \left[ \frac{\pi(|f| - f_1)}{2(B_0 - f_1)} \right] \right\}$   $(f_1 \leq |f| \leq 2B_0 - f_1)$

- $P(f) = 0$   $(2B_0 - f_1 \leq |f|)$



# Raised Cosine Pulse Spectrum

- $P(f) = \frac{\sqrt{E}}{2B_0}$   $(0 \leq |f| \leq f_1)$
- $P(f) = \frac{\sqrt{E}}{4B_0} \left\{ 1 + \cos \left[ \frac{\pi(|f| - f_1)}{2(B_0 - f_1)} \right] \right\}$   $(f_1 \leq |f| \leq 2B_0 - f_1)$
- $P(f) = 0$   $(2B_0 - f_1 \leq |f|)$

- slope  $m = \frac{\pi}{2(B_0 - f_1)}$
- x intercept point  $(f_1, 0) \quad x \implies (x - f_1)$
- argument equation  $\theta = \frac{\pi(f - f_1)}{2(B_0 - f_1)}$
- raised cosine  $\frac{1}{2} \left\{ 1 + \cos \left[ \frac{\pi(|f| - f_1)}{2(B_0 - f_1)} \right] \right\}$

## Roll-off Factor $\alpha$

- $P(f) = \frac{\sqrt{E}}{2B_0}$   $(0 \leq |f| \leq f_1)$
- $P(f) = \frac{\sqrt{E}}{4B_0} \left\{ 1 + \cos \left[ \frac{\pi(|f| - f_1)}{2(B_0 - f_1)} \right] \right\}$   $(f_1 \leq |f| \leq 2B_0 - f_1)$
- $P(f) = 0$   $(2B_0 - f_1 \leq |f|)$

• roll-off factor  $\alpha = \frac{(B_0 - f_1)}{B_0} = 1 - \frac{f_1}{B_0}$

• normalized by  $\frac{2B_0}{\sqrt{E}}$

• normalized frequency  $\frac{f}{B_0}$

$$p(t) = \sqrt{E} \operatorname{sinc}(2B_0 t) \left( \frac{\cos(2\pi\alpha B_0 t)}{1 - 16\alpha^2 B_0^2 t^2} \right)$$

# Raised Cosine Pulse Spectrum & Shape

## Raised Cosine Pulse Spectrum

- $P(f) = \frac{\sqrt{E}}{2B_0}$   $(0 \leq |f| \leq f_1)$
- $P(f) = \frac{\sqrt{E}}{4B_0} \left\{ 1 + \cos \left[ \frac{\pi(|f| - f_1)}{2(B_0 - f_1)} \right] \right\}$   $(f_1 \leq |f| \leq 2B_0 - f_1)$
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## Raised Cosine Pulse Shape

- $p(t) = \sqrt{E} \operatorname{sinc}(2B_0 t) \left( \frac{\cos(2\pi\alpha B_0 t)}{1 - 16\alpha^2 B_0^2 t^2} \right)$

# Raised Cosine Pulse Shape

- $p(t) = \sqrt{E} \operatorname{sinc}(2B_0 t) \left( \frac{\cos(2\pi\alpha B_0 t)}{1 - 16\alpha^2 B_0^2 t^2} \right)$
- $\sqrt{E} \operatorname{sinc}(2B_0 t)$  Nyquist channel
  - ▶ makes zero crossings at the sampling instants  $t = iT_b$
- $\left( \frac{\cos(2\pi\alpha B_0 t)}{1 - 16\alpha^2 B_0^2 t^2} \right)$  decreases as  $\frac{1}{|t|^2}$  for large  $|t|$ 
  - ▶ reduces the tails of the pulse significantly low
  - ▶ makes the transmitted signal insensitive to sampling time errors
  - ▶ the ISI error due to a timing error  $\Delta t$  decreases as  $\alpha \rightarrow 1$



## Raised Cosine Pulse Shape ( $\alpha \rightarrow 1$ )

- $p(t) = \sqrt{E} \operatorname{sinc}(2B_0 t) \left( \frac{\cos(2\pi\alpha B_0 t)}{1 - 16\alpha^2 B_0^2 t^2} \right)$
- the ISI error due to a timing error  $\Delta t$  decreases as  $\alpha \rightarrow 1$

- $$p(t) = \sqrt{E} \left( \frac{\sin(2\pi B_0 t)}{2\pi B_0 t} \right) \left( \frac{\cos(2\pi B_0 t)}{1 - 16B_0^2 t^2} \right)$$
$$= \sqrt{E} \left( \frac{\sin(4\pi B_0 t)}{2 \cdot 2\pi B_0 t} \right) \left( \frac{1}{1 - 16B_0^2 t^2} \right) = \sqrt{E} \left( \frac{\operatorname{sinc}(4B_0 t)}{1 - 16B_0^2 t^2} \right)$$

## Zero Crossings of Raised Cosine Pulse Shape ( $\alpha \rightarrow 1$ )

- $p(t) = \sqrt{E} \text{sinc}(2B_0 t) \left( \frac{\cos(2\pi\alpha B_0 t)}{1-16\alpha^2 B_0^2 t^2} \right) \Rightarrow \sqrt{E} \left( \frac{\text{sinc}(4B_0 t)}{1-16B_0^2 t^2} \right)$

- zero crossings of  $\text{sinc}(4B_0 t)$  :  $t = k \frac{1}{4B_0} = k \frac{T_b}{2}$

- but, at  $t = \pm \frac{T_b}{2} = \pm \frac{1}{4B_0}$ ,

$$\Rightarrow 1 - 16B_0^2 t^2 = 0 \text{ denominator is also zero}$$

- $\frac{\sin(4\pi B_0 t)}{4\pi B_0 t(1-16B_0^2 t^2)}$  when  $t = \pm \frac{T_b}{2} = \pm \frac{1}{4B_0}$

$$\Rightarrow \frac{4\pi B_0 \cos(4\pi B_0 t)}{4\pi B_0 (1-16B_0^2 t^2)} = \frac{1}{2}$$

$$\Rightarrow p(t) = 0.5\sqrt{E}$$

- the same zero crossings:  $t = \pm \frac{2}{2} T_b, \pm \frac{4}{2} T_b, \pm \frac{6}{2} T_b, \dots$

- another zero crossings:  $t = \pm \frac{3}{2} T_b, \pm \frac{5}{2} T_b, \pm \frac{7}{2} T_b, \dots$

# Transmission Bandwidth

- Transmission Bandwidth  $B_T = 2B_0 - f_1$
- Roll-off factor  $\alpha = \frac{(B_0 - f_1)}{B_0} = 1 - \frac{f_1}{B_0}$
- $B_T = B_0 + B_0 - f_1 = B_0 + \alpha B_0 = (1 + \alpha)B_0$
- Excess Bandwidth  $f_v = \alpha B_0$
- Roll-off factor = Excess bandwidth factor

When  $\alpha \rightarrow 0$

- $f_v \rightarrow 0$
- $B_T \rightarrow B_0 = \frac{1}{2B_0}$  minimum bandwidth

When  $\alpha \rightarrow 1$

- $f_v \rightarrow B_0$
- $B_T \rightarrow 2B_0 = \frac{1}{B_0}$  doubled bandwidth
- used for synchronizing the receiver to the transmitter

# The Infinite Replicas of the Raised Cosine Pulse Spectrum

## The Infinite Replication

The infinite summation of replicas of the raised cosine pulse spectrum, spaced by  $2B_0$  Hz, equals a constant.

$$\sum_{m=-\infty}^{\infty} P(f - m2B_0) = \frac{\sqrt{E}}{2B_0}$$

$$\sum_{n=-\infty}^{\infty} p\left(\frac{n}{2B_0}\right)\delta\left(t - \frac{n}{2B_0}\right) \Leftrightarrow 2B_0 \sum_{m=-\infty}^{\infty} P(f - m2B_0)$$

$$p(t) = \sqrt{E} \operatorname{sinc}(2B_0 t) \left( \frac{\cos(2\pi\alpha B_0 t)}{1 - 16\alpha^2 B_0^2 t^2} \right)$$

$$p\left(\frac{n}{2B_0}\right) = \sqrt{E} \operatorname{sinc}\left(2B_0 \frac{n}{2B_0}\right) \left( \frac{\cos\left(2\pi\alpha B_0 \frac{n}{2B_0}\right)}{1 - 16\alpha^2 B_0^2 \left(\frac{n}{2B_0}\right)^2} \right) = \sqrt{E} \operatorname{sinc}(n) \left( \frac{\cos(\pi n\alpha)}{1 - 4n^2\alpha^2} \right)$$

$$\operatorname{sinc}(n) = \frac{\sin(n\pi)}{n\pi} \quad (= 1 \text{ when } n = 0, = 0 \text{ when } n = \pm 1, \pm 2, \dots)$$

$$\cos(\pi n\alpha) = 1 \text{ when } n = 0$$

# The Infinite Replicas of the Raised Cosine Pulse Spectrum

$$p\left(\frac{n}{2B_0}\right) = \sqrt{E} \operatorname{sinc}(n) \left( \frac{\cos(\pi n \alpha)}{1 - 4n^2 \alpha^2} \right)$$

$$\operatorname{sinc}(n) = \frac{\sin(n\pi)}{n\pi} \quad (= 1 \text{ when } n = 0, = 0 \text{ when } n = \pm 1, \pm 2, \dots)$$

$$\cos(\pi n \alpha) = 1 \text{ when } n = 0$$

$$p\left(\frac{n}{2B_0}\right) = \sqrt{E} \text{ when } n = 0$$
$$= 0 \text{ when } n \neq 0$$

$$\sqrt{E} \delta(t) \Leftrightarrow 2B_0 \sum_{m=-\infty}^{\infty} P(f - m2B_0)$$

$$\frac{\sqrt{E}}{2B_0} \delta(t) \Leftrightarrow \sum_{m=-\infty}^{\infty} P(f - m2B_0)$$

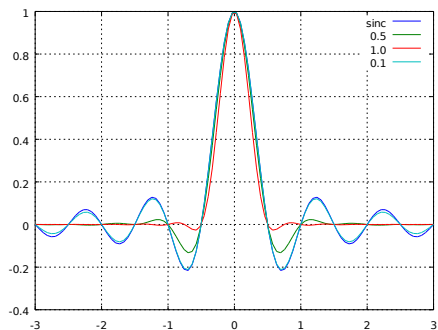
# The Criterion for Zero ISI

Given the modified pulse shape  $p(t)$  for transmitting data over an imperfect channel using discrete pulse-amplitude modulation at the data rate  $1/T$ , the pulse shape  $p(t)$  eliminates intersymbol interference if, and only if, its spectrum  $P(f)$  satisfies the condition

$$\sum_{m=-\infty}^{\infty} P(f - m/T) = \sum_{m=-\infty}^{\infty} P(f - m2B_0) = \text{const} \quad |f| \leq \frac{1}{2T}$$

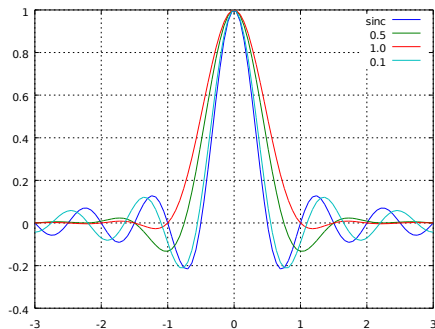
## Plots with the extended bandwidth

- $p(t) = \text{sinc}(2t) \left( \frac{\cos(2\pi\alpha t)}{1-16\alpha^2 t^2} \right)$



## Plots with the fixed bandwidth

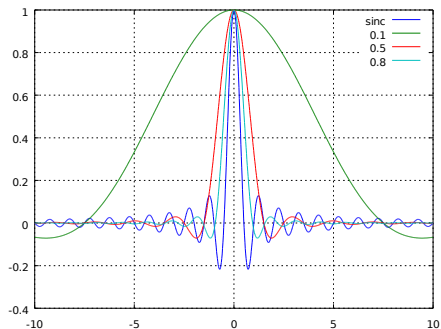
•  $p(t) = \text{sinc}(2t) \left( \frac{\cos(2\pi\alpha B_0 t)}{1 - 16\alpha^2 B_0^2 t^2} \right) \quad \alpha B_0 = 1$





## Plots with the cosine term

- $\rho(t) = \left( \frac{\cos(2\pi\alpha t)}{1-16\alpha^2 t^2} \right)$



# Reference

[1] S. Haykin, M Moher, “Introduction to Analog and Digital Communications”, 2ed